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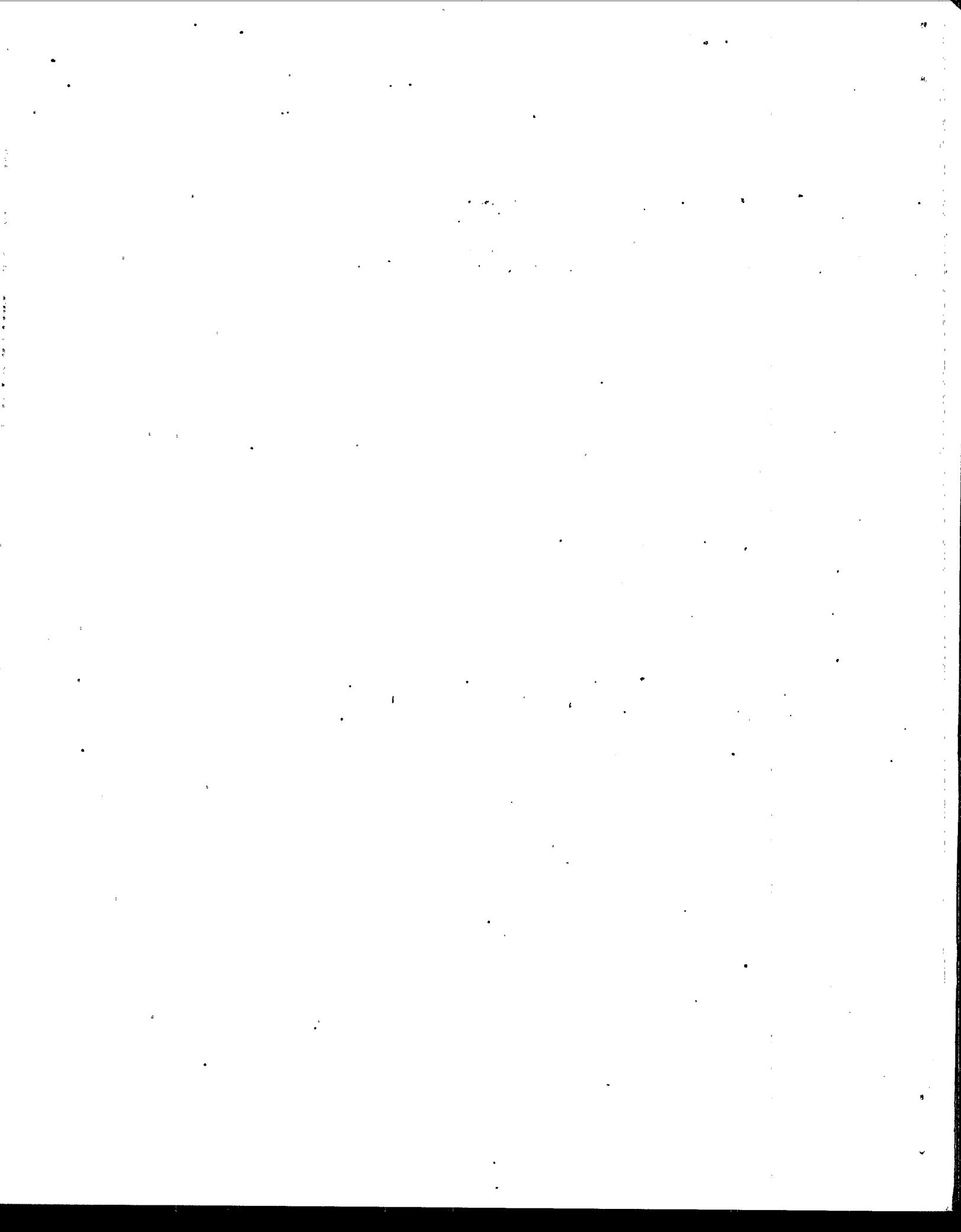
Office of Air Quality  
Planning and Standards  
Research Triangle Park NC 27711

EPA-450/2-90-009  
May 1990

Air



# **LOCATING AND ESTIMATING AIR TOXICS EMISSIONS FROM SEWAGE SLUDGE INCINERATORS**



# LOCATING AND ESTIMATING AIR TOXICS EMISSIONS FROM SEWAGE SLUDGE INCINERATORS

By

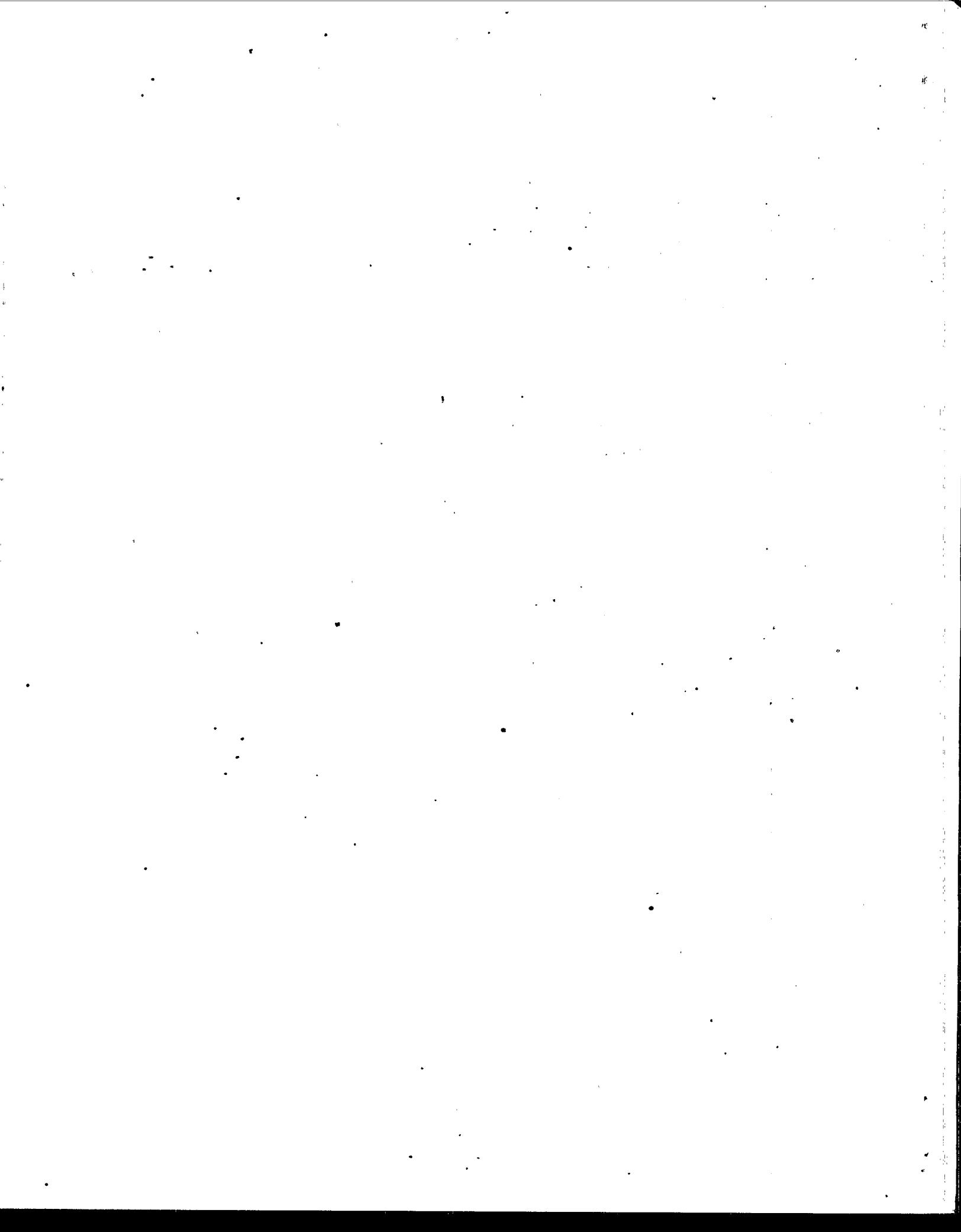
Radian Corporation  
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EPA Contract No. 68-02-4392

EPA Project Officer: William B. Kuykendal

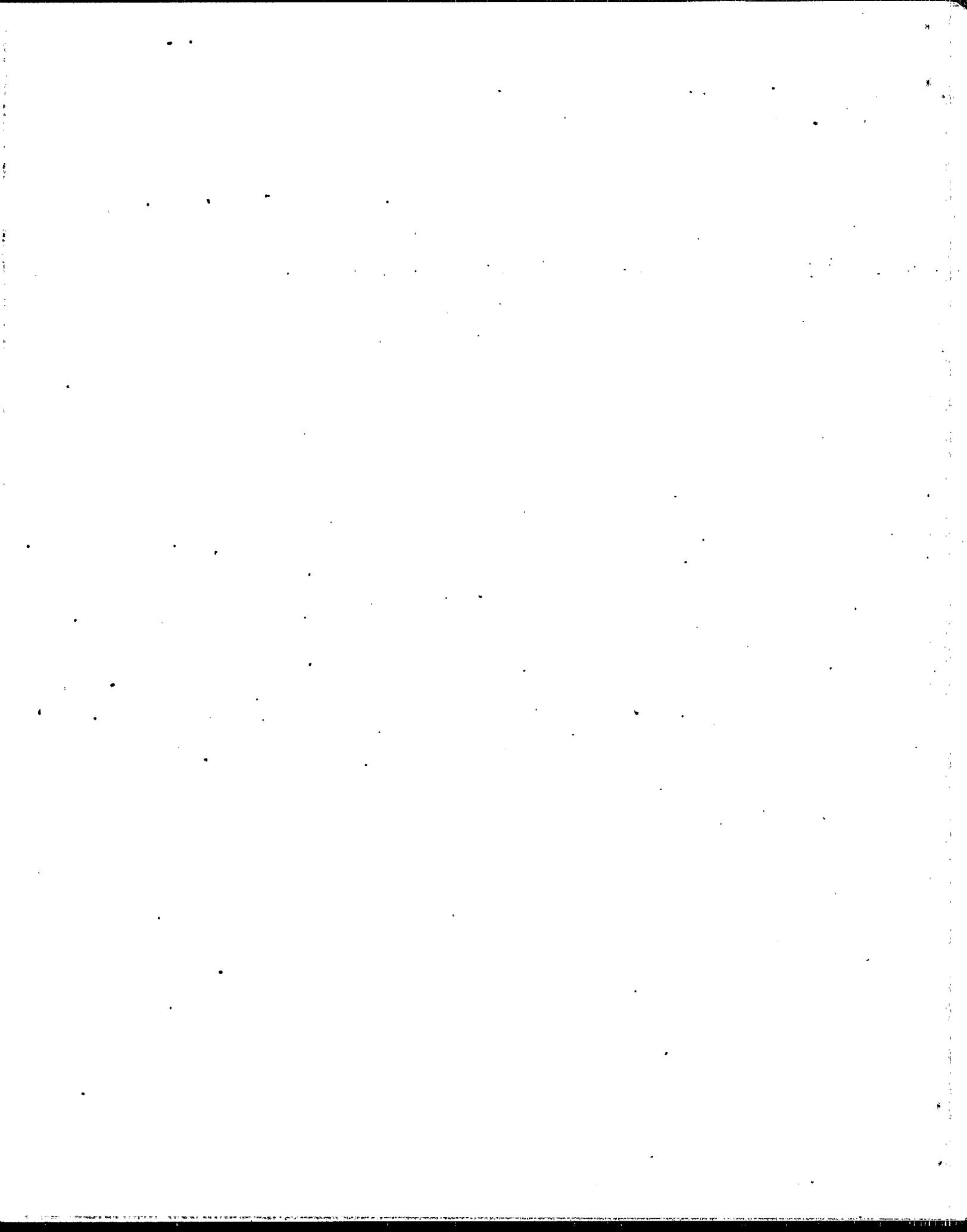
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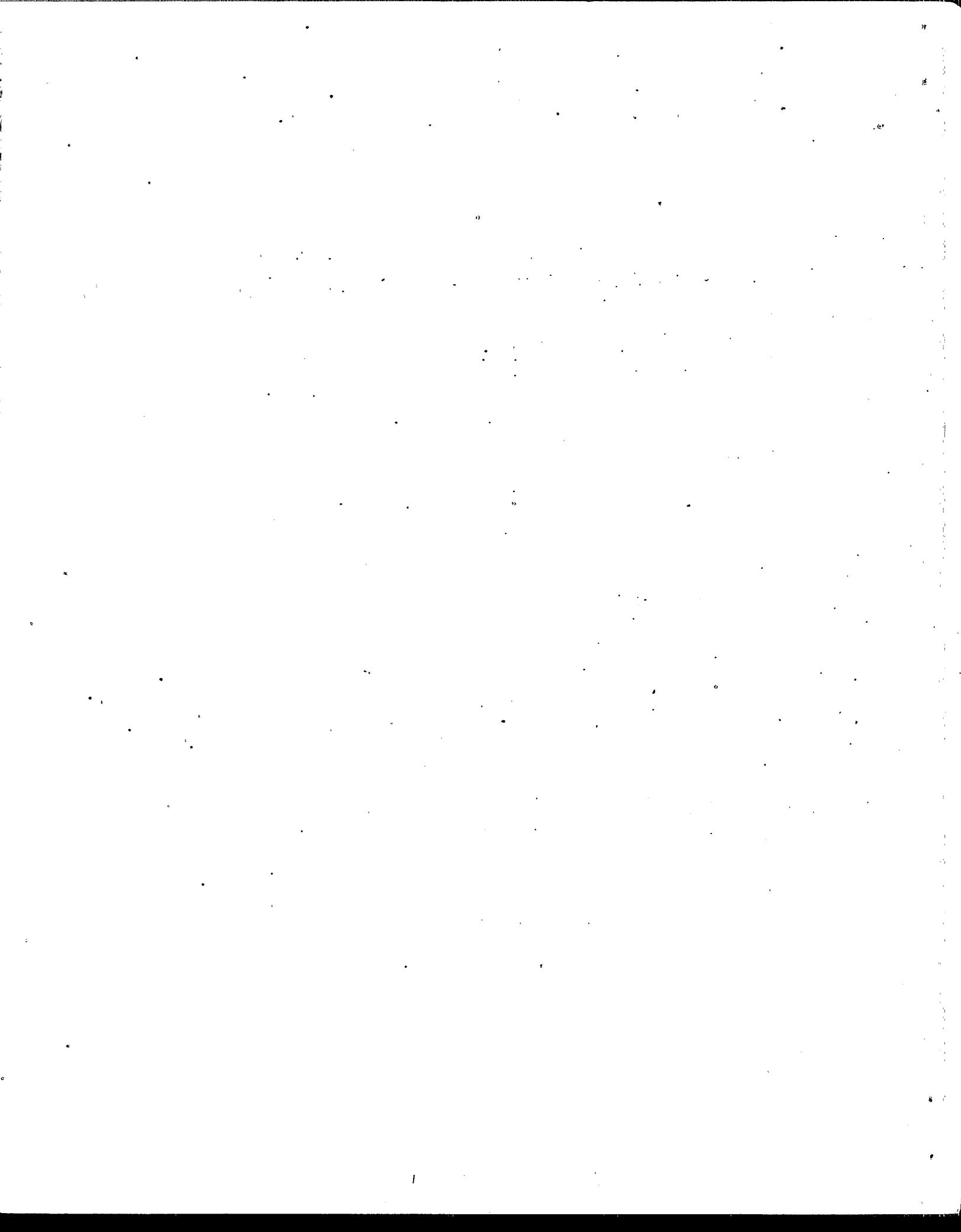
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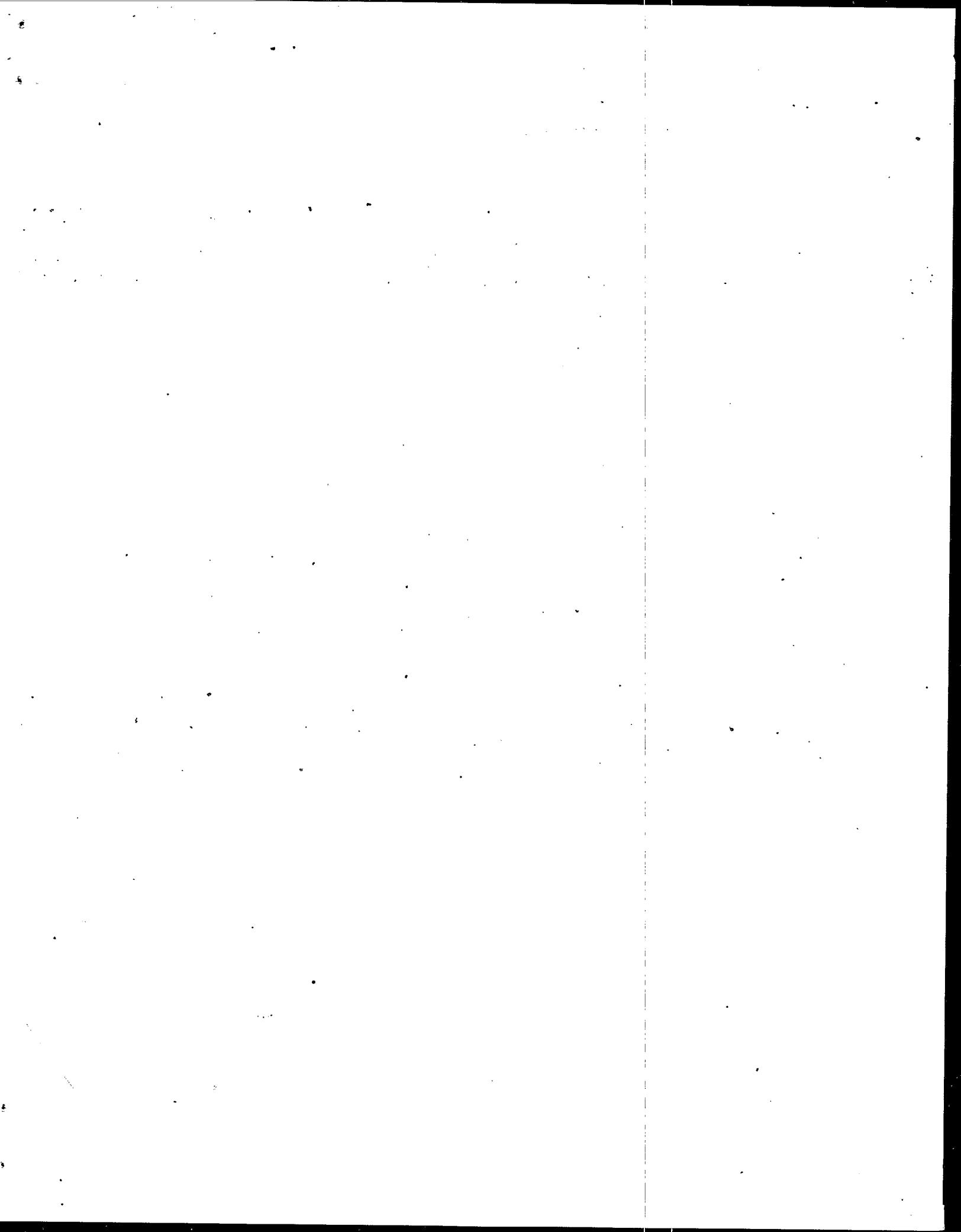
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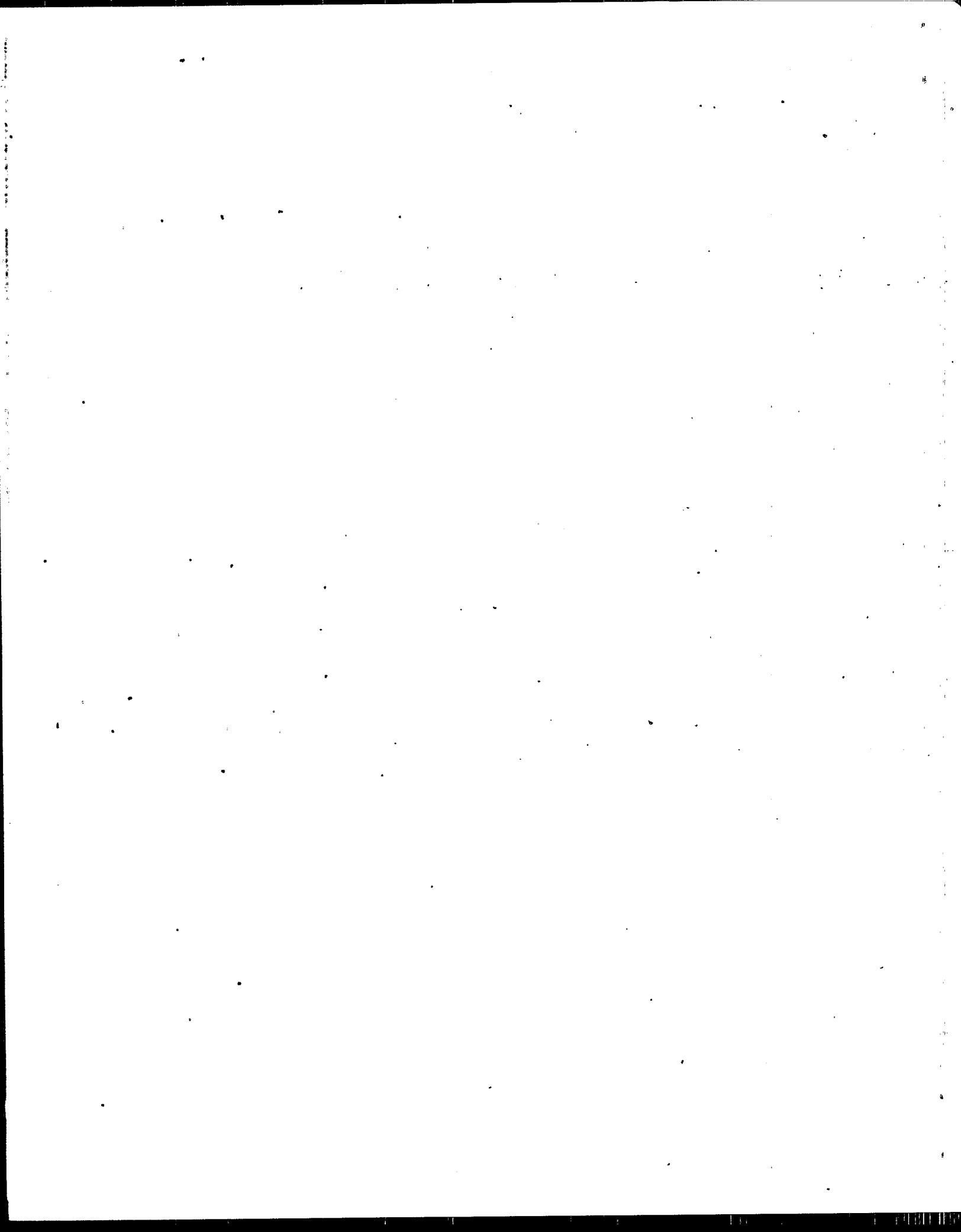
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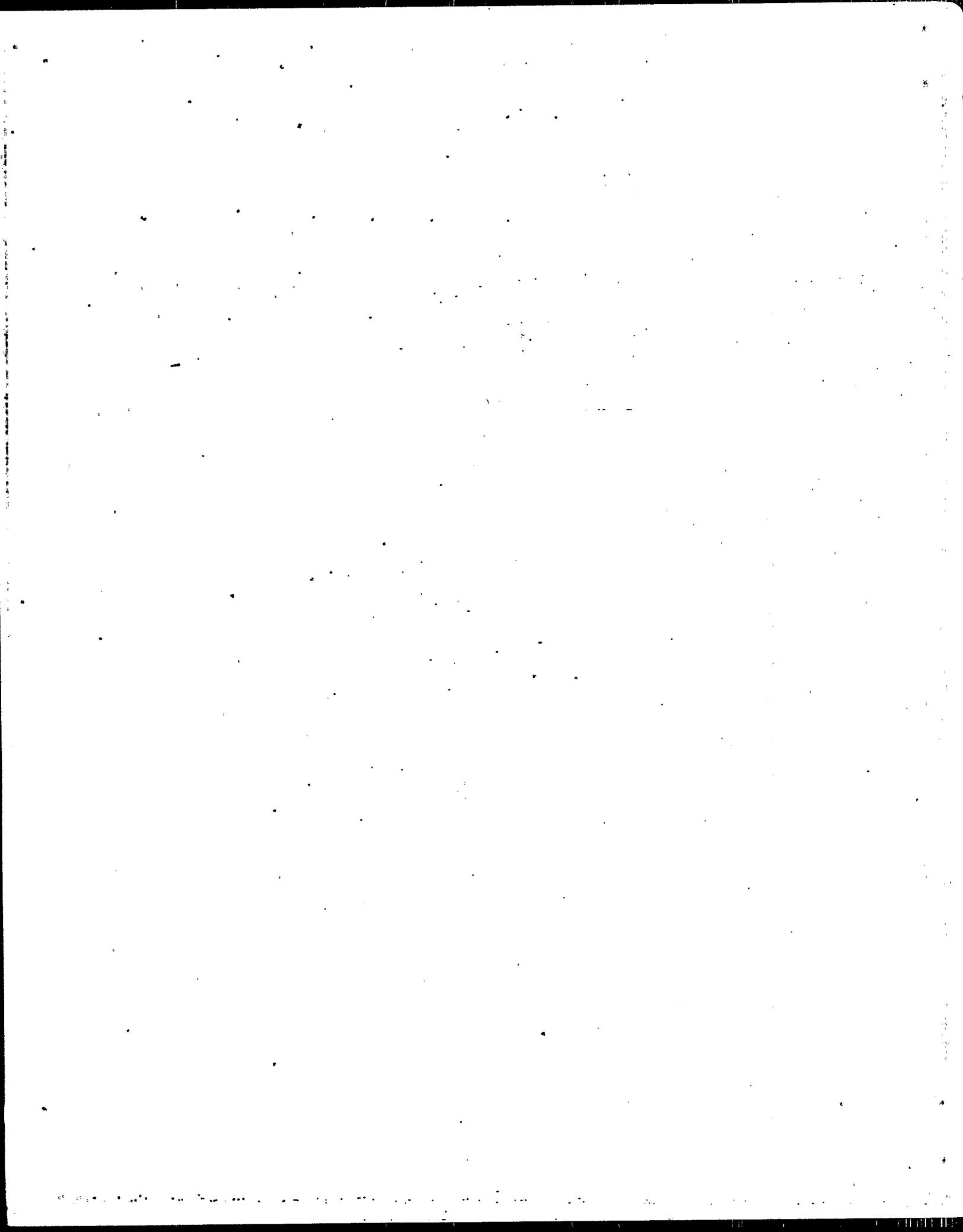






