

## Investigation of Fugitive Emissions from Petrochemical Transport Barges Using Optical Remote Sensing

Final Report



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**Investigation of Fugitive Emissions from Petrochemical Transport  
Barges Using Optical Remote Sensing**

by

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## TABLE OF CONTENTS

<b>List of Appendices</b>	<b>ii</b>
<b>List of Tables</b>	<b>iii</b>
<b>List of Figures</b>	<b>iv</b>
<b>List of Acronyms</b>	<b>v</b>
<b>Executive Summary</b>	<b>vii</b>
<b>1. Introduction</b>	<b>1</b>
1.1 Background	1
1.2 Project Description	1
<b>2. Description of Test Sites, Measurement Methods and Site Deployment</b>	<b>4</b>
2.1 Aerial PGIE Observations	5
2.2 Ground-based PGIE Observations	7
2.3 Scanning OP-FTIRs and OTM 10 Protocol	7
2.3.1 OTM 10 and the Vertical Radial Plume Mapping Method	10
2.3.2 OTM 10 Fugitive Emission Quantification	14
2.3.3 Supporting Measurements for Ground-based ORS	14
2.3.3.1 Meteorological Data	14
2.3.3.2 OP-FTIR Instrument-Mirror Distance	15
2.3.4 PIC Emission Measurements with OP-FTIR Instrument	15
2.3.5 Meteorological Data Collection with the R.M. Young Heads	16
2.3.6 Optical Path Length Determination with the Topcon Theodolite	17
2.3.7 Calculating Emission Flux using the VRPM Method	17
2.3.8 Site Deployment Description at the Lock	18
2.4 Bagging Tests	18
<b>3. Aerial and Ground-based PGIE Results and Discussion</b>	<b>20</b>
3.1 Aerial PGIE Observations by LSI	20
3.2 On board Barge PGIE Observations by LSI	24
3.3 PGIE Observations From the Lock Wall	34
<b>4. OTM 10 AM Emission Flux and Trace Compound Speciation Results</b>	<b>42</b>
4.1 Data Graphs and Tables for Select Events	42
4.1.1 Summary of the Results of Analysis of Trace VOC Concentrations	54
4.2 Instances of Emissions Detected with the PGIE but not with ORS Measurements	54

4.3	Evaluation of AM Emissions from Tugs	55
<b>5.</b>	<b>Bagging Test Emission Estimate Results</b>	<b>57</b>
<b>6.</b>	<b>Comparison of OP-FTIR and Bagging Test Emission Flux Results</b>	<b>58</b>
<b>7.</b>	<b>Quality Assurance/Quality Control</b>	<b>61</b>
7.1	Instrument Calibration	61
7.2	Assessment of DQI Goals	61
7.2.1	DQI Check for Analyte PIC (OP-FTIR) Measurement	62
7.2.2	PGIE Relative Opacity DQI Assessment	63
7.2.3	Meteorological Head DQI Assessment	63
7.2.4	Topcon Theodolite DQI Assessment	64
7.2.5	QC Checks of OP-FTIR Instrument Performance	64
7.3	Estimate of Uncertainty in the OTM 10 Emission Flux Measurements	65
7.4	Uncertainty in the LDEQ Leak Bagging Estimates	67
7.5	General Data Limitations	68
7.6	Deviations from the QAPP	68
<b>8.</b>	<b>Summary</b>	<b>69</b>
<b>9.</b>	<b>References</b>	<b>72</b>

## List of Appendices

- A. LSI Report: Leak Detection using LSI Infrared Gas Imaging, BEM 1 Barge Study; Aerial Imaging (October 27, 2008)
- B. LSI Aerial PGIE Images
- C. LSI Report: Leak Detection using LSI Infrared Gas Imaging, BEM 1 Barge Study; Ground Crew Survey (October 21, 2008)
- D. LSI Ground Survey PGIE Images
- E. LDEQ/ARCADIS Lock Wall PGIE Images
- F. Alkane Mixture (AM) Measurement by OP-FTIR
- G. OTM 10 Data Graphs and Tables
- H. LDEQ Onboard Leak Bagging Test Report: Barge Emissions Measurement Project Final Report; SAGE Environmental Consulting (December 29, 2008)
- I. Comparison of Carbon Monoxide and Alkane Mixture Concentrations for 9 Barge Emissions Events to Investigate the Contribution of Emissions from Tugs
- J. Response to Comments from the American Waterways Operators



## List of Tables

Table 2-1.	Relative Response of Hydrocarbon with LSI Infrared Imaging Camera (FLIR)	6
Table 2-2.	Target Compound List	16
Table 3-1.	Summary Table of Barge Leaks Identified by LSI Aerial Survey	20
Table 3-2.	Summary Table of Barge Leaks Identified by LSI Ground-based Observations	25
Table 3-3.	Summary Table of Barge Leaks Identified by LSI Lock Wall Observations	35
Table 3-4.	Summary Table of Barge Leaks Identified by LDEQ/ARCADIS Lock Wall Observations	38
Table 4-1.	9/24/ 2008 – Event #1	43
Table 4-2.	AM Flux Values Measured during 9/24/ 2008, Event #1	43
Table 4-3.	9/29/ 2008 – Event #2	44
Table 4-4.	AM Flux Values Measured during 9/29/ 2008, Event #2	45
Table 4-5.	10/1/ 2008– Event #2	46
Table 4-6.	AM Flux Values Measured during 10/1/ 2008, Event #2	47
Table 4-7.	10/2/ 2008 – Event #2	48
Table 4-8.	AM Flux Values Measured during 10/2/ 2008, Event #2	49
Table 4-9.	10/5/ 2008 – Event #1	50
Table 4-10.	AM Flux Values Measured during 10/5/ 2008, Event #1	51
Table 4-11.	10/9/2008- Event #7	52
Table 4-12.	AM Flux Values Measured during 10/9/ 2008, Event #7	53
Table 4-13.	Summary of VOC Analysis	54
Table 4-14.	Summary of Leak Events Detected by the PGIE but not ORS Instrumentation	55
Table 5-1.	Summary of LDEQ Bagging Test Results	57
Table 6-1.	Summary of LDEQ Bagging Test Barge Totals and Most Significant OTM 10 Results	59
Table 7-1.	Instrumentation Calibration Frequency and Description	61
Table 7-2.	Data Quality Indicator Goals for the Project	62
Table 7-3.	Results of Flux Values Calculated by the VRPM Fit Explorer Program With a Fixed Peak Plume Concentration Location and Varying Values of the $\sigma_y$ Parameter	66
Table 7-4.	Results of Flux Values Calculated by the VRPM Fit Explorer Program with a Fixed $\sigma_y$ Parameter and Varying Peak Plume Concentration Locations	66

## List of Figures

Figure 2-1.	U.S. Army Corps of Engineers Lock Study Site and Measurement Configurations	9
Figure 2-2.	Images Illustrating OTM 10 Setup and Barges at the Port Allen Lock	10
Figure 2-3.	General OTM 10 VRPM Measurement Configuration	11
Figure 2-4.	Representation of Lock Cross Section and Wind Flow	13
Figure 2-5.	IMACC OP-FTIR Instrument and Scanner	15
Figure 2-6.	Images from LDEQ Leak Bagging Study	19
Figure 3-1.	Example #1 from LSI Helicopter Survey – Leak from Vent on Aft Side of Barge A27	22
Figure 3-2.	Example #2 from LSI Helicopter Survey – Leak from Vent Stack in Center of Barge A34	23
Figure 3-3.	Example #3 from LSI Helicopter Survey – Leak from Top Hatches on Bow of Barge A31	23
Figure 3-4.	Example from LSI Ground Survey – Sampling During Bagging Test	28
Figure 3-5.	Leak from Cargo Hatch on Barge G2- Mass Leak 1.86 g/s	28
Figure 3-6.	Leak from Ullage Hatch on Barge G4- Mass Leak 0.31 g/s	29
Figure 3-7.	Leak from Ullage Hatch on Barge G4- Mass Leak 0.19 g/s	29
Figure 3-8.	Leak from Ullage Hatch on Barge G4- Mass Leak 0.24 g/s	30
Figure 3-9.	Leak from Ullage Hatch on Barge G5- Mass Leak 0.73 g/s	30
Figure 3-10.	Leak from Ullage Hatch on Barge G5- Mass Leak 1.43 g/s	31
Figure 3-11.	Leak from Vent on Barge G6- Mass Leak 1.45 g/s	31
Figure 3-12.	Leak from Cofferdam Hatch on Barge G6- Mass Leak 1.99 g/s	32
Figure 3-13.	Leak from Cargo Hatch on Barge G7- Mass Leak 3.12 g/s	32
Figure 3-14.	Leak from Pressure Relief Valve on Barge G8- Mass Leak 5.78 g/s	33
Figure 3-15.	Example #1 from LSI Ground Survey – Leaking Hatch on Barge L1- Total Mass Emission from Barge 0.521 g/s	36
Figure 3-16.	Example #2 from LSI Ground Survey – Leaking Valve on Barge L2- Total Mass Emission from Barge 0.521 g/s	37
Figure 3-17.	Example #3 from LSI Ground Survey – Leaking Hatch on Barge L6- Total Mass Emission from Barge 0.415 g/s	37
Figure 3-18.	Example #1 from Ground Survey with LDEQ Camera – Leaking Hatch from Barge L10 (there was no OTM 10 emission flux measurement for this time period)	39
Figure 3-19.	Example #2 from Ground Survey with LDEQ Camera – Leaking Vent from Barge L23- Total OTM 10 Mass Emission from Barge 0.490 g/s	40

Figure 3-20. Example #3 from Ground Survey with LDEQ Camera – Leaking Valve from Barge L13- Total OTM 10 Mass Emission from Barge 0.106 g/s	40
Figure 4-1. Screenshot from FLIR Camera Showing Leak from 9/24/ 2008, Event #1	44
Figure 4-2. Screenshot from FLIR Camera Showing Leak from 9/29/ 2008, Event #2	46
Figure 4-3. Screenshot from FLIR Camera Showing Leak from 10/1/ 2008, Event #2	48
Figure 4-4. Screenshot from FLIR Camera Showing Leak from 10/2/ 2008, Event #3	50
Figure 4-5. Screenshot from FLIR Camera Showing Leak from 10/5/ 2008, Event #1	52
Figure 4-6. Screenshot from FLIR Camera Showing Leak from 10/9/ 2008, Event #7	53

### List of Acronyms

AM	Alkane Mixture
BEM	Barge Emission Measurement
DQI	Data Quality Indicators
ECPB	Emissions Characterization and Prevention Branch
EPA	U.S. Environmental Protection Agency
FAA	Federal Aviation Administration
HLDS	Hawk Leak Detection System
LDEQ	Louisiana Department of Environmental Quality
LSI	Leak Surveys Inc.
MDL	Minimum Detection Limit
MOP	Miscellaneous Operating Procedures
MSCHD	Memphis and Shelby County Tennessee Health Department
NEdT	Noise Equivalent Delta Temperature
NERL	National Exposure Research Laboratory
NRML	National Risk Management Research Laboratory
OAQPS	Office of Air Quality Planning and Standards
OP-FTIR	Open-Path Fourier Transform Infrared
ORD	Office of Research and Development
ORS	Optical Remote Sensing
OTM 10	EPA ORS Test Method OTM 10
PAC	Path Averaged Concentration
PAMS	Photochemical Assessment Monitoring Station
PGIE	Passive Gas Imaging Equipment

PIC	Path Integrated Concentration
QA	Quality Assurance
QAPP	Quality Assurance Project Plan
QC	Quality Control
R4	EPA Region 4
R6	EPA Region 6
RSD	Relative Standard Deviation
SOP	Standard Operating Procedures
SSE	Sum of Squared Errors
TCEQ	Texas Commission on Environmental Quality
AM	Total Hydrocarbon
TNMHC	Total Non-methane Hydrocarbons
UV-DOAS	Ultraviolet Differential Optical Absorption Spectroscopy
VOC	Volatile Organic Compound
VRPM	Vertical Radial Plume Mapping
WAM	Work Assignment Manager
WC	Wind Criteria
WSC	Wind Speed Criteria

## Executive Summary

Recent airborne remote sensing survey data acquired with passive gas imaging equipment (PGIE), also known as infrared cameras, have shown potentially significant fugitive volatile organic carbon (VOC) emissions from petrochemical transport barges. A collaborative group with members from the United States Environmental Protection Agency Region 6 (EPA R6), the EPA Office of Research and Development (ORD) National Risk Management Research Laboratory (NRMRL) and National Exposure Research Laboratory (NERL), the Louisiana Department of Environmental Quality (LDEQ) and the Texas Commission on Environmental Quality (TCEQ) was formed to further investigate this topic. The common goals of the collaboration centered on improving knowledge of fugitive emissions from this source category and advancing field application information for select remote sensing techniques useful for identification and assessment of fugitive emissions from difficult to monitor sources such as barges.

To meet these goals the group conducted a field campaign in Baton Rouge, Louisiana from September 24 through October 9, 2008. This field campaign is described in this report and involved several complementary remote sensing and onboard leak rate measurement efforts. The study included aerial PGIE surveys of barges located on the Mississippi River and inter-coastal Waterway to identify barges with significant fugitive emissions. Additional ground-based PGIE observations of barges from the Port Allen Lock wall and also onboard a number of barges were conducted to closely observe fugitive leaks and identify leaking components. To support this work, an LDEQ study quantified emission leak rates using a bagging technique from a total of eight barges that were identified by the aerial remote sensing PGIE survey. To complement these efforts, EPA method OTM 10 with open-path Fourier transform infrared spectroscopy was used at the Port Allen lock to produce hydrocarbon emission measurements from barge traffic traveling through the lock.

The aerial PGIE survey detected leaks from 45 different barges located in the Mississippi River and the Intracoastal Waterway over a five day period. The ground-based PGIE monitoring detected leaks from over 18 different barges in the Port Allen lock during the study. The remote sensing surveys provided significant information regarding the practical use of infrared cameras for detection of emissions from petrochemical transport barges. This study produced a PGIE image database that informs the use of this technology by providing a basis for comparison of the qualitative PGIE leak images with estimated leak rates. This comparison helps improve PGIE survey technique understanding for barge emissions and other source categories.

In general, the employed PGIE equipment was found to be robust, easy to use, and possessed sufficient detection sensitivity for this application. The PGIE remote sensing approach was judged to be extremely useful for both aerial survey and close range fugitive leak inspection of petrochemical transport barges. The PGIE technique was able to identify a large range of leaks with large leaks detectable from the air and smaller leaks more easily observed at close range. PGIE observations were easier to execute during mid-day to late afternoon time periods due to more favorable background imaging conditions (improved background radiance from hot barge surfaces and lower shadow interference) and because fugitive emissions were likely more pronounced as the barges became heated by solar radiation and ambient temperature during the day. PGIE observations were very useful for identification of specific leaking components and verification of subsequent leak repair activities.

Based on aerial observations, eight barges with observed large leaks were selected for onboard leak emission rate measurements as part of the LDEQ bagging survey. For this effort, a total of 23 leak points from eight barges were bagged to estimate mass emission rates. The measured total non-methane hydrocarbon emissions flux values from individual leaks during the bagging study ranged from 0.07 g/s to 5.77 g/s. Summing all measured leaks for each individual barge yielded a barge total leak rate ranging from 1.13 g/s to 6.24 g/s. The average value of total leak rate measurement for eight barges was 3.3 g/s.

EPA method OTM 10 monitoring was conducted at the Port Allen lock wall from September 24 through October 9. A total of 97 barge sets passed through the lock during the observation period. Six barge events showed significant fugitive hydrocarbon emissions as measured by OTM 10 with values ranging from 0.047 g/s to 3.39 g/s alkane mixture (AM) flux rate with an average value of 0.83 g/s. The instrumentation used to apply the OTM 10 method exhibited sufficient operational robustness and detection sensitivity during the current study. Additionally, the OTM 10 technique was able to identify and assess emission rates from a range of leak sizes as long as the prevailing wind brought the emitted plume through the vertical plane of the measurement configuration.

Due to project constraints, there was no opportunity to conduct simultaneous emission measurements by OTM 10 and the bagging technique on the same barge. A baseline comparison of measurement results on different barges shows that the average total barge emission estimate by OTM 10 (0.83 g/s) was lower than the similar average from the bagging study (3.3 g/s). The maximum total barge emission estimates from the two techniques were more comparable (3.39 g/s with OTM 10 and 6.24 g/s with the bagging method). The somewhat lower OTM 10 values may be partially explained by the fact that the barges selected for the bagging experiments were identified by airborne survey as

having very significant leaks and may not represent an average emission case whereas the OTM 10 measurements were conducted on barges moving through the lock with no selection process and therefore may represent a more typical sample cross section.

Note that the emission estimates presented in this report represent a snapshot in time. Fugitive emissions from petrochemical barges are believed to vary significantly due to ambient temperature, thermal load, product mix, load state, and equipment condition and equipment design. Since there is limited information on how these variables affect fugitive emissions, extrapolation of data contained in this report is not recommended.

## **1. Introduction**

### **1.1 Background**

Recent airborne survey data using passive gas imaging equipment (PGIE), also known as infrared cameras, have shown potentially significant fugitive volatile organic compound (VOC) emissions from petrochemical transport barges. This is of interest as VOCs are precursors to ground-level ozone formation, contributing to the degradation of air quality, especially in urban areas. A collaboration of interested parties was formed to further investigate this issue. This group has common interests to expand knowledge of this source category and to further develop Optical Remote Sensing (ORS) techniques which facilitate fugitive emission identification and measurements from these and related sources.

The collaborative group consists of two main sub-groups which will individually sponsor and execute two separate Barge Emission Measurement (BEM) studies. Subgroup 1 consists of the United States Environmental Protection Agency Region 6 (EPA R6), the EPA Office of Research and Development (ORD) National Risk Management Research Laboratory (NRMRL) and National Exposure Research Laboratory (NERL), the Louisiana Department of Environmental Quality (LDEQ) and the Texas Commission on Environmental Quality (TCEQ). Subgroup 1 financially sponsored and executed BEM1 which occurred in Baton Rouge, Louisiana in September 24 through October 9, 2008 and is the subject of this report.

Subgroup 2 consists of EPA Region 4 (EPA R4) and the Memphis and Shelby County Tennessee Health Department (MSCHD) which was awarded an EPA Communities-Scale Monitoring Grant to plan and execute BEM2 in the fall of 2009. Each BEM project will benefit through active involvement of the above mentioned subgroups in addition to consultation from the EPA Office of Air Quality Planning and Standards (OAQPS), the BLF Consulting Group, and interested industry groups. The results of the studies will likely be compared in a separate publication.

### **1.2 Project Description**

This report describes the BEM 1 field campaign conducted in Baton Rouge, Louisiana from September 24 to October 9, 2008. BEM 1 investigated VOC emissions from petro-chemical transport barges using portable gas imaging equipment PGIE (infrared cameras), EPA Method OTM 10 with Open-path Fourier transform infrared (OP-FTIR) spectrometers, in addition to leak bagging tests (manual leak rate measurements).



The objectives of the study were:

- To improve knowledge of fugitive VOC emissions from petrochemical transport barges.
- To demonstrate and advance the field application of select ORS techniques (EPA OTM 10 OP-FTIR and PGIE) for identification and quantification of fugitive emissions from difficult to monitor sources.
- Identify sources of fugitive leaks from multiple barges

To accomplish these goals, the project team conducted several complementary efforts:

1. Aerial PGIE surveys of barges located on the Mississippi River and inter-coastal water ways identified barges with significant fugitive emissions.
2. Ground-based PGIE observations of barges from the Port Allen Lock wall and also onboard several barges identified and closely observe fugitive leaks.
3. Onboard leak emission bagging measurements were conducted by LDEQ on several barges to quantify leak rates and allow comparison with PGIE images.
4. EPA Method OTM 10 with open-path Fourier transform infrared spectroscopy was used at the Port Allen lock to produce hydrocarbon emission measurements from barge traffic traveling through the lock.

The body of this report summarizes the main aspects of the BEM 1 study with collections of representative images and emission measurement details contained in the Appendices A through I. With the exceptions noted below, this project was conducted by ARCADIS U.S., Inc. (ARCADIS), Durham, NC, under EPA ORD contract No. EP-C-04-023, Work Assignment No. 4-47. ARCADIS executed the OTM 10 portion of the field campaign, analyzed the OP-FTIR and OTM 10 data, produced draft versions of data tables and image collections and contributed to descriptions continued in this report. EPA Personnel were primary authors on the main body and summary sections of the report.

Section 2 of this report describes the measurement methods, instruments, and field setup for the BEM1 campaign.

Section 3 of the report describes the aerial and ground-based PGIE observations of barges on the Mississippi River and Intracoastal Waterway and Port Allen Lock. This portion of the

study was funded by EPA and was executed by Leak Surveys, Inc. (LSI), under subcontract to ARCADIS and by ARCADIS using PGIE owned by LDEQ. A summary of LSI results along with several representative PGIE screenshots are presented in Sections 3.1 (aerial) and 3.2 (ground-based). Section 3.3 presents this same information for the PGIE observations made on the lock wall by ARCADIS. Additional details and images from this part of the project are contained in Appendices A through E.

Section 4 of the report describes measurements made on the Port Allen Lock wall by ARCADIS using two scanning optical remote sensing instruments (OP-FTIR), in combination with the OTM 10 protocol (see <http://www.epa.gov/ttn/emc/prelim.html>). These measurements provided hydrocarbon emission estimates of a representative alkane mixture (AM) and speciated concentration measurements for several trace compounds for barges passing through the lock. Section 4 presents a description of notable events, the AM mass emission flux values measured during each event, a screenshot of the leaks from the PGIE observations, and the results of the trace compound analysis. Additional information on the OTM 10 portion of the study is contained in Appendices F and G.

Section 5 summarizes the findings of the onboard leak rate measurements performed by Sage Environmental for LDEQ on several barges during the study. The leak bagging measurements used U.S. EPA *Protocol for Equipment Leak Emission Estimates* (U.S. EPA, 1995), with some variations. The LDEQ report on the bagging experiments is reproduced in its entirety in Appendix H for reference. It is noted that a draft version of this BEM 1 study report was reviewed by the American Waterways Operators and their comments concerning the LDEQ bagging study along with responses from Sage Environmental Consulting are reproduced in Appendix J.

Section 6 of the report presents a general comparison of emissions levels from the set of barges passing through the Port Allen lock observed during the OTM 10 study with the barges measured during the LDEQ bagging study. Section 7 provides QA information including discussions on general uncertainty and data limitations. Section 8 summarizes the conclusions for the study.

This report has been reviewed by the Office of Research and Development, U.S. EPA, and approved for publication. Approval does not signify that the contents necessarily reflect the views and policies of the agency nor does mention of trade names or commercial products constitute endorsement or recommendation for use.

## 2. Description of Test Sites, Measurement Methods and Site Deployment

The experimental approach for BEM1 included three main elements: PGIE for aerial and ground-based observations, fugitive emission estimation by EPA Method OTM 10 at the Port Allen and leak bagging tests of emissions from several barges. Following a general description of PGIE, Sections 2.1 and 2.2 describe the details of the aerial and ground-based PGIE observations conducted for this study. Section 2.3 shows the U.S. Army Corps of Engineers Port Allen lock site and describes the EPA OTM 10 method used to assess the mass emission flux of a representative alkane mixture (AM) in addition to trace compound speciation. Section 2.4 describes the bagging procedure employed in the LDEQ effort to quantify fugitive emissions leaks onboard several barges.

Of special interest to this study is the use of PGIE remote sensing systems to investigate fugitive emissions from barges. The PGIE infrared cameras were used to qualitatively detect the presence of fugitive emissions and to observe the leaking component to inform emissions inventory knowledge. The details of the specific PGIE used in this study are provided in Section 2.1. In general, the infrared camera detects thermal energy emitted by objects in the optic field of view or scene as motion imagery or video. Thermal energy is absorbed by molecules in the camera's field of view. If the molecules are present in high concentrations, and if their infrared-active molecular vibrations are within the bandpass of the camera, the molecules are detected. The fugitive emission or leak is detected by the PGIE operator by observing the relative brightness of the camera pixels that comprise the scene. Gas leaks appear as black or very dark plumes in the video relative to other objects in the scene. These plumes are dynamic as well, which assists in discriminating gas leaks from other scene objects such as thermal shadows or cold objects. The camera video is recorded onto a solid state recorder for future analysis. More information on the PGIE camera can be found in the Texas Commission on Environmental Quality SOP #SAMP-020, *Operation of FLIR Systems THERMAGAS GasFindIR Camera*, presented as Appendix C of the project Quality Assurance Project Plan (QAPP) (EPA, 2008).

The study was conducted from September 24 through October 9, although measurements from each of the three study elements were not collected continuously during this time. The weather conditions observed during the study period were relatively normal conditions for the Port Allen area (normal average daytime high temperatures ranging from 86° F on September 24 to 82° F on October 9).

## 2.1 Aerial PGIE Observations

The aerial PGIE observations were made by Leak Surveys Inc. (LSI) from September 24 through October 1, 2008 (10 am to 5 pm). The crew used the Hawk Leak Detection System (HLDS), developed by LSI after 12 years of research and development on optical imaging.

The PGIE used was a modified Indigo (FLIR/Indigo Systems Corp., Goleta, CA) Merlin MID camera, which is a specialized thermal imaging camera that allows the operator to visualize a plume of VOC gases, allowing the leaking barge component to be identified. The PGIE was mounted on a helicopter using a FAA inspected and certified Tyler vibration isolating mount. The camera video was cabled to the operator inside the aircraft. The aircraft was generally deployed to conduct monitoring of barges upriver of the lock prior to actual arrival at the lock site. A standard digital camera was used for photographing the barge under surveillance for future reference. A GPS unit was used to log the location and time and date of the contact.

The PGIE has a nominal spectral range of 1 to 5.4  $\mu\text{m}$ . Using a  $30 \times 30 \mu\text{m}$  InSb detector with a  $320 \times 240$  pixel array, the camera has the capability to vary the integration times from 5 ms to 16.5 ms. The detector is operated at near liquid nitrogen temperatures using an integral Sterling cooler which provides the system with an NEdT of no more than 18 mK providing excellent sensitivity.

The spectral range is further limited with the use of a notch filter specifically designed for the detection of hydrocarbon infrared adsorption in the 3 micron region. The narrow bandpass range of the filter is less than the infrared spectral absorption of gas-phase hexane. The filter notch is positioned so that alkane gases have a significant response within the bandpass range.

Various lenses including a 25 mm, a 50 mm, and a 100 mm lens were used. The 25 mm lens provided a  $22 \times 16$  degrees field of view with an f-number of 2.3. The 50 mm lens provided an  $11 \times 8$  degrees field of view with an f-number of 2.3.

The use of a narrow bandpass filter provides spectral discrimination that allows the detection of compounds that have a vibration mode in the infrared region of the filter. Not all hydrocarbons have infrared absorptions within the filter range. Table 2-1 shows the theoretical relative response of various compounds of interest using  $1 \text{ cm}^{-1}$  resolution infrared spectra (Infrared Analysis, Inc., Anaheim, CA). Using propane as the reference spectrum with a relative response of 100, methane's response is approximately 10 percent of the same concentration of propane and hexane is 1.5 times the response of propane at

the same concentration. The filter is set to the infrared region of the spectrum that primarily corresponds to the infrared absorption of alkanes. Other hydrocarbons exhibit various degrees of absorption of infrared energy in this region as indicated in the table.

**Table 2-1. Relative Response of Hydrocarbon with LSI Infrared Imaging Camera (FLIR)**

<b>Compound</b>	<b>Relative Response Propane = 100%</b>
Methane	9
Ethane	43
Propane	100
Butane	118
Iso-Butane	137
Pentane	143
Hexane	155
Heptane	157
Octane	136
Ethylene	3
Propylene	20
Iso-Butylene	37
2-Methyl-2-Butane	4
1-Pentene	7
2-Methyl-2-Pentene	7
Benzene	4
Toluene	21
<i>o</i> -Xylene	38
<i>p</i> -Xylene	23
<i>m</i> -Xylene	32

The aerial surveys were performed using a two-person crew consisting of the pilot and the camera operator. The survey was conducted by focusing the PGIE on the river and searching for barge leaks. If a leak was found, the pilot circled back above the source and the camera operator recorded the leaking emissions for a period of approximately 2 minutes. The results of the aerial survey are presented in *Report: Leak Detection using LSI Infrared Gas Imaging, LDEQ Barge Study (27 October 2008)* which is included as Appendix A.

## 2.2 Ground-based PGIE Observations

The ground-based PGIE observations at the lock were made by LSI (September 24 and September 28-30, 2008) using a modified Indigo (FLIR/Indigo Systems Corp., Goleta, CA) GasfindIR MID camera and by ARCADIS using the LDEQ FLIR camera (September 28 and October 1-9, 2008). There were no FLIR observations made at the lock on September 25-27, 2008. LSI also made the observations at the onboard several barges during the LDEQ bagging study (September 24-28, 2008). The PGIE used to perform these optical imaging leak surveys was similar to the camera used for the aerial surveys described in Section 2.1.

The light weight and small size of the PGIE allowed it to be hand-carried for ground observations of barges. Leaking components on the barge (if present) were identified and logged. The potential source of the leak was identified (i.e., hatch cover, pressure relief valve) and the position on the barge (i.e., cargo tank #4) was determined.

The results of the LSI ground survey are presented in *Report: Leak Detection using LSI Infrared Gas Imaging, BEM1 Barge Study; Ground Crew Survey (21 October 2008)* which is included as Appendix C.

Images from the LSI and ARCADIS ground PGIE observations are presented in Appendices D and E.

## 2.3 Scanning OP-FTIRs and OTM 10 Protocol

Two scanning open path Fourier transform infrared (OP-FTIR) spectrometers, in combination with the OTM 10 protocol (see <http://www.epa.gov/ttn/emc/prelim.html>), were used to provide alkane mixture (AM) emission flux and speciated measurements for nine trace compounds (methane, methanol, benzene, ethylene, acetylene, propylene, propane, ethane, and carbon monoxide).

Supporting measurements for this phase of the study included meteorological data and distance measurements. Testing and measurement protocols included:

- PIC emission measurements with two OP-FTIR instruments
- Meteorological data collection with the R.M. Young heads
- Optical path length determination with a Topcon theodolite

- Calculation of AM emission flux using *Flux Calc* (ARCADIS software employing the VRPM method).

Figure 2-1 shows an overhead view of the U.S. Army Corps of Engineers Port Allen lock study site, with the approximate locations of the project measurement configurations. Two 3-beam OTM -10 configuration planes were deployed along the southern edge of the lock (denoted by the red lines, not to scale vertically) using one EPA and one ARCADIS scanning OP-FTIR. The end of the two planes was defined by one common scissor lift (tower in the middle), which was used to mount the two elevated mirrors of each OTM 10 configuration. The lowest mirror in each configuration was deployed on the surface of the lock wall walkway (0.1 m height) and the elevated mirrors were positioned at heights of approximately 3 m and 6 m above the walkway. The locations of the two scanning OP-FTIR instruments were near each end of the lock as indicated in the figure. The length of the EPA and ARCADIS OP-FTIR plane configurations were 169 m and 153 m, respectively. The overall length of the lock from gate to gate was approximately 360 m and the width of the lock was 25 m. The OTM 10 planes were located approximately 1 m away from the inside lock wall edge. Additional images illustrating the OTM 10 deployment and barge traffic in the lock are contained in Figures 2-2 and 2.4.

Two additional optical beam paths were deployed (one from each OP-FTIR instrument) across the surface of the lock to collect supplemental data on alkane mixture and trace VOC concentrations. Although the project Quality Assurance Project Plan stated that these data would be collected with ultraviolet differential optical absorption spectroscopy (UV-DOAS), the project team determined that the OP-FTIR data could be analyzed for trace VOC concentrations, so the UV-DOAS instrument was not deployed at the site due to limited project resources and eye safety concerns for lock personnel.

Originally, it was anticipated that the OTM 10 configuration would be deployed along the northern edge of the lock. However, at the time of the field campaign, the winds were largely from the north, and the configuration was deployed on the southern edge of the lock. The prevailing winds at the site during the measurements are denoted by the wind rose in the lower left hand corner of Figure 2-1. Note that in order for the OTM 10 configuration to measure fugitive emission from a particular barge, the wind vector must have a significant component from the north in order for the emitted plume to traverse the OTM 10 measurement plane.

OP-FTIR data were collected with each configuration from September 24 through October 9, 2008. Data from the barge traffic were recorded including the time of entry and exit from lock, reported cargo from the U.S. Army Corps of Engineers traffic log, and visual inspection of

cargo labels on each barge. Emissions flux values were calculated for each event by summing the flux values measured from each configuration.

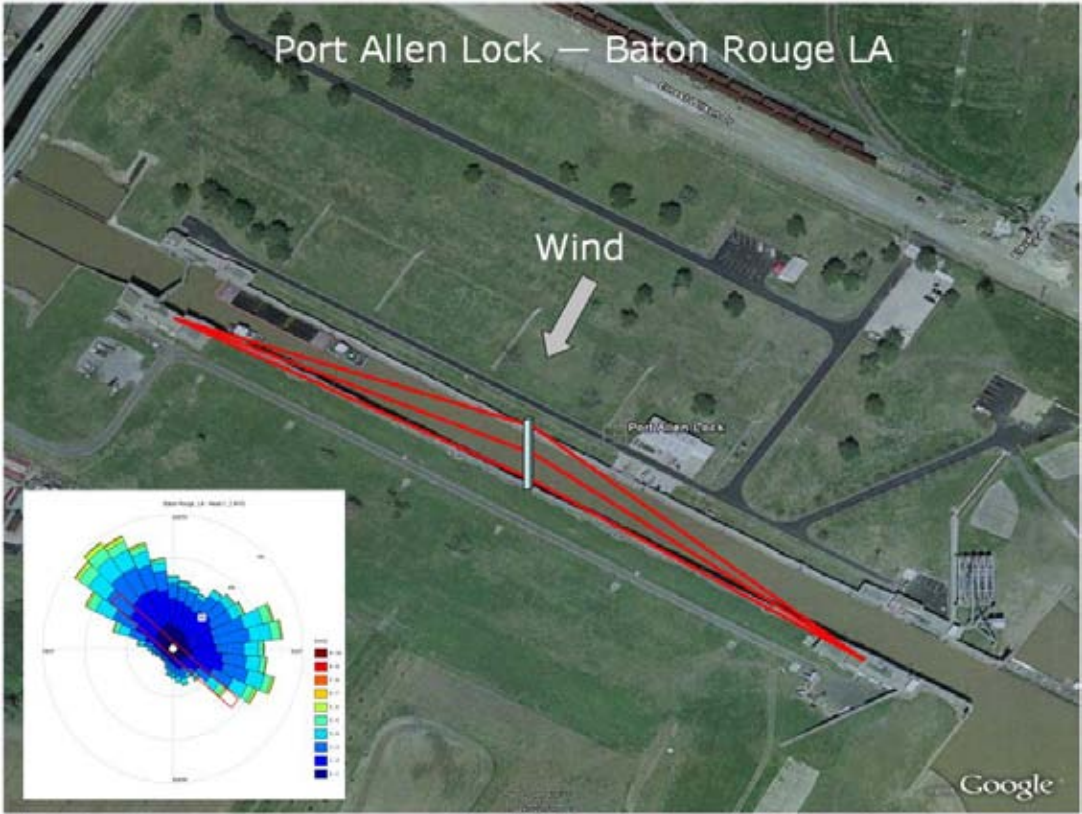


Figure 2-1. U.S. Army Corps of Engineers Lock Study Site and Measurement Configurations





**Figure 2-2. Images Illustrating OTM 10 Setup and Barges at the Port Allen Lock**

### 2.3.1 OTM 10 and the Vertical Radial Plume Mapping Method

The following is a general description of the ground-based barge measurements at the U.S. Army Corps of Engineers Port Allen lock. For this phase of the campaign, two OP-FTIR instruments were placed around the lock area to execute a modified version (3-beam) of EPA Method OTM 10 to quantify the mass emission flux of an alkane mixture (AM) from the barges located in the lock.

The project used two 3-beam OTM 10 flux measurement configurations to quantify the fugitive emissions from the barge. The Vertical Radial Plume Mapping (VRPM) method is the analytical part of the OTM 10 flux measurement and generally discussed in EPA OTM 10 *Optical remote sensing for emission characterization from non-point sources*, which describes direct measurement of pollutant mass emission flux from area sources using ground-based optical remote sensing (ORS). The OTM 10 technique utilizes open-path spectroscopic instrumentation to obtain path-integrated pollutant concentration information along multiple optical paths. The multi-path pollutant concentration data along with wind vector information are processed with a plane-integrating VRPM computer algorithm to yield

a mass emission flux for the source. Figure 2-3 shows a general 5-beam TOM 10 VRPM measurement configuration. For this project, a 3-beam configuration was used having no intermediate mirrors with 3 beams extending along the ground (mirror deployed on surface of top of the lock wall), middle, and top scissor lift positions.

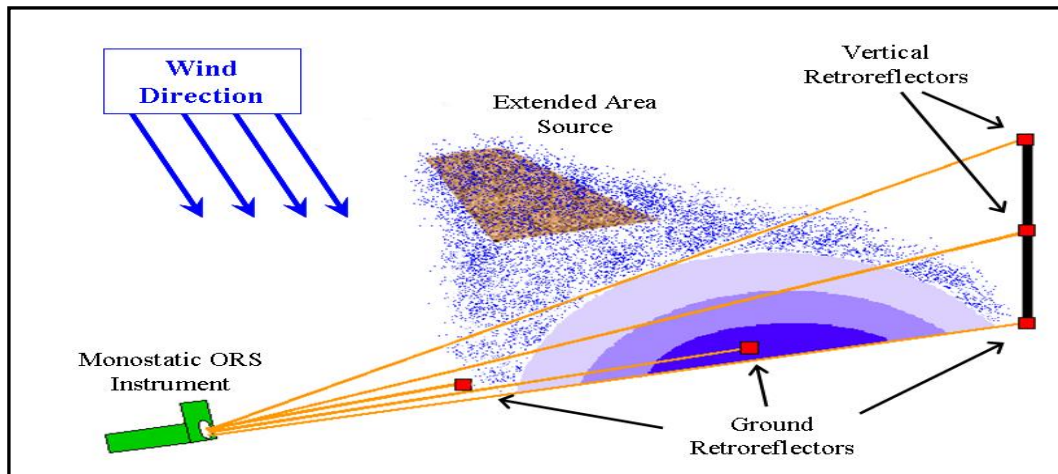


Figure 2-3. General OTM 10 VRPM Measurement Configuration

The VRPM computer algorithm uses a smooth basis function minimization routine of a bivariate Gaussian function to generate mass emission flux information from species concentration and wind data. For this measurement campaign, the VRPM configuration utilized a three-beam configuration which leads to a reduced form of the bivariate Gaussian in polar coordinates ( $r, \theta$ ). The standard deviation in the crosswind direction is assumed to be about four times the length of vertical plane ( $r_1$ ).

$$G(A, \sigma_z, m_z) = \frac{A}{2\pi(4r_1)\sigma_z} \exp \left\{ -\frac{1}{2} \left[ \frac{(r \cdot \cos \theta - \frac{1}{2}r_1)^2}{(4r_1)^2} + \frac{(r \cdot \sin \theta - m_z)^2}{\sigma_z^2} \right] \right\} \quad (1)$$

Where:

- $A$  = normalizing coefficient, adjusts for the peak value of the bivariate surface;  
 $m_z$  = peak location in Cartesian coordinates;  
 $\sigma_z$  = vertical standard deviation in Cartesian coordinates;  
 $r_1$  = length of VRPM plane;

$A$ ,  $m_z$ , and  $\sigma_z$  are the unknown parameters to be retrieved by the fitting procedure. An error function (sum of squared errors, SSE) for minimization is defined as:

$$SSE(A, \sigma_z, m_z) = \sum_i \left( PAC_i - \int_0^{r_i} G(r_i, \theta_i, A, \sigma_{m_z}) dr / r_i \right)^2 \quad (2)$$

Where  $PAC_i$  is the measured path-averaged concentration (PAC) value for the  $i^{th}$  beam. The SSE function is minimized using the Simplex method to solve for the three unknown parameters. This process is for determining the vertical gradient in concentration. It allows an accurate integration of concentrations across the vertical plane as the long-beam ground level PAC provides a direct integration of concentration at the lowest level.

Once the parameters of the function are found for a specific run, the VRPM procedure calculates the concentration values for every square elementary unit in a vertical plane. Then, the VRPM procedure integrates the values, incorporating wind speed data at each height level to compute the flux. This enables the direct calculation of the flux in grams per second (g/s), using wind speed data in meters per second (m/s). Further information on the VRPM method for fugitive source emission measurements in general can be found in Thoma 2005, U.S. EPA 2007a with specific details of this deployment in U.S. EPA 2007b.

This measurement project has several unique features regarding the use of EPA Method OTM 10 which is typically used for ground-level area source measurements using a 5-beam approach. Specifically, this field study utilized a 3-beam approach and the source was not the typical ground level area source. The 3-beam OTM 10 approach was chosen for this project since it was much more important to obtain a larger number of measurement cycles while the mobile source was contained in the lock rather than a fewer number of cycles with a five beam approach since the horizontal spatial location of the plume was not of primary importance. In analyzing the PIC data using the 3-beam approach, several assumptions are required. The peak plume concentration was assumed to be centered along the crosswind axis of the OTM 10 configuration, and the  $\sigma_y$  parameter (horizontal dispersion coefficient) of

the measured plume was assumed to be equal to  $\frac{1}{2}$  the length of the OTM 10 configurations. It was necessary to make these assumptions because the 3-beam OTM 10 approach does not include two intermediate surface beam paths which are used to obtain information on the horizontal location and dispersion of the plume. Section 7.3 has contains a discussion of uncertainty associated with these assumptions.

The lock wall configuration was not a typical area source deployment however it was assumed that the emission form the barges acted similarly to a close-coupled area source. The emitted plumes from the barges were assumed to be initially small in spatial extent but would experience significant dispersion by eddy mixing before exiting the lock and passing through the OTM 10 plane. This is likely since the barges were significantly below the lock wall top (approximately 7m to 12 m) and the emitted plumes could experience several dispersive/mixing mechanisms (such as stagnation, turbulence, channeling) depending on ambient wind direction and speed so the plumes could evolve more than in a flat wind swept scenario with similar downwind standoff. This results in a relatively well-developed plume exiting the lock and being transported by the free-flowing winds to the OTM 10 plane. This is illustrated in Figure 2.4 and these assumptions are further discussed in Section 7.3. The distance range below the lock wall ( $\approx 7$  m to 12 m) reflects the approximate lock operation water level height change during the study.

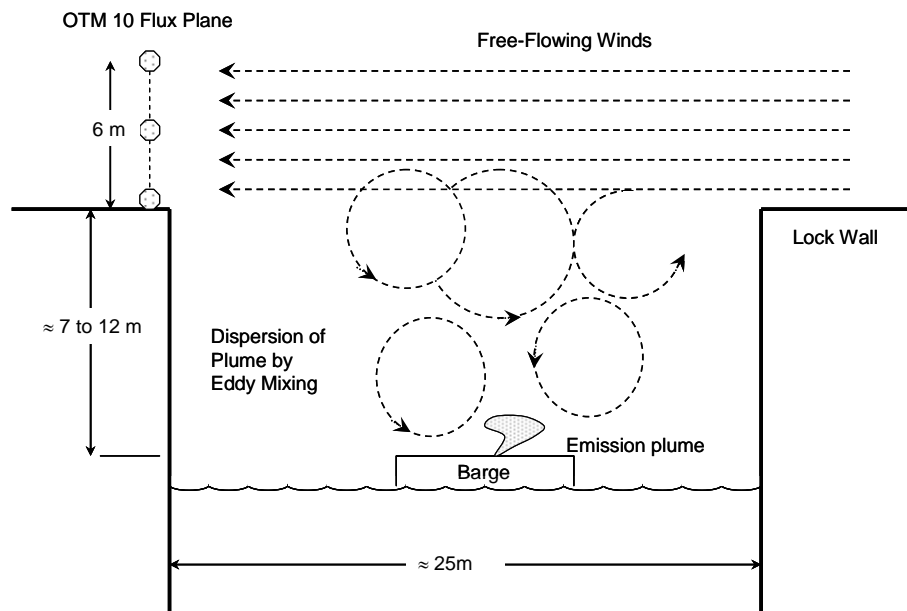


Figure 2-4. Representation of Lock Cross Section and Wind Flow

### 2.3.2 OTM 10 Fugitive Emission Quantification

The scanning OP-FTIR measurement system and associated OTM 10 planes employed a default configuration as described above. The default dwell time for each mirror was 30 seconds. In general, the OP-FTIR spectrometer is designed for both fence-line monitoring applications and real-time, on-site, remediation monitoring and source characterization. The OP-FTIR instrument consists of an infrared light beam, modulated by a Michelson interferometer. The infrared beam is transmitted from a single telescope to a retro-reflecting mirror target, which is usually set up at a range of 100 to 500 m. The returned light signal is received by the single telescope and directed to a detector. The light is absorbed by the molecules in the beam path as the light propagates to the retro-reflecting mirror and again as the light is reflected back to the analyzer. The advantage of OP-FTIR monitoring is that the concentrations of a multitude of infrared absorbing gaseous chemicals can be detected and measured simultaneously, with high temporal resolution. Figure 2-5 presents a picture of the OP-FTIR instrument.

### 2.3.3 Supporting Measurements for Ground-based ORS

#### 2.3.3.1 Meteorological Data

Meteorological data including wind direction and wind speed were continuously collected during the measurement campaign with two R.M. Young model 05103 meteorological heads. The instrument is automated and collects real-time data from its sensors and records time-stamped data, which are transmitted to a desktop computer via a radio frequency modem R. M. Young model 32500. The meteorological heads were deployed to collect wind speed and wind direction data during the study. As part of each VRPM configuration, one head was deployed on the surface of the lock wall at a height of approximately 3 meters, and the other head was deployed on top of the scissor lift platform at a height of approximately 6 meters above the lock wall.

More information on deploying R.M. Young meteorological heads can be found in MOP 6803 "Guidance for Deploying and Using ORS Supplemental Instrumentation" of the Emissions Characterization and Prevention Branch (ECPB) *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004).



**Figure 2-5. IMACC OP-FTIR Instrument and Scanner**

#### 2.3.3.2 OP-FTIR Instrument-Mirror Distance

The physical distance between the ORS instruments and the mirrors was measured using a Topcon, Inc. model GTS-211D theodolite. More information on setting up and operating the theodolite can be found in MOP 6822 "Determining the Geographical Locations of the ORS Measurement Locations" of the *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004).

#### 2.3.4 PIC Emission Measurements with OP-FTIR Instrument

To calculate the mass emission flux using the OTM 10 method, the acquired OP-FTIR data must be analyzed to produce a PIC value. For this project, OP-FTIR data reduction focused on the PIC values of a representative alkane mixture (AM) by spectroscopic analysis of the infrared absorption features in the C-H stretch spectral region around  $2950\text{ cm}^{-1}$ . The analysis focused on an alkane mixture (butane, pentane, hexane, heptane, octane, nonane, decane) since performing spectral analysis of each individual compound is not possible due to the similarity in the shapes of the absorption bands. Additionally, the molecular weight of the target compound is necessary to calculate the mass emission flux using the OTM 10 method. Spectroscopic analysis of the AM also yielded the average molecular weight of AM for each concentration determination. More information on the method used for spectroscopic analysis of the AM can be found in Appendix F of this report.

In addition to the AM quantification, individually quantifiable hydrocarbons species (e.g., methane) were analyzed if present at concentrations above the MDL for the OP-FTIR.

The general measurement of the Path Integrated Concentration (PIC) of individually identifiable analyte gases using the IMACC OP-FTIR instrument is described in MOP 6808 “Multiple-Path Data Collection Using a Scanning IMACC Monostatic OP-FTIR” of the *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004). A detailed description of the procedure used for PIC concentration analysis with *IMACCQuant* software is contained in MOP 6827 “Procedures for OP-FTIR Concentration Data Analysis Using IMACCQuant Software”. The estimated minimum detection levels for the target analytes of the OP-FTIR instrument are presented in Table 2-2.

**Table 2-2. Target Compound List**

Compound	OP-FTIR Estimated Detection Limit for Optical Path Length = 300 m, 1 min. averaging (ppb)
Alkane Mixture (AM)	2
Methane	2
Methanol	4
Benzene	20
Ethylene	1
Acetylene	2
Propylene	4
Propane	10
Ethane	10

### 2.3.5 Meteorological Data Collection with the R.M. Young Heads

Meteorological data including wind direction and wind speed were continuously collected during the sampling/measurement campaign with an R.M. Young Model 05103 meteorological head. The instrument is automated and collects real-time data from its sensors and records time-stamped data, which are transmitted to a desktop computer via a transmitter.

For this project, a wind direction and speed-sensing head was used to collect data at heights of approximately two and six meters above ground. The sensing head for wind direction incorporates an auto-northing function (automatically adjusts to magnetic north) that

eliminates the errors associated with subjective field alignment to a compass heading. The sensing heads incorporate standard cup-type wind speed sensors. Post-collection, a linear interpolation between the two sets of data is done to estimate wind velocity as a function of height. More information on deploying and operating the R.M. Young Model 05103 meteorological instrumentation can be found in MOP 6803 of the *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004).

#### 2.3.6 Optical Path Length Determination with the Topcon Theodolite

The physical distance between an OP-FTIR instrument and a mirror was determined by measurement with a Topcon, Inc. model GTS-211D theodolite. The instrument manufacturer certifies the instrument accuracy and precision to better than 1 cm. Azimuth and elevation angles can also be determined using the theodolite. The measurement is a manual operation, with the results recorded by hand, and is followed by transcription to a spreadsheet for data archiving and calculations.

Due to folding of the optical beam by the mirror, the optical path length is twice the physical distance between the instrument and mirror. In other words, the optical beam passes through the physical path twice. More information on deploying and operating the Topcon theodolite can be found in MOP 6822 of the *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004).

#### 2.3.7 Calculating Emission Flux using the VRPM Method

The calculated emission flux is generated by inputting the measured PIC data into the VRPM algorithm. The algorithm is performed using Matlab software (MathWorks, Inc., Natick, MA). The VRPM method maps the concentrations in the plane of the measurement. The horizontal dimension of this plane is defined as the distance between the OP-FTIR instrument and the most distant mirror used in the configuration. The vertical dimension of this plane is defined as the distance from the surface to the point where the extrapolated concentration values (extrapolated based on the vertical concentration gradient) approaches zero. This height is not determined until the data are processed in the VRPM algorithm. By scanning in a vertical plane downwind from an area source, one can obtain plume concentration profiles and calculate the plane-integrated concentrations. The flux is calculated by multiplying the plane-integrated concentration by the wind speed component perpendicular to the vertical plane. The flux leads directly to a determination of the emission rate (Hashmonay et al., 1998; Hashmonay and Yost, 1999; Hashmonay et al., 2001; Thoma et al. 2005). More information on the procedures used to generate the plume maps and the calculated emission flux can be found in MOP 6842 "Using the vertical Radial Plume



Mapping (VRPM) Configuration with Wind Data to Create Plume Concentration Profiles and Calculate Emission Fluxes” of the *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004).

#### 2.3.8 Site Deployment Description at the Lock

The prevailing winds during the time of the field campaign were largely from the north, and the dual OP-FTIR configuration was deployed on the southern edge of the lock. Figure 2-1 shows the VRPM configurations at the U.S. Army Corps of Engineers lock. Following ORS instrument setup and Data Quality Indicator (DQI) checks, ORS data acquisition began, continuously, for a period of several hours each day. During the surveys, measurements were taken along each optical path length (mirror) sequentially. The averaging time for each optical path was thirty seconds. Emissions flux values were calculated for each event by summing the average flux values measured from each configuration.

Data from barge traffic were recorded including time of entry and exit from lock, reported cargo from the U.S. Army Corps of Engineers traffic log, and visual inspection of cargo labels on each barge. The ground-based PGIE (FLIR camera) measurements were conducted simultaneously with the ORS measurements for a period of several hours each day, for all but three days of the sampling campaign. It is noted that Barge traffic through the Port Allen lock was lighter than usual during the study due to repair activities on the Intracoastal Waterway Bayou Sorrel Bridge, which was damaged by a tug boat accident just prior to the start of the field campaign.

#### 2.4 Bagging Tests

The onboard-barge leak bagging tests were performed by SAGE Environmental Consulting for LDEQ from September 24-28, 2008. Some of the results from this study are presented in Sections 5 and 6 for comparison purposes with the full LDEQ report reproduced as Appendix H for reference. For the bagging measurements, SAGE followed the vacuum method described in the U.S. EPA Protocol for Equipment Leak Emission Estimates (U.S. EPA, 1995), with some variations. For compositional analysis, samples were collected by LDEQ in aluminum Summa canisters. A maximum of one canister was filled for each point tested. One canister was sometimes used for multiple sampling points in the same product service on the same barge. The LDEQ laboratory did the analysis using EPA PAMS analysis by GC/FID. Figure 2.6 shows images from the LDEQ leak bagging study.



Figure 2-6. Images from LDEQ Leak Bagging Study

### 3. Aerial and Ground-based PGIE Results and Discussion

The aerial and ground-based PGIE observations of barges on the Mississippi River and Intracoastal Waterway are summarized in this section. Representative PGIE snapshots are presented in Sections 3.1 (aerial) and 3.2 (ground-based). Section 3.3 presents this same information for the PGIE observations made in the lock on several other days by ARCADIS, with the LDEQ camera. No PGIE observations were made at the lock on September 25-27, 2008. Note that it is not possible to reproduce the details of a visible leak (as captured with video footage) using a single representative snap shot as required for this report.

#### 3.1 Aerial PGIE Observations by LSI

The aerial (helicopter) PGIE observations were made by Leak Surveys, Inc. (LSI) from September 24 through September 30, 2008. The helicopter was airborne for approximately 6 hours each day. The LSI aerial crew dataset contains movies showing leaks from a total of 45 different barges located in Mississippi River and Intracoastal Waterway. Table 3-1 lists the LSI snapshot identification number, barge number, and a description of the suspected source of the leak(s). Additional information is contained in Appendices A and B.

**Table 3-1. Summary Table of Barge Leaks Identified by LSI Aerial Survey**

Filename	Date	Part Leaking	Barge #
L000	9/24/2008	Two Large Valve Settings Towards Aft Side	A1
L001	9/24/2008	Vent Stack at Bow of Barge	A2
L002	9/24/2008	Vent Stack at Bow of Barge	A3
L003	9/24/2008	Top Loading Hatches	A4
L004	9/25/2008	Top Loading Hatches at Placid Refinery	A5
L005	9/25/2008	Top Loading Hatches to the Aft of Barge	A6
L006	9/25/2008	Top Loading Hatches at Bow of Barge	A7
L007	9/25/2008	Top Loading Hatches at Bow of Barge	A8
L008	9/25/2008	Top Loading Hatches at Bow of Barge	A9
L009	9/26/2008	Top Loading Hatch at Bow of Barge	A10
L010	9/26/2008	Top Loading Hatches and Vent	A11
L011	9/26/2008	Top Loading Hatches at Aft side of Barge at Placid Refinery	A12
L012	9/26/2008	Top Hatches on Barge	A13
L013	9/26/2008	Top Hatches on Barge	A14

<b>Filename</b>	<b>Date</b>	<b>Part Leaking</b>	<b>Barge #</b>
	9/26/2008	Top Hatches and Vent Stack on Barge	A15
L014	9/26/2008	Top Hatches and Vent Stack on Barge	A16
	9/26/2008	Top Hatches on Barge	A17
	9/26/2008	Top Hatches on Barge	A11
L015	9/27/2008	Vent Stack on Barge	A18
L016	9/27/2008	Repeat of Video 003, Boarded by Bagging Team	A4
L017	9/27/2008	Top Loading Hatches at Placid Refinery	A19
L018a	9/27/2008	Top Hatches on Barge	A20
L018b	9/27/2008	Top Hatches on Barge	A21
L018c	9/27/2008	Top Hatches on Barge	A22
L019	9/27/2008	Top Hatches at TT Barge Cleaning Facility --Refilm	A13
	9/27/2008	Top Hatches at TT Barge Cleaning Facility	A14
L020	9/27/2008	Vent Stack on Barge --Refilm	A23
	9/27/2008	Vent Stack on Barge	A24
L021	9/27/2008	Hatches at Aft Side --in Intracoastal Waterway	A25
	9/27/2008	Vent at Aft Side --in Intracoastal Waterway	A26
L022a	9/27/2008	Vent at Aft Side	A27
L022b	9/27/2008	Vent Stack on Bow of Barge	A28
L023a	9/27/2008	Center Vent on Barge	A29
L023b	9/27/2008	Cent Hatch on Barge	A30
L024	9/28/2008	Bow Hatch and Deck Hatch on Barge	A31
L025	9/28/2008	Two Aft Hatches and one Side Hatch	A32
L026	9/29/2008	Top Hatches on Barge --in Intracoastal Waterway	A33
L027	9/29/2008	Vent Stack in Center of Barge --in Intracoastal Waterway	A34
L028	9/29/2008	Vent Stack on Bow of Barge --Refilm	A1
L029	9/29/2008	Vent Stack on Bow of Barge	A35
L030	9/29/2008	Vent Stack on Bow of Barge --Refilm	A36
L031a	9/29/2008	Top Hatches on Barge --Across from Locks	A37
L031b	9/29/2008	Top Hatches on Bow --Across from Locks	A31
L032	9/30/2009	Vent at the Bow of Barge --North of Locks	A23
L033	9/30/2009	Forward Bow Hatch on Barge --in Intracoastal Waterway	A38

Figures 3-1 through 3-3 show three example snapshots from the LSI Aerial survey illustrating the type of leaks that were detected: Example #1 shows a vent on the aft side of Barge A27; Example #2 shows a vent stack in the center of Barge A34 from the Intracoastal Waterway; and Example #3 shows the top hatches on the bow of Barge A31 across from the lock. Appendix B contains a larger collection of images providing information on various types of leaks identified during the helicopter survey.

Note that it is impossible to represent visual acuity of observed leaks with single image snapshots reproduced in this report. The leaks as viewed in moving video images are much more pronounced and generally easier to identify, particularly for small leaks.



**Figure 3-1. Example #1 from LSI Helicopter Survey – Leak from Vent on Aft Side of Barge A27**



**Figure 3-2. Example #2 from LSI Helicopter Survey – Leak from Vent Stack in Center of Barge A34**



**Figure 3-3. Example #3 from LSI Helicopter Survey – Leak from Top Hatches on Bow of Barge A31**

The LSI aerial surveys provided the following general conclusions about this remote sensing approach for fugitive emission detection from petrochemical transport barges:

1. The deployed PGIE equipment and airborne platform exhibited sufficient mobility, operational robustness, and detection sensitivity and are judged to be extremely useful for airborne remote monitoring of this type. This conclusion agrees with previous similar studies using this technology.
2. The PGIE technique was able to easily identify apparent large leaks from the air with smaller leaks somewhat more difficult to identify likely requiring an expert operator.
3. Ground surveys indicated that the leaks seen from the air were many times composed of numerous individual leaks upon closer inspection.
4. In all studied cases, leaks identified from the air were verified as being VOC leaks of significant volume upon ground inspection.
5. Aerial observations were easier to execute during mid-day to late afternoon time periods due to more favorable background imaging conditions (improved background radiance from hot barge surfaces and lower shadow interference) and because fugitive emissions were likely more pronounced as the barges became heated by solar radiation and ambient temperature during the day.

### **3.2 On board Barge PGIE Observations by LSI**

LSI conducted ground-based PGIE observations on board eight barges in conjunction with the LDEQ bagging studies (September 24-28, 2008). The barges where monitoring occurred represented a subset of those identified by the aerial survey (Section 3.1) having large apparent leaks as viewed from the air. The purpose of the onboard PGIE observations was to provide close-up views of leaks prior to and during the bagging measurements. Table 3-2 lists the LSI filename number, the date of the observation, a description of the leak source, and the barge number or other descriptor.

**Table 3-2. Summary Table of Barge Leaks Identified by LSI Ground-based Observations**

<b>Filename</b>	<b>Date</b>	<b>Part Leaking</b>	<b>Barge # or Other Descriptor</b>
7	9/24/2008	Hatch	Barge G1
8	9/24/2008	Hatch	Barge G1
9	9/24/2008	Hatch	Barge G1
10	9/24/2008	Hatch	Barge G1
11	9/24/2008	Hatch	Barge G1
12	9/24/2008	Hatch	Barge G1
13	9/24/2008	Hatch	Barge G1
14	9/24/2008	Hatch	Barge G1
15	9/25/2008	Ullage Hatch	Barge G2 #2 Port Lower
16	9/25/2008	Cargo Hatch	Barge G2 #2 Port
17	9/25/2008	Butterworth Hatch	Barge G2 #2 Starboard Middle
18	9/25/2008	Butterworth Hatch	Barge G2 #2 Port Middle
19	9/25/2008	Butterworth Hatch	Barge G2 #1 Starboard Lower
20	9/25/2008	Alarm Test Rod	Barge G2 #2 Starboard
21	9/25/2008	Butterworth Hatch	Barge G2 #1 Port Lower
22	9/25/2008	Alarm Test Rod	Barge G2 #2 Port
23	9/25/2008	Cargo Hatch	Barge G2 #1 Starboard
24	9/25/2008	Butterworth Hatch	Barge G2 #1 Starboard Middle
25	9/25/2008	Butterworth Hatch	Barge G2 #1 Port Middle
26	9/25/2008	Butterworth Hatch	Barge G2 #1 Starboard Upper
27	9/25/2008	Butterworth Hatch	Barge G2 #1 Port Upper
28	9/25/2008	Butterworth Hatch	Barge G2 #2 Port Lower
29	9/25/2008	Overview of Leaks	Barge G2
30	9/25/2008	Bagging Process	Showing Gas Venting Through Dry Gas Meter
31	9/25/2008	Vent	Barge G3
32	9/25/2008	Pressure Relief Valve	Barge G3
33	9/25/2008	Butterworth Hatch	Barge G3 #1 Port Forward
34	9/25/2008	Ullage Hatch	Barge G3 #1
35	9/25/2008	Butterworth Hatch	Barge G3 #1 Port Aft
36	9/25/2005	Cargo Hatch Control Valve	Barge G3 #1
37	9/25/2008	Butterworth Hatch	Barge G3 Starboard Forward



September 2009

<b>Filename</b>	<b>Date</b>	<b>Part Leaking</b>	<b>Barge # or Other Descriptor</b>
38	9/25/2008	Butterworth Hatch	Barge G3 #2 Port Forward
39	9/25/2008	Cargo Hatch Control Valve	Barge G3 #2
40	9/25/2008	Butterworth Hatch	Barge G3 #3 Starboard Forward
41	9/25/2008	Butterworth Hatch	Barge G3 #3 Port Forward
42	9/25/2008	Butterworth Hatch	Barge G3 #3 Port Aft
43	9/25/2008	Cargo Hatch Control Valve	Barge G3 #3
44	9/26/2008	Ullage Hatch	Barge G4 #1 Port & #1 Starboard
45	9/26/2008	Both Hatches & Valve	Barge G4 #2 Port
46	9/26/2008	Both Hatches & Valve	Barge G4 #2 Starboard
47	9/26/2008	Ullage & Cargo Hatches	Barge G4 #3 Starboard
48	9/26/2008	Cargo Hatch Control Valve	Barge G4 #3 Port
49	9/26/2008	Alarm Test Rod	Barge G5 #1 Starboard
50	9/26/2008	Ullage Hatch	Barge G5 #1 Starboard
51	9/26/2008	Ullage Hatch & Valve	Barge G5 #1 Port
52	9/26/2008	Ullage Hatch	Barge G5 #2 Port
53	9/26/2008	Ullage & Cargo Hatches	Barge G5 #2 Starboard
54	9/26/2008	Ullage & Cargo Hatches	Barge G5 #3 Starboard
55	9/26/2008	Ullage Hatch	Barge G5 #3 Port
56	9/26/2008	Alarm Test Rod	Barge G5 #3 Starboard
57	9/26/2008	Same as Video 045	Barge G4 Filmed Again After Repair Attempt
58	9/26/2008	Same as Video 047	Barge G4 Filmed Again After Repair Attempt
59	9/27/2008	Vent	Barge G6
60	9/27/2008	Cofferdam Hatch	Barge G6 Forward
61	9/27/2008	Cargo Hatch	Barge G6 #3 Port
62	9/27/2008	Cargo Hatch	Barge G6 #3 Starboard
63	9/27/2008	Ullage Hatch	Barge G6 #4 Port
64	9/27/2008	Ullage Hatch	Barge G6 #4 Starboard
65	9/27/2008	Cargo Hatch	Barge G6 #4 Starboard
66	9/27/2008	Same as Video 063	Barge G6 Filmed Again
67	9/27/2008	Same as Video 063	Barge G6 Filmed Again After Vent Was Closed
68	9/27/2008	Same as Video 063	Barge G6 Filmed Again After Vent Was Closed
69	9/28/2008	Overview of Leaks	Barge G7 Overview of #2 & #3 Cargo Hatches

<b>Filename</b>	<b>Date</b>	<b>Part Leaking</b>	<b>Barge # or Other Descriptor</b>
87	9/28/2008	Pressure Relief Valve	Barge G8
88	9/28/2008	Cargo Hatch	Barge G8 #2 Port
89	9/28/2008	Cargo Hatch Control Valve	Barge G8 #2 Port
90	9/28/2008	Control Valve Grease Cert	Barge G8 #2 Starboard
91	9/28/2008	Hatch & Control Valve	Barge G8 #3 Starboard
92	9/28/2008	Hatch & Control Valve	Barge G8 #3 Port
93	9/28/2008	Overview of Leaks	Barge G8 Overview of Videos 87 thru 92
94	9/28/2008	Block Valve	Barge G8 #3
95	9/28/2008	Butterworth Hatch	Barge G8 #3 Port Rear
96	9/28/2008	Butterworth Hatch	Barge G8 #3 Starboard Rear
97	9/28/2008	Slop Tank Vent	Barge G8
98	9/28/2008	Master Suction Valve	Barge G8
99	9/28/2008	Butterworth Hatch	Barge G8 #2 Port Forward
100	9/28/2008	Cargo Hatch	Barge G8 #1 Port
101	9/28/2008	Cargo Hatch Control Valve	Barge G8 #1 Port
102	9/28/2008	Cargo Hatch Control Valve	Barge G8 #1 Starboard
103	9/28/2008	Slop Tank Hatch	Barge G8

Figures 3-4 through 3-14 show snapshots of LSI PGIE observations onboard several barges acquired in conjunction with the LDEQ bagging. The figure captions also show the emission rate estimates from the LDEQ bagging survey report (Appendix H) converted to g/s for comparison purposes.

Note that it is impossible to represent the visual acuity of observed leaks with single image snapshots reproduced in this report. The leaks as viewed in moving video images are much more pronounced and generally easier to identify, particularly for small leaks.



Figure 3-4. Example from LSI Ground Survey – Sampling During Bagging Test



Figure 3-5. Leak from Cargo Hatch on Barge G2- Mass Leak 1.86 g/s



Figure 3-6. Leak from Ullage Hatch on Barge G4- Mass Leak 0.31 g/s



Figure 3-7. Leak from Ullage Hatch on Barge G4- Mass Leak 0.19 g/s



Figure 3-8. Leak from Ullage Hatch on Barge G4- Mass Leak 0.24 g/s



Figure 3-9. Leak from Ullage Hatch on Barge G5- Mass Leak 0.73 g/s



Figure 3-10. Leak from Ullage Hatch on Barge G5- Mass Leak 1.43 g/s



Figure 3-11. Leak from Vent on Barge G6- Mass Leak 1.45 g/s



Figure 3-12. Leak from Cofferdam Hatch on Barge G6- Mass Leak 1.99 g/s



Figure 3-13. Leak from Cargo Hatch on Barge G7- Mass Leak 3.12 g/s



**Figure 3-14. Leak from Pressure Relief Valve on Barge G8- Mass Leak 5.78 g/s**

Additional information on LSI ground videos can be found in Appendices C and D. Note that the screenshots shown in Appendix D do not include all detected leak events, but are only from events where the leaks are easily apparent in the screenshots taken from the camera videos.

The LSI ground surveys onboard the barges provided the following general conclusions about this remote sensing approach for fugitive emission detection from petrochemical transport barges:

1. The deployed PGIE equipment exhibited sufficient operational robustness and detection sensitivity and was judged to be extremely useful for type of close range fugitive leak inspection. This conclusion agrees with previous similar studies using this technology.
2. The PGIE technique was able to easily identify apparent large leaks with smaller leaks somewhat more difficult to identify, likely requiring an expert operator.
3. Ground surveys on board the barges indicated that the leaks originally seen from the air were many times composed of numerous individual leaks upon closer inspection.



4. In all studied cases, leaks identified with the PGIE were verified as being significant by the LDEQ bagging study
5. Ground observations were easier to execute during mid-day to late afternoon time periods due to more favorable background imaging conditions (improved background radiance from hot barge surfaces and lower shadow interference) and because fugitive emissions were likely more pronounced as the barges became heated by solar radiation and ambient temperature during the day. Onboard observations were less sensitive to ambient conditions as compared to aerial observations (Section 3.1) due to the close-in nature of the inspection.
6. Onboard observations allow identification of much smaller leaks compared to airborne observations due to the close-in nature of the inspection and the ability to optimize viewing angles and focus.
7. Onboard PGIE observations are very useful for identification of specific leaking components and verification of subsequent leak repair activities.

### **3.3 PGIE Observations From the Lock Wall**

Ground-based PGIE observations of fugitive emissions from petrochemical transport barges were made by LSI, LDEQ, and ARCADIS personnel from the Port Allen lock wall during the BEM 1 study. The purpose of the lock wall PGIE observations was to provide mid-range views of leaks from barges that were being measured by the OTM 10 OP-FTIR survey. PGIE Observations were conducted by LSI using the LSI FLIR camera on September 24 and September 28-30, 2008 and by LDEQ and ARCADIS using LDEQ FLIR camera on September 28 and October 1-9, 2008. The dataset contains multiple movies showing various leaks from several different barges. Table 3-3 lists the LSI observations with representative images contained in the Figures 3-15 through 3-17. Table 3-4 lists the LDEQ/ARCADIS PGIE observations from the lock wall with representative images contained in Figures 3-18 through 3-20. The tables contain video filename number, the date of the observation, and the barge number or other descriptor. Additional information and images are contained in Appendices C-E.

**Table 3-3. Summary Table of Barge Leaks Identified by LSI Lock Wall Observations**

<b>Filename</b>	<b>Date</b>	<b>Part Leaking</b>	<b>Barge # or Other Descriptor</b>
0	9/24/2008	Hatch	Barge L1
1	9/24/2008	Hatch	Barge L1
2	9/24/2008	Hatch	Barge L1
3	9/24/2008	Hatch	Barge L1
4	9/24/2008	Hatch	Barge L1
5	9/24/2008	Hatch	Barge L2
6	9/24/2008	Hatch	Barge L2
70	9/28/2008	Cargo Hatch	Barge L3 #2 Port
71	9/28/2008	Cargo Hatch	Barge L3 #2 Starboard
72	9/28/2008	Cargo Hatch	Barge L3 #3 Starboard
73	9/28/2008	Cargo Hatch	Barge L3 #3 Port
74	9/28/2008	Same as Video 71	Barge L3 Filmed Again With Bag On
75	9/28/2008	Pressure Relief Valve	Barge L3
76	9/28/2008	Overview of Leaks	Barge L3 Another Overview of #2 & #3 Cargo Hatches
77	9/28/2008	Cargo Hatch	Barge L4 #3 Starboard
78	9/28/2008	Alarm Test Rod	Barge L4 #3 Port
79	9/28/2008	Cargo Hatch	Barge L4 #2 Port
80	9/28/2008	Ullage Hatch	Barge L4 #2 Port
81	9/28/2008	Ullage Hatch	Barge L4 #2 Starboard
82	9/28/2008	Cargo Hatch	Barge L4 #1 Starboard
83	9/28/2008	Cargo Hatch	Barge L4 #1 Port
84	9/28/2008	Vent	Barge L4
85	9/28/2008	Ullage Hatch	Barge L4 #1 Port
86	9/28/2008	Ullage Hatch	Barge L4 #1 Starboard
104	9/29/2008	Cargo Hatch	Barge L5 #1 Port
105	9/29/2008	Cargo Hatch	Barge L5 #2 Port & #3 Starboard
106	9/29/2008	Hatch & Pressure Valve	Barge L6 #3 Port & Pressure Relief Valve
107	9/29/2008	Butterworth & Cargo	Barge L6 #2 Starboard Forward & #1 Starboard
108	9/29/2008	Butterworth Hatch	Barge L6 #1 Starboard Middle
109	9/29/2008	Cargo Hatch	Barge L7 #3 Starboard
110	9/30/2008	Hatch & Pressure Valve	Barge L8 Pressure Relief Valve & #2 Starboard
111	9/30/2008	Slop Tank Vent	Barge L9

Figures 3-15 through 3-17 show three example snapshots from the lock wall observation illustrating the types of leaks that were detected: Example #1 shows a leaking hatch on Barge L1; Example #2 shows a leaking valve on Barge L2; and Example #3 shows a leaking hatch on Barge L6. The OTM 10 measured emission rates from barges in the lock are discussed in Sections 4 and 5.

Note that it is impossible to represent visual acuity of observed leaks with single image snapshots reproduced in this report. The leaks as viewed in moving video images are much more pronounced and generally easier to identify, particularly for small leaks.



**Figure 3-15. Example #1 from LSI Ground Survey – Leaking Hatch on Barge L1- Total Mass Emission from Barge 0.521 g/s**



Figure 3-16. Example #2 from LSI Ground Survey – Leaking Valve on Barge L2- Total Mass Emission from Barge 0.521 g/s



Figure 3-17. Example #3 from LSI Ground Survey – Leaking Hatch on Barge L6- Total Mass Emission from Barge 0.415 g/s

**Table 3-4. Summary Table of Barge Leaks Identified by LDEQ/ARCADIS Lock Wall Observations**

Filename	Date	Part Leaking	Barge # or Other Descriptor
VIDEO_080928_002	9/28/2008	Hatch	L10
VIDEO_080928_002	9/28/2008	Hatch	L10
VIDEO_081001_001	10/1/2008	Hatch	L11
VIDEO_081001_002	10/1/2008	Hatch	L11
VIDEO_081001_003	10/1/2008	Hatch	L11
VIDEO_081001_004	10/1/2008	Hatch	L11
VIDEO_081001_005	10/1/2008	Hatch	L11
VIDEO_081001_006	10/1/2008	Valve	L12
VIDEO_081001_007	10/1/2008	Vent	L12
VIDEO_081002_001	10/2/2008	Hatch	L13
VIDEO_081002_002	10/2/2008	Hatch	L13
VIDEO_081002_003	10/2/2008	Hatch	L13
VIDEO_081002_004	10/2/2008	Hatch	L13
VIDEO_081002_005	10/2/2008	Hatch	L13
VIDEO_081002_006	10/2/2008	Hatch	L14
VIDEO_081002_007	10/2/2008	Hatch	L15
VIDEO_081004_001	10/4/2008	Hatch	L16
VIDEO_081004_002	10/4/2008	Hatch	L17
VIDEO_081005_001	10/5/2008	Valve	L18
VIDEO_081005_002	10/5/2008	Hatch	L19
VIDEO_081005_003	10/5/2008	Hatch	L20
VIDEO_081006_001	10/6/2008	Hatch	L21
VIDEO_081008_001	10/8/2008	Vent	L22
VIDEO_081008_002	10/8/2008	Vent	L22
VIDEO_081009_001	10/9/2008	Vent	L23
VIDEO_081009_002	10/9/2008	Vent	L23

Figures 3-18 through 3-20 are three example snapshots illustrating the types of leaks that were detected: Example #1 shows a leaking hatch on Barge L10; Example #2 shows a leaking vent on Barge L23; and Example #3 shows a leaking valve on Barge L18. Additional example screenshots from the LDEQ camera videos can be found in Appendix E with discussion on OTM 10 emission flux measurement in Sections 4 and 5.



**Figure 3-18. Example #1 from Ground Survey with LDEQ Camera – Leaking Hatch from Barge L10 (there was no OTM 10 emission flux measurement for this time period)**



Figure 3-19. Example #2 from Ground Survey with LDEQ Camera – Leaking Vent from Barge L23- Total OTM 10 Mass Emission from Barge 0.490 g/s



Figure 3-20. Example #3 from Ground Survey with LDEQ Camera – Leaking Valve from Barge L13- Total OTM 10 Mass Emission from Barge 0.106 g/s

The lock wall PGIE observations provided the following general conclusions about this remote sensing approach for fugitive emission detection from petrochemical transport barges:

1. The deployed PGIE equipment exhibited sufficient operational robustness and detection sensitivity and was judged to be extremely useful for this type of mid-range distance fugitive leak inspection. This conclusion agrees with previous similar studies using this technology.
2. The PGIE technique was able to easily identify apparent large leaks with smaller leaks somewhat more difficult to identify, likely requiring an expert operator.
3. Lock wall mid-range observations were easier to execute during mid-day to late afternoon time periods due to more favorable background imaging conditions (improved background radiance from hot barge surfaces and lower shadow interference) and because fugitive emissions were likely more pronounced as the barges became heated by solar radiation and ambient temperature during the day. Lock wall observations were affected by strong shadows present in the deep lock under certain lighting conditions.
4. Mid-range Lock wall PGIE observations allow identification of much smaller leaks compared to airborne observations but were not as sensitive as close-range inspection onboard the barges which benefited from shorter range and the ability to optimize viewing angles.
5. Lock wall PGIE observations are judged to be very useful for routine inspection of barges passing through the lock.



#### **4. OTM 10 AM Emission Flux and Trace Compound Speciation Results**

The OTM 10 measurement at the Port Allen lock was performed from September 24 through October 9, 2008 from approximately 8:00 a.m. to 5:00 p.m. each day. The OTM 10 measurement attempted to assess emissions from all barge traffic that passed through the lock during this time period. In addition to OTM 10 measurements, PGIE camera images were acquired to compare measured flux rates leak appearance (Section 3.3). OTM 10 measurements focused on quantification of an alkane mixture (AM) flux (Appendix F).

Recorded barge traffic data included time of lock entry and exit and visual inspection of cargo labels on each barge. The reported cargo from the U.S. Army Corps of Engineers traffic log was also recorded. Note that the Corps of Engineers lock staff advised that the lock traffic reports are not necessarily accurate with regard to barge cargo. Of the six highest emissions events recorded by OTM 10, two occurred during times with barges that coded as carrying petroleum pitches, two with barges coded as carrying crude petroleum, and two with barges coded as empty (however the field crew smelled aromatics during one of these events). All OTM measured events and barge information are contained in Appendix G with a subset of the most interesting events presented in this section

##### **4.1 Data Graphs and Tables for Select Events**

A total of 97 barge sets (one or more barges per tug) passed through the lock during the OTM 10 observation period. AM fluxes were measured in a total of 62 temporally defined events. Many of these events exhibited small but measureable AM fluxes ( $< 0.1$  g/s) and occurred when non-petrochemical transport barges were in the lock indicating that the measured AM emissions were possibly associated with hydrocarbon emissions from the tug diesel engines from the tugs idling in the lock. A significant portion of the events exhibited high AM flux emissions and occurred in conjunction with PGIE leak identification from lock wall observations. These events are believed to be related to fugitive emissions from the barge with only a small relative component of AM emissions from tugs.

A subset of OTM 10 measurements is provided below with a complete listing contained in Appendix G. The summary contains a description of the event, the AM flux values measured during the event (presented in Tables 4-1 through 4-12), and a screenshot of a leak detected during the event from the PGIE observations when available (presented in Figures 4-1 through 4-6). The spectral data from each of these events were also screened for trace VOC compounds. The results of the trace compound analysis (when detected) are presented in Section 4.1.1. For some of the events, we report "WC" as the AM flux value. In these instances, AM concentrations were detected by the OP-FTIR instrumentation, but the

prevailing winds during the time of the measurement did not meet minimum data quality indicator levels regarding normal wind direction so an AM flux value could not be calculated.

**Table 4-1. 9/24/ 2008 – Event #1**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
9/24/2008	10:32	11:03	Two	Labeled as benzene. Reported as empty. Noticeable aromatic smell,

**Table 4-2. AM Flux Values Measured during 9/24/ 2008, Event #1**

<b>Time</b>	<b>AM Flux (g/s)</b>
10:36:59	0.124
10:39:37	0.237
10:42:17	0.321
10:44:56	0.431
10:47:35	0.558
10:50:13	0.637
10:52:53	0.730
10:55:33	0.912
10:58:12	0.956
11:00:15	0.308
<i>Average:</i>	<i>0.521</i>



Figure 4-1. Screenshot from FLIR Camera Showing Leak from 9/24/ 2008, Event #1

Table 4-3. 9/29/ 2008 – Event #2

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/29/2008	9:23	10:23	Three tugs with barges, one empty and two manned	Equipment/machinery/other

**Table 4-4. AM Flux Values Measured during 9/29/ 2008, Event #2**

<b>Time</b>	<b>AM Flux (g/s)</b>
9:39:26	0.514
9:42:06	0.374
9:44:45	0.305
9:47:23	0.325
9:50:00	0.410
9:52:39	0.457
9:55:16	0.596
9:57:55	0.590
10:00:33	0.463
10:03:11	0.324
10:05:50	0.297
10:08:29	0.389
10:11:09	0.374
10:13:48	0.390
<i>Average:</i>	<i>0.415</i>



Figure 4-2. Screenshot from FLIR Camera Showing Leak from 9/29/ 2008, Event #2

Table 4-5. 10/1/ 2008— Event #2

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/1/2008	9:10	9:58	Two	Organic industrial chemicals

**Table 4-6. AM Flux Values Measured during 10/1/ 2008, Event #2**

<b>Time</b>	<b>AM Flux (g/s)</b>
9:14:56	wc
9:17:33	wc
9:20:12	wc
9:22:51	wc
9:25:30	wc
9:28:09	0.019
9:30:52	wsc
9:33:30	0.035
9:36:09	0.046
9:38:54	0.067
9:41:31	0.065
9:44:12	0.058
9:46:48	0.04
9:49:23	wc
9:52:01	wc
<i>Average:</i>	<i>0.047</i>

wc = Wind criteria were not met.

wsc = Wind speed criteria not met.



Figure 4-3. Screenshot from FLIR Camera Showing Leak from 10/1/ 2008, Event #2

Table 4-7. 10/2/ 2008 – Event #2

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/2/2008	9:45	10:42	One tug with one barge, one tug with two barges	Butane, propylene, one empty

**Table 4-8. AM Flux Values Measured during 10/2/ 2008, Event #2**

<b>Time</b>	<b>AM Flux (g/s)</b>
9:48:36	wc
9:51:16	wc
9:53:53	wc
9:56:31	wc
9:59:09	0.072
10:01:46	0.141
10:04:24	0.126
10:07:02	0.084
10:09:41	wc
10:12:18	wc
10:14:57	wc
10:17:35	wc
10:20:11	wc
10:22:48	wc
10:25:28	wc
10:28:05	wc
10:30:41	wc
10:33:21	wc
10:36:00	wc
10:38:38	wc
<i>Average:</i>	<i>0.106</i>

wc = Wind criteria were not met.





Figure 4-4. Screenshot from FLIR Camera Showing Leak from 10/2/ 2008, Event #3

Table 4-9. 10/5/ 2008 – Event #1

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/5/2008	9:23	10:04	Two	Petroleum

**Table 4-10. AM Flux Values Measured during 10/5/ 2008, Event #1**

<b>Time</b>	<b>AM Flux (g/s)</b>
9:26:53	2.48
9:29:31	4.07
9:32:09	4.84
9:34:48	4.02
9:37:25	4.03
9:41:21	4.31
9:43:59	3.30
9:46:40	3.00
9:49:18	2.85
9:51:56	2.90
9:54:35	2.33
9:57:13	2.57
<i>Average:</i>	3.39



Figure 4-5. Screenshot from FLIR Camera Showing Leak from 10/5/ 2008, Event #1

Table 4-11. 10/9/2008- Event #7

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/9/2008	14:47	15:25	Two	Petroleum products, Empty

**Table 4-12. AM Flux Values Measured during 10/9/ 2008, Event #7**

Time	AM Flux (g/s)
14:51:46	0.286
14:54:24	0.331
14:57:02	0.635
14:59:40	0.794
15:02:17	0.819
15:04:55	0.877
15:07:32	0.661
15:10:11	0.432
15:12:49	0.206
15:15:28	0.18
15:18:05	0.174
Average:	0.490



**Figure 4-6. Screenshot from FLIR Camera Showing Leak from 10/9/ 2008, Event #7**

#### 4.1.1 Summary of the Results of Analysis of Trace VOC Concentrations

As mentioned above, the spectral data from each of the six events described above were screened for the presence of trace VOC. The data were collected with the EPA OP-FTIR along an optical beam path that extended along the surface of the lock, from one side of the lock to the other. The results of this analysis are presented in Table 4-13. The table also includes the measured alkane mixture concentration for each event. The instrument minimum detection limit for each compound is shown in parentheses. Additional VOC analysis was performed for all other temporally defined events during the OTM 10 measurements. The results of this analysis are presented in Appendix G of this document.

**Table 4-13. Summary of VOC Analysis**

Event Date	Alkane Mixture (ppb)	Mol. Mass Alkane Mixture (g/mole)	Benzene (ppb)	Toluene (ppb)	<i>m</i> -Xylene (ppb)	Styrene (ppb)	Ethylene (ppb)	1,3-Butadiene (ppb)	Methane* (ppb)
9/24/08	1002	79	ND(47)	ND(77)	37(34)	ND(11)	ND(7)	ND(12)	115
9/29/08	736	61	ND(61)	ND(96)	ND(52)	ND(17)	ND(9)	ND(18)	ND
10/1/08	184	58	ND(41)	ND(51)	ND(26)	ND(16)	8(7)	17(13)	302
10/2/08	1954	68	ND(44)	73(51)	ND(27)	18(12)	ND(7)	ND(10)	114
10/5/08	3826	62	71(66)	ND(80)	ND(36)	ND(21)	ND(10)	16(15)	172
10/9/08	768	60	ND(55)	ND(85)	ND(39)	ND(13)	ND(7)	ND(18)	40

\*Methane concentrations reported were measured along the ground-level beam path of the EPA OP- FTIR OTM 10 Configuration

ND = Not detected

#### 4.2 Instances of Emissions Detected with the PGIE but not with ORS Measurements

An analysis of the PGIE observations made by the LSI Ground Crew and ARCADIS personnel in the lock revealed that there were instances where the PGIE detected barge leaks, but the events were not detected by the ORS instrumentation deployed on the southern side of the lock. Table 4-14 presents a summary of six events that were detected by the PGIE but not the ORS instrumentation. The table includes the date and time of the events, as well as the average prevailing wind direction during the time the PGIE detected the leaks.

**Table 4-14. Summary of Leak Events Detected by the PGIE but not ORS Instrumentation**

Date	Time	Barge Number(s)	Prevailing Wind Direction (degrees)
9/28/08	11:30 am	L10	120
9/29/08	4:32 pm	L7	320
9/30/08	2:46 pm	L8	300
10/2/08	10:25 am	L18, L19	140
10/2/08	1:00 pm	L14	180
10/2/08	2:35 pm	L15	150
10/8/08	9:21 am	L22	320

The orientation of the ORS measurement planes (when looking from the OP-FTIR to the scissor lift) were 133° and 311° for the EPA and ARCADIS OP-FTIR measurement planes, respectively. Considering the ORS configurations used in the study, a prevailing wind direction of approximately 41° is ideal for emissions measurements (perpendicular to the configuration planes). As can be seen in Table 4-14, the prevailing winds during the events not detected by the ORS instrumentation were close to parallel to the measurement configurations, or in some cases the winds were not from the direction of the lock (wind direction greater than 133° or less than 311°). The prevailing winds during the times the leaks were detected by the PGIE did not carry the winds through the ORS measurement plane, which explains why the leaks were not detected by the ORS instrumentation.

### 4.3 Evaluation of AM Emissions from Tugs

In order to evaluate the contribution of exhaust from the tugs to the alkane mixture (AM) emissions fluxes measured during the project, carbon monoxide concentrations were analyzed along the ground level beam path of the ARCADIS OP-FTIR VRPM configuration. Carbon monoxide was chosen for this analysis because it is a byproduct of combustion, and has relatively low detection limits with the OP-FTIR instrument. For the nine events detected from barges classified as “empty-no further information”, the carbon monoxide and alkane mixture concentrations measured along the ground level beam path were compared to investigate any possible correlations between the two compounds. A correlation between the two compounds would suggest that the source of the total hydrocarbon emissions measured was the emissions from the tug engines.

Of the nine events analyzed, eight of the events showed no correlation between the measured carbon monoxide and total hydrocarbon concentrations. The analysis did indicate a strong correlation between the concentrations of the two compounds during the 9/28/08

9:38 am to 10:11 am event ( $r^2=0.83$ ). However, the alkane mixture concentrations measured during this event were relatively low and close to the minimum detection limits of the OP-FTIR instrument. Based on these findings, we conclude that emissions of alkane mixture from the tug exhaust are negligible. The data from this analysis are presented in Appendix I of this document.

The OTM 10 lock wall mass flux measurements provided the following general conclusions about this remote sensing approach for fugitive emission detection and quantification from petrochemical transport barges:

- (1) The deployed OTM 10 equipment exhibited sufficient operational robustness and detection sensitivity and was judged to be useful for this type of mid-range distance leak detection/quantification activities where compound speciation is important.
- (2) The OTM 10 technique was able to identify and assess emission rates from a range of leak sizes as long as the prevailing wind brought the emitted plume through the vertical plane of the EPA OTM-10 measurement configuration.

## 5. Bagging Test Emission Estimate Results

As described previously, onboard leak bagging tests were performed by SAGE Environmental Consulting for LDEQ (Appendix H). The testing was performed directly at the source of the leak on each barge. During the five day bagging test, 23 leak points from a total of eight barges were measured to determine approximate THC mass emission rates. Table 5-1 reproduces the bagging test results contained in the LDEQ report including the measured total non-methane hydrocarbon emissions with values converted to g/s for comparison. The table shows that the measured total non-methane hydrocarbon emissions flux values ranged from 0.07 to 5.77 g/s.

**Table 5-1. Summary of LDEQ Bagging Test Results**

Test#	Barge#	Cargo	Mass Leak (g/s)
1	G1	Unleaded Gasoline	2.53
2	G2	Trans Mix	0.31
3	G2	Trans Mix	0.57
4	G2	Trans Mix	1.86
5	G2	Trans Mix	0.32
6	G3	Trans Mix	0.89
7	G3	Trans Mix	1.32
8	G4	Naphtha but cleaned	0.31
9	G4	Naphtha but cleaned	0.18
10	G4	Naphtha but cleaned	0.24
11	G4	Naphtha but cleaned	0.13
12	G4	Naphtha but cleaned	0.07
13	G4	Naphtha but cleaned	0.20
14	G5	Raffinate	2.11
15	G5	Raffinate	0.73
16	G5	Raffinate	1.42
17	G5	Raffinate	0.07
18	G6	Gasoline	1.45
19	G6	Gasoline	1.98
20	G7	Naphtha	3.12
21	G7	Naphtha	0.66
22	G8	Unleaded Gasoline	5.77
23	G8	Unleaded Gasoline	0.47



## 6. Comparison of OP-FTIR and Bagging Test Emission Flux Results

It is instructive to compare OTM 10 measurements and LDEQ bagging study results to help draw overall conclusions regarding the study. However, it is important to note that the results of the bagging method report emissions flux values from each individual leak, while the OTM 10 results report emissions flux values for each barge (possible multiple barges) and could consist of multiple leaks. Additionally, as mentioned in a previous section of the report, barge traffic through the Port Allen Lock was much lighter than normal due to repair activities on the Intracoastal Waterway Bayou Sorrel Bridge. Although study personnel originally planned to conduct bagging tests on barges immediately upon exiting the lock, this was not possible due to a lack of barge traffic through the lock during the period that Sage Environmental personnel were at the site. Instead, the barges selected for monitoring using the bagging method were chosen because they were identified as having very significant leaks from the airborne PGIE surveys. Therefore, the barges selected for the bagging experiments may not represent an average case, whereas the OTM 10 measurements were conducted on barges moving through the lock with no selection process and may represent a more typical sample cross-section. Even with these differences, it is useful to compare the results of emissions flux values determined from each method on different barges.

As discussed, the LDEQ bagging test results report findings for individual leaks on the barge as compared to the OTM 10 results which can include emissions from multiple leak points on a given barge or multiple barges. Table 6-1 presents results from the two measurement methods expressing the results of the LDEQ bagging test as a summation of measured leaks from a given barge and tabulating this with the most significant OTM 10 flux rate measurements. Note the measurements are from different barges so they serve as only a range comparison. The LDEQ bagging test results are labeled (Bag) and show leak rates of THC whereas the OTM 10 results, labeled (OTM 10), show AM flux rates.

**Table 6-1. Summary of LDEQ Bagging Test Barge Totals and Most Significant OTM 10 Results**

Test	Barge Number(s)	Cargo	Total Mass Leak Rate (g/s)
Bag	G1	Unleaded Gasoline	2.53
Bag	G2	Trans Mix	3.06
Bag	G3	Trans Mix	2.21
Bag	G4	Naphtha but cleaned	1.13
Bag	G5	Raffinate	4.33
Bag	G6	Gasoline	3.43
Bag	G7	Naphtha	3.78
Bag	G8	Unleaded Gasoline	6.24
OTM 10	L1	Benzene (Empty)	0.521
OTM 10	L5, L6	Equipment/Machinery/Other	0.415
OTM 10	L11	Organic industrial chemicals	0.047
OTM 10	L13	Butane, propylene, one empty	0.106
OTM 10	L18, L19	Petroleum	3.39
OTM 10	L23	Petroleum products, one empty	0.490

The above comparison is for different barges using different measurement techniques each of which can possess significant uncertainty due to the difficulty of the assessment. The primary sources of uncertainty are described in Section 7. With the difficulties these measurements present, the relative agreement between the two techniques may provide some confidence in the individual measures. From Table 6-1 the range of AM flux values found with the OTM 10 method was generally lower than the values found using the bagging method although the maximum flux values measured are comparable (3.39 with the OTM 10 method and 6.24 with the bagging method). The barges selected for the bagging experiments were identified as having very significant leaks from the airborne survey so they may not represent an average case whereas the OTM 10 measurements were conducted on barges moving through the lock with no selection process and therefore represent a more typical sample cross-section. This fact could help explain the lower values observed by OTM 10. Additionally, we would expect some underestimation of the alkane mixture (AM) flux measurement by OP-FTIR in comparison to the total non-methane hydrocarbon measurement produced in the bagging studies since non-alkane compounds can be somewhat underrepresented in the OP-FTIR AM approximation due to lack of signal in the spectral analysis region.

Note that these emission estimates presented in this report represent a snapshot in time. Fugitive emissions from petrochemical barges are believed to vary significantly due to ambient temperature, thermal load, product mix, load state, and equipment condition.

## 7. Quality Assurance/Quality Control

The following sections discuss the quality assurance methods used for the OTM 10 measurements. Note that quality assurance methods and procedures for the bagging tests can be found in Appendix H of this document.

### 7.1 Instrument Calibration

As stated in the *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004), all equipment is calibrated annually and / or cal-checked at the U.S. EPA facility as part of standard operating procedures. Certificates of calibration are kept on file. Maintenance records are kept for any equipment adjustments or repairs in bound project notebooks that include the data and description of maintenance performed. Instrument calibration procedures and frequency are listed in Table 7-1 and further described in the text.

**Table 7-1. Instrumentation Calibration Frequency and Description**

Instrument	Measurement	Calibration Date	Calibration Detail
IMACC, Inc. OP-FTIR	Analyte PIC	Pre-deployment and in-field checks	MOP-6802 and 6823 of the ECPB Optical Remote Sensing <i>Facility Manual</i>
R.M. Young Model 05103 Meteorological Head	Wind Speed in miles/hour	6/21/08	U.S. EPA Wind Tunnel Cal. Records on file at EPA Metrology Lab
R.M. Young Model 05103 Meteorological Head	Wind direction in degrees from North	6/21/08	U.S. EPA Wind Tunnel Cal. Records on file at EPA Metrology Lab
Topcon Model GTS-211D Theodolite	Distance Measurement	6/17/08	Calibration of distance measurement. Actual distance = 42.5 ft Measured distance = 43.11 ft
Topcon Model GTS-211D Theodolite	Angle Measurement	6/17/08	Calibration of angle measurement. Actual angle = 360° Measured angle = 359°01'08"

### 7.2 Assessment of DQI Goals

The critical measurements associated with this project and the established data quality indicator (DQI) goals in terms of accuracy, precision, and completeness are listed in Table 7-2. More information on the procedures used to assess DQI goals can be found in Section 10 of the *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004).

**Table 7-2. Data Quality Indicator Goals for the Project**

Measurement Parameter	Analysis Method	Accuracy	Precision	Completeness
Analyte PIC	OP-FTIR: Nitrous Oxide Concentrations	$\pm 25\%/15\%/10\%$ <sup>a</sup>	$\pm 10\%$	90%
Ambient Wind Speed	R.M. Young Met heads pre-deployment calibration in EPA Metrology Lab	$\pm 1$ m/s	$\pm 1$ m/s	90%
Ambient Wind Direction	R.M. Young Met heads pre-deployment calibration in EPA Metrology Lab	$\pm 10^\circ$	$\pm 10^\circ$	90%
Distance Measurement	Theodolite- Topcon	$\pm 1$ m	$\pm 1$ m	100%
Gas plume relative opacity	PGIE: gasoline vapor release	N/A <sup>b</sup>	N/A <sup>b</sup>	100%

(a) The accuracy acceptance criterion of  $\pm 25\%$  is for path lengths of less than 50 m,  $\pm 15\%$  is for path lengths between 50 and 100 m, and  $\pm 10\%$  is for path lengths greater than 100 m.

(b) The PGIE is not a quantitative device and does not provide a numerical output.

#### 7.2.1 DQI Check for Analyte PIC (OP-FTIR) Measurement

The precision and accuracy of the concentration data may be checked by looking at the analyzed nitrous oxide concentrations. The known atmospheric background nitrous oxide concentration is around 315 ppbv (this is an average value, as the value exhibits a slight seasonal variation). The acceptable range of nitrous oxide concentrations is 315 ppb  $\pm 25\%$  for path lengths of less than 50 m, 315 ppb  $\pm 15\%$  for path lengths between 50 and 100 m, and 315 ppb  $\pm 10\%$  for path lengths greater than 100 m. Verifying this background concentration provides a good QC check of the data collected. Obviously, this method is not valid for data collected at a site that is a source of nitrous oxide.

The precision of the analyte PIC measurements was evaluated by calculating the relative standard deviation (RSD) from one data subset collected near the surface of the suspected source. A subset is defined as the data collected along one particular path length during one particular survey in one survey sub-area.

The accuracy of the analyte PIC measurements was evaluated by comparing the calculated nitrous oxide concentrations from one data subset to the background value of 315 ppb. The number of calculated nitrous oxide concentrations that failed to meet the DQI accuracy criterion was recorded.

Overall, a total of three datasets were analyzed from three different time periods, one at the beginning of the project (September 24), one during the middle of the project (September 28), and one at the end of the project (October 9). Based on the DQI criterion set forth for precision of  $\pm 10\%$ , all of the data subsets were found to be acceptable, for a completeness of 100%. The range of calculated relative standard deviations for the data subsets from this field campaign was 1.8 to 4.0 ppb, which represents 0.57 to 1.27% RSD.

Each data point (calculated nitrous oxide concentration) in the data subsets was analyzed to assess whether or not it met the DQI criterion for accuracy of  $\pm 10\%$  ( $315 \pm 32$  ppb), as the path lengths used for measurements were greater than 100 meters. A total of 233 data points were analyzed, and 176 of the points met the DQI criteria for accuracy for a completeness of 76%.

#### 7.2.2 PGIE Relative Opacity DQI Assessment

The PGIE used in this study are not quantitative instruments and therefore do not provide calibrated numerical data for images. The performance of the device can be assessed in a basic way by imaging a known gas release against a stable background, such as a concrete pad. During the current campaign, the vapors from an opened container of gasoline were used for the known gas release. Imaging this test release ensured the camera was operating properly and device firmware was set correctly.

#### 7.2.3 Meteorological Head DQI Assessment

The meteorological head DQIs are checked annually as part of the routine annual calibration procedure. Before deployment to the field, the user verified the calibration date of the instrument by referencing the calibration sticker. If the date indicates the instrument is in need of calibration, it should be returned to the APPCD Metrology Laboratory before deployment to the field. The precision and accuracy of the heads is assessed by conducting a calibration in the EPA Metrology Lab using the exhaust from a bench top wind tunnel. This calibration procedure differs from the procedure used to perform the annual calibration of the instruments.

Additionally, a couple of reasonableness checks were performed in the field on the measured wind direction data. While data collection is occurring, the field team leader compares wind direction measured with the heads to the forecasted wind direction for that particular day. Another reasonableness check involves manually setting the vane on the meteorological heads to magnetic north (this is done with a hand held compass). The observed wind direction during this test should be very close to  $360^\circ$ .

#### 7.2.4 Topcon Theodolite DQI Assessment

Before field deployment, ensure the battery packs are charged for this equipment. The following additional checks (which are performed at least annually) were made on June 17, 2008. The calibration of distance measurement was done at the EPA Facility using a tape measure. The actual distance was 42.5 feet, and the measured distance was 43.11 feet. The results indicate that instrument accuracy falls well within the DQI goals. The calibration of angle measurement was also performed. The actual angle was 360°, and the measured angle was 359°01'08". The results indicate accuracy falls well within the DQI goals.

Additionally, there are several internal checks in the theodolite software that prevent data collection from occurring if the instrument is not properly aligned on the object being measured, or if the instrument has not been balanced correctly. When this occurs, it is necessary to re-initialize the instrument to collect data.

#### 7.2.5 QC Checks of OP-FTIR Instrument Performance

At the beginning of the project, a series of QC checks were performed on both OP-FTIR instruments to assess the instrument performance. On September 25, 2008, the Single Beam Ratio, Baseline Stability, Noise Equivalent Absorbance, ZPD Stability, Saturation, Random Baseline Noise, and Stray Light diagnostic tests were performed. The results of the tests indicated that the ARCADIS and EPA OP-FTIR instruments were operating within the acceptable criteria for each QC check. More information on the diagnostic checks that are performed as part of a typical ORS field campaign can be found in MOP 6802 and 6823 of the *ECPD Optical Remote Sensing Facility Manual* (U.S. EPA, 2004).

In addition to the QC checks performed on the OP-FTIR instruments, the quality of the instrument signals (interferogram) was checked constantly during the field campaigns by ensuring that the intensity of the signal was at least 5 times the intensity of the stray light signal (the stray light signal is collected as background data prior to actual data collection, and measures internal stray light from the instrument itself). In addition to checking the strength of the signal, checks were done constantly in the field to ensure that the data were being collected and stored to the data collection computer. During the campaign, a member of the field team monitored the data collection computer to make sure these checks were completed.

### 7.3 Estimate of Uncertainty in the OTM 10 Emission Flux Measurements

As mentioned in Section 2, the OTM 10 measurement configurations consisted of three measurement paths which extended from the OP-FTIR instrument to the scissor lift. The 3-beam OTM 10 approach was chosen for this project since it was much more important to obtain a larger number of measurement cycles while the mobile source was contained in the lock rather than a fewer number of cycles with a five beam approach since the horizontal spatial location of the plume was not of primary importance. It was generally assumed that the plumes emitted from the barges would be initially small in spatial extent but would likely experience significant dispersion before exiting the lock and passing through the OTM 10 plane. It is likely that this assumption is correct since the barges were significantly below the lock wall top (approximately 7m to 12 m) and the emitted plumes could experience several dispersive/mixing mechanisms (such as stagnation, turbulence, channeling) depending on ambient wind direction and speed so the plumes could evolve more than in a flat wind swept scenario with similar downwind standoff.

In analyzing the PIC data using the 3-beam approach, the peak plume concentration was assumed to be centered along the crosswind axis of the OTM 10 configuration, and the  $\sigma_y$  parameter (horizontal dispersion coefficient) of the measured plume was assumed to be equal to  $\frac{1}{2}$  the length of the OTM 10 configurations. It was necessary to make these assumptions because the 3-beam OTM 10 approach does not include two intermediate surface beam paths which are used to obtain information on the horizontal location and dispersion of the plume.

In order to estimate the uncertainty associated with assuming a fixed peak plume concentration location and  $\sigma_y$  parameter, we used the VRPM Fit Explorer program (described by Abichou et al., 2009) to run a series of simulations to assess the variability in flux results from the OTM 10 method as a result of assuming different  $\sigma_y$  and peak plume concentration locations. In this simulation program, a downwind concentration field is generated from an area source using EPA ISC Gaussian dispersion model and then analyzed using OTM 10 algorithms and optical beam geometries.

Table 7-3 presents the results of a simulation done for three different assumed plume sizes where the  $\sigma_y$  parameter was varied, but the plume location was assumed to be fixed in the center of a 160 meter measurement configuration. The plume dimensions are shown in Table 7-3 as: *width (m) by crosswind distance (m)*. The results are shown in units of g/s, and are compared to an OTM 10 calculation of 1.0 g/s for the same plume size assuming a  $\sigma_y$  value of 80 meters and a peak plume concentration location at 80 meters (as measured



along the surface of the OTM 10 configuration plane from the OP-FTIR instrument), which is approximately equal to the parameters used for data analysis in the current study.

**Table 7-3. Results of Flux Values Calculated by the VRPM Fit Explorer Program With a Fixed Peak Plume Concentration Location and Varying Values of the  $\sigma_y$  Parameter**

$\sigma_y$ Value	5 m × 40 m	5 m × 80 m	5 m × 120 m
$\sigma_y = 8$ m	1.002	1.030	1.068
$\sigma_y = 80$ m	0.921	0.945	0.978
$\sigma_y = 800$ m	0.914	0.938	0.970

The results of the simulation show that the OTM 10 calculation is insensitive to varying the value of the  $\sigma_y$  parameter (the OTM 10-derived flux values from the simulation were within  $\pm 8.6\%$  of control simulated values).

Table 7-4 presents the results of a second simulation done for three different assumed plume sizes where the plume center location was varied, but the  $\sigma_y$  parameter was assumed to be 80 m. The results are shown in units of g/s, and are compared to an OTM 10 calculation of 1.0 g/s for the same plume size assuming a  $\sigma_y$  value of 80 meters and a peak plume concentration location at 80 meters.

**Table 7-4. Results of Flux Values Calculated by the VRPM Fit Explorer Program with a Fixed  $\sigma_y$  Parameter and Varying Peak Plume Concentration Locations**

Peak Plume Concentration Location (m)	5 m × 40 m	5 m × 80 m	5 m × 120 m
20	3.651	N/A	N/A
40	2.066	1.910	N/A
60	1.305	1.322	1.300
80	0.921	0.945	0.978
100	0.700	0.718	0.743
120	0.545	0.554	N/A
140	0.412	N/A	N/A

N/A- Simulation results not included because plume would not be located within the confines of the OTM 10 configuration plane

The results of the simulation show that the 3-beam OTM 10 calculation is highly dependent upon the peak plume concentration location along the OTM 10 configuration plane. When the simulation was run with the peak concentration location close to the location of the OP-FTIR instrument (peak concentration location < 40 m), the OTM 10-derived flux values from the simulation were as much as 265% higher than control simulated values. However, the OTM 10-derived flux values from the simulation agreed better with control values as the plume becomes larger and is more centered on the optical configuration. Underestimation is evident closer to the end of the configuration defined by the location of the scissor lift.

Additional analysis was performed to compare the AM concentrations measured on the lowest beam path of each OTM 10 configuration during the AM emissions events described in Section 4.1. The analysis showed the average AM concentration ratio of the lowest OTM 10 beam paths for the two measurement planes for the several measurement periods presented in the report (in ppb) are: 324/63, 271/59, 244/39, 1563/945, 306/211, with baseline levels below 10 ppb. This suggests that the peak plume concentration location for each emissions event was located at a position along the OTM 10 configuration plane closer to the scissor lift ( $\geq 80$  m) and/or that the effective plume size was more similar to the 120m (large plume) case. Based on the above plane to plane ratio analysis, a small plume located near the vertex of the beams (highly overestimated case) was not likely. Based on the simulation results and information on OTM 10 measurement accuracy from previous tracer-release validations studies, it is reasonable to assume that the overall uncertainty in the AM flux results for this effort are likely within  $\pm 50\%$ .

#### **7.4 Uncertainty in the LDEQ Leak Bagging Estimates**

The on-board leak bagging measurements conducted by SAGE Environmental Consultants for LDEQ is described in Appendix H of this report. Sage identifies several factors which can impact uncertainty in mass emission estimates including: sampling and analytical variability, leak capture/containment variability, inter-dependence of multiple leaks, and temperature effects. Additionally, this measurement campaign represented the first attempt, to our knowledge, to produce leak emission rate estimates from these source types using the component bagging technique. As a consequence, there is inherent uncertainty associated with novel application. To supplement Appendix H, further information on the execution of the bagging study and potential areas leading to uncertainty can be found in Appendix J which reproduces comments from the American Waterways Operators on this testing procedure along with responses from Sage Environmental Consulting.

## 7.5 General Data Limitations

One aspect of this report centers on the use of optical remote sensing equipment (especially PGIE) for identification of significant fugitive leaks from this difficult to measure source category in real-world scenarios. There are few perceived limitations on the use of the acquired remote sensing and imagery data in support the conclusion that these tools are generally useful for this purpose. Questions still remain as to the limits of detection and how these limits are affected by various field, target, and instrument parameters and these questions should be the subject of further study.

Another aspect of this report relates to estimates of emissions from this source category. Both measurement techniques, (EPA OTM 10 from the lock wall and the LDEQ bagging study) produced results which indicate a potentially significant level of short-term fugitive VOC emissions can occur. As discussed, measurements from this source category are difficult, and there is significant uncertainty in the absolute measurement results from both techniques and this should be considered a limitation of the data. Additionally, a more significant data limitation centers on the short-duration nature of these measurements which represent a snap-shot in time. Fugitive emissions from petrochemical barges are believed to vary significantly due to ambient temperature, thermal load, product mix, load state, and equipment condition. Since there is little information on the influence of these factors, extrapolation of these short term emission rate estimates is not recommended.

## 7.6 Deviations from the QAPP

The Quality Assurance Project Plan indicated that an ultraviolet differential optical absorption spectroscopy (UV-DOAS) instrument would be deployed to collect supplemental measurements of the BTEX compounds. The UV-DOAS instrument was not deployed at the site due to limited project resources and potential eye safety issues at the site. Instead, two additional OP-FTIR optical beam paths were deployed (one from each OP-FTIR instrument) across the surface of the lock to collect supplemental data on alkane mixture and trace VOC concentrations.

Also, it was originally anticipated that the VRPM configuration would be deployed along the northern edge of the lock. However, at the time of the field campaign, the winds were largely from the north, and the configuration was deployed on the southern edge of the lock.

## 8. Summary

This report describes the BEM 1 field campaign conducted in Baton Rouge, Louisiana from September 24 to October 9, 2008. BEM 1 investigated VOC emissions from petrochemical transport barges using portable gas imaging equipment PGIE (infrared cameras), and EPA Method OTM 10 with Open-path Fourier transform infrared (OP-FTIR) spectrometers, in addition to leak bagging tests.

The objectives of the study were:

- To improve knowledge of fugitive VOC emissions from petrochemical transport barges.
- To demonstrate and advance the field application of select ORS techniques (EPA OTM 10 OP-FTIR and PGIE) for identification and quantification of fugitive emissions from difficult to monitor sources.
- Identify sources of fugitive leaks from multiple barges

To accomplish these goals, the project team conducted several complementary efforts:

1. Aerial PGIE surveys of barges located on the Mississippi River and inter-coastal water ways to identify barges with significant fugitive emissions.
2. Ground-based PGIE observations of barges from the Port Allen Lock wall and also onboard several barges to identify and closely observe fugitive leaks.
3. Onboard leak emission bagging measurements conducted by LDEQ on several barges to quantify leak rates and allow comparison with PGIE images.
4. EPA method OTM 10 with open-path Fourier transform infrared spectroscopy used at the Port Allen lock to produce hydrocarbon emission measurements from barge traffic traveling through the lock.

The aerial PGIE camera monitoring performed by LSI, Inc. detected leaks from 45 different barges located in the Mississippi River and the Intracoastal Waterway. The ground-based monitoring performed by LSI, Inc. detected leaks from 18 different barges in the U.S. Army Corps of Engineers lock and in the Mississippi River. Additional infrared camera monitoring performed by ARCADIS and LDEQ personnel in the lock detected multiple leaks from

several barges. This report contains a number of leak images that serve to further understanding of fugitive emissions from various barge components.

The remote sensing surveys provided significant information regarding the use of infrared cameras for detection of fugitive emissions from petrochemical transport barges. The PGIE equipment was robust, easy to use, and possessed sufficient detection sensitivity for this application. The PGIE remote sensing approach is judged to be extremely useful for both aerial survey and close range fugitive leak inspection of petrochemical transport barges. The PGIE technique was able to identify a large range of leaks with large leaks detectable from the air and smaller leaks more easily observed at close range. PGIE observations were easier to execute during mid-day to late afternoon time periods due to more favorable background imaging conditions (improved background radiance from hot barge surfaces and lower shadow interference) and because fugitive emissions were likely more pronounced as the barges became heated by solar radiation and ambient temperature during the day. PGIE observations were very useful for identification of specific leaking components and verification of subsequent leak repair activities.

Based on aerial observations, eight barges with observed large leaks were selected for onboard leak emission rate measurements as part of the LDEQ on-board bagging survey. For this effort, a total of 23 leak points from eight barges were bagged to determine mass emission rates. The measured total non-methane hydrocarbon emissions flux values from individual leaks during the bagging study ranged from 0.07 g/s to 5.77 g/s. Summing all measured leaks for each individual barge yielded a barge total leak rate ranging from 1.13 to 6.24 g/s.

OTM 10 Monitoring was conducted at the Port Allen lock wall from September 24 through October 9. A total of 97 barge sets passed through the lock during the OTM 10 observation period. Six events showed significant fugitive hydrocarbon emissions as measured by OTM 10 with values ranging from 0.047g/s to 3.39 g/s AM flux rate. The equipment deployed to apply the OTM 10 approach exhibited sufficient operational robustness and detection sensitivity and was judged to be useful for mid-range distance leak detection/quantification activities where compound speciation is important. Additionally, the OTM 10 technique was able to identify and assess emission rates from a range of leak sizes as long as the prevailing wind brought the emitted plume through the vertical plane of the OTM-10 measurement configuration.

In comparing the LDEQ bagging measurements with the OTM 10 measurements (different barges), the range of AM flux values found with the OTM 10 method were generally lower than the values found using the bagging method although the maximum flux values

measured are comparable (3.39 g/s with the OTM 10 method and 6.24 g/s with the bagging method). The barges selected for the bagging experiments were identified as having very significant leaks from the airborne survey so they may not represent an average case whereas the OTM 10 measurements were conducted on barges moving through the lock with no selection process and therefore represent a more typical sample cross-section. This fact could help explain the lower values observed by OTM 10.

An analysis of the infrared camera observations and ORS measurements made in the lock revealed that there were seven instances where the camera detected barge leaks, but the events were not detected by the ORS measurements. However, further analysis showed that the prevailing winds during the time of these events were parallel to the ORS measurement plane, or actually contained a southerly component (the lock was located to the north of the measurement configuration), so the barge emissions were not captured by the ORS measurement configuration.

A significant output of this project is represented in the image database which provides a comparison of PGIE images of leaks with measured leak rates which helps improve the understanding of the qualitative information provided by the infrared cameras for this source category.

Emission estimates contained in this report represent a snapshot in time. Fugitive emissions from petrochemical barges are believed to vary significantly due to ambient temperature, thermal load, product mix, load state, and equipment condition.

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## **APPENDIX A**

LSI Report: Leak Detection using LSI Infrared Gas Imaging, BEM 1  
Barge Study; Aerial



# **Report: Leak Detection using LSI Infrared Gas Imaging**

## **BEM1 Barge Study**

David Furry, President, LSI  
Date: October 27, 2008

## **Executive Summary**

Leak Surveys Inc. (Early, TX) was commissioned by Arcadis to conduct an optical imaging survey on barges located in various waterways within the Mississippi River Delta as part of the BEM1 Project. The optical imaging survey looked at various components within these processes. The aerial optical imaging leak (smart LDAR) survey was conducted from September 24<sup>th</sup> thru October 1<sup>st</sup>, 2008. The Hawk Leak Detection System visualized a total of 40 leaks on the various barges. Carl Hacking, Pilot and David Varner, camera technician, performed the leak survey.

## **Standard Operating Procedure Aerial Pipeline Survey**

When performing an aerial pipeline survey, there are some standard operating procedures that must be followed in order to ensure the variables of the survey are constant and do not change according to user.

1. Fully charge all batteries and digital video recorders the night before starting the pipeline survey
2. Surveys will commence at 9:00 am unless unfavorable weather or other factors are involved.
3. The pilot will perform a preflight briefing prior to each day's survey.
  - a. Included in this preflight meeting are the following:
    - i. Safety issues
    - ii. Terrain evaluation
    - iii. Survey Speed/Height
    - iv. Emergency Procedures
4. Once the preflight briefing has been performed, the passenger door will need to be removed in preparation for the survey.
5. The camera crew will now check all equipment to make sure batteries are fully charged and ready to go. Once this has been checked all equipment will remain on and the survey will commence.
6. The camera operator will hold the camera outside the door focusing on the pipeline right of way.
7. If any leaks are found during the pipeline survey the following steps will be taken:
  - a. Pilot will circle back around to approximately ½ mile before leak on pipeline for optimum video footage.
  - b. The camera operator will record the leaking gas emissions for a predetermined amount of time.
  - c. Once the leak has been recorded, a digital picture will be taken of the source where the leak is occurring.

- d. Finally GPS coordinates will be taken to ensure an accurate location of the leak.
8. At the completion of the pipeline survey, a daily briefing will take place to discuss any issues encountered during the day. All leak data will be relayed to the appropriate personnel for immediate remediation.
9. All of these actions must be taken into account each day to ensure the integrity of the pipeline patrol process.

## **Background**

Leak Surveys Inc. is an international company with 4-½ years experience using the Hawk Leak Detection System (HLDS). LSI developed the HLDS after 12 years of research and development on optical imaging and has applied for international patents.

LSI and the API committee introduced using optical imaging to conduct surveys in refinery and chemical plants on a commercial basis to the industry in February of 2004.

Our international smart LDAR crews have performed actual leak surveys in the Asia Pacific area, Europe and North America for a variety of different customers over the past 3-½ years.

The human eye more readily perceives motion than contrast. Movie or real time images are used as the basis for leak detection in the data presented here. Image quality is affected by the temperature and emissivity difference between the gas cloud and the background.

At this point, no infrared gas imaging cameras are capable of providing quantitative measurements of gas concentration, however, studies funded by the American Petroleum Institute that shows the detection limits accomplished by passive gas imaging systems are within the bounds necessary for equivalent detection of leaks at less than 10,000 ppm (60 g/hr).

Gas imaging provides the user with a real time achievable record of leaking components as well as providing specific locations of leaks within a component.

## **Camera Description**

The infrared gas imaging camera used by Leak Surveys, Inc., consists of a modified Indigo (FLIR/Indigo Systems Corp., Goleta CA) Merlin MID camera with a nominal spectra range of 1- 5.4  $\mu\text{m}$ . Using a 30 x 30 m InSb detector with a 320 x 240 pixel array, the camera has capabilities of varying the integration times from 5  $\mu\text{s}$  to 16.5 ms. The detector is operated at near liquid nitrogen temperatures using an integral Stirling cooler which provides the system with an NEdT of no more than an 18 mK providing excellent sensitivity.

The spectral range was further limited with the use of a notch filter specifically designed for the detection of hydrocarbon infrared absorptions in the 3 micron region. The narrow band pass range of the filter is less than the infrared spectral absorption of gas phase hexane. The filter notch is positioned such that alkane gases have a significant response within the band pass range.

Various lens including a 25 mm, a 50 mm and a 100 mm lens were used during the experiments. The 25 mm lens provides a 22 x 16 degrees field of view with an f-number of 2.3. The 50 mm lens provides an 11 x 8 degrees field of view with an f-number of 2.3.

The use of a narrow band pass filter provides spectral discrimination that allows the detection of compounds that have a vibration mode in the infrared region of the filter. Not all hydrocarbons have infrared absorptions within the filter range. Table I (below) shows the theoretical relative response of various compounds of interest using 1 cm-1 resolution infrared spectra (Infrared Analysis, Inc., Anaheim, CA). Using propane as the reference spectrum with a relative response of 100, methane's response is approximately 10% of the same concentration of propane and hexane is 1.5 times the response of propane at the same concentration. The filter is set to the infrared region of the spectrum that corresponds to the infrared absorption of alkanes, primarily. Other hydrocarbons exhibit various degrees of absorption of infrared energy in this region as indicated in the Table.

The infrared video images were recorded on digital tape recorder. A digital camera was used to document the components being observed with the infrared camera.

**Table I - Relative Response of Hydrocarbon with LSI Infrared Imaging Camera**

Compound	Relative Response Propane =100%
Methane	9
Ethane	43
Propane	100
Butane	118
Iso-Butane	137
Pentane	143
Hexane	155
Heptane	157
Octane	136

Compound	Relative Response Propane =100%
Ethylene	3
Propylene	20
Iso Butylene	37
2 Methyl 2 Butane	4
1 Pentene	7
2 Methyl 2 Pentene	7
Benzene	4
Toluene	21
o-Xylene	38
p-Xylene	23
m-Xylene	32

File Descriptions			Barge #	Description
SnapShot	Named	Unnamed		
L000	Video 000	NN000	A1	Two Large Valve Settings Towards Aft Side
L001	Video 001	NN001	A2	Vent Stack at Bow of Barge
L002	Video 002	NN002	A3	Vent Stack at Bow of Barge
L003	Video 003	NN003	A4	Top Loading Hatches
L004	Video 004	NN004	A5	Top Loading Hatches at Placid Refinery
L005	Video 005	NN005	A6	Top Loading Hatches to the Aft of Barge
L006	Video 006	NN006	A7	Top Loading Hatches at Bow of Barge
L007	Video 007	NN007	A8	Top Loading Hatches at Bow of Barge
L008	Video 008	NN008	A9	Top Loading Hatches at Bow of Barge
L009	Video 009	NN009	A10	Top Loading Hatch at Bow of Barge
L010	Video 010	NN010	A11	Top Loading Hatches and Vent
L011	Video 011	NN011	A12	Top Loading Hatches at Aft side of Barge at Placid Refinery
L012	Video 012	NN012	A13	Top Hatches on Barge
L013	Video 013	NN013	A14	Top Hatches on Barge
L014	Video 014	NN014	A15	Top Hatches and Vent Stack on Barge
			A16	Top Hatches and Vent Stack on Barge
			A17	Top Hatches on Barge
			A11	Top Hatches on Barge
L015	Video 015	NN015	A18	Vent Stack on Barge
L016	Video 016	NN016	A4	Repeat of Video 003, Boarded by Bagging Team
L017	Video 017	NN017	A19	Top Loading Hatches at Placid Refinery
L018a	Video 018a	NN018a	A20	Top Hatches on Barge
L018b	Video 018b	NN018b	A21	Top Hatches on Barge
L018c	Video 018c	NN018c	A22	Top Hatches on Barge
L019	Video 019	NN019	A13	Top Hatches at TT Barge Cleaning Facility Refilm
			A14	Top Hatches at TT Barge Cleaning Facility
L020	Video 020	NN020	A23	Vent Stack on Barge Refilm

File Descriptions			Barge #	Description
SnapShot	Named	Unnamed		
			A24	Vent Stack on Barge
L021	Video 021	NN021	A25	Hatches at Aft Side in Intercoastal Canal
			A26	Vent at Aft Side in Intercoastal Canal
L022a	Video 022a	NN022a	A27	Vent at Aft Side
L022b	Video 022b	NN022b	A28	Vent Stack on Bow of Barge
L023a	Video 023a	NN023a	A29	Center Vent on Barge
L023b	Video 023b	NN023b	A30	Cent Hatch on Barge
L024	Video 024	NN024	A31	Bow Hatch and Deck Hatch on Barge
L025	Video 025	NN025	A32	Two Aft Hatches and one Side Hatch
L026	Video 026	NN026	A33	Top Hatches on Barge in Intercoastal Canal
L027	Video 027	NN027	A34	Vent Stack in Center of Barge in Intercoastal Canal
L028	Video 028	NN028	A1	Vent Stack on Bow of Barge Refilm
L029	Video 029	NN029	A35	Vent Stack on Bow of Barge
L030	Video 030	NN030	A36	Vent Stack on Bow of Barge Refilm
L031a	Video 031a	NN031a	A37	Top Hatches on Barge Across from Locks
L031b	Video 031b	NN031b	A31	Top Hatches on Bow Across from Locks
L032	Video 032	NN032	A23	Vent at the Bow of Barge North of Locks
L033	Video 033	NN033	A38	Forward Bow Hatch on Barge in Intercoastal Canal

## **Conclusion**

The LSI crew was able to find a total of 40 barges leaking from either hatches or vents during the survey. It is in LSI's opinion that the major source of emissions for the barges came from the hatches and vents. These hatch leaks were very common amongst the various barges we surveyed. Had there been any sizable leaks on the barges, the Hawk Leak Detection System would have seen them.

I would also like to take this opportunity to thank you for allowing our leak survey crews to conduct the survey on your pipeline. We would like to have the opportunity to bid on future jobs whether it is aerial or ground level. We have the most experienced IR crews in the industry. If we can be of further assistance please do not hesitate to contact me.

David Furry  
President -LSI  
P.O. Box 3066  
Early, Texas 76803



## **APPENDIX B**

LSI Aerial PGIE Images

## **APPENDIX B: LSI Aerial PGIE Images**

The following appendix contains a selection of screen shots from the LSI airborne portion of the BEM 1 study conducted in Baton Rouge LA September 24<sup>th</sup> through October 1<sup>st</sup> 2008.



Figure B-1. Leak from Barge A12



Figure B-2. Leak from Barge A13



Figure B-3. Leak from Barge A14

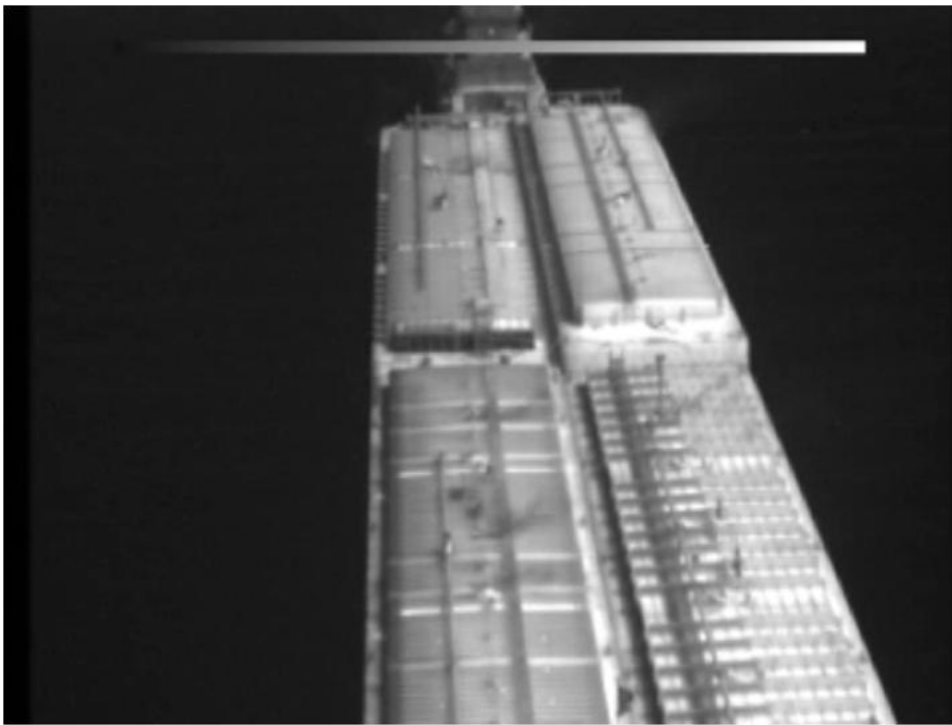


Figure B-4. Leak from Barge A15

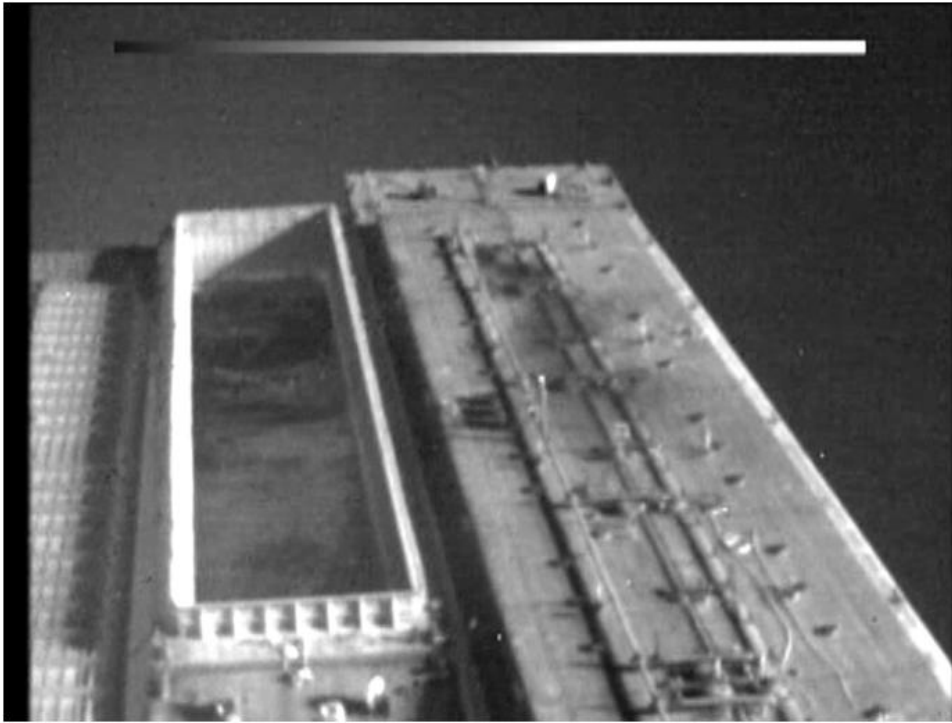


Figure B-5. Leak from Barge A18



Figure B-6. Leak from Barge A19

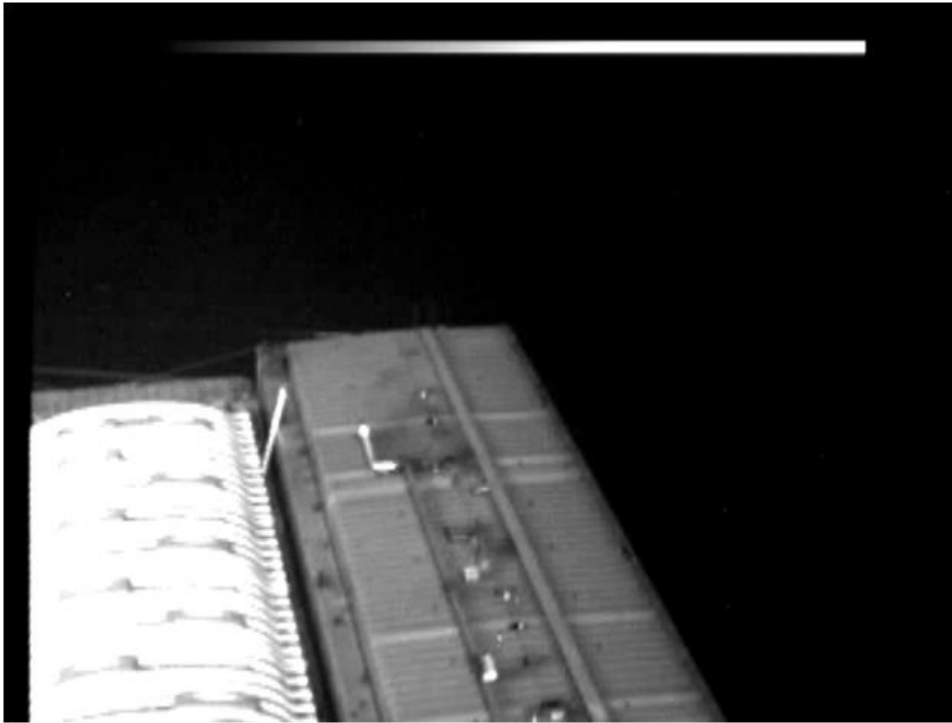


Figure B-7. Leak from Barge A22



Figure B-8. Leak from Barge A13



Figure B-9. Leak from Barge A23

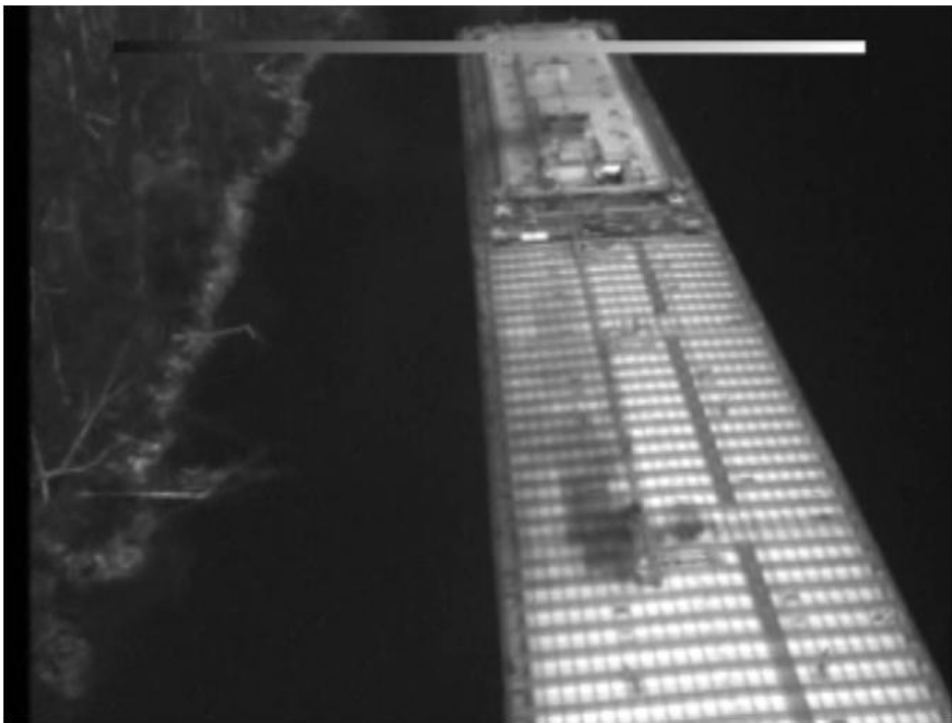


Figure B-10. Leak from Barge A25

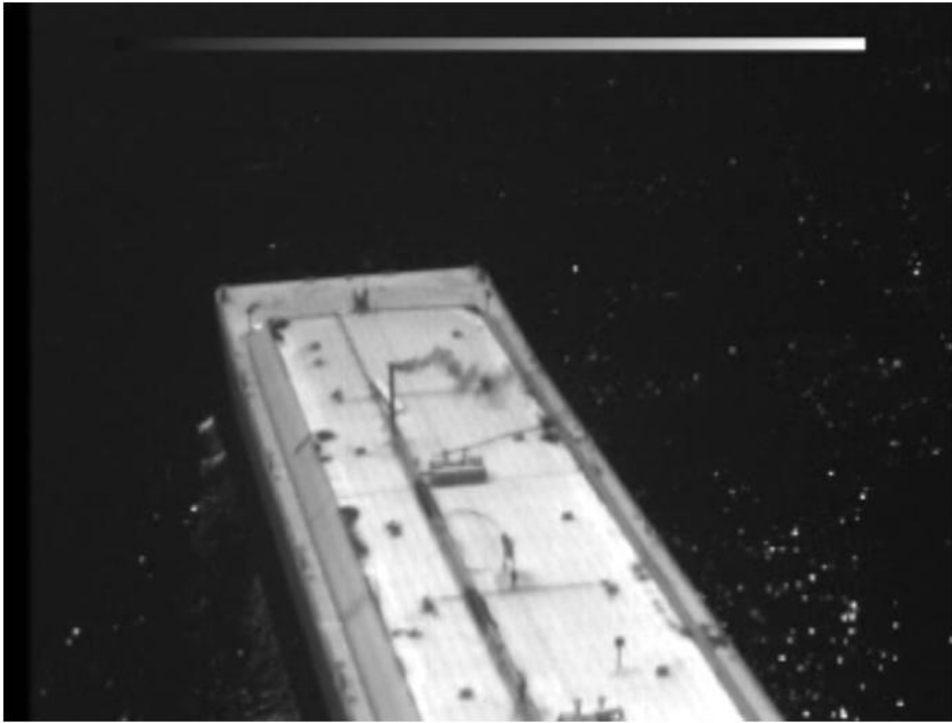


Figure B-11. Leak from Barge A27



Figure B-12. Leak from Barge A29



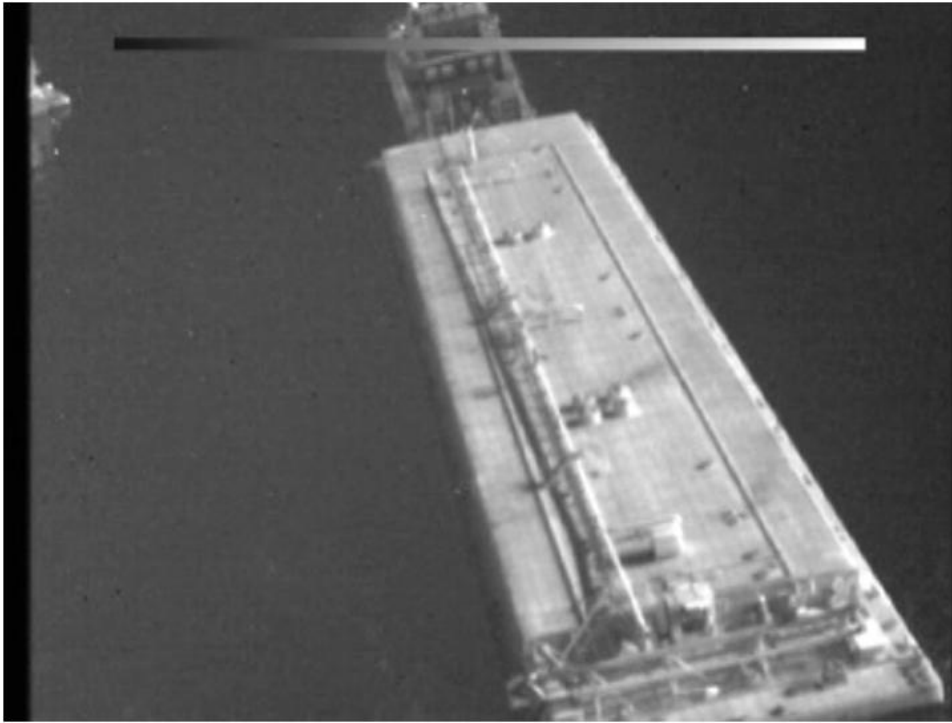


Figure B-13. Leak from Barge A31



Figure B-14. Leak from Barge A32



Figure B-15. Leak from Barge A34

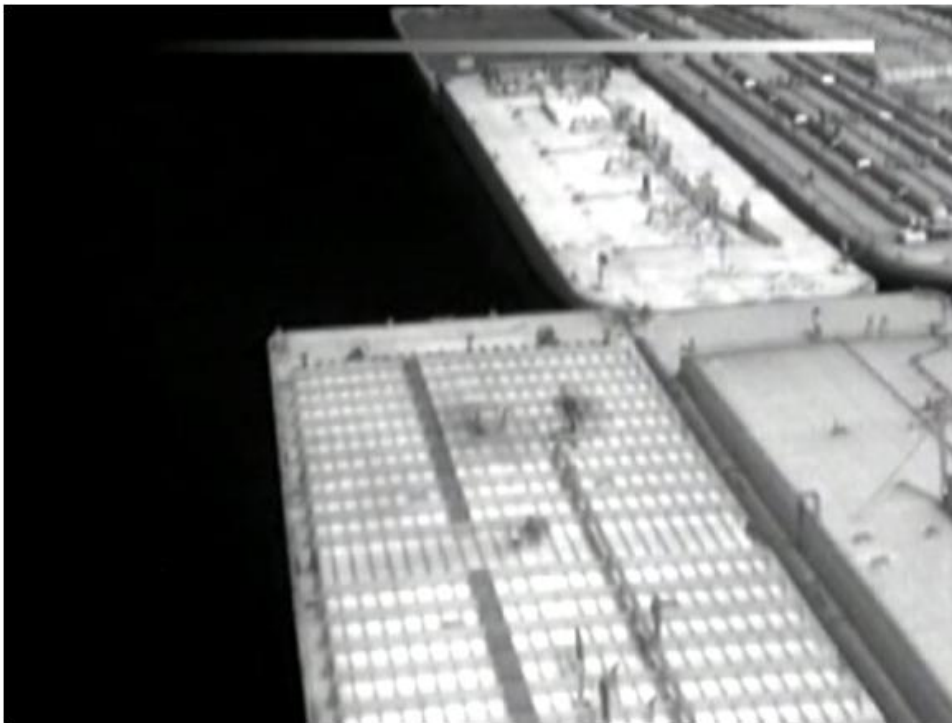


Figure B-16. Leak from Barge A1

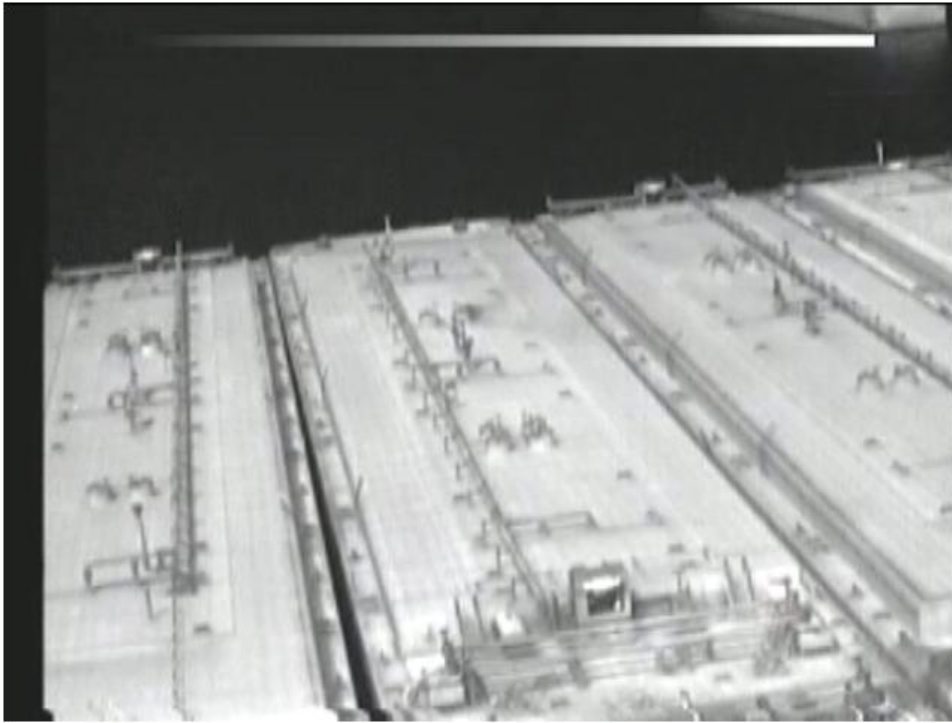


Figure B-17. Leak from Barge A36



Figure B-18. Leak from Barge A37

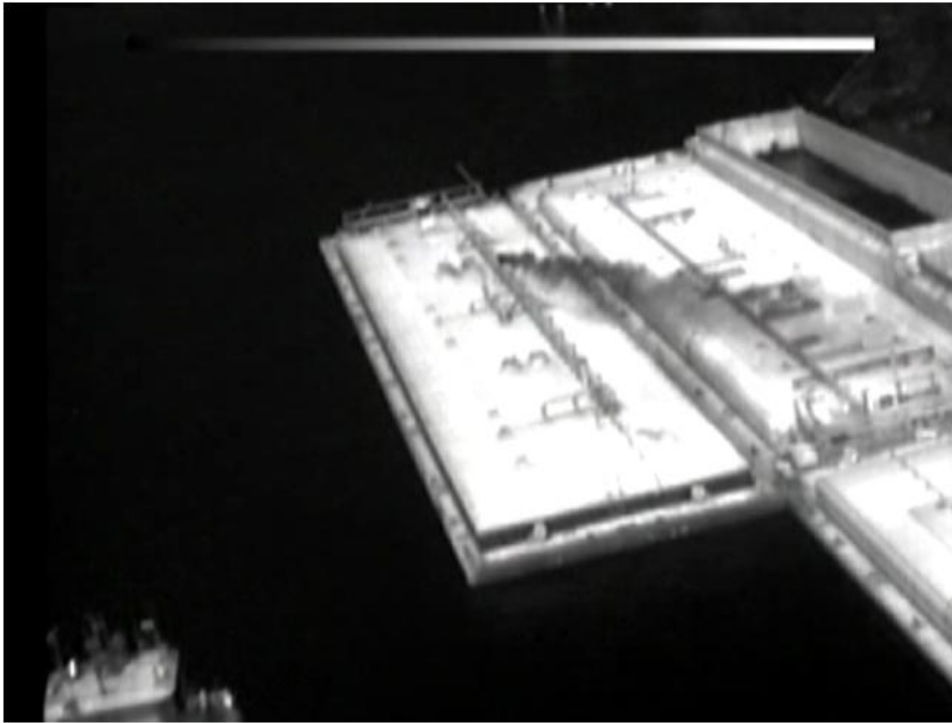


Figure B-19. Leak from Barge A31



Figure B-20. Leak from Barge A23

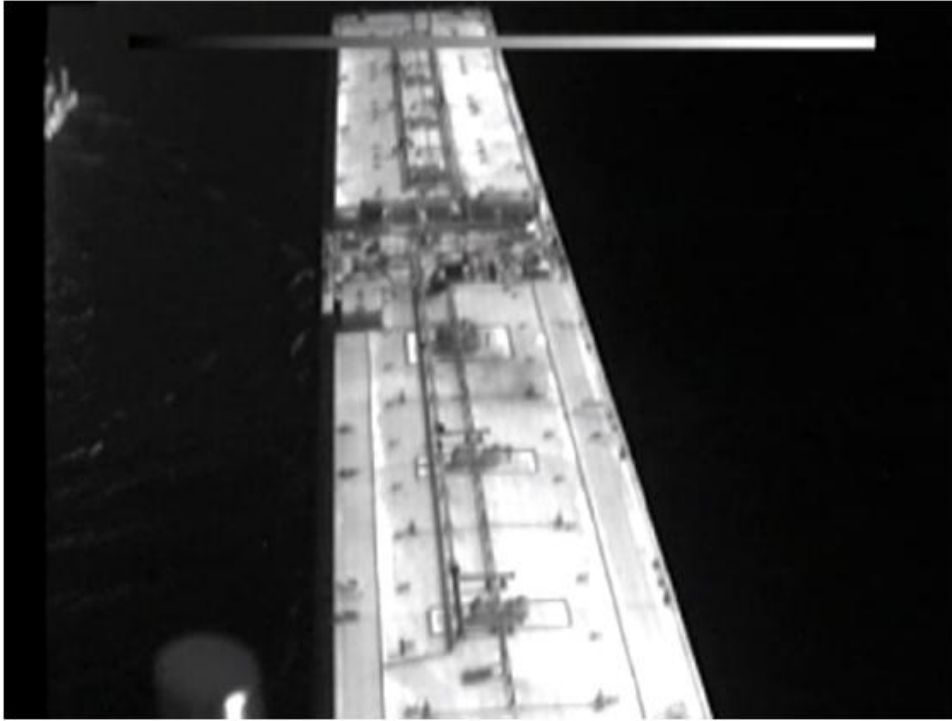


Figure B-21. Leak from Barge A12

## **APPENDIX C**

LSI Report: Leak Detection using LSI Infrared Gas Imaging, BEM 1  
Barge Study; Ground Crew Survey (October 21, 2008)



**Report:**  
**Leak Detection using**  
**LSI Infrared Gas**  
**Imaging**

**BEM1 Barge Study**  
**Ground Crew Survey**

David Furry, President, LSI  
Date: October 21, 2008

## **Executive Summary**

Leak Surveys Inc. (Early, TX) was commissioned by ARCADIS to conduct a leak survey at the Baton Rouge locks and on various barges as part of the BEM1 Project. The optical imaging survey looked at various components within each of these processes. The optical imaging leak (smart LDAR) survey was conducted on September 24<sup>th</sup>-30<sup>th</sup>, 2008. The Hawk Leak Detection System visualized numerous hydrocarbon gas leaks on various components.

Kevin McGinnis, a Leak Surveys' technician, performed the leak survey.

## **Background**

Leak Surveys Inc. is an international company with 4-½ years experience using the Hawk Leak Detection System (HLDS). LSI developed the HLDS after 12 years of research and development on optical imaging and has applied for international patents.

LSI and the API committee introduced using optical imaging to conduct surveys in refinery and chemical plants on a commercial basis to the industry in February of 2004.

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The human eye more readily perceives motion than contrast. Movie or real time images are used as the basis for leak detection in the data presented here. Image quality is affected by the temperature and emissivity difference between the gas cloud and the background.

At this point, no infrared gas imaging cameras are capable of providing quantitative measurements of gas concentration, however, studies funded by the American Petroleum Institute that shows the detection limits accomplished by passive gas imaging systems are within the bounds necessary for equivalent detection of leaks at less than 10,000 ppm (60 g/hr). With 2 plus years of leak surveying experience LSI staff has a library of known gas leak quantifications. We have the ability to compare images of known leak amounts to images taken in the field and estimate the total gas quantity. This is only an estimate of the total leak and does not take into consideration any diluted streams. Again we can only estimate and the volumes are for information purposes only.

Gas imaging provides the user with a real time achievable record of leaking components as well as providing specific locations of leaks within a component.



## Camera Description

The infrared gas imaging camera used by Leak Surveys, Inc., consists of a modified Indigo (FLIR/Indigo Systems Corp., Goleta CA) GasfindIR MID camera with a nominal spectra range of 1- 5.4  $\mu\text{m}$ . Using a 30 x 30  $\text{m}$  InSb detector with a 320 x 240 pixel array, the camera has capabilities of varying the integration times from 5  $\mu\text{s}$  to 16.5 ms. The detector is operated at near liquid nitrogen temperatures using an integral Stirling cooler which provides the system with an NE $\Delta$ T of no more than an 18 mK providing excellent sensitivity.

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Various lens including a 25 mm, a 50 mm and a 100 mm lens were used during the experiments. The 25 mm lens provides a 22 x 16 degrees field of view with an f-number of 2.3. The 50 mm lens provides an 11 x 8 degrees field of view with an f-number of 2.3.

The use of a narrow band pass filter provides spectral discrimination that allows the detection of compounds that have a vibration mode in the infrared region of the filter. Not all hydrocarbons have infrared absorptions within the filter range. Table I (below) shows the theoretical relative response of various compounds of interest using 1  $\text{cm}^{-1}$  resolution infrared spectra (Infrared Analysis, Inc., Anaheim, CA). Using propane as the reference spectrum with a relative response of 100, methane's response is approximately 10% of the same concentration of propane and hexane is 1.5 times the response of propane at the same concentration. The filter is set to the infrared region of the spectrum that corresponds to the infrared absorption of alkanes, primarily. Other hydrocarbons exhibit various degrees of absorption of infrared energy in this region as indicated in the Table.

The infrared video images were recorded on digital hard drive. A digital camera was used to document the components being observed with the infrared camera.

**Table I - Relative Response of Hydrocarbon with LSI Infrared Imaging Camera**

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<b>Compound</b>	<b>Relative Response Propane =100%</b>
Ethylene	3
Propylene	20
Iso Butylene	37
2 Methyl 2 Butane	4
1 Pentene	7
2 Methyl 2 Pentene	7
Benzene	4
Toluene	21
o-Xylene	38
p-Xylene	23
m-Xylene	32

**Areas Examined**

Below is a list of the areas surveyed relative to their location and the source of the leaking emission. All data shown below was taken directly off the field notes of the LSI technicians.

**BEM1 Barge Study**

<b>File</b>	<b>Date</b>	<b>Process</b>	<b>Part Leaking</b>	<b>Barge #</b>	<b>Description of Leak</b>
000	9/24/2008	BEM1 Barge Study	Hatch	L1	N/A
001	9/24/2008	BEM1 Barge Study	Hatch	L1	N/A
002	9/24/2008	BEM1 Barge Study	Hatch	L1	N/A
003	9/24/2008	BEM1 Barge Study	Hatch	L1	N/A
004	9/24/2008	BEM1 Barge Study	Hatch	L1	N/A
005	9/24/2008	BEM1 Barge Study	Hatch	L1	N/A
006	9/24/2008	BEM1 Barge Study	Hatch	L1	N/A

File	Date	Process	Part Leaking	Barge #	Description of Leak
007	9/24/2008	BEM1 Barge Study	Hatch	G1	N/A
008	9/24/2008	BEM1 Barge Study	Hatch	G1	N/A
009	9/24/2008	BEM1 Barge Study	Hatch	G1	N/A
010	9/24/2008	BEM1 Barge Study	Hatch	G1	N/A
011	9/24/2008	BEM1 Barge Study	Hatch	G1	N/A
012	9/24/2008	BEM1 Barge Study	Hatch	G1	N/A
013	9/24/2008	BEM1 Barge Study	Hatch	G1	N/A
014	9/24/2008	BEM1 Barge Study	Hatch	G1	N/A
015	9/25/2008	BEM1 Barge Study	Ullage Hatch	G2	#2 Port Lower
016	9/25/2008	BEM1 Barge Study	Cargo Hatch	G2	#2 Port
017	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#2 Starboard Middle
018	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#2 Port Middle
019	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#1 Starboard Lower
020	9/25/2008	BEM1 Barge Study	Alarm Test Rod	G2	#2 Starboard
021	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#1 Port Lower
022	9/25/2008	BEM1 Barge Study	Alarm Test Rod	G2	#2 Port
023	9/25/2008	BEM1 Barge Study	Cargo Hatch	G2	#1 Starboard
024	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#1 Starboard Middle
025	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#1 Port Middle
026	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#1 Starboard Upper

File	Date	Process	Part Leaking	Barge #	Description of Leak
027	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#1 Port Upper
028	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G2	#2 Port Lower
029	9/25/2008	BEM1 Barge Study	Overview of Leaks	G2	N/A
030	9/25/2008	BEM1 Barge Study	Bagging Process		Showing Gas Venting Through Dry Gas Meter
031	9/25/2008	BEM1 Barge Study	Vent	G3	N/A
032	9/25/2008	BEM1 Barge Study	Pressure Relief Valve	G3	N/A
033	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G3	#1 Port Forward
034	9/25/2008	BEM1 Barge Study	Ullage Hatch	G3	N/A
035	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G3	#1 Port Aft
036	9/25/2005	BEM1 Barge Study	Cargo Hatch Control Valve	G3	N/A
037	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G3	#2 Starboard Forward
038	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G3	#2 Port Forward
039	9/25/2008	BEM1 Barge Study	Cargo Hatch Control Valve	G3	N/A
040	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G3	#3 Starboard Forward
041	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G3	#3 Port Forward
042	9/25/2008	BEM1 Barge Study	Butterworth Hatch	G3	#3 Port Aft
043	9/25/2008	BEM1 Barge Study	Cargo Hatch Control Valve	G3	N/A
044	9/26/2008	BEM1 Barge Study	Ullage Hatch	G4	#1 Port & #1 Starboard
045	9/26/2008	BEM1 Barge Study	Both Hatches & Valve	G4	#2 Port
046	9/26/2008	BEM1 Barge Study	Both Hatches & Valve	G4	#2 Starboard

File	Date	Process	Part Leaking	Barge #	Description of Leak
047	9/26/2008	BEM1 Barge Study	Ullage & Cargo Hatches	G4	#3 Starboard
048	9/26/2008	BEM1 Barge Study	Cargo Hatch Control Valve	G4	#3 Port
049	9/26/2008	BEM1 Barge Study	Alarm Test Rod	G5	#1 Starboard
050	9/26/2008	BEM1 Barge Study	Ullage Hatch	G5	#1 Starboard
051	9/26/2008	BEM1 Barge Study	Ullage Hatch & Valve	G5	#1 Port
052	9/26/2008	BEM1 Barge Study	Ullage Hatch	G5	#2 Port
053	9/26/2008	BEM1 Barge Study	Ullage & Cargo Hatches	G5	#2 Starboard
054	9/26/2008	BEM1 Barge Study	Ullage & Cargo Hatches	G5	#3 Starboard
055	9/26/2008	BEM1 Barge Study	Ullage Hatch	G5	#3 Port
056	9/26/2008	BEM1 Barge Study	Alarm Test Rod	G5	#3 Starboard
057	9/26/2008	BEM1 Barge Study	Same as Video 045	G4	Filmed Again After Repair Attempt
058	9/26/2008	BEM1 Barge Study	Same as Video 047	G4	Filmed Again After Repair Attempt
059	9/27/2008	BEM1 Barge Study	Vent	G6	N/A
060	9/27/2008	BEM1 Barge Study	Cofferdam Hatch	G6	Forward
061	9/27/2008	BEM1 Barge Study	Cargo Hatch	G6	#3 Port
062	9/27/2008	BEM1 Barge Study	Cargo Hatch	G6	#3 Starboard
063	9/27/2008	BEM1 Barge Study	Ullage Hatch	G6	#4 Port
064	9/27/2008	BEM1 Barge Study	Ullage Hatch	G6	#4 Starboard
065	9/27/2008	BEM1 Barge Study	Cargo Hatch	G6	#4 Starboard
066	9/27/2008	BEM1 Barge Study	Same as Video 063	G6	Filmed Again

File	Date	Process	Part Leaking	Barge #	Description of Leak
067	9/27/2008	BEM1 Barge Study	Same as Video 063	G6	Filmed Again After Vent Was Closed
068	9/27/2008	BEM1 Barge Study	Same as Video 063	G6	Filmed Again After Vent Was Closed
069	9/28/2008	BEM1 Barge Study	Overview of Leaks	G7	Overview of #2 & #3 Cargo Hatches
070	9/28/2008	BEM1 Barge Study	Cargo Hatch	G7	#2 Port
071	9/28/2008	BEM1 Barge Study	Cargo Hatch	G7	#2 Starboard
072	9/28/2008	BEM1 Barge Study	Cargo Hatch	G7	#3 Starboard
073	9/28/2008	BEM1 Barge Study	Cargo Hatch	G7	#3 Port
074	9/28/2008	BEM1 Barge Study	Same as Video 71	G7	Filmed Again With Bag On
075	9/28/2008	BEM1 Barge Study	Pressure Relief Valve	G7	N/A
076	9/28/2008	BEM1 Barge Study	Overview of Leaks	G7	Another Overview of #2 & #3 Cargo Hatches
077	9/28/2008	BEM1 Barge Study	Cargo Hatch	L4	#3 Starboard
078	9/28/2008	BEM1 Barge Study	Alarm Test Rod	L4	#3 Port
079	9/28/2008	BEM1 Barge Study	Cargo Hatch	L4	#2 Port
080	9/28/2008	BEM1 Barge Study	Ullage Hatch	L4	#2 Port
081	9/28/2008	BEM1 Barge Study	Ullage Hatch	L4	#2 Starboard
082	9/28/2008	BEM1 Barge Study	Cargo Hatch	L4	#1 Starboard
083	9/28/2008	BEM1 Barge Study	Cargo Hatch	L4	#1 Port
084	9/28/2008	BEM1 Barge Study	Vent	L4	N/A
085	9/28/2008	BEM1 Barge Study	Ullage Hatch	L4	#1 Port
086	9/28/2008	BEM1 Barge Study	Ullage Hatch	L4	#1 Starboard

<b>File</b>	<b>Date</b>	<b>Process</b>	<b>Part Leaking</b>	<b>Barge #</b>	<b>Description of Leak</b>
087	9/28/2008	BEM1 Barge Study	Pressure Relief Valve	G8	N/A
088	9/28/2008	BEM1 Barge Study	Cargo Hatch	G8	#2 Port
089	9/28/2008	BEM1 Barge Study	Cargo Hatch Control Valve	G8	#2 Port
090	9/28/2008	BEM1 Barge Study	Control Valve Grease Cert	G8	#2 Starboard
091	9/28/2008	BEM1 Barge Study	Hatch & Control Valve	G8	#3 Starboard
092	9/28/2008	BEM1 Barge Study	Hatch & Control Valve	G8	#3 Port
093	9/28/2008	BEM1 Barge Study	Overview of Leaks	G8	Overview of Videos 87 thru 92
094	9/28/2008	BEM1 Barge Study	Block Valve	G8	#3
095	9/28/2008	BEM1 Barge Study	Butterworth Hatch	G8	#3 Port Rear
096	9/28/2008	BEM1 Barge Study	Butterworth Hatch	G8	#3 Starboard Rear
097	9/28/2008	BEM1 Barge Study	Slop Tank Vent	G8	N/A
098	9/28/2008	BEM1 Barge Study	Master Suction Valve	G8	N/A
099	9/28/2008	BEM1 Barge Study	Butterworth Hatch	G8	#2 Port Forward
100	9/28/2008	BEM1 Barge Study	Cargo Hatch	G8	#1 Port
101	9/28/2008	BEM1 Barge Study	Cargo Hatch Control Valve	G8	#1 Port
102	9/28/2008	BEM1 Barge Study	Cargo Hatch Control Valve	G8	#1 Starboard
103	9/28/2008	BEM1 Barge Study	Slop Tank Hatch	G8	N/A
104	9/29/2008	BEM1 Barge Study	Cargo Hatch	L5	#1 Port
105	9/29/2008	BEM1 Barge Study	Cargo Hatch	L5	#2 Port & #3 Starboard
106	9/29/2008	BEM1 Barge Study	Hatch & Pressure Valve	L6	#3 Port & Pressure Relief Valve

<b>File</b>	<b>Date</b>	<b>Process</b>	<b>Part Leaking</b>	<b>Barge #</b>	<b>Description of Leak</b>
107	9/29/2008	BEM1 Barge Study	Butterworth & Cargo	L6	#2 Starboard Forward & #1 Starboard
108	9/29/2008	BEM1 Barge Study	Butterworth Hatch	L6	#1 Starboard Middle
109	9/29/2008	BEM1 Barge Study	Cargo Hatch	L7	#3 Starboard
110	9/30/2008	BEM1 Barge Study	Hatch & Pressure Valve	L8	Pressure Relief Valve & #2 Starboard
111	9/30/2008	BEM1 Barge Study	Slop Tank Vent	L9	N/A

### **Conclusion**

The LSI technician found and recorded a total of 112 videos during the seven-day survey.

I would also like to take this opportunity to thank you for allowing our leak survey crews to conduct the survey in your facility. If we can be of further assistance please do not hesitate to contact me.

David Furry  
 President –LSI  
 P.O. Box 3066  
 Early, Texas 76803



## **APPENDIX D**

LSI Ground Survey PGIE Images

## **APPENDIX D: LSI Ground Survey PGIE Images**

The following appendix contains a selection of screen shots from the LSI ground survey portion of the BEM 1 study conducted in Baton Rouge LA September 24<sup>th</sup> through September 30<sup>th</sup> 2008.



Figure D-1. Leak from Barge L1 (captured while barge in lock)



Figure D-2. Leak from Barge L1 (captured while barge in lock)

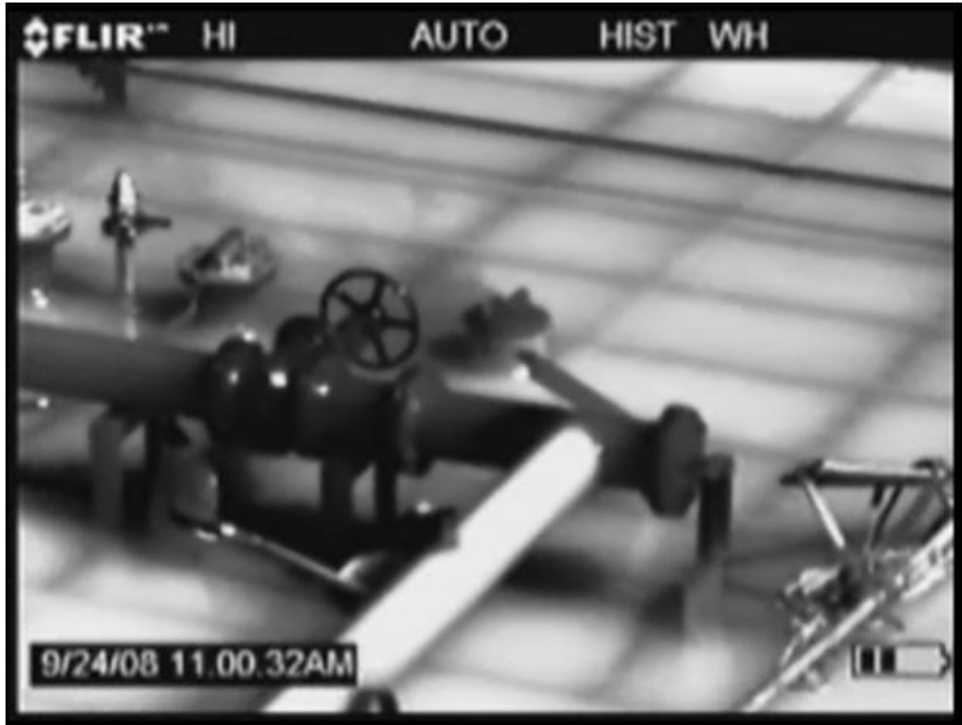


Figure D-3. Leak from Barge L2 (captured while barge in lock)



Figure D-4. Leak from Barge G1 (captured while onboard barge)



Figure D-5. Leak from Barge G1 (captured while onboard barge)



Figure D-6. Leak from Barge G2 (captured while onboard barge)



Figure D-7. Leak from Barge G2 (captured while onboard barge)



Figure D-8. Leak from Barge G2 (captured while onboard barge)



Figure D-9. Leak from Barge G2 (captured while onboard barge)



Figure D-10. Leak from Barge G2 (captured while onboard barge)



Figure D-11. Leak from Barge G2 (captured while onboard barge)



Figure D-12. Leak from Barge G3 (captured while onboard barge)





Figure D-13. Leak from Barge G3 (captured while onboard barge)



Figure D-14. Leak from Barge G3 (captured while onboard barge)



Figure D-15. Leak from Barge G3 (captured while onboard barge)



Figure D-16. Leak from Barge G3 (captured while onboard barge)



Figure D-17. Leak from Barge G5 (captured while onboard barge)



Figure D-18. Leak from Barge G5 (captured while onboard barge)



Figure D-19. Leak from Barge G6 (captured while onboard barge)

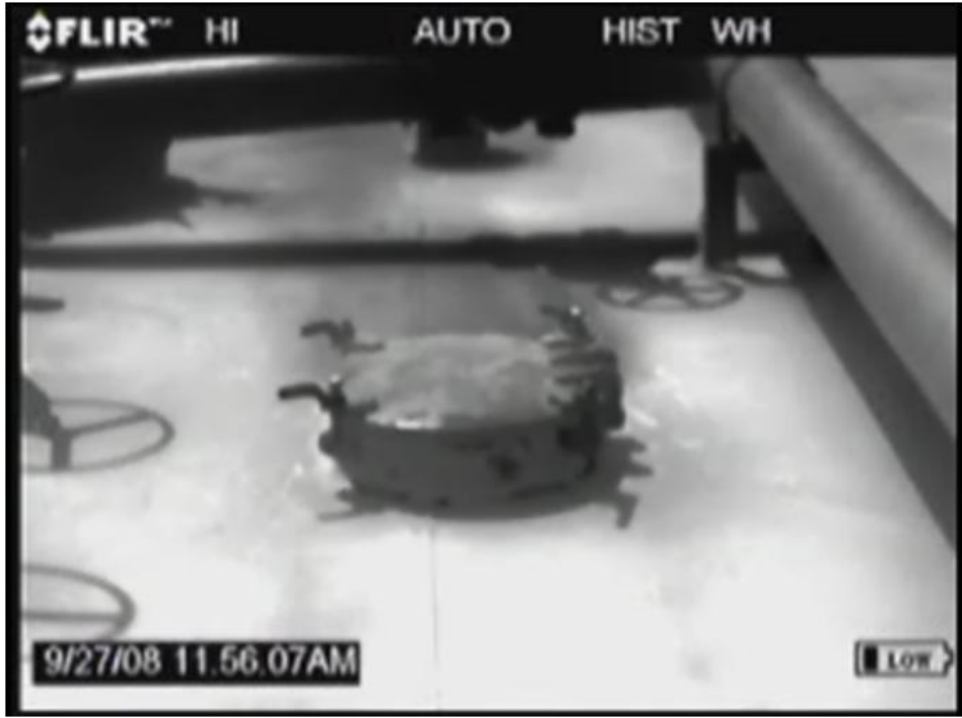


Figure D-20. Leak from Barge G6 (captured while onboard barge)



Figure D-21. Leak from Barge G6 (captured while onboard barge)



Figure D-22. Leak from Barge G6 (captured while onboard barge)

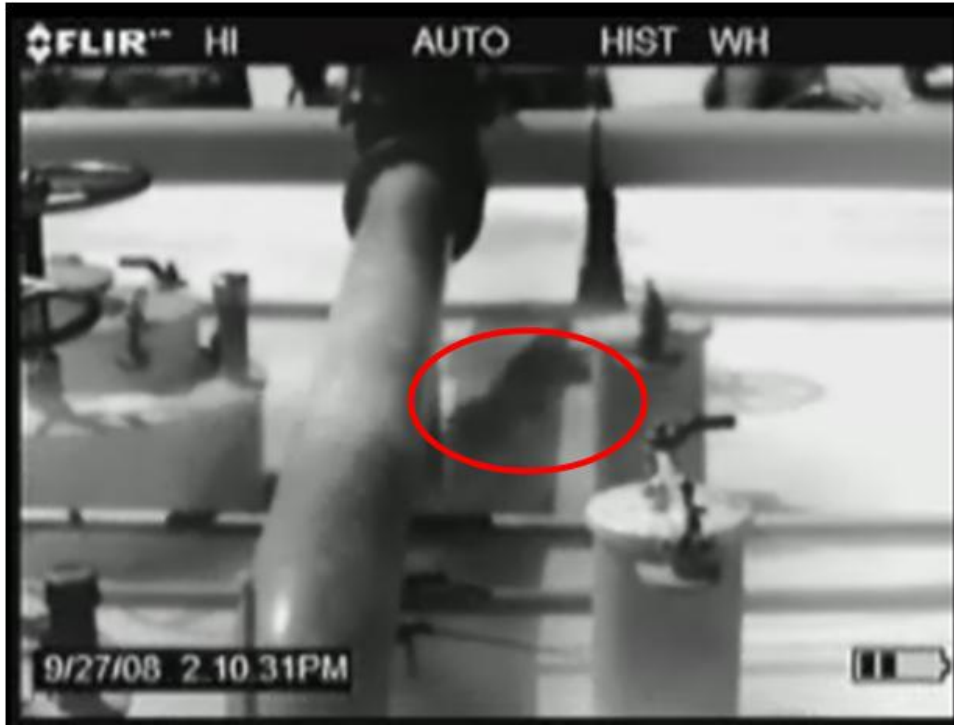


Figure D-23. Leak from Barge G6 (captured while onboard barge)



Figure D-24. Leak from Barge G7 (captured while onboard barge)





Figure D-25. Leak from Barge G7 (captured while onboard barge)



Figure D-26. Leak from Barge G7 (captured while onboard barge)



Figure D-27. Leak from Barge G8 (captured while onboard barge)



Figure D-28. Leak from Barge G8 (captured while onboard barge)





Figure D-29. Leak from Barge G8 (captured while onboard barge)



Figure D-30. Leak from Barge G8 (captured while onboard barge)



Figure D-31. Leak from Barge G8 (captured while onboard barge)



Figure D-32. Leak from Barge G8 (captured while onboard barge)



Figure D-33. Leak from Barge G8 (captured while onboard barge)



Figure D-34. Leak from Barge G8 (captured while onboard barge)



Figure D-35. Leak from Barge G8 (captured while onboard barge)



Figure D-36. Leak from Barge G8 (captured while onboard barge)



Figure D-37. Leak from Barge G8 (captured while onboard barge)



Figure D-38. Leak from Barge G8 (captured while onboard barge)

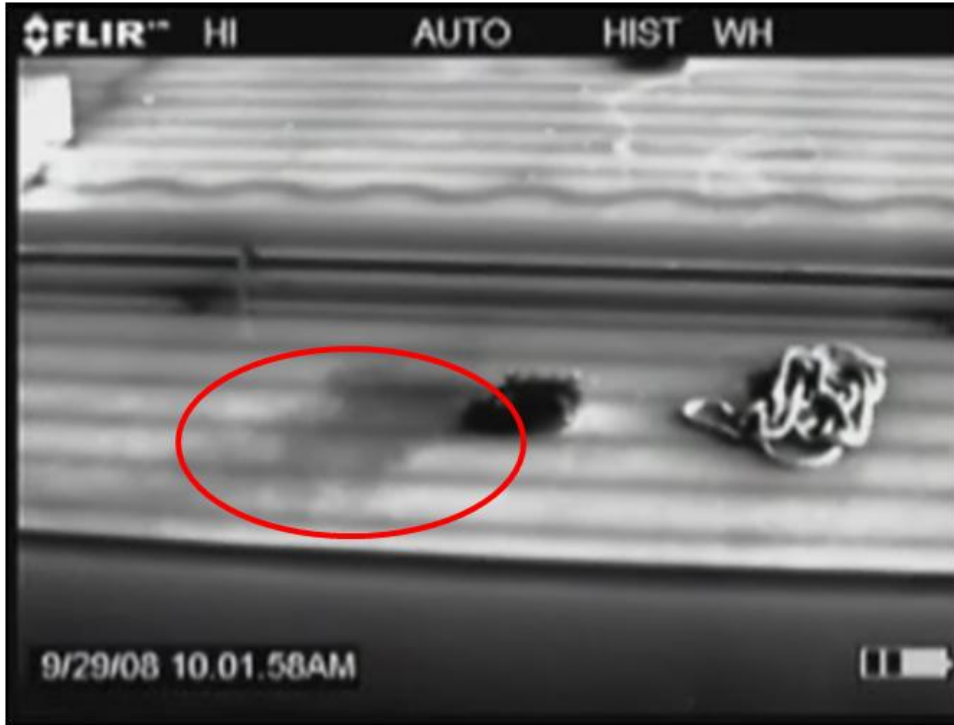


Figure D-39. Leak from Barge L6 (captured while barge in lock)



Figure D-40. Leak from Barge L6 (captured while barge in lock)



Figure D-41. Leak from Barge L8 (captured while barge in lock)

## **APPENDIX E**

LDEQ/ARCADIS Lock Wall PGIE Images



## **APPENDIX E: LDEQ/ARCADIS Lock Wall PGIE Images**

The following appendix contains a selection of screen shots from the Port Allen Lock wall survey portion of the portion of the BEM 1 study conducted in Baton Rouge LA September 24<sup>th</sup> through October 9<sup>th</sup>, 2008 using the LDEQ FLIR camera. These images were acquired by LDEQ and ARCADIS.



Figure E-1. Leak from Hatch 9/28



Figure E-2. Leak from Hatch 9/28



Figure E-3. Leak from Hatch 10/1

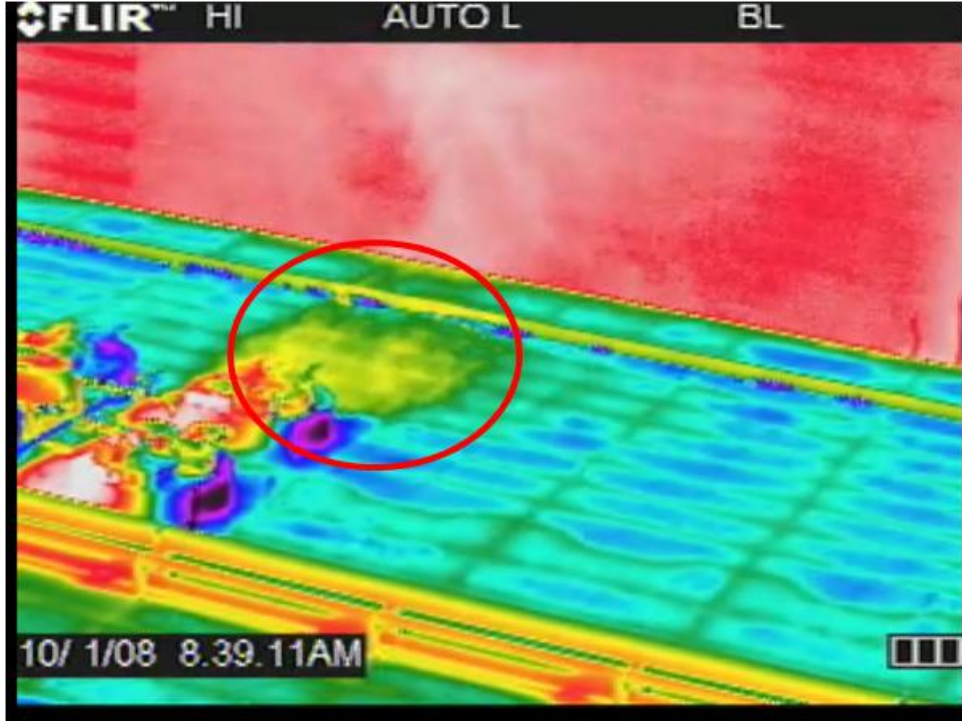


Figure E-4. Leak from Hatch 10/1



Figure E-5. Leak from Hatch 10/1



Figure E-6. Leak from Hatch 10/1



Figure E-7. Leak from Hatch 10/2

Figure E-8. Leak from Hatch 10/2





Figure E-11. Leak from Valve 10/2



Figure E-12. Leak from Hatches 10/2





Figure E-13. Leak from Hatches 10/2



Figure E-14. Leak from Valves 10/5





Figure E-15. Leak from Pipes 10/5



Figure E-16. Leak from Pipes 10/8



Figure E-17. Leak from Hatches 10/9

## **APPENDIX F**

Alkane Mixture (AM) Measurement by OP-FTIR

## APPENDIX F: Alkane Mixture (AM) Measurement by OP-FTIR

Emissions from fugitive or area sources containing fuel-based hydrocarbon mixtures can be estimated using EPA Method OTM 10 with OP-FITR by quantifying the infrared absorbance of the alkane mixture (AM) in the C-H stretch infrared vibration region around  $2950\text{ cm}^{-1}$ . If some species of hydrocarbons are present at concentrations above the MDL for the OP-FTIR, they can be quantified individually in separate spectral regions using standard procedures.

This appendix describes the AM procedure to convert OP-FTIR volume-concentration determinations of alkane mixtures that originate from fuels to mass concentrations. The use of OTM 10 for the purpose of determination of emission fluxes and/or emission rates requires the conversion of the volume path-integrated concentrations (VPIC) to mass path-integrated concentrations (MPICs). The conversion requires knowledge of the molecular mass of the target gas so the analytical method for determining the mean molecular mass of alkane mixtures by OP-FTIR is therefore described.

The shapes of the  $3.3\text{ }\mu\text{m}$  absorption bands of the individual components of alkane mixtures, butane (C-4) to decane (C-10) are similar to each other. Figure 1 shows the comparison of the absorption bands of the straight-chain alkanes C-4 to C-8 (n-butane to n-octane). Starting with C-4, the similarity is greatest between the components with consecutive carbon numbers (e.g. butane and pentane) and the similarities decrease for components with greater difference in carbon numbers (e.g. C-4 and C-8, butane and octane). The similarity in band shapes makes it impossible to include all of the components of the mixture in the classic least squares (CLS) regression fit of measured absorbance to calibrated reference absorbance spectra to determine the concentration of the individual compounds.

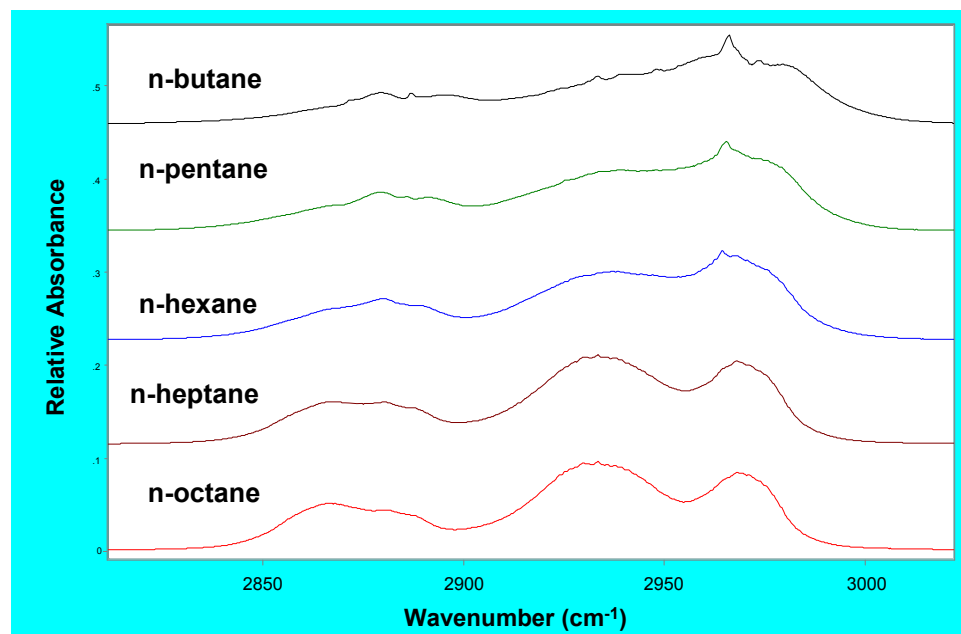


Figure F-1. Comparison of the Absorption Bands of Straight-chain Alkanes, C-4 (n-butane) to C-8 (n-octane), Measured with  $0.5\text{ cm}^{-1}$  Resolution

The AM method provides a direct measurement-based determination of the mean carbon number that is required in order to convert the VPIC of the mixture to MPIC values. We assume that the vapor emitted from the alkane mixture is mainly composed of C-4, C-5, C-6, C-7, C-8. The alkanes with carbon numbers less than 4 (methane, ethane and propane) are not expected to be components of the mixture because these species are gases at standard atmospheric conditions and if present upon manufacture, would have outgassed from the liquid fuel. Alkanes with higher carbon numbers than C-8 (nonane, decane, etc) have low vapor pressures and therefore would not be present in the vapor at significant levels for most applications of the measurement.

Additional information on this analysis and associated QA procedures can be found in SOP that follows.

**SOP TITLE:** PROCEDURE TO CONVERT OP-FTIR VOLUME-CONCENTRATION DETERMINATIONS OF ALKANE MIXTURE THAT ORIGINATE FROM PETROLEUM-BASE FUELS TO MASS CONCENTRATIONS.

**SCOPE:** Describes the Optical Remote Sensing (ORS) analytical method for determining the mean molecular mass of alkane mixtures that are emitted from petroleum-based fuels.

**PURPOSE:** Quantitative measurements by OP-FTIR of vapors and gases are determined as volume path-integrated concentrations (VPICs). The use of VRPM for the purpose of determination of emission fluxes and/or emission rates required the conversion of the VPIC to mass path-integrated concentrations (MPICs). The conversion requires knowledge of the molecular mass of the target gas.

## DEFINITIONS

Absolute Background      Absolute backgrounds are either zero-path or synthetic backgrounds and will contain little or no absorption features.

CLS      Classical Least Squares, regression fit of measured absorbance to calibrated reference absorbance spectra.

${}^m\hat{C}_{mix}$       Arbitrated mass path-integrated concentration of alkane mixture, usually with units of ppb·meter or ppm·meter. usually with units of mg/m<sup>2</sup> or g/m<sup>2</sup>.

${}^v\hat{C}_x^A$       Volume path-integrated concentration of alkane component, x, analyzed in regions A (A = LAL, HAL or arbitrated), usually with units of ppm·meter or ppb·meter.

HAL      High Alkane Level region of analysis, 2694.0 to 2915.7 cm<sup>-1</sup>. This region contains weaker bands of n-butane and n-octane and is the region of choice when the alkane concentrations are high enough to distort the strong bands.

LAL      Low Alkane Level region of analysis, 2004.2 to 3001.2 cm<sup>-1</sup>. This region contains the strong bands n-butane and n-octane bands, and is the region of choice for low concentration levels.

$\overline{M}_{mix}$       Mean molecular mass of the alkane mixture in units of g/mole

Relative Background      Background that was measured over the same path as the sample, single beams. These background spectra will produce absorbance spectra in which the atmospheric absorption bands will be wholly or nearly cancelled. In some cases these backgrounds may contain absorption features of the target species that may require correction.

## INTRODUCTION

The shapes of the 3.3  $\mu\text{m}$  absorption bands of the individual components of alkane mixtures, butane (C-4) to decane (C-10) are similar to each other. Figure 1 shows the comparison of the absorption bands of the straight-chain alkanes C-4 to C-8 (n-butane to n-octane). Starting with C-4, the similarity is greatest between the components with consecutive carbon numbers (e.g. butane and pentane) and the similarities decrease for components with greater difference in carbon numbers (e.g. C-4 and C-8, butane and octane). The similarity in band shapes makes it impossible to include all of the components of the mixture in the CLS analysis. The CLS multi-component regression analysis requires that the absorption bands of the co-analyzed species do not correlate, i.e. the band shapes of the components are not too similar. When the bands of two or more co-analyzed species correlate, the respective concentration determinations become unreliable.

For the past twenty years, the analysis of alkane mixtures has been performed using a surrogate to represent the total volume concentration of the entire mixture. The surrogate species was often n-octane, but in some cases another alkane was chosen because its band had a better fit to the shape of the mixture band. However this method results in a volume concentration and to convert to mass concentration, one had to estimate (or guess) the mean carbon number of the mixture.

The present method provides a direct measurement-based determination of the mean carbon number that is required in order to convert the VPIC of the mixture to MPIC values. We assume that the vapor emitted from the alkane mixture is mainly composed of C-4, C-5, C-6, C-7, C-8. The alkanes with carbon numbers less than 4 (methane, ethane and propane) are not expected to be components of the mixture because these species are gases at standard atmospheric conditions and if present upon manufacture, would have outgassed from the liquid fuel. Alkanes with higher carbon numbers than C-8 (nonane, decane, etc) have low vapor pressures and therefore would not be present in the vapor at significant levels.

The fuel-alkane analysis method involves analyzing two of the straight-chain alkanes members of C-4 to C-8 that have the least correlated absorption bands, n-butane and n-octane (C-4 and C-8). The correlation between these two bands, at  $0.5\text{ cm}^{-1}$  resolution, is low enough to ensure a statistically valid regression fit (see Figure 2).

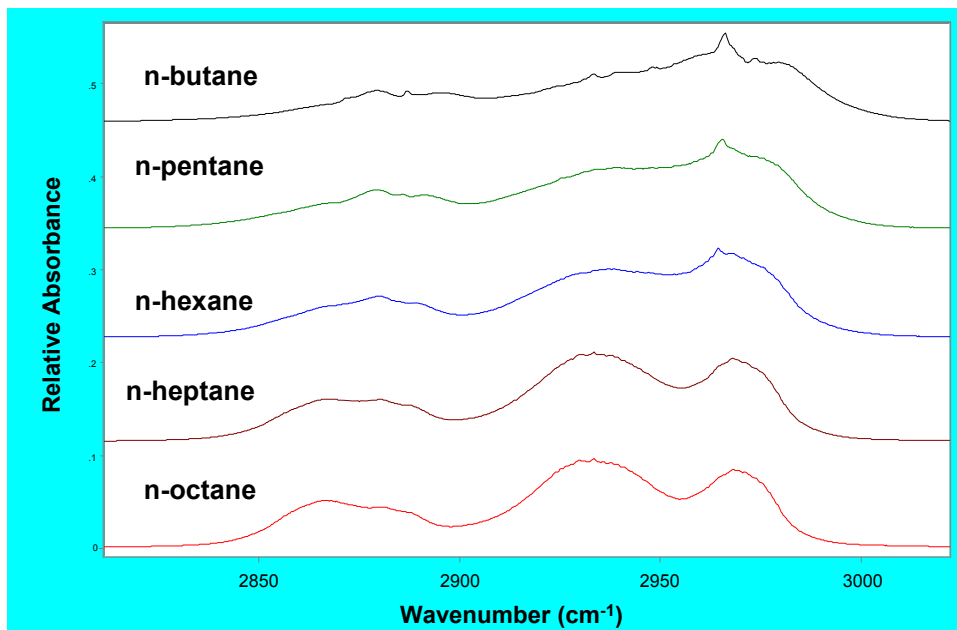


Figure 1. Comparison of the absorption bands of straight-chain alkanes, C-4 (n-butane) to C-8 (n-octane), measured with  $0.5\text{ cm}^{-1}$  resolution.

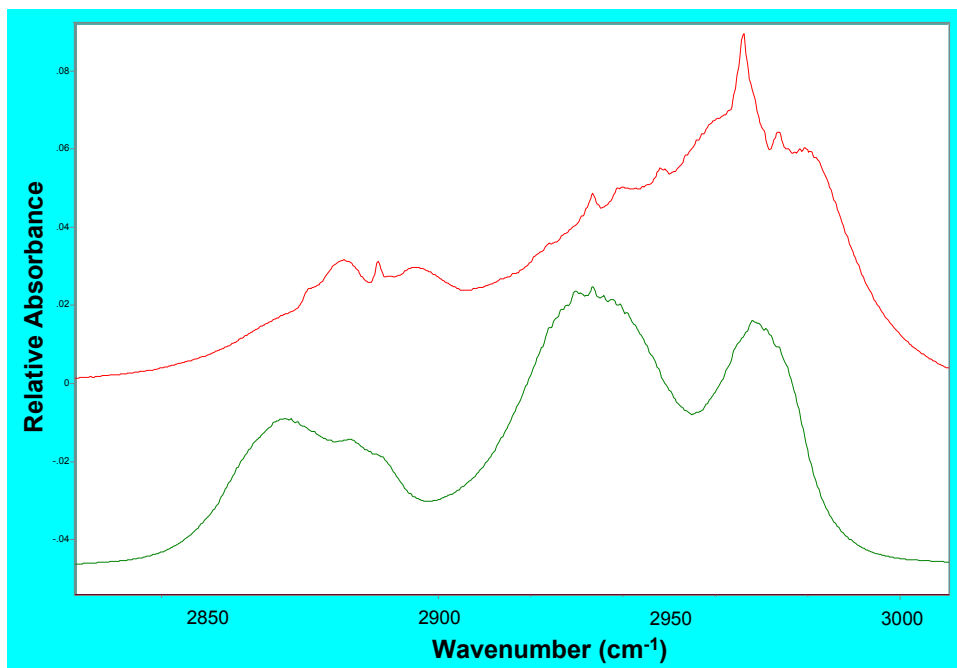


Figure 2. Comparison of the absorption bands of n-butane (red trace) and n-octane (green trace), measured with  $0.5\text{ cm}^{-1}$  resolution.



## 1.0 PROCEDURE

### 1.1 Set Up Region(s) of Analysis.

The OP-FTIR field measurements should be performed along with the QA/QC procedures described in the EPA ORS Facility Manual (ECPB 2004). The primary region of analysis is 2004.2 to 3001.2  $\text{cm}^{-1}$ . This region fully encumbers the main bands of the alkane mixture. If the path-average concentrations are expected to be high enough to distort the band-shapes, a second analysis, high alkane level (HAL) could be performed in the region from 2694.0 to 2915.7  $\text{cm}^{-1}$ . Weaker bands of n-butane and n-octane lie in this region and they exhibit little correlation. Depending on the requirements of the field measurement, the HAL analysis could either be performed at the time of the measurements (in real-time) or in a post-measurement analysis.

### 1.2 Set Up the Chemical Species for Analysis.

The Two analytes are n-butane and n-Octane. The atmosphere interferences are methane and water vapor. If other species might be present that have absorption bands in the regions of analysis (e.g. methanol, formaldehyde, etc), they should be included in the analysis as interferents, providing that their absorption bands do not correlate with either the n-butane or the n-octane bands.

### 1.3 Arbitration Rules for Combined LAL and HAL Analysis.

This step only applies if both LAL and HAL analyses on n-butane and n-octane have been performed. The volume PIC for the alkane mixture,  ${}^v C_{mix}^A$ , is the sum of the CLS determinations for n-butane and n-octane in region A, and the standard error of the  ${}^v C_{mix}^A$  determination is the square root of the sum of the squares of the respective standard error for the n-butane and n-octane determinations. Using labels to depict the LAL and HAL analyses, we have four metrics,

$${}^v C_{mix}^{LAL} \mid {}^v C_{butane}^{LAL} \ 2 \ {}^v C_{octane}^{LAL} ,$$

$$\omega_{mix}^{LAL} \mid \sqrt{(\omega_{butane}^{LAL})^2 \ 2 \ (\omega_{octane}^{LAL})^2} ,$$

$${}^v C_{mix}^{HAL} \mid {}^v C_{butane}^{HAL} \ 2 \ {}^v C_{octane}^{HAL} ,$$

and

$$\omega_{mix}^{HAL} \mid \sqrt{(\omega_{butane}^{HAL})^2 \ 2 \ (\omega_{octane}^{HAL})^2} .$$

The arbitration between using the LAL or the HAL determinations is made for each measurement in the set, according to the following logic conditions,

1. **IF**  ${}^v\hat{C}_{mix}^{LAL} \geq 3\omega_{mix}^{LAL}$  **AND**  ${}^v\hat{C}_{mix}^{HAL} \geq 3\omega_{mix}^{HAL}$   
**AND**  ${}^v\hat{C}_{mixture}^{HAL} \geq {}^v\hat{C}_{mixture}^{LAL}$   
**THEN**  ${}^v\hat{C}_{mixture}^{Arbitrated} = {}^v\hat{C}_{mixture}^{HAL}$
2. **IF**  ${}^v\hat{C}_{mix}^{LAL} \geq 3\omega_{mix}^{LAL}$  **AND**  ${}^v\hat{C}_{mix}^{HAL} \geq 3\omega_{mix}^{HAL}$   
**AND**  ${}^v\hat{C}_{mix}^{HAL} \geq {}^v\hat{C}_{mix}^{LAL}$   
**THEN**  ${}^v\hat{C}_{mix}^{Arbitrated} = {}^v\hat{C}_{mix}^{HAL}$
3. **IF**  ${}^v\hat{C}_{mix}^{LAL} \geq 3\omega_{mix}^{LAL}$  **AND**  ${}^v\hat{C}_{mix}^{HAL} \geq 3\omega_{mix}^{HAL}$   
**THEN**  ${}^v\hat{C}_{mix}^{Arbitrated} = {}^v\hat{C}_{mix}^{HAL}$
4. **IF**  ${}^v\hat{C}_{mix}^{LAL} \geq 3\omega_{mix}^{LAL}$  **AND**  ${}^v\hat{C}_{mix}^{HAL} \geq 3\omega_{mix}^{HAL}$   
**THEN**  ${}^v\hat{C}_{mix}^{Arbitrated} = {}^v\hat{C}_{mix}^{LAL}$
5. **IF**  ${}^v\hat{C}_{mix}^{LAL} \geq 2\omega_{mix}^{LAL}$  **AND**  ${}^v\hat{C}_{mix}^{HAL} \geq 2\omega_{mix}^{HAL}$   
**THEN**  ${}^v\hat{C}_{mix}^{Arbitrated}$  is below the Detection Limit

Criteria 1 and 2 address the issue of whether the strong band in LAL is saturated due to very high levels of alkanes. If saturation occurs, then the band intensity will grow at a rate that is less than linear resulting in a concentration determination that is less than the value that would occur if linearity prevailed. In this case one would expect that the analysis in the HAL region (where the bands are much weaker and more likely to maintain linearity) would yield a higher determination than in the saturated LAL region. This leads to the criterion, if both analysis results are above detection limits one chooses higher value. However, as stated below in the section on QA/QC, the analyst must validate the results in the HAL region when the concentration determinations are not much above detection limits.

#### 1.4 Determination of the Mean Molecular Mass, $\overline{M}_{mix}$ ,

The mean molecular mass of the alkane mixture,  $\overline{M}_{mix}$ , is given as

$$\overline{M}_{mix} = \frac{M_{butane} \int^V \hat{C}_{butane}^{Arbitrated} + 2 M_{octane} \int^V \hat{C}_{octane}^{Arbitrated}}{\int^V \hat{C}_{mix}^{Arbitrated}}, \quad (1)$$

where  $M_{butane} = 58.12$  g/mole (molecular mass of butane),

$M_{octane} = 114.23$  g/mole (molecular mass of octane),

$\int^V \hat{C}_{butane}^{Arbitrated}$  and  $\int^V \hat{C}_{octane}^{Arbitrated}$  are the butane and octane determinations from the analysis of the arbitration-chosen region.

#### 1.5 Determination of the Mass Path-Integrated Concentration, ${}^m\hat{C}_{mix}$ ,

The mass path-integrated concentration of the alkane mixture,  ${}^m\hat{C}_{mix}$ , is given as

$${}^m\hat{C}_{mix} = \frac{L(T, P) \int \overline{M}_{mix}}{A} \int^V \hat{C}_{mix}^{Arbitrated}$$

Where  $L(T)$  is Loschmidt's Number at temperature,  $T$  and pressure  $P$ ,

$$L(T) = 2.4793 \times 10^{25} \left( \frac{296K}{T} \right) \left( \frac{P}{1 atm} \right) \text{ molecules/m}^3,$$

and  $A$  is Avogadro's number,  $6.0220 \times 10^{23}$  molecules/mole. The numerical solution is

$${}^m\hat{C}_{mix} [g/m^3] = 4.1171 \times 10^{45} \left[ \overline{M}_{mix} \left( \frac{296K}{T} \right) \left( \frac{P}{1 atm} \right) \right] \int^V \hat{C}_{mix}^{Arbitrated} [ppm] \quad (2)$$

The procedure for converting the volume PICs of alkane vapor mixtures from petroleum-base fuels to mass PIC is summarized by Equations 1 and 2.

## 2.0 QA/QC CHECKS ON THE ANALYSIS

The QA/QC checks on the analysis must be carried out as a post-measurement procedure. If in performing the QA/QC checks, one finds quality problems that degrade the precision and accuracy analytical results to levels below those permitted by the Data Quality Objectives (DQOs) of the field project, the analysis should be repeated with corrections.

### 2.1 Check the Background Spectra

The QA/QC procedure on Relative Backgrounds is different than the procedure for Absolute Backgrounds. The Relative Backgrounds may contain the absorption bands due to the alkane, which would produce a negative bias on the alkane determinations. Many of the OP-FTIR systems produce single-beam spectra that have inherent hydrocarbon bands present, due to adsorption of oils on the optical surfaces. These “oil” bands are cancelled out in zero-path backgrounds, but may be present in the field absorbance spectra that were created using synthetic backgrounds. Therefore the QA/QC check on the zero-path Background should follow the same procedure as for Relative Backgrounds.

#### 2.1.1 Relative and Zero-Path Backgrounds

##### 1. Create Synthetic Backgrounds

For each Relative Background create an associated synthetic background, taking care not to place any points in the region between 2804 and 3002  $\text{cm}^{-1}$ .

##### 2. Create Absorbance Spectra

For each Relative Background create a absorbance spectrum using the relative background as the sample single beam and the synthetic background as the background.

##### 3. Analyze Absorbance Spectra

Analyze each of the absorbance spectra for the alkanes using the same method as used for the field measurement. Record the results as part of the QA/QC report.

##### 4. Correct Path-Integrated Concentrations (If Necessary)

If the path-integrated concentrations for n-butane and/or n-octane determined in Step 3 are above detection limits, determine whether the values are significant compared to the values determined on the field data. If they are, correct the field measurements by adding the background values that are above detection limits to the corresponding field values for n-butane and n-octane in the respective LAL and HAL regions. If corrections were made, then repeat the arbitration and mass integrated concentration determination procedures in Steps 1.3 to 1.5, above.

#### 2.1.2 Synthetic Backgrounds

##### 1. Prepare an Absorbance Spectrum from Alkane-Free Single Beam

Create an absorbance spectrum using any available single-beam spectrum that was measured (in the time period of the project) in an environment in which no hydrocarbons were present in the atmosphere

and using the synthetic background as the background. Unless there is expectation that the adsorbed oils on the OP-FTIR optics will change over the course of the project, only one absorbance spectrum will be necessary for this check for the entire project.

## **2. Analyze Absorbance Spectra**

Follow Step 3 in Section 2.1.1

## **3. Correct Path-Integrated Concentrations (If Necessary)**

Follow Step 4 in Section 2.1.1

*A single-beam spectrum from the project's quality assurance procedures could be used.*

### **2.2 Check for Interfering Absorption Features**

Check the LAL spectral region (and HAL region if used) for the presence of overlapping absorption bands by outlier species. Look for features that deviate from the band shapes of the C-4 to C-8 species shown in Figure 1. Search the Finger Print Region ( $723$  to  $1400\text{ cm}^{-1}$ ) for absorption bands or lines due to the presence of unexpected species. If any are found determine if there are corresponding C-H stretch bands.

Add all the spectral references of any species, which have been found to have overlapping bands in the LAL region (or HAL region if used), to the CLS analysis as interferents. This procedure needs to be performed only on measurement sets in which the outlier features are present and cause the data quality to not meet the project DQO.