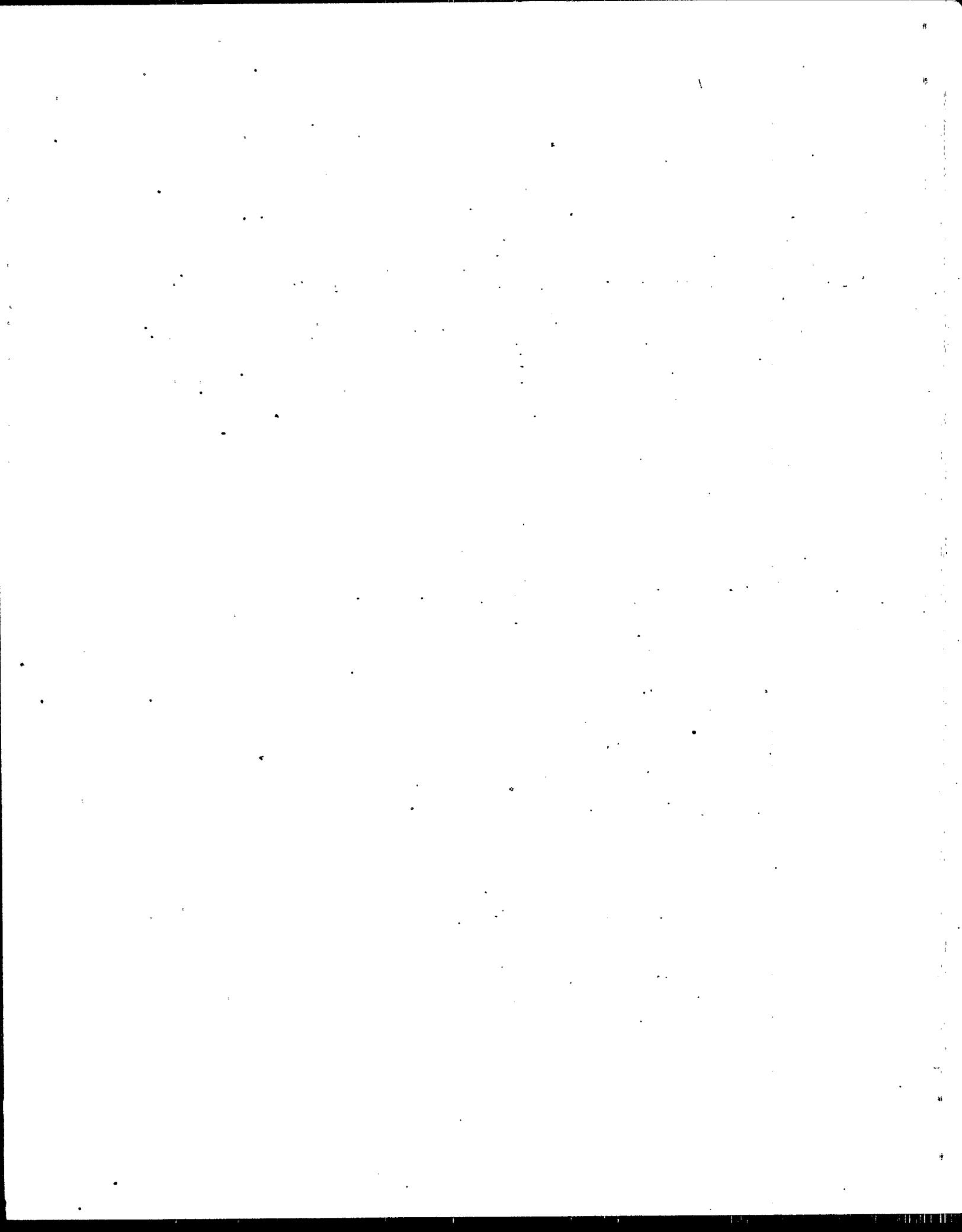
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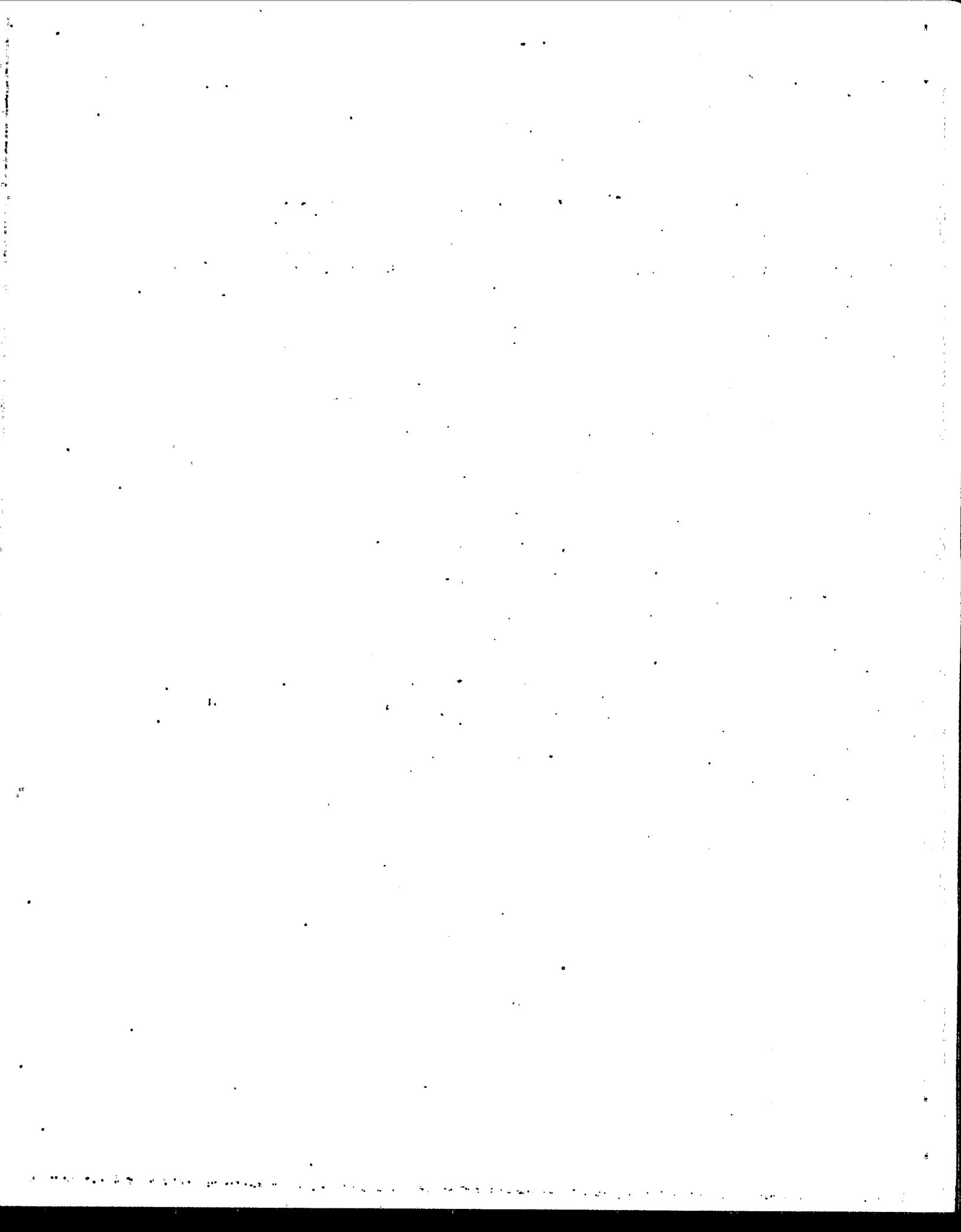
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## 1. PURPOSE OF DOCUMENT

This document is designed to assist Federal, State, and local air pollution agencies in inventorying air emissions of potentially toxic substances. It is one of a series the Environmental Protection Agency (EPA) is preparing to compile information on sources and emissions of these pollutants. Specifically, this document deals with emissions from sewage sludge incinerators (SSIs).

The emissions information in this document will be most useful in making preliminary estimates of air emissions and should not be used in exact assessments of emissions from any particular facility. The reason for this is that insufficient data are available to estimate the statistical accuracy of these emission factors. In addition, variability in sludge composition contributes to variations in emission factors. In fact, the difference between actual and calculated emissions could be as great as orders of magnitude in extreme cases. The size of error would depend on differences in source configurations, variability of sludge composition, control equipment design and operation, and overall operating practices. A source test is the best way to determine air emissions from a particular source. However, even when a source test is used for a specific facility, variability of sludge composition could change the composition of emissions.

To date, 22 reports in this series have been published, each with the generic title "Locating and Estimating (Toxic) Emissions from (or of) (Source Category or Substance)." Reports are available for the following substances or source categories: acrylonitrile, 1,3-butadiene, carbon tetrachloride, chloroform, ethylene dichloride, formaldehyde, nickel, chromium, manganese, phosgene, epichlorohydrin, vinylidene chloride, ethylene oxide, chlorobenzenes, polychlorinated biphenyls (PCBs), polycyclic organic matter (POM), benzene, organic liquid storage tanks, coal and oil combustion sources, municipal waste combustors, perchloroethylene and trichloroethylene. A report is in production for styrene and others are planned.



## 2. OVERVIEW OF DOCUMENT

This section briefly outlines the contents of this report.

Section 3 is an overview of the sewage sludge incineration (SSI) industry, describing the major types of SSIs in the existing population: multiple hearth furnaces, fluidized bed furnaces, and electric furnaces. Several types of lesser importance are also presented. Included is a process description for each type of combustor, as well as a current facility list. In addition, this section describes the air emission control technologies currently in use at SSI facilities.

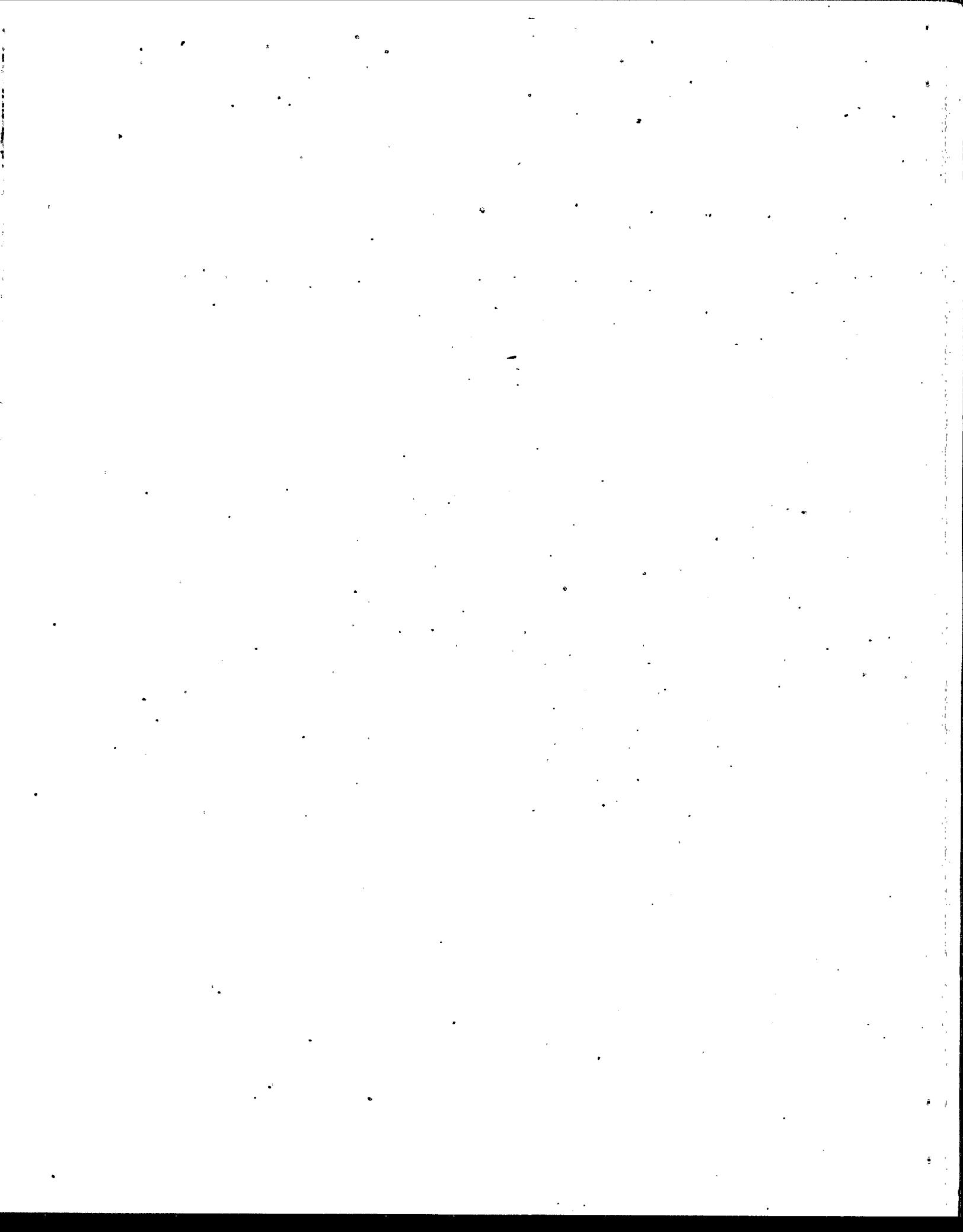
Section 4 focuses on the air emissions from SSIs. Emission factors are given in tabular format for organics and inorganics including metals.