### **2.3 Check for Saturation in the LAL Region**

Determine if any of the measured alkane absorption bands in the LAL region exhibit saturation. Generally, these bands become saturated at path-integrated concentration levels greater than  $2000\text{ ppm}\cdot\text{m}$ . Saturation can be recognized by view the peak band features and noting if they have a flattened appearance. This effect can be seen in Figure 3, which shows a saturated alkane mixture band measured at a refinery compared to a measured band that is still in the linear regime. The absorbance scales are different for the two traces. The scale for the green trace is greatly expanded compared to the red trace. If saturation is detected, then the analysis must be performed in the HAL region and the results must follow the arbitration procedure listed in Section 1.3.

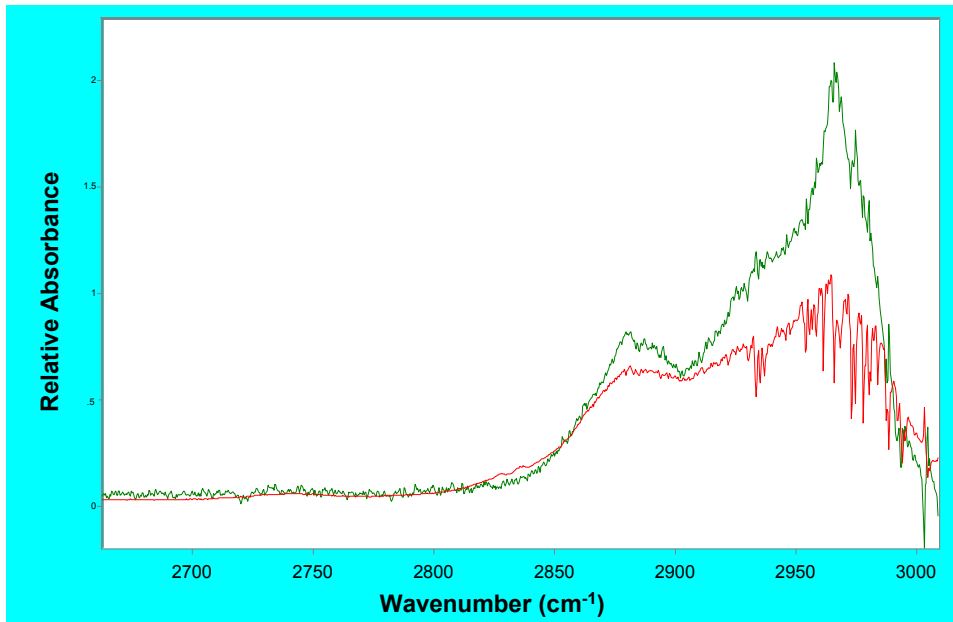


Figure 3. Comparison of a saturated alkane-mixture band (red trace) to one that is not saturated (green trace). The two traces are on plotted on the same ordinate scale. Note the difference in noise.

#### 2.4 If Using HAL Region Check Arbitrated HAL Values Close to Detection Limits

Check all arbitrated values close to detection limits are valid. These values should smoothly transition to the lower values that arbitrate towards LAL. If these results seem to not connect to the HAL arbitrated values smoothly, then one may consider raising the detection-limit criterion for the HAL values  $4 \cdot \omega$  or greater.

### 3.0 REFERENCE

ECPB 2004 ECPB (Emission Characterization Prevention Branch) Optical Remote Sensing Facility Manual, Prepared for the US EPA NRMRL Revision 1 April 2004

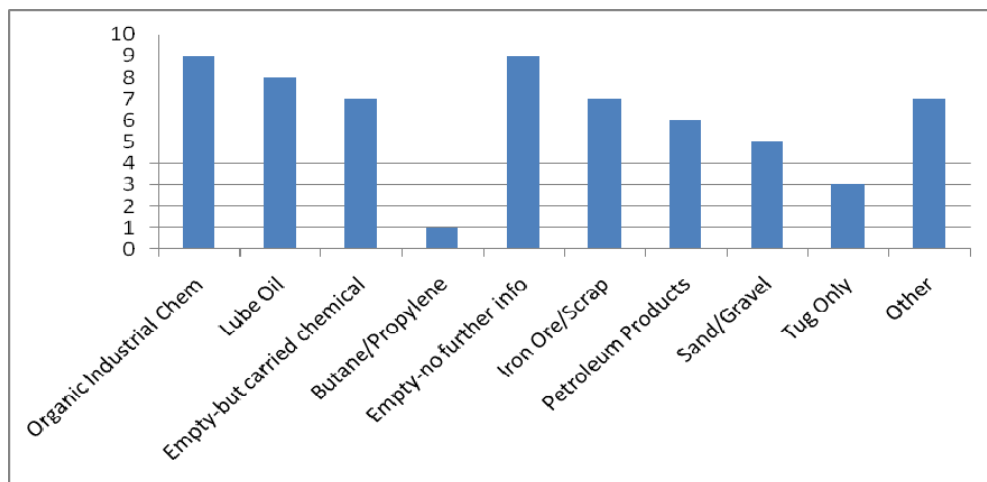
## **APPENDIX G**

### OTM 10 Data Graphs and Tables

## Appendix G: OTM 10 Data Graphs and Tables

This Appendix contains the results of the OTM 10, OP-FTIR monitoring performed from September 24 to October 9, 2008 at the U.S. Army Corps of Engineers Port Allen Lock. A total of 97 lockings occurred during the OTM 10 observation period. Some of the lockings included multiple tugs and barges. There were a total of 62 defined events in which alkane mixture (AM) fluxes were measured. Many of these flux events occurred when non-petrochemical transport barges were in the lock indicating that the measured AM flux was associated with hydrocarbon emissions from the tug diesel engines. This confounding factor is further discussed at the end of the appendix.

Figure G-1 shows the distribution of barge types for these defined events based on the Corps of Engineers traffic log information. The six highest emissions events, two occurred during times with barges that were coded as carrying petroleum pitches, two with barges coded as carrying crude petroleum, and two with barges coded as empty (however the field crew smelled aromatics during one of these events).



**Figure G-1. Distribution of Barge Types for Emission Events According to the U.S. Army Corps of Engineers Traffic Log**

For each of the 62 defined events, a description of the event, the AM flux values measured during the event, a screenshot of a leak detected during the event from the PGIE observations (when available), and the results of the trace compound analysis (when detected) are presented. For some of the events, we report “WC” as the AM flux value. In these instances, AM concentrations were detected by the OP-FTIR instrumentation, but the prevailing winds during the time of the measurement contained a southerly component, so a AM flux value could not be calculated. The trace compound concentrations presented represent the average concentration for the event measured along the ground level beam path of the VRPM configurations.

**Table G-1. 9/24/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/24/2008	10:32	11:03	Two	Labeled as benzene and smelled like benzene, but Corps of Engineers report said it was empty



Table G-2. AM Flux Values Measured during 9/24/ 2008, Event #1

Time	AM Flux (g/s)
10:33:48	0.060
10:36:59	0.124
10:39:37	0.237
10:42:17	0.321
10:44:56	0.431
10:47:35	0.558
10:50:13	0.637
10:52:53	0.730
10:55:33	0.912
10:58:12	0.956
11:00:15	0.308
11:02:54	0.067
<b>Average:</b>	<b>0.445</b>



Figure G-2. Screenshot from FLIR Camera Showing Leak from 9/24/ 2008, Event #1

**Table G-3. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/24/ 2008, Event #1**

Path	Methane	Acetylene	Propane	2-Methylbutane
EPA OP-FTIR (West)	115	11.1	92.1	96.1
ARCADIS OP-FTIR (East)	113	14.5	26.6	24.4

**Table G-4. 9/25/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/25/2008	7:40	8:08	One	May be carrying lube oil, per LADEQ, labeled as empty

**Table G-5. AM Flux Values Measured during 9/25/ 2008, Event #1**

Time	AM Flux (g/s)
7:44:17	0.004
7:46:59	0.008
7:49:39	0.022
7:52:21	0.029
7:55:00	0.025
7:57:43	0.004
8:00:23	0.003
<b>Average:</b>	<b>0.014</b>

**Table G-6. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/25/ 2008, Event #1**

Path	Methane
EPA OP-FTIR (West)	ND
ARCADIS OP-FTIR (East)	122

**Table G-7. 9/25/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/25/2008	8:34	9:15	Six	Gravel

**Table G-8. AM Flux Values Measured during 9/25/ 2008, Event #2**

Time	AM Flux (g/s)
8:38:00	0.009
8:40:38	0.006
8:43:15	0.008
8:45:53	0.006
8:48:30	0.009
8:51:12	0.009
8:53:50	0.009
8:56:31	0.007
8:59:11	0.007
9:01:50	0.008
9:04:28	0.008
9:07:08	0.016
<b>Average:</b>	<b>0.009</b>

**Table G-9. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/25/ 2008, Event #2**

Path	Methane
EPA OP-FTIR (West)	66.7
ARCADIS OP-FTIR (East)	109

**Table G-10. 9/25/ 2008 Event #3**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/25/2008	9:52	10:36	Six	Visual as scrap, but Corps of Engineers report says Sugar/Iron Ore

**Table G-11. AM Flux Values Measured during 9/25/ 2008, Event #3**

Time	AM Flux (g/s)
9:56:08	0.010
10:14:43	0.008
10:17:21	0.008
10:20:00	0.011
10:22:39	0.010
10:25:17	0.010
10:27:55	0.008
10:30:33	0.007
<b>Average:</b>	<b>0.009</b>

**Table G-12. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/25/ 2008, Event #3**

Path	Methane
EPA OP-FTIR (West)	17.4
ARCADIS OP-FTIR (East)	44.4

**Table G-13. 9/25/ 2008 Event #4**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/25/2008	11:14	11:51	One	Chemicals, but Corps of Engineers report says empty

**Table G-14. AM Flux Values Measured during 9/25/ 2008, Event #4**

Time	AM Flux (g/s)
11:19:05	0.008
11:21:46	0.009
11:24:25	0.009
11:27:06	0.008
11:29:46	0.007
11:32:27	0.007
11:35:09	0.009
11:37:50	0.013
11:40:33	0.012
11:43:17	0.007
<b>Average:</b>	<b>0.009</b>

**Table G-15. 9/25/ 2008 Event #5**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/25/2008	15:09	16:00	Six	Corps of Engineers Report says sand, gravel, stone

**Table G-16. AM Flux Values Measured during 9/25/ 2008, Event #5**

Time	AM Flux (g/s)
15:11:53	0.007
15:14:30	0.007
15:17:08	0.006
15:19:45	0.005
15:22:24	0.005
15:25:01	0.005
15:27:40	0.006
15:30:18	0.003
15:32:54	0.005
15:35:34	0.006
15:38:11	0.005
15:40:49	0.007
15:44:44	0.005
15:47:21	0.005
15:50:00	0.003
15:52:37	0.004
15:55:14	0.003
<b>Average:</b>	<b>0.005</b>

**Table G-17. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/25/ 2008, Event #5**

Path	Methane
EPA OP-FTIR (West)	45.6
ARCADIS OP-FTIR (East)	18.5

**Table G-18. 9/26/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/26/2008	9:10	9:52	Two	Empty, per Corps of Engineers report, but may have carried benzene

**Table G-19. AM Flux Values Measured during 9/26/ 2008, Event #1**

<b>Time</b>	<b>AM Flux (g/s)</b>
9:13:45	0.045
9:16:19	0.053
9:18:54	0.060
9:21:29	0.070
9:24:40	0.159
9:27:15	0.105
9:29:50	0.137
9:32:25	0.179
9:34:59	0.113
9:37:34	0.045
9:40:45	0.048
9:43:21	0.064
9:45:56	0.063
<b>Average:</b>	<b>0.088</b>

**Table G-20. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/26/ 2008, Event #1**

<b>Path</b>	<b>Methane</b>	<b>2-Methylbutane</b>
EPA OP-FTIR (West)	220	23.6
ARCADIS OP-FTIR (East)	ND	ND

**Table G-21. 9/27/ 2008 Event #1**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
9/27/2008	8:45	9:35	One tug with no barge, and one tug with six barges	Building cement and concrete; lime; glass

**Table G-22. AM Flux Values Measured during 9/27/ 2008, Event #1**

Time	AM Flux (g/s)
8:49:18	0.001
8:51:53	0
8:54:07	0
8:56:47	0
8:59:24	0
9:02:02	0
9:04:40	0
9:07:17	0.003
9:09:54	0
9:12:30	0.010
9:15:07	0.007
9:17:45	0.013
9:20:23	0.006
9:23:00	0.007
9:25:38	0.016
9:28:16	0.030
<b>Average:</b>	<b>0.006</b>

**Table G-23. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/27/ 2008, Event #1**

Path	Methane	Methanol	Benzene	2-Methylbutane	Ethylene
EPA OP-FTIR (West)	64.2	ND	ND	34.2	20.2
ARCADIS OP-FTIR (East)	459	24.3	198	34.8	ND

**Table G-24. 9/27/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/27/2008	10:06	10:55	Six	Empty, per Corps of Engineers report and visual

**Table G-25. AM Flux Values Measured during 9/27/ 2008, Event #2**

Time	AM Flux (g/s)
10:08:58	0.079
10:11:36	0.057
10:14:13	0.008
10:16:50	0
10:19:27	0.011
10:22:05	0.051
10:24:42	0.060
10:27:20	0.065
10:29:58	0.085
10:32:35	0.112
10:35:12	0.136
10:37:51	0.120
10:40:28	0.108
10:43:06	0.078
10:45:45	0.060
10:47:44	0.040
<b>Average:</b>	<b>0.067</b>

**Table G-26. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/27/ 2008, Event #2**

Path	Methane	Ethylene	Propane	2-Methylbutane
EPA OP-FTIR (West)	100	17.4	99.7	64.4
ARCADIS OP-FTIR (East)	570	18.4	110	69.1

**Table G-27. 9/27/ 2008 Event #3**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/27/2008	11:21	11:58	Three	Per Corps of Engineers report and visual, lube oils or organic chemicals, possibly phenol



**Table G-28. AM Flux Values Measured during 9/27/ 2008, Event #3**

Time	AM Flux (g/s)
11:23:43	0.024
11:26:19	0.042
11:28:55	0.027
11:31:32	0.031
11:34:10	0.011
11:36:47	0.007
11:39:26	0.003
11:42:03	0
11:44:42	wc
11:47:19	wc
11:49:56	wc
11:52:33	0.001
<b>Average:</b>	<b>0.016</b>

wc = Wind criteria was not met.

**Table G-29. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/27/ 2008, Event #3**

Path	Propane	2-Methylbutane
EPA OP-FTIR (West)	ND	15.5
ARCADIS OP-FTIR (East)	32.3	18.4

**Table G-30. 9/28/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/28/2008	8:44	9:28	Two	Organic industrial chemicals

**Table G-31. AM Flux Values Measured during 9/28/ 2008, Event #1**

Time	AM Flux (g/s)
8:46:56	0
8:49:34	0
8:52:12	0
8:54:50	0
8:57:28	0
9:00:06	0
9:02:44	0
9:05:22	0
9:08:01	0
9:10:40	0
9:13:18	0.195
9:15:55	0.071
9:18:33	0.025
9:21:11	0.07
<b>Average:</b>	<b>0.026</b>

**Table G-32. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/28/ 2008, Event #1**

Path	Methane	Ethylene	Acetylene	Propane	2-Methylbutane
EPA OP-FTIR (West)	861	27.7	ND	144	139
ARCADIS OP-FTIR (East)	751	ND	25.3	143	142

**Table G-33. 9/28/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/28/2008	9:38	10:11	One	Possibly grain, although Corps of Engineers report said empty

**Table G-34. AM Flux Values Measured during 9/28/ 2008, Event #2**

Time	AM Flux (g/s)
9:41:12	0
9:43:31	0
9:46:09	0
9:48:47	0
9:51:24	0
9:54:03	0
9:56:42	0
9:59:21	0
10:01:59	0
10:04:39	0.012
<b>Average:</b>	<b>0.001</b>

**Table G-35. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/28/ 2008, Event #2**

Path	Methane	Ethylene	2-Methylbutane
EPA OP-FTIR (West)	271	16.5	44.4
ARCADIS OP-FTIR (East)	182	ND	19.9

**Table G-36. 9/29/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/29/2008	8:24	9:12	Two	Dry sulfur, iron and steel products

**Table G-37. AM Flux Values Measured during 9/29/ 2008, Event #1**

<b>Time</b>	<b>AM Flux (g/s)</b>
8:29:20	0.015
8:31:58	0.017
8:34:36	0.02
8:37:14	0.02
8:39:54	0.016
8:42:32	0.015
8:45:11	0.014
8:47:49	0.012
8:50:27	0.01
8:53:06	0.01
8:55:44	0.011
8:58:23	0.013
9:01:01	0.014
9:03:39	0.017
9:06:16	0.017
<b>Average:</b>	<b>0.015</b>

**Table G-38. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/29/ 2008, Event #1**

<b>Path</b>	<b>Methane</b>
EPA OP-FTIR (West)	ND
ARCADIS OP-FTIR (East)	148

**Table G-39. 9/29/ 2008 Event #2**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
9/29/2008	9:23	10:23	Three tugs with barges, one empty and two manned	Equipment/machinery

**Table G-40. AM Flux Values Measured during 9/29/ 2008, Event #2**

<b>Time</b>	<b>AM Flux (g/s)</b>
9:14:43	0.011
9:17:21	0.006
9:20:02	0.005
9:27:26	0.014
9:30:06	0.015
9:34:08	0.105
9:36:47	0.279
9:39:26	0.514
9:42:06	0.374
9:44:45	0.305
9:47:23	0.325
9:50:00	0.410
9:52:39	0.457
9:55:16	0.596
9:57:55	0.590
10:00:33	0.463
10:03:11	0.324
10:05:50	0.297
10:08:29	0.389
10:11:09	0.374
10:13:48	0.390
10:16:28	0.252
<b>Average:</b>	<b>0.295</b>



Figure G-3. Screenshot from FLIR Camera Showing Leak from 9/29/ 2008, Event #2

Table G-41. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/29/ 2008, Event #2

Path	Methane	Propane	2-Methylbutane
EPA OP-FTIR (West)	ND	220	140
ARCADIS OP-FTIR (East)	92.6	53.1	34.1

Table G-42. 9/29/ 2008 Event #3

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/29/2008	11:01	11:51	Six	Clay, steel, ore scrap, machinery, fertilizer

**Table G-43. AM Flux Values Measured during 9/29/ 2008, Event #3**

Time	AM Flux (g/s)
11:04:35	0.008
11:07:17	0.003
11:09:57	0.002
11:12:38	0.004
11:15:19	0.003
11:17:59	0.002
11:20:07	0
11:22:45	0.002
11:25:23	0.006
11:28:01	0.006
11:30:39	0.005
11:34:34	0.005
11:37:13	0.006
11:39:51	0.005
11:42:30	0.005
11:45:09	0.005
11:59:44	0.003
12:02:22	0.002
12:05:01	0.004
<b>Average:</b>	<b>0.004</b>

**Table G-44. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/29/ 2008, Event #3**

Path	Methane	Acetylene
EPA OP-FTIR (West)	44.4	15.2
ARCADIS OP-FTIR (East)	41.7	ND

**Table G-45. 9/29/ 2008 Event #4**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/29/2008	12:15	13:00	Six	Sand, gravel

**Table G-46. AM Flux Values Measured during 9/29/ 2008, Event #4**

<b>Time</b>	<b>AM Flux (g/s)</b>
12:19:36	0.008
12:22:15	0.018
12:24:55	0.031
12:27:33	0.017
12:30:11	0.008
12:32:48	0.007
12:35:27	0.005
12:38:06	0.006
12:40:44	0.007
12:43:21	0.007
12:46:01	0.006
12:48:38	0.005
12:51:16	0.003
12:53:56	0.003
<b>Average:</b>	<b>0.009</b>

**Table G-47. 9/29/ 2008 Event #5**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
9/29/2008	13:07	14:06	Three	Empty , organic industrial chemicals, butane, propylene, propane



**Table G-48. AM Flux Values Measured during 9/29/ 2008, Event #5**

<b>Time</b>	<b>AM Flux (g/s)</b>
13:11:12	0.008
13:13:49	0.007
13:16:27	0.006
13:19:05	0.007
13:21:44	0.006
13:24:22	0.009
13:27:01	0.009
13:29:38	0.018
13:32:16	0.021
13:34:54	0.022
13:37:33	0.016
13:40:10	0.016
13:42:50	0.008
13:45:28	0.011
13:48:06	0.009
13:50:47	0.012
13:53:26	0.011
13:56:05	0.013
13:58:45	0.005
14:01:27	0.005
<b><i>Average:</i></b>	<b><i>0.011</i></b>

**Table G-49. 9/29/ 2008 Event #6**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
9/29/2008	14:13	14:57	One tug with no barge, one tug with two barges	Empty per Corps of Engineers report

**Table G-50. AM Flux Values Measured during 9/29/ 2008, Event #6**

<b>Time</b>	<b>AM Flux (g/s)</b>
14:17:21	0.011
14:20:01	0.007
14:22:41	0.017
14:25:19	0.013
14:28:00	0.012
14:30:39	0.007
14:33:18	0.011
14:36:36	0.011
14:38:40	0.011
14:41:18	0.009
14:43:59	0.011
14:47:55	0.003
14:50:34	0.002
<b>Average:</b>	<b>0.010</b>

**Table G-51. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/29/ 2008, Event #6**

<b>Path</b>	<b>2-Methylbutane</b>
EPA OP-FTIR (West)	10.4
ARCADIS OP-FTIR (East)	ND

**Table G-52. 9/29/ 2008 Event #7**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
9/29/2008	15:10	15:51	One tug with no barges, one tug with six barges	Overlap, scrap ore and two with organic industrial chemicals

**Table G-53. AM Flux Values Measured during 9/29/ 2008, Event #7**

<b>Time</b>	<b>AM Flux (g/s)</b>
15:14:25	wc
15:17:03	0.002
15:19:41	0.004
15:22:19	0.006
15:24:58	0.008
15:27:38	0.008
15:30:17	0.008
15:33:12	0.008
15:35:34	0.005
15:38:12	0.008
15:40:50	0.007
15:43:27	0.006
15:46:05	0.007
<b>Average:</b>	<b>0.006</b>

wc Wind criteria was not met.

**Table G-54. 9/30/ 2008 Event #1**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
9/30/2008	8:11	9:11	One tug with no barges, one tug with two barges	May be chemical barges, although the Corps of Engineers report said empty

**Table G-55. AM Flux Values Measured during 9/30/ 2008, Event #1**

Time	AM Flux (g/s)
8:26:54	0
8:28:53	0
8:30:12	0
8:36:54	0
8:39:33	0
8:41:32	0
8:42:34	0.007
8:44:12	0.012
8:45:19	0.021
8:46:51	0.018
8:48:04	0.016
8:49:31	0.017
8:52:10	0
8:54:50	0
9:02:00	0.002
9:03:20	0.003
9:04:40	0.007
9:06:06	0.006
<b>Average:</b>	<b>0.007</b>

**Table G-56. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/30/ 2008, Event #1**

Path	Methane	2-Methylbutane
EPA OP-FTIR (West)	ND	18.2
ARCADIS OP-FTIR (East)	458	ND

**Table G-57. 9/30/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/30/2008	9:20	9:58	One	May be chemical barge, although the Corps of Engineers report said empty

**Table G-58. AM Flux Values Measured during 9/30/ 2008, Event #2**

Time	AM Flux (g/s)
9:23:40	0.014
9:25:02	0.021
9:34:37	0.017
9:36:36	0.025
9:41:30	0.021
9:42:52	0.040
9:44:13	0.017
9:45:33	0.013
9:46:54	0.012
9:48:16	0.010
9:49:37	0.002
9:55:04	wc
<b>Average:</b>	<b>0.017</b>

wc Wind criteria was not met.

**Table G-59. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/30/ 2008, Event #2**

Path	Methane	2-Methylbutane
EPA OP-FTIR (West)	ND	ND
ARCADIS OP-FTIR (East)	362	42.7

**Table G-60. 9/30/ 2008 Event #3**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/30/2008	10:16	11:25	Six	Dry sulfur, clay

**Table G-61. AM Flux Values Measured during 9/30/ 2008, Event #3**

<b>Time</b>	<b>AM Flux (g/s)</b>
10:22:01	0.001
10:27:29	0.018
10:28:49	0.014
10:30:11	wc
10:31:31	wc
10:32:49	wc
10:34:13	wc
10:35:29	wc
10:38:08	0.005
10:39:38	0.005
10:40:47	wc
10:42:19	wc
10:43:26	wc
10:45:47	wc
10:46:21	wc
10:47:43	wc
10:48:44	wc
10:50:43	wc
10:51:46	wc
10:53:21	wc
10:54:24	wc
10:55:59	0.001
10:57:07	0.002
10:58:39	0.014
10:59:49	0.001
11:04:36	0.007
11:11:57	0
11:13:26	0.001
11:14:35	wc
11:16:07	wc
11:17:15	wc
11:18:48	wc
11:19:53	wc
11:21:31	wc
<b>Average:</b>	<b>0.006</b>

wc Wind criteria was not met.

**Table G-62. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 9/30/ 2008, Event #3**

Path	Methane	2-Methylbutane
EPA OP-FTIR (West)	133	20.1
ARCADIS OP-FTIR (East)	56.4	23.0

**Table G-63. 9/30/ 2008 Event #4**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
9/30/2008	11:49	12:56	One tug with one barge, one tug with six barges	One barge lubricating oil, other barges gravel

**Table G-64. AM Flux Values Measured during 9/30/ 2008, Event #4**

Time	AM Flux (g/s)
11:51:51	wc
11:54:01	wc
11:56:39	wc
11:59:17	0.005
12:01:58	0.009
12:04:36	0.009
12:08:33	0.004
12:11:10	0.003
12:13:49	0.002
12:16:27	0.001
12:19:05	0.001
12:21:44	wc
12:24:23	wc
12:27:02	wc
12:29:40	0
12:32:20	0.004
12:34:58	0.005
12:37:37	0.002
12:40:15	0
12:42:55	wc
12:45:33	0.002
12:48:11	0.015
12:50:50	0.032
<b>Average:</b>	<b>0.006</b>

wc Wind criteria was not met.

**Table G-65. 10/1/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/1/2008	8:00	8:21	One	Iron ore, scrap

**Table G-66. AM Flux Values Measured during 10/1/ 2008, Event #1**

Time	AM Flux (g/s)
8:11:19	0.002
8:14:53	0.002
<b>Average:</b>	<b>0.002</b>

**Table G-67. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/1/ 2008, Event #1**

Path	Methane	2-Methylbutane
EPA OP-FTIR (West)	220	ND
ARCADIS OP-FTIR (East)	268	22.0

**Table G-68. 10/1/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/1/2008	9:10	9:58	Two	Organic industrial chemicals

**Table G-69. AM Flux Values Measured during 10/1/ 2008, Event #2**

Time	AM Flux (g/s)
9:14:56	0
9:17:33	0
9:20:12	0.01
9:22:51	0.008
9:25:30	0.012
9:28:09	0.019
9:30:52	0
9:33:30	0.035
9:36:09	0.046
9:38:54	0.067
9:41:31	0.065
9:44:12	0.058
9:46:48	0.04
9:49:23	0.022



Time	AM Flux (g/s)
9:52:01	0.026
<b>Average:</b>	<b>0.027</b>



Figure G-4. Screenshot from FLIR Camera Showing Leak from 10/1/ 2008, Event #2

Table G-70. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/1/ 2008, Event #2

Path	Methane	Ethylene	Propane	2-Methylbutane
EPA OP-FTIR (West)	302	15.4	66.1	63.6
ARCADIS OP-FTIR (East)	234	13.4	275	242

Table G-71. 10/1/ 2008 Event #3

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/1/2008	10:43	11:43	One tug with no barges, one tug with five barges	Metal ores, scrap, organic industrial chemicals

**Table G-72. AM Flux Values Measured during 10/1/ 2008, Event #3**

<b>Time</b>	<b>AM Flux (g/s)</b>
10:47:09	0.011
10:49:47	0.010
10:52:25	0.027
10:55:03	0.029
10:57:39	0.037
11:00:18	0.022
11:02:56	0.022
11:05:34	0.014
11:08:12	0.019
11:10:53	0.011
11:13:32	0.012
11:16:10	0.008
11:18:51	0.008
11:21:29	0.003
11:24:09	0.006
11:26:48	0.013
11:29:26	0.034
11:32:08	0.034
11:34:46	0.024
11:36:54	0.006
<b>Average:</b>	<b>0.018</b>

**Table G-73. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/1/ 2008, Event #3**

<b>Path</b>	<b>Methane</b>	<b>Propane</b>	<b>2-Methylbutane</b>
EPA OP-FTIR (West)	68.8	ND	24.9
ARCADIS OP-FTIR (East)	62.5	24.4	21.4

**Table G-74. 10/1/ 2008 Event #4**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
10/1/2008	12:33	13:29	Six	Empties and scrap

**Table G-75. AM Flux Values Measured during 10/1/ 2008, Event #4**

Time	AM Flux (g/s)
12:37:03	0
12:39:43	0.001
12:42:20	0.002
12:44:59	0.003
12:47:38	0.002
12:50:16	0.002
12:52:54	0.003
12:55:33	0.005
12:58:13	0.002
13:00:53	0.001
13:03:32	0.002
13:06:12	0.001
13:08:50	0.001
13:11:30	wc
13:14:08	wc
13:16:47	wc
13:19:27	0.003
13:22:03	0.006
13:24:15	0.002
<b>Average:</b>	<b>0.002</b>

wc Wind criteria was not met.

**Table G-76. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/1/ 2008, Event #4**

Path	Methane	Methanol
EPA OP-FTIR (West)	41.3	15.8
ARCADIS OP-FTIR (East)	33.6	15.7

**Table G-77. 10/1/ 2008 Event #5**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/1/2008	13:40	14:37	One tug with one barge, one tug with six barges	Empty. Dry sulfur clay, organic industrial chemicals

**Table G-78. AM Flux Values Measured during 10/1/ 2008, Event #5**

<b>Time</b>	<b>AM Flux (g/s)</b>
13:44:27	0.009
13:47:06	0.006
13:49:45	0.021
13:52:24	0.008
13:55:06	0.002
13:57:45	wc
14:00:25	0.001
14:03:06	0.002
14:05:45	0.002
14:08:25	0
14:11:03	0.002
14:13:41	0.004
14:16:21	0.004
14:18:58	0.002
14:21:38	0.003
14:24:16	0.001
14:26:54	0.002
14:29:49	0.001
14:32:30	0.004
<b>Average:</b>	<b>0.004</b>

wc Wind criteria was not met.

**Table G-79. 10/1/ 2008 Event #6**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
10/1/2008	15:04	15:51	Two	Distillate, lube oils

**Table G-80. AM Flux Values Measured during 10/1/ 2008, Event #6**

Time	AM Flux (g/s)
15:09:26	0.001
15:12:05	0
15:14:42	wc
15:17:21	0
15:20:02	0.001
15:22:41	0.001
15:25:21	0.002
15:28:01	0.004
15:30:41	0.005
15:33:21	0.007
15:36:01	0.006
15:38:41	0.004
15:41:19	0.001
15:43:59	wc
15:46:05	0
<b>Average:</b>	<b>0.002</b>

wc Wind criteria was not met.



**Figure G-5. Screenshot from FLIR Camera Showing Leak from 10/1/ 2008, Event #6**

**Table G-81. 10/2/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/2/2008	7:45	8:03	Three	Empty. Organic industrial chemicals

**Table G-82. AM Flux Values Measured during 10/2/ 2008, Event #1**

Time	AM Flux (g/s)
7:51:45	0.05
7:54:21	0.022
7:56:57	0
<b>Average:</b>	<b>0.024</b>

**Table G-83. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/2/ 2008, Event #1**

Path	Methane	Methanol	2-Methylbutane
EPA OP-FTIR (West)	642	18.4	60.0
ARCADIS OP-FTIR (East)	No Data	No Data	No Data

**Table G-84. 10/2/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/2/2008	9:45	10:42	One tug with one barge, one tug with two barges	Butane, propylene, one empty

**Table G-85. AM Flux Values Measured during 10/2/ 2008, Event #2**

<b>Time</b>	<b>AM Flux (g/s)</b>
9:48:36	wc
9:51:16	wc
9:53:53	wc
9:56:31	0
9:59:09	0.072
10:01:46	0.141
10:04:24	0.126
10:07:02	0.084
10:09:41	0.014
10:12:18	wc
10:14:57	wc
10:17:35	wc
10:20:11	wc
10:22:48	wc
10:25:28	wc
10:28:05	wc
10:30:41	wc
10:33:21	wc
10:36:00	wc
10:38:38	wc
<b><i>Average:</i></b>	<b><i>0.073</i></b>

wc Wind criteria was not met.



Figure G-6. Screenshot from FLIR Camera Showing Leak from 10/2/ 2008, Event #3

Table G-86. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/2/ 2008, Event #2

Path	Methane	Propane	2-Methylbutane
EPA OP-FTIR (West)	114	266	351
ARCADIS OP-FTIR (East)	216	ND	123

Table G-87. 10/3/ 2008 Event #1

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/3/2008	9:20	10:20	Five	Empties and distillate lube oil



**Table G-88. AM Flux Values Measured during 10/3/ 2008, Event #1**

<b>Time</b>	<b>AM Flux (g/s)</b>
9:23:32	WC
9:26:11	WC
9:28:49	WC
9:31:27	WC
9:34:05	WC
9:36:42	WC
9:39:21	WC
9:42:01	WC
9:44:39	WC
9:47:36	WC
9:50:17	WC
9:52:27	WC
9:54:32	WC
9:57:10	WC
9:59:50	WC
10:02:29	WC
10:05:08	WC
10:07:47	WC
10:10:25	WC
10:13:06	WC
<b>Average:</b>	<b>WC</b>

WC Wind criteria was not met.

**Table G-89. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/3/ 2008, Event #1**

<b>Path</b>	<b>Methane</b>
EPA OP-FTIR (West)	117
ARCADIS OP-FTIR (East)	106

**Table G-90. 10/3/ 2008 Event #2**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
10/3/2008	10:31	10:51	Tug, no barges	N/A

**Table G-91. AM Flux Values Measured during 10/3/ 2008, Event #2**

Time	AM Flux (g/s)
10:34:19	WC
10:36:58	WC
10:39:36	WC
10:42:15	WC
10:44:54	WC
10:47:12	<b>WC</b>
<b>Average:</b>	WC

wc Wind criteria was not met.

**Table G-92. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/3/ 2008, Event #2**

Path	Methane
EPA OP-FTIR (West)	56.1
ARCADIS OP-FTIR (East)	ND

**Table G-93. 10/3/ 2008 Event #3**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/3/2008	11:09	11:52	Six	Empties, lube oil, organic industrial chemicals

**Table G-94. AM Flux Values Measured during 10/3/ 2008, Event #3**

Time	AM Flux (g/s)
11:12:42	WC
11:15:24	WC
11:18:02	WC
11:20:40	WC
11:23:18	WC
11:25:57	0
11:28:36	WC
11:31:15	WC
11:33:55	WC
11:36:34	WC
11:39:12	WC
11:41:52	WC
11:44:30	WC
<b>Average:</b>	<b>0.000</b>

wc Wind criteria was not met.

**Table G-95. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/3/ 2008, Event #3**

Path	Methane
EPA OP-FTIR (West)	76.6
ARCADIS OP-FTIR (East)	74.7

**Table G-96. 10/3/ 2008 Event #4**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/3/2008	12:39	13:17	Two	Empty

**Table G-97. AM Flux Values Measured during 10/3/ 2008, Event #4**

Time	AM Flux (g/s)
12:42:43	wc
12:44:43	wc
12:46:39	wc
12:49:20	wc
12:51:59	wc
12:54:37	wc
12:57:15	0
12:59:53	0
13:02:31	0
13:05:08	wc
13:07:47	wc
13:10:45	wc
<b>Average:</b>	<b>0.000</b>

wc Wind criteria was not met.

**Table G-98. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/3/ 2008, Event #4**

Path	Methane
EPA OP-FTIR (West)	45.1
ARCADIS OP-FTIR (East)	57.1

**Table G-99. 10/3/ 2008 Event #5**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/3/2008	13:25	14:26	One tug with one barge, one tug with two barges	Organic industrial chemicals/ butane propellant. One empty

**Table G-100. AM Flux Values Measured during 10/3/ 2008, Event #5**

Time	AM Flux (g/s)
13:17:16	wc
13:19:51	wc
13:22:29	wc
13:28:54	0
13:31:32	wc
13:34:11	wc
13:36:50	wc
13:39:28	wc
13:42:07	wc
13:44:46	0
13:47:26	wc
13:50:04	wc
13:52:43	wc
13:55:24	wc
13:58:04	0
14:00:42	0.001
14:03:20	0
14:05:59	wc
14:08:38	wc
14:11:17	wc
14:13:55	wc
14:16:35	wc
14:19:12	0
14:21:16	0
<b>Average:</b>	<b>0.000</b>

wc Wind criteria was not met.

**Table G-101. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/3/ 2008, Event #5**

Path	Methane
EPA OP-FTIR (West)	45.3
ARCADIS OP-FTIR (East)	59.7

**Table G-102. 10/4/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/4/2008	8:35	9:14	Six	Sand, gravel

**Table G-103. AM Flux Values Measured during 10/4/ 2008, Event #1**

Time	AM Flux (g/s)
8:54:54	0.004
8:58:35	0.002
9:01:14	0.002
<b>Average:</b>	<b>0.003</b>

**Table G-104. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/4/ 2008, Event #1**

Path	Methane
EPA OP-FTIR (West)	136
ARCADIS OP-FTIR (East)	442

**Table G-105. 10/4/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/4/2008	9:42	10:20	Six	Coal, iron ore scrap, empty

**Table G-106. AM Flux Values Measured during 10/4/ 2008, Event #2**

Time	AM Flux (g/s)
9:46:51	wc
9:49:32	0
9:52:14	0.001
9:54:56	0.001
9:57:38	0.002
10:00:17	0.002
10:02:58	0.002
10:05:40	0.002
10:08:20	0.002
10:11:01	0.001
10:13:41	0.002
<b>Average:</b>	<b>0.002</b>

wc Wind criteria was not met.

**Table G-107. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/4/ 2008, Event #2**

Path	Methane
EPA OP-FTIR (West)	ND
ARCADIS OP-FTIR (East)	248

**Table G-108. 10/4/ 2008 Event #3**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/4/2008	11:01	11:41	Five	Lube oil

**Table G-109. AM Flux Values Measured during 10/4/ 2008, Event #3**

Time	AM Flux (g/s)
11:04:32	0.004
11:07:11	0.005
11:09:48	0.003
11:12:26	0.001
11:15:03	0
11:17:42	0
11:20:21	0
11:22:59	0
11:25:40	wc
11:28:20	wc
11:31:01	wc
11:33:39	wc
<b>Average:</b>	<b>0.002</b>

wc Wind criteria was not met.

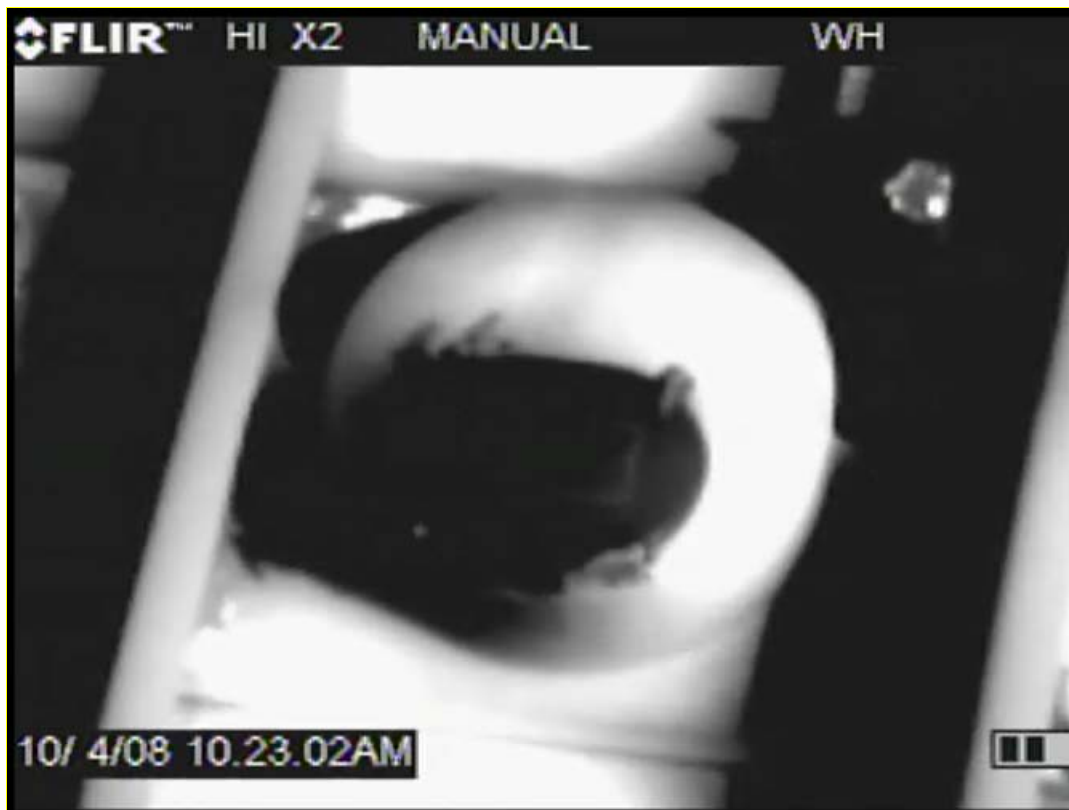


Figure G-7. Screenshot from FLIR Camera Showing Leak from 10/4/ 2008, Event #3

Table G-110. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/4/ 2008, Event #3

Path	Methane
EPA OP-FTIR (West)	46.2
ARCADIS OP-FTIR (East)	41.5

Table G-111. 10/4/ 2008 Event #4

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/4/2008	12:23	12:54	Two	Petroleum, iron ore scrap

**Table G-112. AM Flux Values Measured during 10/4/ 2008, Event #4**

<b>Time</b>	<b>AM Flux (g/s)</b>
12:28:04	0.001
12:30:42	0.001
12:33:20	0.002
12:35:59	0.005
12:38:38	0.005
12:41:16	0.005
12:43:54	0.003
12:46:32	0.002
<b>Average:</b>	<b>0.003</b>

**Table G-113. 10/4/ 2008 Event #5**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
10/4/2008	13:12	13:46	Two	Empty

**Table G-114. AM Flux Values Measured during 10/4/ 2008, Event #5**

<b>Time</b>	<b>AM Flux (g/s)</b>
13:15:41	0
13:18:19	0
13:20:59	0
13:23:38	0.003
13:26:17	0.004
13:28:57	0.005
13:31:36	0.004
13:34:15	0.003
13:36:56	0.003
13:39:35	0.003
<b>Average:</b>	<b>0.003</b>

**Table G-115. 10/4/ 2008 Event #6**

<b>Date</b>	<b>Entry Time</b>	<b>Exit Time</b>	<b>Number of Barges</b>	<b>Description of Commodity</b>
10/4/2008	14:21	14:52	Three	Dry sulfur, clay



**Table G-116. AM Flux Values Measured during 10/4/ 2008, Event #6**

Time	AM Flux (g/s)
14:25:49	0.012
14:28:29	0.011
14:31:08	0.009
14:33:46	0.009
14:36:27	0.006
14:39:05	0.007
14:41:43	0.008
14:44:20	0.007
14:46:59	0.007
<b>Average:</b>	<b>0.008</b>

**Table G-117. Average Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/4/ 2008, Event #6**

Path	Methane	2-Methylbutane
EPA OP-FTIR (West)	ND	11.9
ARCADIS OP-FTIR (East)	70.5	10.0

**Table G-118. 10/4/ 2008 Event #7**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/4/2008	15:09	15:44	Two	Welding barges/machinery

**Table G-119. AM Flux Values Measured during 10/4/ 2008, Event #7**

Time	AM Flux (g/s)
15:13:25	0.012
15:16:04	0.012
15:18:42	0.009
15:21:21	0.012
15:24:24	0.009
15:26:38	0.008
15:29:16	0.01
15:31:54	0
15:34:32	0.012
15:37:09	0
<b>Average:</b>	<b>0.008</b>

**Table G-120. 10/4/ 2008 Event #8**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/4/2008	15:53	16:15	Tug with no barges	N/A

**Table G-121. AM Flux Values Measured during 10/4/ 2008, Event #8**

Time	AM Flux (g/s)
15:56:57	0
15:59:35	0
16:02:13	0.009
16:04:53	0.01
16:07:31	0.007
16:10:10	0.002
<b>Average:</b>	<b>0.005</b>

**Table G-122. 10/5/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/5/2008	9:23	10:04	Two	Petroleum

**Table G-123. AM Flux Values Measured during 10/5/ 2008, Event #1**

Time	AM Flux (g/s)
9:26:53	2.483
9:29:31	4.074
9:32:09	4.840
9:34:48	4.023
9:37:25	4.033
9:41:21	4.305
9:43:59	3.302
9:46:40	3.001
9:49:18	2.854
9:51:56	2.895
9:54:35	2.325
9:57:13	2.566
<b>Average:</b>	<b>3.392</b>



Figure G-8. Screenshot from FLIR Camera Showing Leak from 10/5/ 2008, Event #1

Table G-124. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/5/ 2008, Event #1

Path	Methane	Propane	2-Methylbutane
EPA OP-FTIR (West)	172	1159	1157
ARCADIS OP-FTIR (East)	367	757	781

Table G-125. 10/5/ 2008 Event #2

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/5/2008	12:04	12:53	Five	Lube oils, organic industrial chemicals

Table G-126. AM Flux Values Measured during 10/5/ 2008, Event #2

Time	AM Flux (g/s)
12:08:06	0.003
12:10:46	0.003
12:13:27	0.003
12:16:08	0.004
12:18:47	0.005
12:21:29	0.007
12:24:09	0.007
12:26:49	0.007
12:29:31	0.006
12:32:12	0.009
12:34:51	0.009
12:37:32	0.008
12:40:12	0.004
12:42:52	0.004
12:45:33	0.003
12:48:14	0.005
<b>Average:</b>	<b>0.005</b>



Figure G-9. Screenshot from FLIR Camera Showing Leak from 10/5/ 2008, Event #2

**Table G-127. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/5/ 2008, Event #2**

Path	Methane
EPA OP-FTIR (West)	39.7
ARCADIS OP-FTIR (East)	43.2

**Table G-128. 10/6/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/6/2008	9:18	10:03	Two	Petroleum

**Table G-129. AM Flux Values Measured during 10/6/ 2008, Event #1**

Time	AM Flux (g/s)
9:22:14	0.014
9:24:51	0.018
9:27:30	0.018
9:30:07	0.022
9:34:03	0.023
9:36:42	0.022
9:39:19	0.014
9:41:57	0.011
9:44:36	0.012
9:47:15	0.013
9:49:53	0.012
9:52:31	0.011
9:55:09	0.010
9:57:47	0.009
<b>Average:</b>	<b>0.015</b>

**Table G-130. 10/6/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/6/2008	10:07	10:28	One tug	N/A

**Table G-131. AM Flux Values Measured during 10/6/ 2008, Event #2**

Time	AM Flux (g/s)
10:11:00	0.006
10:13:37	0.007
10:16:14	0.003
10:18:52	0.014
10:21:30	0.012
<b>Average:</b>	<b>0.008</b>

**Table G-132. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/6/ 2008, Event #2**

Path	Methane
EPA OP-FTIR (West)	ND
ARCADIS OP-FTIR (East)	60.9

**Table G-133. 10/6/ 2008 Event #3**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/6/2008	12:28	13:00	Six	Empty

**Table G-134. AM Flux Values Measured during 10/6/ 2008, Event #3**

Time	AM Flux (g/s)
12:33:11	0.005
12:35:49	0.005
12:38:27	0.006
12:41:06	0.004
12:43:43	0.002
12:46:22	0
12:49:00	0
12:51:38	0.002
12:54:18	0.006
<b>Average:</b>	<b>0.003</b>

**Table G-135. 10/6/ 2008 Event #4**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/6/2008	13:15	13:51	One	Lube oils

**Table G-136. AM Flux Values Measured during 10/6/ 2008, Event #4**

Time	AM Flux (g/s)
13:18:09	0.004
13:20:48	0.003
<b>Average:</b>	<b>0.004</b>

**Table G-137. 10/6/ 2008 Event #5**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/6/2008	14:29	15:11	Six	Gravel

**Table G-138. AM Flux Values Measured during 10/6/ 2008, Event #5**

Time	AM Flux (g/s)
14:31:47	0.005
14:34:26	0.004
14:37:06	0.004
14:39:47	0.004
14:42:27	0.004
14:45:06	0.003
14:47:48	0.002
14:50:29	0.002
14:53:07	0.002
14:55:49	0.003
14:58:29	0.003
15:01:08	0.002
15:03:49	0.001
15:06:29	0.002
<b>Average:</b>	<b>0.003</b>

**Table G-139. 10/8/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/8/2008	10:10	10:42	Three	Iron Ore Scrap

**Table G-140. AM Flux Values Measured during 10/8/ 2008, Event #1**

Time	AM Flux (g/s)
10:13:59	WC
10:16:36	WC
10:19:18	WC
10:21:56	WC
10:24:34	WC
10:27:15	WC
10:29:53	WC
10:32:33	WC
10:35:12	WC
10:37:50	WC
<b>Average:</b>	<b>WC</b>

wc Wind criteria was not met.

**Table G-141. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/8/ 2008, Event #1**

Path	Methane
EPA OP-FTIR (West)	ND
ARCADIS OP-FTIR (East)	46.7

**Table G-142. 10/8/ 2008 Event #2 [Exit time does not match end time]**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/8/2008	11:05	11:40	Five	Empty, corn, organic chemicals. Dry sulfur, clay. Lube oils.



**Table G-143. AM Flux Values Measured during 10/8/ 2008, Event #2**

Time	AM Flux (g/s)
11:10:18	0.001
11:15:42	0.001
11:21:06	wc
11:23:48	wc
11:26:30	wc
11:31:51	wc
11:34:33	wc
11:38:34	wc
11:41:17	wc
11:44:02	wc
<b>Average:</b>	<b>0.001</b>

wc Wind criteria was not met.

**Table G-144. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/8/ 2008, Event #2**

Path	Methane
EPA OP-FTIR (West)	70.5
ARCADIS OP-FTIR (East)	49.2

**Table G-145. 10/8/ 2008 Event #3**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/8/2008	12:02	12:37	Six	Dry Sulfur, clay

**Table G-146. AM Flux Values Measured during 10/8/ 2008, Event #3**

Time	AM Flux (g/s)
12:04:36	0.001
12:07:21	0.001
12:10:02	0.001
12:18:19	0.002
12:21:02	0.001
12:23:52	0.001
12:26:34	wc
12:31:57	0.001
12:34:36	0.002
12:37:16	0.001
<b>Average:</b>	<b>0.001</b>

**Table G-147. 10/8/ 2008 Event #4**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/8/2008	12:52	13:25	One	Empty

**Table G-148. AM Flux Values Measured during 10/8/ 2008, Event #4**

Time	AM Flux (g/s)
12:53:39	wc
12:56:21	wc
12:58:59	wc
13:04:23	0.001
13:07:03	0.005
13:09:41	0.001
13:20:24	0.001
13:31:04	0.001
<b>Average:</b>	<b>0.002</b>

**Table G-149. 10/9/ 2008 Event #1**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/9/2008	8:07	8:38	One	Empty

**Table G-150. AM Flux Values Measured during 10/9/ 2008, Event #1**

Time	AM Flux (g/s)
8:11:33	0.002
8:15:14	0.002
8:17:56	0.001
8:20:35	0.001
8:23:18	wc
8:25:59	wc
8:28:41	wc
8:34:05	wc
<b>Average:</b>	<b>0.002</b>

wc Wind criteria was not met.

**Table G-151. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/9/ 2008, Event #1**

Path	Methane
EPA OP-FTIR (West)	211
ARCADIS OP-FTIR (East)	346

**Table G-152. 10/9/ 2008 Event #2**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/9/2008	8:51	9:34	One	Petroleum products

**Table G-153. AM Flux Values Measured during 10/9/ 2008, Event #2**

Time	AM Flux (g/s)
8:55:28	0.002
8:58:09	0.002
9:00:52	0.003
9:03:32	0.003
9:06:15	0.006
9:08:54	0.008
9:11:36	0.010
9:16:57	0.005
9:19:39	0.006
9:22:20	0.017
9:25:00	0.018
9:27:42	0.014
<b>Average:</b>	<b>0.008</b>

**Table G-154. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/9/ 2008, Event #2**

Path	Methane
EPA OP-FTIR (West)	ND
ARCADIS OP-FTIR (East)	236

**Table G-155. 10/9/ 2008 Event #3**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/9/2008	10:05	10:52	Four	Organic industrial chemicals.



**Table G-156. AM Flux Values Measured during 10/9/ 2008, Event #3**

Time	AM Flux (g/s)
10:08:00	0.006
10:10:40	0.005
10:13:20	0.003
10:16:01	0.004
10:18:42	0.003
10:21:21	0.003
10:23:43	0.004
10:26:50	0.006
10:29:27	0.009
10:32:05	0.007
10:34:42	0.004
10:37:21	0.004
10:39:58	0.005
10:42:36	0.006
10:45:14	0.013
10:48:15	0.012
10:50:29	0.005
<b>Average:</b>	<b>0.006</b>

**Table G-157. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/9/ 2008, Event #3**

Path	Methane	2-Methylbutane
EPA OP-FTIR (West)	147	14.1
ARCADIS OP-FTIR (East)	183	16.0

**Table G-158. 10/9/ 2008 Event #4**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/9/2008	11:36	12:13	One	Petroleum Products

**Table G-159. AM Flux Values Measured during 10/9/ 2008, Event #4**

Time	AM Flux (g/s)
11:36:32	0.017
11:39:10	0.012
11:41:48	0.007
11:44:27	0.014
11:47:05	0.037
11:49:43	0.051
11:52:21	0.059
11:55:01	0.049
11:57:37	0.033
12:00:15	0.018
12:02:52	0.025
12:05:30	0.029
12:08:08	0.024
12:10:45	0.011
12:13:22	0.008
12:15:59	0.009
12:18:37	0.009
<b>Average:</b>	<b>0.024</b>

**Table G-160. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/9/ 2008, Event #4**

Path	Methane	2-Methylbutane
EPA OP-FTIR (West)	104	22.5
ARCADIS OP-FTIR (East)	72.8	25.0

**Table G-161. 10/9/ 2008 Event #5**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/9/2008	12:23	13:45	One tug two barges, One tug with four barges	Five empty barges, one with petroleum,

**Table G-162. AM Flux Values Measured during 10/9/ 2008, Event #5**

<b>Time</b>	<b>AM Flux (g/s)</b>
12:23:52	0.011
12:26:30	0.009
12:29:08	0.013
12:31:47	0.011
12:34:26	0.013
12:37:04	0.009
12:39:42	0.014
12:42:21	0.019
12:45:45	0.018
12:47:38	0.019
12:50:16	0.016
12:54:13	0.012
12:56:51	0.022
12:59:29	0.021
13:02:07	0.015
13:04:45	0.017
13:07:23	0.015
13:10:01	0.018
13:12:38	0.017
13:15:17	0.015
13:17:56	0.012
13:20:34	0.014
13:23:13	0.017
13:25:51	0.020
13:28:31	0.017
13:31:08	0.017
13:33:49	0.020
13:36:28	0.018
13:39:07	0.014
<b>Average:</b>	<b>0.016</b>

**Table G-163. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/9/ 2008, Event #5**

<b>Path</b>	<b>Methane</b>	<b>2-Methylbutane</b>
EPA OP-FTIR (West)	71.2	ND
ARCADIS OP-FTIR (East)	61.0	14.8

**Table G-164. 10/9/ 2008 Event #6**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/9/2008	14:05	14:34	Four	Empty

**Table G-165. AM Flux Values Measured during 10/9/ 2008, Event #6**

Time	AM Flux (g/s)
14:08:10	0.016
14:10:50	0.018
14:13:28	0.021
14:16:06	0.024
14:20:03	0.018
14:22:41	0.019
14:25:19	0.02
14:28:00	0.026
<b>Average:</b>	<b>0.020</b>

**Table G-166. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/9/ 2008, Event #6**

Path	Methane
EPA OP-FTIR (West)	44.0
ARCADIS OP-FTIR (East)	39.7

**Table G-167. 10/9/ 2008 Event #7**

Date	Entry Time	Exit Time	Number of Barges	Description of Commodity
10/9/2008	14:47	15:25	Two	Petroleum products, Empty



Table G-168. AM Flux Values Measured during 10/9/ 2008, Event #7

Time	AM Flux (g/s)
14:37:13	0.015
14:39:52	0.053
14:42:32	0.143
14:51:46	0.286
14:54:24	0.331
14:57:02	0.635
14:59:40	0.794
15:02:17	0.819
15:04:55	0.877
15:07:32	0.661
15:10:11	0.432
15:12:49	0.206
15:15:28	0.18
15:18:05	0.174
15:20:44	0.064
<b>Average:</b>	<b>0.378</b>



Figure G-10. Screenshot from FLIR Camera Showing Leak from 10/9/ 2008, Event #7



**Table G-169. Trace Compound Concentrations (ppb) Detected Along the Ground Level Beam Path of the VRPM Configurations during 10/9/ 2008, Event #7**

Path	Methane	Propane	2-Methylbutane
EPA OP-FTIR (West)	40.3	258	228
ARCADIS OP-FTIR (East)	46.0	160	158

**Instances of Emissions Detected with the PGIE but not with ORS Measurements**

An analysis of the PGIE observations made by the LSI Ground Crew and ARCADIS personnel in the lock revealed that there were instances where the PGIE detected barge leaks, but the events were not detected by the ORS instrumentation deployed on the southern side of the lock. Table G-170 presents a summary of seven events that were detected by the PGIE but not the ORS instrumentation. The table includes the date and time of the events, as well as the average prevailing wind direction during the time the PGIE detected the leaks.

**Table G-170. Summary of Leak Events Detected by the PGIE but not ORS Instrumentation**

Date	Time	Barge Number(s)	Prevailing Wind Direction (degrees)
9/28	11:30 am	323, 348	120
9/29	4:32 pm	28038	320
9/30	2:46 pm	28068, 29030	300
10/2	10:25 am	3001, 3003	140
10/2	1:00 pm	00217, 9977, 500, 9, 230	180
10/2	2:35 pm	3027, 3116, 3168	150
10/8	9:21 am	940B, 1842, 5214	320

The orientation of the ORS measurement planes (when looking from the OP-FTIR to the scissor lift) was 133° and 311° for the EPA and ARCADIS OP-FTIR measurement planes, respectively. Considering the ORS configurations used in the study, a prevailing wind direction of approximately 41° is ideal for emissions measurements (perpendicular to the configuration planes). As can be seen in Table G-170, the prevailing winds during the events not detected by the ORS instrumentation were close to parallel to the measurement configurations, or in some cases the winds were not from the direction of the lock (wind direction greater than 133° or less than 311°). The prevailing winds during the times the leaks were detected by the PGIE did not carry the winds through the ORS measurement plane, which explains why the leaks were not detected by the ORS instrumentation.

## Evaluation of AM Emissions from Tugs

In order to evaluate the contribution of exhaust from the tugs to the Alkane Mixture (AM) hydrocarbon emissions fluxes measured during the project, carbon monoxide concentrations were analyzed along the ground level beam path of the ARCADIS OP-FTIR VRPM configuration. Carbon monoxide was chosen for this analysis because it is a by-product of combustion, and has relatively low detection limits with the OP-FTIR instrument. For the nine events detected from barges classified as “empty-no further information”, the carbon monoxide and total hydrocarbon concentrations measured along the ground level beam path were compared to investigate any possible correlations between the two compounds. A correlation between the two compounds would suggest that the source of the total hydrocarbon emissions measured was the emissions from the tug engines.

Of the nine events analyzed, eight of the events showed no correlation between the measured carbon monoxide and total hydrocarbon concentrations. The analysis did indicate a strong correlation between the concentrations of the two compounds during the 9/28/08 9:38 am to 10:11 am event ( $r^2=0.87$ ). However, the total hydrocarbon concentrations measured during this event were relatively low and close to the minimum detection limits of the OP-FTIR instrument. Based on these findings, we conclude that emissions of total hydrocarbons from the tug exhaust are negligible.

## **APPENDIX H**

LDEQ Onboard Leak Bagging Test Report: Barge Emissions  
Measurement Project Final Report; SAGE Environmental Consulting  
(December 29, 2008)



*"Friendly Service, No Surprises!"*

**BAGGING TEST REPORT:  
Barge Emission Measurement Project  
Final Report**

**Prepared for:**

**Louisiana Department of Environmental Quality  
Baton Rouge, Louisiana**

**Prepared by:**

**Graham Harris  
Sage Environmental  
Austin, Texas**

## Table of Contents

1. Introduction.....	3
2. Results.....	3
3. Bagging Methodology .....	15
4. Analytical Procedures .....	15
5. Quality Assurance/Quality Control (QA/QC) .....	16

## List of Tables

1	Summary of Total Non-Methane Hydrocarbon Mass Emissions Results .....	4
2	Summary of Chemical Compound Mass Emission Results .....	5-14
3	Summary of Duplicate/Triplicate Sampling Variability.....	20
4	Summary of Bagging System Known Leak Rate Tests.....	21
5	Summary of Dry Gas Meter Calibration Tests .....	21

## Appendices

Appendix A – Bagging Field Data

Appendix B – EPA Protocol Bagging Procedures

Appendix C –Laboratory Results with QC Data

## **1.0 INTRODUCTION**

This report documents the results of bagging tests performed on low vapor pressure tank barges in the Baton Rouge, Louisiana area from September 24 to 28, 2008, while under contract to the Louisiana Department of Environmental Quality. The bagging tests were intended to determine the mass of hydrocarbon emissions that would add to the VOC emission inventory around Baton Rouge and could be contributing to excess ozone formation. This report includes sections describing the results, methodology, and QA/QC related to the bagging tests.

## **2.0 RESULTS**

During the five day bagging program, a total of 23 leak points from a total of 8 barges were bagged to determine mass emission rates. The total hydrocarbon emission results of the bagging tests are summarized in Table 1 and individual compound emission rates are presented in Table 2. Two sets of sampling data were collected from each bagged component, along with a single canister sample for analysis. The reported emission rates represent the average of the two sampling runs. The bagging field data was recorded electronically, and copies of the data sheets for each test are included as Appendix A. The laboratory analytical data are presented in Appendix C, including a list of all chemical compounds for which a specific analysis was performed (presented in both alpha-numeric and carbon number order).

The emission figures in Tables 1 and 2 are presented in pounds per hour. The leak rates from these barge tanks are driven by vapor pressure and volume expansion, both of which vary with temperature. The ambient temperature has both seasonal and diurnal variations, so there is considerable uncertainty in extrapolating the measured emissions to an annual basis. As a rough assumption, if the measured rates persist for 12 hours per day (daylight warming time) and 365 days per year, the total emissions for the 23 leak points tested would be around 465 tons per year. See Section 5 for additional discussion of uncertainties.



**Table 1. Summary of Total Non-Methane Hydrocarbon Mass Emission Results**

Test #	Barge #	Cargo	Canister Number	Point Tested	Test Type <sup>1</sup>	Total Non Methane Hydrocarbon	
						Volumetric Leak, scfm	Mass Leak, lb/hour
1	G1	Unleaded Gasoline	1481	#2 Center Ullage Hatch	DGM	1.93	20.12
2	G2	Trans Mix	1374	#3 Starboard Cargo Hatch	DGM	0.22	2.48
3	G2	Trans Mix	1322	#2 Starboard Cargo Hatch	Vacuum	0.41	4.56
4	G2	Trans Mix	1397	#2 Port Cargo Hatch	Vacuum	1.95	14.77
5	G2	Trans Mix	1490	Starboard Lower Butterworth Hatch	Vacuum	0.23	2.58
6	G3	Trans Mix	1502	PV Bullet Valve	DGM	0.63	7.09
7	G3	Trans Mix	1375	Vent Stack (leaking Butterfly valve)	DGM	0.94	10.50
8	G4	Naphtha but cleaned	1470	#1 Port Cargo & Ullage Hatch	DGM	0.19	2.48
9	G4	Naphtha but cleaned	1478	#2 Starboard Cargo Ullage Hatch	DGM	0.11	1.46
10	G4	Naphtha but cleaned	1418	#3 Starboard Cargo Ullage Hatch	Vacuum	0.14	1.89
11	G4	Naphtha but cleaned	1394	#2 Port Cargo Valve	DGM	0.08	1.01
12	G4	Naphtha but cleaned	None	# Starboard Stripping Valve	DGM	0.05	0.59
13	G4	Naphtha but cleaned	None	#3 Port Cargo Valve	DGM	0.13	1.62
14	G5	Raffinate	1396	#1 Port Cargo Valve	DGM	1.26	16.78
15	G5	Raffinate	1348	#1 Port Ullage Hatch	Vacuum	0.44	5.81
16	G5	Raffinate	1431	#3 Starboard Cargo Ullage Hatch	Vacuum	0.85	11.32
17	G5	Raffinate	1347	Starboard High Level Alarm Test	Vacuum	0.04	0.52
18	G6	Gasoline	1376	Vent Stack	DGM	1.05	11.54
19	G6	Gasoline	1482	Forward Cofferdam Hatch	Vacuum	1.51	15.77
20	G7	Naphtha	1462	No. 2 Starboard Cargo Hatch	DGM	2.12	24.80
21	G7	Naphtha	None	PV Vent	DGM	0.45	5.26
22	G8	Unleaded Gasoline	1359	PV Vent	DGM	4.32	45.92
23	G8	Unleaded Gasoline	1491	Slop Tank PV Vent	DGM	0.36	3.70
<b>Totals</b>						<b>19.40</b>	<b>212.56</b>

<sup>1</sup> DGM means “dry gas meter direct drive test”. Vacuum means “vacuum bagging method”.

**Table 2. Summary of Chemical Compound Mass Emission Results**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		1,2,3 Trimethylbenzene	1,2,4 Trimethylbenzene	1,3,5 Trimethylbenzene	1,3 butadiene	1 Butene	1 Hexene
1	Unleaded Gasoline	8.85E 04	5.21E 03	2.10E 03	2.03E 03	7.18E 02	1.36E 02
2	Trans Mix	7.51E 05	4.06E 04	1.89E 04	6.85E 04	2.47E 02	8.08E 03
3	Trans Mix	3.59E 05	8.92E 04	4.02E 04	1.02E 03	4.00E 02	1.50E 02
4	Trans Mix	1.33E 04	4.03E 03	1.59E 03	3.26E 03	1.25E 01	4.91E 02
5	Trans Mix	5.78E 05	1.84E 03	6.84E 04	4.74E 04	2.05E 02	9.20E 03
6	Trans Mix	1.25E 04	7.57E 04	3.49E 04	1.13E 03	3.74E 02	1.21E 02
7	Trans Mix	4.28E 05	1.61E 03	7.01E 04	1.47E 03	5.42E 02	1.73E 02
8	Naphtha but cleaned	4.52E 04	5.92E 03	3.82E 03	2.11E 04	1.44E 04	5.30E 04
9	Naphtha but cleaned	2.98E 04	3.14E 03	2.52E 03	1.11E 04	2.63E 04	2.53E 04
10	Naphtha but cleaned	8.98E 04	6.91E 03	4.71E 03	1.59E 04	2.60E 04	5.39E 04
11	Naphtha but cleaned	3.58E 04	1.56E 03	2.00E 03	6.87E 05	6.87E 05	2.01E 04
12	Naphtha but cleaned	2.11E 04	9.16E 04	1.18E 03	4.04E 05	4.04E 05	1.18E 04
13	Naphtha but cleaned	5.77E 04	2.51E 03	3.23E 03	1.11E 04	1.11E 04	3.24E 04
14	Raffinate	2.23E 04	2.32E 03	1.50E 03	9.74E 04	4.55E 04	5.65E 03
15	Raffinate	1.00E 04	1.39E 03	7.19E 04	0.00E+00	4.30E 04	9.40E 03
16	Raffinate	4.11E 04	3.15E 03	1.82E 03	2.74E 04	6.50E 04	1.26E 02
17	Raffinate	1.45E 05	9.35E 05	5.20E 05	2.54E 05	1.06E 05	6.67E 04
18	Gasoline	1.65E 03	8.47E 03	3.25E 03	7.34E 04	3.50E 02	2.28E 02
19	Gasoline	1.38E 04	7.14E 03	2.44E 03	1.56E 03	5.46E 02	1.50E 02
20	Naphtha	2.62E 03	2.94E 02	8.46E 03	5.27E 04	2.08E 02	3.65E 03
21	Naphtha	5.56E 04	6.23E 03	1.80E 03	1.12E 04	4.43E 03	7.75E 04
22	Unleaded Gasoline	2.07E 04	1.22E 02	4.94E 03	3.68E 02	9.21E 01	4.29E 02
23	Unleaded Gasoline	4.30E 05	1.15E 03	5.56E 04	3.34E 03	8.55E 02	8.05E 04
<b>Totals, pounds per hour</b>		1.01E 02	1.07E 01	4.90E 02	5.51E 02	1.50E+00	2.41E 01

**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		1 Pentene	2,2,4 Trimethylpentane	2,2 Dimethylbutane	2,3,4 Trimethylpentane	2,3 Dimethylbutane	2,3 Dimethylpentane
1	Unleaded Gasoline	1.47E 01	1.21E 01	4.89E 03	2.75E 02	1.40E 01	3.25E 02
2	Trans Mix	5.03E 02	4.82E 03	1.23E 03	8.20E 04	2.68E 02	4.04E 03
3	Trans Mix	9.69E 02	8.54E 03	2.39E 03	9.52E 04	7.80E 03	9.98E 04
4	Trans Mix	3.11E 01	2.92E 02	7.63E 03	3.38E 03	2.55E 02	3.44E 03
5	Trans Mix	5.38E 02	5.52E 03	8.09E 03	6.75E 04	4.63E 03	6.32E 04
6	Trans Mix	1.03E 01	8.62E 03	9.07E 03	1.19E 03	1.31E 02	3.32E 02
7	Trans Mix	1.52E 01	1.27E 02	1.32E 02	1.80E 03	1.92E 02	4.94E 02
8	Naphtha but cleaned	2.45E 04	5.27E 05	4.88E 03	6.42E 04	1.32E 02	1.44E 02
9	Naphtha but cleaned	1.16E 04	4.49E 05	2.60E 03	6.22E 05	7.28E 03	8.72E 03
10	Naphtha but cleaned	1.27E 04	5.05E 05	3.73E 03	3.61E 04	1.06E 02	1.12E 02
11	Naphtha but cleaned	1.01E 04	1.01E 02	1.90E 03	3.03E 04	5.23E 03	3.84E 03
12	Naphtha but cleaned	5.93E 05	5.96E 03	1.12E 03	1.79E 04	3.08E 03	2.26E 03
13	Naphtha but cleaned	1.62E 04	1.63E 02	3.06E 03	4.89E 04	8.43E 03	6.18E 03
14	Raffinate	2.59E 03	1.16E 02	7.96E 01	2.59E 04	6.42E 01	4.28E 01
15	Raffinate	1.06E 03	3.42E 03	2.56E 01	1.43E 04	9.51E 01	5.35E 02
16	Raffinate	2.16E 03	5.60E 03	5.24E 01	2.05E 04	1.80E+00	9.79E 02
17	Raffinate	9.30E 05	2.56E 04	2.23E 02	1.43E 05	8.57E 02	4.59E 03
18	Gasoline	1.20E 01	1.08E 01	3.56E 02	2.53E 03	2.85E 01	2.92E 02
19	Gasoline	1.65E 01	8.64E 02	4.43E 02	1.66E 03	1.28E 02	1.59E 03
20	Naphtha	4.78E 02	4.93E 02	3.09E 01	2.00E 03	2.04E 01	1.46E 02
21	Naphtha	1.02E 02	1.05E 02	6.57E 02	4.24E 04	4.34E 02	3.09E 03
22	Unleaded Gasoline	2.14E 01	9.97E 02	2.16E 01	2.61E 02	3.74E 01	9.99E 02
23	Unleaded Gasoline	1.55E 02	5.53E 03	1.40E 02	1.09E 04	2.11E 02	5.06E 03
<b>Totals, pounds per hour</b>		1.49E+00	6.03E 01	2.35E+00	7.18E 02	4.71E+00	9.08E 01

**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		2,4 Dimethylpentane	2 Methylheptane	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
1	Unleaded Gasoline	2.91E 02	1.07E 02	6.56E 02	2.03E 02	1.09E 02	6.46E 02
2	Trans Mix	2.66E 03	2.96E 03	1.28E 02	1.04E 01	1.99E 03	1.17E 02
3	Trans Mix	4.70E 03	6.90E 04	2.27E 02	1.21E 02	1.05E 04	6.73E 04
4	Trans Mix	1.59E 02	2.41E 03	7.76E 02	3.93E 02	3.74E 04	2.29E 03
5	Trans Mix	2.92E 03	1.83E 03	1.47E 02	7.43E 03	1.00E 03	4.48E 04
6	Trans Mix	7.02E 02	6.26E 04	1.29E 03	2.31E 02	5.84E 05	2.82E 02
7	Trans Mix	1.04E 01	9.53E 04	1.89E 03	3.35E 02	8.70E 05	4.20E 02
8	Naphtha but cleaned	6.27E 03	2.82E 03	3.20E 02	6.65E 02	1.40E 03	3.85E 02
9	Naphtha but cleaned	3.72E 03	1.85E 03	1.94E 02	3.68E 02	9.19E 04	2.34E 02
10	Naphtha but cleaned	5.11E 03	1.76E 03	2.46E 02	5.43E 02	8.51E 04	2.94E 02
11	Naphtha but cleaned	2.53E 03	1.15E 03	1.27E 02	2.64E 02	5.86E 04	1.54E 02
12	Naphtha but cleaned	1.49E 03	6.79E 04	7.49E 03	1.55E 02	3.45E 04	9.06E 03
13	Naphtha but cleaned	4.07E 03	1.86E 03	2.05E 02	4.25E 02	9.44E 04	2.48E 02
14	Raffinate	1.20E 01	5.39E 03	1.99E 03	2.63E+00	3.78E 03	4.62E 01
15	Raffinate	3.77E 02	4.20E 04	1.27E 01	6.95E 03	3.30E 04	1.37E 01
16	Raffinate	7.08E 02	1.13E 03	2.35E 01	1.29E 02	6.59E 04	2.53E 01
17	Raffinate	3.29E 03	3.89E 05	1.08E 02	6.63E 04	2.70E 05	1.17E 02
18	Gasoline	2.22E 02	7.59E 03	6.67E 02	1.82E 02	5.05E 03	6.52E 02
19	Gasoline	2.16E 02	9.24E 03	5.79E 02	2.06E 02	8.51E 03	1.54E 03
20	Naphtha	1.97E 02	1.93E 02	8.07E 02	7.97E 01	4.20E 02	9.75E 02
21	Naphtha	4.19E 03	4.10E 03	1.71E 02	1.69E 01	8.92E 03	2.07E 02
22	Unleaded Gasoline	3.29E 02	3.20E 03	1.23E 03	1.27E+00	6.37E 03	1.00E 01
23	Unleaded Gasoline	1.75E 03	1.00E 03	4.02E 05	7.76E 02	8.57E 04	5.07E 03
<b>Totals, pounds per hour</b>		5.87E 01	8.18E 02	9.13E 01	5.48E+00	9.61E 02	1.44E+00

**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		3 Methylpentane	Acetylene	Benzene	cis 2 Butene	cis 2 Pentene	Cumene
1	Unleaded Gasoline	2.28E 01	0.00E+00	1.41E 01	2.60E 01	1.54E 01	1.09E 03
2	Trans Mix	5.37E 02	2.20E 05	1.01E 02	2.36E 02	4.76E 02	8.65E 05
3	Trans Mix	9.74E 02	9.05E 05	1.91E 02	4.40E 02	9.07E 02	1.61E 04
4	Trans Mix	3.21E 01	1.40E 04	6.47E 02	1.40E 01	2.90E 01	5.36E 04
5	Trans Mix	5.87E 02	6.81E 05	1.24E 02	2.27E 02	5.15E 02	1.71E 04
6	Trans Mix	1.49E 01	4.78E 05	2.41E 02	9.70E 02	1.84E 01	9.80E 05
7	Trans Mix	2.20E 01	1.33E 04	3.58E 02	1.42E 01	2.74E 01	2.24E 04
8	Naphtha but cleaned	4.81E 02	1.92E 04	2.20E 02	1.53E 04	1.92E 04	3.53E 03
9	Naphtha but cleaned	2.70E 02	1.24E 04	1.25E 02	0.00E+00	2.60E 04	2.29E 03
10	Naphtha but cleaned	3.96E 02	2.02E 04	1.77E 02	1.73E 04	1.85E 04	3.42E 03
11	Naphtha but cleaned	1.93E 02	9.92E 05	7.76E 03	6.49E 05	7.02E 05	1.50E 03
12	Naphtha but cleaned	1.13E 02	5.84E 05	4.57E 03	3.82E 05	4.13E 05	8.84E 04
13	Naphtha but cleaned	3.10E 02	1.60E 04	1.25E 02	1.05E 04	1.13E 04	2.42E 03
14	Raffinate	2.03E+00	1.76E 04	2.51E+00	8.70E 04	4.77E 03	7.16E 04
15	Raffinate	7.19E 01	0.00E+00	8.31E 01	3.22E 04	1.83E 03	2.62E 04
16	Raffinate	1.37E+00	0.00E+00	1.64E+00	7.19E 04	3.99E 03	4.41E 04
17	Raffinate	6.47E 02	1.47E 05	7.67E 02	2.78E 05	1.61E 04	2.22E 05
18	Gasoline	1.76E 01	1.47E 04	1.24E 01	1.80E 01	2.94E 01	1.40E 03
19	Gasoline	1.98E 01	1.73E 04	1.18E 01	2.67E 01	1.75E 01	9.52E 04
20	Naphtha	4.38E 01	5.59E 04	8.01E 02	1.81E 02	4.35E 02	7.01E 03
21	Naphtha	9.30E 02	1.19E 04	1.70E 02	3.85E 03	9.24E 03	1.49E 03
22	Unleaded Gasoline	6.97E 01	8.42E 03	1.06E 01	8.13E 01	2.30E 01	1.30E 03
23	Unleaded Gasoline	4.08E 02	7.83E 04	5.52E 03	6.39E 02	1.60E 02	1.64E 04
<b>Totals, pounds per hour</b>		<b>7.13E+00</b>	<b>1.17E 02</b>	<b>5.89E+00</b>	<b>2.08E+00</b>	<b>1.87E+00</b>	<b>3.02E 02</b>

**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		Cyclohexane	Cyclopentane	Ethane	Ethylbenzene	Ethylene	Isobutane
1	Unleaded Gasoline	1.62E 02	5.66E 02	1.39E 01	1.50E 02	0.00E+00	4.46E+00
2	Trans Mix	4.92E 03	1.78E 02	4.77E 02	6.20E 04	1.73E 03	6.18E 02
3	Trans Mix	1.99E 03	3.31E 02	7.53E 02	2.75E 03	2.83E 03	9.63E 03
4	Trans Mix	6.70E 03	1.07E 01	2.05E 01	1.07E 02	7.40E 03	2.86E 02
5	Trans Mix	1.08E 03	1.93E 02	2.89E 02	2.69E 03	9.41E 04	7.21E 03
6	Trans Mix	9.62E 04	3.46E 02	5.12E 02	2.52E 03	9.88E 04	1.02E 01
7	Trans Mix	1.40E 03	5.13E 02	7.51E 02	4.05E 03	1.44E 03	1.46E 01
8	Naphtha but cleaned	7.85E 02	1.57E 02	3.38E 02	1.05E 02	1.92E 04	4.16E 02
9	Naphtha but cleaned	4.65E 02	8.53E 03	1.86E 02	6.33E 03	1.24E 04	1.98E 02
10	Naphtha but cleaned	6.42E 02	1.26E 02	2.47E 02	7.53E 03	2.02E 04	2.67E 02
11	Naphtha but cleaned	5.09E 05	6.17E 03	1.27E 02	3.13E 03	1.15E 04	1.45E 02
12	Naphtha but cleaned	2.99E 05	3.63E 03	7.45E 03	1.84E 03	6.74E 05	8.51E 03
13	Naphtha but cleaned	8.20E 05	9.94E 03	2.04E 02	5.05E 03	1.85E 04	2.33E 02
14	Raffinate	4.42E 03	1.28E 01	3.43E 03	3.67E 03	1.12E 04	4.60E 02
15	Raffinate	5.08E 03	2.79E 01	2.30E 03	1.44E 03	1.02E 04	1.34E 02
16	Raffinate	7.65E 03	5.49E 01	3.94E 03	2.28E 03	1.88E 04	2.92E 02
17	Raffinate	3.86E 04	2.46E 02	3.34E 04	1.31E 04	1.15E 05	1.18E 03
18	Gasoline	1.69E 02	1.01E 01	6.52E 02	1.90E 02	1.47E 04	1.59E+00
19	Gasoline	2.39E 03	4.52E 02	9.92E 02	1.13E 02	1.73E 04	2.47E+00
20	Naphtha	1.32E 01	4.04E 01	8.80E 02	1.56E 02	1.28E 03	1.55E+00
21	Naphtha	2.79E 02	8.57E 02	1.87E 02	3.31E 03	2.72E 04	3.29E 01
22	Unleaded Gasoline	1.54E 03	3.28E 01	1.71E 01	1.81E 02	1.37E 02	5.62E+00
23	Unleaded Gasoline	1.72E 03	2.04E 02	2.64E 05	1.39E 03	0.00E+00	5.58E 01
<b>Totals, pounds per hour</b>		4.22E 01	2.34E+00	1.19E+00	1.49E 01	3.22E 02	1.71E+01

**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		Isopentane	Isoprene	m/p Xylene	m Diethylbenzene	Methylcyclohexane	Methylcyclopentane
1	Unleaded Gasoline	3.35E+00	1.21E 02	4.46E 02	1.25E 04	1.29E 02	1.01E 01
2	Trans Mix	7.33E 01	3.27E 03	3.02E 03	2.06E 05	6.59E 03	2.89E 02
3	Trans Mix	1.28E+00	6.48E 03	9.20E 03	1.81E 05	1.26E 03	5.26E 02
4	Trans Mix	4.18E+00	2.09E 02	3.47E 02	1.44E 04	4.31E 03	1.74E 01
5	Trans Mix	7.03E 01	3.58E 03	9.08E 03	9.41E 05	8.34E 04	3.28E 02
6	Trans Mix	2.53E+00	3.92E 03	1.16E 02	3.72E 05	4.38E 03	6.71E 04
7	Trans Mix	3.74E+00	5.49E 03	1.44E 02	5.48E 05	6.62E 03	1.01E 03
8	Naphtha but cleaned	1.23E 01	0.00E+00	6.16E 02	1.65E 04	1.33E 01	7.70E 02
9	Naphtha but cleaned	6.25E 02	0.00E+00	3.86E 02	9.12E 05	8.53E 02	4.41E 02
10	Naphtha but cleaned	8.95E 02	0.00E+00	4.78E 02	3.17E 04	1.02E 01	6.38E 02
11	Naphtha but cleaned	4.50E 02	1.83E 04	1.37E 02	7.63E 05	5.38E 02	3.08E 02
12	Naphtha but cleaned	2.64E 02	1.08E 04	8.07E 03	4.49E 05	3.16E 02	1.81E 02
13	Naphtha but cleaned	7.25E 02	2.95E 04	2.21E 02	1.23E 04	8.67E 02	4.96E 02
14	Raffinate	1.56E+00	7.21E 04	1.50E 02	8.62E 05	1.21E 02	1.41E 01
15	Raffinate	5.71E 01	1.06E 03	3.84E 03	6.35E 05	2.92E 03	4.69E 02
16	Raffinate	1.18E+00	8.35E 04	8.50E 03	1.13E 04	4.00E 03	8.83E 02
17	Raffinate	5.12E 02	1.35E 04	4.33E 04	4.58E 06	2.42E 04	4.23E 03
18	Gasoline	1.79E+00	9.71E 03	6.46E 02	3.19E 04	6.28E 03	9.21E 02
19	Gasoline	2.49E+00	1.30E 02	3.92E 02	2.87E 04	1.56E 03	9.51E 02
20	Naphtha	7.19E+00	4.19E 03	9.19E 02	1.25E 03	2.21E 01	2.69E 01
21	Naphtha	1.53E+00	8.89E 04	1.95E 02	2.65E 04	4.70E 02	5.72E 02
22	Unleaded Gasoline	7.56E+00	2.13E 02	6.71E 02	4.77E 04	4.28E 02	2.70E 01
23	Unleaded Gasoline	5.68E 01	1.62E 03	4.72E 03	5.98E 05	2.24E 03	1.41E 02
<b>Totals, pounds per hour</b>		4.14E+01	1.10E 01	6.33E 01	4.24E 03	8.69E 01	1.75E+00

**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		m Ethyltoluene	n Butane	n Decane	n Heptane	n Hexane	n Nonane
1	Unleaded Gasoline	5.03E 03	4.40E+00	1.16E 04	3.38E 02	1.63E 01	1.09E 03
2	Trans Mix	3.76E 04	1.33E 01	4.92E 05	1.04E 02	3.52E 02	4.45E 04
3	Trans Mix	7.99E 04	2.22E 01	1.67E 04	5.07E 03	8.10E 03	1.10E 03
4	Trans Mix	3.18E 03	7.03E 01	6.66E 04	2.23E 02	2.68E 02	4.34E 03
5	Trans Mix	1.26E 03	1.14E 01	3.33E 04	4.33E 03	5.05E 03	1.14E 03
6	Trans Mix	7.34E 04	1.91E 01	8.29E 05	2.34E 03	1.35E 02	7.21E 04
7	Trans Mix	1.34E 03	2.78E 01	2.77E 04	3.50E 03	1.99E 02	1.46E 03
8	Naphtha but cleaned	6.18E 03	1.11E 01	3.48E 03	7.52E 02	1.01E 01	2.53E 02
9	Naphtha but cleaned	3.89E 03	5.44E 02	2.44E 03	4.64E 02	5.74E 02	1.64E 02
10	Naphtha but cleaned	7.04E 03	7.47E 02	6.04E 03	5.43E 02	8.33E 02	2.36E 02
11	Naphtha but cleaned	2.43E 03	3.92E 02	2.07E 03	2.95E 02	3.99E 02	1.05E 02
12	Naphtha but cleaned	1.43E 03	2.31E 02	1.22E 03	1.74E 02	2.35E 02	6.16E 03
13	Naphtha but cleaned	3.92E 03	6.33E 02	3.33E 03	4.75E 02	6.43E 02	1.69E 02
14	Raffinate	2.03E 03	2.08E 01	1.34E 03	1.74E 01	2.01E+00	4.45E 03
15	Raffinate	9.46E 04	7.25E 02	6.02E 04	5.06E 02	6.81E 01	1.38E 03
16	Raffinate	2.07E 03	1.55E 01	2.02E 03	9.27E 02	1.29E+00	1.73E 03
17	Raffinate	6.91E 05	6.44E 03	7.37E 05	4.16E 03	6.10E 02	1.29E 04
18	Gasoline	7.16E 03	2.61E+00	4.59E 04	3.55E 02	1.32E 01	1.98E 03
19	Gasoline	5.14E 03	3.96E+00	7.63E 04	1.43E 02	1.68E 02	1.75E 03
20	Naphtha	2.12E 02	2.73E+00	1.05E 02	1.50E 01	6.39E 01	2.94E 02
21	Naphtha	4.51E 03	5.80E 01	2.24E 03	3.17E 02	1.36E 01	6.25E 03
22	Unleaded Gasoline	9.67E 03	1.48E+01	1.31E 03	5.63E 02	5.14E 01	4.36E 03
23	Unleaded Gasoline	1.03E 03	1.30E+00	2.74E 04	2.89E 03	2.87E 02	6.61E 04
<b>Totals, pounds per hour</b>		9.15E 02	3.28E+01	3.99E 02	9.64E 01	6.15E+00	1.61E 01



**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		n Octane	n Pentane	n Propylbenzene	n Undecane	o Xylene	o Ethyltoluene
1	Unleaded Gasoline	7.88E 03	8.43E 01	1.97E 03	0.00E+00	1.74E 02	1.75E 03
2	Trans Mix	3.75E 03	2.60E 01	1.08E 04	1.20E 05	1.06E 03	1.23E 04
3	Trans Mix	5.34E 04	4.87E 01	1.94E 04	2.23E 05	3.11E 03	2.69E 04
4	Trans Mix	1.89E 03	1.57E+00	7.40E 04	1.34E 04	1.22E 02	9.80E 04
5	Trans Mix	9.37E 04	2.76E 01	3.18E 04	1.67E 04	3.33E 03	4.21E 04
6	Trans Mix	4.61E 04	4.35E 01	1.75E 04	1.23E 04	2.94E 03	2.14E 04
7	Trans Mix	7.24E 04	6.43E 01	3.82E 04	6.33E 05	4.91E 03	4.15E 04
8	Naphtha but cleaned	7.53E 02	1.34E 01	2.52E 03	8.02E 05	2.29E 02	2.25E 03
9	Naphtha but cleaned	4.82E 02	6.99E 02	1.58E 03	4.52E 05	1.31E 02	1.39E 03
10	Naphtha but cleaned	5.11E 02	1.01E 01	1.73E 03	2.52E 04	1.42E 02	2.67E 03
11	Naphtha but cleaned	1.39E 03	5.06E 02	5.29E 04	4.72E 05	5.17E 03	8.26E 04
12	Naphtha but cleaned	8.16E 04	2.98E 02	3.11E 04	2.78E 05	3.04E 03	4.86E 04
13	Naphtha but cleaned	2.24E 03	8.16E 02	8.53E 04	7.61E 05	8.33E 03	1.33E 03
14	Raffinate	6.84E 03	1.05E+00	9.47E 04	1.07E 04	6.20E 03	7.66E 04
15	Raffinate	1.45E 03	4.39E 01	2.96E 04	5.21E 05	1.75E 03	3.41E 04
16	Raffinate	1.04E 03	8.81E 01	5.59E 04	2.18E 04	2.70E 03	9.28E 04
17	Raffinate	1.11E 04	3.90E 02	1.35E 05	7.74E 06	1.58E 04	2.62E 05
18	Gasoline	1.38E 03	5.65E 01	2.59E 03	1.03E 04	2.17E 02	2.54E 03
19	Gasoline	8.11E 04	7.58E 01	1.69E 03	5.40E 04	1.30E 02	1.98E 03
20	Naphtha	9.22E 02	6.45E+00	1.05E 02	6.70E 04	3.78E 02	9.23E 03
21	Naphtha	1.96E 02	1.37E+00	2.23E 03	1.42E 04	8.03E 03	1.96E 03
22	Unleaded Gasoline	1.53E 03	4.64E+00	2.64E 03	2.09E 04	2.08E 02	3.02E 03
23	Unleaded Gasoline	1.30E 03	3.39E 01	3.57E 04	6.16E 05	1.98E 03	3.40E 04
<b>Totals, pounds per hour</b>		3.21E 01	2.15E+01	3.32E 02	3.16E 03	2.26E 01	3.43E 02

**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour					
		p Diethylbenzene	p Ethyltoluene	Propane	Propylene	Styrene	Toluene
1	Unleaded Gasoline	1.99E 04	2.15E 03	1.92E+00	2.15E 02	4.95E 04	1.55E 01
2	Trans Mix	3.01E 05	1.96E 05	9.79E 02	2.06E 02	6.43E 05	1.16E 02
3	Trans Mix	9.18E 05	3.88E 05	1.46E 01	3.00E 02	3.10E 04	2.45E 02
4	Trans Mix	3.99E 04	1.60E 04	4.16E 01	8.35E 02	1.31E 03	9.09E 02
5	Trans Mix	8.05E 05	6.33E 05	6.60E 02	1.27E 02	2.11E 04	1.92E 02
6	Trans Mix	4.67E 05	3.07E 05	5.66E 02	2.24E 02	1.46E 04	2.70E 02
7	Trans Mix	3.85E 05	7.73E 05	8.26E 02	3.22E 02	2.83E 04	4.11E 02
8	Naphtha but cleaned	2.61E 04	1.44E 03	8.94E 02	2.94E 04	1.36E 03	5.20E 02
9	Naphtha but cleaned	9.68E 05	9.22E 04	4.21E 02	1.66E 04	8.67E 04	3.13E 02
10	Naphtha but cleaned	1.21E 04	1.62E 03	5.65E 02	2.50E 04	1.12E 03	3.61E 02
11	Naphtha but cleaned	6.11E 05	6.53E 04	3.20E 02	9.67E 05	5.61E 04	1.72E 02
12	Naphtha but cleaned	3.59E 05	3.84E 04	1.88E 02	5.69E 05	3.30E 04	1.01E 02
13	Naphtha but cleaned	9.84E 05	1.05E 03	5.16E 02	1.56E 04	9.04E 04	2.78E 02
14	Raffinate	1.63E 04	3.51E 04	5.58E 03	1.17E 04	7.26E 04	4.67E 01
15	Raffinate	7.78E 05	1.11E 04	1.88E 03	0.00E+00	1.33E 04	1.47E 01
16	Raffinate	1.51E 04	2.09E 04	3.99E 03	0.00E+00	1.37E 04	3.13E 01
17	Raffinate	5.24E 06	1.09E 05	1.98E 04	0.00E+00	1.35E 05	1.42E 02
18	Gasoline	1.94E 04	3.02E 04	7.72E 01	3.25E 03	5.04E 04	1.71E 01
19	Gasoline	2.97E 04	2.20E 04	1.22E+00	5.38E 03	1.86E 04	1.20E 01
20	Naphtha	1.18E 03	2.39E 03	3.75E 01	1.51E 02	3.43E 03	1.11E 01
21	Naphtha	2.51E 04	5.08E 04	7.97E 02	3.20E 03	7.28E 04	2.37E 02
22	Unleaded Gasoline	3.56E 04	4.51E 04	5.21E 01	9.62E 02	5.35E 04	1.42E 01
23	Unleaded Gasoline	5.46E 05	7.92E 05	5.30E 02	9.03E 03	5.50E 05	8.17E 03
<b>Totals, pounds per hour</b>		4.29E 03	1.32E 02	6.10E+00	3.56E 01	1.44E 02	2.06E+00

**Table 2. Summary of Chemical Compound Mass Emission Results (Cont'd)**

Test #	Cargo	Individual Compound Emissions, pounds per hour			
		trans 2 Butene	trans 2 Pentene	Unidentified <sup>2</sup>	Total NMOC
1	Unleaded Gasoline	2.71E 01	2.85E 01	2.23E+00	2.01E+01
2	Trans Mix	2.69E 02	8.97E 02	4.83E 01	2.48E+00
3	Trans Mix	4.79E 02	1.71E 01	1.47E+00	4.56E+00
4	Trans Mix	1.52E 01	5.48E 01	4.83E+00	1.48E+01
5	Trans Mix	2.45E 02	9.73E 02	8.65E 01	2.58E+00
6	Trans Mix	1.29E 01	4.56E 01	2.21E+00	7.09E+00
7	Trans Mix	1.89E 01	6.79E 01	3.30E+00	1.05E+01
8	Naphtha but cleaned	2.59E 04	2.53E 04	9.31E 01	2.48E+00
9	Naphtha but cleaned	2.14E 04	1.11E 04	5.89E 01	1.46E+00
10	Naphtha but cleaned	4.18E 04	1.50E 04	7.19E 01	1.89E+00
11	Naphtha but cleaned	3.59E 04	1.04E 04	4.79E 01	1.01E+00
12	Naphtha but cleaned	2.11E 04	6.11E 05	2.82E 01	5.92E 01
13	Naphtha but cleaned	5.78E 04	1.67E 04	7.73E 01	1.62E+00
14	Raffinate	1.94E 03	9.14E 03	1.26E+00	1.68E+01
15	Raffinate	5.48E 04	3.32E 03	3.45E 01	5.81E+00
16	Raffinate	1.12E 03	7.76E 03	6.54E 01	1.13E+01
17	Raffinate	3.68E 05	2.99E 04	3.04E 02	5.21E 01
18	Gasoline	1.55E 01	2.43E 01	1.44E+00	1.15E+01
19	Gasoline	2.36E 01	3.26E 01	2.56E+00	1.58E+01
20	Naphtha	6.38E 02	8.83E 02	1.65E+00	2.48E+01
21	Naphtha	1.35E 02	1.87E 02	3.50E 01	5.26E+00
22	Unleaded Gasoline	1.16E+00	5.42E 01	4.00E+00	4.59E+01
23	Unleaded Gasoline	9.50E 02	3.81E 02	2.84E 01	3.70E+00
<b>Totals, pounds per hour</b>		2.57E+00	3.61E+00	3.17E+01	2.13E+02

<sup>2</sup> "Unidentified" would include any hydrocarbon peak for which there was no standard. These compounds are quantified but not identified.

### 3.0 BAGGING METHODOLOGY

The bagging technique is used to measure the mass emissions from equipment leaks. It is documented in the US EPA *Protocol for Equipment Leak Emission Estimates*, 1995 (EPA Protocol, see Appendix B), and those procedures are adopted here by reference. There are two basic variations in the bagging approach: the vacuum method and the blow-through method. Both methods have advantages in certain circumstances, however, during this test program the vacuum method was used exclusively. The only variations from this procedure include:

- € No background bags were taken, since they would have a negligible effect on the results from high leaking components that are the focus of this work;
- € No analytical tests were performed on any liquid leak materials collected, since the objective was to only quantify the vapor leaks;
- € A single canister sample was taken for analysis for most of the points tested; and
- € The dry gas meter was driven directly on components leaking at a rate greater than the pump capacity.

### 4.0 ANALYTICAL PROCEDURES

Samples were collected in evacuated aluminum summa canisters provided by LDEQ. A maximum of one canister was filled for each point tested. One canister was sometimes used for multiple sampling points in the same product service on the same barge. The LDEQ laboratory did the analysis using EPA PAMS analysis by GC/FID. The detailed laboratory results are presented in Appendix C.

Analytical data were compiled for 56 individual chemical compounds, plus an unidentified hydrocarbon and total non-methane hydrocarbons (TNMHC). Compound concentrations were reported in parts per billion as carbon (ppbC). The carbon numbers for each chemical compound were used to calculate the average carbon number for the TNMHC, along with an assumed carbon number of 4.5 for category of unidentified hydrocarbons. The molecular weight of the TNMHC was then calculated as the average carbon number times 14 plus 2, which corresponds to alkane hydrocarbons. This value comes from the generalized alkane formula of  $C_nH_{2n+2}$ , and substituting a carbon atomic weight of 12 and hydrogen of 1, the molecular weight can be expressed as  $14n + 2$ .

## 5.0 QUALITY ASSURANCE/QUALITY CONTROL (QA/QC)

A variety of QA/QC checks were run on both the sampling and analytical portions of this work. This section presents the results of those QA/QC tests. In general the QC activities consisted of the following:

- € Duplicate sampling data collection;
- € Analytical QA/QC;
- € Known leak rate testing; and
- € Dry gas meter calibration check.

### **Duplicate/Triplicate Sampling Data**

Each component tested had sampling data collected in duplicate and about half the runs were tested in triplicate. The duplicate/triplicate data was for flow rate (time elapsed for a given flow volume), temperature, and pressure at the dry gas meter. The flow rates in liters per minute at actual conditions were compared across the duplicate or triplicate runs. The bagging procedure requires that the individual runs agree within  $\pm 20\%$ , in which case the runs are averaged as the final result. These tests showed a variation from  $-17.3\%$  to  $+9.8\%$ . The  $-17.3\%$  result was the first run on a vacuum bagging train run where the plastic bag was observed to collapse around the suction line reducing flow. Two other sampling runs were performed with the plastic held away from the suction line, which showed  $\pm 5.8\%$  variation. The first run at  $-17.3\%$  was discarded because of the known flaw. With that one sampling run discarded, the range of variation in flow data were  $\pm 9.8\%$ . The duplicate/triplicate sampling data is given in Table 3.

### **Analytical QA/QC Data**

A total of 20 canisters were sent to the laboratory for analysis. Standard cylinder gases were used to calibrate the instrument and to check for calibration drift 3 to 4 times during each day of analysis on the barge test canisters. A total of 6 canister blanks were tested. A total of 6 canisters were analyzed in duplicate. Two system blanks were tested. All these QA/QC test results fell within the ranges allowed for the analytical method. Detailed documentation of the analytical data can be found in Appendix C.

## **Known Leak Rate Tests**

A known leak rate check of the bagging system was performed before and after the sampling effort. The known leak-rate test involved introducing a known artificial leak rate into a dummy bag, and then running the bagging test in the normal fashion. The emission rate calculated from the bagging test was then compared to the known artificial leak rate, with a criterion of  $\pm 20\%$  (80% to 120% recovery) of the known rate to pass the test.

The known artificial leak was generated by connecting a cylinder of calibration gas to the dummy bag and operating the bagging test using standard procedures. The flow rate into the bag was measured before and after each leak check using a Dry-Cal flow-measuring device traced to a primary standard.

In Table 4, we present the results of the known leak rate checks done before and after the set of barge bagging tests. The known leak rate tests were done at the beginning of the study before any field samples were collected and again following the completion of the bagging study. The initial and final vacuum method tests showed good results for methane at both the high and low concentration levels. However, it should be noted that the high level calibration gas did not match the concentrations of the large leaks encountered in the barge testing.