Section 5 discusses the EPA reference methods and generally accepted methods of sampling and analysis for each pollutant. Appendix A contains a list of the existing SSI facilities. Included in the list are incinerator type, unit size, start-up date and type of air pollution control device.

This document does not discuss health or other environmental effects of emission from SSIs, nor does it discuss ambient air levels or ambient air monitoring techniques for emissions associated with SSIs.

Comments on this document are welcome, including information on process descriptions, operating practices, control measures, and emissions information that would enable EPA to improve the contents. All comments should be sent to:

Chief, Pollutant Characterization Section (MD-15)  
Noncriteria Pollutant Programs Branch  
U. S. Environmental Protection Agency  
Research Triangle Park, North Carolina 27711



### 3. BACKGROUND INFORMATION

Incineration is a means of disposing of sewage sludge generated by the treatment of wastewater from residential, commercial, and industrial establishments. When compared to other forms of disposal, incineration has the advantages of reducing the solid mass and the potential for recovering energy through combustion. Disadvantages include the necessity of ash disposal and the potential for air emissions of pollutants.

This section provides background information on the current status of sewage sludge incineration. In Section 3.1, the sewage sludge incineration industry is briefly overviewed. Incinerator and emission control design are described in detail in Sections 3.2 and 3.3, respectively.

#### 3.1 CHARACTERIZATION OF THE INDUSTRY

There are currently about 200 sewage sludge incineration (SSI) plants in operation in the United States. Three main types of incinerators are used: multiple hearth, fluidized bed, and electric infrared.<sup>1</sup> Some sludge is co-fired with municipal solid waste in combustors based on refuse combustion technology. Unprocessed refuse co-fired with sludge in combustors based on sludge incinerating technology is limited to multiple hearth incinerators only.

Over 80 percent of the identified operating sludge incinerators are of the multiple hearth design. About 15 percent are fluidized bed combustors and 3 percent are electric. The remaining combustors co-fire refuse with sludge.

Figure 3-1 shows the approximate geographic distribution of the existing SSI population. Most sludge incineration facilities are located in the Eastern United States, though there are a significant number on the West Coast. New York has the largest number of facilities with 33. Pennsylvania and Michigan have the next-largest numbers of facilities with 21 and 19 sites, respectively.

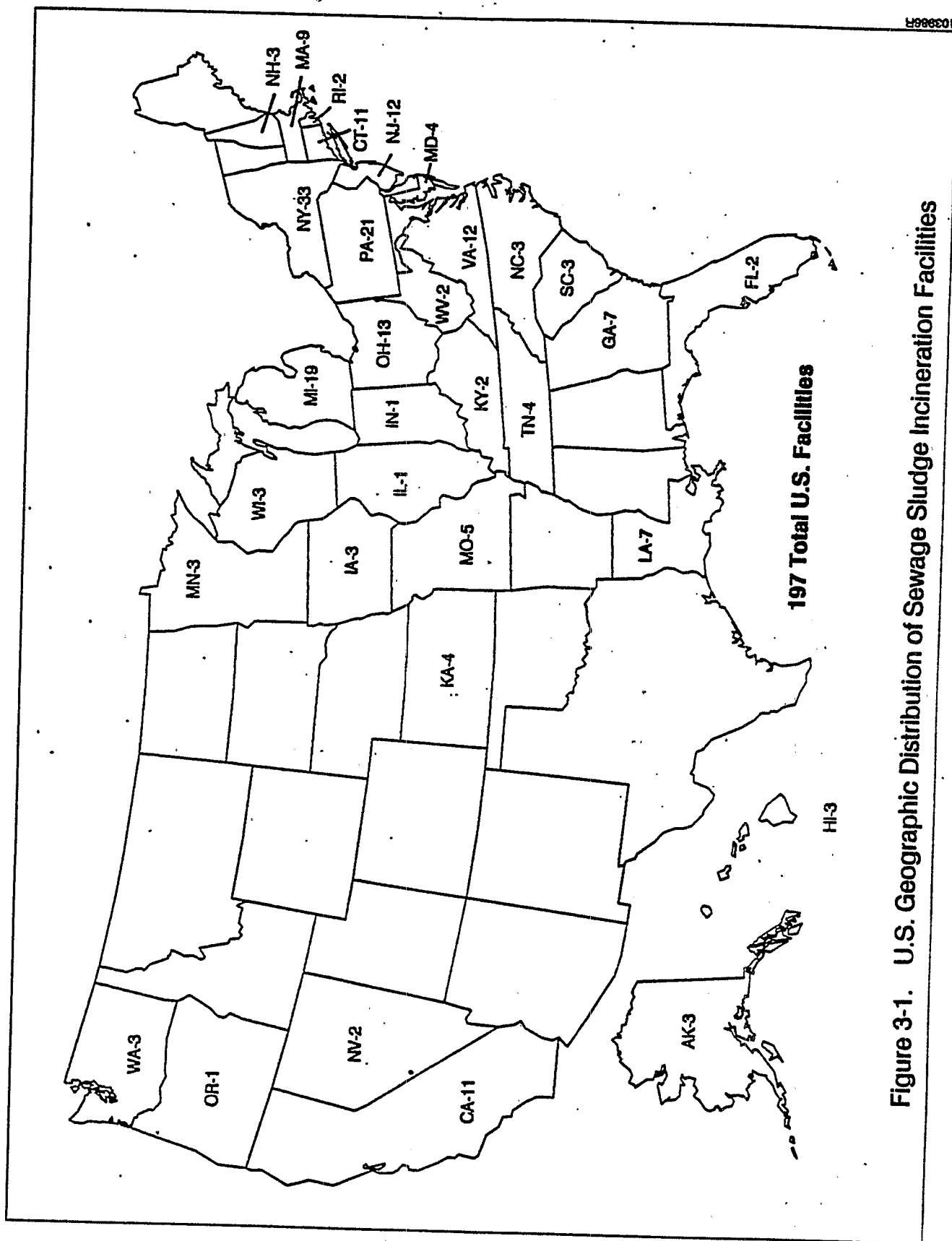


Figure 3-1. U.S. Geographic Distribution of Sewage Sludge Incineration Facilities

A list of the existing facilities is in Appendix A. Table A-1 is sorted by combustor technology, and shows incinerator type, unit capacity, year of facility start-up, and type of air pollution control device.

### 3.2 INCINERATOR PROCESS DESCRIPTIONS

Types of incineration described in this section include:

- Multiple hearth
- Fluidized bed
- Electric
- Single hearth cyclone
- Rotary kiln
- High pressure, wet air oxidation
- Co-incineration with refuse

#### 3.2.1 Multiple Hearth Furnaces

The multiple hearth furnace was originally developed for mineral ore roasting nearly a century ago. The air-cooled variation has been used to incinerate sewage sludge since the 1930's. A cross section diagram of a typical multiple hearth furnace is shown in Figure 3-2. The basic multiple hearth furnace (MHF) is cylinder-shaped and oriented vertically. The outer shell is constructed of steel, lined with refractory, and surrounds a series of horizontal refractory hearths. A hollow cast iron rotating shaft runs through the center of the hearths. Cooling air for the center shaft and rabble arms is introduced into the shaft by a fan located at its base. Attached to the central shaft are the rabble arms, which extend above the hearths. Each rabble arm is equipped with a number of teeth, approximately 6 inches in length, and spaced about 10 inches apart. The teeth are shaped to rake the sludge in a spiral motion, alternating in direction from the outside in, to the inside out, between hearths. Typically, the upper and lower hearths are fitted with 4 rabble arms, and the middle hearths are fitted with two. Burners, providing auxiliary heat, are located in the sidewalls of the hearths.

Partially dewatered sludge is fed onto the perimeter of the top hearth by conveyors or pumps. The motion of the rabble arms rakes the sludge toward the center shaft where it drops through holes located at the center

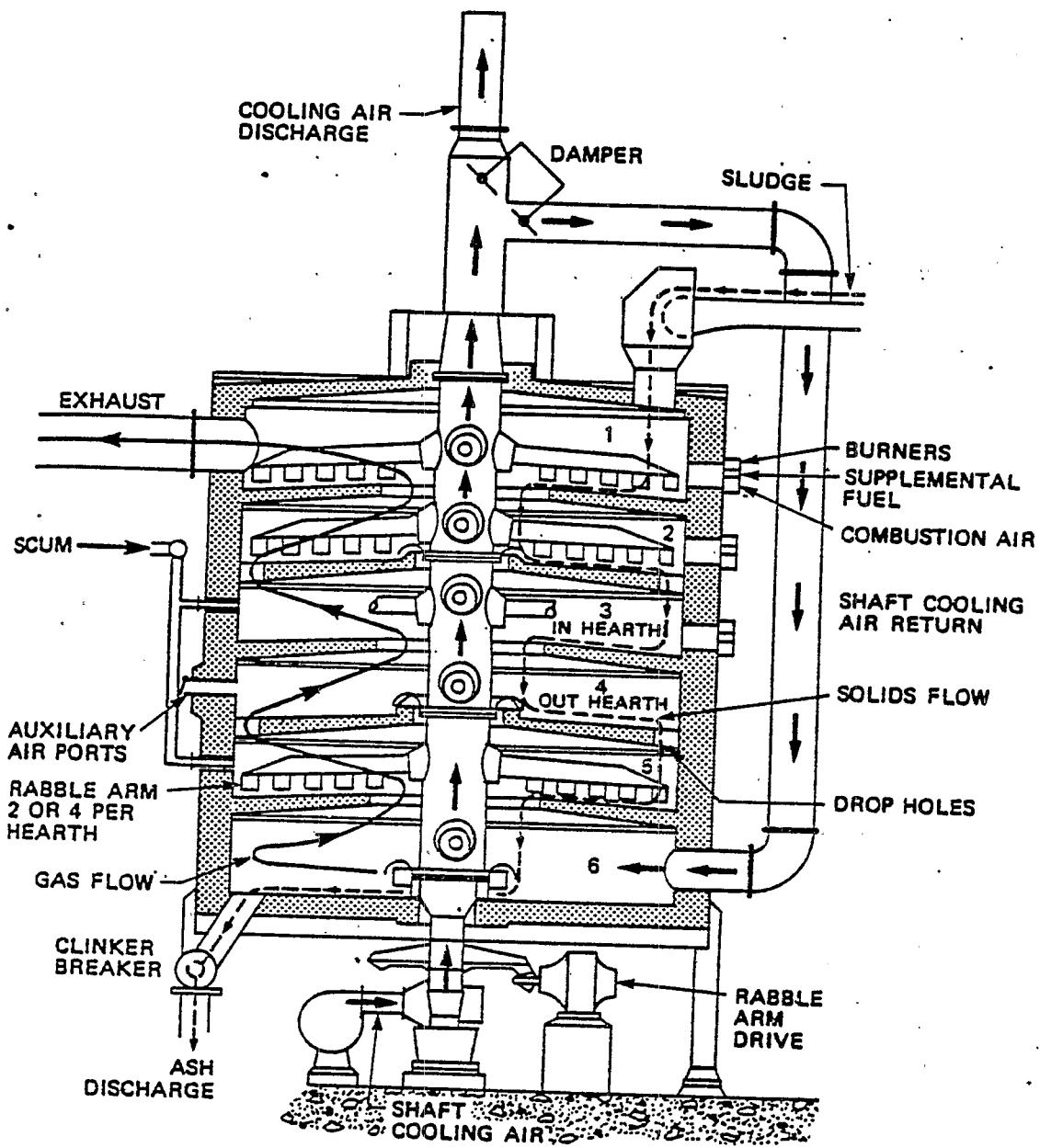


Figure 3-2. Cross section of a multiple hearth furnace.

of the hearth. In the next hearth the sludge is raked in the opposite direction. This process is repeated in all of the subsequent hearths. The effect of the rabble motion is to break up solid material to allow better surface contact with heat and oxygen, and is arranged so that sludge depth of about one inch is maintained in each hearth at the design sludge flow rate.

Scum may also be fed to one or more hearths of the incinerator. Scum is the material that floats on wastewater. It is generally composed of vegetable and mineral oils, grease, hair, waxes, fats, and other materials that will float and usually has a higher heating value and larger volatile fraction than sludge. Scum may be removed from many treatment units including preparation tanks, skimming tanks, and sedimentation tanks. Quantities of scum are generally small compared to those of other wastewater solids.

Ambient air is first ducted through the central shaft and its associated rabble arms. A portion, or all, of this air is then taken from the top of the shaft and recirculated into the lowermost hearth as preheated combustion air. Shaft cooling air which is not circulated back into the furnace is ducted into the stack downstream of the air pollution control devices. The combustion air flows upward through the drop holes in the hearths, countercurrent to the flow of the sludge, before being exhausted from the top hearth. Provisions are usually made to inject ambient air directly into on the middle hearths as well.

From the standpoint of the overall incineration process, multiple hearth furnaces can be divided into three zones. The upper hearths comprise the drying zone where most of the moisture in the sludge is evaporated. The temperature in the drying zone is typically between 425 and 760°C (800 and 1,400°F). Sludge combustion occurs in the middle hearths (second zone) as the temperature is increased between 815 and 925°C (1,500 and 1,700°F). The combustion zone can be further subdivided into the upper-middle hearths where the volatile gases and solids are burned, and the lower-middle hearths where most of the fixed carbon is combusted. The third zone, made up of the lowermost hearth(s), is the cooling zone. In this zone the ash is cooled as its heat is transferred to the incoming combustion air.

Multiple hearth furnaces are sometimes operated with afterburners to further reduce odors and concentrations of unburned hydrocarbons. In afterburning, furnace exhaust gases are ducted to a chamber where they are mixed with supplemental fuel and air and completely combusted. Some incinerators have the flexibility to allow sludge to be fed to a lower hearth, thus allowing the upper hearth(s) to function essentially as an afterburner.

Under normal operating conditions, 50 to 100 percent excess air must be added to an MHF in order to ensure complete combustion of the sludge. Besides enhancing contact between fuel and oxygen in the furnace, these relatively high rates of excess air are necessary in order to compensate for normal variations in both the organic characteristics of the sludge feed and the rate at which it enters the incinerator. When an inadequate amount of excess air is available, only partial oxidation of the carbon will occur with a resultant increase in emissions of carbon monoxide, soot, and hydrocarbons. Too much excess air, on the other hand, can cause increased entrainment of particulate and unnecessarily high auxiliary fuel consumption.

Some MHFs have been designed to operate in a starved air mode. Starved air combustion (SAC) is, in effect, incomplete combustion. The key to SAC is the usage of less than theoretical quantities of air in the furnace--30 to 90 percent of stoichiometric quantities. This makes SAC more fuel efficient than an excess air mode MHF. The SAC reaction products are combustible gases, tars and oils, and a solid char that can have appreciable heating value. The most effective utilization of these products is by burning of the total gas stream with subsequent heat recovery. When an SAC MHF is combined with an afterburner, an overall excess air rate of 25 to 50 percent can be maintained (as compared to 75 to 200 percent overall for an excess air MHF with an afterburner).

Multiple hearth furnace emissions are usually controlled by a venturi scrubber, an impingement tray scrubber, or a combination of both. Wet cyclones are also used.

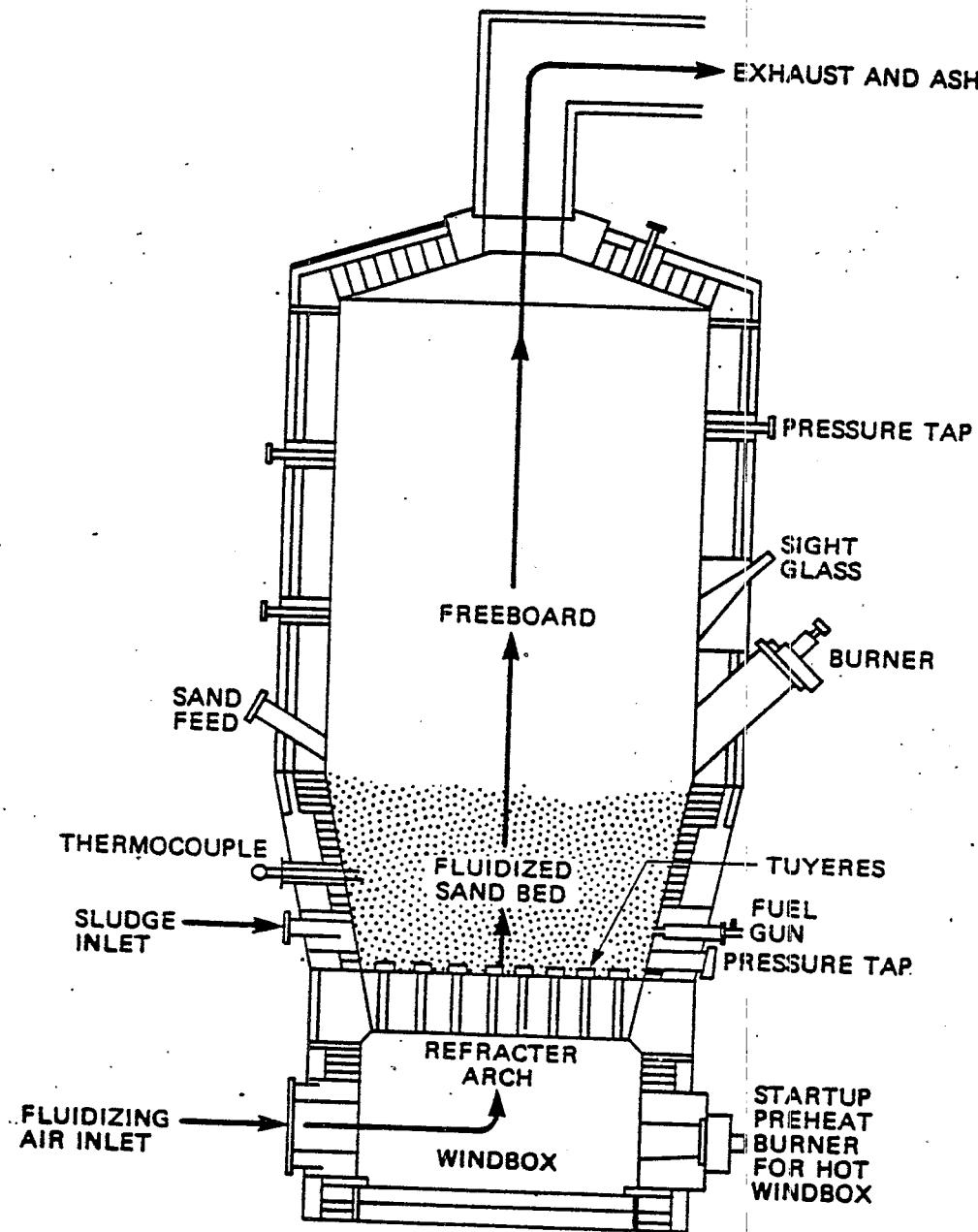


Figure 3-3. Cross section of a fluidized bed furnace.