## **Dry Gas Meter Calibration Checks**

On 15 out of 23 component tests, the leak rate from the component exceeded the pump rate of the dry gas meter. For these tests, the dry gas meter was disconnected from the pump and the component leak rate was routed directly through the dry gas meter (i.e., the leak was driving the meter with no external driving force). Since this mode of measurement does not use the entire bagging train, the dry gas meter was sent to Carl Poe Company for a calibration check against a National Institute of Standards (NIST) traceable prover. In Table 5, we present the results of testing the dry gas meter at three different flow rates, which cover almost the entire range of flow rates encountered during the barge testing. The dry gas meter was found to have minimal error rates of +1% to +1.5% throughout this range. Since the dry gas meter was found to have a bias toward reading slightly high, the measured flow rates were corrected by a factor of 0.99 (for flow rates under 30 liters/minute) and by a factor of 0.985 (for flow rates greater than 30 liters/minute).

**Table 3. Summary of Duplicate/Triplicate Sampling Variability**

Test #	Run #1		Run #2		Run #3		Average
	Liter/min.	% Deviation	Liter/min.	% Deviation	Liter/min.	% Deviation	
1	66.67	-3.1%	72.99	+6.1%	66.77	-3.0%	68.81
2	14.75	-0.7%	14.96	+0.7%	NA	NA	14.85
3	36.23	+0.1%	36.17	-0.1%	NA	NA	36.20
4	127.90	+1.1%	125.00	-1.1%	NA	NA	126.45
5	36.79	-2.2%	38.41	+2.2%	NA	NA	37.60
6	25.43	-0.8%	25.84	+0.8%	NA	NA	25.64
7	37.71	+3.0%	35.50	-3.0%	NA	NA	36.61
8	81.30	-1.1%	83.45	+1.5%	81.91	-0.4%	82.22
9	63.16	+2.0%	61.16	-1.2%	61.44	-0.8%	61.92
10	114.94	-0.3%	111.73	-3.1%	119.28	+3.4%	115.32
11	36.52	-0.02%	36.28	-0.6%	36.74	+0.6%	36.51
12	21.65	0.0%	21.65	0.0%	NA	NA	21.65
13	59.82	+0.7%	58.94	-0.7%	NA	NA	59.38
14	69.77	+2.4%	66.45	-2.4%	NA	NA	68.11
15	31.53	-17.3% <sup>3</sup>	40.35	+5.8%	35.93	-5.8%	38.14
16	68.81	-4.7%	74.17	+4.7%	NA	NA	71.49
17	6.43	+9.3%	5.33	-9.3%	NA	NA	5.88
18	86.45	-1.2%	88.89	+1.5%	87.27	-0.3%	87.54
19	127.25	+1.2%	124.35	-1.2%	NA	NA	125.80
20	136.99	-3.7%	142.18	-0.1%	147.78	+3.8%	142.32
21	36.36	-1.4%	37.57	+1.9%	36.71	-0.5%	36.88
22	123.95	-8.8%	139.73	+3.6%	141.84	+5.2%	134.88
23	13.93	+0.8%	13.23	-4.3%	14.32	+3.5%	13.83

<sup>3</sup> The suction line was observed to be partially blocked by plastic from the enclosure. The plastic was held away in the next two runs, and a funnel was added inside the bag to minimize this effect in future tests. This run was discarded and was not used to calculate the average for this test.

**Table 4. Summary of Bagging System Known Leak Rate Tests**

Sample Description	Known Leak, kg/hr	Bag Test, kg/hr	Percent Error
Pre Test QA Vacuum High Range	0.000163	0.000151	7.5%
Pre Test QA Vacuum Low Range	0.000017	0.0000148	13.3%
Post Test QA Vacuum High Range	0.00175	0.00160	8.2%
Post Test QA Vacuum Low Range	0.000431	0.000423	2.0%

**Table 5. Summary of Dry Gas Meter Calibration Tests**

Test #	Flow Rate Tested, liter/min.	DGM Percent Error	DGM Correction Factor
1	5	+1%	0.99
2	20	+1%	0.99
3	85	+1.5%	0.985



## Overall Analysis of Uncertainty in Mass Emission Estimates

There are a number of factors which contribute to uncertainty in the measured mass emission estimates, including:

- € Sampling variability;
- € Analytical variability;
- € Leak capture/containment variability;
- € Inter-dependence of multiple leak sites on a barge; and
- € Temperature effects (both diurnal and seasonal).

In addition to these factors causing uncertainty in the measured emissions, there is additional uncertainty in an extrapolation of measured emissions to total emissions from barges in the Baton Rouge area. Each of these uncertainties is discussed below.

### Sampling and Analytical Variability

Sampling variability has been addressed quantitatively in the preceding subsections and falls within the acceptable range for the method. The analytical data provided by the laboratory at the Louisiana Department of Environmental Quality (LDEQ) in Baton Rouge is documented in Appendix C. The analytical procedures included testing blank canisters (6 total), duplicate analyses (6 total), and standard calibration gases (4) with results that fall within the acceptable ranges for the method. Sampling variability is generally greater than analytical variability, and the bagging method is expected to have better than  $\pm 20\%$  variability overall.

### Capture Efficiency

Another part of sampling variability that is outside the quantitative QA/QC tests presented earlier is variability in the capture efficiency of the bag enclosure. There were cases where the FLIR camera could detect leakage around the area where the bag was secured to the component by a combination of duct tape and turnbuckle compression. In most cases, any visible leaks were corrected before sample data were collected. Some bagged components were not imaged with the FLIR camera during bagging, so we do not know if there may have been detectable leakage around the bag on those components. Some other bagged components were imaged, but we could not completely eliminate detectable leakage. Any of these leaks around the bag enclosure would not be directed through the dry gas meter on the 15 direct drive tests. This variable

capture efficiency cannot be quantitatively estimated, but it is clear that this factor would cause the measured emissions to be biased low.

### Inter-Dependence of Leaking Components

The next area of uncertainty is the inter-dependence of leaking components on the barges. The barges have multiple storage compartments that can isolate the stored liquid materials, but we understand, based on conversations with several barge company representatives, that the vapor spaces of all the compartments are connected to a common header going to the pressure/vacuum (P/V) relief valve and the vent stack. The barges tested all operated at low pressures, with P/V relief valves starting to vent at pressures of 1 psig to 6 psig. The seals on the hatches and valve packing are designed to minimize leakage at these low pressure differentials. During the testing, we came to realize that everything we did to one sample point affected the emissions from the other potential leak points around it. The dry gas meter creates only a few inches of water back pressure, but we bagged many leaking components that would inflate the bag, but would not drive the dry gas meter. Presumably this happened because the slight increase in back pressure from the dry gas meter caused the leak to move from the bagged component to a neighboring component. Conversely, when we did a vacuum bagging test, there was the potential to pull hydrocarbons that might have been emitted from another component through the bagged component. Both of these phenomena were verified by imaging with the FLIR camera. We believe that if the vacuum bagging test had been run for all the components on a barge, the sum of the emissions measured could have been greater than the total actual emissions. We did not perform vacuum bagging on all or even a majority of components on any given barge, however, and most of the vacuum bagging emission rates were lower than other direct drive dry gas meter tests on the same barge. Since the majority of the tests were done by direct drive of the dry gas meter, we believe this factor would result in biasing the calculated emissions on the low side.

### Diurnal Temperature Effects

The ambient temperature was observed to have an effect on emission rates from the barges. The helicopter-based FLIR camera found few, if any, leaks during flights before 10 AM, and progressively more leaks as the ambient temperature rose in the afternoon. The barge storage compartments can be likened to atmospheric storage tanks with P/V relief valves that activate at low pressures to protect the structural integrity of the compartment. When ambient temperatures are increasing, the vapor pressure of the stored material increases and the volume of the gas above the stored material expands. This results in higher concentrations of hydrocarbon in the

vapor space and gas escaping through the P/V valve or other imperfectly sealed fittings. Conversely when ambient temperature is decreasing, vapor pressure of the stock is decreasing and the gas volume contracts, which should result in negligible emissions. The P/V valve opens to allow air into the cargo compartment during decreasing temperature operation to protect the compartment from the destructive effects of vacuum, which likely explains the lower TNMHC concentrations found in the laboratory analyses. The bagging tests were performed between about 11:00 AM and 4:00 PM. These times were all during the increasing temperature portion of the day, but not at the peak temperature for the day during daylight savings time with sunset around 7:00 PM. The leak rates measured would likely underestimate the peak leak rate. It is difficult to extrapolate the short-term measured emissions to a daily average basis.

### Seasonal Temperature Effects

The barge measurements reported here were performed in late September. The weather during that week of testing was unseasonably cool, with average daily temperatures ranging from 67.1 °F to 73.2 °F vs. a historical average of about 75 °F for that time period in Baton Rouge. It would be difficult to extrapolate the short-term measured emissions to an annual basis because of seasonal temperature variations, but the leak rates measured are undoubtedly well below the maximum summer emission rates for similarly sealed barges. It is the ozone exceedance times in the summer that are of primary interest to this study, however, so we can say that the measured emission rates would underestimate barge emissions during those critical ozone exceedance days.

### Extrapolation to Untested Components and Barges

The 23 leaking components measured in this project represent less than half of the components on the 8 barges tested for which leaks could be detected by using the Hawk Leak Detection System from the deck of the barge. The components selected for testing were biased towards the larger leaks, but some components with large leaks were not tested because of difficulty in access / making a good seal for the bag and some components with relatively low leak rates were selected to better characterize the range of imaged leaks.

The Leak Surveys, Inc. helicopter crew flying with the Hawk Leak Detection System mounted with a Taylor mount onboard their Robinson 44 Raven II helicopter found numerous other “leaking” barges; however, time did not permit the leak measurement of all the leaking tank barges found. When the Hawk camera was used from the deck of the selected barges, many more

leaking components could typically be imaged than were imaged from the air. It is likely that there were leaks on tank barges not imaged from the air that could have been imaged from the deck of the barge.

In summary, the net emission rate from the 23 components tested was about 212 pounds per hour. Since most of the recognized sources of uncertainty identified in this study would tend to bias the sample results low, it is likely that the actual emissions rate was well in excess of the 212 pounds per hour for the 23 points measured. The total emissions from the dozens of imaged leaks that were not measured, and the hundreds of barges in the Baton Rouge area that were not tested, would be difficult to estimate, but would likely contribute significant emissions beyond the tested components.

## APPENDIX A

### Bagging Field Data Sheets

#### Notes:

These are the field data recorded, and format and types of data included may vary from one test to the next.

Temperature was measured by a dial thermometer mounted in the gas flow path, and many readings exceeded the apparent ambient temperature.

Barometric pressure was measured by a dial barometer mounted to the supports for the dry gas meter.

A Thermo Environmental TVA-1000B analyzer was used to check for approach to steady-state conditions and to provide a rough idea of the concentration of the samples to act as a guide for the laboratory. The TVA proved to be of minimal use for this project, because it flamed out for almost every test. Flame out occurs when the hydrocarbon concentration in the sample is so high that oxygen is displaced to the point where the hydrogen flame in the flame ionization detector is extinguished. An attempt was made to fashion a dilution probe to prevent flame out and get on-scale TVA readings, but the dilution ratio could not be kept constant, and the vast majority of tests experienced flame out even with the dilution probe. None of the TVA data were used in calculation of emission rates.

Abbreviations used on the data sheets include:

Sec	seconds
mmHg	millimeters of mercury barometric pressure
F	° Fahrenheit
baro	barometric pressure
FO	flame out of the TVA
FO w Dil	flame out of the TVA when using the dilution probe
Pure HC	pure hydrocarbon, an assumption for direct flow through the dry gas meter

DGM Test		Test 1	
Barge G1		Unleaded Gasoline	
No. 2 Center Ullage Hatch			
10 liter time		9	sec
10 liter time		8.22	
20 liter time		17.97	
temp	104	F	
baro	759	mm Hg	
canister	1481		

DGM Test		No. 2	
Barge	G2		
	No. 3 starboard cargo hatch		
	Trans Mix		
10 liter time	No. 1	40.68	sec
	No. 2	40.12	sec
	No. 3		sec
Temp	96	F	97
Baro press	764	mm hg	764
TVA	FO w Dil	ppm	
Canister	1374		

Vacuum Bagging Test		No. 3	
Barge	G2		
	No. 2 starboard cargo hatch		
	Trans Mix		
10 liter time	No. 1	14.91	sec
	No. 2	16.56	sec
	No. 3	16.59	
Temp	94	F	94
Baro press	764	mm hg	764
TVA	about 400000 ppm	ppm	
		ppm	
Canister	1322		

Vacuum Bagging Test		No. 4	
Barge	G2		
	No. 2 port cargo hatch		
	Trans Mix		
100 liter time	No. 1	46.91	sec
	No. 2	48	sec
	No. 3		
Temp	99	F	96
Baro press	764	mm hg	763
TVA	FO w Dil	ppm	
		ppm	
Canister	1397		

Vacuum Bagging Test		No. 5	
Barge	G2		
	Starboard Lower Butterworth Hatch		
	Trans Mix		
10 liter time	No. 1	16.31	sec
	No. 2	15.62	sec
	No. 3		
Temp	93	F	93
Baro press	763	mm hg	763
TVA	FO w Dil	ppm	
		ppm	
Canister	1490		

DGM Test		No. 6	
Barge	G3		
	PV Bullet Valve		
	Trans Mix		
10 liter time	No. 1	23.59	sec
	No. 2	23.22	sec
	No. 3		sec
Temp	92	F	94
Baro press	762	mm hg	762
TVA	pure HC	ppm	
Canister	1502		



	No. 7	
G3		
Vent stack		
Trans Mix		
No. 1	15.91	sec
No. 2	16.9	sec
No. 3	21	sec
92	F	92
762	mm hg	762
pure HC	ppm	
1375		

DGM Test		No. 8	9/26/2008	
Barge	G4		11	AM
	No. 1 Port Cargo/Ullage Hatch			
	Naphtha but cleaned			
10 liter time	No. 1	7.38	sec	
10	No. 2	7.19	sec	
20 liter	No. 3	14.65	sec	
Temp	90	F	90	
Baro press	762	mm hg	762	
TVA	pure HC	ppm		
Canister	1470			

DGM Test		No. 9	9/26/2008	
Barge	G4		1120	AM
	No. 2 Starboard Cargo/Ullage Hatch			
	Naphtha but cleaned			
10 liter time	No. 1	9.5	sec	
10	No. 2	9.81	sec	
20 liter	No. 3	19.53	sec	
Temp	95	F	95	
Baro press	763	mm hg	763	
TVA	pure HC	ppm		
Canister	1478			

Vacuum Bag Train		No. 10	9/26/2008	
Barge	G4		1145	AM
	No. 3 Starboard Cargo/Ullage Hatch			
	Naphtha but cleaned			
Liter Time	No. 1	5.22	sec	
10	No. 2	5.37	sec	
20	No. 3	10.06	sec	
Temp	91	F	91	
Baro press	763	mm hg	763	
TVA	FO w Dil	ppm		
Canister	1418			

DGM Direct		No. 11	9/26/2008	
Barge	G4		12	PM
	No. 2 Port Cargo Valve			
	Naphtha but cleaned			
10 liter time	No. 1	16.43	sec	
10	No. 2	16.54	sec	
20 liter	No. 3	32.66	sec	
Temp	93	F	93	
Baro press	763	mm hg	763	
TVA	pure HC	ppm		
Canister	1394			

DGM Direct		No. 12	9/26/2008	
Barge	G4		1220	PM
	No. 2 Starboard Stripping Valve			
	Naphtha but cleaned			
10 liter time	No. 1	27.72	sec	
10	No. 2	27.72	sec	
20 liter	No. 3		sec	
Temp	100	F	100	
Baro press	763	mm hg	763	
TVA	pure HC	ppm		
Canister	None			

DGM Direct		No. 13	9/26/2008	
Barge	G4		1235	PM
	No. 3 Port Cargo Valve			
	Naphtha but cleaned			
10 liter time	No. 1	10.03	sec	
10	No. 2	10.18	sec	
20 liter	No. 3		sec	
Temp	95	F	95	
Baro press	759	mm hg	759	
TVA	pure HC	ppm		
Canister	None			

DGM Direct		No. 14	9/26/2008	
Barge	G5		1335	PM
	No. 1 Port Cargo Valve			
	Raffinate			
10 liter time	No. 1	8.6	sec	
10	No. 2	9.03	sec	
20 liter	No. 3		sec	
Temp	95	F	95	
Baro press	757	mm hg	757	
TVA	pure HC	ppm		
Canister	1396			

Vacuum Bagging		No. 15	9/26/2008	
Barge	G5		1410	PM
	No. 1 Port Ullage Hatch			
	Raffinate			
10 liter time	No. 1	19.03	sec	
10	No. 2	14.87	sec	
20 liter	No. 3	33.4	sec	
Temp	96	F	96	
Baro press	752.5	mm hg	752	
TVA	FO w Dil	ppm		
Canister	1348			

Vacuum Bagging		No. 16	9/26/2008	
Barge	G5		1450	PM
	No. 3 Starboard Cargo Ullage Hatch			
	Raffinate			
10 liter time	No. 1	8.72	sec	
10	No. 2	8.09	sec	
20 liter	No. 3		sec	
Temp	98	F	98	
Baro press	749	mm hg	749	
TVA	3	ppm		
Canister	1431			

Vacuum Bagging		No. 17	9/26/2008	
Barge	G5		1530	PM
	No. 3 Starboard High Level Alarm Tester			
	8			
5 liter time	No. 1	46.65	sec	
5	No. 2	56.25	sec	
	No. 3		sec	
Temp	98	F	98	
Baro press	758	mm hg	758	
TVA		ppm		
Canister	1347			

DGM Test		No. 18	9/27/2008	
Barge	G6		1205	PM
	Vent stack		Gasoline	
Liters Timed				
10	No. 1	6.94	sec	
10	No. 2	6.75	sec	
20	No. 3	13.75	sec	
Temp	90	F	90	
Baro press	758	mm hg	758	
TVA	pure HC	ppm		
Canister	1376			

Vacuum Bag Test		No. 19	9/27/2008	
Barge	G6		1250	PM
	Forward Cofferdam		Gasoline	
Liters Timed				
20	No. 1	9.43	sec	
20	No. 2	9.65	sec	
20	No. 3		sec	
Temp	98	F	100	
Baro press	762	mm hg	762	
TVA	FO w Dil	ppm		
Canister	1482			

DGM		No. 20	9/28/2008	
Barge	G7		1140	PM
	No. 2 Starboard Cargo Hatch		Naphtha	
Liters Timed				
10	No. 1	4.38	sec	
10	No. 2	4.22	sec	
20	No. 3	8.12	sec	
Temp	99	F	100	
Baro press	751.5	mm hg	751	
TVA	Pure HC	ppm		
Canister	1462			
Comments- all hatches and PV connected in vapor space.				
Had to tighten other hatches to get this one to drive DGM.				

DGM		No. 21	9/28/2008	
Barge	G7			PM
	PV Vent		Naphtha	
Liters Timed				
	10	No. 1	16.5	sec
	10	No. 2	15.97	sec
	20	No. 3	32.69	sec
Temp	90	F	90	
Baro press	759	mm hg	760	
TVA	Pure HC	ppm		
Canister				
Comments- all hatches and PV connected in vapor space.				
Had to tighten other hatches to get this one to drive DGM.				

DGM		No. 22	9/28/2008	
Barge	G8		1450	PM
	PV Vent		Unleaded Gasoline	
Liters Timed				
	50	No. 1	24.38	sec
	50	No. 2	21.47	sec
	50	No. 3	21.15	sec
Temp	98	F	98	
Baro press	755	mm hg	754	
TVA	Pure HC	ppm		
Canister	1359			



DGM		No. 23	9/28/2008	
Barge	G8		1550	PM
	Slop Tank PV Vent		Unleaded Gasoline	
Liters Timed				
10	No. 1	43.06	sec	
10	No. 2	45.34	sec	
10	No. 3	41.91	sec	
Temp	98	F	100	
Baro press	754	mm hg	755	
TVA	Pure HC	ppm		
Canister	1491			

## **APPENDIX B**

### **EPA Protocol Bagging Procedures**

**Extracted from EPA *Protocol for Equipment Leaks Emission Estimating, 1995:*  
4.0 MASS EMISSION SAMPLING**

#### **4.1 INTRODUCTION**

This chapter describes the procedures for "bagging" equipment to measure mass emissions of organic compounds. An equipment component is bagged by enclosing the component to collect leaking vapors. Measured emission rates from bagged equipment coupled with screening values can be used to develop unit-specific screening value/mass emission rate correlation equations. Unit-specific correlations can provide precise estimates of mass emissions from equipment leaks at the process unit. However, it is recommended that unit-specific correlations are only developed in cases where the existing EPA correlations do not give reasonable mass emission estimates for the process unit. The focus of the chapter is on bagging equipment containing organic compounds, but similar procedures can be applied to bag equipment containing inorganic compounds as long as there are comparable analytical techniques for measuring the concentration of the inorganic compound.

This chapter is divided into four sections. In section 4.2, the methods for bagging equipment are discussed. Considerations for bagging each equipment type are discussed in section 4.3. In section 4.4, techniques used in the laboratory analysis of bagged samples are discussed. Section 4.4 also includes a description of a rigorous calibration procedure for the portable monitoring device that must be followed. Finally, in section 4.5, quality assurance and quality control (QA/QC) guidelines are provided.

#### **4.2 SAMPLING METHODS**

The emission rate from an equipment component is measured by bagging the component--that is, isolating the component from ambient air to collect any leaking compound(s). A tent (i.e., bag) made of material impermeable to the compound(s) of interest is constructed around the leak interface of the piece of equipment. A known rate of carrier gas is induced through the bag and a sample of the gas from the bag is collected and analyzed to determine the concentration (in parts per million by volume [ppmv]) of leaking material. The concentration is measured using laboratory instrumentation and procedures. Mass emissions are calculated based on the measured concentration and the flow rate of carrier gas through the bag. In some cases, it may be necessary to collect liquid leaking from a bagged equipment piece. Liquid can either be dripping from the equipment piece prior to bagging, and/or be formed as condensate within the bag. If liquid accumulates in the bag, then the bag should be configured so that there is a low point to collect the liquid. The time in which the liquid accumulates should be recorded. The accumulated liquid should then be taken to the laboratory and transferred to a graduated cylinder to measure the volume of organic material. Based on the volume of organic material in the cylinder (with the

volume of water or non-organic material subtracted out), the density of the organic material, and the time in which the liquid accumulated, the organic liquid leak rate can be calculated. Note that the density can be assumed to be equivalent to the density of organic material in the equipment piece, or, if sufficient volume is collected, can be measured using a hydrometer. It should be noted that in some cases condensate may form a light coating on the inside surface of the bag, but will not accumulate. In these cases, it can be assumed that an equilibrium between condensate in and evaporation has been reached and that the vapor emissions are equivalent to total emissions from the source. When bagging an equipment piece, the enclosure should be kept as small as practical. This has several beneficial effects:

- € The time required to reach equilibrium is kept to a minimum;
- € The time required to construct the enclosure is minimized;
- € A more effective seal results from the reduced seal area; and
- € Condensation of heavy organic compounds inside the enclosure is minimized or prevented due to reduced residence time and decreased surface area available for heat transfer.

Two methods are generally employed in sampling source enclosures: the vacuum method and the blow-through method. Both methods involve enclosing individual equipment pieces with a bag and setting up a sampling train to collect two samples of leaking vapors to be taken to the laboratory for analysis. Both methods require that a screening value be obtained from the equipment piece prior to and after the equipment piece is enclosed. The methods differ in the ways in which the carrier gas is conveyed through the bag. In the vacuum method, a vacuum pump is used to pull air through the bag. In the blow-through method, a carrier gas such as nitrogen (or other inert gas) is blown into the bag.

In general, the blow-through method has advantages over the vacuum method. These advantages are as follows.

- (1) The blow-through method is more conducive to better mixing in the bag.
- (2) The blow-through method minimizes ambient air in the bag and thus reduces potential error associated with background organic compound concentrations. (For this reason the blow-through method is especially preferable when measuring the leak rate from components with zero or very low screening values.)
- (3) The blow-through method minimizes oxygen concentration in the bag (assuming air is not used as the carrier gas) and the risk of creating an explosive environment.
- (4) In general, less equipment is required to set up the blow-through method sampling train.

However, the blow-through method does require a carrier gas source, and preferably the carrier gas should be inert and free of any organic compounds and moisture. The vacuum method does not require a special carrier gas.

Details of the sampling train of each of these bagging methods are discussed in sections 4.2.1 and 4.2.2, respectively. These sections also contain summaries of the steps of the sampling procedure for each method. For both methods, the approach described above for collecting and measuring liquid leak rates can be utilized. In addition to the sampling descriptions presented in

the following sections, the quality control and assurance guidelines presented in section 4.5 must also be followed when bagging equipment.

### 4.2.1 Vacuum Method

The sampling train used in the vacuum method is depicted in figure 4-1. The train can be mounted on a portable cart, which can be moved around the process unit from component to component. The major equipment items in the sampling train are the vacuum pump used to draw air through the system, and the dry gas meter used to measure the flow rate of gas through the train. In previous studies that the EPA conducted, a 4.8-cubic feet per minute Teflon® ring piston-type vacuum pump equipped with a 3/4-horsepower, air-driven motor was used. Other equipment that may be used in the train includes valves, copper and stainless steel tubing, Teflon® tubing and tape, thermometer, pressure-reading device, liquid collection device, and air-driven diaphragm sampling pumps. It also may be necessary to use desiccant preceding the dry gas meter to remove any moisture.

The bag is connected by means of a bulkhead fitting and Teflon® tubing to the sampling train. A separate line is connected from the bag to a pressure-reading device to allow continuous monitoring of the pressure inside the bag. If a significant vacuum exists inside the bag when air is being pulled through, a hole is made in the opposite side of the bag from the outlet to the sampling train. This allows air to enter the bag more easily and, thus, reduces the vacuum in the enclosure. However, it is important to maintain a vacuum in the bag, since VOC could be lost through the hole if the bag became pressurized.

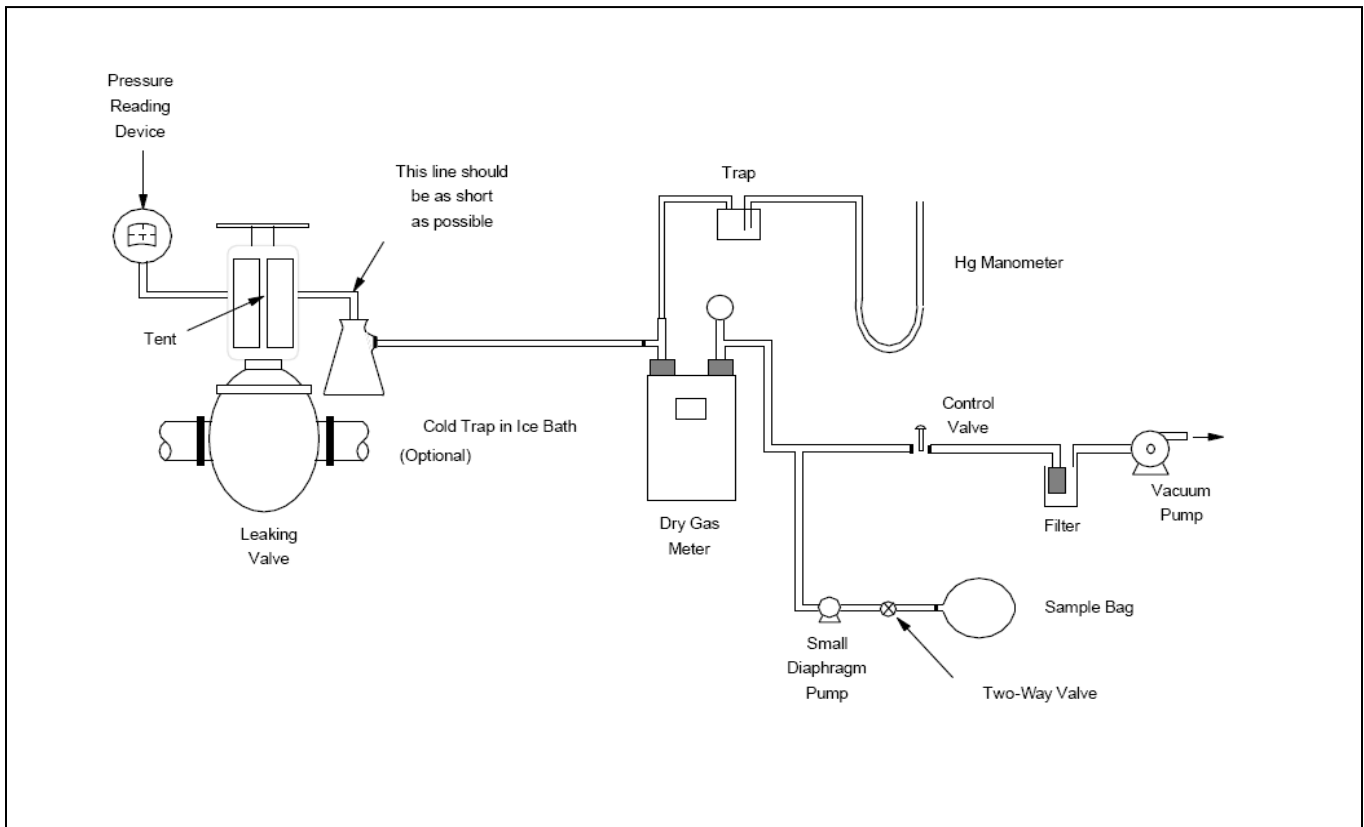


Figure 4-1. Sampling train for bagging a source using the vacuum method.

In practice, it has been found that only a very slight vacuum (0.1 inches of water) is present in the bag during most of the sampling, even in the absence of a hole through the bag wall. Sufficient air enters around the seals to prevent the development of a significant vacuum in the bag. A small diaphragm sampling pump can be used to collect two samples into sample bags or canisters, which are then transported to the laboratory for analysis.

The diaphragm pump can also be used to collect a background sample of the ambient air near the bagged component. The concentration in the background bag is subtracted from the average concentration in the sample bags when calculating the leak rate. Often this correction is insignificant (particularly for components with high leak rates or in cases where there is no detectable volatile organic compound (VOC) concentration measured by the portable monitoring device), and collection of a background bag is optional. However, in some cases collection of a background bag is important so that emission rates are not biased high.

Any liquid that accumulates in the bag should be collected using the approach described in section 4.2. Note that if there is a concern that condensation will occur in equipment downstream from the bag outlet, a cold trap can be placed as close to the bag outlet as possible to remove water or heavy organic compounds that may condense downstream. Any organic condensate that collects in the cold trap must be measured to calculate the total leak rate.

The flow rate through the system can be varied by throttling the flow with a control valve immediately upstream of the vacuum pump. Typical flow rates are approximately 60 liters per minute (l/min) or less. A good flow rate to use is one in which a balance can be found between reaching equilibrium conditions and having a high enough concentration of organic compounds in the bag outlet to accurately measure the concentration in the laboratory. As the flow rate is decreased, the concentration of organic compounds increases in the gas flowing through the sampling system. The flow rate should be adjusted to avoid any operations with an explosive mixture of organic compounds in air. It may also be possible to increase the flow rate in order to minimize liquid condensation in the bag.

The flow rate should be set to a constant rate and kept at that rate long enough for the system to reach equilibrium. To determine if equilibrium conditions have been reached, a portable monitoring device can be used to indicate if the outlet concentration has stabilized.

It is not recommended that the vacuum method be used to measure the leak rate from equipment that have low screening values (approximately 10 ppmv or less), because considerable error can be introduced due to the background organic concentration in the ambient air that is pulled through the bag.

In summary, the vacuum sampling procedure consists of the following steps.

- (1) Determine the composition of material in the designated equipment component, and the operating conditions of the component.
- (2) Obtain and record a screening value with the portable monitoring instrument.
- (3) Cut a bag from appropriate material (see section 4.3) that will easily fit over the equipment component.

- (4) Connect the bag to the sampling train.
- (5) If a cold trap is used, immerse the trap in an ice bath.
- (6) Note the initial reading of the dry gas meter.
- (7) Start the vacuum pump and a stopwatch simultaneously. Make sure a vacuum exists within the bag.
- (8) Record the temperature and pressure at the dry gas meter.
- (9) Observe the VOC concentration at the vacuum pump exhaust with the monitoring instrument. Make sure concentration stays below the lower explosive limit.
- (10) Record the temperature, pressure, dry gas meter reading, outlet VOC concentration and elapsed time every 2 to 5 minutes.
- (11) Collect 2 gas samples from the discharge of the diaphragm sampling pump when the outlet concentration stabilizes (i.e., the system is at equilibrium).
- (12) Collect a background bag (optional).
- (13) Collect any liquid that accumulated in the bag as well as in the cold trap (if used) in a sealed container.
- (14) Take a final set of readings and stop the vacuum pump.
- (15) Transport all samples to the laboratory, along with the data sheet.
- (16) Remove the bag.
- (17) Rescreen the source with the portable monitoring instrument and record.

Based on the data collected in the steps described above, mass emissions are calculated using the equation presented in Table 4-1.

TABLE 4-1. CALCULATION PROCEDURES FOR LEAK RATE WHEN USING THE VACUUM METHOD

$$\text{Leak Rate (kg/hr)} = \frac{9.63 \times 10^{-10} (Q) (MW) (GC) (P)}{T + 273.15} + \frac{(\rho) (V_L)}{16.67(t)}$$

where:

- $9.63 \times 10^{-10}$  = A conversion factor using the gas constant:  

$$\frac{^{\circ}\text{K} \times 10^6 \times \text{kg-mol} \times \text{min}}{\ell \times \text{hour} \times \text{mmHg}} ;$$
- $Q$  = Flow rate out of bag ( $\ell/\text{min}$ );  
 $MW^a$  = Molecular weight of organic compound(s) in the sample bag<sup>c</sup> or alternatively in the process stream contained within the equipment piece being bagged (kg/kg-mol);  
 $GC^b$  = Sample bag organic compound concentration (ppmv) minus background bag organic compound concentration<sup>c</sup> (ppmv);  
 $P$  = Absolute pressure at the dry gas meter (mmHg);  
 $T$  = Temperature at the dry gas meter ( $^{\circ}\text{C}$ );  
 $\rho$  = Density of organic liquid collected (g/ml);  
 $V_L$  = Volume of liquid collected (ml);  
 $16.67$  = A conversion factor to adjust term to units of kilograms per hour (g  $\times$  hr)/(kg  $\times$  min)  
 $t$  = Time in which liquid is collected (min); and

<sup>a</sup>For mixtures calculate MW as:

$$= \frac{\sum_{i=1}^n MW_i X_i}{\sum_{i=1}^n X_i}$$

where:

- $MW_i$  = Molecular weight of organic compound  $i$ ;  
 $X_i$  = Mole fraction of organic compound  $i$ ; and  
 $n$  = Number of organic compounds in mixture.

<sup>b</sup>For mixtures, the value of GC is the total concentration of all the organic compounds in the mixture.

<sup>c</sup>Collection of a background bag is optional. If a background bag is not collected, assume the background concentration is zero.



## 4.2.2 Blow-Through Method

The sampling train for the blow-through method is presented in figure 4-2. The temperature and oxygen concentrations are measured inside the bag with a thermocouple (or thermometer) and an oxygen/combustible gas monitor. The carrier gas is metered into the bag through one or two tubes (two tubes provide for better mixing) at a steady rate throughout the sampling period. The flow rate of the carrier gas is monitored in a gas rotameter calibrated to the gas. Typical flow rates are approximately 60 /min or less. It is preferable to use an inert gas such as nitrogen for the blow-through method so as to minimize the risk of creating an explosive environment inside the bag. Also, the carrier gas should be free of any organic compounds and moisture. The pressure in the bag should never exceed 1 pound per square inch gauge (psig).

The flow rate through the bag can be varied by adjusting the carrier gas regulator. As mentioned in section 4.2.1, a good flow rate to use is one in which a balance can be found between reaching equilibrium conditions and having a high enough concentration of organic compounds in the bag outlet to accurately measure the concentration in the laboratory. Adjustments to the flow rate may also help minimize liquid condensation in the bag. Any liquid that does accumulate in the bag should be collected using the approach described in Sec.4.2.

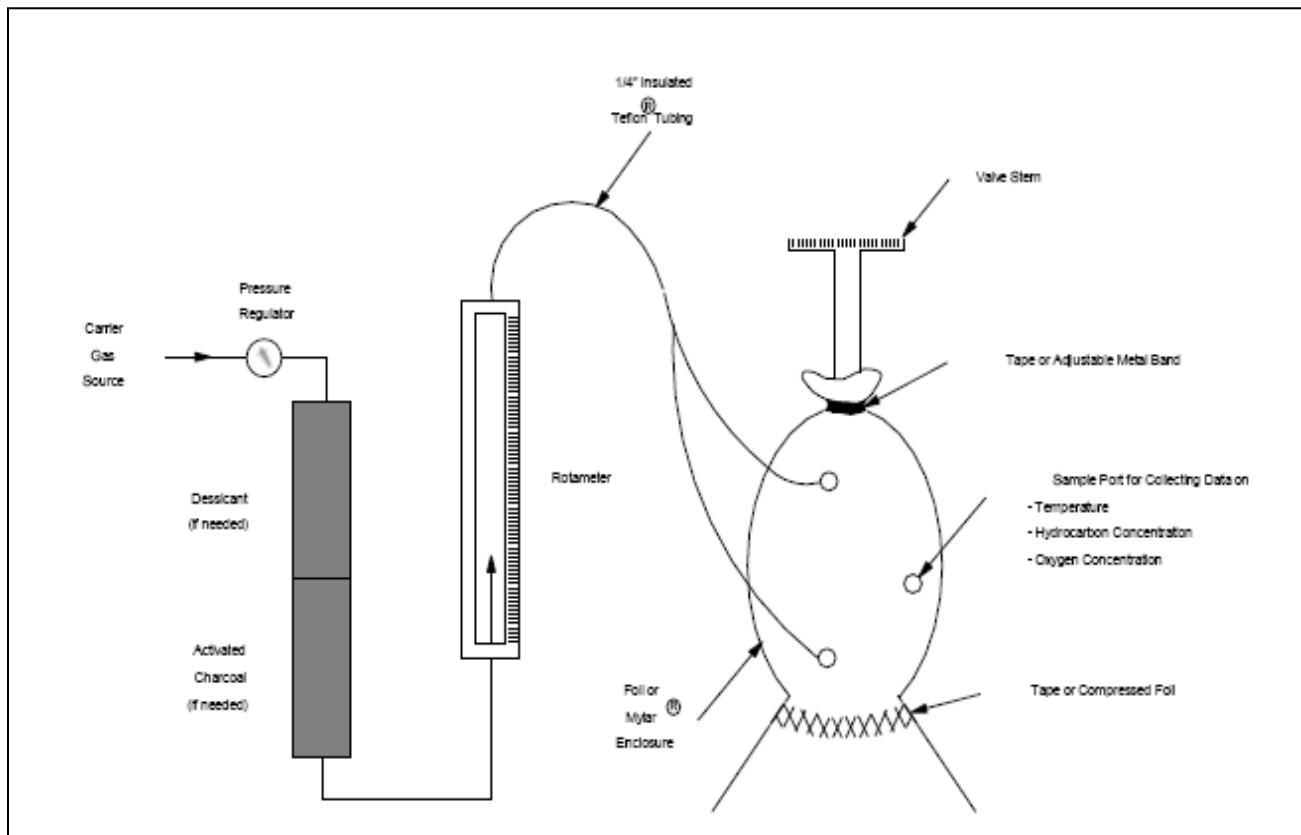


Figure 4-2. Equipment Required for the Blow-Through Sampling Technique

The carrier gas flow rate should be set to a constant rate and kept at that rate long enough for the system to reach equilibrium. In addition to the carrier gas flow through the bag, some ambient air may enter the bag if it is not airtight. The oxygen measurements are used to determine the flow of ambient air through the bag. The oxygen measurements are also an indication of the quality of the bagging procedure (the lower the oxygen concentration the better). Once oxygen concentration falls below 5 percent, the portable monitoring instrument is used to check organic compound concentrations at several locations within the bag to ensure that the bag contents are at steady state. Once the bag contents are at steady state, two gas samples are drawn out of the bag for laboratory analysis using a portable sampling pump. It may also be necessary to collect a background bag sample, particularly if the source had screened at zero and if there is still a detectable level of oxygen in the bag. However, collection of a background bag is optional. In summary, the blow-through method consists of the following steps, which assume nitrogen is used as the carrier gas.

- (1) Determine the composition of the material in the designated equipment component, and the operating conditions of the component.
- (2) Screen the component using the portable monitoring instrument.
- (3) Cut a bag that will easily fit over the equipment component.
- (4) Connect tubing from the nearest nitrogen source to a rotameter stand.
- (5) Run tubing from the rotameter outlet to a "Y" that splits the nitrogen flow into two pieces of tubing and insert the tubes into openings located on either side of the bag.
- (6) Turn on the nitrogen flow and regulate it at the rotameter to a constant rate and record the time.
- (7) After the nitrogen is flowing, wrap aluminum foil around those parts of the component where air could enter the bag-enclosed volume.
- (8) Use duct tape, wire, and/or rope to secure the bag to the component.
- (9) Put a third hole in the bag roughly equidistant from the two carrier gas-fed holes.
- (10) Measure the oxygen concentration in the bag by inserting the lead from an oxygen meter into the third hole. Adjust the bag (i.e., modify the seals at potential leak points) until the oxygen concentration is less than 5 percent.
- (11) Measure the temperature in the bag.
- (12) Check the organic compound concentration at several points in the bag with the portable monitoring instrument to ensure that carrier gas and VOC are well mixed throughout the bag.
- (13) Collect samples in sample bags or canisters by drawing a sample out of the bag with a portable sampling pump.
- (14) Collect a background bag (optional).
- (15) Remove the bag and collect any liquid that accumulated in the bag in a sealed container. Note the time over which the liquid accumulated.
- (16) Rescreen the source.

Table 4-2 gives equations used to calculate mass emission rates when using the blow-through method. An adjustment is provided for the leak rate equation in table 4-2 to account for the total flow through the bag. This adjustment is recommended and represents an improvement over previous versions.

TABLE 4-2. CALCULATION PROCEDURES FOR LEAK RATE  
WHEN USING THE BLOW-THROUGH METHOD

$$\text{Leak Rate (kg/hr)} = \left( \frac{1.219 \times 10^{-5} (Q) (MW) (GC)}{T + 273.15} + \frac{(\rho) (V_L)}{16.67 (t)} \right) \times \left( \frac{10^6 \text{ppmv}}{10^6 \text{ppmv} - GC} \right)$$

where:

$1.219 \times 10^{-5}$  = A conversion factor taking into account the gas constant and assuming a pressure in the tent of 1 atmosphere:

$$\frac{^{\circ}\text{K} \times 10^6 \times \text{kg-mol}}{\text{m}^3} ;$$

Q = flow rate out of tent ( $\text{m}^3/\text{hr}$ );

$$= \frac{\text{N}_2 \text{ Flow Rate (}\ell/\text{min)}}{1 - [\text{Tent Oxygen Conc. (volume \%)/21]} \times \frac{[0.06 (\text{m}^3/\text{min})]}{(\ell/\text{hr})}$$

MW<sup>a</sup> = Molecular weight of organic compounds in the sample bag or alternatively in the process stream contained within the equipment piece being bagged (kg/kg-mol);

GC<sup>b</sup> = Sample bag organic compound concentration (ppmv), corrected for background bag organic compound concentration (ppmv);<sup>c</sup>

T = Temperature in tent ( $^{\circ}\text{C}$ );

$\rho$  = Density of organic liquid collected (g/ml);

V<sub>L</sub> = Volume of liquid collected (ml);

16.67 = A conversion factor to adjust term to units of Kilograms per hour (g × hr)/(kg × min); and

t = Time in which liquid is collected (min).

<sup>a</sup>For mixtures calculate MW as:

$$= \frac{\sum_{i=1}^n \text{MW}_i X_i}{\sum_{i=1}^n X_i}$$

where:

MW<sub>i</sub> = Molecular weight of organic compound i;

TABLE 4-2. CALCULATION PROCEDURES FOR LEAK RATE  
WHEN USING THE BLOW-THROUGH METHOD  
(Continued)

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$X_i$  = Mole fraction of organic compound  $i$ ; and  
 $n$  = Number of organic compounds in mixture.

<sup>b</sup>For mixtures, the value of GC is the total concentration of all the organic compounds in the mixture.

<sup>c</sup>Collection of a background bag is optional. If a background bag is not collected, assume the background concentration is zero. To correct for background concentration, use the following equation:

$$\text{GC (ppmv)} = \text{SB} - \left( \frac{\text{TENT}}{21} \times \text{BG} \right)$$

where:

SB = Sample bag concentration (ppmv);  
TENT = Tent oxygen concentration (volume %); and  
BG = Background bag concentration (ppmv)

### **4.3 SOURCE ENCLOSURE**

In this section, choosing a bagging material and the approach for bagging specific equipment types are discussed. An important criteria when choosing the bagging material is that it is impermeable to the specific compounds being emitted from the equipment piece. This criteria is also applicable for sample gas bags that are used to transport samples to the laboratory. A bag stability test over time similar to the Flexible Bag Procedure described in section 5.3.2 of the EPA method 18 is one way to check the suitability of a bagging material. After a bag has been used, it must be purged. Bags containing residual organic compounds that cannot be purged should be discarded. Mylar®, Tedlar®, Teflon®, aluminum foil, or aluminized Mylar® are recommended potential bagging materials. The thickness of the bagging material can range from 1.5 to 15 millimeters (mm), depending on the bagging configuration needed for the type of equipment being bagged, and the bagging material. Bag construction for individual sources is discussed in sections 4.3.1 through 4.3.5. For convenience, Mylar® will be used as an example of bagging material in the following discussions.

#### **4.3.1 Valves**

When a valve is bagged, only the leak points on the valve should be enclosed. Do not enclose surrounding flanges. The most important property of the valve that affects the type of enclosure selected for use is the metal skin temperature where the bag will be sealed. At skin temperatures of approximately 200 °C or less, the valve stem and/or stem support can be wrapped with 1.5- to 2.0-mm Mylar® and sealed with duct tape at each end and at the seam. The Mylar® bag must be constructed to enclose the valve stem seal and the packing gland seal. When skin temperatures are in excess of 200 °C, a different method of bagging the valve should be utilized. Metal bands, wires, or foil can be wrapped around all hot points that would be in contact with the Mylar® bag material. Seals are then made against the insulation using duct tape or adjustable metal bands of stainless steel. At extremely high temperatures, metal foil can be used as the bagging material and metal bands used to form seals. At points where the shape of the equipment prevent a satisfactory seal with metal bands, the foil can be crimped to make a seal.

#### **4.3.2 Pumps and Agitators**

As with valves, a property of concern when preparing to sample a pump or agitator is the metal skin temperature at areas or points that are in contact with the bag material. At skin temperatures below 200 °C, Mylar® plastic and duct tape are satisfactory materials for constructing a bag around a pump or agitator seal. If the temperature is too high or the potential points of contact are too numerous to insulate, an enclosure made of aluminum foil can be constructed. This enclosure is sealed around the pump and bearing housing using silicone fabric insulating tape, adjustable metal bands, or wire. The configuration of the bag will depend upon the type of pump. Most centrifugal pumps have a housing or support that connects the pump drive (or bearing housing) to the pump itself. The support normally encloses about one-half of the area between the pump and drive motor, leaving open areas on the sides. The pump can be bagged by cutting panels to fit these open areas. These panels can be made using thicker bagging material such as 14-mm Mylar®. In cases where supports are absent or quite narrow, a cylindrical enclosure around the seal can be made so that it extends from the pump housing to the motor or

bearing support. As with the panels, this enclosure should be made with thicker bagging material to provide strength and rigidity.

Reciprocating pumps can present a somewhat more difficult bagging problem. If supports are present, the same type of two-panel Mylar® bag can be constructed as that for centrifugal pumps. In many instances, however, sufficiently large supports are not provided, or the distance between pump and driver is relatively long. In these cases, a cylindrical enclosure as discussed above can be constructed. If it is impractical to extend the enclosure all the way from the pump seal to the pump driver, a seal can be made around the reciprocating shaft. This can usually be best completed by using heavy aluminum foil and crimping it to fit closely around the shaft. The foil is attached to the Mylar® plastic of the enclosure and sealed with the duct tape.

In cases where liquid is leaking from a pump, the outlet from the bag to the sampling train should be placed at the top of the bag and as far away from spraying leaks as practical. A low point should be formed in the bag to collect the liquid so that the volume of the liquid can be measured and converted to a mass rate.

### **4.3.3 Compressors**

In general, the same types of bags that are suitable for pumps can be directly applied to compressors. However, in some cases, compressor seals are enclosed and vented to the atmosphere at a high-point vent. If the seals are vented to a high-point vent, this vent line can be sampled. A Mylar® bag can be constructed and sealed around the outlet of the vent and connected to the sampling train. If the high-point vents are inaccessible, the vent lines from the compressor seal enclosures can be disconnected at some convenient point between the compressor and the normal vent exit. Sampling is then conducted at this intermediate point. In other cases, enclosed compressor seals are vented by means of induced draft blowers or fans. In these cases, if the air flow rate is known or can be determined, the outlet from the blower/fan can be sampled to determine the emission rate.

### **4.3.4 Connectors**

In most cases, the physical configurations of connectors lend themselves well to the determination of leak rates. The same technique can be used for a connector whether it is a flanged or a threaded fitting. To bag a connector with a skin temperature below 200 °C, a narrow section of Mylar® film is constructed to span the distance between the two flange faces or the threaded fitting of the leaking source. The Mylar® is attached and sealed with duct tape. When testing connectors with skin temperatures above 200 °C, the outside perimeter of both sides of the connector are wrapped with heat-resistant insulating tape. Then, a narrow strip of aluminum foil can be used to span the distance between the connection. This narrow strip of foil can be sealed against the insulating tape using adjustable bands of stainless steel.

### **4.3.5 Relief Valves**

Relief devices in gas/vapor service generally relieve to the atmosphere through a large-diameter pipe that is normally located at a high point on the process unit that it serves. The "horns" can be

easily bagged by placing a Mylar® plastic bag over the opening and sealing it to the horn with duct tape. Because many of these devices are above grade level, accessibility to the sampling train may be limited or prevented. It is sometimes possible to run a long piece of tubing from the outlet connection on the bag to the sampling train located at grade level or on a stable platform.

As discussed previously in section 3.0, the purpose of pressure relief devices makes them inherently dangerous to sample, especially over a long period of time. If these equipment are to be sampled for mass emissions, special care and precautions should be taken to ensure the safety of the personnel conducting the field sampling.

#### **4.4 ANALYTICAL TECHNIQUES**

The techniques used in the laboratory analysis of the bagged samples will depend on the type of processes sampled. The following sections describe the analytical instrumentation and calibration, and analytical techniques for condensate. These are guidelines and are not meant to be a detailed protocol for the laboratory personnel. Laboratory personnel should be well-versed in the analysis of organic compound mixtures and should design their specific analyses to the samples being examined. Also discussed is the calibration protocol for the portable monitoring instrument. When bagging data are collected, it is critical that the screening value associated with mass emission rates is accurate. For this reason, a more rigorous calibration of the portable monitoring instrument is required than if only screening data are being collected.

##### **4.4.1 Analytical Instrumentation**

The use of analytical instrumentation in a laboratory is critical to accurately estimate mass emissions. The analytical instrument of choice depends on the type of sample being processed. Gas chromatographs (GC's) equipped with a flame ionization detector or electron capture detector are commonly used to identify individual constituents of a sample. Other considerations besides instrument choice are the type of column used, and the need for temperature programming to separate individual constituents in the process stream with sufficient resolution. For some process streams, total hydrocarbon analyses may be satisfactory.

##### **4.4.2 Calibration of Analytical Instruments**

Gas chromatographs should be calibrated with either gas standards generated from calibrated permeation tubes containing individual VOC components, or bottled standards of common gases. Standards must be in the range of the concentrations to be measured. If cylinder calibration gas mixtures are used, they must be analyzed and certified by the manufacturer to be within  $\pm 2$  percent accuracy, and a shelf life must be specified. Cylinder standards beyond the shelf life must either be reanalyzed or replaced.

Field experience indicates that certified accuracies of  $\pm 2$  percent are difficult to obtain for very low-parts per million (ppm) calibration standards ( $< 10$  ppm). Users of low-parts per million calibration standards should strive to obtain calibration standards that are as accurate as possible. The accuracy must be documented for each concentration standard. The results of all calibrations should be recorded on





#### **4.4.3 Analytical Techniques for Condensate**

Any condensate collected should be brought to the laboratory sealed in the cold trap flask. This material is transferred to a graduated cylinder to measure the volume collected. If there is enough volume to make it feasible, the organic layer should be separated from the aqueous layer (if present) and weighed to determine its density. If water-miscible organic compounds are present, both the aqueous and organic phases should be analyzed by GC to determine the total volume of organic material.

#### **4.4.4. Calibration Procedures for the Portable Monitoring Instrument**

To generate precise screening values, a rigorous calibration of the portable monitoring instrument is necessary. Calibrations must be performed at the start and end of each working day, and the instrument reading must be within 10 percent of each of the calibration gas concentrations. A minimum of five calibration gas standards must be prepared including a zero gas standard, a standard approaching the maximum readout of the screening instrument, and three standards between these values. If the monitoring instrument range is from 0 to 10,000 ppmv, the following calibration gases are required:

- € A zero gas (0-0.2 ppm) organic in air standard;
- € A 9.0 ppm (8-10 ppm) organic in air standard;
- € A 90 ppm (80-100 ppm) organic in air standard;
- € A 900 ppm (800-1,000 ppm) organic in air standard; and
- € A 9,000 ppm (8,000-10,000 ppm) organic in air standard.

The same guidelines for the analysis and certification of the calibration gases as described for calibrating laboratory analytical instruments must be followed for calibrating the portable monitoring instrument.

#### **4.5 QUALITY CONTROL AND QUALITY ASSURANCE GUIDELINES**

To ensure that the data collected during the bagging program is of the highest quality, the following QC/QA procedures must be followed. Quality control requirements include procedures to be 4-21 followed when performing equipment leak mass emissions sampling. Quality assurance requirements include accuracy checks of the instrumentation used to perform mass emissions sampling. Each of these QC/QA requirements are discussed below.

### 4.5.1 Quality Control Procedures

A standard data collection form must be prepared and used when collecting data in the field. Tables 4-4 and 4-5 are examples of data collection forms for the blow-through and vacuum methods of mass emissions sampling, respectively. In addition to completing the data collection forms, the following guidelines need to be adhered to when performing the bagging analysis:

- € Background levels near equipment that is selected for bagging must not exceed 10 ppmv, as measured with the portable monitoring device.
- € Screening values for equipment that is selected for bagging must be readable within the spanned range of the monitoring instruments. If a screening value exceeds the highest reading on the meter (i.e., "pegged reading"), a dilution probe should be used, or in the event that this is not possible, the reading should be identified as pegged.
- € Only one piece of equipment can be enclosed per bag; a separate bag must be constructed for each equipment component.
- € A separate sample bag must be used for each equipment component that is bagged. Alternatively, bags should be purged and checked for contamination prior to reuse.
- € A GC must be used to measure the concentrations from gas samples.
- € Gas chromatography analyses of bagged samples must follow the analytical procedures outlined in the EPA Method 18.
- € To ensure adequate mixing within the bag when using the blow-through method, the dilution gas must be directed onto the equipment leak interface.
- € To ensure that steady-state conditions exist within the bag, wait at least five time constants (volume of bag dilution/gas flow rate) before withdrawing a sample for recording the analysis.
- € The carrier gas used in the blow-through method of bagging should be analyzed by GC before it is used, and the concentration of organic compounds in the sample should be documented. For cylinder purge gases, one gas sample should be analyzed. For plant purge gas systems, gas samples should be analyzed with each bagged sample unless plant personnel can demonstrate that the plant gas remains stable enough over time to allow a one-time analysis.
- € The portable monitoring instrument calibration procedure described in section 4.4.4 should be performed at the beginning and end of each day.

TABLE 4-5. EXAMPLE DATA COLLECTION FORM FOR FUGITIVE EMISSIONS  
BAGGING TEST (VACUUM METHOD)

---

Equipment Type _____	Component ID _____
Equipment Category _____	Plant ID _____
Line Size _____	Date _____
Stream Phase (G/V, LL, HL) _____	Analysis Team _____
Barometric Pressure _____	_____
Ambient Temperature _____	Instrument ID _____
Stream Temperature _____	Stream Pressure _____
Stream Composition (Wt %) _____,	_____
_____,	_____

---

Time

Bagging Test Measurement Data

\_\_\_\_\_ Initial Screening (ppmv) Equipment Piece<sup>a</sup> \_\_\_\_\_ Bkgd. \_\_\_\_\_

\_\_\_\_\_ Background Bag Organic Compound Conc. (ppmv)<sup>b</sup> \_\_\_\_\_

\_\_\_\_\_ Dry Gas Meter Reading (ℓ/min) \_\_\_\_\_

\_\_\_\_\_ Sample Bag 1 Organic Compound Conc. (ppmv) \_\_\_\_\_

\_\_\_\_\_ Vacuum Check in Bag (Y/N) (Must be YES to collect sample.) \_\_\_\_\_

\_\_\_\_\_ Dry Gas Meter Temperature<sup>c</sup> (°C) \_\_\_\_\_

\_\_\_\_\_ Dry Gas Meter Pressure<sup>c</sup> (mmHg) \_\_\_\_\_

\_\_\_\_\_ Dry Gas Meter Reading (ℓ/min) \_\_\_\_\_

\_\_\_\_\_ Sample Bag 2 Organic Compound Conc. (ppmv) \_\_\_\_\_

\_\_\_\_\_ Vacuum Check in Bag (Y/N) (Must be YES to collect sample.) \_\_\_\_\_

\_\_\_\_\_ Dry Gas Meter Temperature<sup>c</sup> (°C) \_\_\_\_\_

\_\_\_\_\_ Dry Gas Meter Pressure<sup>c</sup> (mmHg) \_\_\_\_\_

Condensate Accumulation: Starting Time \_\_\_\_\_ Final Time \_\_\_\_\_

Organic Condensate Collected (mℓ) \_\_\_\_\_

Density of Organic Condensate (g/mℓ) \_\_\_\_\_

\_\_\_\_\_ Final Screening (ppmv) Equip. Piece<sup>a</sup> \_\_\_\_\_ Bkgd. \_\_\_\_\_

---

<sup>a</sup>The vacuum method is not recommended if the screening value is approximately 10 ppmv or less.

<sup>b</sup>Collection of a background bag is optional.

<sup>c</sup>Pressure and temperature are measured at the dry gas meter.

## 4.5.2 Quality Assurance Procedures

Accuracy checks on the laboratory instrumentation and portable monitoring device must be performed to ensure data quality. These checks include a leak rate check performed in the laboratory, blind standards to be analyzed by the laboratory instrumentation, and drift checks on the portable monitoring device.

### 4.5.2.1 Leak Rate Check

A leak rate check is normally performed in the laboratory by sampling an artificially induced leak rate of a known gas. This can clarify the magnitude of any bias in the combination of sampling/test method, and defines the variance in emissions estimation due to the sampling. If the result is outside the 80 to 120 percent recovery range, the problem must be investigated and corrected before sampling continues. The problems and associated solutions should be noted in the test report.

Leak rate checks should be performed at least two times per week during the program. The leak rate checks should be conducted at two concentrations: (1) within the range of 10 multiplied by the calculated lower limit of detection for the laboratory analytical instrument; and (2) within 20 percent of the maximum concentration that has been or is expected to be detected in the field during the bagging program.

To perform a leak rate check, first induce a known flow rate with one of the known gas concentrations into a sampling bag. For example, this can be done using a gas permeation tube of a known organic compound constituent. Next, determine the concentration of the gas using a laboratory analytical instrument and compare the results to the known gas concentration. If the calculated leak rate is not within  $\pm 20$  percent of the induced leak rate, further analysis should be performed to determine the reason. Areas that can potentially induce accuracy problems include:

- € Condensation,
- € Pluggage,
- € Seal of bag not tight (leakage),
- € Adsorption onto bag, and
- € Permeation of bag.

The results of all accuracy checks should be recorded on prepared data sheets.

### 4.5.2.2 Blind Standards Preparation and Performance

Blind standards are analyzed by the laboratory instrumentation to ensure that the instrument is properly calibrated. Blind standards must be prepared and submitted at least two times per week during the program. The blind standards are prepared by diluting or mixing known gas concentrations in a prescribed fashion so that the resulting concentrations are known. The analytical results should be within  $\pm 25$  percent of the blind standard gas concentration. If the results are not within 25 percent of the blind standard concentration, further analyses must be performed to determine the reason. Use of blind standards not only defines the analytical

variance component and analytical accuracy, but it can serve to point out equipment malfunctions and/or operator error before questionable data are generated.

#### **4.5.2.3 Drift Checks**

Drift checks need to be performed to ensure that the portable monitoring instrument remains calibrated. At a minimum, drift checks must be performed before and after a small group of components (i.e., two or three) are bagged. Preferably, drift checks should be performed on the screening instrument immediately before and after each component is bagged. These checks should be performed by analyzing one of the calibration gases used to calibrate the portable monitoring instrument. The choice of calibration gas concentration should reflect the anticipated screening value of the next component to be monitored. For example, if a component had previously screened at 1,000 ppmv and been identified for bagging, the calibration standard should be approximately 900 ppmv. Drift check data must be recorded on data sheets containing the information shown in the example in table 4-6. If the observed instrument reading is different from the certified value by greater than  $\pm 20$  percent, then a full multipoint calibration must be performed (see section 3.2.4.1). Also, all those components analyzed since the last drift check must be retested. Drift checks should also be performed if flameout of the portable monitoring instrument occurs. Using the lowest calibration gas standard (i.e., approximately 9 ppmv standard), determine the associated response on the portable monitoring instrument. If the response is not within  $\pm 10$  percent of the calibration gas concentration, a full multipoint calibration is required before testing resumes.



#### 4.6 REFERENCES

1. Code of Federal Regulations, Title 40, Part 60, Appendix A. Reference Method 21, Determination of Volatile Organic Compound Leaks. Washington, DC. U.S. Government Printing Office. Revised June 22, 1990.

## **APPENDIX C**

### **Laboratory Results with QC Data**



## Listing of Chemical Compounds Analyzed

Sorted Alpha-Numerically

Compound	Carbon #
1,2,3 Trimethylbenzene	9
1,2,4 Trimethylbenzene	9
1,3,5 Trimethylbenzene	9
1,3 butadiene	4
1 Butene	4
1 Hexene	6
1 Pentene	5
2,2,4 Trimethylpentane	8
2,2 Dimethylbutane	6
2,3,4 Trimethylpentane	8
2,3 Dimethylbutane	6
2,3 Dimethylpentane	7
2,4 Dimethylpentane	7
2 Methylheptane	8
2 Methylhexane	7
2 Methylpentane	6
3 Methylheptane	8
3 Methylhexane	7
3 Methylpentane	6
Acetylene	2
Benzene	6
cis 2 Butene	4
cis 2 Pentene	5
Cumene	9
Cyclohexane	6
Cyclopentane	5
Ethane	2
Ethylbenzene	8
Ethylene	2
Isobutane	4
Isopentane	5
Isoprene	5
m/p Xylene	8
m Diethylbenzene	10
Methylcyclohexane	7
Methylcyclopentane	6
m Ethyltoluene	9

Sorted by Carbon Number

Compound	Carbon #
Acetylene	2
Ethane	2
Ethylene	2
Propane	3
Propylene	3
1,3 butadiene	4
1 Butene	4
cis 2 Butene	4
Isobutane	4
n Butane	4
trans 2 Butene	4
Un Identified	4.5
1 Pentene	5
cis 2 Pentene	5
Cyclopentane	5
Isopentane	5
Isoprene	5
n Pentane	5
trans 2 Pentene	5
1 Hexene	6
2,2 Dimethylbutane	6
2,3 Dimethylbutane	6
2 Methylpentane	6
3 Methylpentane	6
Benzene	6
Cyclohexane	6
Methylcyclopentane	6
n Hexane	6
2,3 Dimethylpentane	7
2,4 Dimethylpentane	7
2 Methylhexane	7
3 Methylhexane	7
Methylcyclohexane	7
n Heptane	7
Toluene	7
2,2,4 Trimethylpentane	8
2,3,4 Trimethylpentane	8

Compound	Carbon #
n Butane	4
n Decane	10
n Heptane	7
n Hexane	6
n Nonane	9
n Octane	8
n Pentane	5
n Propylbenzene	9
n Undecane	11
o Xylene	8
o Ethyltoluene	9
p Diethylbenzene	10
p Ethyltoluene	9
Propane	3
Propylene	3
Styrene	8
Toluene	7
Total NMOC	
trans 2 Butene	4
trans 2 Pentene	5
Un Identified	4.5

Compound	Carbon #
2 Methylheptane	8
3 Methylheptane	8
Ethylbenzene	8
m/p Xylene	8
n Octane	8
o Xylene	8
Styrene	8
1,2,3 Trimethylbenzene	9
1,2,4 Trimethylbenzene	9
1,3,5 Trimethylbenzene	9
Cumene	9
m Ethyltoluene	9
n Nonane	9
n Propylbenzene	9
o Ethyltoluene	9
p Ethyltoluene	9
m Diethylbenzene	10
n Decane	10
p Diethylbenzene	10
n Undecane	11
Total NMOC	

## **APPENDIX C**

### **Laboratory Results with QC Data**

Lab Results: EPA PAMS Analysis via GC/FID, reported in ppbC

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz	
AL21640	9/24/2008	Test # 1	14:55	.02	347518.50	2047337.25	
Can ID 1481							
#2 Center Ullage Hatch							
Unleaded Gasoline							
					Area%ppbC	0.01%	0.05%
					ppbC*#C	3127666.5	18426035.25
					ppbv	38613.16667	227481.9167

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz	
AL21641	9/25/2008	Test #2	12:08	.02	122461.20	661556.70	
Can ID 1374							
#3 Starboard Cargo Hatch							
Trans Mix							
					Area%ppbC	0.01%	0.03%
					ppbC*#C	1102150.8	5954010.3
					ppbv	13606.8	73506.3

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz	
AL21695	9/26/2008	Test #14	13:40	.02	68429.97	710368.26	
Can ID 1396							
No. 1 Port Cargo Valve							
Raffinate							
					Area%ppbC	0.00%	0.02%
					ppbC*#C	615869.73	6393314.34
					ppbv	7603.33	78929.80667

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz	
AL21703	9/28/2008	Test 23	15:50	.02	83609.24	2234646.96	
Can ID 1491							
Slop Tank PV Vent							
Unleaded Gasoline							
					Area%ppbC	0.00%	0.06%
					ppbC*#C	752483.16	20111822.64
					ppbv	9289.915556	248294.1067

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz	
AL21642	9/25/2008	Test 3	12:44	.02	24738.25	614498.13	
Can ID 1322							
#2 Starboard Cargo Hatch							
Trans Mix							
					Area%ppbC	0.00%	0.04%
					ppbC*#C	222644.25	5530483.17
					ppbv	2748.694444	68277.57

carbon 9 9

Lab Results: EPA PAMS Analysis via GC/

carbon			9	4	4	6
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21640	9/24/2008	Test # 1	824547.00	353562.30	12533977.80	3559798.20
Can ID 1481						
#2 Center Ullage Hatch			0.02%	0.01%	0.33%	0.09%
Unleaded Gasoline			7420923	1414249.2	50135911.2	21358789.2
			91616.33333	88390.575	3133494.45	593299.7

carbon			9	4	4	6
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21641	9/25/2008	Test #2	308815.20	496500.30	17937903.60	8783928.90
Can ID 1374						
#3 Starboard Cargo Hatch			0.01%	0.02%	0.83%	0.41%
Trans Mix			2779336.8	1986001.2	71751614.4	52703573.4
			34312.8	124125.075	4484475.9	1463988.15

carbon			9	4	4	6
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21695	9/26/2008	Test #14	459458.37	132515.18	61912.83	1154619.97
Can ID 1396						
No. 1 Port Cargo Valve			0.01%	0.00%	0.00%	0.03%
Raffinate			4135125.33	530060.72	247651.32	6927719.82
			51050.93	33128.795	15478.2075	192436.6617

carbon			9	4	4	6
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21703	9/28/2008	Test 23	1081219.49	2888319.20	73847861.23	1043215.29
Can ID 1491						
Slop Tank PV Vent			0.03%	0.08%	2.08%	0.03%
Unleaded Gasoline			9730975.41	11553276.8	295391444.9	6259291.74
			120135.4989	722079.8	18461965.31	173869.215

carbon			9	4	4	6
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21642	9/25/2008	Test 3	277068.40	310712.42	12227622.21	6875254.44
Can ID 1322						
#2 Starboard Cargo Hatch			0.02%	0.02%	0.74%	0.42%
Trans Mix			2493615.6	1242849.68	48910488.84	41251526.64
			30785.37778	77678.105	3056905.553	1145875.74

carbon 9 4 4 6

Lab Results: EPA PAMS Analysis via GC/

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpent	2 Dimethylbutan	4 Trimethylpent
AL21640	9/24/2008	Test # 1	32049192.15	42161117.10	1279342.95	9608346.90
Can ID 1481						
#2 Center Ullage Hatch			0.83%	1.10%	0.03%	0.25%
Unleaded Gasoline			160245960.8	337288936.8	7676057.7	76866775.2
			6409838.43	5270139.638	213223.825	1201043.363

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpent	2 Dimethylbutan	4 Trimethylpent
AL21641	9/25/2008	Test #2	45622121.40	6982950.60	1337755.50	1188672.30
Can ID 1374						
#3 Starboard Cargo Hatch			2.11%	0.32%	0.06%	0.05%
Trans Mix			228110607	55863604.8	8026533	9509378.4
			9124424.28	872868.825	222959.25	148584.0375

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpent	2 Dimethylbutan	4 Trimethylpent
AL21695	9/26/2008	Test #14	439906.95	3158640.52	162589608.72	70602.35
Can ID 1396						
No. 1 Port Cargo Valve			0.01%	0.10%	4.91%	0.00%
Raffinate			2199534.75	25269124.16	975537652.3	564818.8
			87981.39	394830.065	27098268.12	8825.29375

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpent	2 Dimethylbutan	4 Trimethylpent
AL21703	9/28/2008	Test 23	16714247.16	9554255.88	18169808.02	188120.79
Can ID 1491						
Slop Tank PV Vent			0.47%	0.27%	0.51%	0.01%
Unleaded Gasoline			83571235.8	76434047.04	109018848.1	1504966.32
			3342849.432	1194281.985	3028301.337	23515.09875

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpent	2 Dimethylbutan	4 Trimethylpent
AL21642	9/25/2008	Test 3	37064825.21	5225707.93	1097388.77	582833.17
Can ID 1322						
#2 Starboard Cargo Hatch			2.25%	0.32%	0.07%	0.04%
Trans Mix			185324126.1	41805663.44	6584332.62	4662665.36
			7412965.042	653213.4913	182898.1283	72854.14625

carbon 5 8 6 8

Lab Results: EPA PAMS Analysis via GC/

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21640	9/24/2008	Test # 1	36714142.35	9915285.60	8900790.60	3744997.50
Can ID 1481						
#2 Center Ullage Hatch			0.95%	0.26%	0.23%	0.10%
Unleaded Gasoline			220284854.1	69406999.2	62305534.2	29959980
			6119023.725	1416469.371	1271541.514	468124.6875

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21641	9/25/2008	Test #2	29181705.30	5123403.90	3375669.60	4290135.30
Can ID 1374						
#3 Starboard Cargo Hatch			1.35%	0.24%	0.16%	0.20%
Trans Mix			175090231.8	35863827.3	23629687.2	34321082.4
			4863617.55	731914.8429	482238.5143	536266.9125

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21695	9/26/2008	Test #14	131167218.21	101993241.00	28666726.48	1467442.69
Can ID 1396						
No. 1 Port Cargo Valve			3.96%	3.08%	0.87%	0.04%
Raffinate			787003309.3	713952687	200667085.4	11739541.52
			21861203.04	14570463	4095246.64	183430.3363

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21703	9/28/2008	Test 23	27382026.10	7654045.88	2645092.32	1731091.31
Can ID 1491						
Slop Tank PV Vent			0.77%	0.22%	0.07%	0.05%
Unleaded Gasoline			164292156.6	53578321.16	18515646.24	13848730.48
			4563671.017	1093435.126	377870.3314	216386.4138

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21642	9/25/2008	Test 3	3582098.60	534346.20	2516374.79	422529.31
Can ID 1322						
#2 Starboard Cargo Hatch			0.22%	0.03%	0.15%	0.03%
Trans Mix			21492591.6	3740423.4	17614623.53	3380234.48
			597016.4333	76335.17143	359482.1129	52816.16375

carbon 6 7 7 8

Lab Results: EPA PAMS Analysis via GC/

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21640	9/24/2008	Test # 1	20030232.45	5313147.75	3822919.35	19742936.10
Can ID 1481						
#2 Center Ullage Hatch			0.52%	0.14%	0.10%	0.51%
Unleaded Gasoline			140211627.2	31878886.5	30583354.8	138200552.7
			2861461.779	885524.625	477864.9188	2820419.443

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21641	9/25/2008	Test #2	16278021.90	113178108.60	2881831.50	14793845.40
Can ID 1374						
#3 Starboard Cargo Hatch			0.75%	5.23%	0.13%	0.68%
Trans Mix			113946153.3	679068651.6	23054652	103556917.8
			2325431.7	18863018.1	360228.9375	2113406.486

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21695	9/26/2008	Test #14	474665.03	536463810.05	1028621.93	110035391.76
Can ID 1396						
No. 1 Port Cargo Valve			0.01%	16.20%	0.03%	3.32%
Raffinate			3322655.21	3218782860	8228975.44	770247742.3
			67809.29	89410635.01	128577.7413	15719341.68

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21703	9/28/2008	Test 23	60806.72	100523009.21	1480263.59	7661646.72
Can ID 1491						
Slop Tank PV Vent			0.00%	2.83%	0.04%	0.22%
Unleaded Gasoline			425647.04	603138055.3	11842108.72	53631527.04
			8686.674286	16753834.87	185032.9488	1094520.96

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21642	9/25/2008	Test 3	12135595.92	5570064.37	64319.45	360188.92
Can ID 1322						
#2 Starboard Cargo Hatch			0.74%	0.34%	0.00%	0.02%
Trans Mix			84949171.44	33420386.22	514555.6	2521322.44
			1733656.56	928344.0617	8039.93125	51455.56

carbon 7 6 8 7



Lab Results: EPA PAMS Analysis via GC/

carbon			6	2	6	4
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21640	9/24/2008	Test # 1	59592083.85	0.00	36843220.65	45418509.45
Can ID 1481						
#2 Center Ullage Hatch			1.55%	0.00%	0.96%	1.18%
Unleaded Gasoline			357552503.1	0	221059323.9	181674037.8
			9932013.975	0	6140536.775	11354627.36

carbon			6	2	6	4
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21641	9/25/2008	Test #2	58376721.60	7986.60	11018845.80	17124601.50
Can ID 1374						
#3 Starboard Cargo Hatch			2.70%	0.00%	0.51%	0.79%
Trans Mix			350260329.6	15973.2	66113074.8	68498406
			9729453.6	3993.3	1836474.3	4281150.375

carbon			6	2	6	4
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21695	9/26/2008	Test #14	414326089.31	11948.09	511921347.00	118394.71
Can ID 1396						
No. 1 Port Cargo Valve			12.51%	0.00%	15.46%	0.00%
Raffinate			2485956536	23896.18	3071528082	473578.84
			69054348.22	5974.045	85320224.5	29598.6775

carbon			6	2	6	4
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21703	9/28/2008	Test 23	52899946.19	338237.38	7150490.23	55187799.03
Can ID 1491						
Slop Tank PV Vent			1.49%	0.01%	0.20%	1.55%
Unleaded Gasoline			317399677.1	676474.76	42902941.38	220751196.1
			8816657.698	169118.69	1191748.372	13796949.76

carbon			6	2	6	4
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21642	9/25/2008	Test 3	44731703.65	13853.42	8750413.79	13466513.77
Can ID 1322						
#2 Starboard Cargo Hatch			2.72%	0.00%	0.53%	0.82%
Trans Mix			268390221.9	27706.84	52502482.74	53866055.08
			7455283.942	6926.71	1458402.298	3366628.443

carbon 6 2 6 4

Lab Results: EPA PAMS Analysis via GC/

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21640	9/24/2008	Test # 1	33656627.10	429757.35	4250302.35	12358275.90
Can ID 1481						
#2 Center Ullage Hatch			0.87%	0.01%	0.11%	0.32%
Unleaded Gasoline			168283135.5	3867816.15	25501814.1	61791379.5
			6731325.42	47750.81667	708383.725	2471655.18

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21641	9/25/2008	Test #2	43131633.30	141096.60	5353684.20	16114296.60
Can ID 1374						
#3 Starboard Cargo Hatch			1.99%	0.01%	0.25%	0.74%
Trans Mix			215658166.5	1269869.4	32122105.2	80571483
			8626326.66	15677.4	892280.7	3222859.32

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21695	9/26/2008	Test #14	811383.93	219410.38	901537.70	21817212.34
Can ID 1396						
No. 1 Port Cargo Valve			0.02%	0.01%	0.03%	0.66%
Raffinate			4056919.65	1974693.42	5409226.2	109086061.7
			162276.786	24378.93111	150256.2833	4363442.468

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21703	9/28/2008	Test 23	17312813.31	319235.28	2225145.91	22067138.73
Can ID 1491						
Slop Tank PV Vent			0.49%	0.01%	0.06%	0.62%
Unleaded Gasoline			86564066.55	2873117.52	13350875.46	110335693.7
			3462562.662	35470.58667	370857.6517	4413427.746

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21642	9/25/2008	Test 3	34711722.87	110827.36	915315.25	12650151.52
Can ID 1322						
#2 Starboard Cargo Hatch			2.11%	0.01%	0.06%	0.77%
Trans Mix			173558614.4	997446.24	5491891.5	63250757.6
			6942344.574	12314.15111	152552.5417	2530030.304

carbon 5 9 6 5

Lab Results: EPA PAMS Analysis via GC/

carbon			2	8	2	4
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21640	9/24/2008	Test # 1	12150412.35	5231988.15	0.00	778192564.95
Can ID 1481						
#2 Center Ullage Hatch			0.32%	0.14%	0.00%	20.22%
Unleaded Gasoline			24300824.7	41855905.2	0	3112770260
			6075206.175	653998.5188	0	194548141.2

carbon			2	8	2	4
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21641	9/25/2008	Test #2	17296313.40	898492.50	628279.20	44818137.00
Can ID 1374						
#3 Starboard Cargo Hatch			0.80%	0.04%	0.03%	2.07%
Trans Mix			34592626.8	7187940	1256558.4	179272548
			8648156.7	112311.5625	314139.6	11204534.25

carbon			2	8	2	4
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21695	9/26/2008	Test #14	233530.85	998208.61	7603.33	6258626.78
Can ID 1396						
No. 1 Port Cargo Valve			0.01%	0.03%	0.00%	0.19%
Raffinate			467061.7	7985668.88	15206.66	25034507.12
			116765.425	124776.0763	3801.665	1564656.695

carbon			2	8	2	4
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21703	9/28/2008	Test 23	11401.26	2407566.07	0.00	481809646.76
Can ID 1491						
Slop Tank PV Vent			0.00%	0.07%	0.00%	13.56%
Unleaded Gasoline			22802.52	19260528.56	0	1927238587
			5700.63	300945.7588	0	120452411.7

carbon			2	8	2	4
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21642	9/25/2008	Test 3	11519118.73	1684180.06	432424.61	2946820.34
Can ID 1322						
#2 Starboard Cargo Hatch			0.70%	0.10%	0.03%	0.18%
Trans Mix			23038237.46	13473440.48	864849.22	11787281.36
			5759559.365	210522.5075	216212.305	736705.085

carbon 2 8 2 4

Lab Results: EPA PAMS Analysis via GC/

carbon			5	5	8	10
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21640	9/24/2008	Test # 1	730255949.40	2645025.90	15574009.20	54394.20
Can ID 1481						
#2 Center Ullage Hatch			18.98%	0.07%	0.40%	0.00%
Unleaded Gasoline			3651279747	13225129.5	124592073.6	543942
			146051189.9	529005.18	1946751.15	5439.42

carbon			5	5	8	10
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21641	9/25/2008	Test #2	664075141.20	2964359.70	4381981.20	37270.80
Can ID 1374						
#3 Starboard Cargo Hatch			30.68%	0.14%	0.20%	0.00%
Trans Mix			3320375706	14821798.5	35055849.6	372708
			132815028.2	592871.94	547747.65	3727.08

carbon			5	5	8	10
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21695	9/26/2008	Test #14	265133548.05	122739.47	4097108.68	29327.13
Can ID 1396						
No. 1 Port Cargo Valve			8.01%	0.00%	0.12%	0.00%
Raffinate			1325667740	613697.35	32776869.44	293271.3
			53026709.61	24547.894	512138.585	2932.713

carbon			5	5	8	10
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21703	9/28/2008	Test 23	613049550.62	1751993.62	8161401.95	129214.28
Can ID 1491						
Slop Tank PV Vent			17.25%	0.05%	0.23%	0.00%
Unleaded Gasoline			3065247753	8759968.1	65291215.6	1292142.8
			122609910.1	350398.724	1020175.244	12921.428

carbon			5	5	8	10
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21642	9/25/2008	Test 3	488623976.82	2478772.65	5628446.64	13853.42
Can ID 1322						
#2 Starboard Cargo Hatch			29.67%	0.15%	0.34%	0.00%
Trans Mix			2443119884	12393863.25	45027573.12	138534.2
			97724795.36	495754.53	703555.83	1385.342

carbon 5 5 8 10

Lab Results: EPA PAMS Analysis via GC/

carbon			7	6	9	4
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21640	9/24/2008	Test # 1	3954803.70	26352694.80	1975243.35	769015270.50
Can ID 1481						
#2 Center Ullage Hatch			0.10%	0.68%	0.05%	19.98%
Unleaded Gasoline			27683625.9	158116168.8	17777190.15	3076061082
			564971.9571	4392115.8	219471.4833	192253817.6

carbon			7	6	9	4
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21641	9/25/2008	Test #2	8355314.70	31391331.30	613637.10	96587278.20
Can ID 1374						
#3 Starboard Cargo Hatch			0.39%	1.45%	0.03%	4.46%
Trans Mix			58487202.9	188347987.8	5522733.9	386349112.8
			1193616.386	5231888.55	68181.9	24146819.55

carbon			7	6	9	4
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21695	9/26/2008	Test #14	2881662.07	28756880.25	620214.49	28285473.79
Can ID 1396						
No. 1 Port Cargo Valve			0.09%	0.87%	0.02%	0.85%
Raffinate			20171634.49	172541281.5	5581930.41	113141895.2
			411666.01	4792813.375	68912.72111	7071368.448

carbon			7	6	9	4
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21703	9/28/2008	Test 23	3384274.01	18236315.37	2006621.76	1122176616.34
Can ID 1491						
Slop Tank PV Vent			0.10%	0.51%	0.06%	31.57%
Unleaded Gasoline			23689918.07	109417892.2	18059595.84	4488706465
			483467.7157	3039385.895	222957.9733	280544154.1

carbon			7	6	9	4
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21642	9/25/2008	Test 3	672880.40	24161354.01	550178.68	67863946.46
Can ID 1322						
#2 Starboard Cargo Hatch			0.04%	1.47%	0.03%	4.12%
Trans Mix			4710162.8	144968124.1	4951608.12	271455785.8
			96125.77143	4026892.335	61130.96444	16965986.62

carbon 7 6 9 4

Lab Results: EPA PAMS Analysis via GC/

carbon			10	7	6	9
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21640	9/24/2008	Test # 1	50724.75	10327559.10	42735709.80	429757.35
Can ID 1481						
#2 Center Ullage Hatch			0.00%	0.27%	1.11%	0.01%
Unleaded Gasoline			507247.5	72292913.7	256414258.8	3867816.15
			5072.475	1475365.586	7122618.3	47750.81667

carbon			10	7	6	9
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21641	9/25/2008	Test #2	89183.70	13191201.00	38299740.30	725449.50
Can ID 1374						
#3 Starboard Cargo Hatch			0.00%	0.61%	1.77%	0.03%
Trans Mix			891837	92338407	229798441.8	6529045.5
			8918.37	1884457.286	6383290.05	80605.5

carbon			10	7	6	9
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21695	9/26/2008	Test #14	456199.80	41485940.86	410553751.44	1363168.45
Can ID 1396						
No. 1 Port Cargo Valve			0.01%	1.25%	12.40%	0.04%
Raffinate			4561998	290401586	2463322509	12268516.05
			45619.98	5926562.98	68425625.24	151463.1611

carbon			10	7	6	9
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21703	9/28/2008	Test 23	590965.31	4372383.21	37192810.33	1284541.96
Can ID 1491						
Slop Tank PV Vent			0.02%	0.12%	1.05%	0.04%
Unleaded Gasoline			5909653.1	30606682.47	223156862	11560877.64
			59096.531	624626.1729	6198801.722	142726.8844

carbon			10	7	6	9
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21642	9/25/2008	Test 3	127649.37	2713291.26	3718653.74	758969.51
Can ID 1322						
#2 Starboard Cargo Hatch			0.01%	0.16%	0.23%	0.05%
Trans Mix			1276493.7	18993038.82	22311922.44	6830725.59
			12764.937	387613.0371	619775.6233	84329.94556

carbon 10 7 6 9

Lab Results: EPA PAMS Analysis via GC/

carbon			8	5	9	11
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21640	9/24/2008	Test # 1	2751008.25	183877866.30	775549.05	0.00
Can ID 1481						
#2 Center Ullage Hatch			0.07%	4.78%	0.02%	0.00%
Unleaded Gasoline			22008066	919389331.5	6979941.45	0
			343876.0313	36775573.26	86172.11667	0

carbon			8	5	9	11
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21641	9/25/2008	Test #2	5436212.40	235455616.80	175705.20	23959.80
Can ID 1374						
#3 Starboard Cargo Hatch			0.25%	10.88%	0.01%	0.00%
Trans Mix			43489699.2	1177278084	1581346.8	263557.8
			679526.55	47091123.36	19522.8	2178.163636

carbon			8	5	9	11
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21695	9/26/2008	Test #14	1861729.66	178515326.50	290012.73	40189.03
Can ID 1396						
No. 1 Port Cargo Valve			0.06%	5.39%	0.01%	0.00%
Raffinate			14893837.28	892576632.5	2610114.57	442079.33
			232716.2075	35703065.3	32223.63667	3653.548182

carbon			8	5	9	11
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21703	9/28/2008	Test 23	2251748.85	365566200.22	693576.65	146316.17
Can ID 1491						
Slop Tank PV Vent			0.06%	10.29%	0.02%	0.00%
Unleaded Gasoline			18013990.8	1827831001	6242189.85	1609477.87
			281468.6063	73113240.04	77064.07222	13301.47

carbon			8	5	9	11
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21642	9/25/2008	Test 3	326544.90	186376985.97	133586.55	18801.07
Can ID 1322						
#2 Starboard Cargo Hatch			0.02%	11.32%	0.01%	0.00%
Trans Mix			2612359.2	931884929.9	1202278.95	206811.77
			40818.1125	37275397.19	14842.95	1709.188182

carbon 8 5 9 11

Lab Results: EPA PAMS Analysis via GC/

carbon			8	9	10	9
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21640	9/24/2008	Test # 1	6072292.20	686187.15	86771.70	843973.50
Can ID 1481						
#2 Center Ullage Hatch			0.16%	0.02%	0.00%	0.02%
Unleaded Gasoline			48578337.6	6175684.35	867717	7595761.5
			759036.525	76243.01667	8677.17	93774.83333

carbon			8	9	10	9
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21641	9/25/2008	Test #2	1538751.60	200996.10	54575.10	31946.40
Can ID 1374						
#3 Starboard Cargo Hatch			0.07%	0.01%	0.00%	0.00%
Trans Mix			12310012.8	1808964.9	545751	287517.6
			192343.95	22332.9	5457.51	3549.6

carbon			8	9	10	9
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21695	9/26/2008	Test #14	1686853.07	234617.04	55395.69	107532.81
Can ID 1396						
No. 1 Port Cargo Valve			0.05%	0.01%	0.00%	0.00%
Raffinate			13494824.56	2111553.36	553956.9	967795.29
			210856.6338	26068.56	5539.569	11948.09

carbon			8	9	10	9
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21703	9/28/2008	Test 23	3418477.79	661273.08	117813.02	153917.01
Can ID 1491						
Slop Tank PV Vent			0.10%	0.02%	0.00%	0.00%
Unleaded Gasoline			27347822.32	5951457.72	1178130.2	1385253.09
			427309.7238	73474.78667	11781.302	17101.89

carbon			8	9	10	9
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21642	9/25/2008	Test 3	1904845.25	185042.11	70256.63	26717.31
Can ID 1322						
#2 Starboard Cargo Hatch			0.12%	0.01%	0.00%	0.00%
Trans Mix			15238762	1665378.99	702566.3	240455.79
			238105.6563	20560.23444	7025.663	2968.59

carbon 8 9 10 9



Lab Results: EPA PAMS Analysis via GC/

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21640	9/24/2008	Test # 1	250978508.25	2821591.20	172680.00	47240067.60
Can ID 1481						
#2 Center Ullage Hatch			6.52%	0.07%	0.00%	1.23%
Unleaded Gasoline			752935524.8	8464773.6	1381440	330680473.2
			83659502.75	940530.4	21585	6748581.086

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21641	9/25/2008	Test #2	53236013.40	11218510.80	93177.00	14712648.30
Can ID 1374						
#3 Starboard Cargo Hatch			2.46%	0.52%	0.00%	0.68%
Trans Mix			159708040.2	33655532.4	745416	102988538.1
			17745337.8	3739503.6	11647.125	2101806.9

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21695	9/26/2008	Test #14	569163.56	11948.09	197686.58	111174805.07
Can ID 1396						
No. 1 Port Cargo Valve			0.02%	0.00%	0.01%	3.36%
Raffinate			1707490.68	35844.27	1581492.64	778223635.5
			189721.1867	3982.696667	24710.8225	15882115.01

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21703	9/28/2008	Test 23	34317792.60	5848846.38	95010.50	12347564.58
Can ID 1491						
Slop Tank PV Vent			0.97%	0.16%	0.00%	0.35%
Unleaded Gasoline			102953377.8	17546539.14	760084	86432952.06
			11439264.2	1949615.46	11876.3125	1763937.797

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21642	9/25/2008	Test 3	33431271.05	6894055.51	189989.76	13097419.08
Can ID 1322						
#2 Starboard Cargo Hatch			2.03%	0.42%	0.01%	0.80%
Trans Mix			100293813.2	20682166.53	1519918.08	91681933.56
			11143757.02	2298018.503	23748.72	1871059.869

carbon 3 3 8 7

Lab Results: EPA PAMS Analysis via GC/

carbon			4	5	4.5	
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21640	9/24/2008	Test # 1	3848454405.00	47302448.25	62206459.05	438194926.50
Can ID 1481						
#2 Center Ullage Hatch			100.00%	1.23%	1.62%	11.39%
Unleaded Gasoline			17584987597	189209793	311032295.3	1971877169
			878021886.7	11825612.06	12441291.81	97376650.33

carbon			4	5	4.5	
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21641	9/25/2008	Test #2	2164634820.00	19509932.70	81247681.80	393531728.40
Can ID 1374						
#3 Starboard Cargo Hatch			100.00%	0.90%	3.75%	18.18%
Trans Mix			10791861304	78039730.8	406238409	1770892778
			448876329.7	4877483.175	16249536.36	87451495.2

carbon			4	5	4.5	
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21695	9/26/2008	Test #14	3311032977.00	263944.17	1554337.89	192914947.33
Can ID 1396						
No. 1 Port Cargo Valve			100.00%	0.01%	0.05%	5.83%
Raffinate			19475864081	1055776.68	7771689.45	868117263
			570959543	65986.0425	310867.578	42869988.3

carbon			4	5	4.5	
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21703	9/28/2008	Test 23	3554152784.00	82030165.49	41105342.72	276389344.92
Can ID 1491						
Slop Tank PV Vent			100.00%	2.31%	1.16%	7.78%
Unleaded Gasoline			16201327275	328120662	205526713.6	1243752052
			799270393.8	20507541.37	8221068.544	61419854.43

carbon			4	5	4.5	
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21642	9/25/2008	Test 3	1646874779.00	14655928.83	65532613.78	505299536.38
Can ID 1322						
#2 Starboard Cargo Hatch			100.00%	0.89%	3.98%	30.68%
Trans Mix			7977154477	58623715.32	327663068.9	2273847914
			348536242.9	3663982.208	13106522.76	112288785.9

carbon 4 5 4.5

Lab Results: EPA PAMS Analysis via GC/

carbon

SAMPNO	COLDATE	LOCCODE	
AL21640	9/24/2008	Test # 1	1.77 scfm
Can ID	1481		50.46673 liters/min
#2 Center Ullage Hatch			1.812307 moles/min
Unleaded Gasoline		4.569363632 average C	119.5598 grams/min
			0.263348 lbs/min
		87.80% by volume	15.80086 lbs/hr
			0.18961 tons/day
			69.20777 tons/year

carbon

SAMPNO	COLDATE	LOCCODE	
AL21641	9/25/2008	Test #2	0.390589 scfm
Can ID	1374		11.11206 liters/min
#3 Starboard Cargo Hatch			0.204006 moles/min
Trans Mix		4.985534375 average C	14.6471 grams/min
			0.032262 lbs/min
		44.89% by volume	1.93574 lbs/hr
			0.023229 tons/day
			8.478539 tons/year

carbon

SAMPNO	COLDATE	LOCCODE	
AL21695	9/26/2008	Test #14	0.390589 scfm
Can ID	1396		50.62509 liters/min
No. 1 Port Cargo Valve			1.182204 moles/min
Raffinate		5.882111177 average C	99.71835 grams/min
			0.219644 lbs/min
		57.10% by volume	13.17864 lbs/hr
			0.158144 tons/day
			57.72243 tons/year

carbon

SAMPNO	COLDATE	LOCCODE	
AL21703	9/28/2008	Test 23	0.357524 scfm
Can ID	1491		10.17139 liters/min
Slop Tank PV Vent			0.332503 moles/min
Unleaded Gasoline		4.558421728 average C	21.88462 grams/min
			0.048204 lbs/min
		79.93% by volume	2.892241 lbs/hr
			0.034707 tons/day
			12.66801 tons/year

carbon

SAMPNO	COLDATE	LOCCODE	
AL21642	9/25/2008	Test 3	
Can ID	1322		
#2 Starboard Cargo Hatch			
Trans Mix		4.843813615 average C	
		34.85% by volume	

carbon

Lab Results: EPA PAMS Analysis via GC/

carbon

SAMPNO	COLDATE	LOCCODE
AL21640	9/24/2008	Test # 1

Can ID 1481  
#2 Center Ullage Hatch  
Unleaded Gasoline

carbon

SAMPNO	COLDATE	LOCCODE
AL21641	9/25/2008	Test #2

Can ID 1374  
#3 Starboard Cargo Hatch  
Trans Mix )

carbon

SAMPNO	COLDATE	LOCCODE
AL21695	9/26/2008	Test #14

Can ID 1396  
No. 1 Port Cargo Valve  
Raffinate )

carbon

SAMPNO	COLDATE	LOCCODE
AL21703	9/28/2008	Test 23

Can ID 1491  
Slop Tank PV Vent  
Unleaded Gasoline )

carbon

SAMPNO	COLDATE	LOCCODE
AL21642	9/25/2008	Test 3

Can ID 1322  
#2 Starboard Cargo Hatch  
Trans Mix

carbon

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21643	9/25/2008	Test 4	13:27	.02	38475.00	1167075.00

Can ID 1397

#2 Port Cargo Hatch

Trans Mix

Area%ppbC	0.00%	0.05%
ppbC*#C	346275	10503675
ppbv	4275	129675

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21644	9/25/2008	Test 5	14:16	.02	37769.76	1200538.80

Can ID 1490

Starboard Lower Butterworth Hatch

Trans Mix

Area%ppbC	0.00%	0.13%
ppbC*#C	339927.84	10804849.2
ppbv	4196.64	133393.2

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21645	9/25/2008	Test 6	14:45	.02	119774.70	724297.95

Can ID 1502

PV Bullet Valve

Trans Mix

Area%ppbC	0.00%	0.02%
ppbC*#C	1077972.3	6518681.55
ppbv	13308.3	80477.55

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21646	9/25/2008	Test 7	15:05	.02	28623.40	1074478.40

Can ID 1375

Vent Stack (leaking Butterfly Valve)

Trans Mix

Area%ppbC	0.00%	0.03%
ppbC*#C	257610.6	9670305.6
ppbv	3180.377778	119386.4889

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21691	9/26/2008	Test 8	10:58	.02	115018.48	1508261.20

Can ID 1470

No. 1 Port Cargo/Ullage Hatch

Naphtha but cleaned

Area%ppbC	0.03%	0.40%
ppbC*#C	1035166.32	13574350.8
ppbv	12779.83111	167584.5778

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21692	9/26/2008	Test 9	11:17	.02	100853.81	1061564.33

Can ID 1478

SAMPNO	COLDATE	LOCCODE	5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21643	9/25/2008	Test 4	460417.50	419377.50	16022272.50	9461002.50

Can ID 1397

#2 Port Cargo Hatch	0.02%	0.02%	0.71%	0.42%
Trans Mix	4143757.5	1677510	64089090	56766015
	51157.5	104844.375	4005568.125	1576833.75

carbon 9 4 4 6

SAMPNO	COLDATE	LOCCODE	5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21644	9/25/2008	Test 5	446942.16	137589.84	5953233.60	4006292.40

Can ID 1490

Starboard Lower Butterworth Hatch	0.05%	0.02%	0.66%	0.45%
Trans Mix	4022479.44	550359.36	23812934.4	24037754.4
	49660.24	34397.46	1488308.4	667715.4

carbon 9 4 4 6

SAMPNO	COLDATE	LOCCODE	5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21645	9/25/2008	Test 6	334465.20	479098.80	15892746.75	7729987.95

Can ID 1502

PV Bullet Valve	0.01%	0.01%	0.44%	0.21%
Trans Mix	3010186.8	1916395.2	63570987	46379927.7
	37162.8	119774.7	3973186.688	1288331.325

carbon 9 4 4 6

SAMPNO	COLDATE	LOCCODE	5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21646	9/25/2008	Test 7	468983.40	435956.40	16130386.80	7711804.50

Can ID 1375

Vent Stack (leaking Butterfly Valve)	0.01%	0.01%	0.43%	0.21%
Trans Mix	4220850.6	1743825.6	64521547.2	46270827
	52109.26667	108989.1	4032596.7	1285300.75

carbon 9 4 4 6

SAMPNO	COLDATE	LOCCODE	5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21691	9/26/2008	Test 8	972231.68	23871.76	16276.20	90061.64

Can ID 1470

No. 1 Port Cargo/Ullage Hatch	0.26%	0.01%	0.00%	0.02%
Naphtha but cleaned	8750085.12	95487.04	65104.8	540369.84
	108025.7422	5967.94	4069.05	15010.27333

carbon 9 4 4 6

SAMPNO	COLDATE	LOCCODE	5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21692	9/26/2008	Test 9	851538.87	16635.68	39509.74	57185.15

Can ID 1478

SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21643	9/25/2008	Test 4	49991850.00	7505190.00	1471027.50	869535.00
Can ID 1397						
#2 Port Cargo Hatch			2.22%	0.33%	0.07%	0.04%
Trans Mix			249959250	60041520	8826165	6956280
			9998370	938148.75	245171.25	108691.875

carbon 5 8 6 8

SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21644	9/25/2008	Test 5	19526965.92	3207731.76	3525177.60	392086.08
Can ID 1490						
Starboard Lower Butterworth Hatch			2.18%	0.36%	0.39%	0.04%
Trans Mix			97634829.6	25661854.08	21151065.6	3136688.64
			3905393.184	400966.47	587529.6	49010.76

carbon 5 8 6 8

SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21645	9/25/2008	Test 6	54767546.55	7329985.65	5786473.95	1011305.25
Can ID 1502						
PV Bullet Valve			1.51%	0.20%	0.16%	0.03%
Trans Mix			273837732.8	58639885.2	34718843.7	8090442
			10953509.31	916248.2063	964412.325	126413.1563

carbon 5 8 6 8

SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21646	9/25/2008	Test 7	56379290.80	7552174.00	5897521.30	1068973.90
Can ID 1375						
Vent Stack (leaking Butterfly Valve)			1.50%	0.20%	0.16%	0.03%
Trans Mix			281896454	60417392	35385127.8	8551791.2
			11275858.16	944021.75	982920.2167	133621.7375

carbon 5 8 6 8

SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21691	9/26/2008	Test 8	34722.56	11935.88	827916.04	145400.72
Can ID 1470						
No. 1 Port Cargo/Ullage Hatch			0.01%	0.00%	0.22%	0.04%
Naphtha but cleaned			173612.8	95487.04	4967496.24	1163205.76
			6944.512	1491.985	137986.0067	18175.09

carbon 5 8 6 8

SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21692	9/26/2008	Test 9	21834.33	13516.49	587447.45	18715.14
Can ID 1478						

SAMPNO	COLDATE	LOCCODE	6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21643	9/25/2008	Test 4	4924800.00	773347.50	3575610.00	620730.00

Can ID 1397

#2 Port Cargo Hatch

Trans Mix

0.22%	0.03%	0.16%	0.03%
29548800	5413432.5	25029270	4965840
820800	110478.2143	510801.4286	77591.25

carbon

6

7

7

8

SAMPNO	COLDATE	LOCCODE	6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21644	9/25/2008	Test 5	2017085.04	321042.96	1482013.44	1064747.52

Can ID 1490

Starboard Lower Butterworth Hatch

Trans Mix

0.22%	0.04%	0.17%	0.12%
12102510.24	2247300.72	10374094.08	8517980.16
336180.84	45863.28	211716.2057	133093.44

carbon

6

7

7

8

SAMPNO	COLDATE	LOCCODE	6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21645	9/25/2008	Test 6	8339031.00	24714266.40	52263577.35	532206.45

Can ID 1502

PV Bullet Valve

Trans Mix

0.23%	0.68%	1.44%	0.01%
50034186	172999864.8	365845041.5	4257651.6
1389838.5	3530609.486	7466225.336	66525.80625

carbon

6

7

7

8

SAMPNO	COLDATE	LOCCODE	6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21646	9/25/2008	Test 7	8582616.40	25686198.80	54206114.20	566963.50

Can ID 1375

Vent Stack (leaking Butterfly Valve)

Trans Mix

0.23%	0.68%	1.44%	0.02%
51495698.4	179803391.6	379442799.4	4535708
1430436.067	3669456.971	7743730.6	70870.4375

carbon

6

7

7

8

SAMPNO	COLDATE	LOCCODE	6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21691	9/26/2008	Test 8	2240690.20	2853760.40	1242416.60	638027.04

Can ID 1470

No. 1 Port Cargo/Ullage Hatch

Naphtha but cleaned

0.59%	0.76%	0.33%	0.17%
13444141.2	19976322.8	8696916.2	5104216.32
373448.3667	407680.0571	177488.0857	79753.38

carbon

6

7

7

8

SAMPNO	COLDATE	LOCCODE	6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21692	9/26/2008	Test 9	1642773.40	2295723.84	979425.66	557295.28

Can ID 1478



SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21643	9/25/2008	Test 4	17459955.00	7575727.50	96187.50	515565.00
Can ID 1397						
#2 Port Cargo Hatch			0.77%	0.34%	0.00%	0.02%
Trans Mix			122219685	45454365	769500	3608955
			2494279.286	1262621.25	12023.4375	73652.14286

carbon 7 6 8 7

SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21644	9/25/2008	Test 5	7489203.84	3234710.16	583632.72	227517.84
Can ID 1490						
Starboard Lower Butterworth Hatch			0.83%	0.36%	0.07%	0.03%
Trans Mix			52424426.88	19408260.96	4669061.76	1592624.88
			1069886.263	539118.36	72954.09	32502.54857

carbon 7 6 8 7

SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21645	9/25/2008	Test 6	957067.65	14720988.60	49717.80	21004640.55
Can ID 1502						
PV Bullet Valve			0.03%	0.41%	0.00%	0.58%
Trans Mix			6699473.55	88325931.6	397742.4	147032483.9
			136723.95	2453498.1	6214.725	3000662.936

carbon 7 6 8 7

SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21646	9/25/2008	Test 7	982002.80	14946919.30	51742.30	21855066.80
Can ID 1375						
Vent Stack (leaking Butterfly Valve)			0.03%	0.40%	0.00%	0.58%
Trans Mix			6874019.6	89681515.8	413938.4	152985467.6
			140286.1143	2491153.217	6467.7875	3122152.4

carbon 7 6 8 7

SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21691	9/26/2008	Test 8	6342292.60	11287002.16	317928.44	7634622.88
Can ID 1470						
No. 1 Port Cargo/Ullage Hatch			1.68%	2.99%	0.08%	2.02%
Naphtha but cleaned			44396048.2	67722012.96	2543427.52	53442360.16
			906041.8	1881167.027	39741.055	1090660.411

carbon 7 6 8 7

SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21692	9/26/2008	Test 9	5096756.46	8312641.35	276568.18	6162479.71
Can ID 1478						

SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21643	9/25/2008	Test 4	61999897.50	8977.50	12480007.50	18019125.00

Can ID 1397

#2 Port Cargo Hatch	2.75%	0.00%	0.55%	0.80%
Trans Mix	371999385	17955	74880045	72076500
	10333316.25	4488.75	2080001.25	4504781.25

carbon 6 2 6 4

SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21644	9/25/2008	Test 5	25586314.56	9892.08	5401974.96	6585427.44

Can ID 1490

Starboard Lower Butterworth Hatch	2.85%	0.00%	0.60%	0.73%
Trans Mix	153517887.4	19784.16	32411849.76	26341709.76
	4264385.76	4946.04	900329.16	1646356.86

carbon 6 2 6 4

SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21645	9/25/2008	Test 6	95159869.20	10169.55	15379749.45	41283853.20

Can ID 1502

PV Bullet Valve	2.62%	0.00%	0.42%	1.14%
Trans Mix	570959215.2	20339.1	92278496.7	165135412.8
	15859978.2	5084.775	2563291.575	10320963.3

carbon 6 2 6 4

SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21646	9/25/2008	Test 7	98043952.20	19816.20	15957545.50	42112727.70

Can ID 1375

Vent Stack (leaking Butterfly Valve)	2.61%	0.00%	0.42%	1.12%
Trans Mix	588263713.2	39632.4	95745273	168450910.8
	16340658.7	9908.1	2659590.917	10528181.93

carbon 6 2 6 4

SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21691	9/26/2008	Test 8	8173907.64	10850.80	3739185.68	17361.28

Can ID 1470

No. 1 Port Cargo/Ullage Hatch	2.16%	0.00%	0.99%	0.00%
Naphtha but cleaned	49043445.84	21701.6	22435114.08	69445.12
	1362317.94	5425.4	623197.6133	4340.32

carbon 6 2 6 4

SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21692	9/26/2008	Test 9	6085539.69	9357.57	2825986.14	0.00

Can ID 1478

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21643	9/25/2008	Test 4	46625287.50	155182.50	1291477.50	17253472.50

Can ID 1397

#2 Port Cargo Hatch

Trans Mix

2.07%	0.01%	0.06%	0.77%
233126437.5	1396642.5	7748865	86267362.5
9325057.5	17242.5	215246.25	3450694.5

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21644	9/25/2008	Test 5	18697829.76	111510.72	471222.72	7008089.04

Can ID 1490

Starboard Lower Butterworth Hatch

Trans Mix

2.08%	0.01%	0.05%	0.78%
93489148.8	1003596.48	2827336.32	35040445.2
3739565.952	12390.08	78537.12	1401617.808

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21645	9/25/2008	Test 6	97655928.75	93785.85	613562.85	18414795.15

Can ID 1502

PV Bullet Valve

Trans Mix

2.69%	0.00%	0.02%	0.51%
488279643.8	844072.65	3681377.1	92073975.75
19531185.75	10420.65	102260.475	3682959.03

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21646	9/25/2008	Test 7	101673619.50	149722.40	626412.10	19084101.50

Can ID 1375

Vent Stack (leaking Butterfly Valve)

Trans Mix

2.70%	0.00%	0.02%	0.51%
508368097.5	1347501.6	3758472.6	95420507.5
20334723.9	16635.82222	104402.0167	3816820.3

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21691	9/26/2008	Test 8	27127.00	899531.32	13326952.56	2216818.44

Can ID 1470

No. 1 Port Cargo/Ullage Hatch

Naphtha but cleaned

0.01%	0.24%	3.53%	0.59%
135635	8095781.88	79961715.36	11084092.2
5425.4	99947.92444	2221158.76	443363.688

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21692	9/26/2008	Test 9	48867.31	774598.85	10489835.97	1604303.39

Can ID 1478

SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21643	9/25/2008	Test 4	13175122.50	2745832.50	475807.50	3683340.00

Can ID 1397

#2 Port Cargo Hatch

Trans Mix

0.58% 0.12% 0.02% 0.16%

26350245 21966660 951615 14733360

6587561.25 343229.0625 237903.75 920835

carbon 2 8 2 4

SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21644	9/25/2008	Test 5	4201436.16	1559351.52	136690.56	2093523.84

Can ID 1490

Starboard Lower Butterworth Hatch

Trans Mix

0.47% 0.17% 0.02% 0.23%

8402872.32 12474812.16 273381.12 8374095.36

2100718.08 194918.94 68345.28 523380.96

carbon 2 8 2 4

SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21645	9/25/2008	Test 6	10891588.05	2148034.95	210170.70	43540363.35

Can ID 1502

PV Bullet Valve

Trans Mix

0.30% 0.06% 0.01% 1.20%

21783176.1 17184279.6 420341.4 174161453.4

5445794.025 268504.3688 105085.35 10885090.84

carbon 2 8 2 4

SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21646	9/25/2008	Test 7	11167529.60	2408769.20	214675.50	43411789.70

Can ID 1375

Vent Stack (leaking Butterfly Valve)

Trans Mix

0.30% 0.06% 0.01% 1.15%

22335059.2 19270153.6 429351 173647158.8

5583764.8 301096.15 107337.75 10852947.43

carbon 2 8 2 4

SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21691	9/26/2008	Test 8	1911910.96	2366559.48	10850.80	4710332.28

Can ID 1470

No. 1 Port Cargo/Ullage Hatch

Naphtha but cleaned

0.51% 0.63% 0.00% 1.25%

3823821.92 18932475.84 21701.6 18841329.12

955955.48 295819.935 5425.4 1177583.07

carbon 2 8 2 4

SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21692	9/26/2008	Test 9	1398436.85	1904785.36	9357.57	2978826.45

Can ID 1478

SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
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AL21643	9/25/2008	Test 4	672115927.50	3353737.50	8921070.00	46170.00
Can ID 1397						
#2 Port Cargo Hatch			29.81%	0.15%	0.40%	0.00%
Trans Mix			3360579638	16768687.5	71368560	461700
			134423185.5	670747.5	1115133.75	4617

carbon 5 5 8 10

SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
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AL21644	9/25/2008	Test 5	255035808.00	1300358.88	5275176.48	68345.28
Can ID 1490						
Starboard Lower Butterworth Hatch			28.41%	0.14%	0.59%	0.01%
Trans Mix			1275179040	6501794.4	42201411.84	683452.8
			51007161.6	260071.776	659397.06	6834.528

carbon 5 5 8 10

SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
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AL21645	9/25/2008	Test 6	1345633726.05	2087017.65	9870113.25	39548.25
Can ID 1502						
PV Bullet Valve			37.05%	0.06%	0.27%	0.00%
Trans Mix			6728168630	10435088.25	78960906	395482.5
			269126745.2	417403.53	1233764.156	3954.825

carbon 5 5 8 10

SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
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AL21646	9/25/2008	Test 7	1388414346.70	2038866.80	8558396.60	40733.30
Can ID 1375						
Vent Stack (leaking Butterfly Valve)			36.93%	0.05%	0.23%	0.00%
Trans Mix			6942071734	10194334	68467172.8	407333
			277682869.3	407773.36	1069799.575	4073.33

carbon 5 5 8 10

SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
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AL21691	9/26/2008	Test 8	17382981.60	0.00	13933512.28	46658.44
Can ID 1470						
No. 1 Port Cargo/Ullage Hatch			4.60%	0.00%	3.69%	0.01%
Naphtha but cleaned			86914908	0	111468098.2	466584.4
			3476596.32	0	1741689.035	4665.844

carbon 5 5 8 10

SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
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AL21692	9/26/2008	Test 9	11746869.54	0.00	11621062.21	34311.09
Can ID 1478						

SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	Methylcyclopentar	m Ethyltoluene	n Butane
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AL21643	9/25/2008	Test 4	970852.50	33622020.00	919552.50	90344430.00
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Can ID 1397

#2 Port Cargo Hatch			0.04%	1.49%	0.04%	4.01%
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Trans Mix			6795967.5	201732120	8275972.5	361377720
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			138693.2143	5603670	102172.5	22586107.5
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carbon 7 6 9 4

SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	Methylcyclopentar	m Ethyltoluene	n Butane
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AL21644	9/25/2008	Test 5	423560.88	14272472.88	825539.04	33123180.24
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Can ID 1490

Starboard Lower Butterworth Hatch			0.05%	1.59%	0.09%	3.69%
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Trans Mix			2964926.16	85634837.28	7429851.36	132492721
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			60508.69714	2378745.48	91726.56	8280795.06
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carbon 7 6 9 4

SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	Methylcyclopentar	m Ethyltoluene	n Butane
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AL21645	9/25/2008	Test 6	3258775.80	428251.05	702828.90	81124760.25
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Can ID 1502

PV Bullet Valve			0.09%	0.01%	0.02%	2.23%
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Trans Mix			22811430.6	2569506.3	6325460.1	324499041
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			465539.4	71375.175	78092.1	20281190.06
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carbon 7 6 9 4

SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	Methylcyclopentar	m Ethyltoluene	n Butane
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AL21646	9/25/2008	Test 7	3446917.90	452469.90	899435.30	82756854.80
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Can ID 1375

Vent Stack (leaking Butterfly Valve)			0.09%	0.01%	0.02%	2.20%
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Trans Mix			24128425.3	2714819.4	8094917.7	331027419.2
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			492416.8429	75411.65	99937.25556	20689213.7
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carbon 7 6 9 4

SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	Methylcyclopentar	m Ethyltoluene	n Butane
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AL21691	9/26/2008	Test 8	26318615.40	13069788.60	1574451.08	12518567.96
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Can ID 1470

No. 1 Port Cargo/Ullage Hatch			6.97%	3.46%	0.42%	3.31%
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Naphtha but cleaned			184230307.8	78418731.6	14170059.72	50074271.84
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			3759802.2	2178298.1	174939.0089	3129641.99
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carbon 7 6 9 4

SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	Methylcyclopentar	m Ethyltoluene	n Butane
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AL21692	9/26/2008	Test 9	22458168.00	9954375.02	1318377.64	8186834.02
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Can ID 1478

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21643	9/25/2008	Test 4	214177.50	5024835.00	5159497.50	1256850.00

Can ID 1397

#2 Port Cargo Hatch

Trans Mix

0.01% 0.22% 0.23% 0.06%

2141775 35173845 30956985 11311650

21417.75 717833.5714 859916.25 139650

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21644	9/25/2008	Test 5	241906.32	2201437.44	2197840.32	747301.68

Can ID 1490

Starboard Lower Butterworth Hatch

Trans Mix

0.03% 0.25% 0.24% 0.08%

2419063.2 15410062.08 13187041.92 6725715.12

24190.632 314491.0629 366306.72 83033.52

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21645	9/25/2008	Test 6	88136.10	1740123.00	8584230.15	690399.45

Can ID 1502

PV Bullet Valve

Trans Mix

0.00% 0.05% 0.24% 0.02%

881361 12180861 51505380.9 6213595.05

8813.61 248589 1430705.025 76711.05

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21646	9/25/2008	Test 7	205868.30	1820888.60	8872153.10	976498.30

Can ID 1375

Vent Stack (leaking Butterfly Valve)

Trans Mix

0.01% 0.05% 0.24% 0.03%

2058683 12746220.2 53232918.6 8788484.7

20586.83 260126.9429 1478692.183 108499.8111

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21691	9/26/2008	Test 8	985252.64	14893808.08	17220219.60	6447545.36

Can ID 1470

No. 1 Port Cargo/Ullage Hatch

Naphtha but cleaned

0.26% 3.94% 4.56% 1.71%

9852526.4 104256656.6 103321317.6 58027908.24

98525.264 2127686.869 2870036.6 716393.9289

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21692	9/26/2008	Test 9	916002.13	12214748.04	12944638.50	5544880.09

Can ID 1478

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
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AL21643	9/25/2008	Test 4	484785.00	252643522.50	214177.50	47452.50
Can ID 1397						
#2 Port Cargo Hatch			0.02%	11.20%	0.01%	0.00%
Trans Mix			3878280	1263217613	1927597.5	521977.5
			60598.125	50528704.5	23797.5	4313.863636

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
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AL21644	9/25/2008	Test 5	544064.40	100025115.84	207733.68	133093.44
Can ID 1490						
Starboard Lower Butterworth Hatch			0.06%	11.14%	0.02%	0.01%
Trans Mix			4352515.2	500125579.2	1869603.12	1464027.84
			68008.05	20005023.17	23081.52	12099.40364

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
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AL21645	9/25/2008	Test 6	392092.65	231529014.90	167232.60	143503.65
Can ID 1502						
PV Bullet Valve			0.01%	6.38%	0.00%	0.00%
Trans Mix			3136741.2	1157645075	1505093.4	1578540.15
			49011.58125	46305802.98	18581.4	13045.78636

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
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AL21646	9/25/2008	Test 7	430451.90	238889795.50	255408.80	51742.30
Can ID 1375						
Vent Stack (leaking Butterfly Valve)			0.01%	6.35%	0.01%	0.00%
Trans Mix			3443615.2	1194448978	2298679.2	569165.3
			53806.4875	47777959.1	28378.75556	4703.845455

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
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AL21691	9/26/2008	Test 8	17040096.32	18919454.88	642367.36	24956.84
Can ID 1470						
No. 1 Port Cargo/Ullage Hatch			4.51%	5.01%	0.17%	0.01%
Naphtha but cleaned			136320770.6	94597274.4	5781306.24	274525.24
			2130012.04	3783890.976	71374.15111	2268.803636

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
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AL21692	9/26/2008	Test 9	14514630.80	13141147.47	533381.49	18715.14
Can ID 1478						



SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
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AL21643 9/25/2008 Test 4  
 Can ID 1397  
 #2 Port Cargo Hatch  
 Trans Mix  
 3149820.00 283432.50 128250.00 46170.00  
 0.14% 0.01% 0.01% 0.00%  
 25198560 2550892.5 1282500 415530  
 393727.5 31492.5 12825 5130

carbon 8 9 10 9

SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
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AL21644 9/25/2008 Test 5  
 Can ID 1490  
 Starboard Lower Butterworth Hatch  
 Trans Mix  
 1935250.56 275179.68 58453.20 41366.88  
 0.22% 0.03% 0.01% 0.00%  
 15482004.48 2476617.12 584532 372301.92  
 241906.32 30575.52 5845.32 4596.32

carbon 8 9 10 9

SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
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AL21645 9/25/2008 Test 6  
 Can ID 1502  
 PV Bullet Valve  
 Trans Mix  
 2497189.50 204520.95 49717.80 29378.70  
 0.07% 0.01% 0.00% 0.00%  
 19977516 1840688.55 497178 264408.3  
 312148.6875 22724.55 4971.78 3264.3

carbon 8 9 10 9

SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
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AL21646 9/25/2008 Test 7  
 Can ID 1375  
 Vent Stack (leaking Butterfly Valve)  
 Trans Mix  
 2919586.80 277426.80 28623.40 51742.30  
 0.08% 0.01% 0.00% 0.00%  
 23356694.4 2496841.2 286234 465680.7  
 364948.35 30825.2 2862.34 5749.144444

carbon 8 9 10 9

SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
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AL21691 9/26/2008 Test 8  
 Can ID 1470  
 No. 1 Port Cargo/Ullage Hatch  
 Naphtha but cleaned  
 5184512.24 572922.24 73785.44 365671.96  
 1.37% 0.15% 0.02% 0.10%  
 41476097.92 5156300.16 737854.4 3291047.64  
 648064.03 63658.02667 7378.544 40630.21778

carbon 8 9 10 9

SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
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AL21692 9/26/2008 Test 9  
 Can ID 1478

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21643	9/25/2008	Test 4	40129425.00	8055382.50	336015.00	20450745.00

Can ID 1397

#2 Port Cargo Hatch

Trans Mix

1.78% 0.36% 0.01% 0.91%

120388275 24166147.5 2688120 143155215

13376475 2685127.5 42001.875 2921535

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21644	9/25/2008	Test 5	14373192.24	2769782.40	122302.08	9776072.88

Can ID 1490

Starboard Lower Butterworth Hatch

Trans Mix

1.60% 0.31% 0.01% 1.09%

43119576.72 8309347.2 978416.64 68432510.16

4791064.08 923260.8 15287.76 1396581.84

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21645	9/25/2008	Test 6	18069030.45	7145803.80	124294.50	20091640.95

Can ID 1502

PV Bullet Valve

Trans Mix

0.50% 0.20% 0.00% 0.55%

54207091.35 21437411.4 994356 140641486.7

6023010.15 2381934.6 15536.8125 2870234.421

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21646	9/25/2008	Test 7	18422460.60	7186675.20	168437.70	21375074.40

Can ID 1375

Vent Stack (leaking Butterfly Valve)

Trans Mix

0.49% 0.19% 0.00% 0.57%

55267381.8 21560025.6 1347501.6 149625520.8

6140820.2 2395558.4 21054.7125 3053582.057

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21691	9/26/2008	Test 8	7591219.68	24956.84	308162.72	10296324.12

Can ID 1470

No. 1 Port Cargo/Ullage Hatch

Naphtha but cleaned

2.01% 0.01% 0.08% 2.73%

22773659.04 74870.52 2465301.76 72074268.84

2530406.56 8318.946667 38520.34 1470903.446

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21692	9/26/2008	Test 9	4753645.56	18715.14	260972.23	8232582.14

Can ID 1478

SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21643	9/25/2008	Test 4	2254763250.00	19552995.00	88144942.50	698285340.00
Can ID 1397						
#2 Port Cargo Hatch			100.00%	0.87%	3.91%	30.97%
Trans Mix			10969390508	78211980	440724712.5	3142284030
			474705970.1	4888248.75	17628988.5	155174520

carbon 4 5 4.5

SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21644	9/25/2008	Test 5	897751224.00	7103412.72	35318322.72	282637409.04
Can ID 1490						
Starboard Lower Butterworth Hatch			100.00%	0.79%	3.93%	31.48%
Trans Mix			4411936475	28413650.88	176591613.6	1271868341
			187395802.1	1775853.18	7063664.544	62808313.12

carbon 4 5 4.5

SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21645	9/25/2008	Test 6	3631546305.00	54914440.05	242296308.45	1057485176.55
Can ID 1502						
PV Bullet Valve			100.00%	1.51%	6.67%	29.12%
Trans Mix			17798670138	219657760.2	1211481542	4758683294
			753951469.3	13728610.01	48459261.69	234996705.9

carbon 4 5 4.5

SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21646	9/25/2008	Test 7	3759463410.00	56204247.70	252398939.40	1103822889.50
Can ID 1375						
Vent Stack (leaking Butterfly Valve)			100.00%	1.50%	6.71%	29.36%
Trans Mix			18428357571	224816990.8	1261994697	4967203003
			780363080.6	14051061.93	50479787.88	245293975.4

carbon 4 5 4.5

SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21691	9/26/2008	Test 8	377716348.00	29297.16	35807.64	118501586.80
Can ID 1470						
No. 1 Port Cargo/Ullage Hatch			100.00%	0.01%	0.01%	31.37%
Naphtha but cleaned			2178030085	117188.64	179038.2	533257140.6
			70055849.14	7324.29	7161.528	26333685.96

carbon 4 5 4.5

SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21692	9/26/2008	Test 9	299130321.00	32231.63	20794.60	99683074.02
Can ID 1478						

SAMPNO	COLDATE	LOCCODE
AL21643	9/25/2008	Test 4

Can ID 1397

#2 Port Cargo Hatch

Trans Mix

4.864985496 average C

47.47% by volume

carbon

SAMPNO	COLDATE	LOCCODE
AL21644	9/25/2008	Test 5

Can ID 1490

Starboard Lower Butterworth Hatch

Trans Mix

4.914431033 average C

18.74% by volume

carbon

SAMPNO	COLDATE	LOCCODE
AL21645	9/25/2008	Test 6

Can ID 1502

PV Bullet Valve

Trans Mix

4.901127135 average C

75.40% by volume

0.68 scfm

19.25197 liters/min

0.593663 moles/min

41.92194 grams/min

0.092339 lbs/min

5.540345 lbs/hr

0.066484 tons/day

24.26671 tons/year

carbon

SAMPNO	COLDATE	LOCCODE
AL21646	9/25/2008	Test 7

Can ID 1375

Vent Stack (leaking Butterfly Valve)

Trans Mix

4.901858473 average C

78.04% by volume

0.97 scfm

27.53988 liters/min

0.878982 moles/min

62.07898 grams/min

0.136738 lbs/min

8.204271 lbs/hr

0.098451 tons/day

35.93471 tons/year

carbon

SAMPNO	COLDATE	LOCCODE
AL21691	9/26/2008	Test 8

Can ID 1470

No. 1 Port Cargo/Ullage Hatch

Naphtha but cleaned

5.766311405 average C

7.01% by volume

2.18 scfm

62.07941 liters/min

0.177874 moles/min

14.71525 grams/min

0.032412 lbs/min

1.944746 lbs/hr

0.023337 tons/day

8.517989 tons/year

carbon

SAMPNO	COLDATE	LOCCODE
AL21692	9/26/2008	Test 9

Can ID 1478

1.630694 scfm

46.39243 liters/min

SAMPNO	COLDATE	LOCCODE
AL21643	9/25/2008	Test 4

Can ID 1397  
 #2 Port Cargo Hatch  
 Trans Mix

carbon

SAMPNO	COLDATE	LOCCODE
AL21644	9/25/2008	Test 5

Can ID 1490  
 Starboard Lower Butterworth Hatch  
 Trans Mix

carbon

SAMPNO	COLDATE	LOCCODE
AL21645	9/25/2008	Test 6

Can ID 1502  
 PV Bullet Valve  
 Trans Mix )

carbon

SAMPNO	COLDATE	LOCCODE
AL21646	9/25/2008	Test 7

Can ID 1375  
 Vent Stack (leaking Butterfly Valve)  
 Trans Mix )

carbon

SAMPNO	COLDATE	LOCCODE
AL21691	9/26/2008	Test 8

Can ID 1470  
 No. 1 Port Cargo/Ullage Hatch  
 Naphtha but cleaned )

carbon

SAMPNO	COLDATE	LOCCODE
AL21692	9/26/2008	Test 9

Can ID 1478

#2 Starboard Cargo & Ullage Hatch  
 Naphtha but cleaned

Area%ppbC 0.03% 0.35%  
 ppbC\*#C 907684.29 9554078.97

ppbv 11205.97889 117951.5922

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21693	9/26/2008	Test 10	11:45	.02	161702.80	1243956.54

Can ID 1418  
 No. 3 Starboard Cargo/Ullage Hatch  
 Naphtha but cleaned

Area%ppbC 0.08% 0.60%  
 ppbC\*#C 1455325.2 11195608.86

ppbv 17966.97778 138217.3933

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21694	9/26/2008	Test 11	12:04	.02	214344.35	932550.30

Can ID 1394  
 No. 2 Port Cargo Valve  
 Naphtha but cleaned

Area%ppbC 0.06% 0.27%  
 ppbC\*#C 1929099.15 8392952.7

ppbv 23816.03889 103616.7

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21696	9/26/2008	Test 15	14:10	.02	55547.36	770088.40

Can ID 1348  
 No. 1 Port Ullage Hatch  
 Raffinate

Area%ppbC 0.00% 0.04%  
 ppbC\*#C 499926.24 6930795.6

ppbv 6171.928889 85565.37778

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21697	9/26/2008	Test 16	14:50	.02	122804.64	942639.32

Can ID 1431  
 No. 3 Starboard Cargo Ullage Hatch  
 Raffinate

Area%ppbC 0.01% 0.04%  
 ppbC\*#C 1105241.76 8483753.88

ppbv 13644.96 104737.7022

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21698	9/26/2008	Test 17	15:30	.02	51880.80	333334.14

Can ID 1347  
 No. 3 Starboard High Level Alarm Tester  
 Raffinate

Area%ppbC 0.00% 0.03%  
 ppbC\*#C 466927.2 3000007.26

#2 Starboard Cargo & Ullage Hatch	0.28%	0.01%	0.01%	0.02%
Naphtha but cleaned	7663849.83	66542.72	158038.96	343110.9
	94615.43	4158.92	9877.435	9530.858333

carbon	9	4	4	6		
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21693	9/26/2008	Test 10	847784.68	12705.22	20790.36	64681.12

Can ID	1418			
No. 3 Starboard Cargo/Ullage Hatch	0.41%	0.01%	0.01%	0.03%
Naphtha but cleaned	7630062.12	50820.88	83161.44	388086.72
	94198.29778	3176.305	5197.59	10780.18667

carbon	9	4	4	6		
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21694	9/26/2008	Test 11	1199718.85	18285.30	18285.30	80252.15

Can ID	1394			
No. 2 Port Cargo Valve	0.34%	0.01%	0.01%	0.02%
Naphtha but cleaned	10797469.65	73141.2	73141.2	481512.9
	133302.0944	4571.325	4571.325	13375.35833

carbon	9	4	4	6		
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21696	9/26/2008	Test 15	398931.04	0.00	106044.96	3479284.64

Can ID	1348			
No. 1 Port Ullage Hatch	0.02%	0.00%	0.01%	0.17%
Raffinate	3590379.36	0	424179.84	20875707.84
	44325.67111	0	26511.24	579880.7733

carbon	9	4	4	6		
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21697	9/26/2008	Test 16	544661.32	36386.56	86418.08	2508398.48

Can ID	1431			
No. 3 Starboard Cargo Ullage Hatch	0.03%	0.00%	0.00%	0.12%
Raffinate	4901951.88	145546.24	345672.32	15050390.88
	60517.92444	9096.64	21604.52	418066.4133

carbon	9	4	4	6		
SAMPNO	COLDATE	LOCCODE	,5 Trimethylbenz	1,3 butadiene	1 Butene	1 Hexene
AL21698	9/26/2008	Test 17	185473.86	40207.62	16861.26	1586255.46

Can ID	1347			
No. 3 Starboard High Level Alarm Tester	0.02%	0.00%	0.00%	0.13%
Raffinate	1669264.74	160830.48	67445.04	9517532.76

#2 Starboard Cargo & Ullage Hatch	0.01%	0.00%	0.20%	0.01%
Naphtha but cleaned	109171.65	108131.92	3524684.7	149721.12
	4366.866	1689.56125	97907.90833	2339.3925

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21693	9/26/2008	Test 10	12705.22	8085.14	448147.76	57751.00

Can ID	1418					
No. 3 Starboard Cargo/Ullage Hatch	0.01%	0.00%	0.22%	0.03%		
Naphtha but cleaned	63526.1	64681.12	2688886.56	462008		
	2541.044	1010.6425	74691.29333	7218.875		

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21694	9/26/2008	Test 11	33523.05	5388068.40	758839.95	161520.15

Can ID	1394					
No. 2 Port Cargo Valve	0.01%	1.55%	0.22%	0.05%		
Naphtha but cleaned	167615.25	43104547.2	4553039.7	1292161.2		
	6704.61	673508.55	126473.325	20190.01875		

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21696	9/26/2008	Test 15	326971.96	1689144.72	94781470.32	70696.64

Can ID	1348					
No. 1 Port Ullage Hatch	0.02%	0.08%	4.59%	0.00%		
Raffinate	1634859.8	13513157.76	568688821.9	565573.12		
	65394.392	211143.09	15796911.72	8837.08		

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21697	9/26/2008	Test 16	359317.28	1487300.64	104407822.68	54579.84

Can ID	1431					
No. 3 Starboard Cargo Ullage Hatch	0.02%	0.07%	4.83%	0.00%		
Raffinate	1796586.4	11898405.12	626446936.1	436638.72		
	71863.456	185912.58	17401303.78	6822.48		

carbon			5	8	6	8
SAMPNO	COLDATE	LOCCODE	1 Pentene	4 Trimethylpentane	2 Dimethylbutane	4 Trimethylpentane
AL21698	9/26/2008	Test 17	184176.84	811934.52	53080543.50	45395.70

Can ID	1347					
No. 3 Starboard High Level Alarm Tester	0.02%	0.07%	4.46%	0.00%		
Raffinate	920884.2	6495476.16	318483261	363165.6		



#2 Starboard Cargo & Ullage Hatch	0.55%	0.77%	0.33%	0.19%
Naphtha but cleaned	9856640.4	16070066.88	6855979.62	4458362.24
	273795.5667	327960.5486	139917.9514	69661.91

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21693	9/26/2008	Test 10	1268211.96	1571982.22	716112.40	281824.88

Can ID	1418					
No. 3 Starboard Cargo/Ullage Hatch	0.62%	0.76%	0.35%	0.14%		
Naphtha but cleaned	7609271.76	11003875.54	5012786.8	2254599.04		
	211368.66	224568.8886	102301.7714	35228.11		

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21694	9/26/2008	Test 11	2086555.90	1786880.15	1176354.30	614589.25

Can ID	1394					
No. 2 Port Cargo Valve	0.60%	0.51%	0.34%	0.18%		
Naphtha but cleaned	12519335.4	12508161.05	8234480.1	4916714		
	347759.3167	255268.5929	168050.6143	76823.65625		

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21696	9/26/2008	Test 15	351900100.24	23076140.76	16274114.04	207040.16

Can ID	1348					
No. 1 Port Ullage Hatch	17.04%	1.12%	0.79%	0.01%		
Raffinate	2111400601	161532985.3	113918798.3	1656321.28		
	58650016.71	3296591.537	2324873.434	25880.02		

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21697	9/26/2008	Test 16	359589042.12	22773438.24	16452410.52	300189.12

Can ID	1431					
No. 3 Starboard Cargo Ullage Hatch	16.64%	1.05%	0.76%	0.01%		
Raffinate	2157534253	159414067.7	115166873.6	2401512.96		
	59931507.02	3253348.32	2350344.36	37523.64		

carbon			6	7	7	8
SAMPNO	COLDATE	LOCCODE	3 Dimethylbutan	3 Dimethylpenta	4 Dimethylpenta	2 Methylheptane
AL21698	9/26/2008	Test 17	203716446.30	12743221.50	9133614.84	123216.90

Can ID	1347					
No. 3 Starboard High Level Alarm Tester	17.12%	1.07%	0.77%	0.01%		
Raffinate	1222298678	89202550.5	63935303.88	985735.2		

#2 Starboard Cargo & Ullage Hatch	1.70%	2.78%	0.09%	2.06%
Naphtha but cleaned	35677295.22	49875848.1	2212545.44	43137357.97
	728108.0657	1385440.225	34571.0225	880354.2443

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21693	9/26/2008	Test 10	3451199.76	6520087.90	136292.36	4121111.36

Can ID	1418					
No. 3 Starboard Cargo/Ullage Hatch	1.68%	3.17%	0.07%	2.00%		
Naphtha but cleaned	24158398.32	39120527.4	1090338.88	28847779.52		
	493028.5371	1086681.317	17036.545	588730.1943		

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21694	9/26/2008	Test 11	5931548.15	10531316.95	311865.95	7174948.55

Can ID	1394					
No. 2 Port Cargo Valve	1.70%	3.02%	0.09%	2.06%		
Naphtha but cleaned	41520837.05	63187901.7	2494927.6	50224639.85		
	847364.0214	1755219.492	38983.24375	1024992.65		

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21696	9/26/2008	Test 15	55004510.80	2570327.84	162854.76	59218535.52

Can ID	1348					
No. 1 Port Ullage Hatch	2.66%	0.12%	0.01%	2.87%		
Raffinate	385031575.6	15421967.04	1302838.08	414529748.6		
	7857787.257	428387.9733	20356.845	8459790.789		

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21697	9/26/2008	Test 16	54693548.00	2574349.12	175110.32	58742689.88

Can ID	1431					
No. 3 Starboard Cargo Ullage Hatch	2.53%	0.12%	0.01%	2.72%		
Raffinate	382854836	15446094.72	1400882.56	411198829.2		
	7813364	429058.1867	21888.79	8391812.84		

carbon			7	6	8	7
SAMPNO	COLDATE	LOCCODE	2 Methylhexane	2 Methylpentane	3 Methylheptane	3 Methylhexane
AL21698	9/26/2008	Test 17	29996181.54	1575879.30	85603.32	32380104.30

Can ID	1347					
No. 3 Starboard High Level Alarm Tester	2.52%	0.13%	0.01%	2.72%		
Raffinate	209973270.8	9455275.8	684826.56	226660730.1		

#2 Starboard Cargo & Ullage Hatch	2.03%	0.00%	0.94%	0.00%
Naphtha but cleaned	36513238.14	18715.14	16955916.84	0
	1014256.615	4678.785	470997.69	0

carbon	6	2	6	4		
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21693	9/26/2008	Test 10	4756372.36	8085.14	2128701.86	13860.24

Can ID	1418			
No. 3 Starboard Cargo/Ullage Hatch	2.31%	0.00%	1.03%	0.01%
Naphtha but cleaned	28538234.16	16170.28	12772211.16	55440.96
	792728.7267	4042.57	354783.6433	3465.06

carbon	6	2	6	4		
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21694	9/26/2008	Test 11	7688968.65	13206.05	3098342.50	17269.45

Can ID	1394			
No. 2 Port Cargo Valve	2.21%	0.00%	0.89%	0.00%
Naphtha but cleaned	46133811.9	26412.1	18590055	69077.8
	1281494.775	6603.025	516390.4167	4317.3625

carbon	6	2	6	4		
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21696	9/26/2008	Test 15	265914049.40	0.00	307376366.32	79533.72

Can ID	1348			
No. 1 Port Ullage Hatch	12.88%	0.00%	14.89%	0.00%
Raffinate	1595484296	0	1844258198	318134.88
	44319008.23	0	51229394.39	19883.43

carbon	6	2	6	4		
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21697	9/26/2008	Test 16	272196484.56	0.00	326294202.64	95514.72

Can ID	1431			
No. 3 Starboard Cargo Ullage Hatch	12.60%	0.00%	15.10%	0.00%
Raffinate	1633178907	0	1957765216	382058.88
	45366080.76	0	54382367.11	23878.68

carbon	6	2	6	4		
SAMPNO	COLDATE	LOCCODE	3 Methylpentane	Acetylene	Benzene	cis 2 Butene
AL21698	9/26/2008	Test 17	153858997.50	11673.18	182281893.78	44098.68

Can ID	1347			
No. 3 Starboard High Level Alarm Tester	12.93%	0.00%	15.32%	0.00%
Raffinate	923153985	23346.36	1093691363	176394.72

#2 Starboard Cargo & Ullage Hatch	0.02%	0.26%	3.51%	0.54%
Naphtha but cleaned	244336.55	6971389.65	62939015.82	8021516.95
	9773.462	86066.53889	1748305.995	320860.678

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21693	9/26/2008	Test 10	18480.32	616780.68	7702828.38	1258971.80

Can ID	1418					
No. 3 Starboard Cargo/Ullage Hatch	0.01%	0.30%	3.74%	0.61%		
Naphtha but cleaned	92401.6	5551026.12	46216970.28	6294859		
	3696.064	68531.18667	1283804.73	251794.36		

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21694	9/26/2008	Test 11	23364.55	900043.10	20317.00	2052017.00

Can ID	1394					
No. 2 Port Cargo Valve	0.01%	0.26%	0.01%	0.59%		
Naphtha but cleaned	116822.75	8100387.9	121902	10260085		
	4672.91	100004.7889	3386.166667	410403.4		

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21696	9/26/2008	Test 15	565573.12	145180.60	1881035.60	86065584.56

Can ID	1348					
No. 1 Port Ullage Hatch	0.03%	0.01%	0.09%	4.17%		
Raffinate	2827865.6	1306625.4	11286213.6	430327922.8		
	113114.624	16131.17778	313505.9333	17213116.91		

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21697	9/26/2008	Test 16	662917.64	131901.28	1524824.28	91182445.20

Can ID	1431					
No. 3 Starboard Cargo Ullage Hatch	0.03%	0.01%	0.07%	4.22%		
Raffinate	3314588.2	1187111.52	9148945.68	455912226		
	132583.528	14655.69778	254137.38	18236489.04		

carbon			5	9	6	5
SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21698	9/26/2008	Test 17	319066.92	79118.22	918290.16	48793892.40

Can ID	1347					
No. 3 Starboard High Level Alarm Tester	0.03%	0.01%	0.08%	4.10%		
Raffinate	1595334.6	712063.98	5509740.96	243969462		

#2 Starboard Cargo & Ullage Hatch	0.47%	0.64%	0.00%	1.00%
Naphtha but cleaned	2796873.7	15238282.88	18715.14	11915305.8
	699218.425	238098.17	4678.785	744706.6125

carbon	2	8	2	4		
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21693	9/26/2008	Test 10	989852.14	1204685.86	8085.14	2134476.96

Can ID	1418			
No. 3 Starboard Cargo/Ullage Hatch	0.48%	0.59%	0.00%	1.04%
Naphtha but cleaned	1979704.28	9637486.88	16170.28	8537907.84
	494926.07	150585.7325	4042.57	533619.24

carbon	2	8	2	4		
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21694	9/26/2008	Test 11	1684279.30	1667009.85	15237.75	3850071.50

Can ID	1394			
No. 2 Port Cargo Valve	0.48%	0.48%	0.00%	1.11%
Naphtha but cleaned	3368558.6	13336078.8	30475.5	15400286
	842139.65	208376.2313	7618.875	962517.875

carbon	2	8	2	4		
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21696	9/26/2008	Test 15	284049.00	709491.28	12624.40	3298755.72

Can ID	1348			
No. 1 Port Ullage Hatch	0.01%	0.03%	0.00%	0.16%
Raffinate	568098	5675930.24	25248.8	13195022.88
	142024.5	88686.41	6312.2	824688.93

carbon	2	8	2	4		
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21697	9/26/2008	Test 16	261528.40	606063.64	12507.88	3879716.96

Can ID	1431			
No. 3 Starboard Cargo Ullage Hatch	0.01%	0.03%	0.00%	0.18%
Raffinate	523056.8	4848509.12	25015.76	15518867.84
	130764.2	75757.955	6253.94	969929.24

carbon	2	8	2	4		
SAMPNO	COLDATE	LOCCODE	Ethane	Ethylbenzene	Ethylene	Isobutane
AL21698	9/26/2008	Test 17	264592.08	415046.40	9079.14	1863817.74

Can ID	1347			
No. 3 Starboard High Level Alarm Tester	0.02%	0.03%	0.00%	0.16%
Raffinate	529184.16	3320371.2	18158.28	7455270.96

#2 Starboard Cargo & Ullage Hatch	3.93%	0.00%	3.88%	0.01%
Naphtha but cleaned	58734347.7	0	92968497.68	343110.9
	2349373.908	0	1452632.776	3431.109

carbon	5	5	8	10		
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21693	9/26/2008	Test 10	8956025.08	0.00	7649697.46	63526.10

Can ID	1418			
No. 3 Starboard Cargo/Ullage Hatch	4.35%	0.00%	3.72%	0.03%
Naphtha but cleaned	44780125.4	0	61197579.68	635261
	1791205.016	0	956212.1825	6352.61

carbon	5	5	8	10		
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21694	9/26/2008	Test 11	14954327.85	60951.00	7302945.65	50792.50

Can ID	1394			
No. 2 Port Cargo Valve	4.29%	0.02%	2.10%	0.01%
Naphtha but cleaned	74771639.25	304755	58423565.2	507925
	2990865.57	12190.2	912868.2063	5079.25

carbon	5	5	8	10		
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21696	9/26/2008	Test 15	175974036.48	326971.96	1892397.56	39135.64

Can ID	1348			
No. 1 Port Ullage Hatch	8.52%	0.02%	0.09%	0.00%
Raffinate	879870182.4	1634859.8	15139180.48	391356.4
	35194807.3	65394.392	236549.695	3913.564

carbon	5	5	8	10		
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21697	9/26/2008	Test 16	196534044.28	138723.76	2259377.96	37523.64

Can ID	1431			
No. 3 Starboard Cargo Ullage Hatch	9.09%	0.01%	0.10%	0.00%
Raffinate	982670221.4	693618.8	18075023.68	375236.4
	39306808.86	27744.752	282422.245	3752.364

carbon	5	5	8	10		
SAMPNO	COLDATE	LOCCODE	Isopentane	Isoprene	m/p Xylene	m Diethylbenzene
AL21698	9/26/2008	Test 17	101521646.46	267186.12	1370950.14	18158.28

Can ID	1347			
No. 3 Starboard High Level Alarm Tester	8.53%	0.02%	0.12%	0.00%
Raffinate	507608232.3	1335930.6	10967601.12	181582.8

#2 Starboard Cargo & Ullage Hatch	7.51%	3.33%	0.44%	2.74%
Naphtha but cleaned	157207176	59726250.12	11865398.76	32747336.08
	3208309.714	1659062.503	146486.4044	2046708.505

carbon	7	6	9	4		
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21693	9/26/2008	Test 10	14217141.18	7654317.54	1268211.96	5981848.58

Can ID	1418			
No. 3 Starboard Cargo/Ullage Hatch	6.91%	3.72%	0.62%	2.91%
Naphtha but cleaned	99519988.26	45925905.24	11413907.64	23927394.32
	2031020.169	1275719.59	140912.44	1495462.145

carbon	7	6	9	4		
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21694	9/26/2008	Test 11	25051876.85	12294832.55	1457744.75	10444969.70

Can ID	1394			
No. 2 Port Cargo Valve	7.19%	3.53%	0.42%	3.00%
Naphtha but cleaned	175363138	73768995.3	13119702.75	41779878.8
	3578839.55	2049138.758	161971.6389	2611242.425

carbon	7	6	9	4		
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21696	9/26/2008	Test 15	1262440.00	17339613.40	525175.04	17879937.72

Can ID	1348			
No. 1 Port Ullage Hatch	0.06%	0.84%	0.03%	0.87%
Raffinate	8837080	104037680.4	4726575.36	71519750.88
	180348.5714	2889935.567	58352.78222	4469984.43

carbon	7	6	9	4		
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21697	9/26/2008	Test 16	928994.36	17605409.64	619708.60	20627768.28

Can ID	1431			
No. 3 Starboard Cargo Ullage Hatch	0.04%	0.81%	0.03%	0.95%
Raffinate	6502960.52	105632457.8	5577377.4	82511073.12
	132713.48	2934234.94	68856.51111	5156942.07

carbon	7	6	9	4		
SAMPNO	COLDATE	LOCCODE	Methylcyclohexan	ethylcyclopentar	m Ethyltoluene	n Butane
AL21698	9/26/2008	Test 17	670559.34	10055796.06	246433.80	10214032.50

Can ID	1347			
No. 3 Starboard High Level Alarm Tester	0.06%	0.85%	0.02%	0.86%
Raffinate	4693915.38	60334776.36	2217904.2	40856130

#2 Starboard Cargo & Ullage Hatch	0.31%	4.08%	4.33%	1.85%
Naphtha but cleaned	9160021.3	85503236.28	77667831	49903920.81
	91600.213	1744964.006	2157439.75	616097.7878

carbon	10	7	6	9		
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21693	9/26/2008	Test 10	1209305.94	7600031.60	10001318.18	4257403.72
Can ID	1418					
No. 3 Starboard Cargo/Ullage Hatch	0.59%	3.69%	4.86%	2.07%		
Naphtha but cleaned	12093059.4	53200221.2	60007909.08	38316633.48		
	120930.594	1085718.8	1666886.363	473044.8578		

carbon	10	7	6	9		
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21694	9/26/2008	Test 11	1374445.05	13734292.00	15913290.25	6265762.80
Can ID	1394					
No. 2 Port Cargo Valve	0.39%	3.94%	4.57%	1.80%		
Naphtha but cleaned	13744450.5	96140044	95479741.5	56391865.2		
	137444.505	1962041.714	2652215.042	696195.8667		

carbon	10	7	6	9		
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21696	9/26/2008	Test 15	371157.36	21840212.00	251875716.60	763776.20
Can ID	1348					
No. 1 Port Ullage Hatch	0.02%	1.06%	12.20%	0.04%		
Raffinate	3711573.6	152881484	1511254300	6873985.8		
	37115.736	3120030.286	41979286.1	84864.02222		

carbon	10	7	6	9		
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21697	9/26/2008	Test 16	670877.20	21554488.48	256588924.48	518508.48
Can ID	1431					
No. 3 Starboard Cargo Ullage Hatch	0.03%	1.00%	11.87%	0.02%		
Raffinate	6708772	150881419.4	1539533547	4666576.32		
	67087.72	3079212.64	42764820.75	57612.05333		

carbon	10	7	6	9		
SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21698	9/26/2008	Test 17	291829.50	11540883.96	144961440.30	460442.10
Can ID	1347					
No. 3 Starboard High Level Alarm Tester	0.02%	0.97%	12.19%	0.04%		
Raffinate	2918295	80786187.72	869768641.8	4143978.9		



#2 Starboard Cargo & Ullage Hatch	4.85%	4.39%	0.18%	0.01%
Naphtha but cleaned	116117046.4	65705737.35	4800433.41	205866.54
	1814328.85	2628229.494	59264.61	1701.376364

carbon	8	5	9	11		
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21693	9/26/2008	Test 10	8179851.64	10151470.78	311855.40	55440.96

Can ID	1418			
No. 3 Starboard Cargo/Ullage Hatch	3.97%	4.93%	0.15%	0.03%
Naphtha but cleaned	65438813.12	50757353.9	2806698.6	609850.56
	1022481.455	2030294.156	34650.6	5040.087273

carbon	8	5	9	11		
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21694	9/26/2008	Test 11	738522.95	16837713.75	316945.20	34538.90

Can ID	1394			
No. 2 Port Cargo Valve	0.21%	4.83%	0.09%	0.01%
Naphtha but cleaned	5908183.6	84188568.75	2852506.8	379927.9
	92315.36875	3367542.75	35216.13333	3139.9

carbon	8	5	9	11		
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21696	9/26/2008	Test 15	715803.48	135420676.36	164117.20	35348.32

Can ID	1348			
No. 1 Port Ullage Hatch	0.03%	6.56%	0.01%	0.00%
Raffinate	5726427.84	677103381.8	1477054.8	388831.52
	89475.435	27084135.27	18235.24444	3213.483636

carbon	8	5	9	11		
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21697	9/26/2008	Test 16	276310.44	146285342.00	167150.76	79595.60

Can ID	1431			
No. 3 Starboard Cargo Ullage Hatch	0.01%	6.77%	0.01%	0.00%
Raffinate	2210483.52	731426710	1504356.84	875551.6
	34538.805	29257068.4	18572.30667	7235.963636

carbon	8	5	9	11		
SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21698	9/26/2008	Test 17	352789.44	77328332.40	47989.74	33722.52

Can ID	1347			
No. 3 Starboard High Level Alarm Tester	0.03%	6.50%	0.00%	0.00%
Raffinate	2822315.52	386641662	431907.66	370947.72

#2 Starboard Cargo & Ullage Hatch	1.32%	0.16%	0.01%	0.10%
Naphtha but cleaned	31516295.76	4229621.64	363905.5	2807271
	492442.1213	52217.55111	3639.055	34657.66667

carbon	8	9	10	9		
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21693	9/26/2008	Test 10	2276544.42	481643.34	24255.42	292220.06

Can ID	1418			
No. 3 Starboard Cargo/Ullage Hatch	1.11%	0.23%	0.01%	0.14%
Naphtha but cleaned	18212355.36	4334790.06	242554.2	2629980.54
	284568.0525	53515.92667	2425.542	32468.89556

carbon	8	9	10	9		
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21694	9/26/2008	Test 11	2749905.95	494718.95	40634.00	391102.25

Can ID	1394			
No. 2 Port Cargo Valve	0.79%	0.14%	0.01%	0.11%
Naphtha but cleaned	21999247.6	4452470.55	406340	3519920.25
	343738.2438	54968.77222	4063.4	43455.80556

carbon	8	9	10	9		
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21696	9/26/2008	Test 15	860984.08	189366.00	47972.72	61859.56

Can ID	1348			
No. 1 Port Ullage Hatch	0.04%	0.01%	0.00%	0.00%
Raffinate	6887872.64	1704294	479727.2	556736.04
	107623.01	21040.66667	4797.272	6873.284444

carbon	8	9	10	9		
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21697	9/26/2008	Test 16	718634.56	277447.52	50031.52	62539.40

Can ID	1431			
No. 3 Starboard Cargo Ullage Hatch	0.03%	0.01%	0.00%	0.00%
Raffinate	5749076.48	2497027.68	500315.2	562854.6
	89829.32	30827.50222	5003.152	6948.822222

carbon	8	9	10	9		
SAMPNO	COLDATE	LOCCODE	o Xylene	o Ethyltoluene	p Diethylbenzene	p Ethyltoluene
AL21698	9/26/2008	Test 17	499352.70	93385.44	20752.32	38910.60

Can ID	1347			
No. 3 Starboard High Level Alarm Tester	0.04%	0.01%	0.00%	0.00%
Raffinate	3994821.6	840468.96	207523.2	350195.4

#2 Starboard Cargo & Ullage Hatch	1.59%	0.01%	0.09%	2.75%
Naphtha but cleaned	14260936.68	56145.42	2087777.84	57628074.98
	1584548.52	6238.38	32621.52875	1176083.163

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21693	9/26/2008	Test 10	3389983.70	15015.26	179028.10	5057832.58

Can ID	1418					
No. 3 Starboard Cargo/Ullage Hatch	1.65%	0.01%	0.09%	2.46%		
Naphtha but cleaned	10169951.1	45045.78	1432224.8	35404828.06		
	1129994.567	5005.086667	22378.5125	722547.5114		

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21694	9/26/2008	Test 11	6391728.20	19301.15	298659.90	8020135.75

Can ID	1394					
No. 2 Port Cargo Valve	1.83%	0.01%	0.09%	2.30%		
Naphtha but cleaned	19175184.6	57903.45	2389279.2	56140950.25		
	2130576.067	6433.716667	37332.4875	1145733.679		

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21696	9/26/2008	Test 15	348433.44	0.00	65646.88	63500732.00

Can ID	1348					
No. 1 Port Ullage Hatch	0.02%	0.00%	0.00%	3.08%		
Raffinate	1045300.32	0	525175.04	444505124		
	116144.48	0	8205.86	9071533.143		

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21697	9/26/2008	Test 16	397978.00	0.00	36386.56	72829974.00

Can ID	1431					
No. 3 Starboard Cargo Ullage Hatch	0.02%	0.00%	0.00%	3.37%		
Raffinate	1193934	0	291092.48	509809818		
	132659.3333	0	4548.32	10404282		

carbon			3	3	8	7
SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21698	9/26/2008	Test 17	234760.62	0.00	42801.66	39489070.92

Can ID	1347					
No. 3 Starboard High Level Alarm Tester	0.02%	0.00%	0.00%	3.32%		
Raffinate	704281.86	0	342413.28	276423496.4		

#2 Starboard Cargo & Ullage Hatch	100.00%	0.01%	0.01%	33.32%
Naphtha but cleaned	1736775389	128926.52	103973	448573833.1
	55061185.28	8057.9075	4158.92	22151794.23

carbon		4	5	4.5		
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21693	9/26/2008	Test 10	205824564.00	33495.58	15015.26	64715770.60
Can ID	1418					
No. 3 Starboard Cargo/Ullage Hatch	100.00%	0.02%	0.01%	31.44%		
Naphtha but cleaned	1197420784	133982.32	75076.3	291220967.7		
	37841457.04	8373.895	3003.052	14381282.36		

carbon		4	5	4.5		
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21694	9/26/2008	Test 11	348334965.00	95489.90	34538.90	143515224.60
Can ID	1394					
No. 2 Port Cargo Valve	100.00%	0.03%	0.01%	41.20%		
Naphtha but cleaned	1929664978	381959.6	172694.5	645818510.7		
	66930177.85	23872.475	6907.78	31892272.13		

carbon		4	5	4.5		
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21696	9/26/2008	Test 15	2064846864.00	135081.08	1025101.28	95761123.76
Can ID	1348					
No. 1 Port Ullage Hatch	100.00%	0.01%	0.05%	4.64%		
Raffinate	12064660615	540324.32	5125506.4	430925056.9		
	358545192.4	33770.27	205020.256	21280249.72		

carbon		4	5	4.5		
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21697	9/26/2008	Test 16	2161134248.00	148957.48	1289448.72	97730888.92
Can ID	1431					
No. 3 Starboard Cargo Ullage Hatch	100.00%	0.01%	0.06%	4.52%		
Raffinate	12605114554	595829.92	6447243.6	439789000.1		
	376002141.9	37239.37	257889.744	21717975.32		

carbon		4	5	4.5		
SAMPNO	COLDATE	LOCCODE	Total NMOC	trans 2 Butene	trans 2 Pentene	unID
AL21698	9/26/2008	Test 17	1189626744.00	58365.90	591441.12	54225812.16
Can ID	1347					
No. 3 Starboard High Level Alarm Tester	100.00%	0.00%	0.05%	4.56%		
Raffinate	6950645874	233463.6	2957205.6	244016154.7		

#2 Starboard Cargo & Ullage Hatch  
Naphtha but cleaned

5.806082725 average C  
5.51% by volume

0.104475 moles/min  
8.701247 grams/min  
0.019166 lbs/min  
1.149944 lbs/hr  
0.013799 tons/day  
5.036757 tons/year

carbon

SAMPNO	COLDATE	LOCCODE
AL21693	9/26/2008	Test 10

Can ID 1418

No. 3 Starboard Cargo/Ullage Hatch  
Naphtha but cleaned

5.817676768 average C  
3.78% by volume

carbon

SAMPNO	COLDATE	LOCCODE
AL21694	9/26/2008	Test 11

Can ID 1394

No. 2 Port Cargo Valve  
Naphtha but cleaned

5.539682123 average C  
6.69% by volume

0.965023 scfm  
27.45442 liters/min  
0.075155 moles/min  
5.978964 grams/min  
0.01317 lbs/min  
0.790171 lbs/hr  
0.009482 tons/day  
3.460951 tons/year

carbon

SAMPNO	COLDATE	LOCCODE
AL21696	9/26/2008	Test 15

Can ID 1348

No. 1 Port Ullage Hatch  
Raffinate

5.842883957 average C  
35.85% by volume

carbon

SAMPNO	COLDATE	LOCCODE
AL21697	9/26/2008	Test 16

Can ID 1431

No. 3 Starboard Cargo Ullage Hatch  
Raffinate

5.832638377 average C  
37.60% by volume

carbon

SAMPNO	COLDATE	LOCCODE
AL21698	9/26/2008	Test 17

Can ID 1347

No. 3 Starboard High Level Alarm Tester  
Raffinate

5.842711513 average C

#2 Starboard Cargo & Ullage Hatch  
Naphtha but cleaned )

carbon

SAMPNO	COLDATE	LOCCODE
AL21693	9/26/2008	Test 10

Can ID 1418

No. 3 Starboard Cargo/Ullage Hatch  
Naphtha but cleaned

carbon

SAMPNO	COLDATE	LOCCODE
AL21694	9/26/2008	Test 11

Can ID 1394

No. 2 Port Cargo Valve  
Naphtha but cleaned )

carbon

SAMPNO	COLDATE	LOCCODE
AL21696	9/26/2008	Test 15

Can ID 1348

No. 1 Port Ullage Hatch  
Raffinate

carbon

SAMPNO	COLDATE	LOCCODE
AL21697	9/26/2008	Test 16

Can ID 1431

No. 3 Starboard Cargo Ullage Hatch  
Raffinate

carbon

SAMPNO	COLDATE	LOCCODE
AL21698	9/26/2008	Test 17

Can ID 1347

No. 3 Starboard High Level Alarm Tester  
Raffinate

ppbv 5764.533333 37037.12667

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21699	9/27/2008	Test 18	12:10	.02	470453.96	2419810.22

Can ID 1376

Vent Stack Area%ppbC 0.03% 0.14%

Gasoline ppbC\*#C 4234085.64 21778291.98

ppbv 52272.66222 268867.8022

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21700	9/27/2008	Test 19	12:50	.02	29240.50	1518166.76

Can ID 1482

Forward Cofferdam Area%ppbC 0.00% 0.09%

Gasoline ppbC\*#C 263164.5 13663500.84

ppbv 3248.944444 168685.1956

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21701	9/28/2008	Test 20	11:45	.02	445183.74	4991529.42

Can ID 1462

No. 2 Starboard Cargo Hatch Area%ppbC 0.02% 0.21%

Naphtha ppbC\*#C 4006653.66 44923764.78

ppbv 49464.86 554614.38

carbon 9 9

SAMPNO	COLDATE	LOCCODE	TART_HOU	DURATION	3 Trimethylbenz	4 Trimethylbenz
AL21702	9/28/2008	Test 22	14:50	.02	41264.78	2421271.65

Can ID 1359

Slop Tank PV Vent Area%ppbC 0.00% 0.05%

Unleaded Gasoline ppbC\*#C 371383.02 21791444.85

ppbv 4584.975556 269030.1833













63813.384 8790.913333 153048.36 9758778.48

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21699	9/27/2008	Test 18	46698377.98	400584.56	3219814.85	16002421.58
Can ID 1376						
Vent Stack			2.77%	0.02%	0.19%	0.95%
Gasoline			233491889.9	3605261.04	19318889.1	80012107.9
			9339675.596	44509.39556	536635.8083	3200484.316

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21700	9/27/2008	Test 19	20619230.98	202344.26	339189.80	5341654.54
Can ID 1482						
Forward Cofferdam			1.26%	0.01%	0.02%	0.33%
Gasoline			103096154.9	1821098.34	2035138.8	26708272.7
			4123846.196	22482.69556	56531.63333	1068330.908

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21701	9/28/2008	Test 20	4111110.18	1192545.27	14924847.06	38147769.81
Can ID 1462						
No. 2 Starboard Cargo Hatch			0.18%	0.05%	0.64%	1.63%
Naphtha			20555550.9	10732907.43	89549082.36	190738849.1
			822222.036	132505.03	2487474.51	7629553.962

carbon 5 9 6 5

SAMPNO	COLDATE	LOCCODE	cis 2 Pentene	Cumene	Cyclohexane	Cyclopentane
AL21702	9/28/2008	Test 22	25423959.16	259725.38	203896.56	36344561.82
Can ID 1359						
Slop Tank PV Vent			0.55%	0.01%	0.00%	0.79%
Unleaded Gasoline			127119795.8	2337528.42	1223379.36	181722809.1
			5084791.832	28858.37556	33982.76	7268912.364









29182.95 1648697.709 24160240.05 51160.23333

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21699	9/27/2008	Test 18	145561.25	7892913.22	25199563.60	565942.14
Can ID 1376						
Vent Stack			0.01%	0.47%	1.49%	0.03%
Gasoline			1455612.5	55250392.54	151197381.6	5093479.26
			14556.125	1127559.031	4199927.267	62882.46

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21700	9/27/2008	Test 19	180121.48	2355614.68	2381346.32	371939.16
Can ID 1482						
Forward Cofferdam			0.01%	0.14%	0.15%	0.02%
Gasoline			1801214.8	16489302.76	14288077.92	3347452.44
			18012.148	336516.3829	396891.0533	41326.57333

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21701	9/28/2008	Test 20	1993378.59	19777101.12	72479146.05	5005208.25
Can ID 1462						
No. 2 Starboard Cargo Hatch			0.09%	0.85%	3.10%	0.21%
Naphtha			19933785.9	138439707.8	434874876.3	45046874.25
			199337.859	2825300.16	12079857.68	556134.25

carbon 10 7 6 9

SAMPNO	COLDATE	LOCCODE	n Decane	n Heptane	n Hexane	n Nonane
AL21702	9/28/2008	Test 22	290067.13	8726287.30	68226459.05	868987.72
Can ID 1359						
Slop Tank PV Vent			0.01%	0.19%	1.48%	0.02%
Unleaded Gasoline			2900671.3	61084011.1	409358754.3	7820889.48
			29006.713	1246612.471	11371076.51	96554.19111

44098.68 15465666.48 5332.193333 3065.683636

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21699	9/27/2008	Test 18	349347.00	89663401.02	740615.64	36099.19
Can ID 1376						
Vent Stack			0.02%	5.31%	0.04%	0.00%
Gasoline			2794776	448317005.1	6665540.76	397091.09
			43668.375	17932680.2	82290.62667	3281.744545

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21700	9/27/2008	Test 19	153220.22	89502831.26	359073.34	140354.40
Can ID 1482						
Forward Cofferdam			0.01%	5.46%	0.02%	0.01%
Gasoline			1225761.76	447514156.3	3231660.06	1543898.4
			19152.5275	17900566.25	39897.03778	12759.49091

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21701	9/28/2008	Test 20	13933753.65	609388145.91	1784465.55	139275.36
Can ID 1462						
No. 2 Starboard Cargo Hatch			0.60%	26.10%	0.08%	0.01%
Naphtha			111470029.2	3046940730	16060189.95	1532028.96
			1741719.206	121877629.2	198273.95	12661.39636

carbon 8 5 9 11

SAMPNO	COLDATE	LOCCODE	n Octane	n Pentane	n Propylbenzene	n Undecane
AL21702	9/28/2008	Test 22	270648.41	514043860.15	526732.78	50974.14
Can ID 1359						
Slop Tank PV Vent			0.01%	11.18%	0.01%	0.00%
Unleaded Gasoline			2165187.28	2570219301	4740595.02	560715.54
			33831.05125	102808772	58525.86444	4634.012727



78253.54 0 5350.2075 5641295.846

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21699	9/27/2008	Test 18	73528227.58	309754.34	128093.90	37996144.21
Can ID 1376						
Vent Stack			4.36%	0.02%	0.01%	2.25%
Gasoline			220584682.7	929263.02	1024751.2	265973009.5
			24509409.19	103251.4467	16011.7375	5428020.601

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21700	9/27/2008	Test 19	86178771.22	381296.12	35088.60	19802836.22
Can ID 1482						
Forward Cofferdam			5.26%	0.02%	0.00%	1.21%
Gasoline			258536313.7	1143888.36	280708.8	138619853.5
			28726257.07	127098.7067	4386.075	2828976.603

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21701	9/28/2008	Test 20	21274311.24	855548.64	518552.01	14740804.62
Can ID 1462						
No. 2 Starboard Cargo Hatch			0.91%	0.04%	0.02%	0.63%
Naphtha			63822933.72	2566645.92	4148416.08	103185632.3
			7091437.08	285182.88	64819.00125	2105829.231

carbon 3 3 8 7

SAMPNO	COLDATE	LOCCODE	Propane	Propylene	Styrene	Toluene
AL21702	9/28/2008	Test 22	34621150.42	6389972.55	94666.26	22017187.47
Can ID 1359						
Slop Tank PV Vent			0.75%	0.14%	0.00%	0.48%
Unleaded Gasoline			103863451.3	19169917.65	757330.08	154120312.3
			11540383.47	2129990.85	11833.2825	3145312.496



20.66% by volume

carbon

SAMPNO	COLDATE	LOCCODE
AL21699	9/27/2008	Test 18

Can ID 1376

Vent Stack

Gasoline

4.830973506 average C

36.63% by volume

2.311047 scfm

65.74815 liters/min  
 0.985129 moles/min  
 68.59813 grams/min  
 0.151097 lbs/min  
 9.065832 lbs/hr  
 0.10879 tons/day  
 39.70834 tons/year

carbon

SAMPNO	COLDATE	LOCCODE
AL21700	9/27/2008	Test 19

Can ID 1482

Forward Cofferdam

Gasoline

4.560862475 average C

37.24% by volume

carbon

SAMPNO	COLDATE	LOCCODE
AL21701	9/28/2008	Test 20

Can ID 1462

No. 2 Starboard Cargo Hatch

Naphtha

5.132232813 average C

46.85% by volume

3.660502 scfm

104.1395 liters/min  
 1.995494 moles/min  
 147.3697 grams/min  
 0.324603 lbs/min  
 19.47618 lbs/hr  
 0.233714 tons/day  
 85.30565 tons/year

carbon

SAMPNO	COLDATE	LOCCODE
AL21702	9/28/2008	Test 22

Can ID 1359

Slop Tank PV Vent

Unleaded Gasoline

4.652611673 average C

101.65% by volume

3.493477 scfm

99.38769 liters/min  
 4.131913 moles/min  
 277.4024 grams/min  
 0.611019 lbs/min  
 36.66112 lbs/hr  
 0.439933 tons/day  
 160.5757 tons/year

carbon

SAMPNO	COLDATE	LOCCODE
AL21699	9/27/2008	Test 18

Can ID 1376

Vent Stack

Gasoline )

carbon

SAMPNO	COLDATE	LOCCODE
AL21700	9/27/2008	Test 19

Can ID 1482

Forward Cofferdam

Gasoline

carbon

SAMPNO	COLDATE	LOCCODE
AL21701	9/28/2008	Test 20

Can ID 1462

No. 2 Starboard Cargo Hatch

Naphtha )

carbon

SAMPNO	COLDATE	LOCCODE
AL21702	9/28/2008	Test 22

Can ID 1359

Slop Tank PV Vent

Unleaded Gasoline )

**GC/FID Daily Worksheet      FID 2**

Date 10/06/08  
 Batch # 192548

Operator SFC  
 QC # AL21990

**Working Gases and Quality Control Standards:**

Carrier Gas Helium Pressure 225      Pulse Gas Pressure 18  
 Combustion Air Pressure 90      Hydrogen Pressure 55  
 Nitrogen Pressure for dewar 22

ZAB Pressure 20; Preparation Date 9-8-08; Canister ID 9259  
 HAB Pressure 21; Preparation date 9-8-08; Canister ID 51503  
 LCS: Std ID 1576175; Preparation Date 9-9-08; Pressure 22; Canister ID 91083  
 PAMS: Std ID 250112; Preparation Date 9-8-08; Pressure 17; Canister ID 51364  
 SRM: Std ID 125077; Preparation Date 9-8-08; Pressure 18; Canister ID 91281

**Entech Setup:**

Name of Sequence: SQ100608  
 Sequence Saved? ✓      Sequence Printed? ✓  
 Leak Check Performed? ✓

**GC/FID Chemstation Setup:**

Name of Sequence: SQ100608  
 Sequence Saved? ✓      Sequence Printed? ✓  
 Bakeout.M Loaded at End? ✓

**Acquisition Startup:**

Do Both Sequences Match? ✓      Canister Valves Open? ✓  
 Entech Sequence Started? ✓      Chemstation Sequence Started? ✓

**Total Runs in the sequences:**

Number of Std: 4  
 Number of Blanks: 2  
 Number of Samples 13  
 Number of Duplicates: 1  
 Number of Sys Blanks: 0  
 Number of Cert Cans: 0  
 Total Runs in the sequences: 20

Date and Time Sequence Started: 10/6/08 12:40

Comments:



PAMS Analysis - FID2

10-06-08

Batch# 192548

Site/dasc Port Canister LIMS# Test Code# Datafile#

SRM	S1	G1083	ALZ1990	\$I - SRM	H5060801 ✓
PAMS	1	51321	↓		2 ✓
HAB	53	51503	↓		3 ✓
LCS	16	G1083	↓		4 ✓
ZAB	54	51259	↓		5 ✓

PRI	9/27/08	2	2350	ALZ1758	\$PPFID	6 ✓
		3	3075	9	↓	7 ✓
		4	6994	60		8 ✓
		5	8085	1		9 ✓
		6	7026	2		10 ✓
CAP	9-29-08	7	1627	ALZ1779		11 ✓
		8	1453	80		12 ✓
		9	1458	1		13 ✓
		10	0981	2		14 ✓
		11	1430	3		15 ✓
		12	8076	4		16 ✓
		13	T93178	5		17 ✓
		14	10017	6		18 ✓

- Repl.	2	2350	ALZ1758	\$D - PPFID	19 ✓
CCV	S1	G1083		\$C - SRM	20 ✓

Recheck 15 808 ALZ1154 \$PPFID 21 ✓  
 of prev. result. (CAP 18-21:00) sample run labeled 9/15/08 ALZ1171, and V. Verst. JC

Grab	4	51481	ALZ1640	\$PPFID	22 ✓
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CleanOut	53	51503	—	\$HBPPFID	23 -OK
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All files transferred 10/08/08



10-08 08

-----SEQUENCE TABLE-----

Sequence Name: C:\Smart\SQ100608.SEQ  
 Date: 10-06-2008  
 Time: 11:17:06  
 Int. Std Volume: 0 cc

Sample Name	Inlet #	Auto #	Samp Pos	Cal Vol.	Std Vol.	Method	Time
AL21990 \$I_SRM	1	1	1	0	200	C:\Smart\PAMS.MPT	12:00
AL21990 \$I_PPFID	1	1	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21990 \$HBPPFID	3	1	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21990 \$L1PPFID	1	16	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21990 \$B_PPFID	4	1	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21758 \$PPFID	1	2	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21759 \$PPFID	1	3	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21760 \$PPFID	1	4	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21761 \$PPFID	1	5	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21762 \$PPFID	1	6	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21779 \$PPFID	1	7	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21780 \$PPFID	1	8	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21781 \$PPF01	1	9	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21782 \$PPF02	1	10	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21783 \$PPF03	1	11	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21784 \$PPF03	1	12	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21785 \$PPF04	1	13	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21786 \$PPF05	1	14	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21758 \$D_PPFID	1	2	2	200	0	C:\Smart\PAMS.MPT	12:00
AL21990 \$C_SRM	1	1	1	0	200	C:\Smart\PAMS.MPT	12:00

*batch modified*

*- See Logbook copy*

*m*

*11/24/08*

Sequence Parameters:

Operator: JPC

Data File Naming: Prefix/Counter

Signal 1 Prefix: HJ0608

Counter: 01

Signal 2 Prefix: 0

Counter: 0000000

Data Directory: C:\HPCHEM\1\DATA\

Data Subdirectory:

Part of Methods to run: According to Runtime Checklist

Barcode Reader: not used

Shutdown Cmd/Macro: none

Sequence Comment:  
Running 5 PRI, 8 CAP.

Sequence Table (Front Injector):

Method and Injection Info Part:

Line	Location	SampleName	Method	Inj	SampleType	InjVolume	DataFile
1	Vial 1	AL21990 \$I_SRM	PAMS	1	Calib		
2	Vial 3	AL21990 \$I_PPFID	PAMS	1	Calib		
3	Vial 2	AL21990 \$HBPPFID	PAMS	1	Ctrl Samp		
4	Vial 4	AL21990 \$L1PPFID	PAMS	1	Ctrl Samp		
5	Vial 1	AL21990 \$B_PPFID	PAMS	1	Ctrl Samp		
6	Vial 2	AL21758 \$PPFID	PAMS	1	Sample		
7	Vial 3	AL21759 \$PPFID	PAMS	1	Sample		
8	Vial 4	AL21760 \$PPFID	PAMS	1	Sample		
9	Vial 5	AL21761 \$PPFID	PAMS	1	Sample		
10	Vial 6	AL21762 \$PPFID	PAMS	1	Sample		
11	Vial 7	AL21779 \$PPFID	PAMS	1	Sample		
12	Vial 8	AL21780 \$PPFID	PAMS	1	Sample		
13	Vial 9	AL21781 \$PPFID	PAMS	1	Sample		
14	Vial 10	AL21782 \$PPFID	PAMS	1	Sample		
15	Vial 11	AL21783 \$PPFID	PAMS	1	Sample		
16	Vial 12	AL21784 \$PPFID	PAMS	1	Sample		
17	Vial 13	AL21785 \$PPFID	PAMS	1	Sample		
18	Vial 14	AL21786 \$PPFID	PAMS	1	Sample		
19	Vial 2	AL21758 \$D_PPFID	PAMS	1	Sample		
20	Vial 1	AL21990 \$C_SRM	PAMS	1	Calib		
21	Vial 15	AL21154 \$PPFID	PAMS	1	Sample		
22	Vial 1	BAKEOUT	BAKEOUT	1	Sample		

*batch modified  
- see logbook copy*

Sequence Table (Back Injector):

No entries - empty table!

*m  
11/24/08*

----- Leak Check Report -----

10/6/2008 11:38:46 AM  
Leak Check for C:\Smart\SQ100608.SEQ  
Report File: C:\Smart\SQ100608.LCR  
Leak Check Method: Evacuation  
Pressurize/Evacuate time(sec) 30  
Equilibration time(sec) 10  
Maintanance time(sec) 30

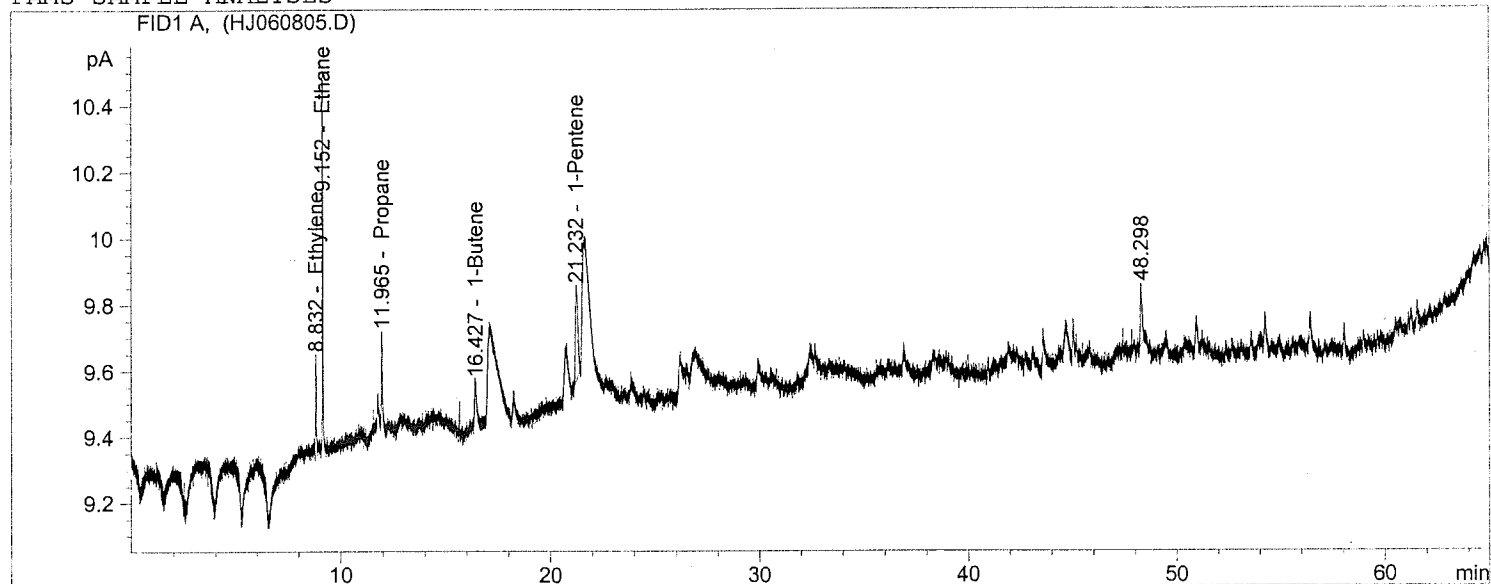
Sample	Inlet	Auto1	Auto2	Auto3	Start	End	Rate(psi/min)
1	1	---	---	0.5	0.6	0.20	
3	1	---	---	0.3	0.4	0.20	
1	16	---	---	0.4	0.4	0.00	
4	16	---	---	0.3	0.3	0.00	
1	2	---	---	0.4	0.4	0.00	
1	3	---	---	0.3	0.4	0.20	
1	4	---	---	0.3	0.3	0.00	
1	5	---	---	0.3	0.3	0.00	
1	6	---	---	0.3	0.3	0.00	
1	7	---	---	0.3	0.4	0.20	
1	8	---	---	0.3	0.4	0.20	
1	9	---	---	0.3	0.3	0.00	
1	10	---	---	0.3	0.4	0.20	
1	11	---	---	0.3	0.3	0.00	
1	12	---	---	0.3	0.3	0.00	
1	13	---	---	0.3	0.4	0.20	
1	14	---	---	0.3	0.4	0.20	

```

=====
Injection Date   : 10/6/2008 6:46:13 PM      Seq. Line   :    5
Sample Name     : AL21990 $B_PPFID          Location    : Vial 1
Acq. Operator  : JPC                       Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026          Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/8/2008 2:20:02 PM by JPC
                (modified after loading)
=====

```

## PAMS SAMPLE ANALYSES



```

=====
External Standard Report
=====

```

```

Sorted By      :      Signal
Calib. Data Modified : 10/7/2008 2:28:57 PM
Multiplier     :      0.5107
Dilution       :      1.0000
Sample Amount  :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs

```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.832	PBA	6.73536e-1	1.00000	3.43975e-1		Ethylene
8.950		-	-	-		Acetylene
9.152	PBA	2.60473	1.00000	1.33024		Ethane
11.762		-	-	-		Propylene
11.965	PBA	1.03681	1.00000	5.29498e-1		Propane
15.083		-	-	-		Isobutane
16.427	PB	8.12684e-1	1.00000	4.15038e-1		1-Butene
16.566		-	-	-		1,3-butadiene
16.751		-	-	-		n-Butane
17.433		-	-	-		t2-Butene
18.083		-	-	-		c2-Butene
20.238		-	-	-		Isopentane
21.232	PP	2.36850	1.00000	1.20959		1-Pentene
21.657		-	-	-		n-Pentane
21.797		-	-	-		Isoprene
22.050		-	-	-		t2-Pentene
22.387		-	-	-		c2-Pentene
23.432		-	-	-		2,2-Dimethylbutane
24.821		-	-	-		Cyclopentane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.901	-	-	-	-	-	2,3-dimethylbutane
25.385	-	-	-	-	-	2-Methylpentane
26.100	-	-	-	-	-	3-Methylpentane
26.351	-	-	-	-	-	1-Hexene
27.004	-	-	-	-	-	n-Hexane
28.659	-	-	-	-	-	Methylcyclopentane
28.825	-	-	-	-	-	2,4-dimethylpentane
30.256	-	-	-	-	-	Benzene
30.740	-	-	-	-	-	Cyclohexane
31.187	-	-	-	-	-	2-Methylhexane
31.320	-	-	-	-	-	2,3-Dimethylpentane
31.775	-	-	-	-	-	3-Methylhexane
32.601	-	-	-	-	-	2,2,4-Trimethylpentane
33.282	-	-	-	-	-	n-Heptane
34.752	-	-	-	-	-	Methylcyclohexane
36.580	-	-	-	-	-	2,3,4-Trimethylpentane
37.101	-	-	-	-	-	Toluene
37.524	-	-	-	-	-	2-Methylheptane
38.029	-	-	-	-	-	3-Methylheptane
39.666	-	-	-	-	-	n-Octane
43.059	-	-	-	-	-	Ethylbenzene
43.617	-	-	-	-	-	m/p-Xylene
44.781	-	-	-	-	-	Styrene
45.064	-	-	-	-	-	o-Xylene
45.851	-	-	-	-	-	n-Nonane
46.921	-	-	-	-	-	Cumene
48.671	-	-	-	-	-	n-Propylbenzene
49.070	-	-	-	-	-	m-Ethyltoluene
49.350	-	-	-	-	-	p-Ethyltoluene
49.565	-	-	-	-	-	1,3,5-Trimethylbenzene
50.165	-	-	-	-	-	o-Ethyltoluene
50.999	-	-	-	-	-	1,2,4-Trimethylbenzene
51.558	-	-	-	-	-	n-Decane
52.863	-	-	-	-	-	1,2,3-Trimethylbenzene
54.045	-	-	-	-	-	m-Diethylbenzene
54.417	-	-	-	-	-	p-Diethylbenzene
56.931	-	-	-	-	-	n-Undecane

Totals : 3.82834

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
48.298	PB	9.82796e-1	1.00000	5.01914e-1	?	

Uncalib. totals : 5.01914e-1

Results obtained with enhanced integrator!  
2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)  
Warning : Time reference compound(s) not found

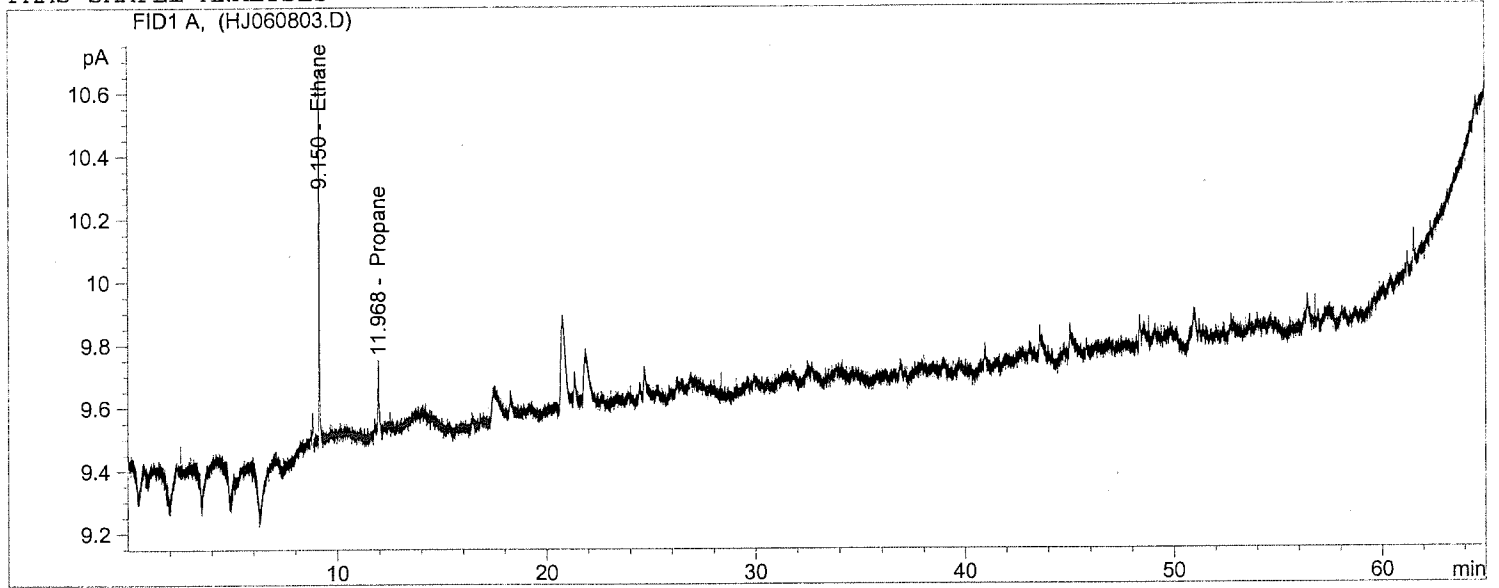
=====  
\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/6/2008 4:09:23 PM      Seq. Line   :    3
Sample Name     : AL21990 $HBPPFID          Location    : Vial 2
Acq. Operator  : JPC                        Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026          Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/8/2008 2:20:02 PM by JPC
                (modified after loading)
=====

```

PAMS SAMPLE ANALYSES



```

=====
External Standard Report
=====

```

```

Sorted By      :      Signal
Calib. Data Modified : 10/7/2008 2:28:57 PM
Multiplier    :      0.5107
Dilution      :      1.0000
Sample Amount  :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs

```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.837		-	-	-		Ethylene
8.950		-	-	-		Acetylene
9.150	BBA	2.82180	1.00000	1.44110		Ethane
11.762		-	-	-		Propylene
11.968	BBA	7.72749e-1	1.00000	3.94643e-1		Propane
15.083		-	-	-		Isobutane
16.411		-	-	-		1-Butene
16.566		-	-	-		1,3-butadiene
16.751		-	-	-		n-Butane
17.433		-	-	-		t2-Butene
18.083		-	-	-		c2-Butene
20.238		-	-	-		Isopentane
21.060		-	-	-		1-Pentene
21.657		-	-	-		n-Pentane
21.797		-	-	-		Isoprene
22.050		-	-	-		t2-Pentene
22.387		-	-	-		c2-Pentene
23.432		-	-	-		2,2-Dimethylbutane
24.821		-	-	-		Cyclopentane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.901	-	-	-	-	-	2,3-dimethylbutane
25.385	-	-	-	-	-	2-Methylpentane
26.100	-	-	-	-	-	3-Methylpentane
26.351	-	-	-	-	-	1-Hexene
27.004	-	-	-	-	-	n-Hexane
28.659	-	-	-	-	-	Methylcyclopentane
28.825	-	-	-	-	-	2,4-dimethylpentane
30.256	-	-	-	-	-	Benzene
30.740	-	-	-	-	-	Cyclohexane
31.187	-	-	-	-	-	2-Methylhexane
31.320	-	-	-	-	-	2,3-Dimethylpentane
31.775	-	-	-	-	-	3-Methylhexane
32.601	-	-	-	-	-	2,2,4-Trimethylpentane
33.282	-	-	-	-	-	n-Heptane
34.752	-	-	-	-	-	Methylcyclohexane
36.580	-	-	-	-	-	2,3,4-Trimethylpentane
37.101	-	-	-	-	-	Toluene
37.524	-	-	-	-	-	2-Methylheptane
38.029	-	-	-	-	-	3-Methylheptane
39.666	-	-	-	-	-	n-Octane
43.059	-	-	-	-	-	Ethylbenzene
43.617	-	-	-	-	-	m/p-Xylene
44.781	-	-	-	-	-	Styrene
45.064	-	-	-	-	-	o-Xylene
45.851	-	-	-	-	-	n-Nonane
46.921	-	-	-	-	-	Cumene
48.671	-	-	-	-	-	n-Propylbenzene
49.070	-	-	-	-	-	m-Ethyltoluene
49.350	-	-	-	-	-	p-Ethyltoluene
49.565	-	-	-	-	-	1,3,5-Trimethylbenzene
50.165	-	-	-	-	-	o-Ethyltoluene
50.999	-	-	-	-	-	1,2,4-Trimethylbenzene
51.558	-	-	-	-	-	n-Decane
52.863	-	-	-	-	-	1,2,3-Trimethylbenzene
54.045	-	-	-	-	-	m-Diethylbenzene
54.417	-	-	-	-	-	p-Diethylbenzene
56.931	-	-	-	-	-	n-Undecane

Totals : 1.83574

Uncalibrated Peaks : using compound Propane

Results obtained with enhanced integrator!

2 Warnings or Errors :

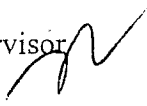
Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

=====  
\*\*\* End of Report \*\*\*



Date: 10/06/2008	Analyst: JPC	Batch: 192548	LIMS: AL21990
	%RECOVERY		
SRM concentration:	100.00		
SRM range:	90.00	110.00	
<b>\$I_SRM Result</b>	<b>Recovery %</b>	<b>In Range? (T/F)</b>	
100.36	100.36	TRUE	
<b>\$C_SRM Result</b>	<b>Recovery %</b>	<b>In Range? (T/F)</b>	
101.57	101.57	TRUE	
	<b>RESPONSE FACTORS</b>		
SRM concentration:	100.00		
SRM range (RF):	0.4594	0.5615	
<b>\$I_SRM area</b>	<b>Response Factor</b>	<b>In Range? (y/n)</b>	
196.52	0.5089	TRUE	
<b>\$C_SRM area</b>	<b>Response Factor</b>	<b>In Range? (y/n)</b>	
198.88	0.5028	TRUE	
RPD (I vs.C)	1.194		

From: Jianzhong Liu  
Environmental Scientist Supervisor  
Air Organics, LSD, DEQ 

Date: May 13, 2008

Re: FID SRM PREPARATION

Stock Standard:

Manufacturer:	Spectra Gases, Inc.
Cylinder #:	CC-162783
Certified Concentration:	1.18 ppm
Expiration Date:	2/25/2009

Working SRM:

Target Concentration:	100.00 ppbC
Flow Rate of the Stock Std:	40 cc/min
Flow Rate of Nitrogen:	1376 cc/min



3434 Route 22 West, Branchburg, New Jersey 08876 USA

ISO 9001:2000

SHIPPED FROM: 80 INDUSTRIAL DRIVE ALPHA, NJ. 08865

SHIPPED TO: Environmental Quality - LA  
Air Organics Lab, LDEQ  
1209 Leesville Road  
Baton Rouge, LA 70802

CERTIFICATE  
OF  
ANALYSIS

SGI ORDER # :	125072	CYLINDER # :	CC-162783
ITEM# :	1	CYLINDER PRES:	2000 psig
CERTIFICATION DATE:	02/25/2008	CYLINDER VALVE:	CGA 350
P.O.# :	CC - J Liu	PRODUCT EXPIRATION DATE:	02/25/2009
BLEND TYPE:	CERTIFIED		

ANALYTICAL ACCURACY: +/- 2%

COMPONENT	REQUESTED GAS CONC	ANALYSIS
Propane	1.20 ppm	1.18 ppm
Nitrogen	Balance	Balance

Received on 3/7/08  
opened on 3/7/08 m

NIST TRACEABLE

ANALYST: CP  
Cheryl Patino

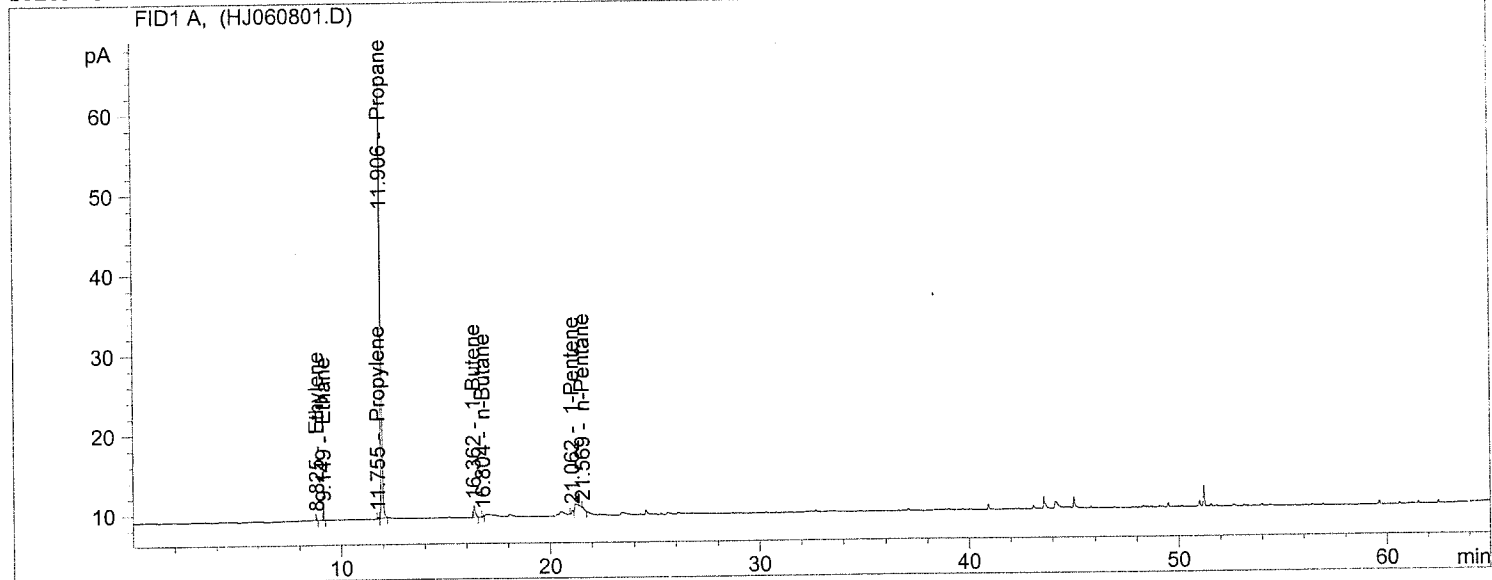
DATE: 02/25/2008

```

=====
Injection Date   : 10/6/2008 1:32:38 PM      Seq. Line   :    1
Sample Name     : AL21990 $I_SRM           Location    : Vial 1
Acq. Operator  : JPC                      Inj        :    1
Acq. Instrument : HP_FID2 SOP 1026        Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/8/2008 11:00:02 AM by JPC
                (modified after loading)
=====

```

## PAMS SAMPLE ANALYSES



```

=====
External Standard Report
=====

```

```

Sorted By      : Signal
Calib. Data Modified : 10/7/2008 2:28:57 PM
Multiplier    : 0.5107
Dilution      : 1.0000
Sample Amount  : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs

```

Signal 1: FID1 A,

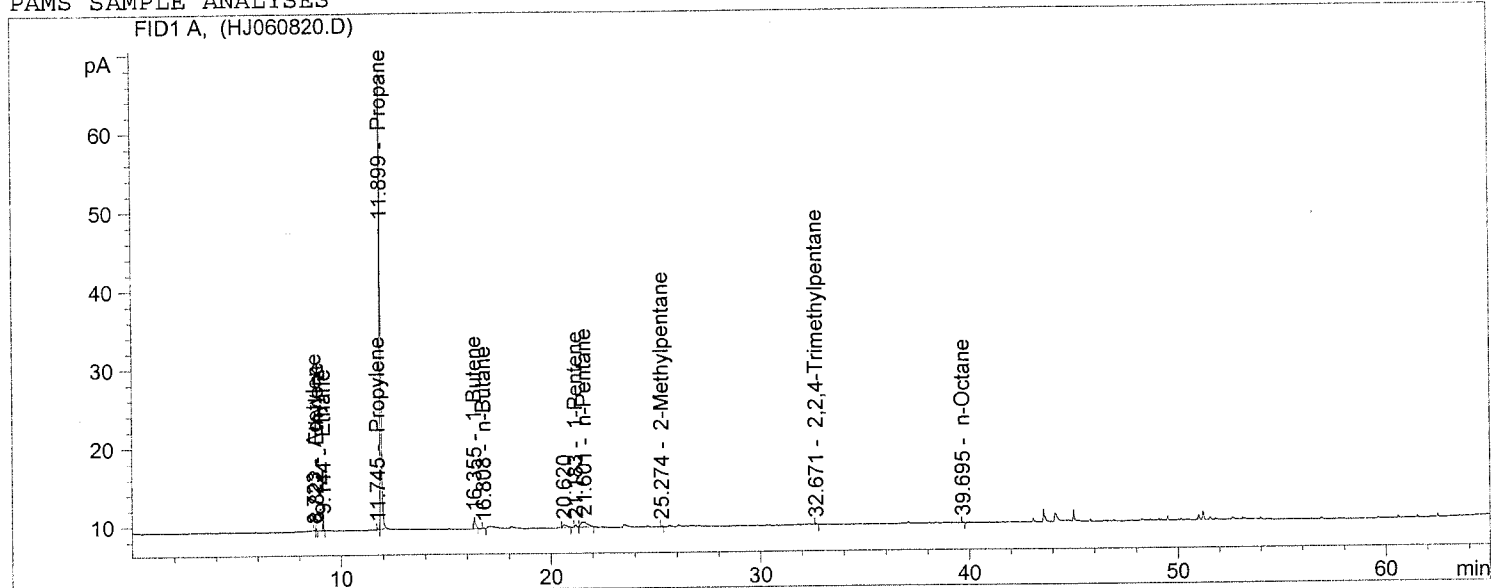
RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.825	PBA	7.49608e-1	1.00000	3.82825e-1		Ethylene
8.950		-	-	-		Acetylene
9.149	BBA	3.69022	1.00000	1.88459		Ethane
11.755	PB	9.80980e-1	1.00000	5.00987e-1		Propylene
11.906	BBA	196.51662	1.00000	100.36104		Propane
15.083		-	-	-		Isobutane
16.362	PB	8.18215	1.00000	4.17862		1-Butene
16.566		-	-	-		1,3-butadiene
16.804	PV	6.76274e-1	1.00000	3.45373e-1		n-Butane
17.433		-	-	-		t2-Butene
18.083		-	-	-		c2-Butene
20.238		-	-	-		Isopentane
21.062	PP	1.74923	1.00000	8.93330e-1		1-Pentene
21.569	PB	9.99140e-1	1.00000	5.10261e-1		n-Pentane
21.797		-	-	-		Isoprene
22.050		-	-	-		t2-Pentene
22.387		-	-	-		c2-Pentene
23.432		-	-	-		2,2-Dimethylbutane
24.821		-	-	-		Cyclopentane

```

=====
Injection Date   : 10/7/2008 3:52:46 PM      Seq. Line :   20
Sample Name     : AL21990 $C_SRM           Location  : Vial 1
Acq. Operator  : JPC                      Inj       :    1
Acq. Instrument : HP_FID2 SOP 1026        Inj Volume: Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/7/2008 11:39:44 AM by JPC
                (modified after loading)
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/8/2008 2:20:02 PM by JPC
                (modified after loading)
=====

```

## PAMS SAMPLE ANALYSES