### 3.2.2 Fluidized Bed Incinerators

Fluidized bed technology was first developed by the petroleum industry to be used for catalyst regeneration. Fluidized bed technology was first used for municipal sludge incineration in 1962. Figure 3-3 shows the cross section diagram of a fluidized bed furnace (FBF). Fluidized bed furnaces are cylindrically shaped and oriented vertically. The outer shell is constructed of steel, and is lined with refractory. Tuyeres (nozzles designed to deliver blasts of air) are located at the base of the furnace within a refractory-lined grid. A bed of sand, approximately 0.75 meters (2.5 feet) thick, rests upon the grid. Two general configurations can be distinguished on the basis of how the fluidizing air is injected into the furnace. In the "hot windbox" design the combustion air is first preheated by passing through a heat exchanger where heat is recovered from the hot flue gases. Alternatively, ambient air can be injected directly into the furnace from a cold windbox.

Partially dewatered sludge is fed into the bed of the furnace. Air injected through the tuyeres, at pressure of from 20 to 35 kPa (3 to 5 psig), simultaneously fluidizes the bed of hot sand and the incoming sludge. Temperatures of 725 to 825°C (1,350 to 1,500°F) are maintained in the bed. Residence times are on the order of 2 to 5 seconds. As the sludge burns, fine ash particles are carried out the top of the furnace. Some sand is also removed in the air stream; sand make-up requirements are on the order of 5 percent for every 300 hours of operation.

The overall process of combustion of the sludge occurs in two zones. Within the bed itself (zone 1) evaporation of the water and pyrolysis of the organic materials occur nearly simultaneously as the temperature of the sludge is rapidly raised. In the second zone, (freeboard area) the remaining free carbon and combustible gases are burned. The second zone functions essentially as an afterburner.

Fluidization achieves nearly ideal mixing between the sludge and the combustion air and the turbulence facilitates the transfer of heat from the hot sand to the sludge. The most noticeable impact of the better burning atmosphere provided by a fluidized bed incinerator is seen in the limited amount of excess air required for complete combustion of the sludge.

These incinerators can achieve complete combustion with 20 to 50 percent excess air, about half the amount of excess air typically required for incinerating sewage sludge in multiple hearth furnaces. As a consequence, FBF incinerators have generally lower fuel requirements compared to MHF incinerators.

Fluidized bed incinerators most often have venturi scrubbers or venturi/impingement tray scrubber combinations for emissions control.

### 3.2.3 Electric Incinerators

Electric furnace technology is new compared to other sludge combustor designs; the first electric furnace was installed in 1975. Electric incinerators consist of a horizontally oriented, insulated furnace. A woven wire belt conveyor extends the length of the furnace and infrared heating elements are located in the roof above the conveyor belt. Combustion air is preheated by the flue gases and is injected into the discharge end of the furnace. Electric incinerators consist of a number of prefabricated modules, which can be linked together to provide the necessary furnace length. A cross section of an electric furnace is shown in Figure 3-4.

The dewatered sludge cake is conveyed into one end of the incinerator. An internal roller mechanism levels the sludge into a continuous layer approximately one inch thick across the width of the belt. The sludge is sequentially dried and then burned as it moves beneath the infrared heating elements. Ash is discharged into a hopper at the opposite end of the furnace. The preheated combustion air enters the furnace above the ash hopper and is further heated by the outgoing ash. The direction of air flow is countercurrent to the movement of the sludge along the conveyor. Exhaust gases leave the furnace at the feed end. Excess air rates vary from 20 to 70 percent.

When compared to MHF and FBF technologies, the electric furnace offers the advantage of lower capital cost, especially for smaller systems. However, electric costs in some areas may make an electric furnace infeasible. Another concern is replacement of various components such as the woven wire belt and infrared heaters, which have 3 to 5 year lifetimes.

Electric incinerators are usually controlled with a venturi scrubber or some other wet scrubber.

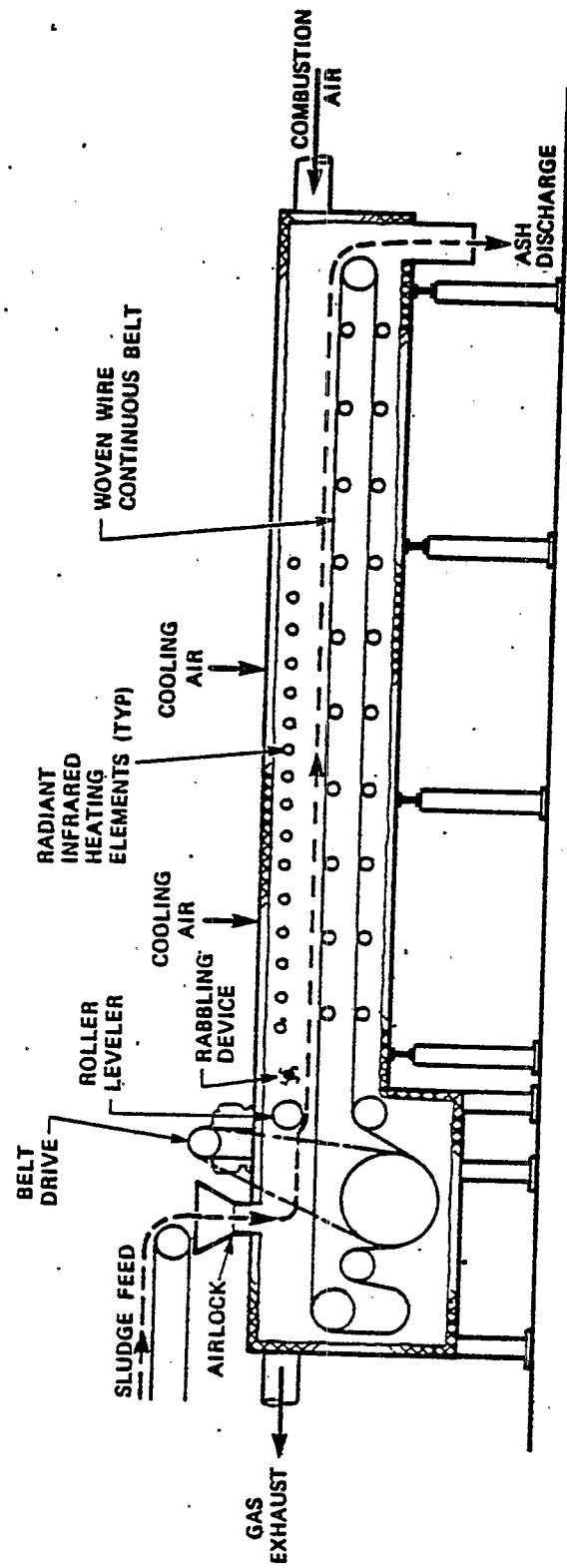


Figure 3-4. Cross section of an electric infrared furnace.

### 3.2.4 Other Technologies

A number of other technologies have been used for incineration of sewage sludge including cyclonic reactors, rotary kilns and wet oxidation reactors. These processes are not in widespread use in the United States and will be discussed only briefly.

The cyclonic reactor is designed for small capacity applications. It is constructed of a vertical cylindrical chamber that is lined with refractory. Preheated combustion air is introduced into the chamber tangentially at high velocities. The sludge is sprayed radially toward the hot refractory walls. Combustion is rapid: the residence time of the sludge in the chamber is on the order of 10 seconds. The ash is removed with the flue gases.

Rotary kilns are also generally used for small capacity applications. The kiln is inclined slightly from the horizontal plane, with the upper end receiving both the sludge feed and the combustion air. A burner is located at the lower end of the kiln. The circumference of the kiln rotates at a speed of about 6 inches per second. Ash is deposited into a hopper located below the burner.

The wet oxidation process is not strictly one of incineration; it instead utilizes oxidation with air at elevated temperature and pressure in the presence of water (flameless combustion). Thickened sludge, at about six percent solids, is first ground and mixed with a stoichiometric amount of compressed air. The sludge-air mixture is then preheated in a heat exchanger using the reactor effluent stream as the heat source before entering the pressurized reactor. The temperature of the reactor is held between 175 and 315°C (350 and 600°F). The pressure is normally 7,000 to 12,500 kPa (1,000 to 1,800 psig). Steam is usually used for auxiliary heat. The water and resulting ash are circulated out the reactor and are separated in a tank or lagoon. The liquid phase is recycled to the treatment plant. Off-gases must be treated to eliminate odors: wet scrubbing, afterburning or carbon absorption may be used.

### 3.2.5 Co-incineration with Refuse

Wastewater treatment plant sludge generally has a high water content and in some cases, fairly high levels of inert materials. As a result, its

net fuel value is often low. If sludge is combined with other combustible materials in a co-combustion scheme, a furnace feed can be created that has both a low water concentration and a heat value high enough to sustain combustion with little or no supplemental fuel.

Virtually any material that can be burned can be combined with sludge in a co-combustion process. Common materials for co-combustion are coal, municipal solid waste, wood waste and agricultural waste. Thus, a municipal or industrial waste can be disposed of while providing an autogenous (self-sustaining) sludge feed, thereby solving two disposal problems.

There are two basic approaches to combusting sludge with municipal solid waste (MSW): 1) use of MSW combustion technology by adding dewatered or dried sludge to the MSW combustion unit, and 2) use of sludge combustion technology by adding raw or processed MSW as a supplemental fuel to the sludge furnace.

With the latter, MSW is processed by removing noncombustibles, shredding, air-classifying, and screening. Waste that is more finely processed is less likely to cause problems such as severe erosion of the hearths, poor temperature control, and refractory failures.<sup>2</sup>

### 3.3 EMISSIONS AND CONTROLS

Sewage sludge incinerators potentially emit significant quantities of pollutants. The major pollutants emitted are: 1) particulate matter, 2) metals, 3) carbon monoxide (CO), 4) nitrogen oxides ( $\text{NO}_x$ ), 5) sulfur dioxide ( $\text{SO}_2$ ) and 6) unburned hydrocarbons. Partial combustion of sludge can result in emissions of intermediate products of incomplete combustion (PICs) including toxic organic compounds.

Uncontrolled particulate emission rates vary widely depending on the type of incinerator, the volatiles and moisture content of the sludge, and the operating practices employed. Generally, uncontrolled particulate emissions are highest from fluidized bed incinerators because suspension burning results in much of the ash being carried out of the incinerator with the flue gas. Uncontrolled emissions from multiple hearth and fluidized bed incinerators are extremely variable, however. Electric incinerators appear to have the lowest rates of uncontrolled particulate release of the three

major furnace types, possibly because the sludge is not disturbed during firing. In general, higher airflow rates increase the opportunity for particulate matter to be entrained in the exhaust gases. Sludge with low volatile content or high moisture content may compound this situation by requiring more supplemental fuel to burn. As more fuel is consumed, the amount of air flowing through the incinerator is also increased. However, no direct correlation has been established between air flow and particulate emissions.

Metals emissions are affected by fuel bed temperature and the level of particulate matter control, since metals which are volatilized in the combustion zone condense in the exhaust gas stream. Most metals (except mercury) are associated with fine particulate and are removed as the fine particulates are removed.

Carbon monoxide is formed when available oxygen is insufficient for complete combustion or when excess air levels are too high, resulting in lower combustion temperatures.

Nitrogen and sulfur oxide emissions are primarily the result of oxidation of nitrogen and sulfur in the sludge. Therefore, these emissions can vary greatly based on local and seasonal sewage characteristics.

Emissions of volatile organic compounds also vary greatly with incinerator type and operation. Incinerators with countercurrent air flow such as multiple hearth designs provide the greatest opportunity for unburned hydrocarbons to be emitted. In the MHF, hot air and wet sludge feed are contacted at the top of the furnace. Any compounds distilled from the solids are immediately vented from the furnace at temperatures too low to completely destruct them.

Particulate emissions from sewage sludge incinerators have historically been controlled by wet scrubbers, since the associated sewage treatment plant provides both a convenient source and a good disposal option for the scrubber water. The types of existing sewage sludge incinerator controls range from low pressure drop spray towers and wet cyclones to higher pressure drop venturi scrubbers and venturi/impingement tray scrubber combinations. A few electrostatic precipitators are employed, primarily where sludge is co-fired with municipal solid waste and baghouses have been

used. The most widely used control device applied to a multiple hearth incinerator is the impingement tray scrubber. Older units use the tray scrubber alone while combination venturi/impingement tray scrubbers are widely applied to newer multiple hearth incinerators and to fluidized bed incinerators. Most electric incinerators and some fluidized bed incinerators use venturi scrubbers only.

In a typical combination venturi/impingement tray scrubber (shown in Figure 3-5), hot gas exits the incinerator and enters the precooling or quench section of the scrubber. Spray nozzles in the quench section cool the incoming gas and the quenched gas then enters the venturi section of the control device.

Venturi water is usually pumped into an inlet weir above the quencher. The venturi water enters the scrubber above the throat and floods the throat completely. This eliminates build-up of solids and reduces abrasion. Turbulence created by high gas velocity in the converging throat section deflects some of the water traveling down the throat into the gas stream. Particulate matter carried along with the gas stream impacts on these water particles and on the water wall. As the scrubber water and flue gas leave the venturi section, they pass into a flooded elbow where the stream velocity decreases, allowing the water and gas to separate. Most venturi sections come equipped with variable throats. By restricting the throat area within the venturi, the linear gas velocity is increased and the pressure drop is subsequently increased. Up to a certain point, increasing the venturi pressure drop increases the removal efficiency. Venturi scrubbers typically attain 60 to 99 percent removal efficiency for particulate matter, depending on pressure drop and particle size distribution.<sup>3</sup>

At the base of the flooded elbow, the gas stream passes through a connecting duct to the base of the impingement tray tower. Gas velocity is further reduced upon entry to the tower as the gas stream passes upward through the perforated impingement trays. Water usually enters the trays from inlet ports on opposite sides and flows across the tray. As gas passes through each perforation in the tray, it creates a jet which bubbles up the water and further entrains solid particles. At the top of the tower is a

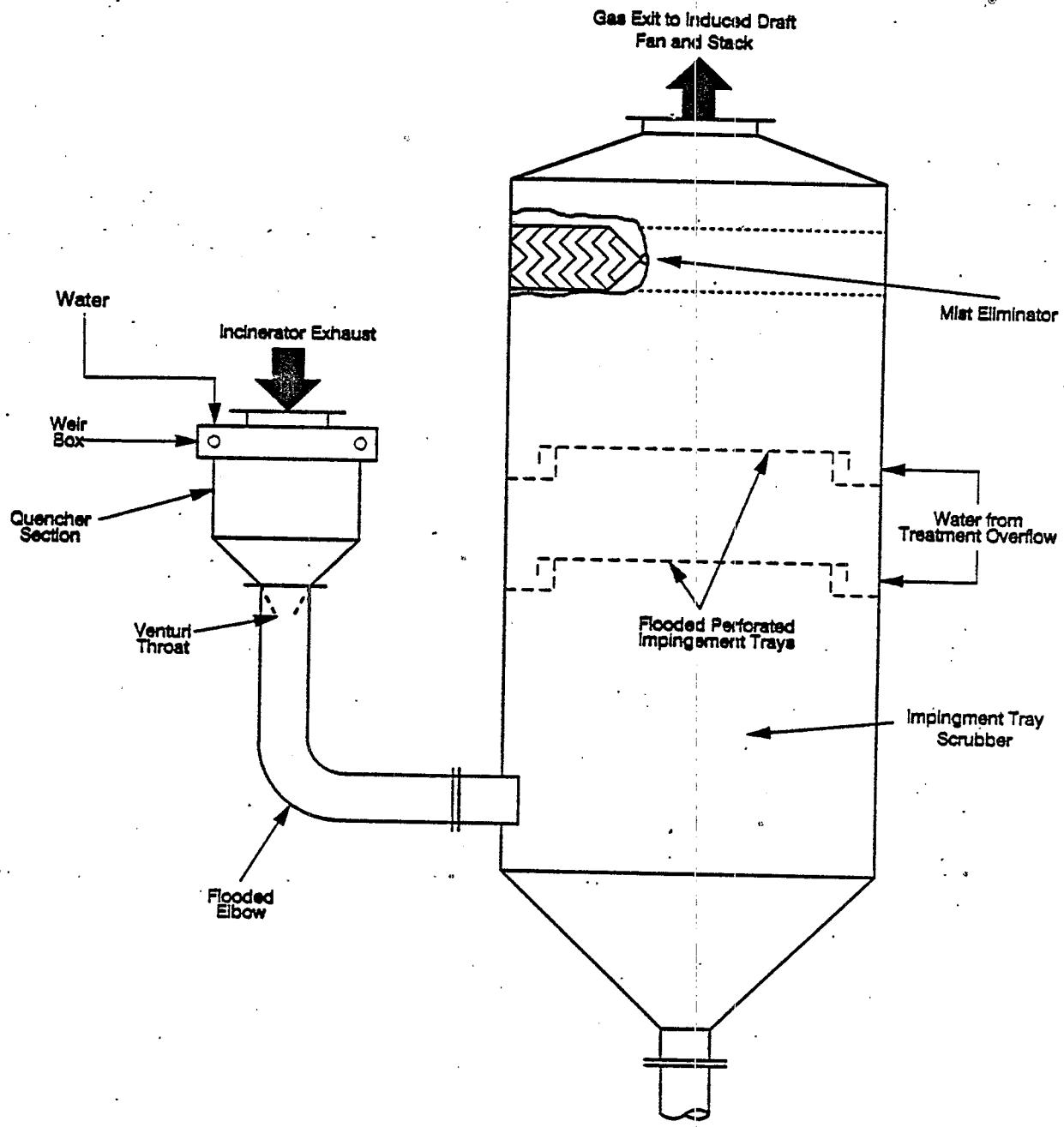
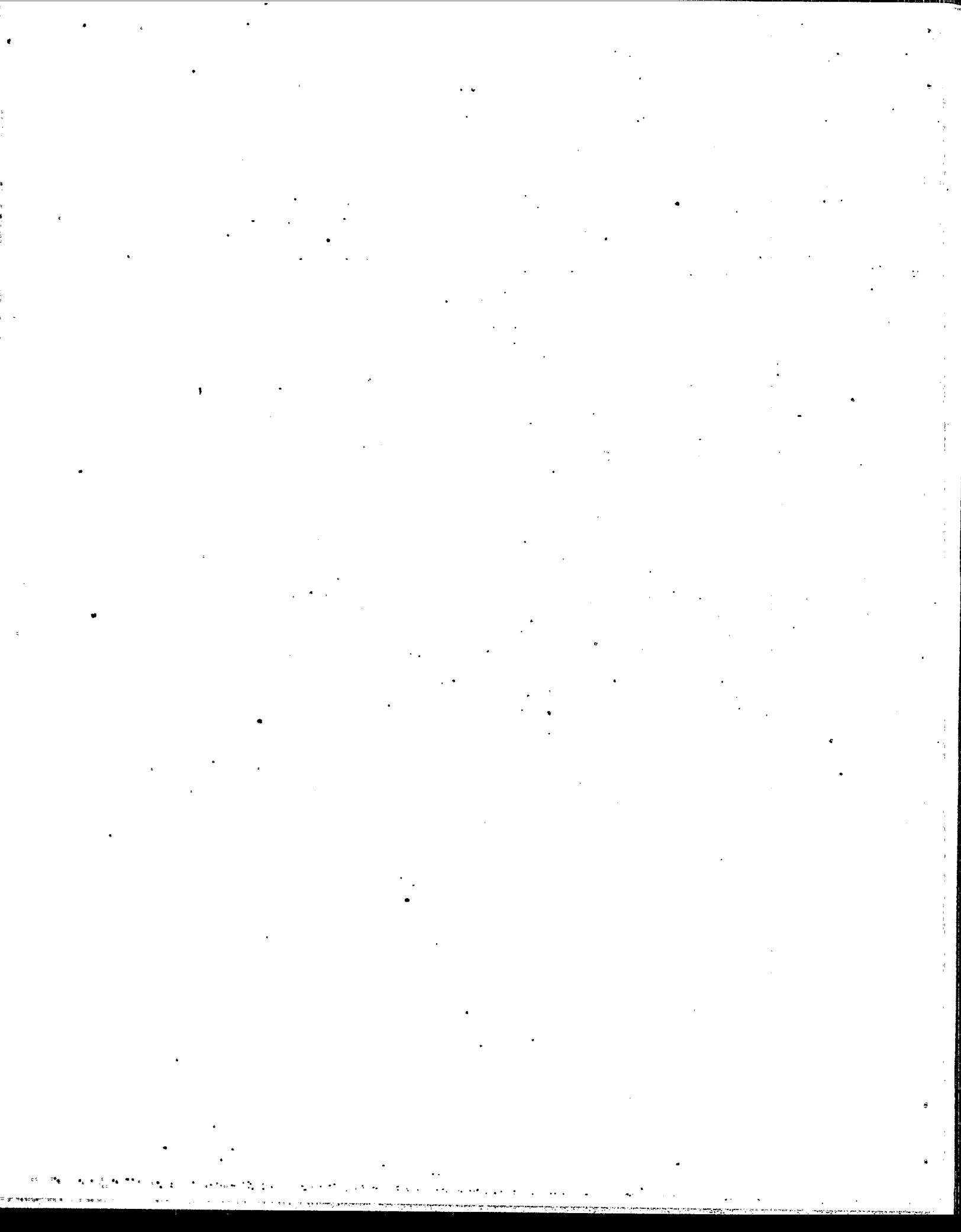


Figure 3-5. Venturi/impingement tray scrubber.

mist eliminator to reduce the carryover of water droplets in the stack effluent gas. The impingement section can contain from one to four trays, but most systems for which data are available have two or three trays.

### 3.4 REFERENCES

1. Second Review of Standards of Performance for Sewage Sludge Incinerators, EPA-450/3-84-010, U.S. Environmental Protection Agency, Research Triangle Park, NC. March 1984.
2. Process Design Manual for Sludge Treatment and Disposal, EPA-625/1-79-011, U.S. Environmental Protection Agency, Cincinnati, OH. September 1979.
3. Control Techniques for Particulate Emissions From Stationary Sources - Volume 1, EPA-450/3-81-005a, U.S. Environmental Protection Agency, Research Triangle Park, NC. September 1982.



#### 4. EMISSION FACTORS

Emission factors have been developed for the various pollutants emitted from SSIs. These emission factors are derived from published emissions data; no new sampling of sources was done for this project. The factors relate the amount of pollutant emitted in the flue gas to the amount of sludge incinerated and may be used to estimate emissions from a facility. Flue gas emissions are the principal source of air toxics emissions from sewage sludge incinerators. The estimated emissions should be used with caution, however, because the emission factors are generally averages from several facilities and are not necessarily representative of the emissions from any particular facility. Additionally, because of limited data, a representative number of facilities could not be used in evaluating emission factors. In some cases, data from only one facility were available; these factors are noted individually, and should only be used with extreme caution.

If more accurate emission estimates are needed, source testing should be done. Data collected should include sludge feed rate and composition, ash composition, and stack emissions. The actual air toxics emissions from any given facility are a function of variables such as capacity, throughput, sludge composition, operating characteristics, and air pollution control device operations. The effects of these factors should be considered when testing. If such testing is done, the Pollutant Characterization Section requests copies of the tests be submitted so that better databases and emission factors may be developed in the future.

In this document, emission factors are presented for 32 inorganic compounds including metals, 25 volatile organic compounds, various isomers of chlorinated dibenzo-p-dioxins and dibenzofurans (CDD and CDF), and 7 other semivolatile organic compounds. Average emissions factors were evaluated per incinerator type and emission control type. The overall averages were derived by combining the average emission factors for each test of the same general incinerator and emission control type. For

facilities where multiple operating conditions were evaluated or multiple tests were performed over a period of years, the average emission factor from each test condition or test was used in deriving the overall average.

Several individual emission factors were derived for each facility. For inorganic compounds, three factors were derived by dividing the mass emission rate of the pollutant by 1) the measured feed rate of that pollutant, by 2) the total particulate matter emission rate, and by 3) the total dry sludge feed rate. Which factor is selected to estimate emissions will depend on what information is available. The first factor should be used when the sludge feed composition is known in addition to the total dry sludge feed rate. The second factor can be used to predict emissions of specific compounds from the total particulate matter emission rate. The third factor can be used if only the total sludge feed rate is known. Organic compound emission factors were derived by dividing the mass emission rate of the pollutant by the total dry sludge feed rate.

The first two inorganic compound factors are presented on a fractional mass basis (ppm). All the emission factors on a total feed basis are presented in both SI and English units. When a pollutant was not detected, no value was reported; overall average emission factors include data from only those facilities where the compound was detected.

Emission factors for the different types of combustors and emission controls are presented in Sections 4.1 to 4.3.

#### 4.1 EMISSION FACTORS FOR MULTIPLE HEARTH FURNACES

Emission factors for inorganic compound emissions from multiple hearth furnaces are presented in Tables 4-1 through 4-4. The emission factors are for uncontrolled flue gas emissions as well as controlled flue gas emissions. Emission factors for controlled emissions are separated by the different types of emission controls used with multiple hearth furnaces including cyclones, impingement tray scrubbers, venturi scrubbers and exhaust gas afterburners. Test data from facilities using a venturi scrubber (with or without other devices) are reported separately from those facilities using only low-energy scrubbers. In addition, pilot scale test data are presented for control by an electrostatic precipitator and by a

TABLE 4-1. INORGANIC COMPOUND EMISSION FACTORS ON A COMPOUND FEED BASIS  
FOR MULTIPLE HEARTH FURNACES BURNING SEWAGE SLUDGE  
(Mass of Pollutant Emitted per Mass Fed)  $\times 10^6$

Pollutant	Uncontrolled		References	After Low-Energy Scrubber <sup>a</sup>		References	After High-Energy Scrubber <sup>b</sup>		References
	Average	Range		Average	Range		Average	Range	
Aluminum	36,000	1700 - 70,000	6.7	917	9.04 -	2,260	19	23,000 <sup>c</sup>	-
Antimony	42,000	690 - 84,000	6.7	4,660	2,570 -	5,960	19	6,800 <sup>c</sup>	6
Arsenic	150,000	890 - 360,000	2.4, 6.7	990	501 -	1,240	19	31,000 <sup>c</sup>	1,2, 4, 6
Barium	33,000	1,500 - 64,000	6.7	1,420	65.9 -	3,670	19	8,700 <sup>c</sup>	6
Beryllium	26,000	26,000	2.4	-	-	2,000	-	-	1,2, 4
Boron	-	-	-	-	-	-	-	-	-
Cadmium	1,100,000 <sup>d</sup>	15,000 - 6,100,000 <sup>d</sup>	2.6, 6.7, 14	129,000	6,410 -	366,000	19	140,000	55,000 - 220,000
Calcium	35,000	1,200 - 69,000 <sup>d</sup>	6.7	933	20.7 -	2,190	19	21,000 <sup>c</sup>	6
Chromium	350,000	76,000 - 1,800,000 <sup>d</sup>	2.4, 6.7, 14	3,430	769 -	5,460	19	11,000 <sup>c</sup>	1,2, 6, 14
Cobalt	29,000	780 - 57,000	6.7	1,440,000,000	762 -	4,320,000,000	19	3,500 <sup>c</sup>	6
Copper	250,000	750 - 900,000	6.7, 14	10,800	1,500 -	36,000	19	6,100 <sup>c</sup>	10,000 - 6,6, 14
Gold	960	290 - 1,600	6.7	-	-	120 <sup>c</sup>	-	-	6
Iron	240,000	59,000 - 1,200,000 <sup>d</sup>	6.7, 14	943	54.1 -	2,160	19	1,500 <sup>c</sup>	18 - 3,900
Lead	640,000	3,700 - 3,800,000 <sup>d</sup>	2.4, 6.7, 14	41,200	11,800 -	128,000	19	87,000 <sup>c</sup>	30,000 - 210,000
Magnesium	30,000	980 - 59,000	6.7	984	29 -	2,280	19	810 <sup>c</sup>	6
Manganese	340,000	610 - 1,300,000 <sup>d</sup>	6.7, 14	2,940	116 -	13,000	19	3,100	36 - 8,800
Molybdenum	200,000	1,300,000 <sup>d</sup>	2.4, 6.7, 14	-	-	-	-	-	6,14
Nickel	31,000	540 - 62,000	6.7	7,250	466 -	23,700	19	14,000 <sup>c</sup>	130 - 51,000
Phosphorus	-	-	-	-	-	580 <sup>c</sup>	-	-	6
Potassium	-	-	-	-	-	-	-	-	-
Selenium	-	-	-	-	-	-	-	-	-
Silicon	-	-	-	-	-	-	-	-	-
Silver	360,000	8,500 - 1,800,000 <sup>d</sup>	7.16	43,200	14,500 -	81,500	19	16,000 <sup>c</sup>	3,700 - 29,000
Sodium	28,000	670 - 56,000	6.7	2,720	1,520 -	4,490	19	7,200 <sup>c</sup>	-
Strontium	-	-	-	-	-	-	-	-	-
Sulfur	1,300,000 <sup>e</sup>	470 - 2,600,000 <sup>e</sup>	6.7	6,630	3,710 -	9,110	-	32,000 <sup>c</sup>	-
Thorium	-	-	-	-	-	-	-	-	-
Tin	70,000	2,800 - 140,000	6.7	12,800	5,260 -	25,500	19	66,000 <sup>c</sup>	6
Titanium	30,000	670 - 59,000	6.7	1,170	17.2 -	3,070	19	2,100 <sup>c</sup>	-
Vanadium	37,000	2,000 - 72,000	6.7	6,900	762 -	15,000	19	7,500	-
Zinc	370,000	200 - 1,200,000 <sup>d</sup>	6.7, 14	15,000	1,550 -	34,700	19	14,000	2,900 - 82,000
Zirconium	-	-	-	-	-	-	-	-	4,6, 14

(continued)

TABLE 4-1. (Continued)

Pollutant	After ESP		After Fabric Filter		After Scrubber and Afterburner <sup>g</sup>	
	Average	Range	References	Average	Range	Average
Aluminum	12,000	-	6	2,000	-	7
Antimony	920	-	6	23	-	7
Arsenic	5,300	-	6	17	-	7
Barium	9,700	-	6	140	-	7
Beryllium	-	-	-	-	-	-
Boron	-	-	-	-	-	-
Cadmium	2,100	-	6	200	-	7
Calcium	18,000	-	6	8.9	-	7
Chromium	6,100	-	6	140	-	7
Cobalt	20,000	-	6	210	-	7
Copper	120	-	6	1.5	-	7
Gold	-	-	-	-	-	-
Iron	1,400	-	6	5.9	-	7
Lead	5,300	-	6	25	-	7
Magnesium	1,200	-	6	6.9	-	7
Manganese	2,600	-	6	2.5	-	7
Molybdenum	-	-	-	-	-	-
Nickel	21,000	-	6	130	-	7
Phosphorus	4,10	-	6	2.1	-	7
Potassium	-	-	-	-	-	-
Selenium	-	-	-	-	-	-
Silicon	-	-	-	-	-	-
Silver	-	-	-	-	-	-
Sodium	220	-	6	400	-	7
Strontium	-	-	-	9.5	-	7
Sulfur	1,300,000 <sup>e</sup>	-	6	13	-	7
Thorium	-	-	-	-	-	-
Tin	1,500	-	6	7.0	-	7
Titanium	390	-	6	3.0	-	7
Vanadium	3,100	-	6	15	-	7
Zinc	180	-	6	20	-	7
Zirconium	-	-	-	-	-	-

<sup>a</sup>cyclone or impingement tray scrubber.<sup>b</sup>Venturi scrubber alone or in series with low-energy devices.<sup>c</sup>One data point.<sup>d</sup>Reference 14 tests are biased; emissions reported are greater than quantity fed in some cases.<sup>e</sup>Includes SO<sub>2</sub> gas from impinger catch, while sludge analysis reported only nonvolatile sulfur compounds.<sup>f</sup>From pilot scale control device.<sup>g</sup>Overall control by venturi scrubber, impingement tray scrubber, and afterburner in series.

TABLE 4-2. INORGANIC COMPOUND EMISSION FACTORS ON A TOTAL PARTICULATE EMISSION BASIS  
FOR MULTIPLE HEARTH FURNACES' BURNING SEWAGE SLUDGE  
(Mass of Pollutant Emitted per Mass of Total Particulate Emitted)  $\times 10^6$

Pollutant	Uncontrolled		After Low-Energy Scrubber <sup>a</sup>		After High-Energy Scrubber <sup>b</sup>		References
	Average	Range	Average	Range	Average	Range	
Aluminum	29,000	3,000 - 180	56,000	6,7 - 240	13,800	600 - 30,500	900,000 <sup>c</sup>
Antimony	210	-	533	-	400	140 -	660
Arsenic	230	7,0 - 210	2,4,6,7	5,310	580	12 - 2,900	6,10,12,4,6,10,14
Barium	1,600	0,10 - 0,12	3,000	6,7	200	5,600	10,000 - 21,000
Boron	1,1	-	-	-	-	-	6,10
Cadmium	1,500	130 -	5,100	2,4,6,7,14	20,800	700 - 77,700	6,7 - 130 <sup>c</sup>
Calcium	71,000	52,000 - 130	89,000	6,7 - 5,100	38,400	2,300 - 62,000	6,300 - 1,300,000 <sup>c,d</sup>
Chromium	1,800	-	5,100	2,4,6,7,14	5,600	2,190 - 9,400	6,400 - 85
Cobalt	53	44 - 62	-	-	500	500 - 500	41,000
Copper	4,200	760 - 8,900	8,900	6,7,14	12,200	7,700 - 18,100	90 - 13,000
Gold	5,0	0,55 - 0,7	-	-	-	-	260
Iron	62,000	4,200 - 190,000	190,000	6,7,14	61,600	3,400 - 130,800	4,800 - 3,400
Lead	6,600	1,500 - 20,000	32,000	2,4,6,7,14	46,900	22,700 - 101,000	110,000 - 12,000
Magnesium	23,000	-	27,000	6,7	5,330	300 - 8,600	39,000 - 3,700
Manganese	12,000	330 -	88,000	6,7,14	1,370	100 - 2,740	22,000 <sup>c</sup> - 1,500
Molybdenum	-	-	-	-	-	-	340 - 5,000
Nickel	990	130 -	4,800	2,4,6,7,14	2,800	1,580 - 4,330	83 <sup>c</sup> - 5,000
Phosphorus	59,000	53,000 - 64,000	6,7	-	29,600	8,000 - 46,900	3,300 - 4,7
Potassium	-	-	-	-	-	-	34,000 - 16,000
Selenium	0.76 <sup>c</sup>	-	-	-	-	-	6,14
Silicon	-	-	6	-	400	1,800 - 17,100	-
Silver	180	62 -	770	6,7,14	45,000	9,100 - 81,100	11,000 - 560
Sodium	6,900	5,400 -	8,500	6,7	975	909 - 1,060	14 - 520
Strontium	-	-	-	-	12,200	3,400 - 27,000	150 - 150
Sulfur	470,000	190,000 -	910,000	6,7	36,300	10,000 - 52,500	74,000 <sup>c</sup> - 970
Thorium	-	-	-	-	-	-	6,10,14
Tin	1,200	1,100 -	1,300	6,7	16,400	11,600 - 23,900	810,000 -
Titanium	7,500	7,100 -	8,000	6,7	3,730	2,600 - 8,100	20,000 - 19,000 <sup>c</sup>
Vanadium	820	300 -	21,000	6,7	1,750	700 - 2,800	19,000 <sup>c</sup> - 53,000
Zinc	10,000	2,400 -	6,7,14	47,300	22,700	9,700 - 14	56 - 9,400

(continued)

TABLE 4-2. (Continued)

Pollutant	After ESP		References	After Fabric Filter		References	After Scrubber f and Afterburner		References
	Average	Range		Average	Range		Average	Range	
Aluminum	220,000	-	6	530,000	-	7	-	-	-
Antimony	4,6	-	6	1,200	-	7	-	-	-
Arsenic	1,400	-	6	2,400	-	7	69	-	4
Barium	11,000	-	6	2,400	-	7	-	-	-
Beryllium	-	-	-	-	-	-	-	-	-
Boron	-	-	-	-	-	-	-	-	-
Cadmium	170	-	6	10,000	-	7	-	-	4
Calcium	530,000	-	6	60,00	-	7	-	-	-
Chromium	1,700	-	6	14,000	-	7	-	-	-
Cobalt	420	-	6	2,000	-	7	-	-	-
Copper	430	-	6	1,900	-	7	-	-	4
Gold	6.3	-	6	-	-	-	-	-	-
Iron	27,000	-	6	83,000	-	7	-	-	-
Lead	2,400	-	6	4,500	-	7	-	-	4
Magnesium	1,400	-	6	24,000	-	7	-	-	-
Manganese	290	-	6	180	-	7	-	-	-
Molybdenum	-	-	-	-	-	-	-	-	-
Nickel	2,000	-	6	5,100	-	7	-	-	4
Phosphorous	11,000	-	6	37,000	-	7	-	-	-
Potassium	-	-	-	-	-	-	-	-	-
Selenium	800	-	6	5,700	-	7	-	-	-
Silicon	-	-	-	-	-	-	-	-	-
Silver	16	-	6	-	-	-	-	-	-
Sodium	1,400	-	6	8,600	-	7	-	-	-
Strontium	-	-	-	-	-	-	-	-	-
Sulfur	19,000,000 <sup>d</sup>	-	6	77,000	-	7	-	-	-
Thorium	-	-	-	-	-	-	-	-	-
Tin	580	-	6	440	-	7	-	-	-
Titanium	1,600	-	6	4,700	-	7	-	-	-
Vanadium	190	-	6	1,700	-	7	-	-	-
Zinc	530	-	6	31,000	-	7	33,000	-	4
Zirconium	-	-	-	-	-	-	-	-	-

<sup>a</sup>Cyclone or impingement tray scrubber.<sup>b</sup>Venturi scrubber alone or in series with low-energy devices.<sup>c</sup>One data point.<sup>d</sup>Includes impinger catch.<sup>e</sup>From pilot scale control device.<sup>f</sup>Overall control by venturi scrubber, impingement tray scrubber, and afterburner in series.