```

=====
External Standard Report
=====

```

```

Sorted By           :      Signal
Calib. Data Modified :      10/7/2008 2:28:57 PM
Multiplier          :      0.5107
Dilution            :      1.0000
Sample Amount       :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs

```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.723	PB	3.48399e-1	1.00000	1.77928e-1		Acetylene
8.822	BBA	6.55641e-1	1.00000	3.34836e-1		Ethylene
9.144	PBA	3.15885	1.00000	1.61322		Ethane
11.745	PB	1.01210	1.00000	5.16881e-1		Propylene
11.899	BBA	198.87964	1.00000	101.56783		Propane
15.083		-	-	-		Isobutane
16.355	PB	7.84820	1.00000	4.00808		1-Butene
16.566		-	-	-		1,3-butadiene
16.808	PP	5.05109e-1	1.00000	2.57959e-1		n-Butane
17.433		-	-	-		t2-Butene
18.083		-	-	-		c2-Butene
20.238		-	-	-		Isopentane
21.183	PB	2.01423	1.00000	1.02866		1-Pentene
21.601	BB	14.17153	1.00000	7.23740		n-Pentane
21.797		-	-	-		Isoprene
22.050		-	-	-		t2-Pentene
22.387		-	-	-		c2-Pentene
23.432		-	-	-		2,2-Dimethylbutane

## Initial Calibration Verification (LCS) FID #2

DATE: 10/6/2008

QC NO: AL21990

BATCH NO: 192548

JPC

Prep'd 9/09/08

COMPONENTS	STD (ppbc)	\$I (ppbc)	REC% \$I
Ethylene	49.20	53.23	108.2
Actetylene	48.90	35.37	72.3
Ethane	48.90	54.92	112.3
Propylene	48.90	44.40	90.8
Propane	49.00	50.28	102.6
n-Butane	48.90		
Isobutane	48.90	50.95	104.2
1-Butene	49.90	50.21	100.6
1,3-Butadiene	48.80	41.06	84.1
n-Butane	48.90	59.31	121.3
t2-butene	48.90	51.02	104.3
c2-butene	48.90	47.95	98.1
Isopentane	49.40	55.93	113.2
1-Pentene	50.70	54.00	106.5
n-Pentane	49.10	52.82	107.6
Isoprene	49.40	49.63	100.5
t2-Pentene	50.30	52.86	105.1
c2-Pentene	49.50	49.00	99.0
2,2-Dimethylbutane	49.90	52.77	105.7
Cyclopentane	59.60	51.95	87.2
2,3-Dimethylbutane	49.50	54.71	110.5
2-Methylpentane	49.10	51.77	105.4
3-Methylpentane	49.50	52.61	106.3
1-Hexene	49.30	44.52	90.3
1-Hexane	49.70	50.49	101.6
Methylcyclopentane	49.10	51.22	104.3
2,4-Dimethylpentane	49.50	51.50	104.0
Benzene	49.30	49.81	101.0
Cyclohexane	48.50	52.22	107.7
2-Methylhexane	48.80	50.08	102.6
2,3-Dimethylpentane	48.60	53.43	109.9
3-Methylhexane	48.80	51.16	104.8
2,2,4-Trimethylpentane	53.70	58.66	109.2
n-Heptane	49.00	48.26	98.5
Methylcyclohexane	49.60	52.99	106.8
2,3,4-Trimethylpentane	48.90	51.59	105.5
Toluene	49.80	48.38	97.1
2-Methylheptane	49.10	51.15	104.2
3-Methylheptane	50.70	51.91	102.4
n-Octane	48.50	48.80	100.6
Ethylbenzne	49.70	48.49	97.6
m/p-Xylene	98.50	97.62	99.1
Styrene	49.30	41.26	83.7
o Xylene	49.00	50.09	102.2
n-Nonane	48.60	47.11	96.9
Cumene	49.40	49.56	100.3
n-Propylbenzene	49.00	46.25	94.4
m-Ethyltoluene	48.70	45.97	94.4
p-Ethyltoluene	48.10	44.88	93.3
1,3,5-Trimethylbenzene	48.70	48.88	100.4
o-Ethyltuene	48.50	47.51	98.0
1,2,4-trimethylbenzene	49.00	47.02	96.0
n-Decane	48.90	45.96	94.0
1,2,3-Trimethylbenzene	48.70	42.56	87.4
m-Diethylbenzene	48.40	41.86	86.5
p-Diethylbenzene	48.40	34.17	70.6
n-Undecane	48.90	41.34	84.5

From: Jianzhong Liu  
Environmental Scientist Supervisor  
Air Organics, LSD, DEQ

Date: June 3, 2008

Re: Low Recovery of p-Diethylbenzene in PAMS LCS Standard

Stock Standard:

Manufacturer:	Matheson Tri-Gas, Inc.
Cylinder #:	SX39238D
Lot#:	1057610175
Expiration Date:	12/03/2009

From the studies of runs in different GC/FIDs, the recovery of p-diethylbenzene is constantly low (~ 75%). However, the recovery of this compound in PAMS standard is normal (~100%). Therefore, 60% (75%\*80%) recovery for this compound in LCS is acceptable.

**Concentrations (ppbC) of Different Diluton of Matheson Stock Standard**

**Cylinder #: SX39238D; Lot #: 1057610175; Expiration Date: 12/3/2008**

COMPONENTS	Stock Std	10 times	71.425 times	166.65 times	250 times	500 times
Ethylene	492.00	49.20	6.89	2.95	1.97	0.98
Actetylene	489.00	48.90	6.85	2.93	1.96	0.98
Ethane	489.00	48.90	6.85	2.93	1.96	0.98
Propylene	489.00	48.90	6.85	2.93	1.96	0.98
Propane	490.00	49.00	6.86	2.94	1.96	0.98
n-Butane	489.00	48.90	6.85	2.93	1.96	0.98
Isobutane	489.00	48.90	6.85	2.93	1.96	0.98
1-Butene	499.00	49.90	6.99	2.99	2.00	1.00
1,3-Butadiene	488.00	48.80	6.83	2.93	1.95	0.98
n-Butane	489.00	48.90	6.85	2.93	1.96	0.98
t2-butene	489.00	48.90	6.85	2.93	1.96	0.98
c2-butene	489.00	48.90	6.85	2.93	1.96	0.98
Isopentane	494.00	49.40	6.92	2.96	1.98	0.99
1-Pentene	507.00	50.70	7.10	3.04	2.03	1.01
n-Pentane	491.00	49.10	6.87	2.95	1.96	0.98
Isoprene	494.00	49.40	6.92	2.96	1.98	0.99
t2-Pentene	503.00	50.30	7.04	3.02	2.01	1.01
c2-Pentene	495.00	49.50	6.93	2.97	1.98	0.99
2,2-Dimethylbutane	499.00	49.90	6.99	2.99	2.00	1.00
Cyclopentane	596.00	59.60	8.34	3.58	2.38	1.19
2,3-Dimethylbutane	495.00	49.50	6.93	2.97	1.98	0.99
2-Methylpentane	491.00	49.10	6.87	2.95	1.96	0.98
3-Methylpentane	495.00	49.50	6.93	2.97	1.98	0.99
1-Hexene	493.00	49.30	6.90	2.96	1.97	0.99
1-Hexane	497.00	49.70	6.96	2.98	1.99	0.99
Methylcyclopentane	491.00	49.10	6.87	2.95	1.96	0.98
2,4-Dimethylpentane	495.00	49.50	6.93	2.97	1.98	0.99
Benzene	493.00	49.30	6.90	2.96	1.97	0.99
Cyclohexane	485.00	48.50	6.79	2.91	1.94	0.97
2-Methylhexane	488.00	48.80	6.83	2.93	1.95	0.98
2,3-Dimethylpentane	486.00	48.60	6.80	2.92	1.94	0.97
3-Methylhexane	488.00	48.80	6.83	2.93	1.95	0.98
2,2,4-Trimethylpentane	537.00	53.70	7.52	3.22	2.15	1.07
n-Heptane	490.00	49.00	6.86	2.94	1.96	0.98
Methylcyclohexane	496.00	49.60	6.94	2.98	1.98	0.99
2,3,4-Trimethylpentane	489.00	48.90	6.85	2.93	1.96	0.98
Toluene	498.00	49.80	6.97	2.99	1.99	1.00
2-Methylheptane	491.00	49.10	6.87	2.95	1.96	0.98
3-Methylheptane	507.00	50.70	7.10	3.04	2.03	1.01
n-Octane	485.00	48.50	6.79	2.91	1.94	0.97
Ethylbenzne	497.00	49.70	6.96	2.98	1.99	0.99
m/p-Xylene	985.00	98.50	13.79	5.91	3.94	1.97
Styrene	493.00	49.30	6.90	2.96	1.97	0.99
o Xylene	490.00	49.00	6.86	2.94	1.96	0.98
n-Nonane	486.00	48.60	6.80	2.92	1.94	0.97
Cumene	494.00	49.40	6.92	2.96	1.98	0.99
n-Propylbenzene	490.00	49.00	6.86	2.94	1.96	0.98
m-Ethyltoluene	487.00	48.70	6.82	2.92	1.95	0.97
p-Ethyltoluene	481.00	48.10	6.73	2.89	1.92	0.96
1,3,5-Trimethylbenzene	487.00	48.70	6.82	2.92	1.95	0.97
o-Ethylouene	485.00	48.50	6.79	2.91	1.94	0.97
1,2,4-trimethylbenzene	490.00	49.00	6.86	2.94	1.96	0.98
n-Decane	489.00	48.90	6.85	2.93	1.96	0.98
1,2,3-Trimethylbenzene	487.00	48.70	6.82	2.92	1.95	0.97
m-Diethylbenzene	484.00	48.40	6.78	2.90	1.94	0.97
p-Diethylbenzene	484.00	48.40	6.78	2.90	1.94	0.97
n-Undecane	489.00	48.90	6.85	2.93	1.96	0.98





# MATHESON TRI-GAS

**Certified Mixture Grade**

**Matheson Tri-Gas**

6874 S Main Street

Morrow, GA 30260

Phone: (770) 961-7891

Fax: (770) 968-1268

To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd  
Baton Rouge, LA 70802

**TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE GREATER THAN PROCESS PRESSURE.**

Phone:  
Fax:

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057610175

**PRODUCT:**

CYLINDER NUMBER: SX39238D  
SIZE: 1L  
CGA/DISS OUTLET: 350  
CONTENT: 131 cu. ft.  
PRESSURE: 1850 psig

Fill Date: 12/3/2007  
Certification Date: 12/3/2007  
Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	500 ppbC	498 ppbC	+/- 5%
2-Methylheptane	500 ppbC	491 ppbC	+/- 5%
3-Methylheptane	500 ppbC	507 ppbC	+/- 5%
n-Octane	500 ppbC	485 ppbC	+/- 5%
Ethylbenzene	500 ppbC	497 ppbC	+/- 5%
p-Xylene	500 ppbC	490 ppbC	+/- 5%
m-Xylene	500 ppbC	495 ppbC	+/- 5%
Styrene	500 ppbC	493 ppbC	+/- 5%
o-Xylene	500 ppbC	490 ppbC	+/- 5%
n-Nonane	500 ppbC	486 ppbC	+/- 5%
Isopropylbenzene	500 ppbC	494 ppbC	+/- 5%
n-Propylbenzene	500 ppbC	490 ppbC	+/- 5%
n-Decane	500 ppbC	489 ppbC	+/- 5%
m-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
p-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
n-Dodecane	500 ppbC	492 ppbC	+/- 5%
m-Ethyltoluene	500 ppbC	487 ppbC	+/- 5%
o-Ethyltoluene	500 ppbC	485 ppbC	+/- 5%
p-Ethyltoluene	500 ppbC	481 ppbC	+/- 5%
n-Undecane	500 ppbC	489 ppbC	+/- 5%
1,2,3-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,3,5-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,2,4-Trimethylbenzene	500 ppbC	490 ppbC	+/- 5%
Nitrogen, Balance			

**SPECIAL INFORMATION / ADDITIONAL COMMENTS**

*Received on 12/16/07*

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

Derek Stuck  
ANALYST

12/4/2007  
DATE SIGNED



# MATHESON TRI-GAS

## Certified Mixture Grade

**Matheson Tri-Gas**

6874 S Main Street

Morrow, GA 30260

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Phone:  
Fax:

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057610175

### PRODUCT:

CYLINDER NUMBER: SX39238D  
SIZE: 11  
CGA/DISS OUTLET: 350  
CONTENT: 131 cu. ft.  
PRESSURE: 1850 psig

Fill Date: 12/3/2007  
Certification Date: 12/3/2007  
Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	500 ppbC	498 ppbC	+/- 5%
2-Methylheptane	500 ppbC	491 ppbC	+/- 5%
3-Methylheptane	500 ppbC	507 ppbC	+/- 5%
n-Octane	500 ppbC	485 ppbC	+/- 5%
Ethylbenzene	500 ppbC	497 ppbC	+/- 5%
p-Xylene	500 ppbC	490 ppbC	+/- 5%
m-Xylene	500 ppbC	495 ppbC	+/- 5%
Styrene	500 ppbC	493 ppbC	+/- 5%
o-Xylene	500 ppbC	490 ppbC	+/- 5%
n-Nonane	500 ppbC	486 ppbC	+/- 5%
Isopropylbenzene	500 ppbC	494 ppbC	+/- 5%
n-Propylbenzene	500 ppbC	490 ppbC	+/- 5%
n-Decane	500 ppbC	489 ppbC	+/- 5%
m-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
p-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
n-Dodecane	500 ppbC	492 ppbC	+/- 5%
m-Ethyltoluene	500 ppbC	487 ppbC	+/- 5%
o-Ethyltoluene	500 ppbC	485 ppbC	+/- 5%
p-Ethyltoluene	500 ppbC	481 ppbC	+/- 5%
n-Undecane	500 ppbC	489 ppbC	+/- 5%
1,2,3-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,3,5-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,2,4-Trimethylbenzene	500 ppbC	490 ppbC	+/- 5%
Nitrogen, Balance			

### SPECIAL INFORMATION / ADDITIONAL COMMENTS

*Received on 12/16/07*

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

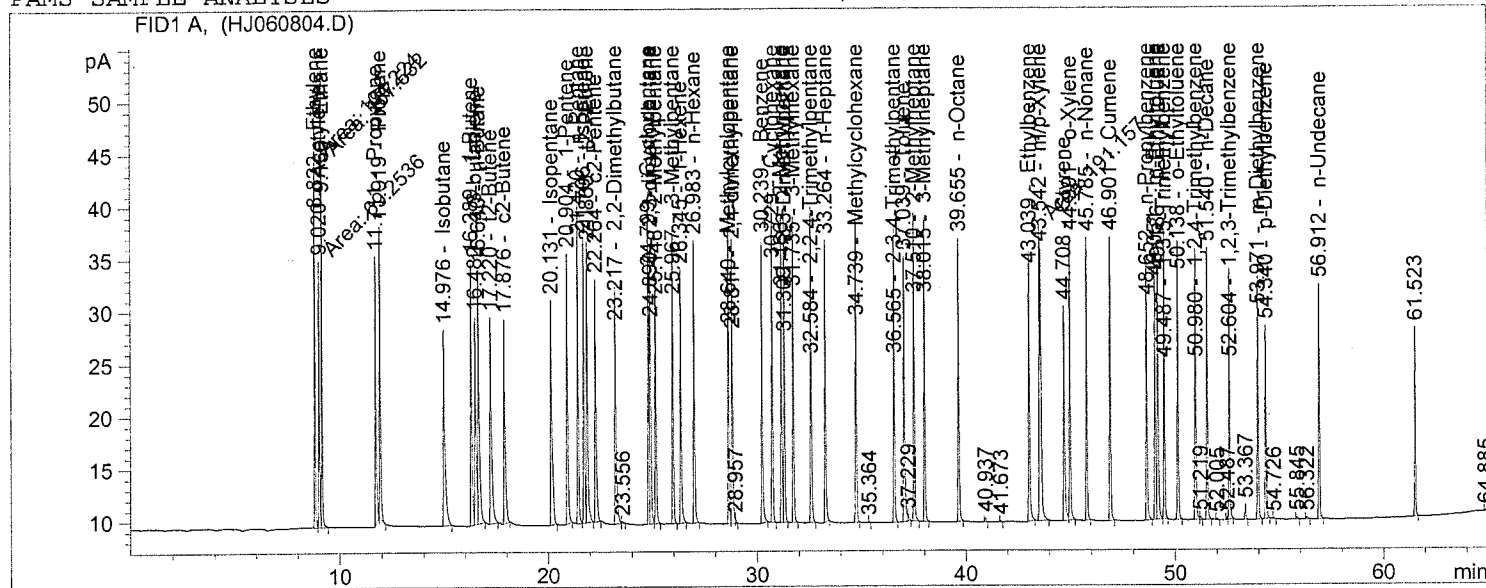
Derek Stuck  
ANALYST

*Derek Stuck*

12/4/2007  
DATE SIGNED

Injection Date : 10/6/2008 5:27:43 PM Seq. Line : 4
Sample Name : AL21990 \$L1PPFID Location : Vial 4
Acq. Operator : JPC Inj : 1
Acq. Instrument : HP\_FID2 SOP 1026 Inj Volume : Manually
Acq. Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed : 10/8/2008 2:27:02 PM by JPC
(modified after loading)

PAMS SAMPLE ANALYSES



External Standard Report

Sorted By : Signal
Calib. Data Modified : 10/8/2008 2:27:00 PM
Multiplier : 0.5107
Dilution : 1.0000
Sample Amount : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs

Signal 1: FID1 A,

Table with 6 columns: RetTime [min], Type, Area [pA\*s], Amt/Area, Amount [ppbc], Grp, Name. Lists various hydrocarbons and their corresponding retention times and areas.

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.890	VV	107.13717	1.00000	54.71495		2,3-dimethylbutane
25.148	VB	101.36118	1.00000	51.76515		2-Methylpentane
25.967	PB	103.01171	1.00000	52.60808		3-Methylpentane
26.345	BB	87.16730	1.00000	44.51634		1-Hexene
26.983	PB	98.86594	1.00000	50.49083		n-Hexane
28.640	BV	100.29522	1.00000	51.22077		Methylcyclopentane
28.811	VV	100.83565	1.00000	51.49677		2,4-dimethylpentane
30.239	PB +	97.53899	1.00000	49.81316		Benzene
30.729	PB	102.25732	1.00000	52.22282		Cyclohexane
31.166	BV	98.05479	1.00000	50.07658		2-Methylhexane
31.309	VB	104.61568	1.00000	53.42723		2,3-Dimethylpentane
31.735	BB	100.18056	1.00000	51.16221		3-Methylhexane
32.584	BB	114.87085	1.00000	58.66454		2,2,4-Trimethylpentane
33.264	PB	94.49777	1.00000	48.26001		n-Heptane
34.739	BB	103.76786	1.00000	52.99425		Methylcyclohexane
36.565	BB	101.02585	1.00000	51.59390		2,3,4-Trimethylpentane
37.039	BV +	94.72859	1.00000	48.37789		Toluene
37.510	BB	100.16042	1.00000	51.15192		2-Methylheptane
38.015	BB	101.65383	1.00000	51.91461		3-Methylheptane
39.655	BB	95.54650	1.00000	48.79560		n-Octane
43.039	BB	94.95210	1.00000	48.49204		Ethylbenzene
43.542	MM	191.15706	1.00000	97.62391		m/p-Xylene
44.708	BV	80.79482	1.00000	41.26192		Styrene
44.991	VB	98.08223	1.00000	50.09059		o-Xylene
45.785	BB	92.23728	1.00000	47.10558		n-Nonane
46.901	BB	97.04679	1.00000	49.56180		Cumene
48.652	BB	90.55850	1.00000	46.24823		n-Propylbenzene
49.051	PV	90.00822	1.00000	45.96720		m-Ethyltoluene
49.186	VV	87.88163	1.00000	44.88115		p-Ethyltoluene
49.487	VB	95.70393	1.00000	48.87600		1,3,5-Trimethylbenzene
50.138	VB	93.03803	1.00000	47.51452		o-Ethyltoluene
50.980	BB	92.07362	1.00000	47.02200		1,2,4-Trimethylbenzene
51.540	BB	89.99635	1.00000	45.96114		n-Decane
52.604	VB	83.34243	1.00000	42.56298		1,2,3-Trimethylbenzene
53.971	BB	81.96743	1.00000	41.86077		m-Diethylbenzene
54.340	BB	66.90073	1.00000	34.16620		p-Diethylbenzene
56.912	BB +	80.93950	1.00000	41.33580		n-Undecane

Totals : 2803.45860

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
23.556	BB	1.24691	1.00000	6.36796e-1	?	
28.957	VB	1.57230	1.00000	8.02974e-1	?	
35.364	BP	3.84897e-1	1.00000	1.96567e-1	?	
37.229	VB	2.65673	1.00000	1.35679	?	
40.937	BB	1.58487	1.00000	8.09393e-1	?	
41.673	PP	5.33042e-1	1.00000	2.72224e-1	?	
51.219	BB	1.39878	1.00000	7.14358e-1	?	
52.005	PB	6.07205e-1	1.00000	3.10099e-1	?	
52.487	PV	7.31412e-1	1.00000	3.73532e-1	?	
53.367	PB	5.23272	1.00000	2.67235	?	
54.726	BP	3.53976e-1	1.00000	1.80775e-1	?	
55.845	PP	1.01993	1.00000	5.20876e-1	?	
56.322	PB	1.10409	1.00000	5.63859e-1	?	
61.523	BB	53.39899	1.00000	27.27087	?	
64.885	PB	3.42649e-1	1.00000	1.74991e-1	?	

Uncalib. totals : 36.85645

Results obtained with enhanced integrator!

1 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

=====  
\*\*\* End of Report \*\*\*

PAMS RETENTION TIME STD FID #2 lot #1057410185

DATE: 10/6/2008

QC NO: AL21990

BATCH NO: 192548

COMPONENTS	STD (ppbc)	SI (ppbc)	REC% (SI)
Ethylene	21.00	22.94	109.2
Actetylene	42.00	11.16	26.6
Ethane	26.00	27.84	107.1
Propylene	26.00	19.11	73.5
Propane	40.00	40.26	100.6
n-Butane	43.00		
Isobutane	25.00	26.05	104.2
1-Butene	32.00	30.48	95.2
1,3-Butadiene	32.00	23.30	72.8
n-Butane	43.00	46.18	107.4
t2-butene	26.00	24.66	94.8
c2-butene	38.00	35.48	93.4
Isopentane	40.00	42.05	105.1
1-Pentene	25.00	24.17	96.7
n-Pentane	26.00	24.95	96.0
Isoprene	42.00	35.83	85.3
t2-Pentene	25.00	25.78	103.1
c2-Pentene	34.00	32.29	95.0
2,2-Dimethylbutane	40.00	42.64	106.6
Cyclopentane	21.00	19.84	94.5
2,3-Dimethylbutane	51.00	54.99	107.8
2-Methylpentane	21.00	21.84	104.0
3-Methylpentane	41.00	41.57	101.4
1-Hexene	61.00	57.10	93.6
1-Hexane	30.00	30.03	100.1
Methylcyclopentane	26.00	26.16	100.6
2,4-Dimethylpentane	40.00	40.34	100.8
Benzene	31.00	28.75	92.7
Cyclohexane	42.00	42.30	100.7
2-Methylhexane	25.00	24.48	97.9
2,3-Dimethylpentane	54.00	52.95	98.0
3-Methylhexane	26.00	25.09	96.5
2,2,4-Trimethylpentane	31.00	31.52	101.7
n-Heptane	26.00	24.10	92.7
Methylcyclohexane	31.00	31.03	100.1
2,3,4-Trimethylpentane	25.00	24.86	99.4
Toluene	40.00	36.01	90.0
2-Methylheptane	25.00	24.24	97.0
3-Methylheptane	25.00	24.82	99.3
n-Octane	31.00	28.01	90.4
Ethylbenzne	25.00	22.21	88.8
m/p-Xylene	42.00	35.72	85.0
Styrene	41.00	31.12	75.9
o Xylene	26.00	23.90	91.9
n-Nonane	25.00	22.68	90.7
Cumene	40.00	37.05	92.6
n-Propylbenzene	30.00	26.45	88.2
m-Ethyltoluene	25.00	22.79	91.2
p-Ethyltoluene	43.00	36.53	84.9
1,3,5-Trimethylbenzene	26.00	22.69	87.3
o-Ethylouene	27.00	31.10	115.2
1,2,4-trimethylbenzene	39.00	35.81	91.8
n-Decane	30.00	26.87	89.6
1,2,3-Trimethylbenzene	25.00	23.31	93.3
m-Diethylbenzene	40.00	35.58	88.9
p-Diethylbenzene	27.00	22.03	81.6
n-Undecane	41.00	24.55	59.9



# MATHESON TRI-GAS

## Certified Mixture Grade

*PAMS*  
Matheson Tri-Gas

6874 S Main Street

Morrow, GA 30260

Phone: (770) 961-7891

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To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd  
Baton Rouge, LA 70802

**TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE GREATER THAN PROCESS PRESSURE.**

Phone:  
Fax:

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057410185

### PRODUCT:

CYLINDER NUMBER: CC-250112

SIZE: 1l

CGA/DISS OUTLET: 350

CONTENT: 131 cu. ft.

PRESSURE: 1850 psig

Fill Date: 12/3/2007

Certification Date: 12/3/2007

Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Ethylene	20 ppbC	21 ppbC	+/- 5%
Ethane	25 ppbC	26 ppbC	+/- 5%
Acetylene	40 ppbC	42 ppbC	+/- 5%
Propylene	25 ppbC	26 ppbC	+/- 5%
Propane	40 ppbC	40 ppbC	+/- 5%
Isobutane	25 ppbC	25 ppbC	+/- 5%
1-Butene	30 ppbC	32 ppbC	+/- 5%
1,3-Butadiene	30 ppbC	32 ppbC	+/- 5%
n-Butane	40 ppbC	43 ppbC	+/- 5%
trans-2-Butene	25 ppbC	26 ppbC	+/- 5%
cis-2-Butene	35 ppbC	38 ppbC	+/- 5%
Isopentane	40 ppbC	40 ppbC	+/- 5%
1-Pentene	25 ppbC	25 ppbC	+/- 5%
n-Pentane	25 ppbC	26 ppbC	+/- 5%
Isoprene	40 ppbC	42 ppbC	+/- 5%
trans-2-Pentene	25 ppbC	25 ppbC	+/- 5%
cis-2-Pentene	35 ppbC	34 ppbC	+/- 5%
Cyclopentene	20 ppbC	21 ppbC	+/- 5%
2,2-Dimethylbutane	40 ppbC	40 ppbC	+/- 5%
2-Methylpentane	20 ppbC	21 ppbC	+/- 5%
3-Methylpentane	40 ppbC	41 ppbC	+/- 5%
2,3-Dimethylbutane	50 ppbC	51 ppbC	+/- 5%
1-Hexene	60 ppbC	61 ppbC	+/- 5%
n-Hexane	30 ppbC	30 ppbC	+/- 5%
Methylcyclopentane	25 ppbC	26 ppbC	+/- 5%
2,4-Dimethylpentane	40 ppbC	40 ppbC	+/- 5%
Benzene	30 ppbC	31 ppbC	+/- 5%
Cyclohexane	40 ppbC	42 ppbC	+/- 5%
2,3-Dimethylpentane	50 ppbC	54 ppbC	+/- 5%
2-Methylhexane	25 ppbC	25 ppbC	+/- 5%
3-Methylhexane	25 ppbC	26 ppbC	+/- 5%
n-Heptane	25 ppbC	26 ppbC	+/- 5%
2,2,4-Trimethylpentane	30 ppbC	31 ppbC	+/- 5%
Methylcyclohexane	30 ppbC	31 ppbC	+/- 5%
2,3,4-Trimethylpentane	25 ppbC	25 ppbC	+/- 5%

*Received on 12/1/07*

TRACEABLE TO REFERENCE STANDARD SOURCE/NUMBER:

TRACEABLE TO NIST TRACEABLE WEIGHT CERTIFICATE:



**MATHESON  
TRI-GAS**

**Certified Mixture Grade**

**Matheson Tri-Gas**

6874 S Main Street

Morrow, GA 30260

Phone: (770) 961-7891

Fax: (770) 968-1268

To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd

**TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE  
GREATER THAN PROCESS PRESSURE.**

Phone:  
Fax:

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057410185

**PRODUCT:**

CYLINDER NUMBER: CC-250112

SIZE: 1l

CGA/DISS OUTLET: 350

CONTENT: 131 liters

PRESSURE: 1850 psig

Fill Date: 12/3/2007

Certification Date: 12/3/2007

Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	40 ppbC	40 ppbC	+/- 5%
2-Methylheptane	25 ppbC	25 ppbC	+/- 5%
3-Methylheptane	25 ppbC	25 ppbC	+/- 5%
n-Octane	30 ppbC	31 ppbC	+/- 5%
Ethylbenzene	25 ppbC	25 ppbC	+/- 5%
p-Xylene	20 ppbC	21 ppbC	+/- 5%
m-Xylene	20 ppbC	21 ppbC	+/- 5%
Styrene	40 ppbC	41 ppbC	+/- 5%
o-Xylene	25 ppbC	26 ppbC	+/- 5%
n-Nonane	25 ppbC	25 ppbC	+/- 5%
Isopropylbenzene	40 ppbC	40 ppbC	+/- 5%
n-Propylbenzene	30 ppbC	30 ppbC	+/- 5%
n-Decane	30 ppbC	30 ppbC	+/- 5%
m-Diethylbenzene	40 ppbC	40 ppbC	+/- 5%
p-Diethylbenzene	25 ppbC	27 ppbC	+/- 5%
n-Dodecane	30 ppbC	31 ppbC	+/- 5%
m-Ethyltoluene	25 ppbC	25 ppbC	+/- 5%
o-Ethyltoluene	30 ppbC	27 ppbC	+/- 5%
p-Ethyltoluene	40 ppbC	43 ppbC	+/- 5%
n-Undecane	40 ppbC	41 ppbC	+/- 5%
1,2,3-Trimethylbenzene	25 ppbC	25 ppbC	+/- 5%
1,3,5-Trimethylbenzene	25 ppbC	26 ppbC	+/- 5%
1,2,4-Trimethylbenzene	40 ppbC	39 ppbC	+/- 5%
Nitrogen, Balance			

**SPECIAL INFORMATION / ADDITIONAL COMMENTS**

Received 12/6/07

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

Derek Stuck  
ANALYST

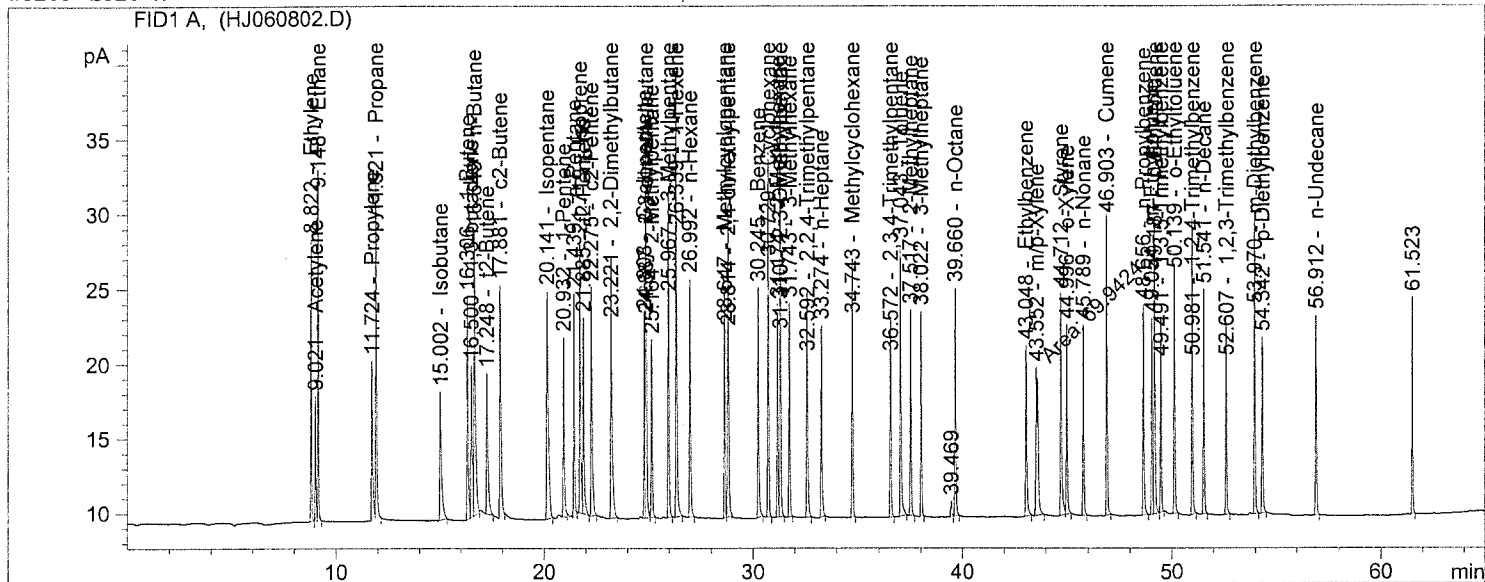
12/4/2007  
DATE SIGNED



```

=====
Injection Date   : 10/6/2008 2:50:58 PM           Seq. Line   :    2
Sample Name     : AL21990 $I_PPFID              Location    : Vial 3
Acq. Operator   : JPC                           Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026              Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/8/2008 2:18:27 PM by JPC
                  (modified after loading)
    
```

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By           :      Signal
Calib. Data Modified : 10/7/2008 2:28:57 PM
Multiplier          :      0.5107
Dilution            :      1.0000
Sample Amount       :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.822	BBA	44.92053	1.00000	22.94091		Ethylene
9.021	BB	21.85233	1.00000	11.15999		Acetylene
9.148	BBA	54.52073	1.00000	27.84374		Ethane
11.724	PB	37.41565	1.00000	19.10817		Propylene
11.921	BBA	78.83289	1.00000	40.25996		Propane
15.002	PB +	51.00570	1.00000	26.04861		Isobutane
16.306	PV	59.67336	1.00000	30.47518		1-Butene
16.500	VV	45.61602	1.00000	23.29610		1,3-butadiene
16.649	VV	90.43373	1.00000	46.18451		n-Butane
17.248	PB	48.28507	1.00000	24.65918		t2-Butene
17.881	PB	69.47704	1.00000	35.48192		c2-Butene
20.141	PB	82.33052	1.00000	42.04620		Isopentane
20.932	BV	47.33178	1.00000	24.17234		1-Pentene
21.439	VB	48.85149	1.00000	24.94846		n-Pentane
21.719	BV	70.16476	1.00000	35.83315		Isoprene
21.885	VB	50.48055	1.00000	25.78042		t2-Pentene
22.275	PB	63.22242	1.00000	32.28769		c2-Pentene
23.221	PB	83.49139	1.00000	42.63905		2,2-Dimethylbutane
24.808	BV	38.84512	1.00000	19.83820		Cyclopentane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.887	VV	107.66957	1.00000	54.98685		2,3-dimethylbutane
25.164	VB	42.76157	1.00000	21.83834		2-Methylpentane
25.967	PB	81.40124	1.00000	41.57161		3-Methylpentane
26.339	PB	111.81145	1.00000	57.10211		1-Hexene
26.992	BB	58.80105	1.00000	30.02970		n-Hexane
28.647	PV	51.22998	1.00000	26.16315		Methylcyclopentane
28.814	VB	78.98666	1.00000	40.33849		2,4-dimethylpentane
30.245	BB +	56.29302	1.00000	28.74885		Benzene
30.729	PB	82.83351	1.00000	42.30307		Cyclohexane
31.174	BV	47.93708	1.00000	24.48147		2-Methylhexane
31.310	VB	103.67268	1.00000	52.94564		2,3-Dimethylpentane
31.743	BB	49.13598	1.00000	25.09375		3-Methylhexane
32.592	BB	61.71513	1.00000	31.51791		2,2,4-Trimethylpentane
33.274	BB	47.18862	1.00000	24.09923		n-Heptane
34.743	BB	60.76443	1.00000	31.03239		Methylcyclohexane
36.572	BB	48.67302	1.00000	24.85731		2,3,4-Trimethylpentane
37.043	PB +	70.50365	1.00000	36.00622		Toluene
37.517	BB	47.46110	1.00000	24.23838		2-Methylheptane
38.022	BB	48.59916	1.00000	24.81959		3-Methylheptane
39.660	BB	54.85380	1.00000	28.01383		n-Octane
43.048	BB	43.48153	1.00000	22.20602		Ethylbenzene
43.552	MM	69.94241	1.00000	35.71959		m/p-Xylene
44.712	BV	60.93937	1.00000	31.12174		Styrene
44.996	VB	46.80718	1.00000	23.90443		o-Xylene
45.789	BB	44.40535	1.00000	22.67781		n-Nonane
46.903	BB	72.55196	1.00000	37.05229		Cumene
48.656	BB	51.79570	1.00000	26.45206		n-Propylbenzene
49.054	BV	44.63218	1.00000	22.79365		m-Ethyltoluene
49.187	VP	71.52545	1.00000	36.52805		p-Ethyltoluene
49.491	VB	44.43419	1.00000	22.69254		1,3,5-Trimethylbenzene
50.139	BB	60.89012	1.00000	31.09658		o-Ethyltoluene
50.981	BB	70.12561	1.00000	35.81315		1,2,4-Trimethylbenzene
51.541	BB	52.62347	1.00000	26.87481		n-Decane
52.607	BB	45.64962	1.00000	23.31326		1,2,3-Trimethylbenzene
53.970	BB	69.66376	1.00000	35.57728		m-Diethylbenzene
54.342	PB	43.14646	1.00000	22.03490		p-Diethylbenzene
56.912	BB +	48.08060	1.00000	24.55476		n-Undecane

Totals : 1705.60458

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
39.469	PP	3.90622	1.00000	1.99490	?	
61.523	BB	42.26542	1.00000	21.58495	?	

Uncalib. totals : 23.57986

Results obtained with enhanced integrator!  
1 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

=====  
\*\*\* End of Report \*\*\*

GC/FID Daily Worksheet FID 2

Date Oct. 9, 2008  
Batch # 192687(A)

Operator JPC/JMK  
QC # AL22195

Dup = AL21743  
(Part 5)

Working Gases and Quality Control Standards:

Carrier Gas Helium Pressure \_\_\_\_\_ Pulse Gas Pressure 15.0  
Combustion Air Pressure 80.0 Hydrogen Pressure 55.0  
Nitrogen Pressure for dewar 25.0

ZAB Pressure 29.5; Preparation Date 10-2-08; Canister ID GCR44  
HAB Pressure 29.0; Preparation date 10-6-08; Canister ID GCR29  
LCS: Std ID 10576175 Preparation Date 10-7-08; Pressure 29.5; Canister ID 51404  
PAMS: Std ID CC250112 Preparation Date 10-2-08; Pressure 30.5; Canister ID G1152  
SRM: Std ID CC162783; Preparation Date 10-2-08; Pressure 30.0; Canister ID G1124

Entech Setup:

Name of Sequence: 100908  
Sequence Saved? Y Sequence Printed? Y  
Leak Check Performed? Y

GC/FID Chemstation Setup:

Name of Sequence: 100908  
Sequence Saved? Y Sequence Printed? Y  
Bakeout.M Loaded at End? Y

Acquisition Startup:

Do Both Sequences Match? Y Canister Valves Open? Y  
Entech Sequence Started? Y Chemstation Sequence Started? Y

Total Runs in the sequences:

Number of Std: 3  
Number of Blanks: 2  
Number of Samples: 13  
Number of Duplicates: 2  
Number of Sys Blanks: -  
Number of Cert Cans: -  
Total Runs in the sequences: 20

Date and Time Sequence Started: 10-9-08 8:45AM

Comments: Re Boot: ?

Site/Desc	Run Date	Port#	Can ID #	LIMS#	Analysis Code #	Data File #
SRM	Oct. 9, 2008	S1	G1124	AL22195	PI-SRM	HJ090801 ✓
PAMS		1-1	G1152		PI-PPFID	2 ✓
HAB		33	GCR24		PI-BIPFID	3 ✓
LCS		16	S1404		PI-LIPFID	4 ✓
ZAB		S4	GCR44		PI-BIPFID	5 ✓

LSU	9-27-08	2	1002	AL 21711	8 PPFID	6 ✓
CARV	9-20-08	3	GCR42	712		7 ✓
CARV	9-21-08	4	CCR7	713		8 ✓
*CAP	9-26-08	5	G1241	743		9 ✓
CAP	9-27-08	6	G1049	744		10 ✓
BAKER	9-27-08	7	3323	763		11 ✓
SU	9-27-08	8	7025	764		12 ✓
PAL	9-27-08	9	S6416	765		13 ✓
CARV	9-26-08	10	1388	839		14 ✓
CARV	9-27-08	11	G1250	840		15 ✓
HAWK	9-27-08	12	G1028	850		16 ✓
CHAL High	9-21-08	13	G1219	862		17 ✓
CHAL VISA	9-21-08	14	G1215	864		18 ✓
Shr. Air	9-21-08	15	G1205	AL21897		19 ✓

Dup/CAP	9-26-08	5	G1241	AL 21743	PI-D-PPFID	20 ✓
CONT	10-9-08	S1	G1124	AL 22195	PI-C-SRM	21 ✓ TRANS

TRANSFERRED LIMS						
LHL	9-27-08	2	5727	AL 22411	PI-PPFID	22 ✓
Shr. Air	9-27-08	3	1467	AL 22413		23 ✓
23 GRAB	9-28-08	6	1491	AL 21703		24 ✓
14 GRAB	9-26-08	7	1356	AL 21655		25 ✓
12 GRAB	9-25-08	8	S1374	AL 21641		26 ✓

LCS/HAB	10-9-08	S3	GCR24	AL 22195	PI-HAPPFID	27 ✓
CONT	10-9-08	S1	G1124	AL 22195	PI-C-SRM	28 ✓

SIGNATURE READ AND UNDERSTOOD

JAK

DATE Oct. 9 20 08

----- Leak Check Report -----

10/9/2008 8:41:22 AM  
Leak Check for C:\Smart\SQ100908.SEQ  
Report File: C:\Smart\SQ100908.LCR  
Leak Check Method: Evacuation  
Pressurize/Evacuate time(sec) 30  
Equilibration time(sec) 10  
Maintanance time(sec) 30

Sample	Inlet	Auto1	Auto2	Auto3	Start	End	Rate(psi/min)
1	1	---	---	0.5	0.6	0.20	
3	1	---	---	0.3	0.3	0.00	
1	16	---	---	0.4	0.5	0.20	
4	16	---	---	0.2	0.3	0.20	
1	2	---	---	0.3	0.4	0.20	
1	3	---	---	0.3	0.3	0.00	
1	4	---	---	0.3	0.3	0.00	
1	5	---	---	0.2	0.3	0.20	
1	6	---	---	0.2	0.3	0.20	
1	7	---	---	0.2	0.3	0.20	
1	8	---	---	0.2	0.3	0.20	
1	9	---	---	0.3	0.3	0.00	
1	10	---	---	0.3	0.3	0.00	
1	11	---	---	0.3	0.3	0.00	
1	12	---	---	0.3	0.3	0.00	
1	13	---	---	0.3	0.3	0.00	
1	14	---	---	0.3	0.3	0.00	

-----SEQUENCE TABLE-----

Sequence Name: C:\Smart\SQ100908.SEQ  
 Date: 10-11-2008  
 Time: 08:02:23  
 Int. Std Volume: 0 cc

Sample Name	Inlet #	Auto #	Samp Pos	Cal Vol.	Std Vol.	Method	Time
AL22195 \$I_SRM	1	1	1	0	200	C:\Smart\PAMS.MPT	12:00
AL22195 \$I_PPFID	1	1	1	200	0	C:\Smart\PAMS.MPT	12:00
AL22195 \$HBPPFID	3	1	1	200	0	C:\Smart\PAMS.MPT	12:00
AL22195 \$L1PPFID	1	16	1	200	0	C:\Smart\PAMS.MPT	12:00
AL22195 \$B_PPFID	4	1	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21711 \$PPFID	1	2	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21712 \$PPFID	1	3	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21713 \$PPFID	1	4	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21743 \$PPFID	1	5	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21744 \$PPFID	1	6	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21763 \$PPFID	1	7	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21764 \$PPFID	1	8	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21765 \$PPFID	1	9	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21839 \$PPFID	1	10	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21840 \$PPFID	1	11	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21850 \$PPFID	1	12	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21862 \$PPFID	1	13	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21864 \$PPFID	1	14	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21897 \$PPFID	1	15	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21743 \$D_PPFID	1	5	1	200	0	C:\Smart\PAMS.MPT	12:00
AL22195 \$C_SRM	1	1	1	0	200	C:\Smart\PAMS.MPT	12:00
AL22411 \$PPFID	1	2	1	200	0	C:\Smart\PAMS.MPT	12:00
AL22413 \$PPFID	1	3	1	200	0	C:\Smart\PAMS.MPT	12:00
AL21703 \$PPFID	1	6	1	40	0	C:\Smart\PAMS.MPT	12:00
AL21695 \$PPFID	1	7	1	40	0	C:\Smart\PAMS.MPT	12:00
AL21641 \$PPFID	1	8	1	40	0	C:\Smart\PAMS.MPT	12:00
CLEANUP \$HBPPFID	3	1	1	200	0	C:\Smart\PAMS.MPT	12:00
AL22195 \$C_SRM	1	1	1	0	200	C:\Smart\PAMS.MPT	12:00

Sequence Parameters:

Operator: JPC

Data File Naming: Prefix/Counter

Signal 1 Prefix: HJ0908

Counter: 01

Signal 2 Prefix: 0

Counter: 0000000

Data Directory: C:\HPCHEM\1\DATA\  
 Data Subdirectory:

Part of Methods to run: According to Runtime Checklist

Barcode Reader: not used

Shutdown Cmd/Macro: none

Sequence Comment:  
 11 SINGLES!

Sequence Table (Front Injector):

Method and Injection Info Part:

Line	Location	SampleName	Method	Inj	SampleType	InjVolume	DataFile
====	=====	=====	=====	===	=====	=====	=====
1	Vial 1	AL22195 \$I_SRM	PAMS	1	Calib		
2	Vial 3	AL22195 \$I_PPFID	PAMS	1	Calib		
3	Vial 2	AL22195 \$HBPPFID	PAMS	1	Ctrl Samp		
4	Vial 4	AL22195 \$L1PPFID	PAMS	1	Ctrl Samp		
5	Vial 1	AL22195 \$B_PPFID	PAMS	1	Ctrl Samp		
6	Vial 2	AL21711 \$PPFID	PAMS	1	Sample		
7	Vial 3	AL21712 \$PPFID	PAMS	1	Sample		
8	Vial 4	AL21713 \$PPFID	PAMS	1	Sample		
9	Vial 5	AL21743 \$PPFID	PAMS	1	Sample		
10	Vial 6	AL21744 \$PPFID	PAMS	1	Sample		
11	Vial 7	AL21763 \$PPFID	PAMS	1	Sample		
12	Vial 8	AL21764 \$PPFID	PAMS	1	Sample		
13	Vial 9	AL21765 \$PPFID	PAMS	1	Sample		
14	Vial 10	AL21839 \$PPFID	PAMS	1	Sample		
15	Vial 11	AL21840 \$PPFID	PAMS	1	Sample		
16	Vial 12	AL21850 \$PPFID	PAMS	1	Sample		
17	Vial 13	AL21862 \$PPFID	PAMS	1	Sample		
18	Vial 14	AL21864 \$PPFID	PAMS	1	Sample		
19	Vial 15	AL21897 \$PPFID	PAMS	1	Sample		
20	Vial 5	AL21743 \$D_PPFID	PAMS	1	Sample		
21	Vial 1	AL22195 \$C_SRM	PAMS	1	Calib		
22	Vial 2	AL22411 \$PPFID	PAMS	1	Sample		
23	Vial 3	AL22413 \$PPFID	PAMS	1	Sample		
24	Vial 6	AL21703 \$PPFID	PAMS	1	Sample		
25	Vial 7	AL21695 \$PPFID	PAMS	1	Sample		
26	Vial 8	AL21641 \$PPFID	PAMS	1	Sample		
27	Vial 2	CLEANUP \$HBPPFID	PAMS	1	Ctrl Samp		
28	Vial 1	AL22195 \$C_SRM	PAMS	1	Calib		
29	Vial 1	BAKEOUT	BAKEOUT	1	Sample		

Sequence Table (Back Injector):

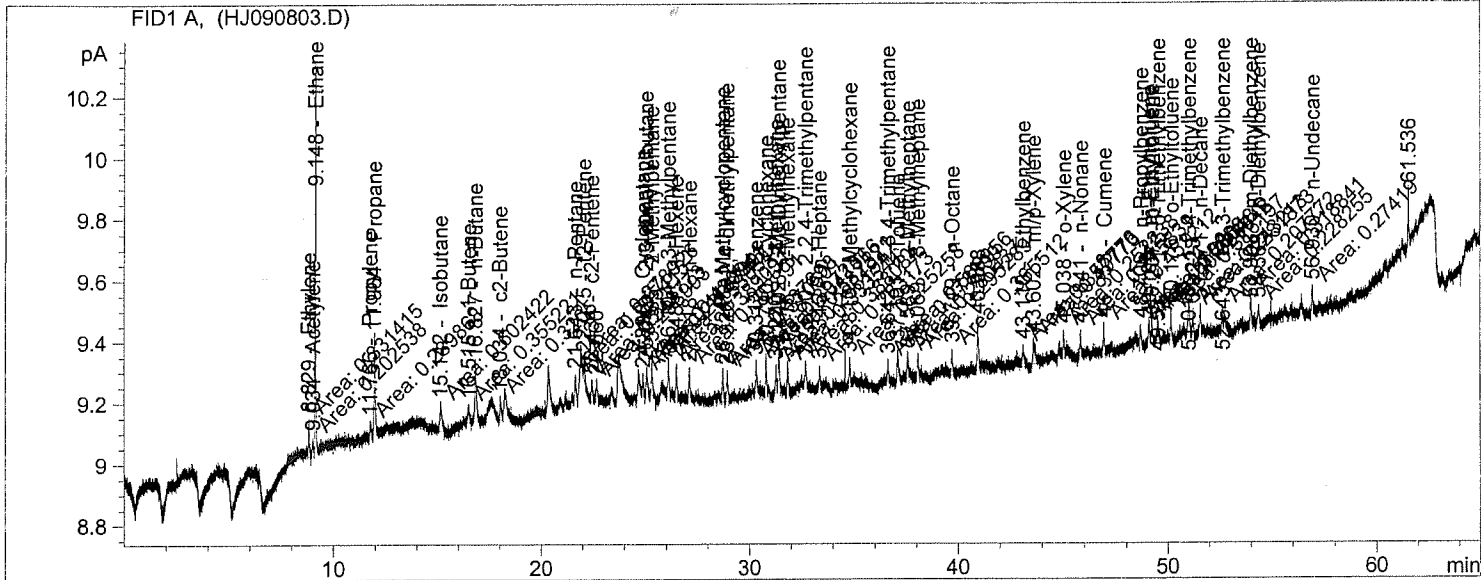
No entries - empty table!

```

=====
Injection Date : 10/9/2008 11:43:01 AM      Seq. Line :    3
Sample Name    : AL22195 $HBPPFID           Location  : Vial 2
Acq. Operator  : JPC                        Inj       :    1
Acq. Instrument: HP FID2 SOP 1026          Inj Volume: Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method: C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/9/2008 12:15:17 PM by JPC
                (modified after loading)
    
```

PAMS SAMPLE ANALYSES

*GCR24*



External Standard Report

```

Sorted By          :      Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier         :      0.5107
Dilution           :      1.0000
Sample Amount      :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.829	MM	3.31415e-1	1.00000	1.69254e-1		Ethylene
9.034	MM	2.02538e-1	1.00000	1.03436e-1		Acetylene
9.148	PBA	2.93498	1.00000	1.49889		Ethane
11.766	MM	2.89868e-1	1.00000	1.48036e-1		Propylene
11.964	PBA	1.20321	1.00000	6.14482e-1		Propane
15.142	MM +	6.02422e-1	1.00000	3.07657e-1		Isobutane
16.515	MM	3.55221e-1	1.00000	1.81412e-1		1-Butene
16.613		-	-	-		1,3-butadiene
16.827	BB	8.54704e-1	1.00000	4.36497e-1		n-Butane
17.473		-	-	-		t2-Butene
18.034	MM	3.20500e-1	1.00000	1.63679e-1		c2-Butene
20.256		-	-	-		Isopentane
21.072		-	-	-		1-Pentene
21.643	MM	2.95415e-1	1.00000	1.50868e-1		n-Pentane
21.803		-	-	-		Isoprene
22.075	MM T	2.78926e-1	1.00000	1.42447e-1		t2-Pentene
22.434	MM T	2.43773e-1	1.00000	1.24495e-1		c2-Pentene
23.425		-	-	-		2,2-Dimethylbutane
24.890	MM T	2.30574e-1	1.00000	1.17754e-1		Cyclopentane

*10-9-08  
JPC*



RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.049	MM T	4.43899e-1	1.00000	2.26699e-1		2,3-dimethylbutane
25.305	MM T	4.30941e-1	1.00000	2.20081e-1		2-Methylpentane
26.104	MM T	5.30541e-1	1.00000	2.70947e-1		3-Methylpentane
26.481	MM T	3.89091e-1	1.00000	1.98709e-1		1-Hexene
27.118	MM T	3.02891e-1	1.00000	1.54686e-1		n-Hexane
28.721	MM T	4.37898e-1	1.00000	2.23635e-1		Methylcyclopentane
28.926	MM T	3.70501e-1	1.00000	1.89215e-1		2,4-dimethylpentane
30.312	MM T+	3.97231e-1	1.00000	2.02866e-1		Benzene
30.790	MM T	3.41066e-1	1.00000	1.74182e-1		Cyclohexane
31.270	MF T	2.96194e-1	1.00000	1.51266e-1		2-Methylhexane
31.402	FM T	5.82521e-1	1.00000	2.97493e-1		2,3-Dimethylpentane
31.816	MM T	3.33544e-1	1.00000	1.70341e-1		3-Methylhexane
32.690	MM T	3.88084e-1	1.00000	1.98195e-1		2,2,4-Trimethylpentane
33.345	MM T	2.83173e-1	1.00000	1.44617e-1		n-Heptane
34.810	MM	3.25258e-1	1.00000	1.66109e-1		Methylcyclohexane
36.642	MM	2.78899e-1	1.00000	1.42434e-1		2,3,4-Trimethylpentane
37.101	MM +	5.69956e-1	1.00000	2.91077e-1		Toluene
37.589	MM	2.80437e-1	1.00000	1.43219e-1		2-Methylheptane
38.069	MM	2.95289e-1	1.00000	1.50804e-1		3-Methylheptane
39.719	MM	3.65512e-1	1.00000	1.86667e-1		n-Octane
43.110	MM	3.57776e-1	1.00000	1.82716e-1		Ethylbenzene
43.602	MM	4.97730e-1	1.00000	2.54191e-1		m/p-Xylene
44.781		-	-	-		Styrene
45.038	MM	2.52238e-1	1.00000	1.28818e-1		o-Xylene
45.841	MM	2.75839e-1	1.00000	1.40871e-1		n-Nonane
46.953	MM	4.53212e-1	1.00000	2.31455e-1		Cumene
48.706	MM	1.88630e-1	1.00000	9.63335e-2		n-Propylbenzene
49.109	MM	1.90640e-1	1.00000	9.73597e-2		m-Ethyltoluene
49.237	MM	2.80481e-1	1.00000	1.43242e-1		p-Ethyltoluene
49.532	MM	3.27042e-1	1.00000	1.67021e-1		1,3,5-Trimethylbenzene
50.176	MM	3.16197e-1	1.00000	1.61482e-1		o-Ethyltoluene
51.018	BB	5.35016e-1	1.00000	2.73233e-1		1,2,4-Trimethylbenzene
51.571	MM	2.81873e-1	1.00000	1.43953e-1		n-Decane
52.643	MM	2.07772e-1	1.00000	1.06109e-1		1,2,3-Trimethylbenzene
53.998	MM	3.18841e-1	1.00000	1.62832e-1		m-Diethylbenzene
54.365	MM	2.28255e-1	1.00000	1.16570e-1		p-Diethylbenzene
56.930	MM +	2.74190e-1	1.00000	1.40029e-1		n-Undecane

Totals : 10.60837

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
22.660	MM T	2.98993e-1	1.00000	1.52696e-1	?	
40.958	PP	7.15209e-1	1.00000	3.65257e-1	?	
51.223	MM	2.43213e-1	1.00000	1.24209e-1	?	
61.536	PB	5.76165e-1	1.00000	2.94248e-1	?	

Uncalib. totals : 9.36409e-1

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

Warning : Calibrated compound(s) not found

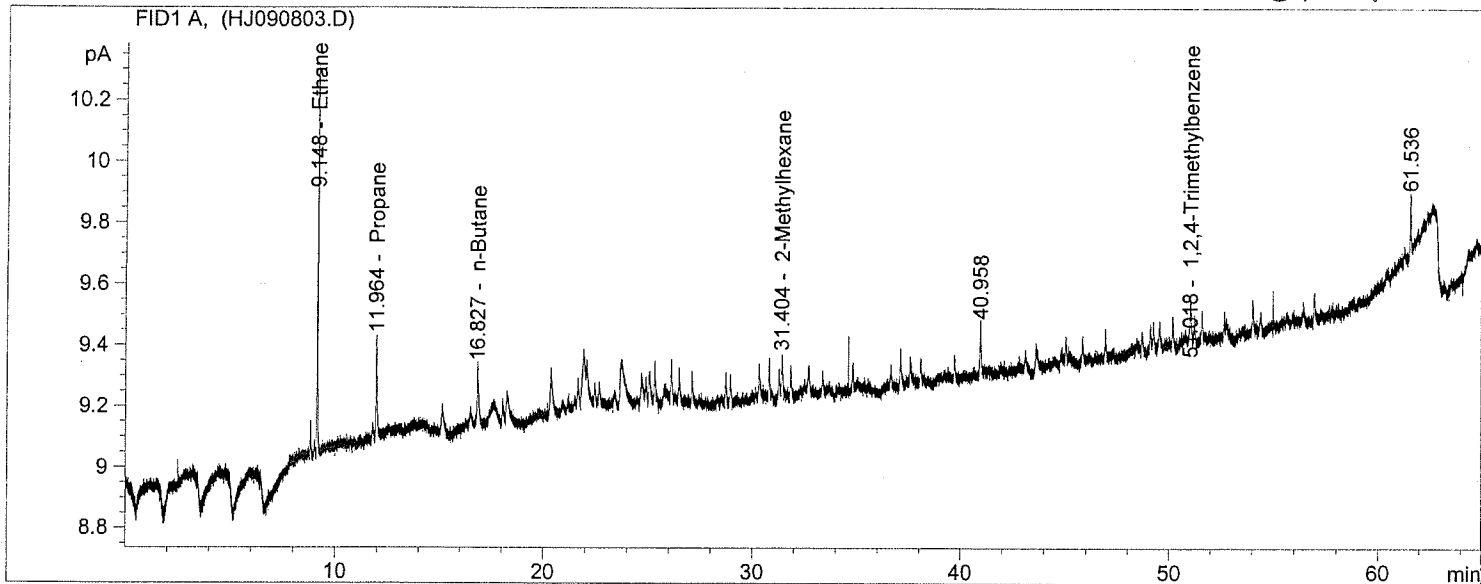
\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/9/2008 11:43:01 AM      Seq. Line   :    3
Sample Name     : AL22195 $HBPPFID           Location    : Vial 2
Acq. Operator   : JPC                       Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026           Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/9/2008 12:15:17 PM by JPC
                  (modified after loading)
=====

```

## PAMS SAMPLE ANALYSES



```

=====
External Standard Report
=====

```

```

Sorted By           :      Signal
Calib. Data Modified :      8/4/2008 10:57:02 AM
Multiplier          :      0.5107
Dilution             :      1.0000
Sample Amount        :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs

```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.837	-	-	-	-	-	Ethylene
8.950	-	-	-	-	-	Acetylene
9.148	PBA	2.93498	1.00000	1.49889	-	Ethane
11.762	-	-	-	-	-	Propylene
11.964	PBA	1.20321	1.00000	6.14482e-1	-	Propane
15.083	-	-	-	-	-	Isobutane
16.411	-	-	-	-	-	1-Butene
16.566	-	-	-	-	-	1,3-butadiene
16.827	BB	8.54704e-1	1.00000	4.36497e-1	-	n-Butane
17.433	-	-	-	-	-	t2-Butene
18.083	-	-	-	-	-	c2-Butene
20.238	-	-	-	-	-	Isopentane
21.060	-	-	-	-	-	1-Pentene
21.657	-	-	-	-	-	n-Pentane
21.797	-	-	-	-	-	Isoprene
22.050	-	-	-	-	-	t2-Pentene
22.420	-	-	-	-	-	c2-Pentene
23.432	-	-	-	-	-	2,2-Dimethylbutane
24.903	-	-	-	-	-	Cyclopentane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.101		-	-	-		2,3-dimethylbutane
25.385		-	-	-		2-Methylpentane
26.200		-	-	-		3-Methylpentane
26.576		-	-	-		1-Hexene
27.237		-	-	-		n-Hexane
28.764		-	-	-		Methylcyclopentane
28.914		-	-	-		2,4-dimethylpentane
30.373		-	-	-		Benzene
31.008		-	-	-		Cyclohexane
31.404	BP	5.13805e-1	1.00000	2.62400e-1		2-Methylhexane
31.584		-	-	-		2,3-Dimethylpentane
32.010		-	-	-		3-Methylhexane
32.869		-	-	-		2,2,4-Trimethylpentane
33.543		-	-	-		n-Heptane
35.039		-	-	-		Methylcyclohexane
36.868		-	-	-		2,3,4-Trimethylpentane
37.101		-	-	-		Toluene
37.806		-	-	-		2-Methylheptane
38.313		-	-	-		3-Methylheptane
39.949		-	-	-		n-Octane
43.059		-	-	-		Ethylbenzene
43.617		-	-	-		m/p-Xylene
44.781		-	-	-		Styrene
45.064		-	-	-		o-Xylene
45.851		-	-	-		n-Nonane
46.921		-	-	-		Cumene
48.671		-	-	-		n-Propylbenzene
49.070		-	-	-		m-Ethyltoluene
49.350		-	-	-		p-Ethyltoluene
49.565		-	-	-		1,3,5-Trimethylbenzene
50.165		-	-	-		o-Ethyltoluene
51.018	BB	5.35016e-1	1.00000	2.73233e-1		1,2,4-Trimethylbenzene
51.558		-	-	-		n-Decane
52.863		-	-	-		1,2,3-Trimethylbenzene
54.045		-	-	-		m-Diethylbenzene
54.417		-	-	-		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 3.08551

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
40.958	PP	7.15209e-1	1.00000	3.65257e-1	?	
61.536	PB	5.76165e-1	1.00000	2.94248e-1	?	

Uncalib. totals : 6.59505e-1

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

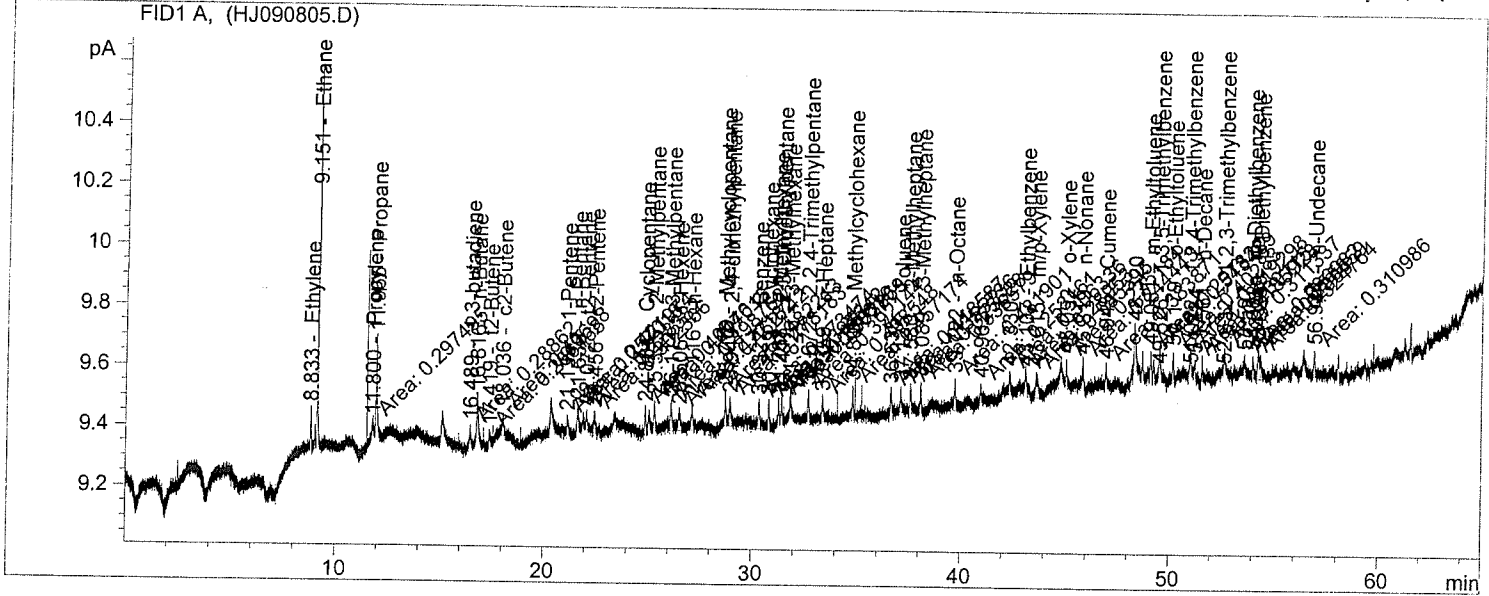
=====  
\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/9/2008 2:22:03 PM      Seq. Line   :    5
Sample Name     : AL22195 $B_PPFID          Location    : Vial 1
Acq. Operator   : JPC                       Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026          Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/9/2008 2:20:47 PM by JPC
                  (modified after loading)
    
```

ECR44

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By           :      Signal
Calib. Data Modified : 10/9/2008 2:20:52 PM
Multiplier          :      0.5107
Dilution            :      1.0000
Sample Amount       :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.833	BBA	3.01725e-1	1.00000	1.54091e-1		Ethylene
9.001		-	-	-		Acetylene
9.151	BBA	3.08258	1.00000	1.57427		Ethane
11.800	MM	2.97495e-1	1.00000	1.51931e-1		Propylene
11.965	PBA	1.18665	1.00000	6.06020e-1		Propane
15.083		-	-	-		Isobutane
16.386		-	-	-		1-Butene
16.489	MM	2.88620e-1	1.00000	1.47398e-1		1,3-butadiene
16.816	BB	6.86147e-1	1.00000	3.50415e-1		n-Butane
17.419	MM	2.66165e-1	1.00000	1.35931e-1		t2-Butene
18.036	MM	4.06980e-1	1.00000	2.07844e-1		c2-Butene
20.207		-	-	-		Isopentane
21.139	MM	2.57018e-1	1.00000	1.31259e-1		1-Pentene
21.639	MM	4.21974e-1	1.00000	2.15502e-1		n-Pentane
21.764		-	-	-		Isoprene
22.072	MM	2.28382e-1	1.00000	1.16635e-1		t2-Pentene
22.456	MM	3.02366e-1	1.00000	1.54418e-1		c2-Pentene
23.396		-	-	-		2,2-Dimethylbutane
24.884	MM	4.00460e-1	1.00000	2.04515e-1		Cyclopentane

10-10-08  
JPC

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.063		-	-	-		2,3-dimethylbutane
25.325	MM	4.17015e-1	1.00000	2.12970e-1		2-Methylpentane
26.114	MM	4.98762e-1	1.00000	2.54718e-1		3-Methylpentane
26.506	MM	4.72182e-1	1.00000	2.41143e-1		1-Hexene
27.116	MM	4.62742e-1	1.00000	2.36323e-1		n-Hexane
28.716	MM	4.82213e-1	1.00000	2.46266e-1		Methylcyclopentane
28.949	MM	4.78183e-1	1.00000	2.44208e-1		2,4-dimethylpentane
30.327	MM +	4.73474e-1	1.00000	2.41803e-1		Benzene
30.789	MM	3.97342e-1	1.00000	2.02923e-1		Cyclohexane
31.268	MM	1.99819e-1	1.00000	1.02048e-1		2-Methylhexane
31.417	MM	3.13386e-1	1.00000	1.60046e-1		2,3-Dimethylpentane
31.826	MM	3.02259e-1	1.00000	1.54364e-1		3-Methylhexane
32.672	MM	3.92144e-1	1.00000	2.00268e-1		2,2,4-Trimethylpentane
33.359	MM	4.08548e-1	1.00000	2.08646e-1		n-Heptane
34.806	MM	4.57174e-1	1.00000	2.33479e-1		Methylcyclohexane
36.889		-	-	-		2,3,4-Trimethylpentane
37.125	MM +	3.55736e-1	1.00000	1.81675e-1		Toluene
37.580	MM	3.25628e-1	1.00000	1.66298e-1		2-Methylheptane
38.089	MM	3.36579e-1	1.00000	1.71891e-1		3-Methylheptane
39.722	MM	4.81901e-1	1.00000	2.46107e-1		n-Octane
43.107	MM	2.89530e-1	1.00000	1.47863e-1		Ethylbenzene
43.615	MM	5.85595e-1	1.00000	2.99063e-1		m/p-Xylene
44.793		-	-	-		Styrene
45.052	MM	2.75184e-1	1.00000	1.40537e-1		o-Xylene
45.819	MM	2.44443e-1	1.00000	1.24837e-1		n-Nonane
46.945	MM	3.83871e-1	1.00000	1.96043e-1		Cumene
48.677		-	-	-		n-Propylbenzene
49.081	MM	2.97822e-1	1.00000	1.52098e-1		m-Ethyltoluene
49.355		-	-	-		p-Ethyltoluene
49.526	MM	5.43489e-1	1.00000	2.77560e-1		1,3,5-Trimethylbenzene
50.179	MM	4.02830e-1	1.00000	2.05725e-1		o-Ethyltoluene
51.022	MM	3.19298e-1	1.00000	1.63066e-1		1,2,4-Trimethylbenzene
51.561	MM	1.85928e-1	1.00000	9.49537e-2		n-Decane
52.632	MM	3.11337e-1	1.00000	1.59000e-1		1,2,3-Trimethylbenzene
54.002	MM	2.35900e-1	1.00000	1.20474e-1		m-Diethylbenzene
54.357	FM	3.24764e-1	1.00000	1.65857e-1		p-Diethylbenzene
56.924	MM +	3.10986e-1	1.00000	1.58820e-1		n-Undecane

Totals : 10.26130

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
36.635	MM	4.18587e-1	1.00000	2.13772e-1		?
40.962	MM	2.53161e-1	1.00000	1.29290e-1		?
42.330	MM	3.06336e-1	1.00000	1.56446e-1		?
48.320	PB	9.16084e-1	1.00000	4.67844e-1		?
51.224	MM	2.39115e-1	1.00000	1.22116e-1		?
53.597	MM	2.36982e-1	1.00000	1.21027e-1		?
54.269	MF	5.58590e-1	1.00000	2.85272e-1		?

Uncalib. totals : 1.49577

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

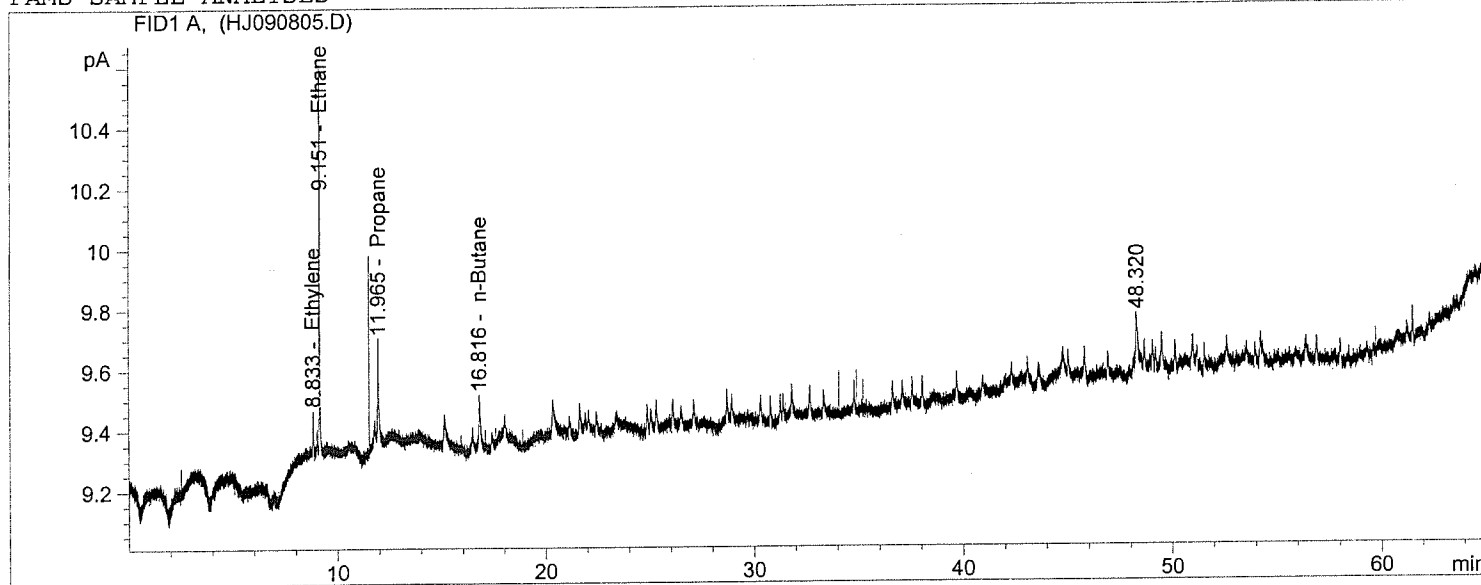
=====  
\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/9/2008 2:22:03 PM      Seq. Line   :    5
Sample Name     : AL22195 $B_PPFID          Location    : Vial 1
Acq. Operator  : JPC                        Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026          Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/9/2008 2:20:47 PM by JPC
                  (modified after loading)
    
```

GCR44

PAMS SAMPLE ANALYSES



External Standard Report

```

=====
Sorted By      : Signal
Calib. Data Modified : 10/9/2008 2:20:52 PM
Multiplier    : 0.5107
Dilution      : 1.0000
Sample Amount  : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.833	BBA	3.01725e-1	1.00000	1.54091e-1		Ethylene
9.015		-	-	-		Acetylene
9.151	BBA	3.08258	1.00000	1.57427		Ethane
11.762		-	-	-		Propylene
11.965	PBA	1.18665	1.00000	6.06020e-1		Propane
15.083		-	-	-		Isobutane
16.411		-	-	-		1-Butene
16.566		-	-	-		1,3-butadiene
16.816	BB	6.86147e-1	1.00000	3.50415e-1		n-Butane
17.433		-	-	-		t2-Butene
18.083		-	-	-		c2-Butene
20.238		-	-	-		Isopentane
21.060		-	-	-		1-Pentene
21.657		-	-	-		n-Pentane
21.797		-	-	-		Isoprene
22.050		-	-	-		t2-Pentene
22.420		-	-	-		c2-Pentene
23.432		-	-	-		2,2-Dimethylbutane
24.903		-	-	-		Cyclopentane

J

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.101	-	-	-	-	-	2,3-dimethylbutane
25.385	-	-	-	-	-	2-Methylpentane
26.200	-	-	-	-	-	3-Methylpentane
26.576	-	-	-	-	-	1-Hexene
27.237	-	-	-	-	-	n-Hexane
28.764	-	-	-	-	-	Methylcyclopentane
28.914	-	-	-	-	-	2,4-dimethylpentane
30.373	-	-	-	-	-	Benzene
31.008	-	-	-	-	-	Cyclohexane
31.348	-	-	-	-	-	2-Methylhexane
31.584	-	-	-	-	-	2,3-Dimethylpentane
32.010	-	-	-	-	-	3-Methylhexane
32.869	-	-	-	-	-	2,2,4-Trimethylpentane
33.543	-	-	-	-	-	n-Heptane
35.039	-	-	-	-	-	Methylcyclohexane
36.868	-	-	-	-	-	2,3,4-Trimethylpentane
37.101	-	-	-	-	-	Toluene
37.806	-	-	-	-	-	2-Methylheptane
38.313	-	-	-	-	-	3-Methylheptane
39.949	-	-	-	-	-	n-Octane
43.059	-	-	-	-	-	Ethylbenzene
43.617	-	-	-	-	-	m/p-Xylene
44.781	-	-	-	-	-	Styrene
45.064	-	-	-	-	-	o-Xylene
45.851	-	-	-	-	-	n-Nonane
46.921	-	-	-	-	-	Cumene
48.671	-	-	-	-	-	n-Propylbenzene
49.070	-	-	-	-	-	m-Ethyltoluene
49.350	-	-	-	-	-	p-Ethyltoluene
49.565	-	-	-	-	-	1,3,5-Trimethylbenzene
50.165	-	-	-	-	-	o-Ethyltoluene
50.999	-	-	-	-	-	1,2,4-Trimethylbenzene
51.558	-	-	-	-	-	n-Decane
52.863	-	-	-	-	-	1,2,3-Trimethylbenzene
54.045	-	-	-	-	-	m-Diethylbenzene
54.417	-	-	-	-	-	p-Diethylbenzene
56.931	-	-	-	-	-	n-Undecane

Totals : 2.68480

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
48.320	PB	9.16084e-1	1.00000	4.67844e-1	?	

Uncalib. totals : 4.67844e-1

Results obtained with enhanced integrator!

2 Warnings or Errors :

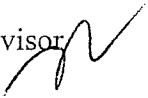
Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

=====  
\*\*\* End of Report \*\*\*

Date: 10/09/2008	Analyst: JAK	Batch: 192687	LIMS: AL22195
	%RECOVERY		
SRM concentration:	100.00		
SRM range:	90.00	110.00	
<b>\$I_SRM Result</b>	<b>Recovery %</b>	<b>In Range? (T/F)</b>	
99.34	99.34	TRUE	
<b>\$C_SRM Result</b>	<b>Recovery %</b>	<b>In Range? (T/F)</b>	
101.02	101.02	TRUE	
	<b>RESPONSE FACTORS</b>		
SRM concentration:	100.00		
SRM range (RF):	0.4594	0.5615	
<b>\$I_SRM area</b>	<b>Response Factor</b>	<b>In Range? (y/n)</b>	
194.52	0.5141	TRUE	
<b>\$C_SRM area</b>	<b>Response Factor</b>	<b>In Range? (y/n)</b>	
197.80	0.5056	TRUE	
RPD (I vs.C)	1.674		



From: Jianzhong Liu  
Environmental Scientist Supervisor  
Air Organics, LSD, DEQ 

Date: May 13, 2008

Re: FID SRM PREPARATION

Stock Standard:

Manufacturer:	Spectra Gases, Inc.
Cylinder #:	CC-162783
Certified Concentration:	1.18 ppm
Expiration Date:	2/25/2009

Working SRM:

Target Concentration:	100.00 ppbC
Flow Rate of the Stock Std:	40 cc/min
Flow Rate of Nitrogen:	1376 cc/min



3434 Route 22 West, Branchburg, New Jersey 08876 USA

ISO 9001:2000

SHIPPED FROM: 80 INDUSTRIAL DRIVE ALPHA, NJ. 08865

SHIPPED TO: Environmental Quality - LA  
Air Organics Lab, LDEQ  
1209 Leesville Road  
Baton Rouge, LA 70802

**CERTIFICATE  
OF  
ANALYSIS**

SGI ORDER # : 125072  
ITEM# : 1  
CERTIFICATION DATE: 02/25/2008  
P.O.# : CC - J Liu  
BLEND TYPE: CERTIFIED

CYLINDER # : CC-162783  
CYLINDER PRES: 2000 psig  
CYLINDER VALVE: CGA 350  
PRODUCT EXPIRATION DATE: 02/25/2009

ANALYTICAL ACCURACY: + / - 2%

<u>COMPONENT</u>	<u>REQUESTED GAS CONC</u>	<u>ANALYSIS</u>
Propane	1.20 ppm	1.18 ppm
Nitrogen	Balance	Balance

Received on 3/7/08  
opened on 3/7/08 m

NIST TRACEABLE

ANALYST: \_\_\_\_\_

*CP*  
Cheryl Patino

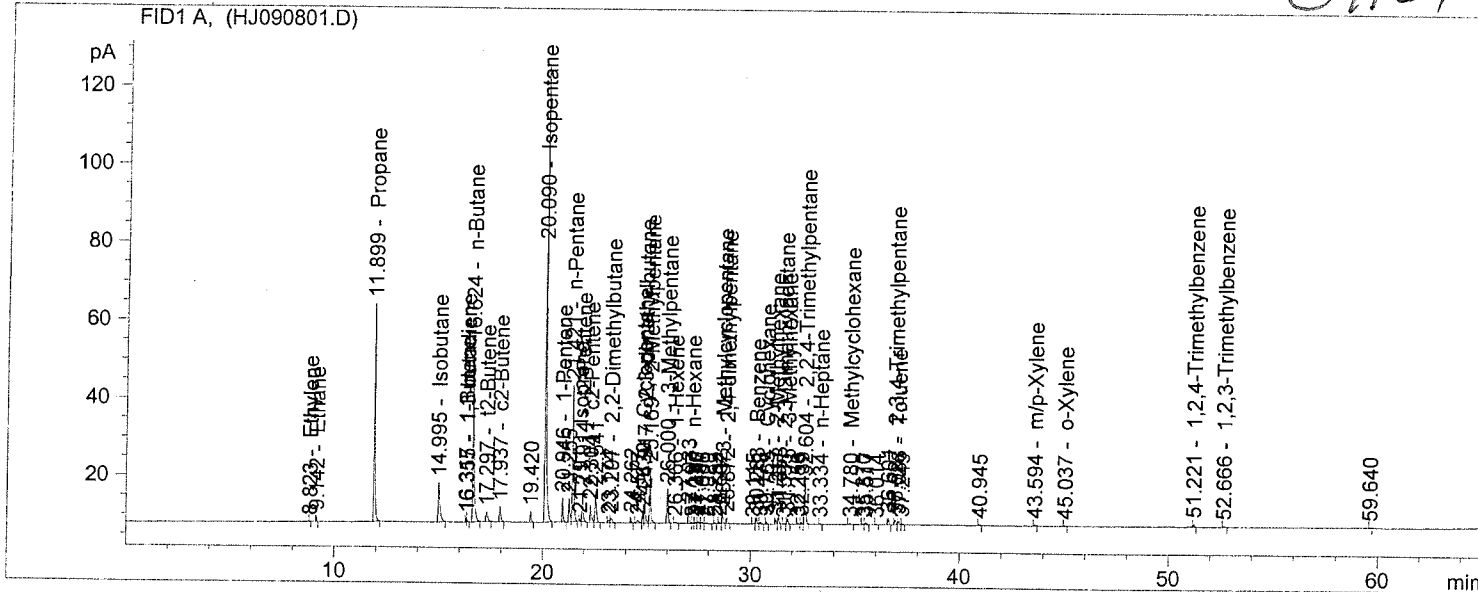
DATE: 02/25/2008

```

=====
Injection Date   : 10/9/2008 9:04:16 AM      Seq. Line   :    1
Sample Name     : AL22195 $I_SRM           Location    : Vial 1
Acq. Operator  : JPC                      Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026        Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method: C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/9/2008 9:17:54 AM by JPC
                (modified after loading)
    
```

G1124

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By           :      Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier          : 0.5107
Dilution            : 1.0000
Sample Amount       : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.823	BBA	2.61487e-1	1.00000	1.33541e-1		Ethylene
8.897		-	-	-		Acetylene
9.142	PBA	2.93590	1.00000	1.49936		Ethane
11.693		-	-	-		Propylene
11.899	PBA	194.51570	1.00000	99.33917		Propane
14.995	PB +	59.44752	1.00000	30.35985		Isobutane
16.317	PV	2.59695	1.00000	1.32626		1-Butene
16.355	VB	2.90993	1.00000	1.48610		1,3-butadiene
16.624	PB	201.51773	1.00000	102.91511		n-Butane
17.297	PB	14.00146	1.00000	7.15054		t2-Butene
17.937	PP	18.09837	1.00000	9.24284		c2-Butene
20.090	PB	442.96112	1.00000	226.22024		Isopentane
20.946	BB	19.75955	1.00000	10.09120		1-Pentene
21.421	VB	150.20596	1.00000	76.71019		n-Pentane
21.791	PV	1.96637	1.00000	1.00423		Isoprene
21.914	VP	29.56368	1.00000	15.09817		t2-Pentene
22.304	PV	18.83040	1.00000	9.61668		c2-Pentene
23.297	VB	7.87133	1.00000	4.01989		2,2-Dimethylbutane
24.830	VV	8.01592	1.00000	4.09373		Cyclopentane

10-9-08  
JAK

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.917	VV	28.82772	1.00000	14.72232		2,3-dimethylbutane
25.169	VB	57.93069	1.00000	29.58520		2-Methylpentane
26.000	BB	35.87003	1.00000	18.31883		3-Methylpentane
26.366	PB	1.65476	1.00000	8.45087e-1		1-Hexene
27.197	BB	8.01157e-1	1.00000	4.09151e-1		n-Hexane
28.673	VB	11.00994	1.00000	5.62278		Methylcyclopentane
28.872	BB	6.39602	1.00000	3.26645		2,4-dimethylpentane
30.283	BB +	6.25712	1.00000	3.19551		Benzene
30.765	BB	1.86090	1.00000	9.50359e-1		Cyclohexane
31.217	BV	4.17835	1.00000	2.13388		2-Methylhexane
31.595	BP	4.61146e-1	1.00000	2.35507e-1		2,3-Dimethylpentane
31.775	BB	4.96585	1.00000	2.53606		3-Methylhexane
32.604	VB	43.81662	1.00000	22.37715		2,2,4-Trimethylpentane
33.334	PP	5.83060e-1	1.00000	2.97769e-1		n-Heptane
34.780	BB	2.05122	1.00000	1.04756		Methylcyclohexane
36.927	BV	5.04707	1.00000	2.57754		2,3,4-Trimethylpentane
37.086	VV +	4.28318	1.00000	2.18742		Toluene
37.791		-	-	-		2-Methylheptane
38.298		-	-	-		3-Methylheptane
39.933		-	-	-		n-Octane
43.042		-	-	-		Ethylbenzene
43.594	PB	1.48484	1.00000	7.58308e-1		m/p-Xylene
44.763		-	-	-		Styrene
45.037	PP	6.97252e-1	1.00000	3.56086e-1		o-Xylene
45.833		-	-	-		n-Nonane
46.902		-	-	-		Cumene
48.652		-	-	-		n-Propylbenzene
49.051		-	-	-		m-Ethyltoluene
49.330		-	-	-		p-Ethyltoluene
49.545		-	-	-		1,3,5-Trimethylbenzene
50.145		-	-	-		o-Ethyltoluene
51.221	BP	2.91077	1.00000	1.48653		1,2,4-Trimethylbenzene
51.538		-	-	-		n-Decane
52.666	BB	1.69162	1.00000	8.63911e-1		1,2,3-Trimethylbenzene
54.024		-	-	-		m-Diethylbenzene
54.395		-	-	-		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 714.08050

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
19.420	PB	9.45925	1.00000	4.83084	?	
21.255	PV	23.64181	1.00000	12.07387	?	
22.541	VP	36.31593	1.00000	18.54655	?	
23.174	PV	3.03796	1.00000	1.55149	?	
24.262	PB	3.61210	1.00000	1.84470	?	
24.577	PV	5.55780	1.00000	2.83837	?	
27.033	PB	13.81527	1.00000	7.05546	?	
27.370	BV	1.16094	1.00000	5.92892e-1	?	
27.497	VV	2.56494	1.00000	1.30991	?	
27.686	VV	1.97282	1.00000	1.00752	?	
27.929	VB	1.08036	1.00000	5.51740e-1	?	
28.292	BB	9.77552e-1	1.00000	4.99236e-1	?	
28.502	BV	2.25036	1.00000	1.14926	?	
30.115	PB	5.48365e-1	1.00000	2.80050e-1	?	
30.473	BP	2.08192	1.00000	1.06324	?	
31.358	VB	6.41636	1.00000	3.27683	?	
32.256	PP	9.34638e-1	1.00000	4.77320e-1	?	
32.439	BV	1.83783	1.00000	9.38580e-1	?	
35.370	PP	7.36042e-1	1.00000	3.75897e-1	?	
35.517	VB	2.49518	1.00000	1.27429	?	

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
36.014	BB	5.08486e-1	1.00000	2.59684e-1	?	
36.601	PB	6.00512	1.00000	3.06681	?	
37.249	VB	1.36379	1.00000	6.96490e-1	?	
40.945	PP	1.65974	1.00000	8.47630e-1	?	
59.640	BB	6.65468e-1	1.00000	3.39854e-1	?	

Uncalib. totals : 66.74851

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

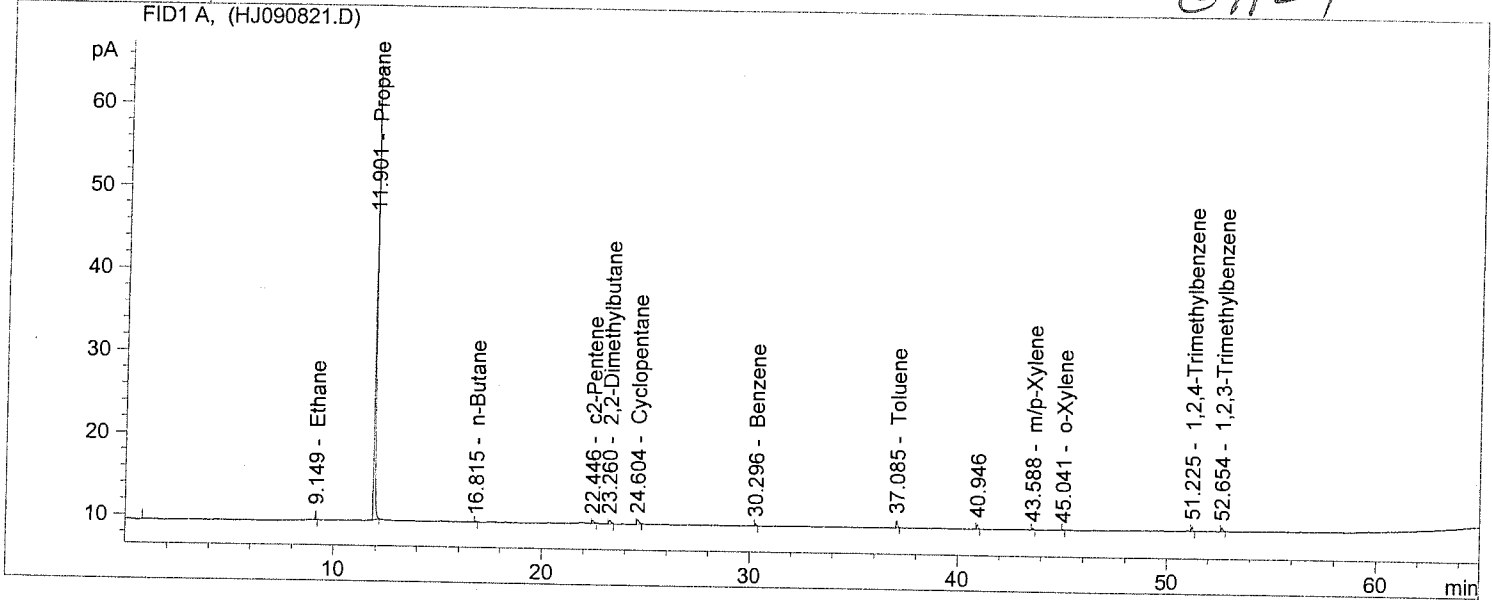
Warning : Time reference compound(s) not found

=====  
\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/10/2008 11:49:34 AM      Seq. Line   : 21
Sample Name     : AL22195 $C_SRM              Location    : Vial 1
Acq. Operator  : JPC                          Inj        : 1
Acq. Instrument : HP_FID2 SOP 1026            Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/10/2008 11:50:57 AM by JPC
                (modified after loading)
    
```

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By           : Signal
Calib. Data Modified : 10/10/2008 11:51:05 AM
Multiplier          : 0.5107
Dilution            : 1.0000
Sample Amount       : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.688		-	-	-		Ethylene
8.927		-	-	-		Acetylene
9.149	PBA	2.48618	1.00000	1.26969		Ethane
11.670		-	-	-		Propylene
11.901	PBA	191.07982	1.00000	97.58446		Propane
15.000		-	-	-		Isobutane
16.369		-	-	-		1-Butene
16.524		-	-	-		1,3-butadiene
16.815	PB	6.31383e-1	1.00000	3.22447e-1		n-Butane
17.389		-	-	-		t2-Butene
18.037		-	-	-		c2-Butene
20.187		-	-	-		Isopentane
21.007		-	-	-		1-Pentene
21.602		-	-	-		n-Pentane
21.795		-	-	-		Isoprene
21.994		-	-	-		t2-Pentene
22.446	PP	2.49812	1.00000	1.27579		c2-Pentene
23.260	PB	3.51899	1.00000	1.79715		2,2-Dimethylbutane
24.604	PB	3.93857	1.00000	2.01143		Cyclopentane

10-10-08  
JPC

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.937		-	-	-		2,3-dimethylbutane
25.126		-	-	-		2-Methylpentane
26.134		-	-	-		3-Methylpentane
26.509		-	-	-		1-Hexene
26.932		-	-	-		n-Hexane
28.691		-	-	-		Methylcyclopentane
28.841		-	-	-		2,4-dimethylpentane
30.296	PB +	1.34777	1.00000	6.88305e-1		Benzene
30.937		-	-	-		Cyclohexane
31.280		-	-	-		2-Methylhexane
31.518		-	-	-		2,3-Dimethylpentane
31.948		-	-	-		3-Methylhexane
32.815		-	-	-		2,2,4-Trimethylpentane
33.300		-	-	-		n-Heptane
35.004		-	-	-		Methylcyclohexane
36.850		-	-	-		2,3,4-Trimethylpentane
37.085	PB +	3.61052	1.00000	1.84389		Toluene
37.790		-	-	-		2-Methylheptane
38.297		-	-	-		3-Methylheptane
39.932		-	-	-		n-Octane
43.041		-	-	-		Ethylbenzene
43.588	PB	1.00328	1.00000	5.12374e-1		m/p-Xylene
44.762		-	-	-		Styrene
45.041	PP	5.15547e-1	1.00000	2.63290e-1		o-Xylene
45.831		-	-	-		n-Nonane
46.901		-	-	-		Cumene
48.650		-	-	-		n-Propylbenzene
49.049		-	-	-		m-Ethyltoluene
49.329		-	-	-		p-Ethyltoluene
49.544		-	-	-		1,3,5-Trimethylbenzene
50.144		-	-	-		o-Ethyltoluene
51.225	PP	2.27219	1.00000	1.16041		1,2,4-Trimethylbenzene
51.536		-	-	-		n-Decane
52.654	PB	2.96308	1.00000	1.51324		1,2,3-Trimethylbenzene
54.022		-	-	-		m-Diethylbenzene
54.394		-	-	-		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 110.24248

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
40.946	BB	2.52436	1.00000	1.28919	?	

Uncalib. totals : 1.28919

Results obtained with enhanced integrator!  
 2 Warnings or Errors :

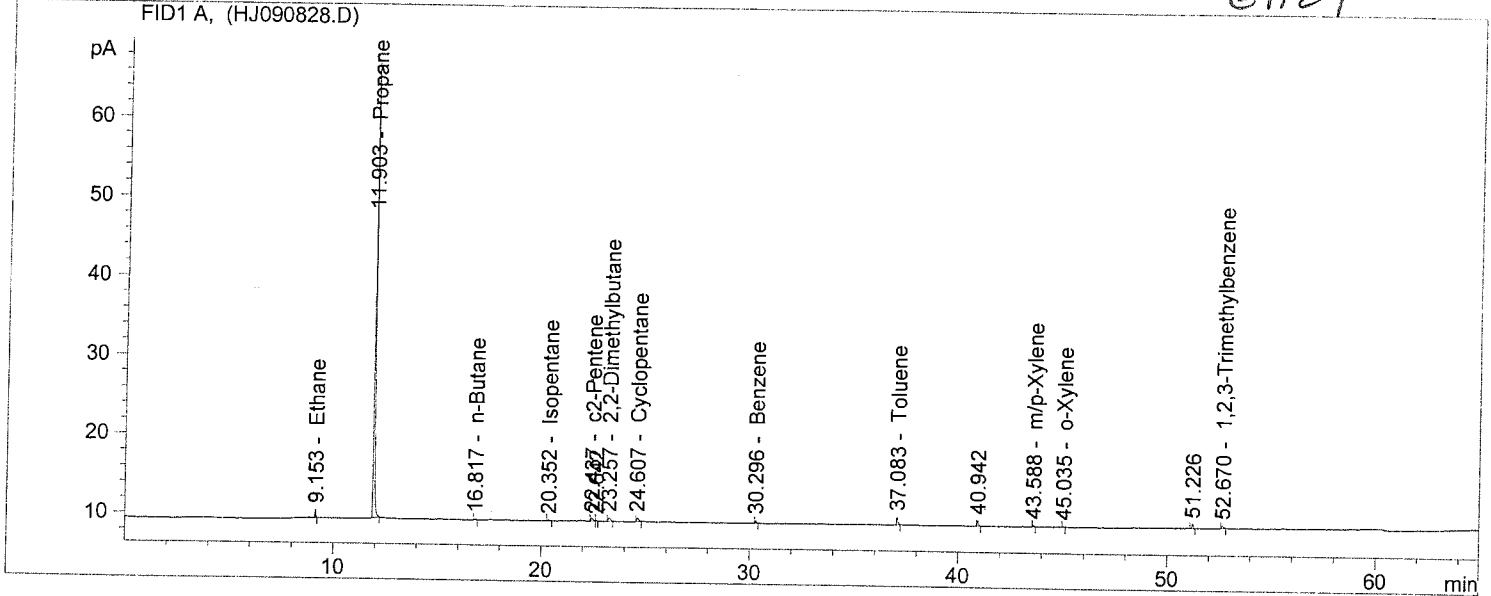
Warning : Calibration warnings (see calibration table listing)  
 Warning : Time reference compound(s) not found

\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/10/2008 9:01:56 PM      Seq. Line   : 28
Sample Name     : AL22195 $C_SRM             Location    : Vial 1
Acq. Operator  : JPC                          Inj         : 1
Acq. Instrument : HP_FID2 SOP 1026           Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/10/2008 11:50:57 AM by JPC
                  (modified after loading)
    
```

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By           : Signal
Calib. Data Modified : 10/10/2008 11:51:05 AM
Multiplier          : 0.5107
Dilution            : 1.0000
Sample Amount       : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.688	-	-	-	-	-	Ethylene
8.927	-	-	-	-	-	Acetylene
9.153	PBA	2.50638	1.00000	1.28001	-	Ethane
11.670	-	-	-	-	-	Propylene
11.903	PBA	197.79846	1.00000	101.01567	-	Propane
15.000	-	-	-	-	-	Isobutane
16.369	-	-	-	-	-	1-Butene
16.524	-	-	-	-	-	1,3-butadiene
16.817	BB	7.47370e-1	1.00000	3.81682e-1	-	n-Butane
17.389	-	-	-	-	-	t2-Butene
18.037	-	-	-	-	-	c2-Butene
20.352	PB	8.45592e-1	1.00000	4.31844e-1	-	Isopentane
21.007	-	-	-	-	-	1-Pentene
21.602	-	-	-	-	-	n-Pentane
21.795	-	-	-	-	-	Isoprene
21.994	-	-	-	-	-	t2-Pentene
22.437	PV	3.23404	1.00000	1.65162	-	c2-Pentene
23.257	PB	3.45859	1.00000	1.76630	-	2,2-Dimethylbutane
24.607	PB	3.47418	1.00000	1.77426	-	Cyclopentane

10-1308  
JAK



RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.937		-	-	-		2,3-dimethylbutane
25.126		-	-	-		2-Methylpentane
26.134		-	-	-		3-Methylpentane
26.509		-	-	-		1-Hexene
26.932		-	-	-		n-Hexane
28.691		-	-	-		Methylcyclopentane
28.841		-	-	-		2,4-dimethylpentane
30.296	PB +	1.39032	1.00000	7.10035e-1		Benzene
30.937		-	-	-		Cyclohexane
31.280		-	-	-		2-Methylhexane
31.518		-	-	-		2,3-Dimethylpentane
31.947		-	-	-		3-Methylhexane
32.814		-	-	-		2,2,4-Trimethylpentane
33.299		-	-	-		n-Heptane
35.003		-	-	-		Methylcyclohexane
36.848		-	-	-		2,3,4-Trimethylpentane
37.083	PP +	3.84051	1.00000	1.96135		Toluene
37.788		-	-	-		2-Methylheptane
38.294		-	-	-		3-Methylheptane
39.929		-	-	-		n-Octane
43.038		-	-	-		Ethylbenzene
43.588	PB	9.46518e-1	1.00000	4.83387e-1		m/p-Xylene
44.759		-	-	-		Styrene
45.035	PP	5.59634e-1	1.00000	2.85805e-1		o-Xylene
45.829		-	-	-		n-Nonane
46.898		-	-	-		Cumene
48.647		-	-	-		n-Propylbenzene
49.046		-	-	-		m-Ethyltoluene
49.326		-	-	-		p-Ethyltoluene
49.541		-	-	-		1,3,5-Trimethylbenzene
50.141		-	-	-		o-Ethyltoluene
50.974		-	-	-		1,2,4-Trimethylbenzene
51.533		-	-	-		n-Decane
52.670	PB	2.11982	1.00000	1.08259		1,2,3-Trimethylbenzene
54.019		-	-	-		m-Diethylbenzene
54.391		-	-	-		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 112.82457

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
22.642	VB	5.43828e-1	1.00000	2.77733e-1	?	
40.942	BB	2.93792	1.00000	1.50040	?	
51.226	VB	2.29285	1.00000	1.17096	?	