TABLE 4-3. INORGANIC COMPOUND EMISSION FACTORS IN SI UNITS ON A TOTAL FEED BASIS  
FOR MULTIPLE HEARTH FURNACES BURNING SEWAGE SLUDGE  
(grams of Pollutant Emitted per megagram of Dry Sludge Feed)  $\times 10^3$

Pollutant	Average	Range	Uncontrolled			After Low-Energy Scrubber <sup>a</sup>			After High-Energy Scrubber <sup>b</sup>			References
			References	Average	Range	References	Average	Range	References	Average	Range	
Aluminum	440,000	770	-	880,000	6.7	10,000	305	25,000	19	290,000	-	-
Antimony	1,600	47	-	3,200	6.7	305	195	370	19	260	-	-
Arsenic	5,500	160	-	28,000	2.4, 6, 7, 14	2,050	115	10,050	19	320	20	850
Barium	23,000	42	-	49,000	6.7	1,700	115	4,650	19	6,700	-	-
Beryllium	9.5	9.0	-	10	2	-	-	-	-	0.85	-	2
Boron	-	-	-	-	-	-	-	-	-	-	-	-
Cadmium	19,000	1,000	-	54,000	2.4, 6, 7, 14	13,500	550	50,000	19	2,000	240	0,000
Calcium	730,000	12,000	-	1,400,000	6.7	23,000	1,350	42,000	19	430,000	-	-
Chromium	160,000	95	-	1,000,000	2.4, 6, 7, 14	3,050	1,900	7,500	19	2,000	150	11,000
Cobalt	520	9	-	1,000	6.7	215	49	400	19	63	-	-
Copper	230,000	1,100	-	900,000	6.7, 14	9,000	2,800	15,000	19	5,500	700	11,000
Gold	2.1	1.0	-	3.0	6.7	-	-	-	-	1.2	-	-
Iron	3,200,000	13,000	-	11,000,000	6.7, 14	32,500	1,900	115,000	19	32,000	1,600	75,000
Lead	340,000	800	-	2,400,000	2.4, 6, 7, 14	37,500	16,500	70,000	19	20,000	3,000	55,000
Magnesium	220,000	4,200	-	440,000	6.7	3,400	175	7,000	19	6,000	-	-
Manganese	180,000	75	-	750,000	6.7, 14	1,300	85	4,300	19	500	45	1,300
Molybdenum	-	-	-	-	-	-	-	-	-	-	-	-
Nickel	45,000	65	-	190,000	2.4, 6, 7, 14	1,750	180	3,100	19	2,200	100	14,000
Phosphorous	530,000	11,000	-	1,100,000	6.7	17,000	6,700	27,500	19	9,000	-	-
Potassium	-	-	-	-	-	-	-	-	-	-	-	-
Selenium	-	-	-	-	-	-	-	-	-	-	-	-
Silicon	-	-	-	-	-	-	-	-	-	-	-	-
Silver	8,500	20	-	23,000	7,14	30,500	5,000	65,000	19	-	-	-
Sodium	70,000	1,000	-	140,000	6.7	6,000	2,000	11,500	19	310	85	550
Strontium	7,900,000	3,800	-	16,000,000	6.7	19,500	15,000	21,500	-	200,000	-	-
Sulfur	-	-	-	-	-	-	-	-	-	-	-	-
Thorium	-	-	-	-	-	-	-	-	-	-	-	-
Tin	9,800	250	-	19,300	6.7	10,500	6,000	19,500	19	9,200	-	-
Titanium	66,000	1,400	-	131,000	6.7	2,750	135	7,000	19	4,700	-	-
Vanadium	2,600	-	-	6,500	6.7	600	49	1,150	19	500	-	-
Zinc	850,000	1,500	-	5,500,000	6.7, 14	2,400	650	60,000	19	26,000	5,500	50,000
Zirconium	-	-	-	-	-	-	-	-	-	-	-	-

(continued)

TABLE 4-3. (Continued)

Pollutant	After ESP Average, <sup>c</sup> Range	After Fabric Filter Average, <sup>c</sup> Range		After Scrubber <sup>d</sup> and Afterburner <sup>d</sup> Average Range		References	References
		After Cyclone <sup>a</sup> Range	References	After Cyclone <sup>a</sup> Range	References		
Aluminum	150,000	6	880	1.5	7	7	-
Antimony	35	6	-	3.1	7	7	-
Arsenic	1,200	6	-	3.9	7	7	-
Barium	7,500	6	-	-	-	-	-
Beryllium	-	-	-	-	-	-	-
Boron	-	-	-	-	-	-	-
Cadmium	150	6	13	7	7	7	4
Calcium	370,000	6	94	17	7	7	-
Chromium	1,500	6	-	2.3	7	7	-
Cobalt	370	6	-	2.2	7	7	4
Copper	200	6	-	-	-	-	-
Gold	-	-	100	-	-	-	-
Iron	27,000	6	6	7	7	7	-
Lead	1,700	6	6	6	7	7	33,000
Magnesium	9,000	6	30	7	7	7	-
Manganese	360	6	0.2	7	7	7	-
Molybdenum	-	-	-	-	-	-	-
Nickel	5,600	6	6.1	7	7	7	200
Phosphous	6,900	6	42	7	7	7	-
Potassium	-	-	-	-	-	-	-
Selenium	-	-	1.9	7	7	7	-
Silicon	-	-	-	-	-	-	-
Silver	-	-	-	1.0	7	7	-
Sodium	540	6	12	-	-	-	-
Strontium	-	-	-	-	-	-	-
Sulfur	7,800,000	6	-	100	7	7	-
Thorium	-	-	-	-	-	-	-
Tin	200	6	0.6	7	7	7	-
Titanium	870	6	6.2	7	7	7	-
Vanadium	200	6	2.0	7	7	7	-
Zinc	410	6	39	7	7	7	-
Zirconium	-	-	-	-	-	-	-

<sup>a</sup>Cyclone or impingement tray scrubber.<sup>b</sup>Venturi scrubber alone or in series with low-energy devices.<sup>c</sup>One data point.<sup>d</sup>Overall control by venturi scrubber, impingement tray scrubber and afterburner in series.<sup>e</sup>From pilot scale control device.

TABLE 4-4. INORGANIC COMPOUND EMISSION FACTORS IN ENGLISH UNITS ON A TOTAL FEED BASIS  
FOR MULTIPLE HEARTH FURNACES BURNING SEWAGE SLUDGE  
(lbs of Pollutant Emitted per ton of Dry Sludge Feed)  $\times 10^6$

Pollutant	Uncontrolled		References	After Low-Energy Scrubber <sup>a</sup>		References	After High-Energy Scrubber <sup>b</sup>	
	Average	Range		Average	Range		Average	Range
Aluminum	860,000	1,500 - 1,800,000	6,7	2,000	610 - 50,000	19	590,000 <sup>c</sup>	-
Antimony	3,200	94 - 6,000	6,7	610	390 - 740	19	510	-
Arsenic	11,000	320 - 57,000	2,4,6,7,14	4,100	230 - 21,000	19	630	41 - 1,700
Barium	49,000	83 - 99,000	6,7	3,400	230 - 9,300	19	13,000 <sup>c</sup>	-
Beryllium	19	17 - 20	2	-	-	-	2	-
Boron	-	-	-	-	-	-	-	-
Cadmium	38,000	2,000 - 110,000	2,4,6,7,14	27,000	1,100 - 100,000	19	4,100	470 - 16,000
Calcium	1,500,000	24,000 - 2,900,000	6,7	46,000	2,700 - 84,000	19	860,000 <sup>c</sup>	-
Chromium	310,000	190 - 2,000,000	2,4,6,7,14	7,900	3,800 - 15,000	19	4,100	300 - 21,000
Cobalt	1,000	17 - 2,000	6,7	430	99 - 800	19	130 <sup>c</sup>	-
Copper	460,000	2,100 - 1,800,000	6,7,14	18,000	5,600 - 30,000	19	11,000 <sup>c</sup>	1,400 - 22,000
Gold	4	2 - 6	6,7	-	-	-	2	-
Iron	6,400,000	25,000 - 22,000,000	6,7,14	65,000	3,800 - 230,000	19	65,500	3,200 - 150,000
Lead	690,000	1,600 - 4,700,000	2,4,6,7,14	75,000	33,000 - 140,000	19	40,000	6,100 - 110,000
Magnesium	440,000	6,500 - 680,000	6,7	6,800	350 - 14,000	19	12,000 <sup>c</sup>	-
Manganese	360,000	150 - 1,500,000	6,7,14	2,600	170 - 8,700	19	990	90 - 2,500
Molybdenum	-	-	-	-	-	-	-	-
Nickel	91,000	130 - 370,000	2,4,6,7,14	3,500	360 - 6,200	19	4,400	210 - 27,000
Phosphorus	1,100,000	21,000 - 2,100,000	6,7	36,000	9,400 - 55,000	19	20,000 <sup>c</sup>	-
Potassium	-	-	-	-	-	-	-	-
Selenium	-	-	-	-	-	-	-	-
Silicon	-	-	-	-	-	-	-	-
Silver	17,000	41 - 46,000	6,7,14	1,900	61,000 - 130,000	19	4,30	-
Sodium	140,000	2,100 - 280,000	6,7	12,000	1,200 - 3,100	19	1,200	-
Strontium	-	-	-	4,000	4,000 - 23,000	19	36,000 <sup>c</sup>	-
Sulfur	16,000,000	7,600 - 32,000,000	6,7	39,000	30,000 - 43,000	19	400,000 <sup>c</sup>	-
Thorium	-	-	-	-	-	-	-	-
Tin	20,000	510 - 39,000	6,7	21,000	12,000 - 39,000	19	18,000 <sup>c</sup>	-
Titanium	120,000	2,500 - 250,000	6,7	5,200	2,700 - 14,000	19	9,000 <sup>c</sup>	-
Vanadium	5,100	540 - 9,700	6,7	1,200	99 - 2,300	19	1,000 <sup>c</sup>	-
Zinc	1,700,000	3,100 - 11,000,000	6,7,14	46,000	1,300 - 120,000	19	53,000	11,000 - 100,000
Zirconium	-	-	-	-	-	-	-	-

(continued)

TABLE 4-4. (Continued)

Pollutant	After ESP		After Fabric Filter		After Scrubber and Afterburner		References
	Average	Range	Average	Range	Average	Range	
Aluminum	300,000	-	6	-	1,800	-	7
Antimony	70	-	6	-	3.1	-	7
Arsenic	2,500	-	6	-	6.2	-	7
Barium	15,000	-	6	-	7.7	-	7
Beryllium	-	-	-	-	-	-	-
Boron	-	-	-	-	-	-	-
Cadmium	310	-	6	-	27	-	4
Calcium	740,000	-	6	-	190	-	7
Chromium	3,000	-	6	-	34	-	7
Cobalt	750	-	6	-	4.7	-	7
Copper	390	-	6	-	4.4	-	7
Gold	-	-	-	-	-	-	-
Iron	54,000	-	6	-	200	-	7
Lead	3,300	-	6	-	11	-	7
Magnesium	18,000	-	6	-	60	-	7
Manganese <sup>e</sup>	730	-	6	-	0.5	-	7
Molybdenum	-	-	-	-	-	-	-
Nickel	11,000	-	6	-	12	-	7
Phosphorus	14,000	-	6	-	83	-	7
Potassium	-	-	-	-	-	-	-
Selenium	-	-	-	-	3.7	-	7
Silicon	-	-	-	-	-	-	-
Silver	-	-	-	-	-	-	-
Sodium	1,100	-	6	-	1.9	-	7
Strontium	-	-	-	-	23	-	7
Sulfur	16,000,000	-	6	-	-	-	7
Thorium	-	-	-	-	200	-	7
Tin	400	-	6	-	1.3	-	7
Titanium	1,700	-	6	-	13	-	7
Vanadium	420	-	6	-	4	-	7
Zinc	820	-	6	-	80	-	7
Zirconium	-	-	-	-	-	-	-

<sup>a</sup>Cyclone or impingement tray scrubber.<sup>b</sup>Venturi scrubber alone or in series with low-energy devices.<sup>c</sup>One data point.<sup>d</sup>Overall control by venturi scrubber, impingement tray scrubber and afterburner in series.<sup>e</sup>From pilot scale control device.

fabric filter. It should be noted that data from reference 14 are apparently biased high. The test report authors noted, but did not explain their "consistent error", and reported an average of 20 percent more mass emitted than fed, on a compound-specific basis. No attempt has been made here to adjust or modify the values reported by the original reference. Unreasonable (physically impossible) results have been individually noted in the tables.

#### 4.2 EMISSION FACTORS FOR FLUIDIZED BED COMBUSTORS

Emission factors for inorganic compound emissions from fluidized bed combustors are presented in Table 4-5 through 4-8. Fluidized bed combustors are generally controlled by high-energy scrubbers, and no data are available for any other control devices. Emission factors are presented for both uncontrolled and controlled emissions.

#### 4.3 EMISSION FACTORS FOR ORGANIC COMPOUNDS

Emission factors for volatile organic compounds are presented in Tables 4-9 and 4-10 in SI and English units, respectively. All data are from multiple hearth furnaces and are separated by control device type. All tested facilities are controlled by a venturi scrubber; emissions controlled by a scrubber and an afterburner are reported separately. Uncontrolled emissions are also reported.

Emission factors for semivolatile compounds are reported in Tables 4-11 and 4-12 in SI and English units, respectively. Emission factors are for uncontrolled and controlled emissions. All data are for emissions from multiple hearth furnaces except one FBC data set controlled by a high energy scrubber. The emission factors from the FBC facility were within the range of the MHF data and were therefore not reported separately.

#### 4.4 OTHER COMBUSTOR TYPES

Emission factors for the other sludge incinerator types described in Section 3 have not been separately prepared because of insufficient data. The expected emissions from electric furnaces, single hearth cyclones, rotary kilns, and high pressure wet air oxidation systems cannot be quantified with the available data. Data for emissions from co-incineration of sewage sludge with refuse are also not available.

TABLE 4-5. INORGANIC COMPOUND EMISSION FACTORS ON A COMPOUND FEED BASIS  
FOR FLUIDIZED BED COMBUSTORS BURNING SEWAGE SLUDGE  
(Mass of Pollutant Emitted per Mass in Sludge Feed)  $\times 10^6$

Pollutant	Uncontrolled		References	After Low-Energy Scrubber <sup>a</sup>		References	After High-Energy Scrubber <sup>b</sup>		References
	Average	Range		Average	Range		Average	Range	
Aluminum	-	-	-	150	-	19	-	-	-
Antimony	-	-	-	760	-	19	-	-	-
Boron	-	-	-	3,700	-	19	4,300 <sup>b</sup>	1,100	7,500
Beryllium	-	-	-	170	-	19	-	-	3,20
Boron	-	-	-	-	-	-	-	-	-
Cadmium	210,000	55,000	360,000	14	360	19	60,000	460	130,000
Calcium	64,000	46,000	82,000	14	220	19	2,600	34	7,000
Chromium	-	-	-	-	-	-	-	-	-
Cobalt	69,000	45,000	93,000	14	2,300	19	-	-	3,14,18,20
Copper	-	-	-	-	-	-	-	-	-
Gold	-	-	-	-	-	-	-	-	-
Iron	85,000	79,000	91,000	14	200	19	1,300	14	6,000
Lead	300,000	72,000	520,000	14	110	19	520	-	14
Magnesium	61,000	41,000	82,000	14	740	19	110,000	160	510,000
Manganese	-	-	-	-	-	-	-	-	3,14,18,20
Molybdenum	-	-	-	-	-	-	-	-	-
Nickel	1,800,000 <sup>c</sup>	53,000	3,500,000 <sup>c</sup>	14	280	19	2,400	0.55	4,700
Phosphorus	-	-	-	-	-	-	-	-	3,14
Potassium	-	-	-	-	-	-	-	-	-
Selenium	-	-	-	-	-	-	-	-	-
Silicon	-	-	-	-	-	-	-	-	-
Silver	2,500,000 <sup>c</sup>	46,000	5,000,000 <sup>c</sup>	14	61	19	1,700,000	40	3,300,000 <sup>d</sup>
Sodium	-	-	-	-	-	-	-	-	-
Strontium	-	-	-	-	-	-	-	-	-
Sulfur	-	-	-	-	-	-	-	-	-
Thorium	-	-	-	-	-	-	-	-	-
Tin	-	-	-	-	-	-	-	-	-
Titanium	-	-	-	-	-	-	-	-	-
Vanadium	-	-	-	-	-	-	-	-	-
Zinc	74,000	52,000	95,000	14	330	19	620	290	1,400
Zirconium	-	-	-	-	-	-	-	-	-

<sup>a</sup>Impingement tray scrubber or cyclone.

<sup>b</sup>Venturi followed by impingement tray scrubber.

<sup>c</sup>One data point.

<sup>d</sup>Reference 14 tests are biased; emissions reported are greater than quantity fed in some cases.

TABLE 4-6. INORGANIC COMPOUND EMISSION FACTORS ON A TOTAL PARTICULATE EMISSION BASIS  
FOR FLUIDIZED BED COMBUSTORS BURNING SEWAGE SLUDGE  
(Mass of Pollutant Emitted per Mass of Total Particulate Emitted)  $\times 10^6$

Pollutant	Average	Uncontrolled Range	After Low-Energy Scrubber <sup>a</sup>		After High-Energy Scrubber <sup>b</sup>		References
			Average	Range	Average	Range	
Aluminum	-	-	31,000	-	19	90,000 <sup>c</sup>	-
Antimony	19	1.3 - 36	14	-	-	-	11
Arsenic	-	-	4,000	-	19	18,000 <sup>c</sup>	3, 11, 14, 20
Barium	-	-	-	-	-	2,200 <sup>c</sup>	11
Beryllium	-	-	-	-	-	-	-
Boron	-	-	-	-	-	670 <sup>c</sup>	11
Cadmium	47	7.9 - 87	14	1,300 - 88,000	19	150,000 <sup>c</sup>	3, 11, 14, 20
Calcium	370	64 - 670	14	2,800 -	19	140,000 <sup>c</sup>	11
Chromium	-	-	-	-	-	360,000 <sup>c</sup>	3, 11, 14, 20
Cobalt	-	-	-	-	-	17 <sup>c</sup>	11
Copper	3,200	170 - 6,300	14	2,800 -	19	12,000 <sup>c</sup>	42,000 <sup>d</sup>
Gold	39,000	770 - 76,000	14	45,000 -	19	12,000 <sup>c</sup>	520 - 24,000 <sup>d</sup>
Iron	1,500	280 - 2,700	14	23,000 -	19	320,000 <sup>c</sup>	1,200,000 <sup>d</sup>
Lead	-	-	-	-	-	-	3, 11, 14, 20
Magnesium	4,400	26 - 8,900	14	10,000 -	19	17,000 <sup>c</sup>	-
Manganese	-	-	-	-	-	1,800 <sup>c</sup>	16 - 4,600
Molybdenum	-	-	-	-	-	6 <sup>c</sup>	11, 14
Nickel	630	600 - 660	14	-	-	3,800,000 <sup>d</sup>	22 - 15,000,000 <sup>d</sup>
Phosphorous	-	-	-	-	-	63,000 <sup>c</sup>	11
Potassium	-	-	-	-	-	9,100 <sup>c</sup>	11
Selenium	-	-	-	-	-	-	-
Silicon	-	-	-	-	-	170,000 <sup>c</sup>	-
Silver	250	150 - 360	14	41,000 -	19	41,000 <sup>c</sup>	36 - 120,000 <sup>d</sup>
Sodium	-	-	-	-	-	31,000 <sup>c</sup>	11
Sulfur	-	-	-	-	-	590 <sup>c</sup>	11
Thorium	-	-	-	-	-	-	-
Tin	-	-	-	-	-	-	-
Titanium	-	-	-	-	-	5,900 <sup>c</sup>	-
Vanadium	-	-	-	-	-	6,600 <sup>c</sup>	11
Zinc	4,000	170 - 7,800	14	20,000 -	19	1,800 <sup>c</sup>	11
Zirconium	-	-	-	-	-	17,000 <sup>c</sup>	6,200 - 4,200 - 9,400

<sup>a</sup>Cyclone or impingement tray scrubber.

<sup>b</sup>Venturi followed by impingement tray scrubber.

<sup>c</sup>One data point.

<sup>d</sup>Reference 14 tests are biased; emissions reported are greater than quantity fed in some cases.

TABLE 4-7. INORGANIC COMPOUND EMISSION FACTORS IN SI UNITS ON A TOTAL FEED BASIS  
 FOR FLUIDIZED BED COMBUSTORS BURNING SEWAGE SLUDGE  
 (grams of Pollutant Emitted per megagram of Dry Sludge Feed)  $\times 10^3$

Pollutant	Average	Uncontrolled Range		References	After Low-Energy Scrubber <sup>a</sup>		References	After High-Energy Scrubber <sup>a</sup>		References
		Average	Range		Average	Range		Average	Range	
Aluminum	-	-	-	-	1,900	-	19	-	-	-
Antimony	-	-	-	-	24	-	19	-	-	-
Arsenic	700	350	1,000	14	360	-	19	50	2,6	120
Barium	-	-	-	-	240	-	19	-	-	-
Beryllium	-	-	-	-	-	-	-	-	-	-
Boron	-	-	-	-	-	-	-	-	-	-
Cadmium	3,500	1,000	6,000	14	85	-	19	800	3,5	3,14,18,20
Calcium	-	-	-	-	5,000	-	19	-	-	-
Chromium	205,000	6,500	500,000	14	170	-	19	280	2,4	700
Cobalt	-	-	-	-	70	-	19	-	-	-
Copper	97,000	60,000	135,000	14	170	-	19	1,300	10	3,800
Gold	-	-	-	-	-	-	-	-	-	-
Iron	670,000	600,000	730,000	14	2,700	-	19	3,200	20	6,500
Lead	125,000	26,000	220,000	14	1,400	-	19	40,000	60	190,000
Magnesium	-	-	-	-	600	-	19	-	-	-
Manganese	52,000	20,000	85,000	14	270	-	19	1,200	0,60	2,400
Molybdenum	-	-	-	-	-	-	-	-	-	-
Nickel	260,000	5,500	520,000	14	260	-	19	35,000	0,80	135,000
Phosphorus	-	-	-	-	2,300	-	19	-	-	-
Potassium	-	-	-	-	650	-	19	-	-	-
Selenium	-	-	-	-	220	-	19	-	-	-
Silicon	-	-	-	-	3,200	-	19	-	-	-
Silver	59,000	3,500	115,000	14	-	-	-	33,000	3,0	67,000
Sodium	-	-	-	-	-	-	-	-	-	-
Strontium	-	-	-	-	1,200	-	19	-	-	-
Sulfur	-	-	-	-	8,500	-	19	-	-	-
Thorium	-	-	-	-	-	-	-	-	-	-
Tin	-	-	-	-	-	-	-	-	-	-
Titanium	-	-	-	-	360	-	19	-	-	-
Vanadium	-	-	-	-	390	-	19	-	-	-
Zinc	100,000	75,000	140,000	14	110	-	19	1,000	-	-
Zirconium	-	-	-	-	-	-	-	1,200	240	2,500
										14,20

<sup>a</sup>Cyclone or impingement tray scrubber.

<sup>b</sup>Venturi followed by impingement tray scrubber.

<sup>c</sup>One data point.

TABLE 4-B. INORGANIC COMPOUND EMISSION FACTORS IN ENGLISH UNITS ON A TOTAL  
FEED BASIS FOR FLUIDIZED BED COMBUSTORS BURNING SEWAGE SLUDGE  
\* (lbs of Pollutant Emitted per ton of Dry Sludge Feed)  $\times 10^3$

Pollutant	Uncontrolled		References	After Low-Energy Scrubber <sup>a</sup> Average Range	References	After High-Energy Scrubber <sup>b</sup> Average Range	References
	Average	Range					
Aluminum	-	-	-	-	-	-	-
Antimony	-	-	-	-	-	-	-
Arsenic	1.4	0.7 - 2.0	14	0.047 0.68 0.47	19 19 19	0.10	0.0056 0.25
Barium	-	-	-	-	-	-	-
Beryllium	-	-	-	-	-	-	-
Boron	-	-	-	-	-	-	-
Cadmium	7.0	2.0 - 12	14	0.17 10	19	1.6	0.007 6.3
Calcium	-	-	-	-	-	-	-
Chromium	57	13 - 100	14	0.33 0.14	19 19	0.56	0.0047 1.4
Cobalt	-	-	-	-	-	-	-
Copper	190	120 - 270	14	0.33 -	19	2.6	0.02 7.6
Gold	-	-	-	-	-	-	-
Iron	1,300	1,200 - 1,500	14	-	19	6.4	0.04 13
Lead	250	52 - 440	14	2.7 1.2	19 19	79	0.12 380
Magnesium	-	-	-	-	-	-	-
Manganese	100	41 - 170	14	0.54 -	19	2.5	0.0012 4.9
Molybdenum	-	-	-	-	-	-	-
Nickel	520	11 - 1,000	14	0.52 5.0 1.3	19 19 19	70	0.0016 270
Phosphorus	-	-	-	-	-	-	-
Potassium	-	-	-	-	-	-	-
Selenium	-	-	-	-	-	-	-
Silicon	-	-	-	-	-	-	-
Silver	120	7.0 - 230	14	6.4 2.4	19 19	67	0.006 130
Sodium	-	-	-	-	-	-	-
Strontium	-	-	-	-	-	-	-
Sulfur	-	-	-	-	-	17	-
Thorium	-	-	-	-	-	19	-
Tin	-	-	-	-	-	-	-
Titanium	-	-	-	-	-	-	-
Vanadium	-	-	-	-	-	-	-
Zinc	210	150 - 270	14	0.21 2.0	19 19	2.4	0.48 5.1
Zirconium	-	-	-	-	-	-	-

<sup>a</sup>Cyclone or impingement tray scrubber.

<sup>b</sup>Venturi followed by impingement tray scrubber.  
One data point.

TABLE 4-9. VOLATILE ORGANIC COMPOUND EMISSION FACTORS IN SI UNITS FOR  
MULTIPLE HEARTH AND FLUIDIZED BED INCINERATORS BURNING SEWAGE SLUDGE  
(grams of Pollutant Emitted per megagram of Dry Sludge Feed)  $\times 10^3$

Pollutant	Uncontrolled		References	After-High Energy Scrubber <sup>a</sup>		References	After Scrubber <sup>b</sup> and Afterburner <sup>b</sup>		References
	Average	Range		Average	Range		Average	Range	
Acetone	-	-	-	-	-	-	-	-	-
Acetonitrile	69,000	54,000 - 97,000	4	3,400 <sup>c</sup>	9,700 <sup>c</sup>	5	4	740	-
Acrylonitrile	34,000	22,000 - 47,000	2.4	22,000	8,200 - 33,000	1,2,4	4	490	-
Benzene	7,500	5,800 - 9,800	2.4,5	6,300 <sup>c</sup>	400 - 14,000	1,2,3,4,5	5	170	-
Bromodichloromethane	9,800 <sup>c</sup>	7,600 - 12,000	4	1,500 <sup>c</sup>	-	5	-	-	-
Bromoethane	760 <sup>c</sup>	-	5	-	-	-	-	-	-
Carbon Tetrachloride	22	3.1 - 37	2.4	26	3.1 - 68	1,2,3,4	6.8	-	-
Chlorobenzene	910	310 - 1,600	2.4,5	900 <sup>c</sup>	5.0 - 3,100	1,2,3,4,5	5	260	-
Chloroethane	430 <sup>c</sup>	-	5	600 <sup>c</sup>	-	5	-	-	-
Chloroform	71	5.1 - 140	2.4,5	3,300	5.1 - 8,500	1,2,3,4,5	5	490	-
1,1-Dichloroethane	-	-	-	550 <sup>c</sup>	-	5	-	-	-
1,2-Dichloroethane	-	-	-	14 <sup>c</sup>	-	5	-	-	-
Trans-1,2-Dichloroethane	49	6.0 - 92	2.5	1,300	6.0 - 5,200	1,2,4,5	5	31	-
1,1-Dichloroethene	20 <sup>c</sup>	-	5	370 <sup>c</sup>	-	5	-	-	-
Ethylbenzene	1,200	300 - 2,500	2.4,5	1,000	22 - 2,300	1,2,3,4,5	5	-	-
Methyl Chloride	.65	29 - 140	4	1,300	76 - 2,200	1,3,4,5	19	-	-
Methyl Ethyl Ketone	6,900	1,200 - 12,000	2.4	5,700	1,200 - 8,900	2,4,5	420	-	-
Pyridine	-	-	-	-	-	5	-	-	-
Tetrachloroethene	800	290 - 1,400	2.4,5	5,700	150 - 21,000	1,2,3,4,5	5	-	-
Toluene	6,800	3,600 - 16,000	2.4,5	9,900	62 - 19,000	1,2,3,4,5	910	-	-
1,1,1-Trichloroethane	70	4.6 - 130	2.4,5	970	4.6 - 3,200	1,2,3,4,5	660	-	-
Trichloroethene	250	55 - 440	2.4,5	1,300	11 - 4,400	1,2,3,4,5	1,400	-	-
Vinyl Chloride	5,100 <sup>c</sup>	1,100 - 9,600	2.4,5	3,600	600 - 9,600	1,2,3,4,5	1,500	-	-
Xylene, m/p-	-	-	5	2,000 <sup>c</sup>	1,300 - 5	1,2,4,5	5	-	-
Xylene, o-	670 <sup>c</sup>	-	5	-	-	-	-	-	-
	950 <sup>c</sup>	-	-	-	-	-	-	-	-

<sup>a</sup>Venturi scrubber alone or in series with other low-energy devices.

<sup>b</sup>Overall control by venturi scrubber, impingement tray scrubber, and afterburner in series.

<sup>c</sup>One date point.

TABLE 4-10. VOLATILE ORGANIC COMPOUND EMISSION FACTORS IN ENGLISH UNITS FOR  
MULTIPLE HEARTH AND FLUIDIZED BED INCINERATORS BURNING SEWAGE SLUDGE  
(lbs of Pollutant Emitted per ton of Dry Sludge Feed)  $\times 10^6$

Pollutant	Uncontrolled		References	After High Energy Scrubber <sup>a</sup>		References	After Scrubber, b and Afterburner <sup>c</sup>		References
	Average	Range		Average	Range		Average	Range	
Acetone	140,000	110,000 - 66,000	4	6,800 <sup>c</sup>	-	5	15	-	4
Acetonitrile	60,000	94,000	2,4	19,000 <sup>c</sup>	-	4	970	-	4
Benzene	15,000	12,000 - 20,000	2,4,5	45,000	16,000 - 67,000	1,2,4	-	-	4
Bromo dichloromethane	20,000	15,000	2,4,5	17,000	800 - 28,000	1,2,3,4,5	340	-	4
Bromochloroethane	1,500 <sup>c</sup>	-	4	3,000 <sup>c</sup>	-	5	-	-	4
Carbon Tetrachloride	45	62	75	2,4	48	6,3	140	1,2,3,4	18
Chlorobenzene	1,800	620	3,300	2,4,5	1,900	10	6,100	1,2,3,4,5	530
Chloroethane	880 <sup>c</sup>	-	5	1,600 <sup>c</sup>	-	5	-	-	4
Chloroform	140	10	240	2,4,5	6,600	10	17,000	1,2,3,4,5	980
1,1-Dichloroethane	-	-	-	700 <sup>c</sup>	-	5	-	-	4
1,2-Dichloroethane	-	-	-	28	-	1	-	-	4
Trans-1,2-Dichloroethene	98	12	180	2,5	2,700	12	10,000	1,2,4,5	62
1,1-Dichloroethene	40 <sup>c</sup>	-	5	740 <sup>c</sup>	-	5	-	-	4
Ethylbenzene	2,400	600	5,100	2,4,5	2,100	43	4,600	1,2,3,4,5	39
Methylene Chloride	170	58	280	4	2,900	150	4,400	1,3,4,5	850
Methyl Ethyl Ketone	14,000	2,300	24,000	2,4	11,000	2,300	18,000	2,4,5	10
Pyridine	-	-	-	-	-	-	-	-	4
Tetrachloroethene	1,600	580	2,900	2,4,5	11,000	270	43,000	1,2,3,4,5	1,800
Toluene	14,000	7,100	33,000	2,4,5	20,000	120	37,000	1,2,3,4,5	1,300
1,1,1-Trichloroethane	140	91	260	2,4,5	1,900	9,1	6,400	1,2,3,4,5	2,700
Trichloroethene	500	110	880	2,4,5	3,000	21	8,800	1,2,3,4,5	3,100
Vinyl Chloride	10,000	2,100	19,000	2,4,5	7,600	1,600	19,000	1,2,4,5	-
Xylene, m/p-Xylene, o-	1,300 <sup>c</sup>	1,900 <sup>c</sup>	-	5	4,000 <sup>c</sup>	3,000	1,900	4,000	5

<sup>a</sup>Venturi scrubber alone or in series with other low-energy devices.

<sup>b</sup>Overall control by venturi scrubber, impingement tray scrubber, and afterburner in series.

<sup>c</sup>One data point.

TABLE 4-11. SEMI-VOLATILE ORGANIC COMPOUND EMISSION FACTORS IN SI UNITS FOR  
MULTIPLE HEARTH AND FLUIDIZED BED INCINERATORS BURNING SEWAGE SLUDGE  
(grams of Pollutant Emitted per Megagram of Dry Sludge Feed)

Pollutant	Dioxins (CDD), g/Mg x 10 <sup>6</sup>	Uncontrolled		References	After Low-Energy Scrubber <sup>b</sup> Range	Average	After High-Energy Scrubber <sup>c</sup> Range	Average	References
		Average	Range.						
<u>Dioxins (CDD), g/Mg x 10<sup>6</sup></u>									
Mono-CDD	-	-	-	-	-	-	-	-	-
Di-CDD	-	-	-	-	-	-	-	-	-
Tri-CDD	-	-	-	-	-	-	-	-	-
2,3,7,8-TetraCDD	-	-	-	-	-	-	-	-	-
Other-TCDD	35	17	0.94	17	60	29	100	4,10	4,10
Penta-CDD	1.4	1.7	56	17	120	1.7	230	4,10	4,10
Hexa-CDD	42	17	7.2	17	90	1.1	2.6	4,15	4,15,16
Hepta-CDD	220	17	47	17	47	0.76	84	4,15	4,15
Octa-CDD	250	17	150	17	38	2.6	67	4,15	4,15,16
Furans (CDF), g/Mg x 10 <sup>6</sup>	-	-	-	-	-	-	-	-	-
Mono-CDF	-	-	-	-	-	-	-	-	-
Di-CDF	-	-	-	-	-	-	-	-	-
Tri-CDF	-	-	-	-	-	-	-	-	-
2,3,7,8-TetraCDF	360	17	350	17	310	2.6	47	4,10	4,10
Other TCDF	980	17	1,000	17	550	7.9	970	4,10	4,10
Penta-CDF	880	17	690	17	39	3.3	88	4,10,16	4,10,16
Hexa-CDF	91	17	220	17	230	19	580	4,10,15,16	4,10,15,16
Hepta-CDF	510	17	430	17	35	4.6	200	4,10,15,16	4,10,15,16
Octa-CDF	520	17	320	17	21	0.60	87	4,10,15,16	4,10,15,16
Other Organics, g/Mg x 10 <sup>3</sup>	-	-	-	-	-	-	-	-	-
Bis (2-ethyl hexyl) phthalate	1,100	-	2	190 <sup>a</sup>	-	-	650	250	1,2,3
1,2-Dichlorobenzene	410	-	2	-	-	-	440 <sup>a</sup>	-	-
1,3-Dichlorobenzene	-	-	-	-	-	-	40 <sup>a</sup>	-	-
1,4-Dichlorobenzene	450	-	-	-	-	-	550 <sup>a</sup>	-	-
Naphthalene	22,000 <sup>e</sup>	20,000	26,000	2,4	8,500 <sup>a</sup>	21	1,300 <sup>a</sup>	510	2,200
2-Nitrophenol	6,000 <sup>e</sup>	49,000	57,000	2,4	490 <sup>a</sup>	21	1,300 <sup>a</sup>	-	-
Phenol	53,000 <sup>e</sup>	-	-	-	-	-	2,000 <sup>a</sup>	-	-

<sup>a</sup>One data point.

<sup>b</sup>Lapingett tray scrubber.

<sup>c</sup>Venturi alone or with other low-energy devices in series.

<sup>d</sup>Includes data from a fluidized bed combustor.

<sup>e</sup>More than one data point.

TABLE 4-12. SEMI-VOLATILE ORGANIC COMPOUND EMISSION FACTORS IN ENGLISH UNITS FOR  
MULTIPLE HEARTH AND FLUIDIZED BED INCINERATORS BURNING SEWAGE SLUDGE  
(lbs of Pollutant Emitted per ton of Dry Sludge Feed)

Pollutant	Dioxins (CDD), lb/ton x 10 <sup>9</sup>	Uncontrolled		After Low-Energy Scrubber <sup>b</sup>		After High-Energy Scrubber <sup>c</sup>		References	References	References
		Average	Range	Average	Range	Average	Range			
<b>Dioxins (CDD), lb/ton x 10<sup>9</sup></b>										
Mono-CDD	-	-	-	-	-	-	-	-	-	-
Di-CDD	-	-	-	-	-	-	-	-	-	-
Tri-CDD	-	-	-	-	-	-	-	-	-	-
2,3,7,8-TCDF	-	-	-	-	-	-	-	-	-	-
Other-TCDF	71	17	1.9	17	17	240	3.5	210	4,10	4,10
Penta-CDD	2,8	17	110	17	17	160	0.44	4,15	5,3	5,15
Hexa-CDD	83	17	15	17	17	94	2.3	310	4,15,16	4,15
Hepta-CDD	450	17	94	17	17	75	1.5	170	4,15	4,15
Octa-CDD	500	17	300	17	17	29	5.2	130	4,15	4,15
<b>furan (CDF), lb/ton x 10<sup>9</sup></b>										
Mono-CDF	-	-	-	-	-	-	-	-	-	-
Di-CDF	-	-	-	-	-	-	-	-	-	-
Tri-CDF	-	-	-	-	-	-	-	-	-	-
2,3,7,8-TCDF	-	-	-	-	-	-	-	-	-	-
Other-TCDF	71	17	700	17	17	1,100	16	620	4,10	4,10
Penta-CDF	2,000	17	2,000	17	17	79	6.6	1,900	4,10	4,10
Hexa-CDF	1,800	17	1,000	17	17	460	36	1,200	4,10,15,16	4,10,15,16
Hepta-CDF	180	17	440	17	17	170	9.6	400	4,10,15,16	4,10,15,16
Octa-CDF	1,000	17	860	17	17	70	1.6	170	4,10,15,16	4,10,15,16
<b>Other Organic, lb/ton x 10<sup>6</sup></b>										
Bis (2-ethyl hexyl) phthalate	2,100	-	2	-	-	-	-	1,300	500	- 1,900
1,2-Dichlorobenzene	620	-	2	-	-	-	-	870 <sup>a</sup>	-	-
1,3-Dichlorobenzene	-	-	-	-	-	-	-	80 <sup>a</sup>	-	-
1,4-Dichlorobenzene	-	-	-	-	-	-	-	2,700	1,000	-
Naphthalene	910	-	2	-	-	-	-	3,900 <sup>a</sup>	4,300	-
2-Nitrophenol	46,000 <sup>e</sup>	40,000	49,000	2.4	17,000	-	-	2,700	-	-
Phenol	12,000 <sup>e</sup>	99,000	120,000	2.4	990 <sup>a</sup>	-	-	4,000	-	-
	110,000 <sup>e</sup>	-	-	-	-	-	-	-	-	-

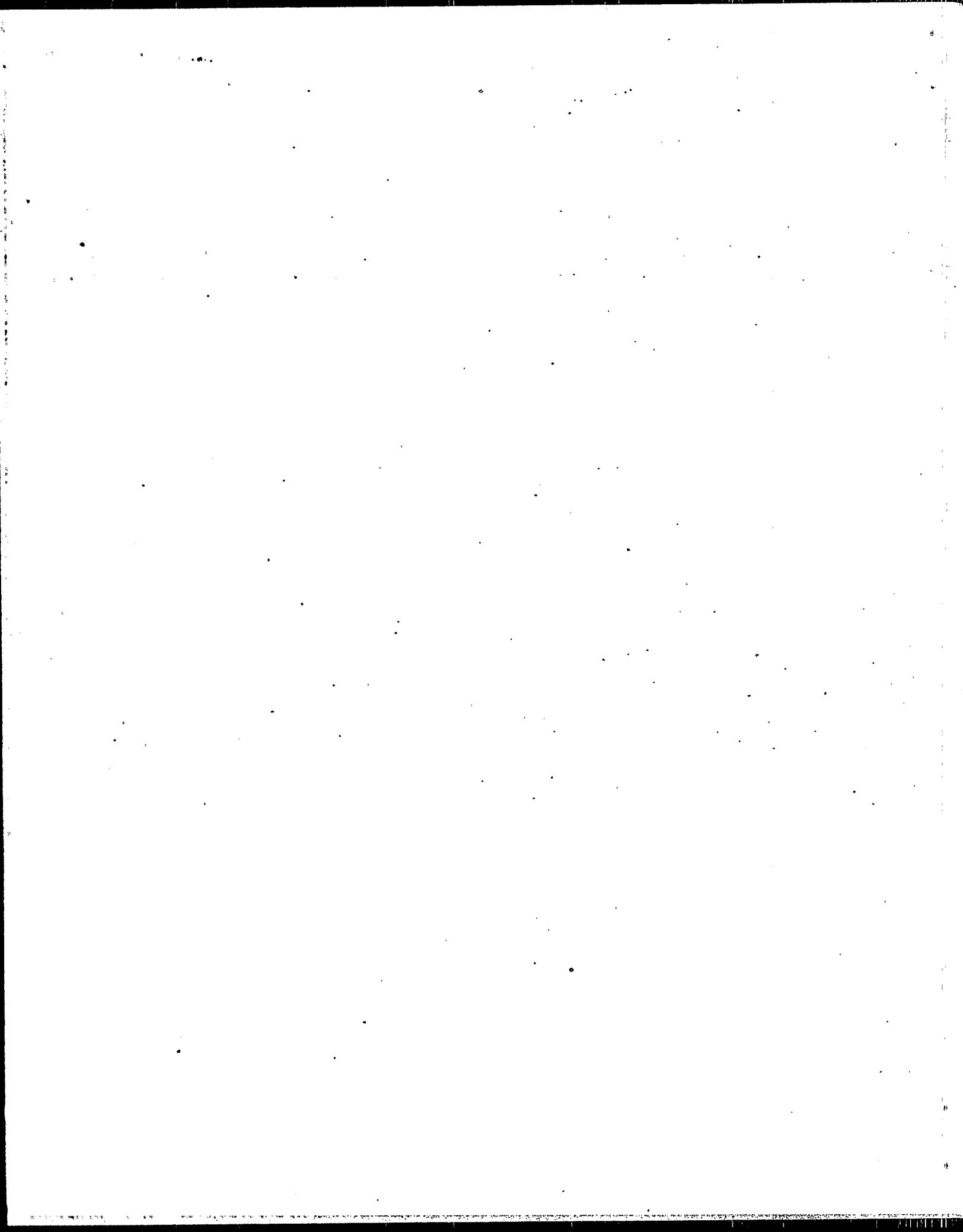
<sup>a</sup>One data point.