Uncalib. totals : 2.94909

Results obtained with enhanced integrator!  
2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)  
Warning : Time reference compound(s) not found

=====  
\*\*\* End of Report \*\*\*

## Initial Calibration Verification (LCS) FID #2

DATE: 10/9/2008

QC NO: AL22195

BATCH NO: 192687

COMPONENTS	STD (ppbc)	\$I (ppbc)	REC% \$I
Ethylene	49.20	51.25	104.2
Actetylene	48.90	54.47	111.4
Ethane	48.90	47.51	97.2
Propylene	48.90	45.53	93.1
Propane	49.00	52.67	107.5
n-Butane	48.90		
Isobutane	48.90	57.67	117.9
1-Butene	49.90	51.54	103.3
1,3-Butadiene	48.80	42.06	86.2
n-Butane	48.90	55.64	113.8
t2-butene	48.90	51.92	106.2
c2-butene	48.90	49.17	100.6
Isopentane	49.40	50.23	101.7
1-Pentene	50.70	55.19	108.9
n-Pentane	49.10	56.57	115.2
Isoprene	49.40	50.08	101.4
t2-Pentene	50.30	55.14	109.6
c2-Pentene	49.50	51.52	104.1
2,2-Dimethylbutane	49.90	54.43	109.1
Cyclopentane	59.60	53.33	89.5
2,3-Dimethylbutane	49.50	56.07	113.3
2-Methylpentane	49.10	53.56	109.1
3-Methylpentane	49.50	54.18	109.4
1-Hexene	49.30	45.50	92.3
1-Hexane	49.70	51.90	104.4
Methylcyclopentane	49.10	51.99	105.9
2,4-Dimethylpentane	49.50	51.90	104.9
Benzene	49.30	51.29	104.0
Cyclohexane	48.50	53.10	109.5
2-Methylhexane	48.80	51.21	104.9
2,3-Dimethylpentane	48.60	54.28	111.7
3-Methylhexane	48.80	52.09	106.7
2,2,4-Trimethylpentane	53.70	60.06	111.8
n-Heptane	49.00	49.36	100.7
Methylcyclohexane	49.60	53.90	108.7
2,3,4-Trimethylpentane	48.90	52.38	107.1
Toluene	49.80	48.79	98.0
2-Methylheptane	49.10	51.86	105.6
3-Methylheptane	50.70	52.61	103.8
n-Octane	48.50	49.44	101.9
Ethylbenzne	49.70	48.62	97.8
m/p-Xylene	98.50	95.39	96.8
Styrene	49.30	41.39	83.9
o Xylene	49.00	50.22	102.5
n-Nonane	48.60	47.85	98.5
Cumene	49.40	49.47	100.1
n-Propylbenzene	49.00	46.04	94.0
m-Ethyltoluene	48.70	45.85	94.2
p-Ethyltoluene	48.10	44.84	93.2
1,3,5-Trimethylbenzene	48.70	48.69	100.0
o-Ethyltouene	48.50	46.99	96.9
1,2,4-trimethylbenzene	49.00	46.72	95.3
n-Decane	48.90	46.14	94.4
1,2,3-Trimethylbenzene	48.70	41.96	86.2
m-Diethylbenzene	48.40	41.29	85.3
p-Diethylbenzene	48.40	33.79	69.8
n-Undecane	48.90	41.65	85.2

JPC

From: Jianzhong Liu  
Environmental Scientist Supervisor  
Air Organics, LSD, DEQ

Date: June 3, 2008

Re: Low Recovery of p-Diethylbenzene in PAMS LCS Standard

Stock Standard:

Manufacturer:	Matheson Tri-Gas, Inc.
Cylinder #:	SX39238D
Lot#:	1057610175
Expiration Date:	12/03/2009

From the studies of runs in different GC/FIDs, the recovery of p-diethylbenzene is constantly low (~75%). However, the recovery of this compound in PAMS standard is normal (~100%). Therefore, 60% (75%\*80%) recovery for this compound in LCS is acceptable.

**Concentrations (ppbC) of Different Diluton of Matheson Stock Standard**

**Cylinder #: SX39238D; Lot #: 1057610175; Expiration Date: 12/3/2008**

COMPONENTS	Stock Std	10 times	71.425 times	166.65 times	250 times	500 times
Ethylene	492.00	49.20	6.89	2.95	1.97	0.98
Actetylene	489.00	48.90	6.85	2.93	1.96	0.98
Ethane	489.00	48.90	6.85	2.93	1.96	0.98
Propylene	489.00	48.90	6.85	2.93	1.96	0.98
Propane	490.00	49.00	6.86	2.94	1.96	0.98
n-Butane	489.00	48.90	6.85	2.93	1.96	0.98
Isobutane	489.00	48.90	6.85	2.93	1.96	0.98
1-Butene	499.00	49.90	6.99	2.99	2.00	1.00
1,3-Butadiene	488.00	48.80	6.83	2.93	1.95	0.98
n-Butane	489.00	48.90	6.85	2.93	1.96	0.98
t2-butene	489.00	48.90	6.85	2.93	1.96	0.98
c2-butene	489.00	48.90	6.85	2.93	1.96	0.98
Isopentane	494.00	49.40	6.92	2.96	1.98	0.99
1-Pentene	507.00	50.70	7.10	3.04	2.03	1.01
n-Pentane	491.00	49.10	6.87	2.95	1.96	0.98
Isoprene	494.00	49.40	6.92	2.96	1.98	0.99
t2-Pentene	503.00	50.30	7.04	3.02	2.01	1.01
c2-Pentene	495.00	49.50	6.93	2.97	1.98	0.99
2,2-Dimethylbutane	499.00	49.90	6.99	2.99	2.00	1.00
Cyclopentane	596.00	59.60	8.34	3.58	2.38	1.19
2,3-Dimethylbutane	495.00	49.50	6.93	2.97	1.98	0.99
2-Methylpentane	491.00	49.10	6.87	2.95	1.96	0.98
3-Methylpentane	495.00	49.50	6.93	2.97	1.98	0.99
1-Hexene	493.00	49.30	6.90	2.96	1.97	0.99
1-Hexane	497.00	49.70	6.96	2.98	1.99	0.99
Methylcyclopentane	491.00	49.10	6.87	2.95	1.96	0.98
2,4-Dimethylpentane	495.00	49.50	6.93	2.97	1.98	0.99
Benzene	493.00	49.30	6.90	2.96	1.97	0.99
Cyclohexane	485.00	48.50	6.79	2.91	1.94	0.97
2-Methylhexane	488.00	48.80	6.83	2.93	1.95	0.98
2,3-Dimethylpentane	486.00	48.60	6.80	2.92	1.94	0.97
3-Methylhexane	488.00	48.80	6.83	2.93	1.95	0.98
2,2,4-Trimethylpentane	537.00	53.70	7.52	3.22	2.15	1.07
n-Heptane	490.00	49.00	6.86	2.94	1.96	0.98
Methylcyclohexane	496.00	49.60	6.94	2.98	1.98	0.99
2,3,4-Trimethylpentane	489.00	48.90	6.85	2.93	1.96	0.98
Toluene	498.00	49.80	6.97	2.99	1.99	1.00
2-Methylheptane	491.00	49.10	6.87	2.95	1.96	0.98
3-Methylheptane	507.00	50.70	7.10	3.04	2.03	1.01
n-Octane	485.00	48.50	6.79	2.91	1.94	0.97
Ethylbenzne	497.00	49.70	6.96	2.98	1.99	0.99
m/p-Xylene	985.00	98.50	13.79	5.91	3.94	1.97
Styrene	493.00	49.30	6.90	2.96	1.97	0.99
o Xylene	490.00	49.00	6.86	2.94	1.96	0.98
n-Nonane	486.00	48.60	6.80	2.92	1.94	0.97
Cumene	494.00	49.40	6.92	2.96	1.98	0.99
n-Propylbenzene	490.00	49.00	6.86	2.94	1.96	0.98
m-Ethyltoluene	487.00	48.70	6.82	2.92	1.95	0.97
p-Ethyltoluene	481.00	48.10	6.73	2.89	1.92	0.96
1,3,5-Trimethylbenzene	487.00	48.70	6.82	2.92	1.95	0.97
o-Ethyltouene	485.00	48.50	6.79	2.91	1.94	0.97
1,2,4-trimethylbenzene	490.00	49.00	6.86	2.94	1.96	0.98
n-Decane	489.00	48.90	6.85	2.93	1.96	0.98
1,2,3-Trimethylbenzene	487.00	48.70	6.82	2.92	1.95	0.97
m-Diethylbenzene	484.00	48.40	6.78	2.90	1.94	0.97
p-Diethylbenzene	484.00	48.40	6.78	2.90	1.94	0.97
n-Undecane	489.00	48.90	6.85	2.93	1.96	0.98



# MATHESON TRI-GAS

## Certified Mixture Grade

Matheson Tri-Gas  
6874 S Main Street  
Morrow, GA 30260  
Phone: (770) 961-7891  
Fax: (770) 968-1268

To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd  
Baton Rouge, LA 70802

Phone:  
Fax:

TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE  
GREATER THAN PROCESS PRESSURE.

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057610175

### PRODUCT:

CYLINDER NUMBER: SX39238D  
SIZE: 1l  
CGA/DISS OUTLET: 350  
CONTENT: 131 cu. ft.  
PRESSURE: 1850 psig

Fill Date: 12/3/2007  
Certification Date: 12/3/2007  
Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	500 ppbC	498 ppbC	+/- 5%
2-Methylheptane	500 ppbC	491 ppbC	+/- 5%
3-Methylheptane	500 ppbC	507 ppbC	+/- 5%
n-Octane	500 ppbC	485 ppbC	+/- 5%
Ethylbenzene	500 ppbC	497 ppbC	+/- 5%
p-Xylene	500 ppbC	490 ppbC	+/- 5%
m-Xylene	500 ppbC	495 ppbC	+/- 5%
Styrene	500 ppbC	493 ppbC	+/- 5%
o-Xylene	500 ppbC	490 ppbC	+/- 5%
n-Nonane	500 ppbC	486 ppbC	+/- 5%
Isopropylbenzene	500 ppbC	494 ppbC	+/- 5%
n-Propylbenzene	500 ppbC	490 ppbC	+/- 5%
n-Decane	500 ppbC	489 ppbC	+/- 5%
m-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
p-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
n-Dodecane	500 ppbC	492 ppbC	+/- 5%
m-Ethyltoluene	500 ppbC	487 ppbC	+/- 5%
o-Ethyltoluene	500 ppbC	485 ppbC	+/- 5%
p-Ethyltoluene	500 ppbC	481 ppbC	+/- 5%
n-Undecane	500 ppbC	489 ppbC	+/- 5%
1,2,3-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,3,5-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,2,4-Trimethylbenzene	500 ppbC	490 ppbC	+/- 5%
Nitrogen, Balance			

### SPECIAL INFORMATION / ADDITIONAL COMMENTS

*Received on 12/16/07*

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

Derek Stuck  
ANALYST

12/4/2007  
DATE SIGNED



# MATHESON TRI-GAS

## Certified Mixture Grade

Matheson Tri-Gas  
6874 S Main Street  
Morrow, GA 30260  
Phone: (770) 961-7891  
Fax: (770) 968-1268

To: Environmental Quality  
DEQ Laboratory Services  
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1209 Leesville Rd  
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Phone:  
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TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE  
GREATER THAN PROCESS PRESSURE.

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057610175

PRODUCT:

CYLINDER NUMBER: SX39238D  
SIZE: 1l  
CGA/DISS OUTLET: 350  
CONTENT: 131 cu. ft.  
PRESSURE: 1850 psig

Fill Date: 12/3/2007  
Certification Date: 12/3/2007  
Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	500 ppbC	498 ppbC	+/- 5%
2-Methylheptane	500 ppbC	491 ppbC	+/- 5%
3-Methylheptane	500 ppbC	507 ppbC	+/- 5%
n-Octane	500 ppbC	485 ppbC	+/- 5%
Ethylbenzene	500 ppbC	497 ppbC	+/- 5%
p-Xylene	500 ppbC	490 ppbC	+/- 5%
m-Xylene	500 ppbC	495 ppbC	+/- 5%
Styrene	500 ppbC	493 ppbC	+/- 5%
o-Xylene	500 ppbC	490 ppbC	+/- 5%
ii-Nonane	500 ppbC	486 ppbC	+/- 5%
Isopropylbenzene	500 ppbC	494 ppbC	+/- 5%
n-Propylbenzene	500 ppbC	490 ppbC	+/- 5%
n-Decane	500 ppbC	489 ppbC	+/- 5%
m-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
p-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
n-Dodecane	500 ppbC	492 ppbC	+/- 5%
m-Ethyltoluene	500 ppbC	487 ppbC	+/- 5%
o-Ethyltoluene	500 ppbC	485 ppbC	+/- 5%
p-Ethyltoluene	500 ppbC	481 ppbC	+/- 5%
n-Undecane	500 ppbC	489 ppbC	+/- 5%
1,2,3-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,3,5-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,2,4-Trimethylbenzene	500 ppbC	490 ppbC	+/- 5%
Nitrogen, Balance			

### SPECIAL INFORMATION / ADDITIONAL COMMENTS

*Received on 12/16/07*

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

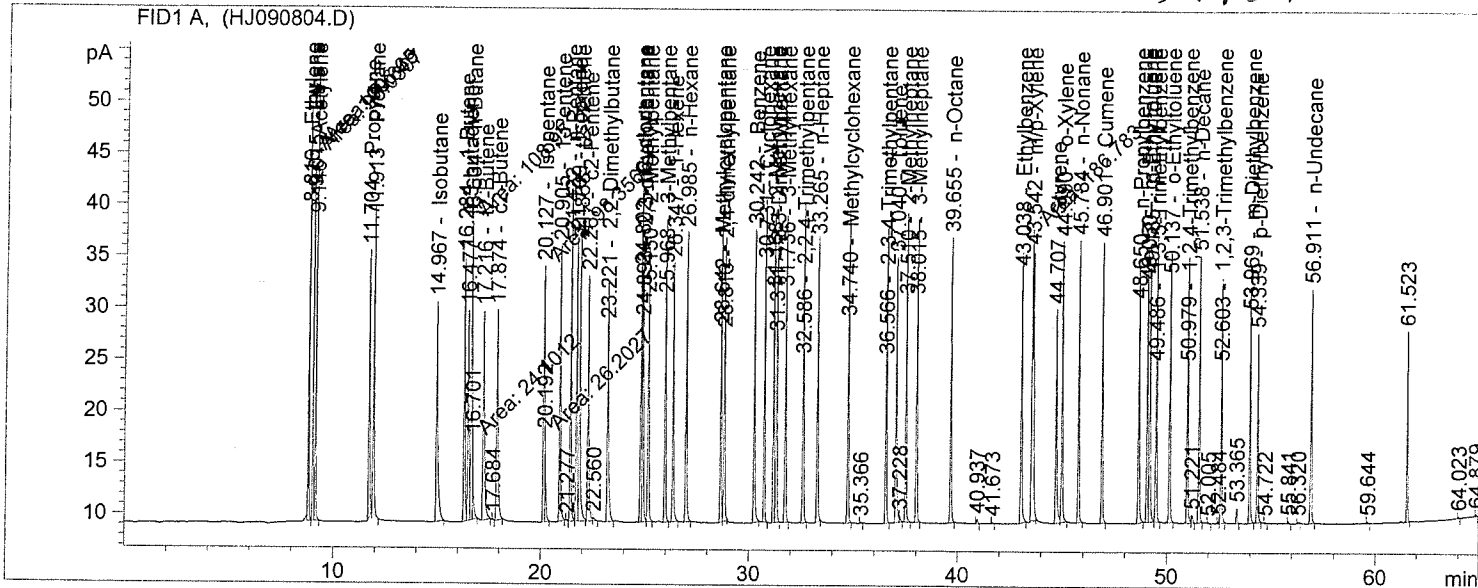
Derek Stuck  
ANALYST

12/4/2007  
DATE SIGNED

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=====
Injection Date   : 10/9/2008 1:02:00 PM      Seq. Line   : 4
Sample Name     : AL22195 $L1PPFID          Location    : Vial 4
Acq. Operator  : JPC                        Inj         : 1
Acq. Instrument : HP_FID2 SOP 1026          Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/9/2008 2:20:47 PM by JPC
                (modified after loading)
    
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PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By      : Signal
Calib. Data Modified : 10/9/2008 2:20:52 PM
Multiplier     : 0.5107
Dilution      : 1.0000
Sample Amount  : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.816	FM	100.34872	1.00000	51.24809		Ethylene
9.015	MF	93.03070	1.00000	47.51078		Ethane
9.146	FM	106.65022	1.00000	54.46627		Acetylene
11.704	PB	89.15047	1.00000	45.52915		Propylene
11.913	BBA	103.12894	1.00000	52.66795		Propene
14.967	PB +	112.93295	1.00000	57.67486		Isobutane
16.284	PV	100.92325	1.00000	51.54150		1-Butene
16.477	VV	82.35313	1.00000	42.05774		1,3-butadiene
16.634	MF	108.95028	1.00000	55.64091		n-Butane
17.216	PB	101.66692	1.00000	51.92130		t2-Butene
17.874	PB	96.28265	1.00000	49.17155		c2-Butene
20.127	MF	98.35686	1.00000	50.23085		Isopentane
20.905	PB	108.06710	1.00000	55.18987		1-Pentene
21.422	VV	110.76101	1.00000	56.56565		n-Pentane
21.709	VV	98.06431	1.00000	50.08144		Isoprene
21.868	VB	107.97594	1.00000	55.14331		t2-Pentene
22.267	BV	100.88352	1.00000	51.52121		c2-Pentene
23.221	BB	106.57977	1.00000	54.43029		2,2-Dimethylbutane
24.802	BV	104.42488	1.00000	53.32979		Cyclopentane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.893	VV	109.78324	1.00000	56.06630		2,3-dimethylbutane
25.150	VB	104.88356	1.00000	53.56403		2-Methylpentane
25.968	PB	106.08242	1.00000	54.17629		3-Methylpentane
26.347	PB	89.08646	1.00000	45.49645		1-Hexene
26.985	PB	101.61629	1.00000	51.89544		n-Hexane
28.642	PV	101.79911	1.00000	51.98881		Methylcyclopentane
28.813	VB	101.62882	1.00000	51.90184		2,4-dimethylpentane
30.242	PB +	100.42205	1.00000	51.28554		Benzene
30.731	PB	103.97024	1.00000	53.09760		Cyclohexane
31.168	BV	100.26856	1.00000	51.20715		2-Methylhexane
31.311	VB	106.27980	1.00000	54.27709		2,3-Dimethylpentane
31.736	PB	101.99803	1.00000	52.09039		3-Methylhexane
32.586	VB	117.60405	1.00000	60.06039		2,2,4-Trimethylpentane
33.265	PB	96.64803	1.00000	49.35815		n-Heptane
34.740	BB	105.54245	1.00000	53.90053		Methylcyclohexane
36.566	BB	102.55840	1.00000	52.37657		2,3,4-Trimethylpentane
37.040	BV +	95.53142	1.00000	48.78790		Toluene
37.510	BB	101.54941	1.00000	51.86128		2-Methylheptane
38.015	BB	103.01980	1.00000	52.61221		3-Methylheptane
39.655	BB	96.80012	1.00000	49.43582		n-Octane
43.038	BB	95.20465	1.00000	48.62102		Ethylbenzene
43.542	MM	186.78299	1.00000	95.39007		m/p-Xylene
44.707	BV	81.03667	1.00000	41.38543		Styrene
44.990	VB	98.32851	1.00000	50.21637		o-Xylene
45.784	BB	93.69817	1.00000	47.85166		n-Nonane
46.901	BB	96.85818	1.00000	49.46547		Cumene
48.650	BB	90.14754	1.00000	46.03835		n-Propylbenzene
49.050	BV	89.78224	1.00000	45.85179		m-Ethyltoluene
49.185	VV	87.80960	1.00000	44.84436		p-Ethyltoluene
49.486	VB	95.34503	1.00000	48.69271		1,3,5-Trimethylbenzene
50.137	VB	92.00356	1.00000	46.98622		o-Ethyltoluene
50.979	BB	91.48391	1.00000	46.72083		1,2,4-Trimethylbenzene
51.538	BB	90.34567	1.00000	46.13954		n-Decane
52.603	VB	82.16355	1.00000	41.96093		1,2,3-Trimethylbenzene
53.969	BB	80.84151	1.00000	41.28576		m-Diethylbenzene
54.339	BB	66.15607	1.00000	33.78591		p-Diethylbenzene
56.911	BB +	81.54855	1.00000	41.64685		n-Undecane

Totals : 2848.24554

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
16.701	FM	24.10120	1.00000	12.30848	?	
17.684	PB	3.09042e-1	1.00000	1.57828e-1	?	
20.192	FM	26.20266	1.00000	13.38170	?	
21.277	PP	4.50500e-1	1.00000	2.30070e-1	?	
22.560	VB	2.07857	1.00000	1.06153	?	
35.366	PP	3.92693e-1	1.00000	2.00548e-1	?	
37.228	VB	2.81350	1.00000	1.43685	?	
40.937	PB	1.71027	1.00000	8.73434e-1	?	
41.673	BB	5.29109e-1	1.00000	2.70216e-1	?	
51.221	BB	3.36630	1.00000	1.71917	?	
52.005	PP	4.53053e-1	1.00000	2.31374e-1	?	
52.484	PV	8.35210e-1	1.00000	4.26542e-1	?	
53.365	BB	5.12836	1.00000	2.61905	?	
54.722	PB	3.95335e-1	1.00000	2.01898e-1	?	
55.841	PB	8.10484e-1	1.00000	4.13914e-1	?	
56.320	PB	8.49413e-1	1.00000	4.33795e-1	?	
59.644	BP	5.23619e-1	1.00000	2.67412e-1	?	
61.523	BB	53.80622	1.00000	27.47884	?	
64.023	PP	5.51542e-1	1.00000	2.81672e-1	?	
64.879	PP	5.57680e-1	1.00000	2.84807e-1	?	



RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
Uncalib. totals :				64.27913		

Results obtained with enhanced integrator!  
2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)  
Warning : Elution order of calibrated compounds may have changed

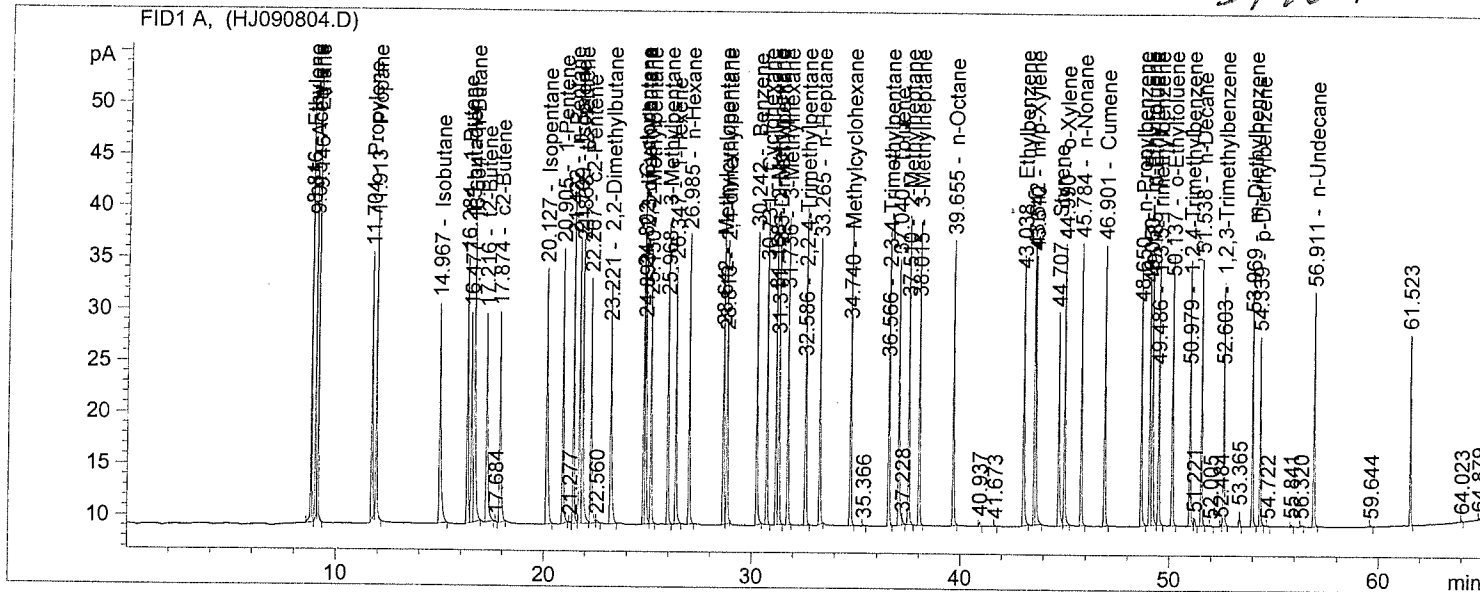
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\*\*\* End of Report \*\*\*

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Injection Date   : 10/9/2008 1:02:00 PM      Seq. Line   : 4
Sample Name     : AL22195 $L1PPFID         Location    : Vial 4
Acq. Operator  : JPC                       Inj         : 1
Acq. Instrument : HP FID2 SOP 1026        Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/9/2008 12:15:17 PM by JPC
                (modified after loading)
    
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PAMS SAMPLE ANALYSES

51404



External Standard Report

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Sorted By           : Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier          : 0.5107
Dilution            : 1.0000
Sample Amount       : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.816	BBA	103.10838	1.00000	52.65745		Ethylene
9.015	PB	89.34997	1.00000	45.63103		Acetylene
9.146	BBA	100.08290	1.00000	51.11234		Ethane
11.704	PB	89.15047	1.00000	45.52915		Propylene
11.913	BBA	103.12894	1.00000	52.66795		Propane
14.967	PB +	112.93295	1.00000	57.67486		Isobutane
16.284	PV	100.92325	1.00000	51.54150		1-Butene
16.477	VV	82.35313	1.00000	42.05774		1,3-butadiene
16.634	VB	133.08276	1.00000	67.96537		n-Butane
17.216	PB	101.66692	1.00000	51.92130		t2-Butene
17.874	PB	96.28265	1.00000	49.17155		c2-Butene
20.127	PB	124.55920	1.00000	63.61238		Isopentane
20.905	PB	108.06710	1.00000	55.18987		1-Pentene
21.422	VV	110.76101	1.00000	56.56565		n-Pentane
21.709	VV	98.06431	1.00000	50.08144		Isoprene
21.868	VB	107.97594	1.00000	55.14331		t2-Pentene
22.267	BV	100.88352	1.00000	51.52121		c2-Pentene
23.221	BB	106.57977	1.00000	54.43029		2,2-Dimethylbutane
24.802	BV	104.42488	1.00000	53.32979		Cyclopentane

I

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.893	VV	109.78324	1.00000	56.06630		2,3-dimethylbutane
25.150	VB	104.88356	1.00000	53.56403		2-Methylpentane
25.968	PB	106.08242	1.00000	54.17629		3-Methylpentane
26.347	PB	89.08646	1.00000	45.49645		1-Hexene
26.985	PB	101.61629	1.00000	51.89544		n-Hexane
28.642	PV	101.79911	1.00000	51.98881		Methylcyclopentane
28.813	VB	101.62882	1.00000	51.90184		2,4-dimethylpentane
30.242	PB +	100.42205	1.00000	51.28554		Benzene
30.731	PB	103.97024	1.00000	53.09760		Cyclohexane
31.168	BV	100.26856	1.00000	51.20715		2-Methylhexane
31.311	VB	106.27980	1.00000	54.27709		2,3-Dimethylpentane
31.736	PB	101.99803	1.00000	52.09039		3-Methylhexane
32.586	VB	117.60405	1.00000	60.06039		2,2,4-Trimethylpentane
33.265	PB	96.64803	1.00000	49.35815		n-Heptane
34.740	BB	105.54245	1.00000	53.90053		Methylcyclohexane
36.566	BB	102.55840	1.00000	52.37657		2,3,4-Trimethylpentane
37.040	BV +	95.53142	1.00000	48.78790		Toluene
37.510	BB	101.54941	1.00000	51.86128		2-Methylheptane
38.015	BB	103.01980	1.00000	52.61221		3-Methylheptane
39.655	BB	96.80012	1.00000	49.43582		n-Octane
43.038	BB	95.20465	1.00000	48.62102		Ethylbenzene
43.542	PV	88.68321	1.00000	45.29052		m/p-Xylene
44.707	BV	81.03667	1.00000	41.38543		Styrene
44.990	VB	98.32851	1.00000	50.21637		o-Xylene
45.784	BB	93.69817	1.00000	47.85166		n-Nonane
46.901	BB	96.85818	1.00000	49.46547		Cumene
48.650	BB	90.14754	1.00000	46.03835		n-Propylbenzene
49.050	BV	89.78224	1.00000	45.85179		m-Ethyltoluene
49.185	VV	87.80960	1.00000	44.84436		p-Ethyltoluene
49.486	VB	95.34503	1.00000	48.69271		1,3,5-Trimethylbenzene
50.137	VB	92.00356	1.00000	46.98622		o-Ethyltoluene
50.979	BB	91.48391	1.00000	46.72083		1,2,4-Trimethylbenzene
51.538	BB	90.34567	1.00000	46.13954		n-Decane
52.603	VB	82.16355	1.00000	41.96093		1,2,3-Trimethylbenzene
53.969	BB	80.84151	1.00000	41.28576		m-Diethylbenzene
54.339	BB	66.15607	1.00000	33.78591		p-Diethylbenzene
56.911	BB +	81.54855	1.00000	41.64685		n-Undecane

Totals : 2820.02765

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
17.684	PB	3.09042e-1	1.00000	1.57828e-1		?
21.277	PP	4.50500e-1	1.00000	2.30070e-1		?
22.560	VB	2.07857	1.00000	1.06153		?
35.366	PP	3.92693e-1	1.00000	2.00548e-1		?
37.228	VB	2.81350	1.00000	1.43685		?
40.937	PB	1.71027	1.00000	8.73434e-1		?
41.673	BB	5.29109e-1	1.00000	2.70216e-1		?
43.610	VB	101.86528	1.00000	52.02260		?
51.221	BB	3.36630	1.00000	1.71917		?
52.005	PP	4.53053e-1	1.00000	2.31374e-1		?
52.484	PV	8.35210e-1	1.00000	4.26542e-1		?
53.365	BB	5.12836	1.00000	2.61905		?
54.722	PB	3.95335e-1	1.00000	2.01898e-1		?
55.841	PB	8.10484e-1	1.00000	4.13914e-1		?
56.320	PB	8.49413e-1	1.00000	4.33795e-1		?
59.644	BP	5.23619e-1	1.00000	2.67412e-1		?
61.523	BB	53.80622	1.00000	27.47884		?
64.023	PP	5.51542e-1	1.00000	2.81672e-1		?
64.879	PP	5.57680e-1	1.00000	2.84807e-1		?

Uncalib. totals : 90.61155

Results obtained with enhanced integrator!

1 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

=====  
\*\*\* End of Report \*\*\*

PAMS RETENTION TIME STD FID #2 lot #1057410185

DATE: 10/9/2008 QC NO: AL22195 BATCH NO: 192687

COMPONENTS	STD (ppbc)	\$I (ppbc)	REC% \$I
Ethylene	21.00	23.96	114.1
Actetylene	42.00	18.87	44.9
Ethane	26.00	30.93	119.0
Propylene	26.00	21.11	81.2
Propane	40.00	44.55	111.4
n-Butane	43.00		
Isobutane	25.00	27.35	109.4
1-Butene	32.00	31.41	98.1
1,3-Butadiene	32.00	24.35	76.1
n-Butane	43.00	50.43	117.3
t2-butene	26.00	25.38	97.6
c2-butene	38.00	37.65	99.1
Isopentane	40.00	44.07	110.2
1-Pentene	25.00	25.23	100.9
n-Pentane	26.00	26.90	103.5
Isoprene	42.00	38.29	91.2
t2-Pentene	25.00	28.21	112.8
c2-Pentene	34.00	33.94	99.8
2,2-Dimethylbutane	40.00	43.77	109.4
Cyclopentane	21.00	20.28	96.5
2,3-Dimethylbutane	51.00	56.71	111.2
2-Methylpentane	21.00	22.58	107.5
3-Methylpentane	41.00	42.93	104.7
1-Hexene	61.00	59.88	98.2
1-Hexane	30.00	31.31	104.4
Methylcyclopentane	26.00	27.05	104.0
2,4-Dimethylpentane	40.00	42.56	106.4
Benzene	31.00	31.28	100.9
Cyclohexane	42.00	43.52	103.6
2-Methylhexane	25.00	25.99	104.0
2,3-Dimethylpentane	54.00	55.69	103.1
3-Methylhexane	26.00	26.78	103.0
2,2,4-Trimethylpentane	31.00	32.15	103.7
n-Heptane	26.00	26.29	101.1
Methylcyclohexane	31.00	32.69	105.5
2,3,4-Trimethylpentane	25.00	26.33	105.3
Toluene	40.00	38.76	96.9
2-Methylheptane	25.00	25.60	102.4
3-Methylheptane	25.00	26.20	104.8
n-Octane	31.00	29.76	96.0
Ethylbenzne	25.00	24.13	96.5
m/p-Xylene	42.00	38.96	92.8
Styrene	41.00	34.05	83.1
o Xylene	26.00	25.62	98.5
n-Nonane	25.00	24.36	97.4
Cumene	40.00	40.68	101.7
n-Propylbenzene	30.00	29.05	96.8
m-Ethyltoluene	25.00	25.00	100.0
p-Ethyltoluene	43.00	40.64	94.5
1,3,5-Trimethylbenzene	26.00	25.65	98.7
o-Ethyltouene	27.00	30.75	113.9
1,2,4-trimethylbenzene	39.00	39.32	100.8
n-Decane	30.00	29.29	97.6
1,2,3-Trimethylbenzene	25.00	25.70	102.8
m-Diethylbenzene	40.00	39.31	98.3
p-Diethylbenzene	27.00	24.15	89.4
n-Undecane	41.00	27.53	67.2



# MATHESON TRI-GAS

## Certified Mixture Grade

*PAMS*  
Matheson Tri-Gas  
6874 S Main Street  
Morrow, GA 30260  
Phone: (770) 961-7891  
Fax: (770) 968-1268

To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd  
Baton Rouge, LA 70802

TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE  
GREATER THAN PROCESS PRESSURE.

Phone:  
Fax:

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057410185

### PRODUCT:

CYLINDER NUMBER: CC-250112  
SIZE: 1l  
CGA/DISS OUTLET: 350  
CONTENT: 131 cu. ft.  
PRESSURE: 1850 psig

Fill Date: 12/3/2007  
Certification Date: 12/3/2007  
Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Ethylene	20 ppbC	21 ppbC	+/- 5%
Ethane	25 ppbC	26 ppbC	+/- 5%
Acetylene	40 ppbC	42 ppbC	+/- 5%
Propylene	25 ppbC	26 ppbC	+/- 5%
Propane	40 ppbC	40 ppbC	+/- 5%
Isobutane	25 ppbC	25 ppbC	+/- 5%
1-Butene	30 ppbC	32 ppbC	+/- 5%
1,3-Butadiene	30 ppbC	32 ppbC	+/- 5%
n-Butane	40 ppbC	43 ppbC	+/- 5%
trans-2-Butene	25 ppbC	25 ppbC	+/- 5%
cis-2-Butene	35 ppbC	38 ppbC	+/- 5%
Isopentane	40 ppbC	40 ppbC	+/- 5%
1-Pentene	25 ppbC	25 ppbC	+/- 5%
n-Pentane	25 ppbC	26 ppbC	+/- 5%
Isoprene	40 ppbC	42 ppbC	+/- 5%
trans-2-Pentene	25 ppbC	25 ppbC	+/- 5%
cis-2-Pentene	35 ppbC	34 ppbC	+/- 5%
Cyclopentene	20 ppbC	21 ppbC	+/- 5%
2,2-Dimethylbutane	40 ppbC	40 ppbC	+/- 5%
2-Methylpentane	20 ppbC	21 ppbC	+/- 5%
3-Methylpentane	40 ppbC	41 ppbC	+/- 5%
2,3-Dimethylbutane	50 ppbC	51 ppbC	+/- 5%
1-Hexene	60 ppbC	61 ppbC	+/- 5%
n-Hexane	30 ppbC	30 ppbC	+/- 5%
Methylcyclopentane	25 ppbC	26 ppbC	+/- 5%
2,4-Dimethylpentane	40 ppbC	40 ppbC	+/- 5%
Benzene	30 ppbC	31 ppbC	+/- 5%
Cyclohexane	40 ppbC	42 ppbC	+/- 5%
2,3-Dimethylpentane	50 ppbC	54 ppbC	+/- 5%
2-Methylhexane	25 ppbC	25 ppbC	+/- 5%
3-Methylhexane	25 ppbC	26 ppbC	+/- 5%
n-Heptane	25 ppbC	26 ppbC	+/- 5%
2,2,4-Trimethylpentane	30 ppbC	31 ppbC	+/- 5%
Methylcyclohexane	30 ppbC	31 ppbC	+/- 5%
2,3,4-Trimethylpentane	25 ppbC	25 ppbC	+/- 5%

*Received on 12/6/07*

TRACEABLE TO REFERENCE STANDARD SOURCE/NUMBER:  
TRACEABLE TO NIST TRACEABLE WEIGHT CERTIFICATE:



# MATHESON TRI-GAS

## Certified Mixture Grade

**Matheson Tri-Gas**

6874 S Main Street

Morrow, GA 30260

Phone: (770) 961-7891

Fax: (770) 968-1268

To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd

**TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE  
GREATER THAN PROCESS PRESSURE.**

Phone:  
Fax:

SALES ORDER NUMBER: 427497

P.O. NUMBER: 3243638

LOT NUMBER: 1057410185

### PRODUCT:

CYLINDER NUMBER: CC-250112

SIZE: 1l

CGA/DISS OUTLET: 350

CONTENT: 131 liters

PRESSURE: 1850 psig

Fill Date: 12/3/2007

Certification Date: 12/3/2007

Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	40 ppbC	40 ppbC	+/- 5%
2-Methylheptane	25 ppbC	25 ppbC	+/- 5%
3-Methylheptane	25 ppbC	25 ppbC	+/- 5%
n-Octane	30 ppbC	31 ppbC	+/- 5%
Ethylbenzene	25 ppbC	25 ppbC	+/- 5%
p-Xylene	20 ppbC	21 ppbC	+/- 5%
m-Xylene	20 ppbC	21 ppbC	+/- 5%
Styrene	40 ppbC	41 ppbC	+/- 5%
o-Xylene	25 ppbC	26 ppbC	+/- 5%
n-Nonane	25 ppbC	25 ppbC	+/- 5%
Isopropylbenzene	40 ppbC	40 ppbC	+/- 5%
n-Propylbenzene	30 ppbC	30 ppbC	+/- 5%
n-Decane	30 ppbC	30 ppbC	+/- 5%
m-Diethylbenzene	40 ppbC	40 ppbC	+/- 5%
p-Diethylbenzene	25 ppbC	27 ppbC	+/- 5%
n-Dodecane	30 ppbC	31 ppbC	+/- 5%
m-Ethyltoluene	25 ppbC	25 ppbC	+/- 5%
o-Ethyltoluene	30 ppbC	27 ppbC	+/- 5%
p-Ethyltoluene	40 ppbC	43 ppbC	+/- 5%
n-Undecane	40 ppbC	41 ppbC	+/- 5%
1,2,3-Trimethylbenzene	25 ppbC	25 ppbC	+/- 5%
1,3,5-Trimethylbenzene	25 ppbC	26 ppbC	+/- 5%
1,2,4-Trimethylbenzene	40 ppbC	39 ppbC	+/- 5%
Nitrogen, Balance			

### SPECIAL INFORMATION / ADDITIONAL COMMENTS

Received 12/6/07 m

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

Derek Stuck  
ANALYST

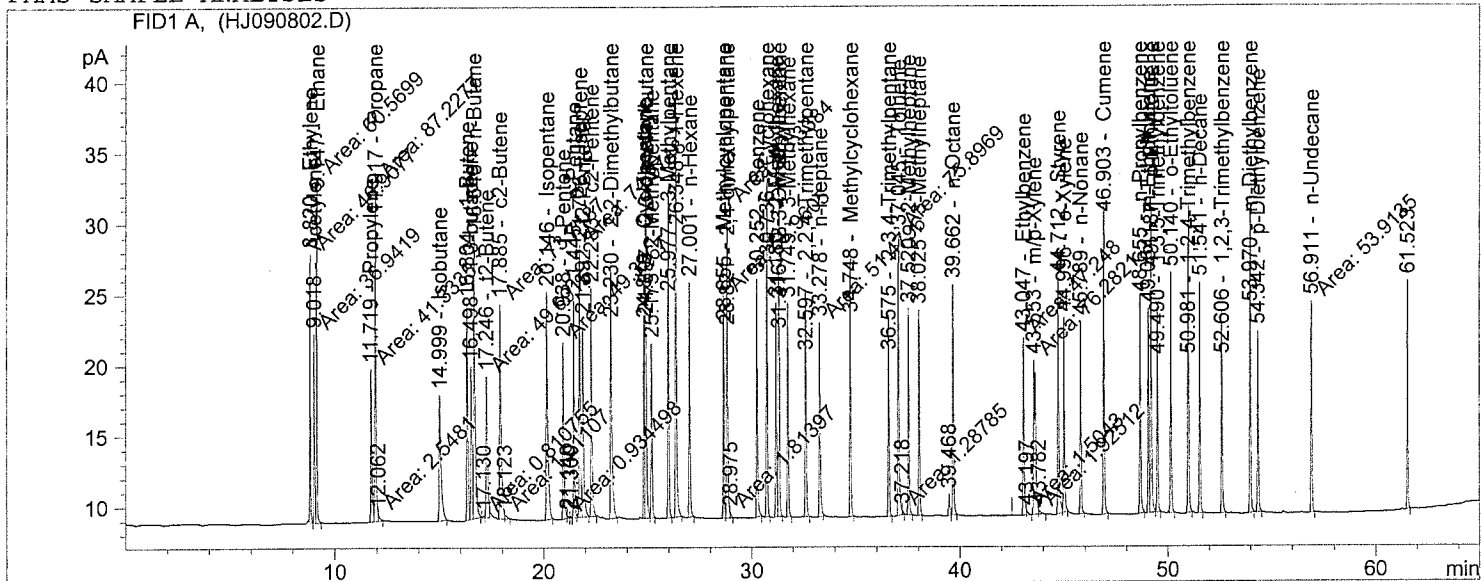
12/4/2007  
DATE SIGNED

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=====
Injection Date   : 10/9/2008 10:23:44 AM      Seq. Line   :    2
Sample Name     : AL22195 $I_PPFID           Location    : Vial 3
Acq. Operator   : JPC                        Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026           Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/9/2008 12:15:17 PM by JPC
                  (modified after loading)
    
```

G1152

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By           : Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier          : 0.5107
Dilution            : 1.0000
Sample Amount       : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.820	FM	46.90773	1.00000	23.95578		Ethylene
9.018	MF	36.94192	1.00000	18.86624		Acetylene
9.147	FM	60.56993	1.00000	30.93306		Ethane
11.719	MF	41.33355	1.00000	21.10904		Propylene
11.917	MF	87.22768	1.00000	44.54718		Propane
14.999	PB +	53.55767	1.00000	27.35190		Isobutane
16.304	BV	61.49738	1.00000	31.40671		1-Butene
16.498	VV	47.68173	1.00000	24.35106		1,3-butadiene
16.646	VB	98.74651	1.00000	50.42984		n-Butane
17.246	MF	49.69148	1.00000	25.37744		t2-Butene
17.885	MF	73.71873	1.00000	37.64815		c2-Butene
20.146	PB	86.29390	1.00000	44.07029		Isopentane
20.938	MF	49.39668	1.00000	25.22688		1-Pentene
21.445	VV	52.67418	1.00000	26.90070		n-Pentane
21.726	FM	74.97482	1.00000	38.28964		Isoprene
21.892	VB	55.23119	1.00000	28.20657		t2-Pentene
22.283	PP	66.45922	1.00000	33.94072		c2-Pentene
23.230	PB	85.71204	1.00000	43.77314		2,2-Dimethylbutane
24.818	BV	39.70129	1.00000	20.27545		Cyclopentane

10-9-08  
OAK



RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.897	VV	111.04067	1.00000	56.70847		2,3-dimethylbutane
25.175	VB	44.21571	1.00000	22.58096		2-Methylpentane
25.977	BB	84.06284	1.00000	42.93089		3-Methylpentane
26.348	BB	117.24971	1.00000	59.87943		1-Hexene
27.001	BB	61.30326	1.00000	31.30758		n-Hexane
28.655	MF	52.96046	1.00000	27.04691		Methylcyclopentane
28.821	MF	83.33839	1.00000	42.56091		2,4-dimethylpentane
30.252	BB +	61.24808	1.00000	31.27939		Benzene
30.736	PB	85.21915	1.00000	43.52142		Cyclohexane
31.180	BV	50.89335	1.00000	25.99123		2-Methylhexane
31.316	VB	109.04791	1.00000	55.69077		2,3-Dimethylpentane
31.749	BB	52.42933	1.00000	26.77566		3-Methylhexane
32.597	BB	62.96000	1.00000	32.15367		2,2,4-Trimethylpentane
33.278	MF	51.47957	1.00000	26.29062		n-Heptane
34.748	BB	64.01354	1.00000	32.69172		Methylcyclohexane
36.575	BB	51.54708	1.00000	26.32509		2,3,4-Trimethylpentane
37.045	MF +	75.89687	1.00000	38.76053		Toluene
37.520	BB	50.13625	1.00000	25.60458		2-Methylheptane
38.025	BB	51.29396	1.00000	26.19582		3-Methylheptane
39.662	VB	58.27401	1.00000	29.76053		n-Octane
43.047	MF	47.24795	1.00000	24.12953		Ethylbenzene
43.553	MF	76.28214	1.00000	38.95729		m/p-Xylene
44.712	PV	66.67661	1.00000	34.05174		Styrene
44.996	VB	50.16097	1.00000	25.61721		o-Xylene
45.789	BB	47.69715	1.00000	24.35894		n-Nonane
46.903	BB	79.66508	1.00000	40.68495		Cumene
48.655	BB	56.87860	1.00000	29.04790		n-Propylbenzene
49.054	BV	48.94999	1.00000	24.99876		m-Ethyltoluene
49.187	VV	79.58132	1.00000	40.64218		p-Ethyltoluene
49.490	VB	50.22721	1.00000	25.65103		1,3,5-Trimethylbenzene
50.140	VB	60.22029	1.00000	30.75450		o-Ethyltoluene
50.981	BB	77.00002	1.00000	39.32391		1,2,4-Trimethylbenzene
51.541	BB	57.35054	1.00000	29.28892		n-Decane
52.606	BB	50.31715	1.00000	25.69697		1,2,3-Trimethylbenzene
53.970	BB	76.97448	1.00000	39.31087		m-Diethylbenzene
54.342	BB	47.28868	1.00000	24.15033		p-Diethylbenzene
56.911	MM +	53.91354	1.00000	27.53365		n-Undecane

Totals : 1824.91467

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
12.062	FM	2.54810	1.00000	1.30131	?	
17.130	MF	8.10755e-1	1.00000	4.14053e-1	?	
18.123	FM	1.91107	1.00000	9.75981e-1	?	
21.140	FM	9.34498e-1	1.00000	4.77248e-1	?	
21.300	PP	4.08646e-1	1.00000	2.08696e-1	?	
28.975	FM	1.81397	1.00000	9.26393e-1	?	
37.218	FM	1.28785	1.00000	6.57706e-1	?	
39.468	BV	5.73210	1.00000	2.92738	?	
43.197	FM	1.50430	1.00000	7.68244e-1	?	
43.782	FM	1.92512	1.00000	9.83159e-1	?	
61.523	BB	47.62742	1.00000	24.32332	?	

Uncalib. totals : 33.96350

Results obtained with enhanced integrator!

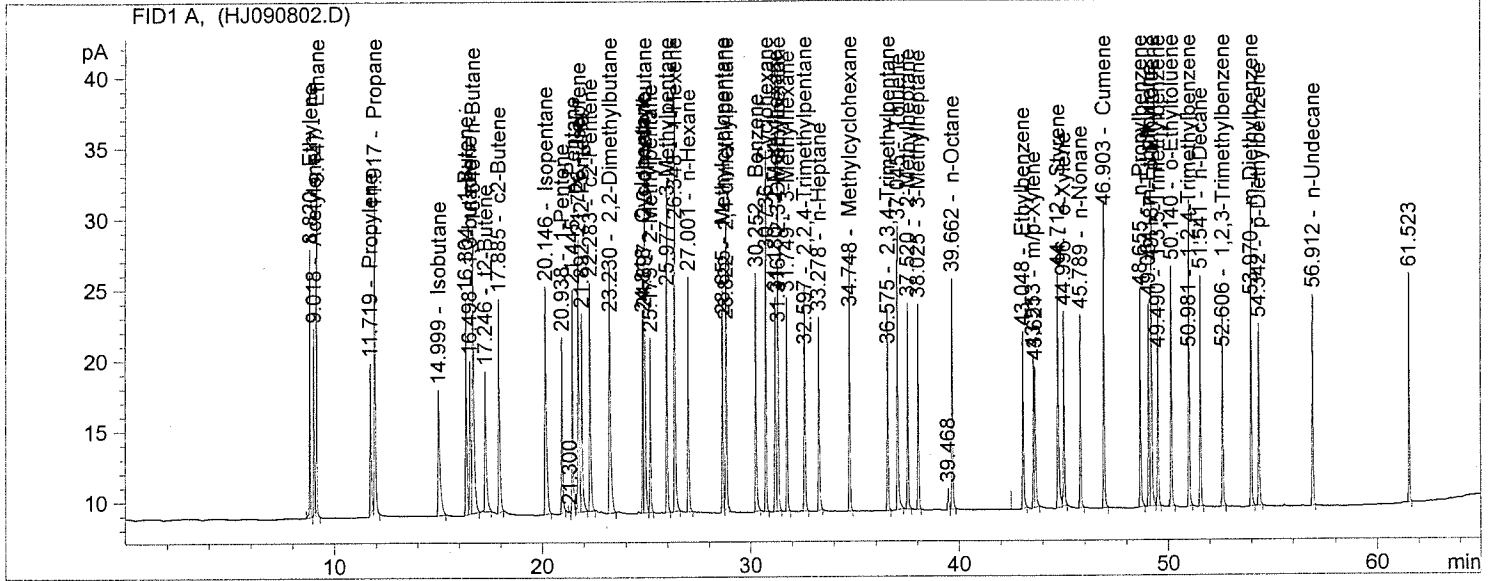
1 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

```

=====
Injection Date   : 10/9/2008 10:23:44 AM      Seq. Line   :    2
Sample Name     : AL22195 $I_PPFID           Location    : Vial 3
Acq. Operator  : JPC                          Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026           Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/9/2008 12:15:17 PM by JPC
                (modified after loading)
    
```

PAMS SAMPLE ANALYSES



External Standard Report

```

=====
Sorted By      :      Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier     :      0.5107
Dilution       :      1.0000
Sample Amount  :      1.00000 [ppbc]   (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.820	BBA	47.14820	1.00000	24.07859		Ethylene
9.018	PB	34.26736	1.00000	17.50034		Acetylene
9.147	BBA	56.03752	1.00000	28.61836		Ethane
11.719	PB	37.91744	1.00000	19.36444		Propylene
11.917	BBA	82.64924	1.00000	42.20897		Propane
14.999	PB +	53.55767	1.00000	27.35190		Isobutane
16.304	BV	61.49738	1.00000	31.40671		1-Butene
16.498	VV	47.68173	1.00000	24.35106		1,3-butadiene
16.646	VB	98.74651	1.00000	50.42984		n-Butane
17.246	BB	50.79647	1.00000	25.94176		t2-Butene
17.885	PB	72.19682	1.00000	36.87092		c2-Butene
20.146	PB	86.29390	1.00000	44.07029		Isopentane
20.938	PB	48.09455	1.00000	24.56189		1-Pentene
21.445	VV	52.67418	1.00000	26.90070		n-Pentene
21.726	VV	75.91888	1.00000	38.77177		Isoprene
21.892	VB	55.23119	1.00000	28.20657		t2-Pentene
22.283	PP	66.45922	1.00000	33.94072		c2-Pentene
23.230	PB	85.71204	1.00000	43.77314		2,2-Dimethylbutane
24.818	BV	39.70129	1.00000	20.27545		Cyclopentane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.897	VV	111.04067	1.00000	56.70847		2,3-dimethylbutane
25.175	VB	44.21571	1.00000	22.58096		2-Methylpentane
25.977	BB	84.06284	1.00000	42.93089		3-Methylpentane
26.348	BB	117.24971	1.00000	59.87943		1-Hexene
27.001	BB	61.30326	1.00000	31.30758		n-Hexane
28.655	PV	52.26686	1.00000	26.69269		Methylcyclopentane
28.822	VB	80.18160	1.00000	40.94874		2,4-dimethylpentane
30.252	BB +	61.24808	1.00000	31.27939		Benzene
30.736	PB	85.21915	1.00000	43.52142		Cyclohexane
31.180	BV	50.89335	1.00000	25.99123		2-Methylhexane
31.316	VB	109.04791	1.00000	55.69077		2,3-Dimethylpentane
31.749	BB	52.42933	1.00000	26.77566		3-Methylhexane
32.597	BB	62.96000	1.00000	32.15367		2,2,4-Trimethylpentane
33.278	PB	50.60601	1.00000	25.84449		n-Heptane
34.748	BB	64.01354	1.00000	32.69172		Methylcyclohexane
36.575	BB	51.54708	1.00000	26.32509		2,3,4-Trimethylpentane
37.045	BB +	77.18384	1.00000	39.41779		Toluene
37.520	BB	50.13625	1.00000	25.60458		2-Methylheptane
38.025	BB	51.29396	1.00000	26.19582		3-Methylheptane
39.662	VB	58.27401	1.00000	29.76053		n-Octane
43.048	PB	46.80545	1.00000	23.90354		Ethylbenzene
43.553	PV	34.56858	1.00000	17.65417		m/p-Xylene
44.712	PV	66.67661	1.00000	34.05174		Styrene
44.996	VB	50.16097	1.00000	25.61721		o-Xylene
45.789	BB	47.69715	1.00000	24.35894		n-Nonane
46.903	BB	79.66508	1.00000	40.68495		Cumene
48.655	BB	56.87860	1.00000	29.04790		n-Propylbenzene
49.054	BV	48.94999	1.00000	24.99876		m-Ethyltoluene
49.187	VV	79.58132	1.00000	40.64218		p-Ethyltoluene
49.490	VB	50.22721	1.00000	25.65103		1,3,5-Trimethylbenzene
50.140	VB	60.22029	1.00000	30.75450		o-Ethyltoluene
50.981	BB	77.00002	1.00000	39.32391		1,2,4-Trimethylbenzene
51.541	BB	57.35054	1.00000	29.28892		n-Decane
52.606	BB	50.31715	1.00000	25.69697		1,2,3-Trimethylbenzene
53.970	BB	76.97448	1.00000	39.31087		m-Diethylbenzene
54.342	BB	47.28868	1.00000	24.15033		p-Diethylbenzene
56.912	BB +	53.52686	1.00000	27.33617		n-Undecane

Totals : 1793.39645

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
21.300	PP	4.08646e-1	1.00000	2.08696e-1	?	
39.468	BV	5.73210	1.00000	2.92738	?	
43.621	VB	41.12904	1.00000	21.00460	?	
61.523	BB	47.62742	1.00000	24.32332	?	

Uncalib. totals : 48.46401

Results obtained with enhanced integrator!

1 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

\*\*\* End of Report \*\*\*

GC/FID Daily Worksheet FID 2  
Date Oct. 15, 2008 Operator JAK  
Batch # 193024(A) QC # AL22735

Dup = AL 22014  
(Part 2)

**Working Gases and Quality Control Standards:**

Carrier Gas Helium Pressure 2100/200 Pulse Gas Pressure 15.0  
Combustion Air Pressure 97.0 Hydrogen Pressure 55.0  
Nitrogen Pressure for dewar 30.0  
ZAB Pressure 26.0; Preparation Date 10-2-08; Canister ID G-CR 44  
HAB Pressure 20.5; Preparation date 10-6-08; Canister ID G-CR 24  
LCS: Std ID 1057610175; Preparation Date 10-7-08; Pressure 26.5;  
- Canister ID S1404  
PAMS: Std ID CC250112; Preparation Date 10-2-08; Pressure 26.5;  
Canister ID: G-1152  
SRM: Std ID CC162783; Preparation Date 10-2-08; Pressure 24.5;  
Canister ID G-1124

**Entech Setup:**

Name of Sequence: 101508  
Sequence Saved? Y Sequence Printed? Y  
Leak Check Performed? Y

**GC/FID Chemstation Setup:**

Name of Sequence: 10-15-08  
Sequence Saved? Y Sequence Printed? Y  
Bakeout.M Loaded at End? Y

**Acquisition Startup:**

Do Both Sequences Match? Y Canister Valves Open? X  
Entech Sequence Started? Y Chemstation Sequence Started? Y

**Total Runs in the sequences:**

Number of Std: 3  
Number of Blanks: 2  
Number of Samples: 17  
Number of Duplicates: 3  
Number of Sys Blanks: 2  
Number of Cert Cans: 0  
Total Runs in the sequences: 27

Date and Time Sequence Started: 10/15/08 8:00AM

Comments: RE Boot: N<sub>2</sub> / close + Reopen - Y's / Chemstation OFFLINE ONLINE  
OFFLINE had A "FATAL EXCEPTION"  
ON 10-14-08

Site/Desc	Run Date	Part #	CANID#	LIMS#	AnalysisCode #	DataFile#
SRM	Oct. 15, 2008	S1	G1124	AL22735	\$I-SRM	HJ150801 ✓
PAMS		1-1	G1152		\$L-PPFID	2 ✓
HAB		S3	GCR24		\$HS-PPFID	3 ✓ 1.8
LCS		16	S1404		\$LL-PPFID	4 X Re-run
ZAB		S4	GCR44		\$B-PPFID	5 ✓ 1.8
*PAL	10-3-08	2	G1269	AL22014	\$PPFID	6 ✓
T3 GRAB	9-25-08	3	S1372	AL21642		7 ✓
T4 GRAB	9-25-08	4	S1418	643		8 ✓
T5 GRAB	9-25-08	5	S1392	644		9 ✓
T6 GRAB	9-25-08	6	S1502	645		10 ✓
T7 GRAB	9-25-08	7	S1375	646		11 ✓
T8 GRAB	9-26-08	8	S1470	691		12 ✓
T25 GRAB	9-26-08	9	S1478	692		13 ✓
T20 GRAB	9-26-08	10	S1418	693		14 ✓
SysBlk	10-15-08	0		AL22735	\$SYSBLK	15 ✓ 2.2
Dup/PAL	10-3-08	2	G1269	AL22014	\$D-PPFID	16 ✓
cont	10-15-08	S1	G1124	AL22735	\$C-SRM	17 ✓
T11 GRAB	9-26-08	11	S1394	AL21694	\$PPFID	18 ✓
T15 GRAB	9-26-08	12	S1348	AL21696	AA	19 ✓
T16 GRAB	9-26-08	13	S1431	AL21697		20 ✓
T17 GRAB	9-26-08	14	S1347	AL21698		21 ✓
T18 GRAB	9-27-08	15	S1376	AL21699		22 ✓
T19 GRAB	9-27-08	2	S1482	AL21700		23 ✓
T20 GRAB	9-28-08	3	S1462	AL21701		24 ✓
T22 GRAB	9-28-08	4	S1359	AL21702		25 Re-run
SysBlk	10-15-08	0		AL22735	\$SYSBLK	26 ✓ 2.3
cont	10-15-08	S1	G1124	AL22735	\$C-SRM	27 ✓
LCS	10-15-08	S3	S1452	AL22735	\$LL-PPFID	28 ✓
SysBlk	10-15-08	0		AL22735	\$SYSBLK	29 ✓ 2.2
BobSTD	10-16-08	1	SERIAL#1574	BobSTD	\$PPFID	30 Re-run
Bob STD	10-16-08	1	SERIAL#1574	BobSTD		31 ✓
T22 GRAB	9-28-0	4	S1359	AL21702		32 ✓
SysBlk	10-15-08	0		AL22735	\$SYSBLK	33 ✓
T20 GRAB	9-26-08	10	S1418	AL21693	\$PPFID	33 X
cont	10-15-08	S1	S1124	AL22735	\$C-PPFID	34 ✓

\* : Autosampler positions not correct, re-load program and re-run. Replaced Power Supply on Tower Oct. 15, 08  
 JAK

CH SIGNATURE  
 READ AND UNDERSTOOD

DATE Oct. 15, 2008  
 DATE 20

----- Leak Check Report -----

10/15/2008 7:59:09 AM  
Leak Check for C:\Smart\SQ101508.SEQ  
Report File: C:\Smart\SQ101508.LCR  
Leak Check Method: Evacuation  
Pressurize/Evacuate time(sec) 30  
Equilibration time(sec) 10  
Maintanance time(sec) 30

Sample	Inlet	Auto1	Auto2	Auto3	Start	End	Rate(psi/min)
1	1	---	---	0.6	0.6	0.00	
3	1	---	---	0.3	0.4	0.20	
1	16	---	---	0.5	0.6	0.20	
4	16	---	---	0.3	0.4	0.20	
1	2	---	---	0.4	0.5	0.20	
1	3	---	---	0.4	0.4	0.00	
1	4	---	---	0.4	0.4	0.00	
1	5	---	---	0.3	0.4	0.20	
1	6	---	---	0.3	0.4	0.20	
1	7	---	---	0.3	0.4	0.20	
1	8	---	---	0.3	0.4	0.20	
1	9	---	---	0.3	0.4	0.20	
1	10	---	---	0.4	0.4	0.00	
1	11	---	---	0.4	0.4	0.00	
1	12	---	---	0.4	0.4	0.00	
1	13	---	---	0.4	0.5	0.20	
1	14	---	---	0.4	0.4	0.00	
1	15	---	---	0.4	0.4	0.00	

-----SEQUENCE TABLE -----

Sequence Name: C:\Smart\SQ101508.SEQ  
 Date: 10-17-2008  
 Time: 12:05:16  
 Int. Std Volume: 0 cc

Sample Name	Inlet #	Auto #	Samp Pos	Cal Vol.	Std Vol.	Method	Time
AL22735 \$I_SRM	1	1	1	0	200	C:\Smart\PAMS.MPT	12:00
AL22735 \$I_PPFID	1	1	1	200	0	C:\Smart\PAMS.MPT	12:00
AL22735 \$HBPPFID	3	1	200	0		C:\Smart\PAMS.MPT	12:00
AL22735 \$L1PPFID	1	16	200	0		C:\Smart\PAMS.MPT	12:00
AL22735 \$B_PPFID	4	1	200	0		C:\Smart\PAMS.MPT	12:00
AL22014 \$PPFID	1	2	200	0		C:\Smart\PAMS.MPT	12:00
AL21642 \$PPFID	1	3	40	0		C:\Smart\PAMS.MPT	12:00
AL21643 \$PPFID	1	4	40	0		C:\Smart\PAMS.MPT	12:00
AL21644 \$PPFID	1	5	40	0		C:\Smart\PAMS.MPT	12:00
AL21645 \$PPFID	1	6	40	0		C:\Smart\PAMS.MPT	12:00
AL21646 \$PPFID	1	7	40	0		C:\Smart\PAMS.MPT	12:00
AL21691 \$PPFID	1	8	40	0		C:\Smart\PAMS.MPT	12:00
AL21692 \$PPFID	1	9	40	0		C:\Smart\PAMS.MPT	12:00
AL21693 \$PPFID	1	10	40	0		C:\Smart\PAMS.MPT	12:00
AL22735 \$SYSBLNK	1	1	0	0		C:\Smart\PAMS.MPT	12:00
AL22014 \$D_PPFID	1	2	200	0		C:\Smart\PAMS.MPT	12:00
AL22735 \$C_SRM	1	1	0	200		C:\Smart\PAMS.MPT	12:00
AL21694 \$PPFID	1	11	40	0		C:\Smart\PAMS.MPT	12:00
AL21696 \$PPFID	1	12	40	0		C:\Smart\PAMS.MPT	12:00
AL21697 \$PPFID	1	13	40	0		C:\Smart\PAMS.MPT	12:00
AL21698 \$PPFID	1	14	40	0		C:\Smart\PAMS.MPT	12:00
AL21699 \$PPFID	1	15	40	0		C:\Smart\PAMS.MPT	12:00
AL21700 \$PPFID	1	2	40	0		C:\Smart\PAMS.MPT	12:00
AL21701 \$PPFID	1	3	40	0		C:\Smart\PAMS.MPT	12:00
AL21702 \$PPFID	1	4	40	0		C:\Smart\PAMS.MPT	12:00
AL22735 \$SYSBLNK	1	1	0	0		C:\Smart\PAMS.MPT	12:00
AL22735 \$C_SRM	1	1	0	200		C:\Smart\PAMS.MPT	12:00
AL22735 \$L1PPFID	3	1	200	0		C:\Smart\PAMS.MPT	12:00
AL22735 \$SYSBLNK	1	1	0	0		C:\Smart\PAMS.MPT	12:00
BOBSTD \$PPFID	1	1	200	0		C:\Smart\PAMS.MPT	12:00
BOBSTD \$PPFID	1	1	200	0		C:\Smart\PAMS.MPT	12:00
AL21702 \$PPFID	1	4	40	0		C:\Smart\PAMS.MPT	12:00
AL21693 \$PPFID	1	10	40	0		C:\Smart\PAMS.MPT	12:00
AL22735 \$C_SRM	1	1	0	200		C:\Smart\PAMS.MPT	12:00

Sequence Parameters:

Operator: JAK

Data File Naming: Prefix/Counter

Signal 1 Prefix: HJ1508

Counter: 01

Signal 2 Prefix: 0

Counter: 0000000

Data Directory: C:\HPCHEM\1\DATA\

Data Subdirectory:

Part of Methods to run: According to Runtime Checklist

Barcode Reader: not used

Shutdown Cmd/Macro: none

Sequence Comment:  
PAL & 16 BARGE GRAB SAMPLES.

Sequence Table (Front Injector):

Method and Injection Info Part:

Line	Location	SampleName	Method	Inj	SampleType	InjVolume	DataFile
1	Vial 1	AL22735 \$I_SRM	PAMS	1	Calib		
2	Vial 3	AL22735 \$I_PPFID	PAMS	1	Calib		
3	Vial 2	AL22735 \$HBPPFID	PAMS	1	Ctrl Samp		
4	Vial 4	AL22735 \$L1PPFID	PAMS	1	Ctrl Samp		
5	Vial 1	AL22735 \$B_PPFID	PAMS	1	Ctrl Samp		
6	Vial 2	AL22014 \$PPFID	PAMS	1	Sample		
7	Vial 3	AL21642 \$PPFID	PAMS	1	Sample		
8	Vial 4	AL21643 \$PPFID	PAMS	1	Sample		
9	Vial 5	AL21644 \$PPFID	PAMS	1	Sample		
10	Vial 6	AL21645 \$PPFID	PAMS	1	Sample		
11	Vial 7	AL21646 \$PPFID	PAMS	1	Sample		
12	Vial 8	AL21691 \$PPFID	PAMS	1	Sample		
13	Vial 9	AL21692 \$PPFID	PAMS	1	Sample		
14	Vial 10	AL21693 \$PPFID	PAMS	1	Sample		
15	Vial 0	AL22525 \$\$SYSBLNK	PAMS	1	Calib		
16	Vial 2	AL22014 \$D_PPFID	PAMS	1	Sample		
17	Vial 1	AL22735 \$C_SRM	PAMS	1	Calib		
18	Vial 11	AL21694 \$PPFID	PAMS	1	Sample		
19	Vial 12	AL21696 \$PPFID	PAMS	1	Sample		
20	Vial 13	AL21697 \$PPFID	PAMS	1	Sample		
21	Vial 14	AL21698 \$PPFID	PAMS	1	Sample		
22	Vial 15	AL21699 \$PPFID	PAMS	1	Sample		
23	Vial 2	AL21700 \$PPFID	PAMS	1	Sample		
24	Vial 3	AL21701 \$PPFID	PAMS	1	Sample		
25	Vial 4	AL21702 \$PPFID	PAMS	1	Sample		
26	Vial 0	AL22735 \$\$SYSBLNK	PAMS	1	Calib		
27	Vial 1	AL22735 \$C_SRM	PAMS	1	Calib		
28	Vial 1	BAKEOUT	BAKEOUT	1	Sample		

*Batch modified  
- see logbook copy  
m  
11/24/08*

Sequence Table (Back Injector):

No entries - empty table!

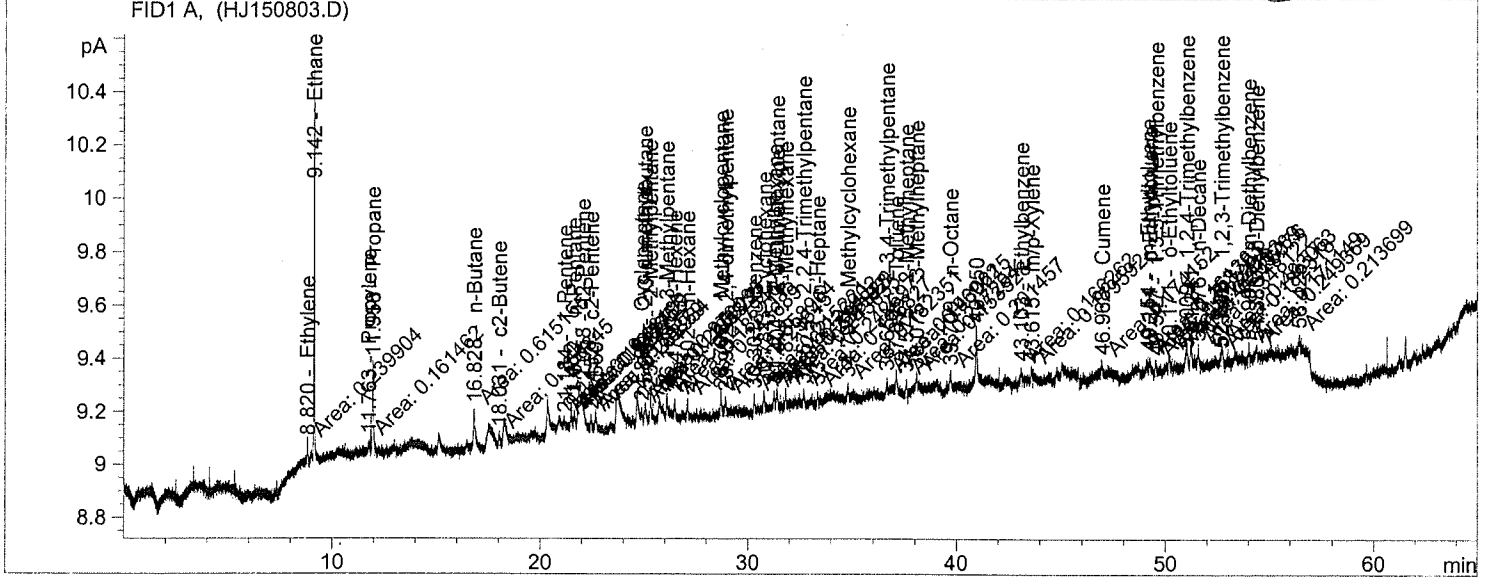


```

=====
Injection Date : 10/15/2008 10:56:16 AM      Seq. Line : 3
Sample Name    : AL22735 $HBPPFID            Location  : Vial 2
Acq. Operator  : JAK                          Inj       : 1
Acq. Instrument: HP_FID2 SOP 1026            Inj Volume: Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method: C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/15/2008 6:38:05 AM by JAK
                (modified after loading)
=====

```

PAMS SAMPLE ANALYSES



```

=====
External Standard Report
=====

```

```

Sorted By      : Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier     : 0.5107
Dilution       : 1.0000
Sample Amount  : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs

```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.820	MM	2.39904e-1	1.00000	1.22519e-1		Ethylene
8.929		-	-	-		Acetylene
9.142	BBA	3.47531	1.00000	1.77484		Ethane
11.763	MM	1.61462e-1	1.00000	8.24585e-2		Propylene
11.958	BBA	1.21404	1.00000	6.20009e-1		Propane
15.083		-	-	-		Isobutane
16.372		-	-	-		1-Butene
16.527		-	-	-		1,3-butadiene
16.828	MM	6.15155e-1	1.00000	3.14160e-1		n-Butane
17.392		-	-	-		t2-Butene
18.031	MM	1.56845e-1	1.00000	8.01010e-2		c2-Butene
20.190		-	-	-		Isopentane
21.184	MM	1.64445e-1	1.00000	8.39820e-2		1-Pentene
21.632	MM	2.12765e-1	1.00000	1.08659e-1		n-Pentane
21.745		-	-	-		Isoprene
22.058	MM	1.81990e-1	1.00000	9.29422e-2		t2-Pentene
22.452	MM	1.78859e-1	1.00000	9.13431e-2		c2-Pentene
23.376		-	-	-		2,2-Dimethylbutane
24.880	MM	1.10830e-1	1.00000	5.66008e-2		Cyclopentane

10-15-08  
JAK

M

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.043	MM	2.05822e-1	1.00000	1.05113e-1		2,3-dimethylbutane
25.301	MM	2.79095e-1	1.00000	1.42534e-1		2-Methylpentane
26.100	MM	2.17946e-1	1.00000	1.11305e-1		3-Methylpentane
26.479	MM	1.88211e-1	1.00000	9.61193e-2		1-Hexene
27.102	MM	2.43689e-1	1.00000	1.24452e-1		n-Hexane
28.705	MM	3.58964e-1	1.00000	1.83323e-1		Methylcyclopentane
28.932	MM	2.96450e-1	1.00000	1.51397e-1		2,4-dimethylpentane
30.301	MM +	2.15221e-1	1.00000	1.09914e-1		Benzene
30.781	MM	2.26902e-1	1.00000	1.15879e-1		Cyclohexane
31.277	MM	2.24192e-1	1.00000	1.14495e-1		2-Methylhexane
31.401	MM	3.15928e-1	1.00000	1.61344e-1		2,3-Dimethylpentane
31.815	MM	2.43635e-1	1.00000	1.24424e-1		3-Methylhexane
32.674	MM	2.42697e-1	1.00000	1.23945e-1		2,2,4-Trimethylpentane
33.353	MM	1.96827e-1	1.00000	1.00520e-1		n-Heptane
34.799	MM	1.82351e-1	1.00000	9.31268e-2		Methylcyclohexane
36.654	MM	1.96062e-1	1.00000	1.00129e-1		2,3,4-Trimethylpentane
37.095	MM +	4.30215e-1	1.00000	2.19711e-1		Toluene
37.575	MM	2.17294e-1	1.00000	1.10972e-1		2-Methylheptane
38.075	MM	1.53528e-1	1.00000	7.84070e-2		3-Methylheptane
39.709	MM	2.01457e-1	1.00000	1.02884e-1		n-Octane
43.103	MM	1.66262e-1	1.00000	8.49100e-2		Ethylbenzene
43.615	MM	1.79592e-1	1.00000	9.17174e-2		m/p-Xylene
44.773		-	-	-		Styrene
45.056		-	-	-		o-Xylene
45.843		-	-	-		n-Nonane
46.968	MM	1.74152e-1	1.00000	8.89396e-2		Cumene
48.663		-	-	-		n-Propylbenzene
49.154	MM	1.61363e-1	1.00000	8.24079e-2		m-Ethyltoluene
49.241	MM	1.58781e-1	1.00000	8.10894e-2		p-Ethyltoluene
49.547	MM	2.17294e-1	1.00000	1.10972e-1		1,3,5-Trimethylbenzene
50.171	MM	2.24793e-1	1.00000	1.14802e-1		o-Ethyltoluene
51.009	MM	2.93789e-1	1.00000	1.50038e-1		1,2,4-Trimethylbenzene
51.576	MM	3.48122e-1	1.00000	1.77786e-1		n-Decane
52.712	FM	4.03063e-1	1.00000	2.05844e-1		1,2,3-Trimethylbenzene
53.997	MM	1.71149e-1	1.00000	8.74056e-2		m-Diethylbenzene
54.380	MM	2.49369e-1	1.00000	1.27353e-1		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 7.30087

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
21.482	MM	1.95602e-1	1.00000	9.98937e-2	?	
22.660	MM	2.82934e-1	1.00000	1.44495e-1	?	
40.950	BB	8.20845e-1	1.00000	4.19206e-1	?	
51.241	MM	3.26076e-1	1.00000	1.66527e-1	?	
52.636	MF	1.32318e-1	1.00000	6.75746e-2	?	
56.425	MM	2.13699e-1	1.00000	1.09136e-1	?	

Uncalib. totals : 1.00683

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

=====  
\*\*\* End of Report \*\*\*

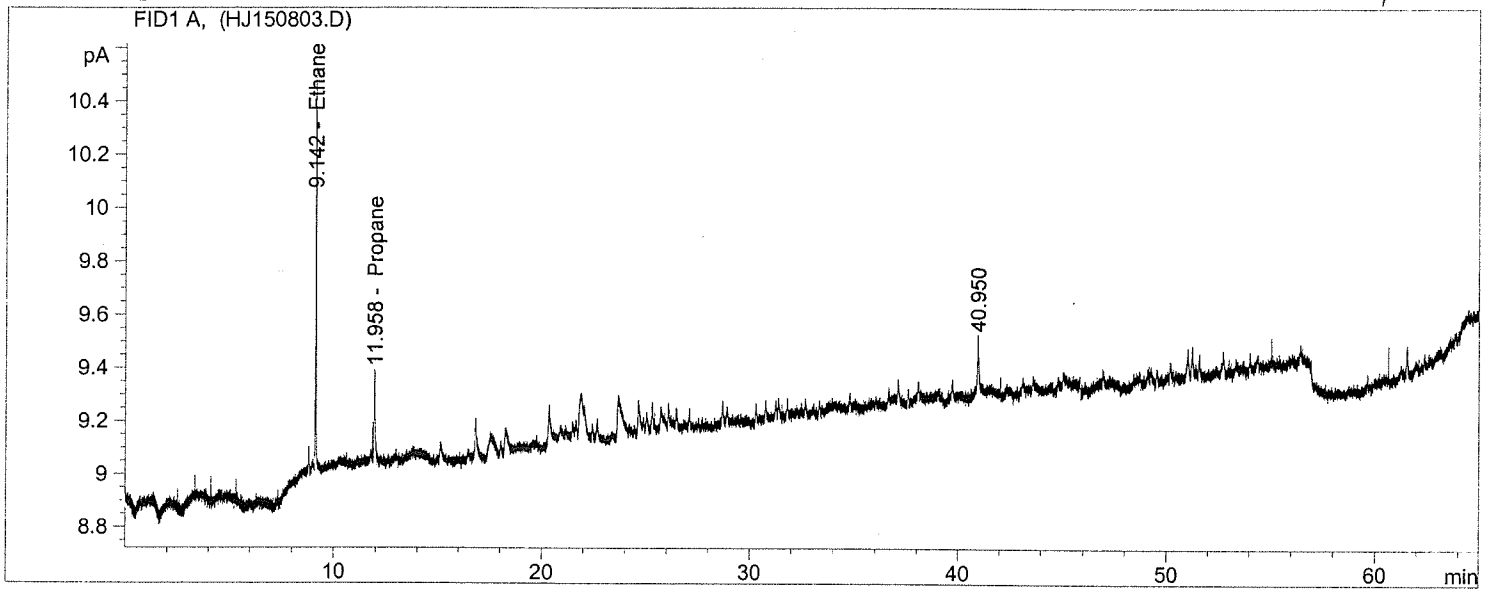
```

=====
Injection Date   : 10/15/2008 10:56:16 AM      Seq. Line   :    3
Sample Name     : AL22735 $HBPPFID             Location    : Vial 2
Acq. Operator  : JAK                           Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026             Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/15/2008 6:38:05 AM by JAK
                (modified after loading)

```

ECR24

PAMS SAMPLE ANALYSES



```

=====
External Standard Report
=====

```

```

Sorted By           :      Signal
Calib. Data Modified :      8/4/2008 10:57:02 AM
Multiplier          :      0.5107
Dilution            :      1.0000
Sample Amount       :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs

```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.837		-	-	-		Ethylene
8.950		-	-	-		Acetylene
9.142	BBA	3.47531	1.00000	1.77484		Ethane
11.762		-	-	-		Propylene
11.958	BBA	1.21404	1.00000	6.20009e-1		Propane
15.083		-	-	-		Isobutane
16.411		-	-	-		1-Butene
16.566		-	-	-		1,3-butadiene
16.751		-	-	-		n-Butane
17.433		-	-	-		t2-Butene
18.083		-	-	-		c2-Butene
20.238		-	-	-		Isopentane
21.060		-	-	-		1-Pentene
21.657		-	-	-		n-Pentane
21.797		-	-	-		Isoprene
22.050		-	-	-		t2-Pentene
22.420		-	-	-		c2-Pentene
23.432		-	-	-		2,2-Dimethylbutane
24.903		-	-	-		Cyclopentane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.101		-	-	-		2,3-dimethylbutane
25.385		-	-	-		2-Methylpentane
26.200		-	-	-		3-Methylpentane
26.576		-	-	-		1-Hexene
27.237		-	-	-		n-Hexane
28.764		-	-	-		Methylcyclopentane
28.914		-	-	-		2,4-dimethylpentane
30.373		-	-	-		Benzene
31.008		-	-	-		Cyclohexane
31.348		-	-	-		2-Methylhexane
31.584		-	-	-		2,3-Dimethylpentane
32.010		-	-	-		3-Methylhexane
32.869		-	-	-		2,2,4-Trimethylpentane
33.543		-	-	-		n-Heptane
35.039		-	-	-		Methylcyclohexane
36.868		-	-	-		2,3,4-Trimethylpentane
37.101		-	-	-		Toluene
37.806		-	-	-		2-Methylheptane
38.313		-	-	-		3-Methylheptane
39.949		-	-	-		n-Octane
43.059		-	-	-		Ethylbenzene
43.617		-	-	-		m/p-Xylene
44.781		-	-	-		Styrene
45.064		-	-	-		o-Xylene
45.851		-	-	-		n-Nonane
46.921		-	-	-		Cumene
48.671		-	-	-		n-Propylbenzene
49.070		-	-	-		m-Ethyltoluene
49.350		-	-	-		p-Ethyltoluene
49.565		-	-	-		1,3,5-Trimethylbenzene
50.165		-	-	-		o-Ethyltoluene
50.999		-	-	-		1,2,4-Trimethylbenzene
51.558		-	-	-		n-Decane
52.863		-	-	-		1,2,3-Trimethylbenzene
54.045		-	-	-		m-Diethylbenzene
54.417		-	-	-		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 2.39485

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
40.950	BB	8.20845e-1	1.00000	4.19206e-1	?	

Uncalib. totals : 4.19206e-1

Results obtained with enhanced integrator!  
2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)  
Warning : Time reference compound(s) not found

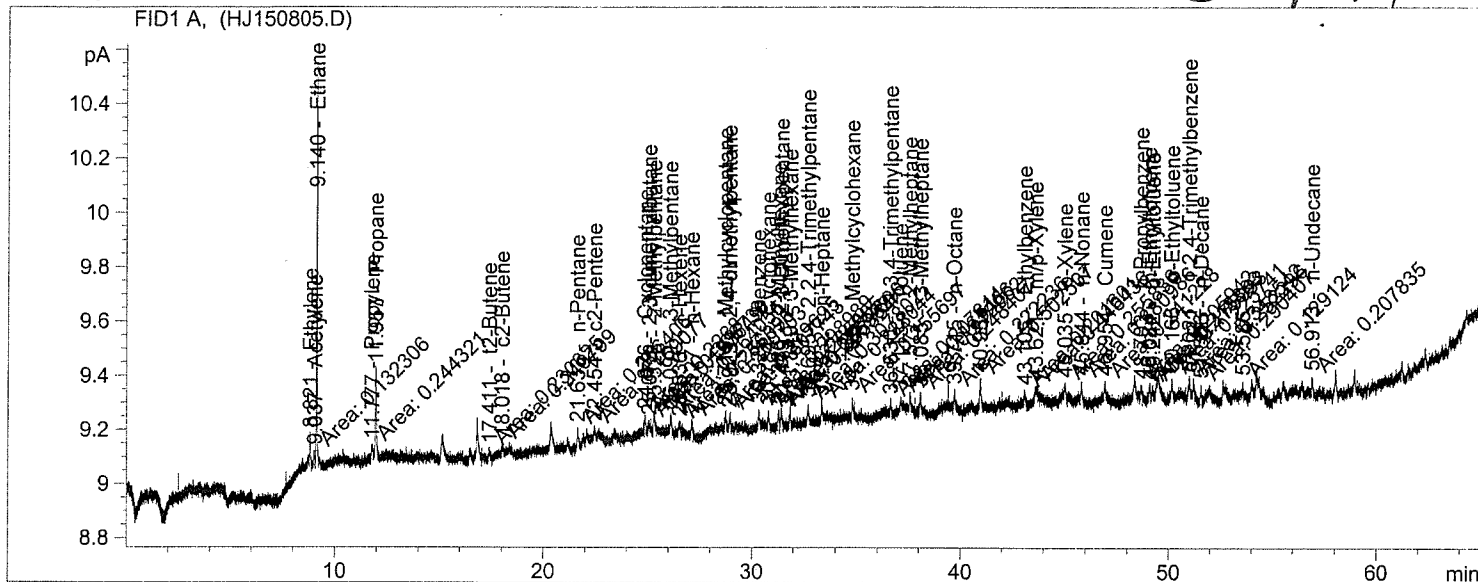
\*\*\* End of Report \*\*\*

```

=====
Injection Date : 10/15/2008 1:35:11 PM      Seq. Line : 5
Sample Name    : AL22735 $B_PPFID           Location  : Vial 1
Acq. Operator  : JAK                        Inj       : 1
Acq. Instrument: HP_FID2 SOP 1026          Inj Volume: Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method: C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/15/2008 3:00:39 PM by JAK
                (modified after loading)
    
```

ECR44

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By      : Signal
Calib. Data Modified : 10/15/2008 3:00:43 PM
Multiplier     : 0.5107
Dilution       : 1.0000
Sample Amount  : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.821	BBA	2.74667e-1	1.00000	1.40272e-1		Ethylene
9.037	MM	1.32306e-1	1.00000	6.75686e-2		Acetylene
9.140	BBA	3.42998	1.00000	1.75169		Ethane
11.777	MM	2.44321e-1	1.00000	1.24775e-1		Propylene
11.957	PBA	1.10603	1.00000	5.64852e-1		Propane
15.083		-	-	-		Isobutane
16.385		-	-	-		1-Butene
16.540		-	-	-		1,3-butadiene
16.725		-	-	-		n-Butane
17.411	MM	2.30825e-1	1.00000	1.17882e-1		t2-Butene
18.018	MM	2.49799e-1	1.00000	1.27572e-1		c2-Butene
20.206		-	-	-		Isopentane
21.027		-	-	-		1-Pentene
21.633	MM	2.56406e-1	1.00000	1.30946e-1		n-Pentane
21.763		-	-	-		Isoprene
22.015		-	-	-		t2-Pentene
22.454	MM	1.69077e-1	1.00000	8.63477e-2		c2-Pentene
23.395		-	-	-		2,2-Dimethylbutane
24.876	MM	2.26800e-1	1.00000	1.15827e-1		Cyclopentane

10-15-08  
JAK

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.079	MM	1.33649e-1	1.00000	6.82545e-2		2,3-dimethylbutane
25.328	MM	3.08738e-1	1.00000	1.57672e-1		2-Methylpentane
26.092	MM	2.64055e-1	1.00000	1.34853e-1		3-Methylpentane
26.536	MM	2.56096e-1	1.00000	1.30788e-1		1-Hexene
27.127	MM	2.60703e-1	1.00000	1.33141e-1		n-Hexane
28.719	MM	2.79695e-1	1.00000	1.42840e-1		Methylcyclopentane
28.929	MM	3.07743e-1	1.00000	1.57164e-1		2,4-dimethylpentane
30.325	MM	2.98989e-1	1.00000	1.52694e-1		Benzene
30.784	MM	2.66905e-1	1.00000	1.36308e-1		Cyclohexane
31.286	MF	2.86962e-1	1.00000	1.46552e-1		2-Methylhexane
31.419	FM	3.55854e-1	1.00000	1.81735e-1		2,3-Dimethylpentane
31.849	MM	2.77696e-1	1.00000	1.41819e-1		3-Methylhexane
32.695	MM	3.07802e-1	1.00000	1.57194e-1		2,2,4-Trimethylpentane
33.332	MM	2.28044e-1	1.00000	1.16462e-1		n-Heptane
34.795	MM	2.55697e-1	1.00000	1.30584e-1		Methylcyclohexane
36.630	MM	2.07814e-1	1.00000	1.06130e-1		2,3,4-Trimethylpentane
37.113	MM	1.65466e-1	1.00000	8.45036e-2		Toluene
37.577	MM	2.12952e-1	1.00000	1.08754e-1		2-Methylheptane
38.085	MM	2.48407e-1	1.00000	1.26862e-1		3-Methylheptane
39.715	MM	2.22236e-1	1.00000	1.13496e-1		n-Octane
43.105	MM	2.01601e-1	1.00000	1.02958e-1		Ethylbenzene
43.621	MM	4.46436e-1	1.00000	2.27995e-1		m/p-Xylene
44.781		-	-	-		Styrene
45.035	MM	2.55836e-1	1.00000	1.30655e-1		o-Xylene
45.844	MM	3.80986e-1	1.00000	1.94569e-1		n-Nonane
46.954	MM	2.41228e-1	1.00000	1.23195e-1		Cumene
48.703	MM	2.05942e-1	1.00000	1.05174e-1		n-Propylbenzene
49.084	MM	2.18883e-1	1.00000	1.11783e-1		m-Ethyltoluene
49.242	MM	1.75993e-1	1.00000	8.98797e-2		p-Ethyltoluene
49.558		-	-	-		1,3,5-Trimethylbenzene
50.166	MM	2.25741e-1	1.00000	1.15286e-1		o-Ethyltoluene
51.021	MM	3.48542e-1	1.00000	1.78001e-1		1,2,4-Trimethylbenzene
51.566	MM	2.90407e-1	1.00000	1.48311e-1		n-Decane
52.851		-	-	-		1,2,3-Trimethylbenzene
54.032		-	-	-		m-Diethylbenzene
54.403		-	-	-		p-Diethylbenzene
56.913	MM	2.07835e-1	1.00000	1.06141e-1		n-Undecane

Totals : 7.48949

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
40.954	MM	5.02507e-1	1.00000	2.56630e-1		?
51.222	MM	2.52296e-1	1.00000	1.28847e-1		?
53.585	MM	1.29124e-1	1.00000	6.59434e-2		?

Uncalib. totals : 4.51421e-1

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

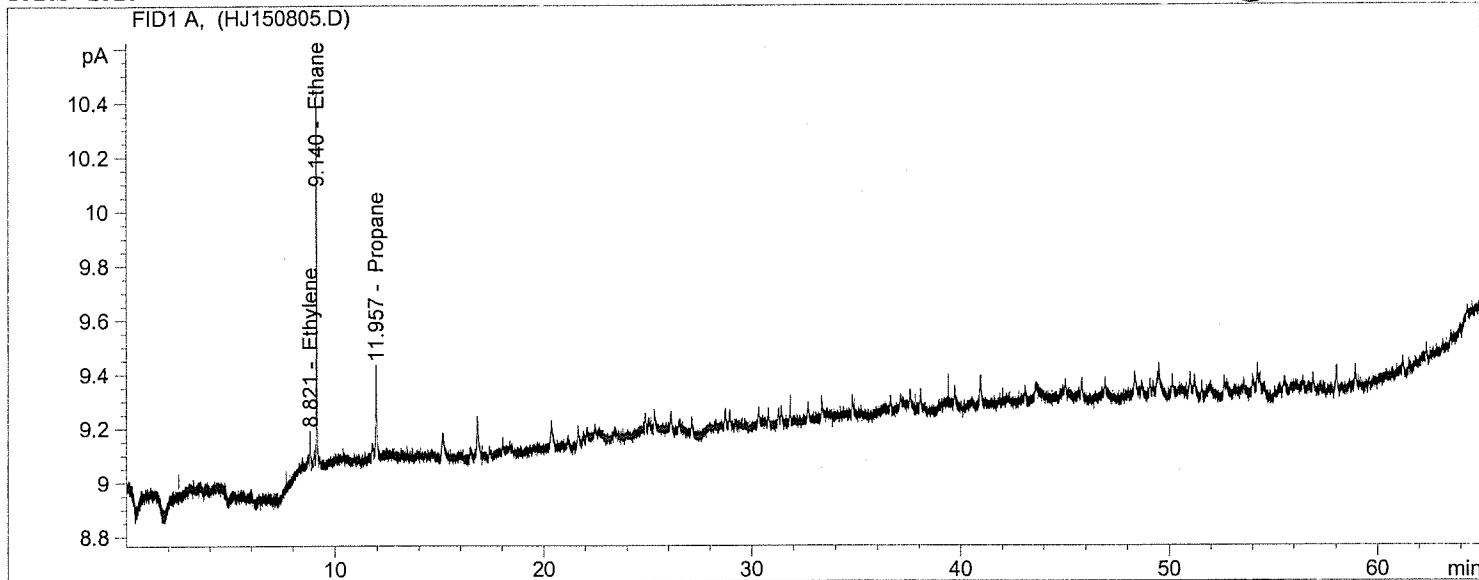
\*\*\* End of Report \*\*\*

```

=====
Injection Date : 10/15/2008 1:35:11 PM      Seq. Line : 5
Sample Name    : AL22735 $B_PPFID           Location  : Vial 1
Acq. Operator  : JAK                        Inj       : 1
Acq. Instrument: HP_FID2 SOP 1026          Inj Volume: Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method: C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/15/2008 3:00:39 PM by JAK
                (modified after loading)
    
```

GCR44

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By      : Signal
Calib. Data Modified : 10/15/2008 3:00:43 PM
Multiplier     : 0.5107
Dilution       : 1.0000
Sample Amount  : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.821	BBA	2.74667e-1	1.00000	1.40272e-1		Ethylene
9.000		-	-	-		Acetylene
9.140	BBA	3.42998	1.00000	1.75169		Ethane
11.762		-	-	-		Propylene
11.957	PBA	1.10603	1.00000	5.64852e-1		Propane
15.083		-	-	-		Isobutane
16.411		-	-	-		1-Butene
16.566		-	-	-		1,3-butadiene
16.751		-	-	-		n-Butane
17.433		-	-	-		t2-Butene
18.083		-	-	-		c2-Butene
20.238		-	-	-		Isopentane
21.060		-	-	-		1-Pentene
21.657		-	-	-		n-Pentane
21.797		-	-	-		Isoprene
22.050		-	-	-		t2-Pentene
22.420		-	-	-		c2-Pentene
23.432		-	-	-		2,2-Dimethylbutane
24.903		-	-	-		Cyclopentane

4

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.101	-	-	-	-	-	2,3-dimethylbutane
25.385	-	-	-	-	-	2-Methylpentane
26.200	-	-	-	-	-	3-Methylpentane
26.576	-	-	-	-	-	1-Hexene
27.237	-	-	-	-	-	n-Hexane
28.764	-	-	-	-	-	Methylcyclopentane
28.914	-	-	-	-	-	2,4-dimethylpentane
30.373	-	-	-	-	-	Benzene
31.008	-	-	-	-	-	Cyclohexane
31.348	-	-	-	-	-	2-Methylhexane
31.584	-	-	-	-	-	2,3-Dimethylpentane
32.010	-	-	-	-	-	3-Methylhexane
32.869	-	-	-	-	-	2,2,4-Trimethylpentane
33.543	-	-	-	-	-	n-Heptane
35.039	-	-	-	-	-	Methylcyclohexane
36.868	-	-	-	-	-	2,3,4-Trimethylpentane
37.101	-	-	-	-	-	Toluene
37.806	-	-	-	-	-	2-Methylheptane
38.313	-	-	-	-	-	3-Methylheptane
39.949	-	-	-	-	-	n-Octane
43.059	-	-	-	-	-	Ethylbenzene
43.617	-	-	-	-	-	m/p-Xylene
44.781	-	-	-	-	-	Styrene
45.064	-	-	-	-	-	o-Xylene
45.851	-	-	-	-	-	n-Nonane
46.921	-	-	-	-	-	Cumene
48.671	-	-	-	-	-	n-Propylbenzene
49.070	-	-	-	-	-	m-Ethyltoluene
49.350	-	-	-	-	-	p-Ethyltoluene
49.565	-	-	-	-	-	1,3,5-Trimethylbenzene
50.165	-	-	-	-	-	o-Ethyltoluene
50.999	-	-	-	-	-	1,2,4-Trimethylbenzene
51.558	-	-	-	-	-	n-Decane
52.863	-	-	-	-	-	1,2,3-Trimethylbenzene
54.045	-	-	-	-	-	m-Diethylbenzene
54.417	-	-	-	-	-	p-Diethylbenzene
56.931	-	-	-	-	-	n-Undecane

Totals : 2.45681

Uncalibrated Peaks : using compound Propane

Results obtained with enhanced integrator!

2 Warnings or Errors :

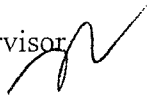
Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

\*\*\* End of Report \*\*\*



Date: 10/15/2008	Analyst: JAK	Batch: 193024	LIMS: AL22735
	%RECOVERY		
SRM concentration:	100.00		
SRM range:	90.00	110.00	
<b>\$I_SRM Result</b>	<b>Recovery %</b>	<b>In Range? (T/F)</b>	
101.44	101.44	TRUE	
<b>\$C_SRM Result</b>	<b>Recovery %</b>	<b>In Range? (T/F)</b>	
101.63	101.63	TRUE	
	<b>RESPONSE FACTORS</b>		
SRM concentration:	100.00		
SRM range (RF):	0.4594	0.5615	
<b>\$I_SRM area</b>	<b>Response Factor</b>	<b>In Range? (y/n)</b>	
198.63	0.5035	TRUE	
<b>\$C_SRM area</b>	<b>Response Factor</b>	<b>In Range? (y/n)</b>	
198.99	0.5025	TRUE	
RPD ( I vs.C)	0.183		

From: Jianzhong Liu  
Environmental Scientist Supervisor  
Air Organics, LSD, DEQ 

Date: May 13, 2008

Re: FID SRM PREPARATION

Stock Standard:

Manufacturer:	Spectra Gases, Inc.
Cylinder #:	CC-162783
Certified Concentration:	1.18 ppm
Expiration Date:	2/25/2009

Working SRM:

Target Concentration:	100.00 ppbC
Flow Rate of the Stock Std:	40 cc/min
Flow Rate of Nitrogen:	1376 cc/min



3434 Route 22 West, Branchburg, New Jersey 08876 USA

ISO 9001:2000

SHIPPED FROM: 80 INDUSTRIAL DRIVE ALPHA, NJ. 08865

SHIPPED TO: Environmental Quality - LA  
Air Organics Lab, LDEQ  
1209 Leesville Road  
Baton Rouge, LA 70802

CERTIFICATE  
OF  
ANALYSIS

SGI ORDER # :	125072	CYLINDER # :	CC-162783
ITEM# :	1	CYLINDER PRES:	2000 psig
CERTIFICATION DATE:	02/25/2008	CYLINDER VALVE:	CGA 350
P.O.# :	CC - J Liu	PRODUCT EXPIRATION DATE:	02/25/2009
BLEND TYPE:	CERTIFIED		

ANALYTICAL ACCURACY: + / - 2%

COMPONENT	REQUESTED GAS CONC	ANALYSIS
Propane	1.20 ppm	1.18 ppm
Nitrogen	Balance	Balance

Received on 3/7/08  
opened on 3/7/08 m

NIST TRACEABLE

ANALYST: CP  
Cheryl Patino

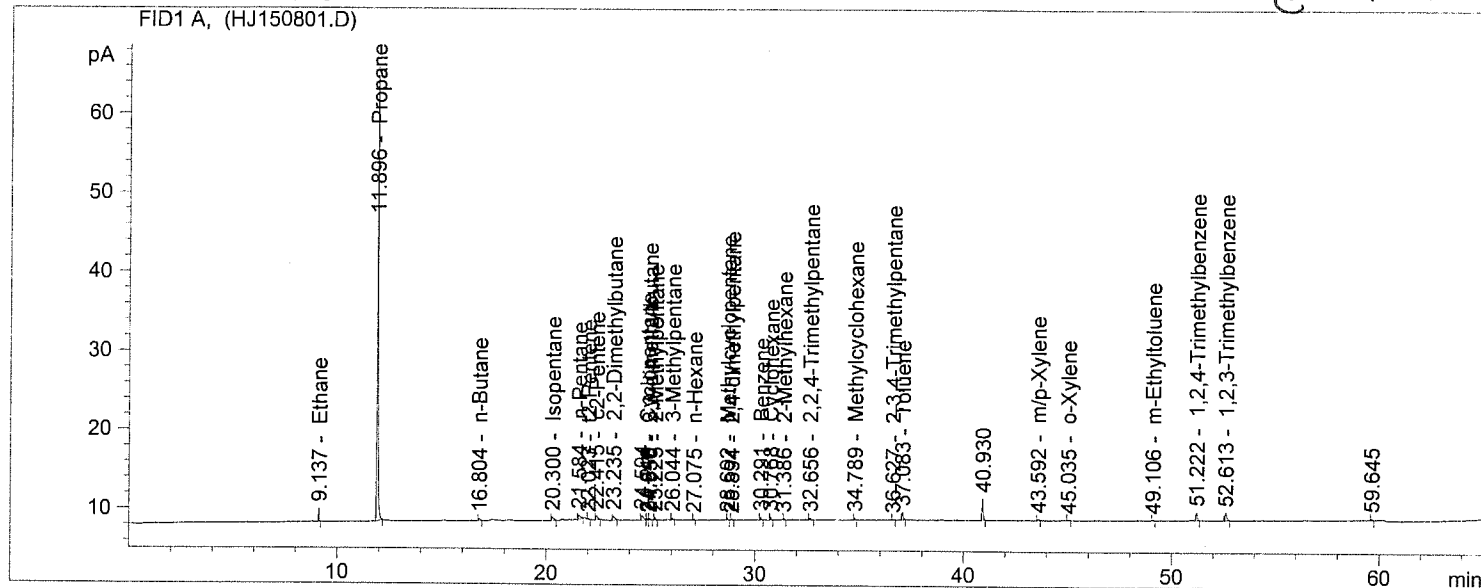
DATE: 02/25/2008

```

=====
Injection Date   : 10/15/2008 8:17:16 AM      Seq. Line   :    1
Sample Name     : AL22735 $I_SRM             Location    : Vial 1
Acq. Operator  : JAK                          Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026           Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/15/2008 6:38:05 AM by JAK
                  (modified after loading)
    
```

G-1124

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By      : Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier     : 0.5107
Dilution       : 1.0000
Sample Amount  : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.813		-	-	-		Ethylene
8.926		-	-	-		Acetylene
9.137	PBA	3.93938	1.00000	2.01184		Ethane
11.730		-	-	-		Propylene
11.896	PBA	198.62938	1.00000	101.44002		Propane
15.083		-	-	-		Isobutane
16.367		-	-	-		1-Butene
16.521		-	-	-		1,3-butadiene
16.804	PB	1.38990	1.00000	7.09822e-1		n-Butane
17.386		-	-	-		t2-Butene
18.034		-	-	-		c2-Butene
20.300	BB	3.09414	1.00000	1.58018		Isopentane
21.003		-	-	-		1-Pentene
21.584	PB	3.94511	1.00000	2.01477		n-Pentane
21.738		-	-	-		Isoprene
22.023	PB	5.66477e-1	1.00000	2.89300e-1		t2-Pentene
22.415	PP	3.15199	1.00000	1.60972		c2-Pentene
23.235	PB	3.38502	1.00000	1.72873		2,2-Dimethylbutane
24.846	BV	9.21160e-1	1.00000	4.70436e-1		Cyclopentane

10-15-08  
JAK

J/M

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.956	VB	1.01160	1.00000	5.16624e-1		2,3-dimethylbutane
25.225	BB	1.25152	1.00000	6.39153e-1		2-Methylpentane
26.044	PB	9.83369e-1	1.00000	5.02207e-1		3-Methylpentane
26.504		-	-	-		1-Hexene
27.075	BB	4.34532e-1	1.00000	2.21915e-1		n-Hexane
28.692	PB	8.22332e-1	1.00000	4.19965e-1		Methylcyclopentane
28.894	PP	6.03021e-1	1.00000	3.07963e-1		2,4-dimethylpentane
30.291	PB +	1.32527	1.00000	6.76814e-1		Benzene
30.768	BB	1.33293	1.00000	6.80726e-1		Cyclohexane
31.386	BB	8.08716e-1	1.00000	4.13011e-1		2-Methylhexane
31.513		-	-	-		2,3-Dimethylpentane
31.943		-	-	-		3-Methylhexane
32.656	PP	1.28984	1.00000	6.58723e-1		2,2,4-Trimethylpentane
33.491		-	-	-		n-Heptane
34.789	BB	9.86934e-1	1.00000	5.04027e-1		Methylcyclohexane
36.627	PB	5.23825e-1	1.00000	2.67517e-1		2,3,4-Trimethylpentane
37.083	PB +	3.95224	1.00000	2.01841		Toluene
37.787		-	-	-		2-Methylheptane
38.294		-	-	-		3-Methylheptane
39.929		-	-	-		n-Octane
43.038		-	-	-		Ethylbenzene
43.592	PB	1.18093	1.00000	6.03100e-1		m/p-Xylene
44.759		-	-	-		Styrene
45.035	PB	5.46907e-1	1.00000	2.79306e-1		o-Xylene
45.828		-	-	-		n-Nonane
46.898		-	-	-		Cumene
48.647		-	-	-		n-Propylbenzene
49.106	BP	5.85634e-1	1.00000	2.99083e-1		m-Ethyltoluene
49.326		-	-	-		p-Ethyltoluene
49.540		-	-	-		1,3,5-Trimethylbenzene
50.140		-	-	-		o-Ethyltoluene
51.222	PB	3.93070	1.00000	2.00741		1,2,4-Trimethylbenzene
51.533		-	-	-		n-Decane
52.613	PB	5.65562	1.00000	2.88832		1,2,3-Trimethylbenzene
54.018		-	-	-		m-Diethylbenzene
54.390		-	-	-		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 125.75910

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.594	PB	4.34410	1.00000	2.21853		?
40.930	BB	11.18780	1.00000	5.71361		?
59.645	PP	8.48758e-1	1.00000	4.33461e-1		?

Uncalib. totals : 8.36561

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

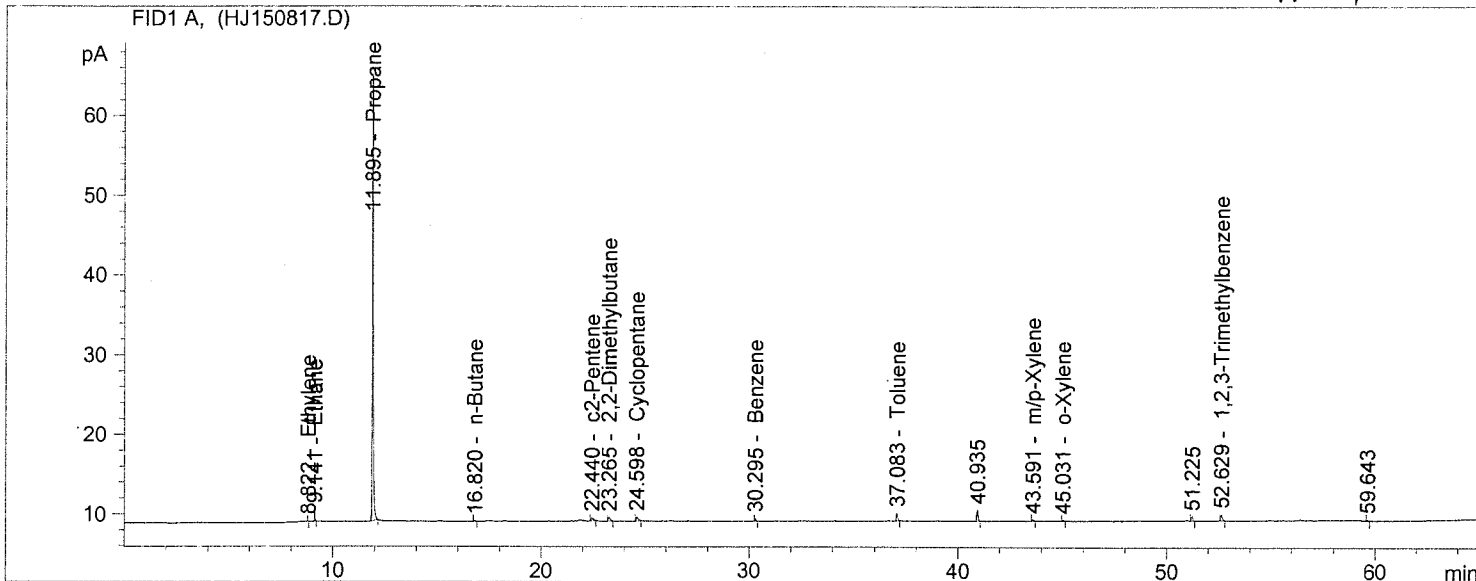
\*\*\* End of Report \*\*\*

```

=====
Injection Date : 10/16/2008 5:13:51 AM      Seq. Line : 17
Sample Name    : AL22735 $C_SRM             Location  : Vial 1
Acq. Operator  : JAK                        Inj       : 1
Acq. Instrument: HP_FID2 SOP 1026          Inj Volume: Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 8/4/2008 1:18:53 PM by JPC
Analysis Method: C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/15/2008 3:00:39 PM by JAK
                (modified after loading)
    
```

G1124

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By      : Signal
Calib. Data Modified : 10/15/2008 3:00:43 PM
Multiplier     : 0.5107
Dilution       : 1.0000
Sample Amount  : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.822	BBA	2.24036e-1	1.00000	1.14415e-1		Ethylene
8.977		-	-	-		Acetylene
9.141	BBA	3.51669	1.00000	1.79598		Ethane
11.732		-	-	-		Propylene
11.895	PBA	196.73717	1.00000	100.47367		Propane
15.083		-	-	-		Isobutane
16.369		-	-	-		1-Butene
16.524		-	-	-		1,3-butadiene
16.820	PB	7.32985e-1	1.00000	3.74336e-1		n-Butane
17.388		-	-	-		t2-Butene
18.037		-	-	-		c2-Butene
20.186		-	-	-		Isopentane
21.006		-	-	-		1-Pentene
21.602		-	-	-		n-Pentane
21.741		-	-	-		Isoprene
21.994		-	-	-		t2-Pentene
22.440	PB	2.46730	1.00000	1.26005		c2-Pentene
23.265	PB	3.51717	1.00000	1.79622		2,2-Dimethylbutane
24.598	PB	3.72463	1.00000	1.90217		Cyclopentane

10-16-08  
DAK

F/m

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
25.037		-	-	-		2,3-dimethylbutane
25.320		-	-	-		2-Methylpentane
26.133		-	-	-		3-Methylpentane
26.508		-	-	-		1-Hexene
27.167		-	-	-		n-Hexane
28.691		-	-	-		Methylcyclopentane
28.840		-	-	-		2,4-dimethylpentane
30.295	PB +	1.38403	1.00000	7.06826e-1		Benzene
30.936		-	-	-		Cyclohexane
31.279		-	-	-		2-Methylhexane
31.517		-	-	-		2,3-Dimethylpentane
31.947		-	-	-		3-Methylhexane
32.814		-	-	-		2,2,4-Trimethylpentane
33.494		-	-	-		n-Heptane
35.003		-	-	-		Methylcyclohexane
36.848		-	-	-		2,3,4-Trimethylpentane
37.083	PB +	3.85212	1.00000	1.96728		Toluene
37.788		-	-	-		2-Methylheptane
38.295		-	-	-		3-Methylheptane
39.929		-	-	-		n-Octane
43.038		-	-	-		Ethylbenzene
43.591	PB	1.04057	1.00000	5.31420e-1		m/p-Xylene
44.760		-	-	-		Styrene
45.031	PB	5.37611e-1	1.00000	2.74558e-1		o-Xylene
45.829		-	-	-		n-Nonane
46.899		-	-	-		Cumene
48.648		-	-	-		n-Propylbenzene
49.046		-	-	-		m-Ethyltoluene
49.326		-	-	-		p-Ethyltoluene
49.541		-	-	-		1,3,5-Trimethylbenzene
50.141		-	-	-		o-Ethyltoluene
50.975		-	-	-		1,2,4-Trimethylbenzene
51.533		-	-	-		n-Decane
52.629	PB	4.39412	1.00000	2.24408		1,2,3-Trimethylbenzene
54.019		-	-	-		m-Diethylbenzene
54.391		-	-	-		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 113.44099

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
40.935	PB	5.96588	1.00000	3.04678		?
51.225	BP	2.34146	1.00000	1.19578		?
59.643	PP	7.09156e-1	1.00000	3.62166e-1		?

Uncalib. totals : 4.60472

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

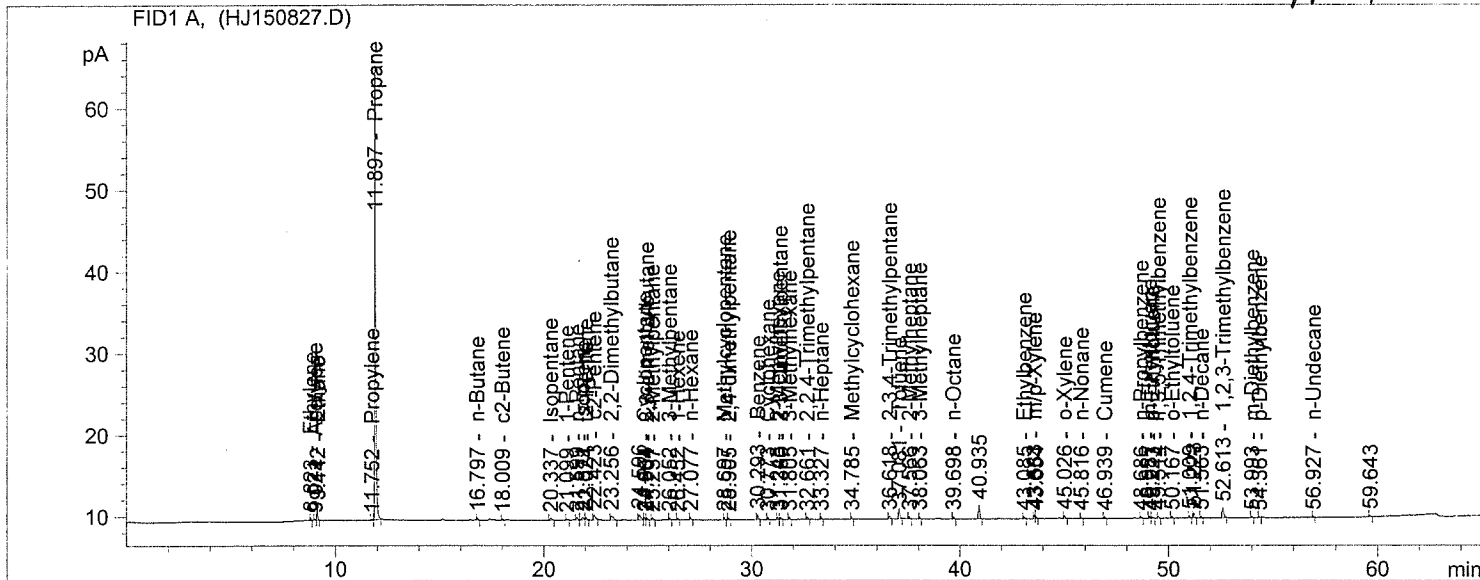
Warning : Time reference compound(s) not found

\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/16/2008 7:06:42 PM      Seq. Line   : 10
Sample Name     : AL22735 $C_SRM             Location    : Vial 1
Acq. Operator   : JAK                       Inj         : 1
Acq. Instrument : HP_FID2 SOP 1026          Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/16/2008 2:49:51 PM by JAK
                  (modified after loading)
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/17/2008 6:32:13 AM by JAK
                  (modified after loading)
    
```

PAMS SAMPLE ANALYSES



External Standard Report

```

=====
Sorted By       : Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier     : 0.5107
Dilution       : 1.0000
Sample Amount   : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.823	BBA	7.93821e-1	1.00000	4.05404e-1		Ethylene
9.021	BB	4.76038e-1	1.00000	2.43112e-1		Acetylene
9.142	BBA	4.11750	1.00000	2.10281		Ethane
11.752	PB	5.41346e-1	1.00000	2.76466e-1		Propylene
11.897	BBA	192.80481	1.00000	98.46542		Propane
15.083		-	-	-		Isobutane
16.368		-	-	-		1-Butene
16.522		-	-	-		1,3-butadiene
16.797	BB	1.50979	1.00000	7.71048e-1		n-Butane
17.387		-	-	-		t2-Butene
18.009	PP	7.29622e-1	1.00000	3.72618e-1		c2-Butene
20.337	PB	1.71260	1.00000	8.74625e-1		Isopentane
21.099	PB	7.59638e-1	1.00000	3.87947e-1		1-Pentene
21.599	BV	1.43838	1.00000	7.34581e-1		n-Pentane
21.871	VV	2.59908	1.00000	1.32735		Isoprene
22.024	VB	1.61021	1.00000	8.22332e-1		t2-Pentene
22.423	PP	3.35658	1.00000	1.71421		c2-Pentene
23.256	BB	4.74432	1.00000	2.42293		2,2-Dimethylbutane

10-17-08  
AKK

I/m



RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.854	BV	1.34449	1.00000	6.86631e-1		Cyclopentane
24.964	VB	1.36218	1.00000	6.95667e-1		2,3-dimethylbutane
25.237	PB	1.21187	1.00000	6.18904e-1		2-Methylpentane
26.052	PB	1.01165	1.00000	5.16648e-1		3-Methylpentane
26.452	BB	7.80066e-1	1.00000	3.98380e-1		1-Hexene
27.077	BB	1.23685	1.00000	6.31661e-1		n-Hexane
28.697	BB	1.18669	1.00000	6.06043e-1		Methylcyclopentane
28.905	BP	1.03437	1.00000	5.28253e-1		2,4-dimethylpentane
30.293	PB +	2.28682	1.00000	1.16788		Benzene
30.773	PB	1.13142	1.00000	5.77817e-1		Cyclohexane
31.245	BV	1.11731	1.00000	5.70609e-1		2-Methylhexane
31.386	VP	1.12893	1.00000	5.76543e-1		2,3-Dimethylpentane
31.805	BB	1.18118	1.00000	6.03231e-1		3-Methylhexane
32.661	PB	1.38191	1.00000	7.05743e-1		2,2,4-Trimethylpentane
33.327	PB	1.10115	1.00000	5.62356e-1		n-Heptane
34.785	BP	1.24123	1.00000	6.33897e-1		Methylcyclohexane
36.618	BB	1.62238	1.00000	8.28551e-1		2,3,4-Trimethylpentane
37.081	PB +	4.87525	1.00000	2.48979		Toluene
37.566	PB	1.09294	1.00000	5.58162e-1		2-Methylheptane
38.063	PB	1.09079	1.00000	5.57064e-1		3-Methylheptane
39.698	BP	1.19115	1.00000	6.08319e-1		n-Octane
43.085	PB	1.26408	1.00000	6.45568e-1		Ethylbenzene
43.583	BV	1.65149	1.00000	8.43414e-1		m/p-Xylene
44.767		-	-	-		Styrene
45.026	PB	1.51419	1.00000	7.73295e-1		o-Xylene
45.816	PP	9.76644e-1	1.00000	4.98772e-1		n-Nonane
46.939	PP	1.06222	1.00000	5.42474e-1		Cumene
48.686	PP	8.63902e-1	1.00000	4.41195e-1		n-Propylbenzene
49.087	BV	1.16538	1.00000	5.95161e-1		m-Ethyltoluene
49.223	VB	8.06003e-1	1.00000	4.11626e-1		p-Ethyltoluene
49.514	BP	1.05815	1.00000	5.40399e-1		1,3,5-Trimethylbenzene
50.167	PB	9.00950e-1	1.00000	4.60115e-1		o-Ethyltoluene
51.009	BB	1.14839	1.00000	5.86481e-1		1,2,4-Trimethylbenzene
51.563	PB	9.20273e-1	1.00000	4.69984e-1		n-Decane
52.613	PB	6.87596	1.00000	3.51155		1,2,3-Trimethylbenzene
53.993	BP	7.07392e-1	1.00000	3.61265e-1		m-Diethylbenzene
54.361	BP	4.57058e-1	1.00000	2.33419e-1		p-Diethylbenzene
56.927	PB +	5.28609e-1	1.00000	2.69961e-1		n-Undecane

Totals : 137.22767

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.596	PB	4.79303	1.00000	2.44780	?	
40.935	PB	7.02902	1.00000	3.58972	?	
43.654	VB	1.49541	1.00000	7.63704e-1	?	
51.223	BB	2.42487	1.00000	1.23838	?	
59.643	PB	7.50064e-1	1.00000	3.83058e-1	?	

Uncalib. totals : 8.42266

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

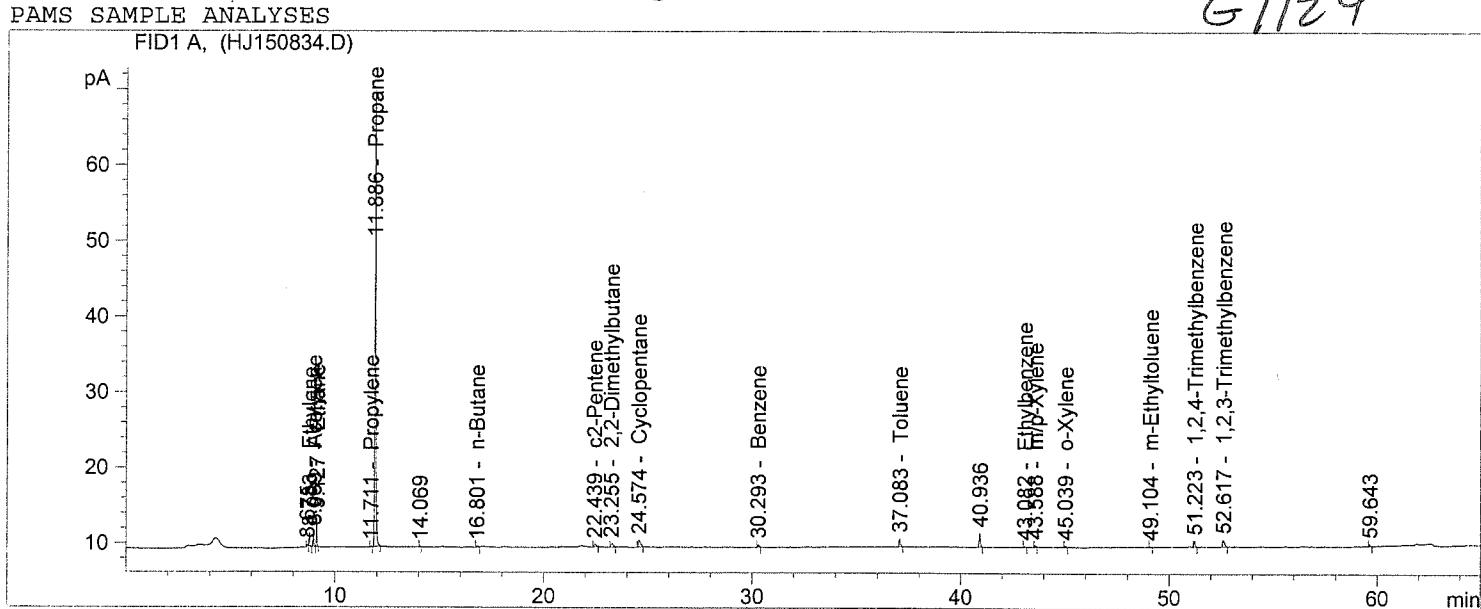
Warning : Time reference compound(s) not found

\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/17/2008 1:00:50 PM      Seq. Line   :    4
Sample Name     : AL22735 $C_PPFID          Location    : Vial 0
Acq. Operator   : JAK                      Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026         Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/17/2008 8:23:46 AM by JAK
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/17/2008 12:56:59 PM by JAK
                  (modified after loading)
    
```

G1124



External Standard Report

```

Sorted By           : Signal
Calib. Data Modified : 10/17/2008 12:57:01 PM
Multiplier          : 0.5107
Dilution            : 1.0000
Sample Amount       : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.783	BBA	4.08677	1.00000	2.08711		Ethylene
8.989	BBA	5.02441	1.00000	2.56597		Acetylene
9.127	BBA	9.39811	1.00000	4.79962		Ethane
11.711	BBA	3.99607e-1	1.00000	2.04079e-1		Propylene
11.886	PBA	198.99361	1.00000	101.62603		Propane
14.960		-	-	-		Isobutane
16.257		-	-	-		1-Butene
16.447		-	-	-		1,3-butadiene
16.801	PP	9.22642e-1	1.00000	4.71193e-1		n-Butane
17.387		-	-	-		t2-Butene
18.036		-	-	-		c2-Butene
20.185		-	-	-		Isopentane
21.005		-	-	-		1-Pentene
21.600		-	-	-		n-Pentane
21.740		-	-	-		Isoprene
21.992		-	-	-		t2-Pentene
22.439	PP	2.58524	1.00000	1.32028		c2-Pentene
23.255	PB	3.56825	1.00000	1.82230		2,2-Dimethylbutane
24.574	PB	6.42842	1.00000	3.28300		Cyclopentane

10-17-08  
JAK

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.885		-	-	-		2,3-dimethylbutane
25.134		-	-	-		2-Methylpentane
26.131		-	-	-		3-Methylpentane
26.271		-	-	-		1-Hexene
26.929		-	-	-		n-Hexane
28.689		-	-	-		Methylcyclopentane
28.838		-	-	-		2,4-dimethylpentane
30.293	BP +	1.38236	1.00000	7.05971e-1		Benzene
30.656		-	-	-		Cyclohexane
31.078		-	-	-		2-Methylhexane
31.330		-	-	-		2,3-Dimethylpentane
31.734		-	-	-		3-Methylhexane
32.531		-	-	-		2,2,4-Trimethylpentane
33.493		-	-	-		n-Heptane
34.706		-	-	-		Methylcyclohexane
36.848		-	-	-		2,3,4-Trimethylpentane
37.083	PB +	4.41837	1.00000	2.25646		Toluene
37.492		-	-	-		2-Methylheptane
37.982		-	-	-		3-Methylheptane
39.641		-	-	-		n-Octane
43.082	PB	4.93319e-1	1.00000	2.51938e-1		Ethylbenzene
43.588	PB	1.20612	1.00000	6.15967e-1		m/p-Xylene
44.760		-	-	-		Styrene
45.039	PP	7.91625e-1	1.00000	4.04283e-1		o-Xylene
45.829		-	-	-		n-Nonane
46.899		-	-	-		Cumene
48.648		-	-	-		n-Propylbenzene
49.104	BB	4.93205e-1	1.00000	2.51880e-1		m-Ethyltoluene
49.326		-	-	-		p-Ethyltoluene
49.541		-	-	-		1,3,5-Trimethylbenzene
50.141		-	-	-		o-Ethyltoluene
51.223	PP	3.31232	1.00000	1.69160		1,2,4-Trimethylbenzene
51.533		-	-	-		n-Decane
52.617	BB	5.25361	1.00000	2.68302		1,2,3-Trimethylbenzene
54.019		-	-	-		m-Diethylbenzene
54.391		-	-	-		p-Diethylbenzene
56.931		-	-	-		n-Undecane

Totals : 127.04071

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.675	PB	8.95369e-1	1.00000	4.57265e-1	?	
14.069	PB	3.58859e-1	1.00000	1.83269e-1	?	
40.936	BB	7.44692	1.00000	3.80314	?	
59.643	PB	1.10320	1.00000	5.63404e-1	?	

Uncalib. totals : 5.00708

Results obtained with enhanced integrator!

2 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

Warning : Time reference compound(s) not found

=====  
\*\*\* End of Report \*\*\*

**Initial Calibration Verification (LCS) FID #2**

DATE: 10/15/2008

QC NO: AL22735

BATCH NO: 193024

COMPONENTS	STD (ppbc)	\$I (ppbc)	REC% \$I	JPC
Ethylene	49.20	55.61	113.0	
Actetylene	48.90	45.59	93.2	
Ethane	48.90	57.12	116.8	
Propylene	48.90	47.77	97.7	
Propane	49.00	55.47	113.2	
n-Butane	48.90			
Isobutane	48.90	50.09	102.4	
1-Butene	49.90	49.54	99.3	
1,3-Butadiene	48.80	41.28	84.6	
n-Butane	48.90	57.29	117.2	
t2-butene	48.90	49.65	101.5	
c2-butene	48.90	48.40	99.0	
Isopentane	49.40	54.58	110.5	
1-Pentene	50.70	53.85	106.2	
n-Pentane	49.10	52.15	106.2	
Isoprene	49.40	49.17	99.5	
t2-Pentene	50.30	54.13	107.6	
c2-Pentene	49.50	50.58	102.2	
2,2-Dimethylbutane	49.90	51.49	103.2	
Cyclopentane	59.60	50.92	85.4	
2,3-Dimethylbutane	49.50	53.52	108.1	
2-Methylpentane	49.10	51.20	104.3	
3-Methylpentane	49.50	51.91	104.9	
1-Hexene	49.30	45.31	91.9	
1-Hexane	49.70	50.71	102.0	
Methylcyclopentane	49.10	50.67	103.2	
2,4-Dimethylpentane	49.50	51.52	104.1	
Benzene	49.30	50.60	102.6	
Cyclohexane	48.50	51.51	106.2	
2-Methylhexane	48.80	50.95	104.4	
2,3-Dimethylpentane	48.60	53.37	109.8	
3-Methylhexane	48.80	51.55	105.6	
2,2,4-Trimethylpentane	53.70	59.30	110.4	
n-Heptane	49.00	50.21	102.5	
Methylcyclohexane	49.60	53.23	107.3	
2,3,4-Trimethylpentane	48.90	52.43	107.2	
Toluene	49.80	49.65	99.7	
2-Methylheptane	49.10	52.33	106.6	
3-Methylheptane	50.70	52.96	104.5	
n-Octane	48.50	50.09	103.3	
Ethylbenzne	49.70	50.25	101.1	
m/p-Xylene	98.50	101.86	103.4	
Styrene	49.30	43.87	89.0	
o Xylene	49.00	51.82	105.8	
n-Nonane	48.60	49.18	101.2	
Cumene	49.40	51.57	104.4	
n-Propylbenzene	49.00	48.73	99.5	
m-Ethyltoluene	48.70	48.79	100.2	
p-Ethyltoluene	48.10	47.71	99.2	
1,3,5-Trimethylbenzene	48.70	51.92	106.6	
o-Ethyltouene	48.50	49.77	102.6	
1,2,4-trimethylbenzene	49.00	49.95	101.9	
n-Decane	48.90	48.32	98.8	
1,2,3-Trimethylbenzene	48.70	45.53	93.5	
m-Diethylbenzene	48.40	44.96	92.9	
p-Diethylbenzene	48.40	37.38	77.2	
n-Undecane	48.90	45.36	92.8	

From: Jianzhong Liu  
Environmental Scientist Supervisor  
Air Organics, LSD, DEQ

Date: June 3, 2008

Re: Low Recovery of p-Diethylbenzene in PAMS LCS Standard

Stock Standard:

Manufacturer:	Matheson Tri-Gas, Inc.
Cylinder #:	SX39238D
Lot#:	1057610175
Expiration Date:	12/03/2009

From the studies of runs in different GC/FIDs, the recovery of p-diethylbenzene is constantly low (~ 75%). However, the recovery of this compound in PAMS standard is normal (~100%). Therefore, 60% (75%\*80%) recovery for this compound in LCS is acceptable.

**Concentrations (ppbC) of Different Diluton of Matheson Stock Standard**

**Cylinder #: SX39238D; Lot #: 1057610175; Expiration Date: 12/3/2008**

COMPONENTS	Stock Std	10 times	71.425 times	166.65 times	250 times	500 times
Ethylene	492.00	49.20	6.89	2.95	1.97	0.98
Actetylene	489.00	48.90	6.85	2.93	1.96	0.98
Ethane	489.00	48.90	6.85	2.93	1.96	0.98
Propylene	489.00	48.90	6.85	2.93	1.96	0.98
Propane	490.00	49.00	6.86	2.94	1.96	0.98
n-Butane	489.00	48.90	6.85	2.93	1.96	0.98
Isobutane	489.00	48.90	6.85	2.93	1.96	0.98
1-Butene	499.00	49.90	6.99	2.99	2.00	1.00
1,3-Butadiene	488.00	48.80	6.83	2.93	1.95	0.98
n-Butane	489.00	48.90	6.85	2.93	1.96	0.98
t2-butene	489.00	48.90	6.85	2.93	1.96	0.98
c2-butene	489.00	48.90	6.85	2.93	1.96	0.98
Isopentane	494.00	49.40	6.92	2.96	1.98	0.99
1-Pentene	507.00	50.70	7.10	3.04	2.03	1.01
n-Pentane	491.00	49.10	6.87	2.95	1.96	0.98
Isoprene	494.00	49.40	6.92	2.96	1.98	0.99
t2-Pentene	503.00	50.30	7.04	3.02	2.01	1.01
c2-Pentene	495.00	49.50	6.93	2.97	1.98	0.99
2,2-Dimethylbutane	499.00	49.90	6.99	2.99	2.00	1.00
Cyclopentane	596.00	59.60	8.34	3.58	2.38	1.19
2,3-Dimethylbutane	495.00	49.50	6.93	2.97	1.98	0.99
2-Methylpentane	491.00	49.10	6.87	2.95	1.96	0.98
3-Methylpentane	495.00	49.50	6.93	2.97	1.98	0.99
1-Hexene	493.00	49.30	6.90	2.96	1.97	0.99
1-Hexane	497.00	49.70	6.96	2.98	1.99	0.99
Methylcyclopentane	491.00	49.10	6.87	2.95	1.96	0.98
2,4-Dimethylpentane	495.00	49.50	6.93	2.97	1.98	0.99
Benzene	493.00	49.30	6.90	2.96	1.97	0.99
Cyclohexane	485.00	48.50	6.79	2.91	1.94	0.97
2-Methylhexane	488.00	48.80	6.83	2.93	1.95	0.98
2,3-Dimethylpentane	486.00	48.60	6.80	2.92	1.94	0.97
3-Methylhexane	488.00	48.80	6.83	2.93	1.95	0.98
2,2,4-Trimethylpentane	537.00	53.70	7.52	3.22	2.15	1.07
n-Heptane	490.00	49.00	6.86	2.94	1.96	0.98
Methylcyclohexane	496.00	49.60	6.94	2.98	1.98	0.99
2,3,4-Trimethylpentane	489.00	48.90	6.85	2.93	1.96	0.98
Toluene	498.00	49.80	6.97	2.99	1.99	1.00
2-Methylheptane	491.00	49.10	6.87	2.95	1.96	0.98
3-Methylheptane	507.00	50.70	7.10	3.04	2.03	1.01
n-Octane	485.00	48.50	6.79	2.91	1.94	0.97
Ethylbenzne	497.00	49.70	6.96	2.98	1.99	0.99
m/p-Xylene	985.00	98.50	13.79	5.91	3.94	1.97
Styrene	493.00	49.30	6.90	2.96	1.97	0.99
o Xylene	490.00	49.00	6.86	2.94	1.96	0.98
n-Nonane	486.00	48.60	6.80	2.92	1.94	0.97
Cumene	494.00	49.40	6.92	2.96	1.98	0.99
n-Propylbenzene	490.00	49.00	6.86	2.94	1.96	0.98
m-Ethyltoluene	487.00	48.70	6.82	2.92	1.95	0.97
p-Ethyltoluene	481.00	48.10	6.73	2.89	1.92	0.96
1,3,5-Trimethylbenzene	487.00	48.70	6.82	2.92	1.95	0.97
o-Ethylouene	485.00	48.50	6.79	2.91	1.94	0.97
1,2,4-trimethylbenzene	490.00	49.00	6.86	2.94	1.96	0.98
n-Decane	489.00	48.90	6.85	2.93	1.96	0.98
1,2,3-Trimethylbenzene	487.00	48.70	6.82	2.92	1.95	0.97
m-Diethylbenzene	484.00	48.40	6.78	2.90	1.94	0.97
p-Diethylbenzene	484.00	48.40	6.78	2.90	1.94	0.97
n-Undecane	489.00	48.90	6.85	2.93	1.96	0.98



# MATHESON TRI-GAS

**Certified Mixture Grade**

**Matheson Tri-Gas**  
6874 S Main Street  
Morrow, GA 30260  
Phone: (770) 961-7891  
Fax: (770) 968-1268

To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd  
Baton Rouge, LA 70802

Phone:  
Fax:

**TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE GREATER THAN PROCESS PRESSURE.**

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057610175

**PRODUCT:**

CYLINDER NUMBER: SX39238D  
SIZE: 1l  
CGA/DISS OUTLET: 350  
CONTENT: 131 cu. ft.  
PRESSURE: 1850 psig

Fill Date: 12/3/2007  
Certification Date: 12/3/2007  
Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	500 ppbC	498 ppbC	+/- 5%
2-Methylheptane	500 ppbC	491 ppbC	+/- 5%
3-Methylheptane	500 ppbC	507 ppbC	+/- 5%
n-Octane	500 ppbC	485 ppbC	+/- 5%
Ethylbenzene	500 ppbC	497 ppbC	+/- 5%
p-Xylene	500 ppbC	490 ppbC	+/- 5%
m-Xylene	500 ppbC	495 ppbC	+/- 5%
Styrene	500 ppbC	493 ppbC	+/- 5%
o-Xylene	500 ppbC	490 ppbC	+/- 5%
n-Nonane	500 ppbC	486 ppbC	+/- 5%
Isopropylbenzene	500 ppbC	494 ppbC	+/- 5%
n-Propylbenzene	500 ppbC	490 ppbC	+/- 5%
n-Decane	500 ppbC	489 ppbC	+/- 5%
m-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
p-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
n-Dodecane	500 ppbC	492 ppbC	+/- 5%
m-Ethyltoluene	500 ppbC	487 ppbC	+/- 5%
o-Ethyltoluene	500 ppbC	485 ppbC	+/- 5%
p-Ethyltoluene	500 ppbC	481 ppbC	+/- 5%
n-Undecane	500 ppbC	489 ppbC	+/- 5%
1,2,3-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,3,5-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,2,4-Trimethylbenzene	500 ppbC	490 ppbC	+/- 5%
Nitrogen, Balance			

**SPECIAL INFORMATION / ADDITIONAL COMMENTS**

*Received on 12/16/07*

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

Derek Stuck  
ANALYST

12/4/2007  
DATE SIGNED



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## Certified Mixture Grade

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Phone:  
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SALES ORDER NUMBER: 427497  
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LOT NUMBER: 1057610175

PRODUCT:

CYLINDER NUMBER: SX39238D  
SIZE: 1l  
CGA/DISS OUTLET: 350  
CONTENT: 131 cu. ft.  
PRESSURE: 1850 psig

Fill Date: 12/3/2007  
Certification Date: 12/3/2007  
Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	500 ppbC	498 ppbC	+/- 5%
2-Methylheptane	500 ppbC	491 ppbC	+/- 5%
3-Methylheptane	500 ppbC	507 ppbC	+/- 5%
n-Octane	500 ppbC	485 ppbC	+/- 5%
Ethylbenzene	500 ppbC	497 ppbC	+/- 5%
p-Xylene	500 ppbC	490 ppbC	+/- 5%
m-Xylene	500 ppbC	495 ppbC	+/- 5%
Styrene	500 ppbC	493 ppbC	+/- 5%
o-Xylene	500 ppbC	490 ppbC	+/- 5%
n-Nonane	500 ppbC	486 ppbC	+/- 5%
Isopropylbenzene	500 ppbC	494 ppbC	+/- 5%
n-Propylbenzene	500 ppbC	490 ppbC	+/- 5%
n-Decane	500 ppbC	489 ppbC	+/- 5%
m-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
p-Diethylbenzene	500 ppbC	484 ppbC	+/- 5%
n-Dodecane	500 ppbC	492 ppbC	+/- 5%
m-Ethyltoluene	500 ppbC	487 ppbC	+/- 5%
o-Ethyltoluene	500 ppbC	485 ppbC	+/- 5%
p-Ethyltoluene	500 ppbC	481 ppbC	+/- 5%
n-Undecane	500 ppbC	489 ppbC	+/- 5%
1,2,3-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,3,5-Trimethylbenzene	500 ppbC	487 ppbC	+/- 5%
1,2,4-Trimethylbenzene	500 ppbC	490 ppbC	+/- 5%
Nitrogen, Balance			

### SPECIAL INFORMATION / ADDITIONAL COMMENTS

*Received on 12/16/07*

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

Derek Stuck  
ANALYST

12/4/2007  
DATE SIGNED

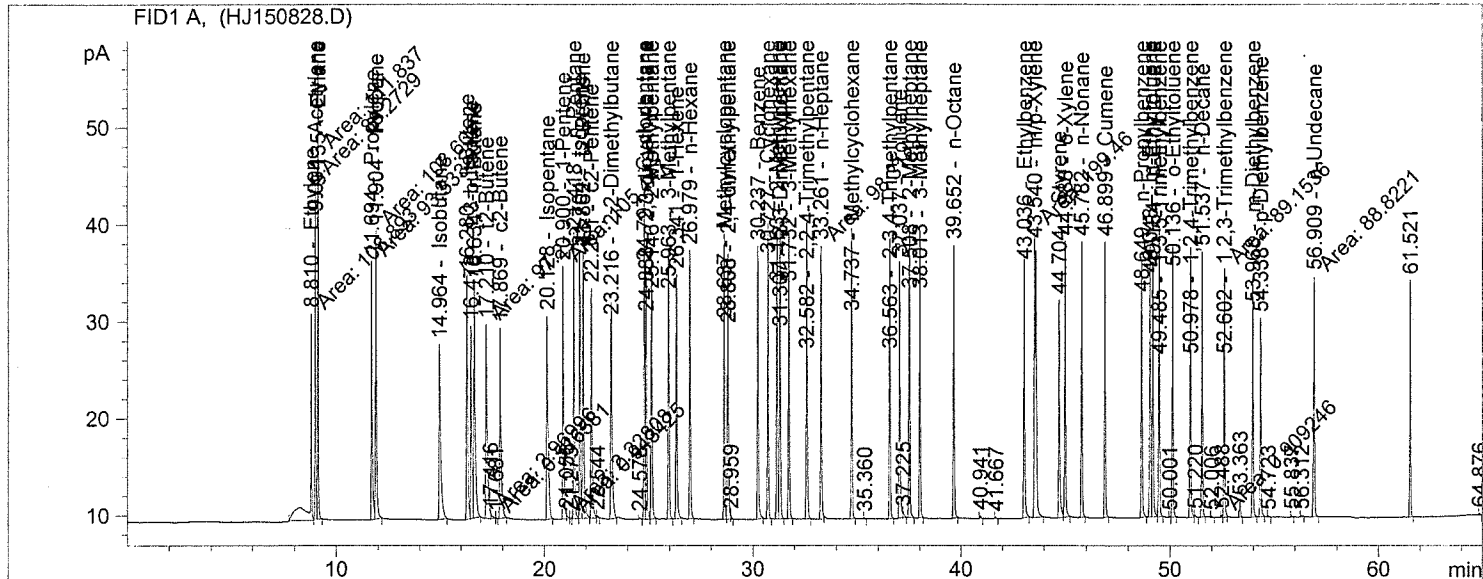


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=====
Injection Date   : 10/16/2008 8:28:13 PM      Seq. Line   : 11
Sample Name     : AL22735 $L1PPFID          Location    : Vial 31
Acq. Operator  : JAK                        Inj         : 1
Acq. Instrument : HP_FID2 SOP 1026         Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/16/2008 2:49:51 PM by JAK
                (modified after loading)
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/17/2008 6:32:13 AM by JAK
                (modified after loading)
    
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51452

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By           : Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier          : 0.5107
Dilution            : 1.0000
Sample Amount       : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.810	MM	108.89320	1.00000	55.61176		Ethylene
9.004	MF	89.27295	1.00000	45.59170		Acetylene
9.135	FM	111.83705	1.00000	57.11518		Ethane
11.694	MF	93.53393	1.00000	47.76778		Propylene
11.904	FM	108.60664	1.00000	55.46541		Propane
14.964	PB +	98.08557	1.00000	50.09230		Isobutane
16.280	PV	96.99831	1.00000	49.53704		1-Butene
16.473	VV	80.82842	1.00000	41.27908		1,3-butadiene
16.634	VB	112.18735	1.00000	57.29408		n-Butane
17.210	MF	97.21261	1.00000	49.64648		t2-Butene
17.869	PB	94.78104	1.00000	48.40468		c2-Butene
20.128	BB	106.86475	1.00000	54.57583		Isopentane
20.900	MF	105.44742	1.00000	53.85200		1-Pentene
21.418	VV	102.11597	1.00000	52.15063		n-Pentane
21.704	VV	96.28439	1.00000	49.17244		Isoprene
21.862	VB	105.98328	1.00000	54.12566		t2-Pentene
22.261	BB	99.03815	1.00000	50.57878		c2-Pentene
23.216	PV	100.81549	1.00000	51.48647		2,2-Dimethylbutane

10-17-08  
JAK

m



RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
61.521	BB	70.57325	1.00000	36.04176	?	
64.876	PP	5.35105e-1	1.00000	2.73278e-1	?	

Uncalib. totals : 49.78753

Results obtained with enhanced integrator!

1 Warnings or Errors :

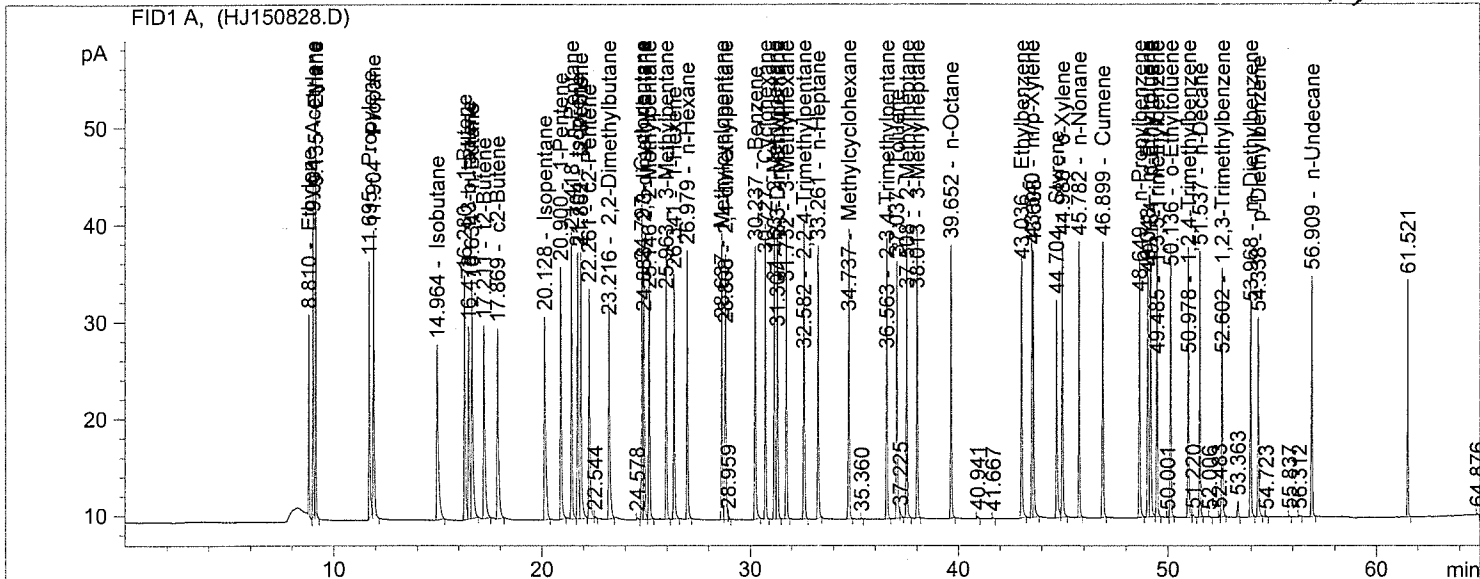
Warning : Calibration warnings (see calibration table listing)

=====  
\*\*\* End of Report \*\*\*

```

=====
Injection Date   : 10/16/2008 8:28:13 PM      Seq. Line   : 11
Sample Name     : AL22735 $L1PPFFID          Location    : Vial 31
Acq. Operator  : JAK                          Inj         : 1
Acq. Instrument : HP_FID2 SOP 1026           Inj Volume  : Manually
Acq. Method    : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/16/2008 2:49:51 PM by JAK
                (modified after loading)
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed   : 10/17/2008 6:32:13 AM by JAK
                (modified after loading)
    
```

PAMS SAMPLE ANALYSES



External Standard Report

```

Sorted By           : Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier          : 0.5107
Dilution            : 1.0000
Sample Amount       : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.810	BB	48.36698	1.00000	24.70102		Ethylene
9.004	BB	85.67876	1.00000	43.75614		Acetylene
9.135	BBA	106.03226	1.00000	54.15068		Ethane
11.695	PB	88.75471	1.00000	45.32703		Propylene
11.904	BBA	100.49319	1.00000	51.32187		Propane
14.964	PB +	98.08557	1.00000	50.09230		Isobutane
16.280	PV	96.99831	1.00000	49.53704		1-Butene
16.473	VV	80.82842	1.00000	41.27908		1,3-butadiene
16.634	VB	112.18735	1.00000	57.29408		n-Butane
17.211	PB	98.03780	1.00000	50.06791		t2-Butene
17.869	PB	94.78104	1.00000	48.40468		c2-Butene
20.128	BB	106.86475	1.00000	54.57583		Isopentane
20.900	PB	106.23857	1.00000	54.25604		1-Pentene
21.418	VV	102.11597	1.00000	52.15063		n-Pentane
21.704	VV	96.28439	1.00000	49.17244		Isoprene
21.862	VB	105.98328	1.00000	54.12566		t2-Pentene
22.261	BB	99.03815	1.00000	50.57878		c2-Pentene
23.216	PV	100.81549	1.00000	51.48647		2,2-Dimethylbutane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.797	BV	99.70258	1.00000	50.91811		Cyclopentane
24.888	VV	104.79393	1.00000	53.51826		2,3-dimethylbutane
25.146	VB	100.25581	1.00000	51.20064		2-Methylpentane
25.963	BB	101.64356	1.00000	51.90937		3-Methylpentane
26.341	PB	88.71393	1.00000	45.30620		1-Hexene
26.979	PB	99.29967	1.00000	50.71234		n-Hexane
28.637	BV	99.22535	1.00000	50.67439		Methylcyclopentane
28.808	VV	100.87298	1.00000	51.51583		2,4-dimethylpentane
30.237	PB	99.08167	1.00000	50.60101		Benzene
30.727	PB	100.85815	1.00000	51.50826		Cyclohexane
31.163	PV	99.76077	1.00000	50.94782		2-Methylhexane
31.307	VB	104.50134	1.00000	53.36883		2,3-Dimethylpentane
31.732	BB	100.93217	1.00000	51.54606		3-Methylhexane
32.582	BB	116.11399	1.00000	59.29942		2,2,4-Trimethylpentane
33.261	PB	96.57597	1.00000	49.32135		n-Heptane
34.737	BB	104.23523	1.00000	53.23293		Methylcyclohexane
36.563	BB	102.65385	1.00000	52.42532		2,3,4-Trimethylpentane
37.037	BV	97.22409	1.00000	49.65234		Toluene
37.508	BB	102.46342	1.00000	52.32807		2-Methylheptane
38.013	BB	103.69798	1.00000	52.95856		3-Methylheptane
39.652	BB	98.07506	1.00000	50.08693		n-Octane
43.036	PB	98.39761	1.00000	50.25166		Ethylbenzene
43.540	PV	92.93414	1.00000	47.46146		m/p-Xylene
44.704	BV	85.90063	1.00000	43.86945		Styrene
44.988	VB	101.47527	1.00000	51.82342		o-Xylene
45.782	BB	96.29155	1.00000	49.17609		n-Nonane
46.899	BB	100.98366	1.00000	51.57235		Cumene
48.649	BB	95.42062	1.00000	48.73131		n-Propylbenzene
49.048	BV	95.52940	1.00000	48.78687		m-Ethyltoluene
49.184	VV	93.41511	1.00000	47.70710		p-Ethyltoluene
49.485	VB	101.65474	1.00000	51.91508		1,3,5-Trimethylbenzene
50.136	VB	97.44906	1.00000	49.76723		o-Ethyltoluene
50.978	BB	97.81036	1.00000	49.95175		1,2,4-Trimethylbenzene
51.537	BB	94.62080	1.00000	48.32284		n-Decane
52.602	VB	88.41506	1.00000	45.15357		1,2,3-Trimethylbenzene
53.968	BB	88.04417	1.00000	44.96416		m-Diethylbenzene
54.338	BB	73.19059	1.00000	37.37843		p-Diethylbenzene
56.909	BB	88.71956	1.00000	45.30908		n-Undecane

Totals : 2777.45156

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
22.544	BB	1.17554	1.00000	6.00349e-1	?	
24.578	PB	1.26304	1.00000	6.45037e-1	?	
28.959	VB	1.64351	1.00000	8.39343e-1	?	
35.360	BB	3.91656e-1	1.00000	2.00019e-1	?	
37.225	VB	2.82216	1.00000	1.44128	?	
40.941	PB	1.10559	1.00000	5.64624e-1	?	
41.667	PB	6.27572e-1	1.00000	3.20501e-1	?	
43.608	VB	105.08286	1.00000	53.66581	?	
50.001	PP	3.40748e-1	1.00000	1.74020e-1	?	
51.220	BB	1.26381	1.00000	6.45429e-1	?	
52.006	PB	5.54539e-1	1.00000	2.83203e-1	?	
52.483	PV	8.54311e-1	1.00000	4.36297e-1	?	
53.363	BB	5.73396	1.00000	2.92833	?	
54.723	PB	4.31328e-1	1.00000	2.20279e-1	?	
55.837	PB	6.35686e-1	1.00000	3.24645e-1	?	
56.312	PB	8.24003e-1	1.00000	4.20818e-1	?	
61.521	BB	70.57325	1.00000	36.04176	?	
64.876	PP	5.35105e-1	1.00000	2.73278e-1	?	

Uncalib. totals : 100.02502

Results obtained with enhanced integrator!

1 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

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\*\*\* End of Report \*\*\*



PAMS RETENTION TIME STD FID #2 lot #1057410185

DATE: 10/15/2008 QC NO: AL22735 BATCH NO: 193024

COMPONENTS	STD (ppbc)	\$I (ppbc)	REC% \$I
Ethylene	21.00	18.60	88.6
Actetylene	42.00	18.70	44.5
Ethane	26.00	30.32	116.6
Propylene	26.00	20.99	80.7
Propane	40.00	44.26	110.7
n-Butane	43.00		
Isobutane	25.00	26.01	104.0
1-Butene	32.00	30.24	94.5
1,3-Butadiene	32.00	24.34	76.1
n-Butane	43.00	49.04	114.0
t2-butene	26.00	25.24	97.1
c2-butene	38.00	35.74	94.1
Isopentane	40.00	41.39	103.5
1-Pentene	25.00	25.38	101.5
n-Pentane	26.00	25.75	99.1
Isoprene	42.00	37.32	88.9
t2-Pentene	25.00	27.65	110.6
c2-Pentene	34.00	33.45	98.4
2,2-Dimethylbutane	40.00	42.30	105.8
Cyclopentane	21.00	19.51	92.9
2,3-Dimethylbutane	51.00	55.18	108.2
2-Methylpentane	21.00	21.98	104.7
3-Methylpentane	41.00	42.00	102.4
1-Hexene	61.00	59.56	97.6
1-Hexane	30.00	30.90	103.0
Methylcyclopentane	26.00	26.54	102.1
2,4-Dimethylpentane	40.00	41.76	104.4
Benzene	31.00	29.94	96.6
Cyclohexane	42.00	42.73	101.7
2-Methylhexane	25.00	25.71	102.9
2,3-Dimethylpentane	54.00	54.89	101.6
3-Methylhexane	26.00	26.39	101.5
2,2,4-Trimethylpentane	31.00	31.68	102.2
n-Heptane	26.00	25.67	98.7
Methylcyclohexane	31.00	32.15	103.7
2,3,4-Trimethylpentane	25.00	26.08	104.3
Toluene	40.00	37.60	94.0
2-Methylheptane	25.00	25.74	103.0
3-Methylheptane	25.00	26.37	105.5
n-Octane	31.00	30.10	97.1
Ethylbenzne	25.00	23.59	94.4
m/p-Xylene	42.00	37.92	90.3
Styrene	41.00	33.75	82.3
o Xylene	26.00	25.16	96.8
n-Nonane	25.00	24.62	98.5
Cumene	40.00	39.60	99.0
n-Propylbenzene	30.00	28.33	94.4
m-Ethyltoluene	25.00	24.39	97.6
p-Ethyltoluene	43.00	39.57	92.0
1,3,5-Trimethylbenzene	26.00	24.83	95.5
o-Ethyltouene	27.00	29.88	110.7
1,2,4-trimethylbenzene	39.00	38.24	98.0
n-Decane	30.00	29.34	97.8
1,2,3-Trimethylbenzene	25.00	25.73	102.9
m-Diethylbenzene	40.00	38.37	95.9
p-Diethylbenzene	27.00	23.68	87.7
n-Undecane	41.00	28.30	69.0





**MATHESON  
TRI-GAS**

**Certified Mixture Grade**

**Matheson Tri-Gas**

6874 S Main Street

Morrow, GA 30260

Phone: (770) 961-7891

Fax: (770) 968-1268

*PAMS*

To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd  
Baton Rouge, LA 70802

**TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE  
GREATER THAN PROCESS PRESSURE.**

Phone:  
Fax:

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057410185

**PRODUCT:**

CYLINDER NUMBER: CC-250112

SIZE: 11

CGA/DISS OUTLET: 350

CONTENT: 131 cu. ft.

PRESSURE: 1850 psig

Fill Date: 12/3/2007

Certification Date: 12/3/2007

Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Ethylene	20 ppbC	21 ppbC	+/- 5%
Ethane	25 ppbC	26 ppbC	+/- 5%
Acetylene	40 ppbC	42 ppbC	+/- 5%
Propylene	25 ppbC	26 ppbC	+/- 5%
Propane	40 ppbC	40 ppbC	+/- 5%
Isobutane	25 ppbC	25 ppbC	+/- 5%
1-Butene	30 ppbC	32 ppbC	+/- 5%
1,3-Butadiene	30 ppbC	32 ppbC	+/- 5%
n-Butane	40 ppbC	43 ppbC	+/- 5%
trans-2-Butene	25 ppbC	26 ppbC	+/- 5%
cis-2-Butene	35 ppbC	38 ppbC	+/- 5%
Isopentane	40 ppbC	40 ppbC	+/- 5%
1-Pentene	25 ppbC	25 ppbC	+/- 5%
n-Pentane	25 ppbC	26 ppbC	+/- 5%
Isoprene	40 ppbC	42 ppbC	+/- 5%
trans-2-Pentene	25 ppbC	25 ppbC	+/- 5%
cis-2-Pentene	35 ppbC	34 ppbC	+/- 5%
Cyclopentene	20 ppbC	21 ppbC	+/- 5%
2,2-Dimethylbutane	40 ppbC	40 ppbC	+/- 5%
2-Methylpentane	20 ppbC	21 ppbC	+/- 5%
3-Methylpentane	40 ppbC	41 ppbC	+/- 5%
2,3-Dimethylbutane	50 ppbC	51 ppbC	+/- 5%
1-Hexene	60 ppbC	61 ppbC	+/- 5%
n-Hexane	30 ppbC	30 ppbC	+/- 5%
Methylcyclopentane	25 ppbC	26 ppbC	+/- 5%
2,4-Dimethylpentane	40 ppbC	40 ppbC	+/- 5%
Benzene	30 ppbC	31 ppbC	+/- 5%
Cyclohexane	40 ppbC	42 ppbC	+/- 5%
2,3-Dimethylpentane	50 ppbC	54 ppbC	+/- 5%
2-Methylhexane	25 ppbC	25 ppbC	+/- 5%
3-Methylhexane	25 ppbC	26 ppbC	+/- 5%
n-Heptane	25 ppbC	26 ppbC	+/- 5%
2,2,4-Trimethylpentane	30 ppbC	31 ppbC	+/- 5%
Methylcyclohexane	30 ppbC	31 ppbC	+/- 5%
2,3,4-Trimethylpentane	25 ppbC	25 ppbC	+/- 5%

*Received on 12/11/07*

TRACEABLE TO REFERENCE STANDARD SOURCE/NUMBER:

TRACEABLE TO NIST TRACEABLE WEIGHT CERTIFICATE:



# MATHESON TRI-GAS

**Certified Mixture Grade**

**Matheson Tri-Gas**

6874 S Main Street

Morrow, GA 30260

Phone: (770) 961-7891

Fax: (770) 968-1268

To: Environmental Quality  
DEQ Laboratory Services  
Central Receiving  
1209 Leesville Rd

**TO AVOID BACKFILL, CYLINDER PRESSURE MUST BE  
GREATER THAN PROCESS PRESSURE.**

Phone:  
Fax:

SALES ORDER NUMBER: 427497  
P.O. NUMBER: 3243638  
LOT NUMBER: 1057410185

**PRODUCT:**

CYLINDER NUMBER: CC-250112  
SIZE: 1l  
CGA/DISS OUTLET: 350  
CONTENT: 131 liters  
PRESSURE: 1850 psig

Fill Date: 12/3/2007  
Certification Date: 12/3/2007  
Expiration Date: 12/3/2008

COMPONENT	REQUESTED CONCENTRATION	CERTIFIED CONCENTRATION	CERTIFICATION ACCURACY
Toluene	40 ppbC	40 ppbC	+/- 5%
2-Methylheptane	25 ppbC	25 ppbC	+/- 5%
3-Methylheptane	25 ppbC	25 ppbC	+/- 5%
n-Octane	30 ppbC	31 ppbC	+/- 5%
Ethylbenzene	25 ppbC	25 ppbC	+/- 5%
p-Xylene	20 ppbC	21 ppbC	+/- 5%
m-Xylene	20 ppbC	21 ppbC	+/- 5%
Styrene	40 ppbC	41 ppbC	+/- 5%
o-Xylene	25 ppbC	26 ppbC	+/- 5%
n-Nonane	25 ppbC	25 ppbC	+/- 5%
Isopropylbenzene	40 ppbC	40 ppbC	+/- 5%
n-Propylbenzene	30 ppbC	30 ppbC	+/- 5%
n-Decane	30 ppbC	30 ppbC	+/- 5%
m-Diethylbenzene	40 ppbC	40 ppbC	+/- 5%
p-Diethylbenzene	25 ppbC	27 ppbC	+/- 5%
n-Dodecane	30 ppbC	31 ppbC	+/- 5%
m-Ethyltoluene	25 ppbC	25 ppbC	+/- 5%
o-Ethyltoluene	30 ppbC	27 ppbC	+/- 5%
p-Ethyltoluene	40 ppbC	43 ppbC	+/- 5%
n-Undecane	40 ppbC	41 ppbC	+/- 5%
1,2,3-Trimethylbenzene	25 ppbC	25 ppbC	+/- 5%
1,3,5-Trimethylbenzene	25 ppbC	26 ppbC	+/- 5%
1,2,4-Trimethylbenzene	40 ppbC	39 ppbC	+/- 5%
Nitrogen, Balance			

**SPECIAL INFORMATION / ADDITIONAL COMMENTS**

*Received 12/6/07*

The product listed above and furnished under the referenced purchase order has been tested and found to contain the component concentration listed above. All values in mole/mole basis gas phase unless otherwise indicated. Matheson Tri-Gas warrants that the above product(s) conform at the time of shipment to the above description. Matheson Tri-Gas' liability does not exceed the value of the product purchased.

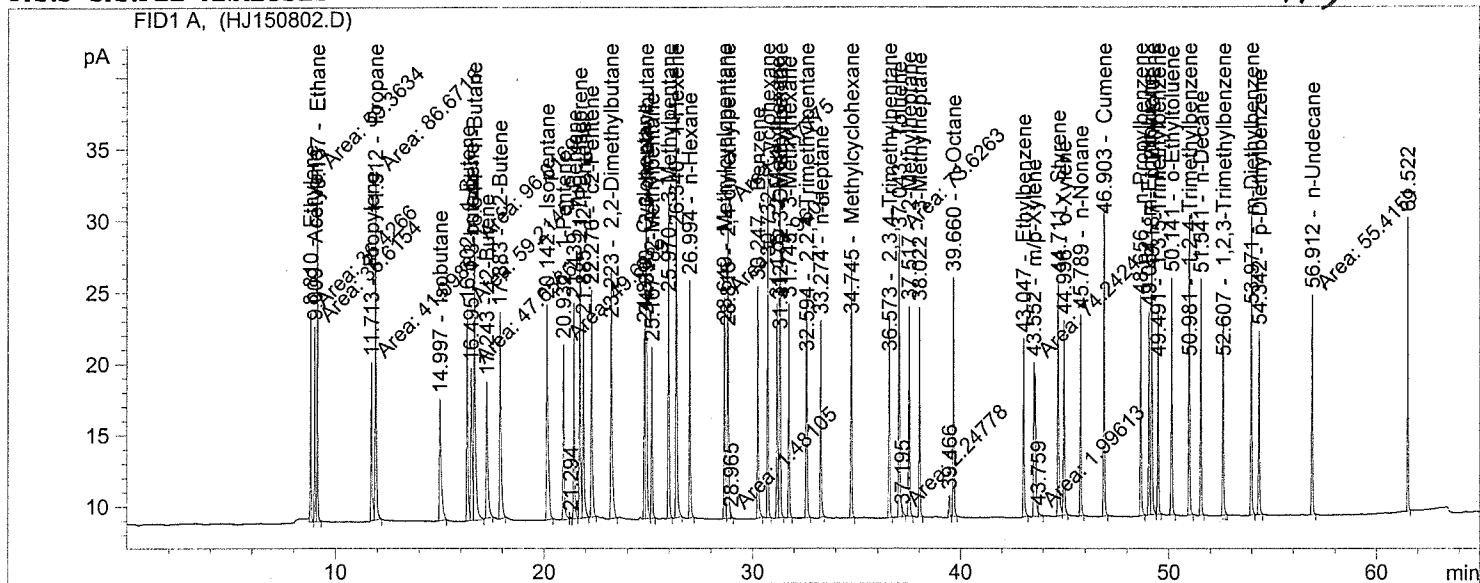
Derek Stuck  
ANALYST

12/4/2007  
DATE SIGNED

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=====
Injection Date   : 10/15/2008 9:36:44 AM      Seq. Line   :    2
Sample Name     : AL22735 $I_PPFID           Location    : Vial 3
Acq. Operator   : JAK                        Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026          Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/15/2008 6:38:05 AM by JAK
                  (modified after loading)
    
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PAMS SAMPLE ANALYSES



External Standard Report

```

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Sorted By      :      Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier     :      0.5107
Dilution       :      1.0000
Sample Amount  :      1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
    
```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.810	MF	36.42662	1.00000	18.60307		Ethylene
9.009	MF	36.61538	1.00000	18.69948		Acetylene
9.137	FM	59.36336	1.00000	30.31687		Ethane
11.713	MF	41.09826	1.00000	20.98888		Propylene
11.912	FM	86.67178	1.00000	44.26328		Propane
14.997	PB +	50.92107	1.00000	26.00539		Isobutane
16.302	MF	59.21451	1.00000	30.24085		1-Butene
16.495	MF	47.65863	1.00000	24.33926		1,3-butadiene
16.644	FM	96.01686	1.00000	49.03581		n-Butane
17.243	BB	49.41847	1.00000	25.23801		t2-Butene
17.883	PB	69.98669	1.00000	35.74220		c2-Butene
20.142	PB	81.05223	1.00000	41.39337		Isopentane
20.932	MM	49.68890	1.00000	25.37612		1-Pentene
21.439	VB	50.42939	1.00000	25.75429		n-Pentane
21.719	BV	73.07383	1.00000	37.31880		Isoprene
21.885	VB	54.14959	1.00000	27.65420		t2-Pentene
22.276	PB	65.50764	1.00000	33.45475		c2-Pentene
23.223	BB	82.83418	1.00000	42.30341		2,2-Dimethylbutane
24.810	BV	38.20219	1.00000	19.50986		Cyclopentane

10-15-08

JAK



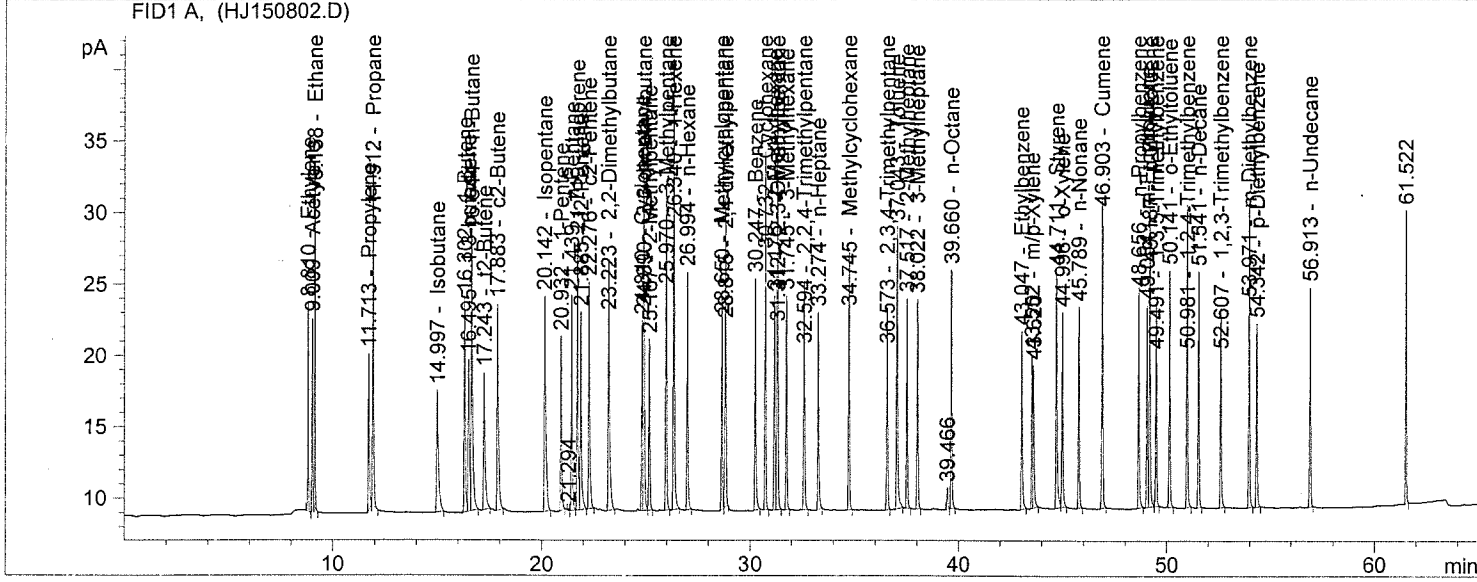
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=====
Injection Date   : 10/15/2008 9:36:44 AM      Seq. Line   :    2
Sample Name     : AL22735 $I_PPFID           Location    : Vial 3
Acq. Operator   : JAK                        Inj         :    1
Acq. Instrument : HP_FID2 SOP 1026           Inj Volume  : Manually
Acq. Method     : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 8/4/2008 1:18:53 PM by JPC
Analysis Method : C:\HPCHEM\1\METHODS\PAMS.M
Last changed    : 10/15/2008 6:38:05 AM by JAK
                  (modified after loading)
=====

```

PAMS SAMPLE ANALYSES

G1152



External Standard Report

```

=====
Sorted By       : Signal
Calib. Data Modified : 8/4/2008 10:57:02 AM
Multiplier      : 0.5107
Dilution        : 1.0000
Sample Amount    : 1.00000 [ppbc] (not used in calc.)
Use Multiplier & Dilution Factor with ISTDs
=====

```

Signal 1: FID1 A,

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
8.810	BBA	35.39693	1.00000	18.07721		Ethylene
9.009	PB	34.71106	1.00000	17.72694		Acetylene
9.138	BBA	55.52883	1.00000	28.35857		Ethane
11.713	PB	38.56823	1.00000	19.69679		Propylene
11.912	BBA	82.35966	1.00000	42.06108		Propane
14.997	PB +	50.92107	1.00000	26.00539		Isobutane
16.302	BV	59.12079	1.00000	30.19299		1-Butene
16.495	VV	46.62464	1.00000	23.81120		1,3-butadiene
16.644	VB	93.29193	1.00000	47.64419		n-Butane
17.243	BB	49.41847	1.00000	25.23801		t2-Butene
17.883	PB	69.98669	1.00000	35.74220		c2-Butene
20.142	PB	81.05223	1.00000	41.39337		Isopentane
20.932	PB	47.55657	1.00000	24.28714		1-Pentene
21.439	VB	50.42939	1.00000	25.75429		n-Pentane
21.719	BV	73.07383	1.00000	37.31880		Isoprene
21.885	VB	54.14959	1.00000	27.65420		t2-Pentene
22.276	PB	65.50764	1.00000	33.45475		c2-Pentene
23.223	BB	82.83418	1.00000	42.30341		2,2-Dimethylbutane
24.810	BV	38.20219	1.00000	19.50986		Cyclopentane

J

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
24.890	VV	108.04584	1.00000	55.17901		2,3-dimethylbutane
25.167	VB	43.03400	1.00000	21.97746		2-Methylpentane
25.970	BB	82.23936	1.00000	41.99964		3-Methylpentane
26.340	BB	116.62192	1.00000	59.55881		1-Hexene
26.994	PB	60.49696	1.00000	30.89580		n-Hexane
28.650	PV	51.14455	1.00000	26.11952		Methylcyclopentane
28.815	VB	79.06260	1.00000	40.37727		2,4-dimethylpentane
30.247	BB +	58.62331	1.00000	29.93892		Benzene
30.732	BB	83.66541	1.00000	42.72792		Cyclohexane
31.176	BV	50.34966	1.00000	25.71357		2-Methylhexane
31.312	VB	107.47405	1.00000	54.88700		2,3-Dimethylpentane
31.745	BB	51.67727	1.00000	26.39158		3-Methylhexane
32.594	BB	62.03165	1.00000	31.67956		2,2,4-Trimethylpentane
33.274	BB	50.27158	1.00000	25.67369		n-Heptane
34.745	BB	62.95742	1.00000	32.15235		Methylcyclohexane
36.573	BB	51.06190	1.00000	26.07731		2,3,4-Trimethylpentane
37.043	PB +	74.92414	1.00000	38.26376		Toluene
37.517	BB	50.40670	1.00000	25.74270		2-Methylheptane
38.022	BB	51.63241	1.00000	26.36867		3-Methylheptane
39.660	BB	58.93094	1.00000	30.09603		n-Octane
43.047	BB	46.18818	1.00000	23.58830		Ethylbenzene
43.552	BV	34.00242	1.00000	17.36504		m/p-Xylene
44.711	BV	66.07603	1.00000	33.74503		Styrene
44.996	VB	49.26915	1.00000	25.16175		o-Xylene
45.789	BB	48.20452	1.00000	24.61805		n-Nonane
46.903	BB	77.54693	1.00000	39.60322		Cumene
48.656	BB	55.46711	1.00000	28.32705		n-Propylbenzene
49.054	BV	47.76506	1.00000	24.39362		m-Ethyltoluene
49.187	VV	77.47455	1.00000	39.56625		p-Ethyltoluene
49.491	VB	48.61859	1.00000	24.82951		1,3,5-Trimethylbenzene
50.141	VB	58.51747	1.00000	29.88487		o-Ethyltoluene
50.981	BB	74.87322	1.00000	38.23775		1,2,4-Trimethylbenzene
51.541	BB	57.45391	1.00000	29.34171		n-Decane
52.607	BB	50.38995	1.00000	25.73415		1,2,3-Trimethylbenzene
53.971	BB	75.13081	1.00000	38.36930		m-Diethylbenzene
54.342	BB	46.36736	1.00000	23.67981		p-Diethylbenzene
56.913	BB +	55.06075	1.00000	28.11952		n-Undecane

Totals : 1752.61597

Uncalibrated Peaks : using compound Propane

RetTime [min]	Type	Area [pA*s]	Amt/Area	Amount [ppbc]	Grp	Name
21.294	PP	4.32705e-1	1.00000	2.20982e-1	?	
39.466	PB	5.65023	1.00000	2.88557	?	
43.620	VB	39.99233	1.00000	20.42408	?	
61.522	BB	59.42428	1.00000	30.34798	?	

Uncalib. totals : 53.87862

Results obtained with enhanced integrator!

1 Warnings or Errors :

Warning : Calibration warnings (see calibration table listing)

\*\*\* End of Report \*\*\*

## **APPENDIX I**

Comparison of Carbon Monoxide and Alkane Mixture Concentrations  
for 9 Barge Emissions Events to Investigate the Contribution of  
Emissions from Tugs

**Appendix I: Comparison of Carbon Monoxide and Alkane Mixture Concentrations for 9 Barge Emissions Events to Investigate the Contribution of Emissions from Tugs**

This appendix presents the results of a comparison of carbon monoxide and alkane mixture concentrations analyzed along the ground level beam path of the ARCADIS OP-FTIR VRPM configuration during nine emissions events from barges classified as empty. The analysis was performed to evaluate the contribution of exhaust from the tugs to the Alkane Mixture (AM) emissions fluxes measured during the project.

**Table I-1. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 9/28/2009 9:38 to 10:11 Event**

Time	Alkane Mixture Concentration (ppb)	Carbon Monoxide Concentration (ppb)
9/28/2008 9:40	33.4	240
9/28/2008 9:43	38.4	404
9/28/2008 9:45	31.0	252
9/28/2008 9:48	34.5	228
9/28/2008 9:51	21.9	136
9/28/2008 9:53	18.6	103
9/28/2008 9:56	18.3	93.0
9/28/2008 9:59	17.7	92.3
9/28/2008 10:01	29.3	95.4
9/28/2008 10:04	5.93	82.1
9/28/2008 10:07	7.12	72.4
9/28/2008 10:09	7.27	73.0

**Table I-2. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 9/29/2009 14:13 to 14:57 Event**

Time	Alkane Mixture Concentration (ppb)	Carbon Monoxide Concentration (ppb)
9/29/2008 14:14	11.5	22.1
9/29/2008 14:17	ND	16.3
9/29/2008 14:20	6.46	ND
9/29/2008 14:22	7.18	20.9
9/29/2008 14:25	13.7	29.8
9/29/2008 14:28	13.0	30.6
9/29/2008 14:31	10.7	29.5
9/29/2008 14:33	13.4	19.3
9/29/2008 14:36	18.7	22.4
9/29/2008 14:39	26.0	20.1
9/29/2008 14:41	26.9	28.1
9/29/2008 14:44	25.6	18.4
9/29/2008 14:47	20.7	31.1
9/29/2008 14:49	20.1	41.2
9/29/2008 14:52	26.5	45.1
9/29/2008 14:55	27.7	136

ND= not detected



**Table I-3. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 10/2/2009 8:32 to 9:23 Event**

<b>Time</b>	<b>Alkane Mixture Concentration (ppb)</b>	<b>Carbon Monoxide Concentration (ppb)</b>
10/2/2008 8:33	12.8	347
10/2/2008 8:36	36.5	376
10/2/2008 8:39	47.8	419
10/2/2008 8:41	27.2	350
10/2/2008 8:44	34.3	333
10/2/2008 8:47	12.7	315
10/2/2008 8:49	30.4	336
10/2/2008 8:52	22.3	325
10/2/2008 8:55	37.1	328
10/2/2008 8:57	55.4	331
10/2/2008 9:00	54.7	368
10/2/2008 9:02	53.1	344
10/2/2008 9:05	44.3	354
10/2/2008 9:08	39.1	346
10/2/2008 9:10	25.8	310
10/2/2008 9:13	28.0	306
10/2/2008 9:16	25.1	299
10/2/2008 9:18	48.2	404
10/2/2008 9:21	24.2	304

**Table I-4. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 10/4/2009 13:12 to 13:46 Event**

<b>Time</b>	<b>Alkane Mixture Concentration (ppb)</b>	<b>Carbon Monoxide Concentration (ppb)</b>
10/4/2008 13:13	ND	19.6
10/4/2008 13:15	ND	27.2
10/4/2008 13:18	ND	58.2
10/4/2008 13:21	ND	151
10/4/2008 13:23	5.00	26.6
10/4/2008 13:26	ND	27.2
10/4/2008 13:29	5.18	23.9
10/4/2008 13:31	ND	22.7
10/4/2008 13:34	ND	31.3
10/4/2008 13:37	ND	32.6
10/4/2008 13:39	4.63	32.8
10/4/2008 13:42	ND	27.6
10/4/2008 13:45	4.37	30.3

ND= not detected

**Table I-5. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 10/6/2009 12:28 to 13:00 Event**

<b>Time</b>	<b>Alkane Mixture Concentration (ppb)</b>	<b>Carbon Monoxide Concentration (ppb)</b>
10/6/2008 12:29	ND	ND
10/6/2008 12:32	ND	ND
10/6/2008 12:35	ND	ND
10/6/2008 12:37	6.56	ND
10/6/2008 12:40	7.89	ND
10/6/2008 12:43	ND	ND
10/6/2008 12:45	10.8	ND
10/6/2008 12:48	ND	ND
10/6/2008 12:51	ND	ND
10/6/2008 12:53	ND	12.4
10/6/2008 12:56	12.5	ND
10/6/2008 12:59	6.44	9.93

ND= not detected

**Table I-6. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 10/8/2009 12:53 to 13:25 Event**

<b>Time</b>	<b>Alkane Mixture Concentration (ppb)</b>	<b>Carbon Monoxide Concentration (ppb)</b>
10/8/2008 12:53	5.80	32.2
10/8/2008 12:56	ND	43.7
10/8/2008 12:58	ND	44.7
10/8/2008 13:01	ND	66.1
10/8/2008 13:04	ND	58.7
10/8/2008 13:06	36.5	59.1
10/8/2008 13:09	28.7	51.7
10/8/2008 13:12	ND	80.0
10/8/2008 13:14	ND	32.8
10/8/2008 13:17	ND	32.6
10/8/2008 13:20	ND	59.5
10/8/2008 13:22	8.71	74.3
10/8/2008 13:25	8.49	53.1

ND= not detected

**Table I-7. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 10/9/2009 8:07 to 8:38 Event**

<b>Time</b>	<b>Alkane Mixture Concentration (ppb)</b>	<b>Carbon Monoxide Concentration (ppb)</b>
10/9/2008 8:07	ND	128
10/9/2008 8:12	12.0	118
10/9/2008 8:15	ND	140
10/9/2008 8:17	21.9	119
10/9/2008 8:20	32.7	110
10/9/2008 8:23	45.1	146
10/9/2008 8:25	ND	134
10/9/2008 8:28	ND	159
10/9/2008 8:31	7.11	140
10/9/2008 8:33	28.1	143
10/9/2008 8:36	21.8	122

ND= not detected

**Table I-8. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 10/9/2009 12:23 to 13:45 Event**

<b>Time</b>	<b>Alkane Mixture Concentration (ppb)</b>	<b>Carbon Monoxide Concentration (ppb)</b>
10/9/2008 12:23	18.5	33.6
10/9/2008 12:26	22.9	34.4
10/9/2008 12:29	18.9	47.2
10/9/2008 12:31	31.8	23.7
10/9/2008 12:34	41.6	45.0
10/9/2008 12:37	31.8	29.0
10/9/2008 12:40	23.3	35.2
10/9/2008 12:42	24.4	39.8
10/9/2008 12:45	22.0	30.5
10/9/2008 12:48	16.2	22.6
10/9/2008 12:50	17.9	13.5
10/9/2008 12:53	16.5	18.7
10/9/2008 12:56	22.5	30.7
10/9/2008 12:58	23.0	46.6
10/9/2008 13:01	32.3	59.5
10/9/2008 13:04	26.9	36.2
10/9/2008 13:06	25.6	39.1
10/9/2008 13:09	23.1	42.3
10/9/2008 13:12	31.0	33.9
10/9/2008 13:14	26.1	40.0
10/9/2008 13:17	26.7	30.1
10/9/2008 13:20	33.0	47.8
10/9/2008 13:22	27.1	31.6
10/9/2008 13:25	11.3	23.2
10/9/2008 13:28	13.0	ND
10/9/2008 13:30	30.2	54.1
10/9/2008 13:33	28.7	34.8
10/9/2008 13:36	26.3	59.4
10/9/2008 13:38	28.1	36.1
10/9/2008 13:41	20.7	31.6
10/9/2008 13:44	11.4	19.6

ND= not detected

**Table I-9. Comparison of Carbon Monoxide and Alkane Mixture Concentrations from the 10/9/2009 14:05 to 14:34 Event**

<b>Time</b>	<b>Alkane Mixture Concentration (ppb)</b>	<b>Carbon Monoxide Concentration (ppb)</b>
10/9/2008 14:05	7.55	ND
10/9/2008 14:08	5.05	ND
10/9/2008 14:11	7.76	ND
10/9/2008 14:13	22.3	34.8
10/9/2008 14:16	19.4	28.4
10/9/2008 14:19	13.5	ND
10/9/2008 14:21	20.1	30.7
10/9/2008 14:24	24.1	ND
10/9/2008 14:27	26.4	ND
10/9/2008 14:30	26.1	ND
10/9/2008 14:32	23.1	31.9

ND= not detected

## **APPENDIX J**

Comments from The American Waterways Operators and Response  
to Comments by Sage Environmental.



**The American Waterways Operators**  
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Lynn M. Muench  
Senior Vice President - Regional Advocacy

August 3, 2009

Dr. Eben Thoma  
Office of Research and Development  
National Risk Management Laboratory  
U.S. Environmental Protection Agency  
109 TW Alexander Drive  
Research Triangle Park, NC 27711

RE: Suggested Revisions to EPA Report:  
“Investigation of Fugitive Emissions from  
Petrochemical Transport Barges using Optical  
Remote Sensing”

Dear Dr. Thoma:

I would like to begin first by thanking EPA for allowing industry to peer review EPA’s draft report entitled, “Investigation of Fugitive Emissions from Petrochemical Transport Barges using Optical Remote Sensing.” As you well know, the members of The American Waterways Operators (AWO) have been and will continue to be proactive in addressing inadvertent tank barge emissions.

In 2006, AWO members created the Tank Barge Emissions Working Group (Working Group). The group has collaborated with the Louisiana Department of Environmental Quality (LDEQ), the Texas Commission for Environmental Quality (TCEQ), the Coast Guard and the Chemical Transportation Advisory Committee (CTAC) to implement necessary changes to mitigate inadvertent emissions. The group first developed Best Management Practices (BMPs) to reduce inadvertent emissions from tank barges in 2006. This document is not only an AWO member standard but was also cited in TCEQ’s State Implementation Plan as an initiative that contributes to emissions reductions in Texas. To work towards continual improvement, the Working Group updated and improved the BMP in 2009 and forwarded the draft to CTAC for review. AWO also has a history of working closely with LDEQ. In April AWO formally partnered with the agency through a Memorandum of Understanding (MOU) to monitor emissions from tank barges in the Baton Rouge nonattainment area.

It is in the same spirit of proactive environmental stewardship that the Working Group reached out to EPA in March 2009 to request the opportunity for a peer review of the EPA Report. That review was granted on June 24, and representatives from the Working Group were invited to participate. On behalf of the Working Group, I would like to express our concerns with the LDEQ report prepared by Sage Environmental entitled, “Bagging Test Report: Barge Emission Measurement Project Final Report” (Bagging Test Report), included as Appendix H of the EPA Report. *We believe that: 1) It is improper to extrapolate quantitative conclusions about tank barge emissions from such a small sample set, as was done on page 3 of the Bagging Test Report; and, 2) The methodologies employed to assess the emissions from the sample set cannot be accurately replicated.* The Working Group suggests the following revisions.

### *Bagging Test Report*

The Bagging Test Report states that “US EPA Protocol for Equipment Leak Emission Estimates 1995” (Appendix B of the LDEQ Bagging Test Report) was employed to measure the samples’ mass emissions. It also noted that the vacuum method was to be used exclusively. However, in reviewing the Bagging Test Report, the Working Group has come to the conclusion that the vacuum method was *not* used exclusively and, in fact, was not even employed properly. The Working Group has made the following observations regarding the Bagging Test Report:

- The vacuum method was only used for 8 of the 23 pieces of equipment sampled; 15 samples were not taken using the cited vacuum method and should therefore be considered invalid, as use of the sampling apparatus without the vacuum pump does not adhere to the prescribed method.
- In Appendix A of the Bagging Test Report it states that samples and/or pieces of equipment were tightened and/or manipulated in certain areas of the barge to increase the flow through other sample locations (i.e. hatches). This directly manipulated the piece of equipment prior to sampling and undoubtedly skewed the results.
- The aluminum summa canisters cited in the Bagging Test Report were used for multiple sample points so as to speciate emissions. Canisters should *not* have been used for multiple sample points across the barge, as this risks tainting the results of each sample analysis. To attain actual, valid results, one to three canisters should have been taken per sample point. We have concerns as to the type of bags employed and the way in which they were used during the study. The brand and type of bag is not referenced in the methods section of the report. The EPA Protocol suggests that impermeable material such as Mylar®, Tedlar®, Teflon®, aluminum foil, or aluminized Mylar® with a thickness ranging from 1.5 to 15 millimeters (mm) be used for the vacuum method. We are concerned that the samples may have reacted with the bagging material if the preceding materials were not used. Additionally, it is known that barge company personnel were asked to provide trash bags for sampling efforts and that these bags did not meet the minimum requirements of the EPA method as referenced above.

Also, we do not believe a correlation can be made between EPA’s Other Test Method (OTM 10) study, “Optical Remote Sensing for Emission Characterization from Non-Point Sources,” and the



LDEQ's bagging study for the following reasons: 1) Different barges/samples were used for the studies; 2) Meteorological conditions were not equivalent during the two studies; 3) The method of sample selection greatly differed between the two studies; and, 4) The EPA's OTM 10 study did not focus upon individual pieces of equipment like that of the LDEQ's bagging study.

The Working Group has significant concerns as to the lack of adherence to the cited method used to generate the data, the validity of the reported concentrations and the manner in which concentrations and observations were described. On behalf of the Working Group, ***I ask that the Bagging Test Report, Appendix H of the EPA Report, be removed and that all reference to the Bagging Test Report also be removed.***

*Barge Identification/Company Identification*

Additionally, AWO believes that it is inappropriate to single out a particular company by specifically referring to the company or unique barge number. These identification numbers are company specific and can be recognized. ***We ask that the barge identification numbers in Table 1 of the Bagging Test Report be removed.*** The identification numbers can simply be replaced with a sample number. ***We also request that any reference to specific company names be removed from the body of the main EPA Report, tables, and appendices.*** When the Working Group first reached out to EPA to request an opportunity to peer review this report, it was in the spirit of collaboration; and it is in that same spirit that I submit the suggested revisions on the Working Group's behalf. It is not in the best interests of either EPA or the tank barge industry to release a report with misleading or otherwise inappropriate data, and for this reason it is imperative that the concerns of the Working Group be reflected in the final EPA Report.

We greatly appreciate the opportunity to review and provide comments to the EPA on this draft. If you have any questions or would like further assistance in this matter please do not hesitate to contact me or any member of the Working Group.

Sincerely,

A handwritten signature in cursive script that reads "Lynn M. Muench". The signature is written in black ink and is positioned below the word "Sincerely,".

Lynn M. Muench

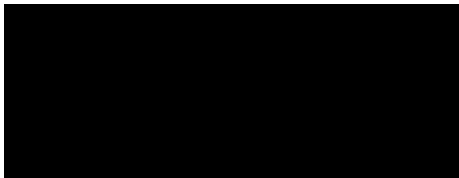


## **Sage Responses to the American Waterways Operators (AWO) Comments**

**AWO Comment:** We believe that: 1) It is improper to extrapolate quantitative conclusions about tank barge emissions from such a small sample set, as was done on page 3 of the Bagging Test Report; and, 2) The methodologies employed to assess the emissions from the sample set cannot be accurately replicated.

**Response to 1:** Sage stated in our report that there is uncertainty in extrapolating emissions from the barge measurements. We did not assume that the measured emissions would continue at the same rate for 24 hours per day and 365 days per year. We assumed that the measured emissions would only take place during the daylight warming times of the day, which we assumed would be an annual average of 12 hours per day (longer in the summer and shorter in the winter). The testing took place in late September, but the weather was unseasonably cool for that time period. As a result, the measured emission rates would have been less than a summer measurement and more than a winter measurement. As a rough estimate (which we called it in the report), the emissions as measured were considered to be close to an annual average rate. We extrapolated these emission rates for 12 hours per day and 365 days per year to arrive at the 465 tons per year estimate. There are obviously a number of uncertainties in this estimate, which is why it was called a rough estimate, but it does help to put the potential emission rates of the barges measured into terms that allow comparison to stationary facilities. There are uncertainties in every measurement and estimate. It is not improper to make an estimate that includes uncertainty if those uncertainties are noted as they were in the Sage report.

**Response to 2:** Sage personnel have tremendous experience and credibility in performing emission measurements, including personnel on the barge test project that were personally involved in the development of the bagging methodology during the middle 1970s. The barge emission points are quite different than components in stationary facilities, so some of the materials and methods had to be adapted to this new type of measurement. All of the methods used during the barge testing have been used in prior EPA testing, such as in the natural gas plant work. These methods provide technically sound measurements that could be replicated with reasonable accuracy.



**AWO Comment:** The Bagging Test Report states that “US EPA Protocol for Equipment Leak Emission Estimates 1995” (Appendix B of the LDEQ Bagging Test Report) was employed to measure the samples’ mass emissions. It also noted that the vacuum method was to be used exclusively. However, in reviewing the Bagging Test Report, the Working Group has come to the conclusion that the vacuum method was *not* used exclusively and, in fact, was not even employed properly.

**Response:** Sage and LDEQ had never intended to use the vacuum bagging method exclusively. The commenter may be confusing a statement that, when performing the bagging test, we would only use the vacuum method and not the blow-through method. The blow-through method is best suited for measuring default zero components, where the background VOC in ambient air would interfere with the low level measurements using the vacuum test. Sage and LDEQ had originally planned to use a number of measurement approaches, including the Hi-Flow Sampler™, the vacuum bagging method, direct dry gas meter (DGM) method, and a chimney/pitot tube method. A subcontractor, Heath Consultants, Inc, was to perform the Hi-Flow Sampler measurements, but they were unable to participate when the barge test was delayed because of Hurricane Ike. In hind sight, the Hi-Flow Sampler would not have been a good measurement tool for the barge emissions, since its high flow rate would have had the potential to over-estimate emissions by pulling emission from other points through the current test point. The chimney/pitot tube method was prepared for the field, but was not used because the vacuum bagging method and the direct DGM methods were able to accommodate the emissions encountered. The tests conducted were done using the vacuum bagging test and the direct DGM methods, both of which were conducted properly, with minor adjustments for the large sample points like hatches and stacks.

**Comment:** The vacuum method was only used for 8 of the 23 pieces of equipment sampled; 15 samples were not taken using the cited vacuum method and should therefore be considered invalid, as use of the sampling apparatus without the vacuum pump does not adhere to the prescribed method.

**Response:** The direct DGM method has been used in approved EPA testing for industries with large leaks, such as natural gas plants and compressor stations. Sage performed the direct DGM method using all the same equipment as the vacuum bagging test except for the pump. The direct DGM method was applied only where the bagged component was emitting at a rate faster than the pump could keep up with. The same component containment was used, the same flow measurement was used, the same temperature measurement was used, and the same pressure measurement was used for the direct DGM method as for the other components tested with the vacuum bagging method. The only difference is the component leak provided all the motive force for the flow measurement, which put the bag under positive pressure rather than the negative pressure of the vacuum bagging method. Having the bag under positive pressure would result in the leakage of gas around the bag seals, as well as displacement of leaks from the component being tested to other nearby leaking components. All factors that are different for the direct DGM test would cause a potential under-estimation, as was noted in the uncertainty discussion. The direct DGM method has not been written up as an EPA method, because it is



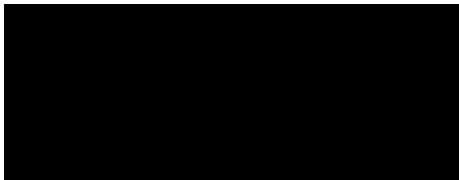
based on fundamental physics: contain the leak, route it through a flow measurement device, measure temperature/pressure to allow conversion to standard conditions, convert to moles, and apply the concentration and molecular weight of each compound to calculate the emissions. There is no reason to discount the 15 samples done by the direct DGM method so long as it is understood that this measurement could be biased low and represents the lower bound of the actual emission rate.

**Comment:** In Appendix A of the Bagging Test Report it states that samples and/or pieces of equipment were tightened and/or manipulated in certain areas of the barge to increase the flow through other sample locations (i.e. hatches). This directly manipulated the piece of equipment prior to sampling and undoubtedly skewed the results.

**Response:** The barge operators made some attempts to stop or reduce leakage from points where our measurements were complete. This was done to try to fix the leaks, as well as to see to what degree leaks visible to the FLIR camera could be eliminated. Some of these actions were noted to increase leak rates from nearby components, which was noted by seeing an increase in visible leak plumes using the FLIR camera. Most repair attempts were done after we had moved to other areas or left the barge entirely. While these repair attempts add another layer of uncertainty to the measurements, they were few enough in number that they are likely to only partially offset the under-estimating inherent in the direct DGM bagging (as described in the previous response).

**Comment:** The aluminum summa canisters cited in the Bagging Test Report were used for multiple sample points so as to speciate emissions. Canisters should *not* have been used for multiple sample points across the barge, as this risks tainting the results of each sample analysis. To attain actual, valid results, one to three canisters should have been taken per sample point.

**Response:** LDEQ handled the sample collection in summa canisters and their analyses, but Sage can comment briefly on this. No canister was filled for more than one sample point on a barge. Based on the assumption that the vapor spaces of the compartments, the relief header, and the stack were all connected, the LDEQ personnel began to only take one summa canister sample for every few components tested on the same barge. Some of the early barges tested had a sample taken for component bagged, and these showed that concentrations were very close to the same from point to point on the same barge (see results for tests 3, 4, and 5 for example). While it is possible that the barge vapor space is not perfectly mixed, the uncertainty associated with this assumption should not prevent attaining valid results.



**Comment:** We have concerns as to the type of bags employed and the way in which they were used during the study. The brand and type of bag is not referenced in the methods section of the report. The EPA Protocol suggests that impermeable material such as Mylar®, Tedlar®, Teflon®, aluminum foil, or aluminized Mylar® with a thickness ranging from 1.5 to 15 millimeters (mm) be used for the vacuum method. We are concerned that the samples may have reacted with the bagging material if the preceding materials were not used. Additionally, it is known that barge company personnel were asked to provide trash bags for sampling efforts and that these bags did not meet the minimum requirements of the EPA method as referenced above.

**Response:** The EPA Protocol is based on the work done over several decades at fixed facilities, and the materials recommended were based on what was reasonable for component sizes in stationary facilities. Materials such as Mylar, Tedlar, and Teflon were specified to minimize adsorption on the surface of the bag and diffusion through the bag. Sage brought supplies of Mylar to the test that had been sufficient for many previous tests at stationary facilities, but none were in sizes that would fit the large hatches and other large irregularly shaped components we faced on the barges. We shifted to use of heavy duty garbage bags to try to minimize the use of taped seams and poor conformance to irregular shapes that was noted for the heavier Mylar sheet. It is possible that surface adsorption occurred on the bag material, as it does to some extent regardless of the type of material. The components were bagged and allowed to fill the bag and emit for a period of time which allowed for a steady-state coating of bag surfaces to occur, which should minimize the effect of adsorption on the results. It is likely that more diffusion of hydrocarbons through the bag occurred with the polyethylene bags than would have happened with Mylar, but not necessarily more than through Mylar with multiple panels taped together and through crimped seals around the base of the hatches. The adaptation of large polyethylene bags was the best overall approach to bagging the extremely large components found on the barges. The flow rates through the bags (as measured with the dry gas meter) were high enough that reaction with the bag material should not have been a significant issue. If there were any reaction, it would have been as a solvent action reducing the thickness of the bag and allowing more diffusion. Again the measured results should be considered as a valid lower bound for actual emissions.

**Response Summary:** This was a first attempt to make measurements of vapor emissions from barges. We would likely approach the measurements somewhat differently based on the experience of that first test. Components in stationary facilities show very little difference in emission rate as a factor of pressure on the outside of the seal and the emission rates from one component are not affected by changes around a nearby component on the same line. Barge components, on the other hand, are very much affected by conditions on nearby components. The barges are mostly rated for 1 psi and will start to leak at the pressure relief valve even if all other potential leak points are sealed. The most valid way to make field measurements of total barge emissions would be to perfectly seal all emission points except the pressure relief valve, and then to measure the emission rate at the pressure relief valve. Unfortunately, it is not really possible to achieve perfect seals on all potential leak areas or to simultaneously measure all potential leak areas. An alternate approach in the future might be to use the TANKS software to model emissions from a barge as if it were an atmospheric storage tank(s).



As might be expected in making the first set of measurements for a source category, there were a number of difficulties encountered, a number of adaptations to the Protocol methods, and many uncertainties. Taken as a whole, there are more uncertainties that indicate the emissions were under-estimated than that indicate over-estimation. The tests done should be considered a valid first attempt to measure a new source category and be interpreted roughly as a lower bound of the actual emissions.

*Graham E. Harris*

Principal Engineer  
Sage Environmental Consulting L.P.  
19 August 2009