<sup>b</sup>Impingement tray scrubber.

<sup>c</sup>Venturi alone or with other low-energy devices in series.

<sup>d</sup>Includes one data set from a fluidized bed combustor; all other data from multiple hearth furnaces.

<sup>e</sup>More than one data point.

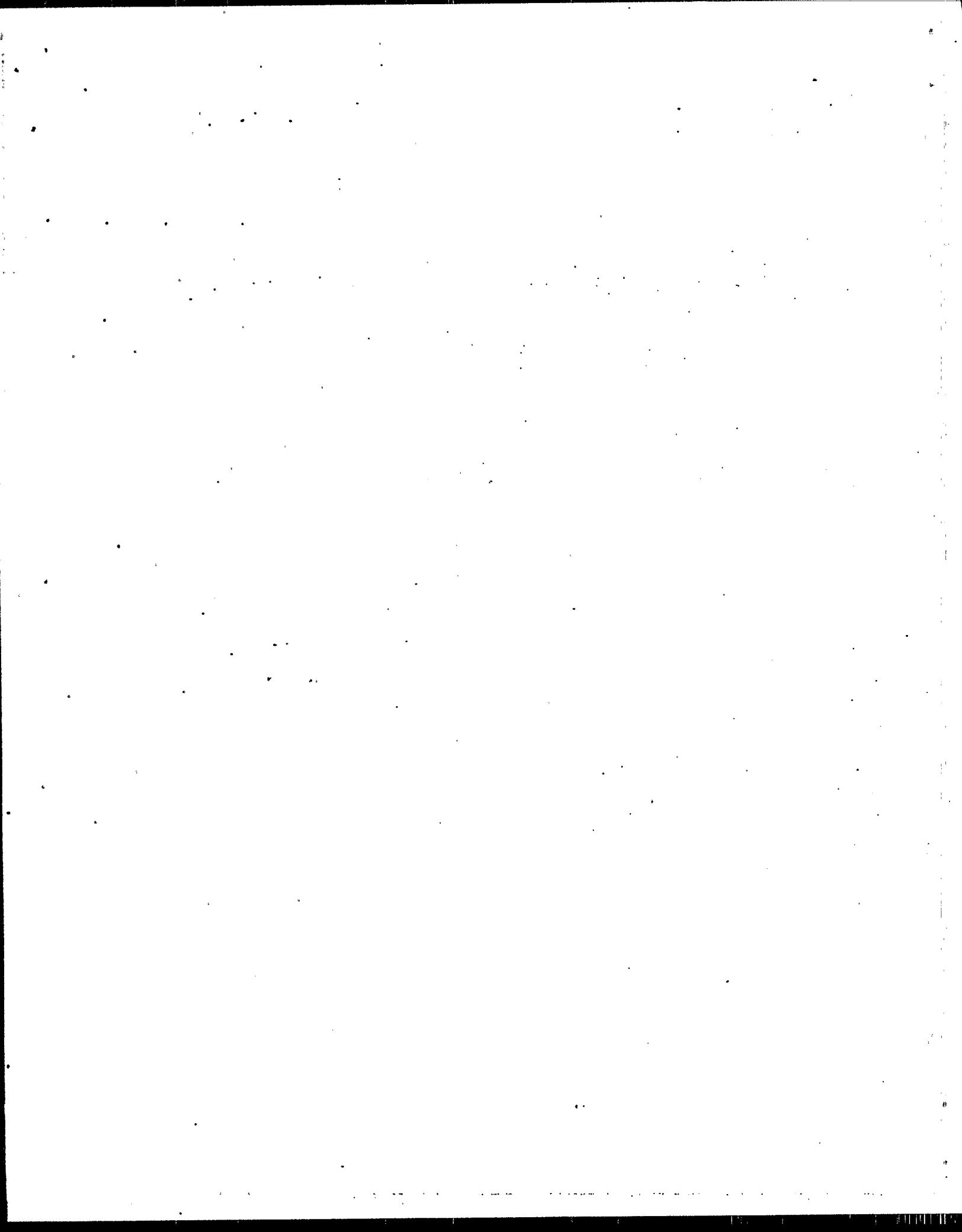


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## 5. SAMPLING AND ANALYSIS PROCEDURES

The purpose of this section is to provide a brief discussion of the EPA reference methods and/or generally accepted methods of sampling and analysis used to gather emissions data on air toxics emitted from sewage sludge incinerators. Different sampling and analytical methods than the ones described may have been used previously. Slight modifications of the methods may be specified by some State agencies to make results consistent with their regulatory compliance results. However, these sampling methods are widely used and accepted and should yield results comparable with data from other facilities.

This section presents a general description of the sampling and analytical methods for the determination of particulate, metals, CDD/CDF and other semivolatile organics, volatile organics and particle size air emissions from sewage sludge incinerators. EPA reference methods are described when available. Otherwise, the state-of-the-art draft methods are described.

### 5.1 PARTICULATE DETERMINATION BY EPA METHOD 5

The particulate mass is defined as any material which condenses at or above the filtration temperature of  $248 \pm 25^{\circ}\text{F}$  after removal of uncombined water. The Method 5 sampling train is shown in Figure 5-1. The particulate matter is withdrawn isokinetically and collected on the glass fiber filter.

The particulate sample is recovered by rinsing the glass probe liner and front half of the glass filter holder with acetone. The acetone rinses are evaporated and desiccated along with the filter. Both fractions are weighed to a constant weight. The final weight is adjusted for an acetone blank.<sup>1</sup>

### 5.2 METALS DETERMINATION BY EPA/EMSL DRAFT PROTOCOL

Sampling for particulate matter and toxic metals is currently performed according to the EPA draft protocol entitled "Methodology for the Determination of Trace Metal Emissions in Exhaust Gases from Stationary

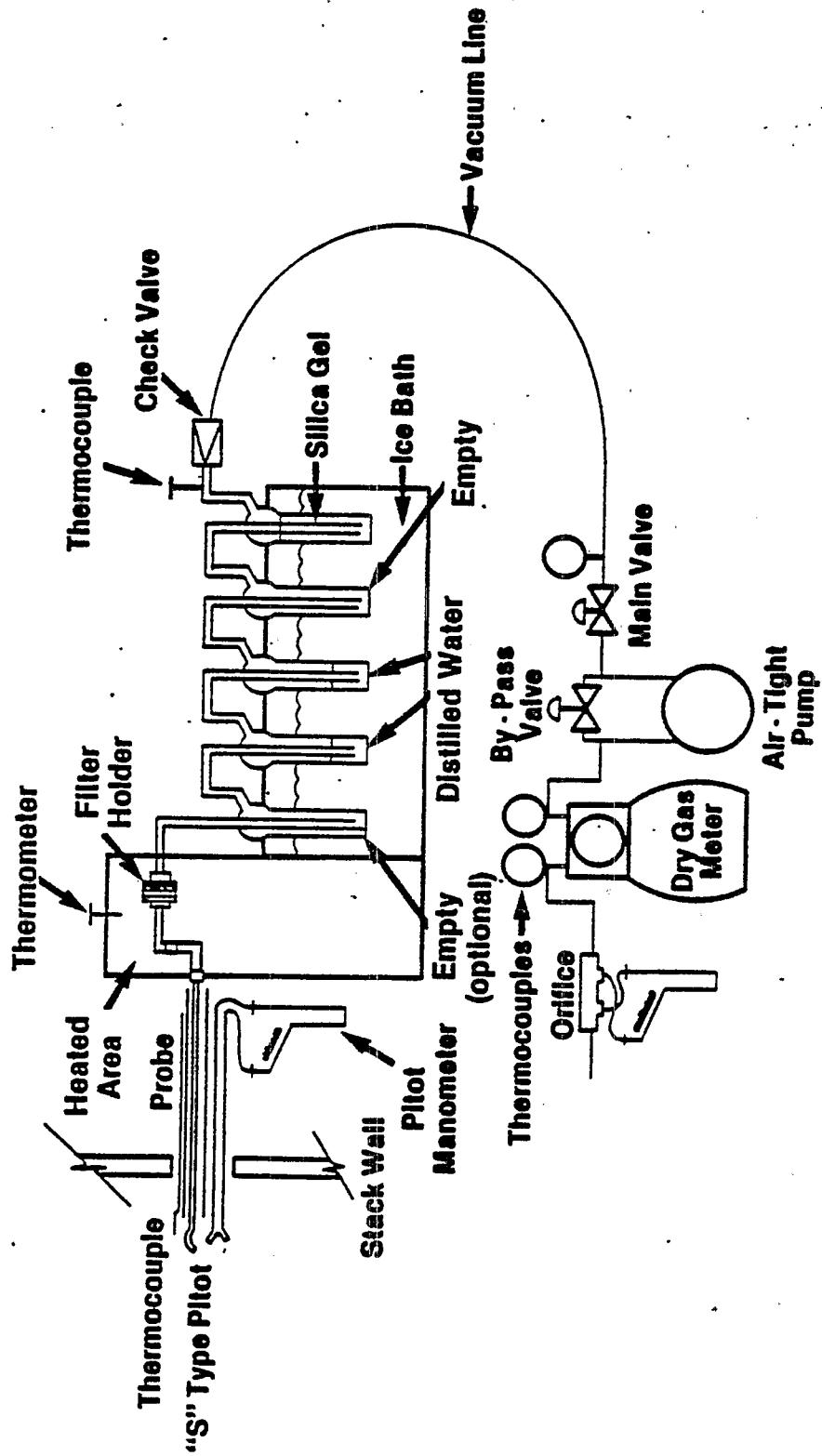


Figure 5-1. Particulate sampling train.

Source Combustion Processes."<sup>2</sup> This method is applicable for the determination of particulates and Pb, Zn P, Cr, Cu, Ni, Mn, Cd, Se, As, Hg, Be, Th, Ag, Sb, and Ba emissions from municipal waste incinerators, sewage sludge incinerators, and hazardous waste incinerators. The metals sampling train is shown in Figure 5-2.

Earlier sampling efforts may have employed EPA Method 12 which is specifically designed for lead. With Method 12, the flue gas passed through nitric acid only impingers which were than analyzed for the desired metals in addition to lead. However, some metals such as nickel and mercury, where found to be insufficiently collected in some cases.

The EPA draft method is based on Method 5 except for the following:

- The glassware is cleaned prior to sampling with an 8 hour soak in 10 percent (v/v) nitric acid solution.
- The impingers contain:
  - first impinger - empty
  - second impinger -  $\text{HNO}_3/\text{H}_2\text{O}_2$
  - third impinger -  $\text{HNO}_3/\text{H}_2\text{O}_2$
  - fourth impinger - acidic  $\text{KMnO}_4$

The sampling train is recovered and the samples are analyzed according to the scheme shown in Figure 5-3. The first, second and third impingers are analyzed for all metals. The fourth impinger is analyzed only for mercury which is typically not collected efficiently in the  $\text{HNO}_3/\text{H}_2\text{O}_2$  impingers.

The digested samples are analyzed by inductively coupled argon plasma (ICAP) spectroscopy for all metals except mercury. If arsenic or lead levels are less than 2 ppm, graphite furnace atomic absorption spectroscopy (AAS) is used. For mercury analysis, cold vapor AAS is used.

### 5.3 CDD/CDF AND PCB/PAH/CB/CP DETERMINATION BY THE DRAFT ASME/EPA METHOD

The state-of-the-art development for organics sampling is to collect CDD/CDF, polychlorinated biphenyls (PCB), polynuclear aromatic hydrocarbons (PAH), chlorobenzenes (CB), and chlorophenols (CP) in a single sampling train and to separate the fractions during analysis.<sup>3,4</sup> Previous sampling methods collected the CDD/CDF and PCB, PAH, CB and CP in separate trains

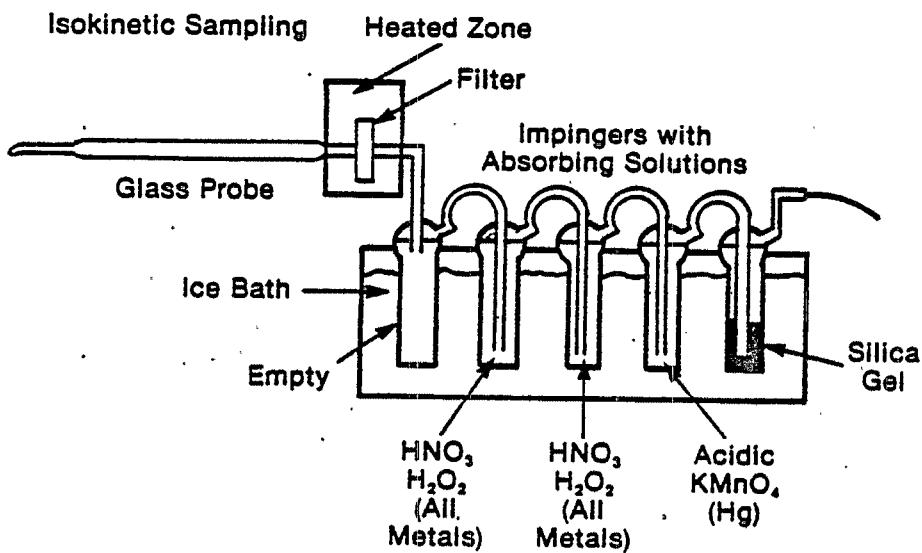


Figure 5-2. EMSL metals sampling train configuration.

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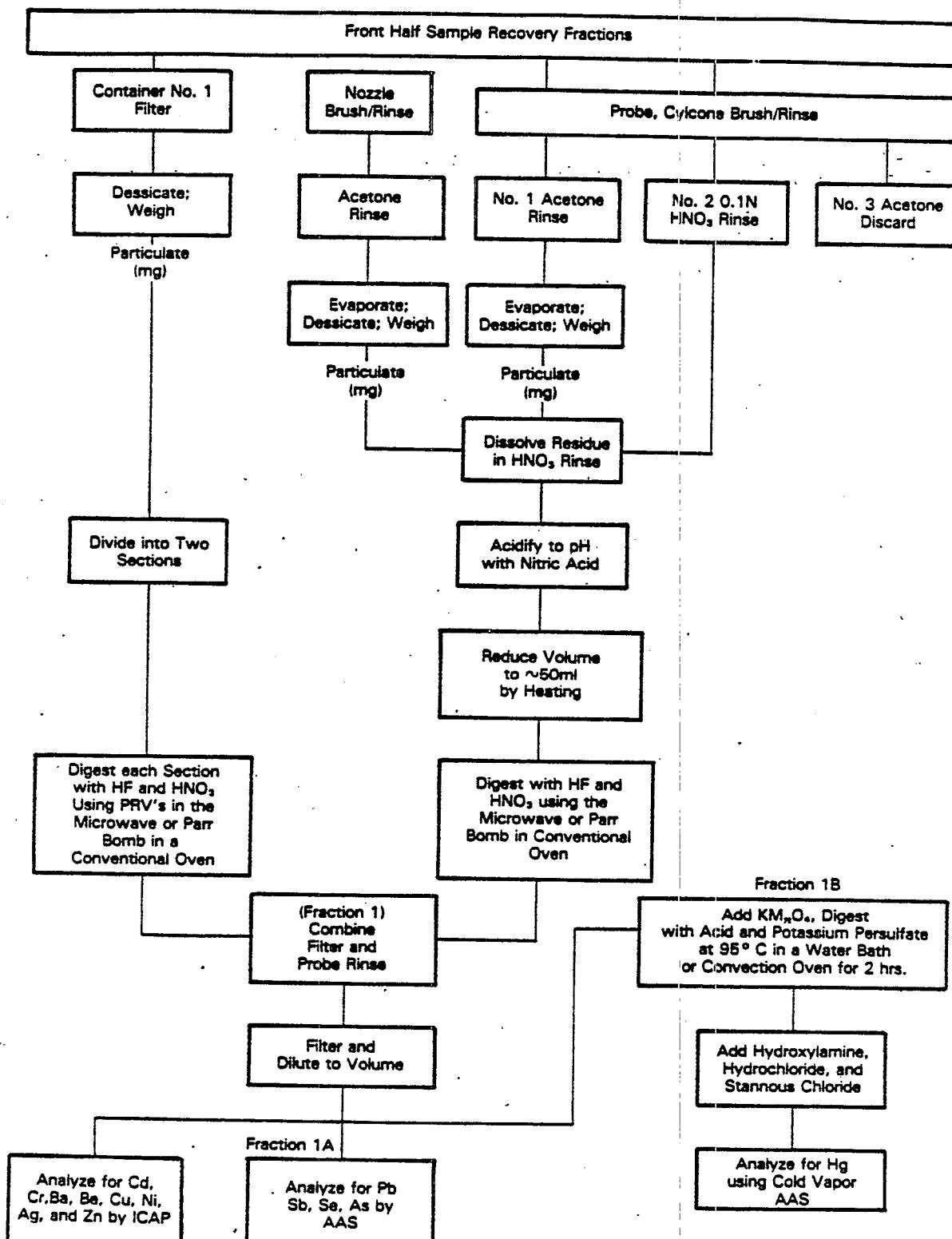


Figure 5-3. Digestion and analysis scheme for EMSL trace metal train components - front half.

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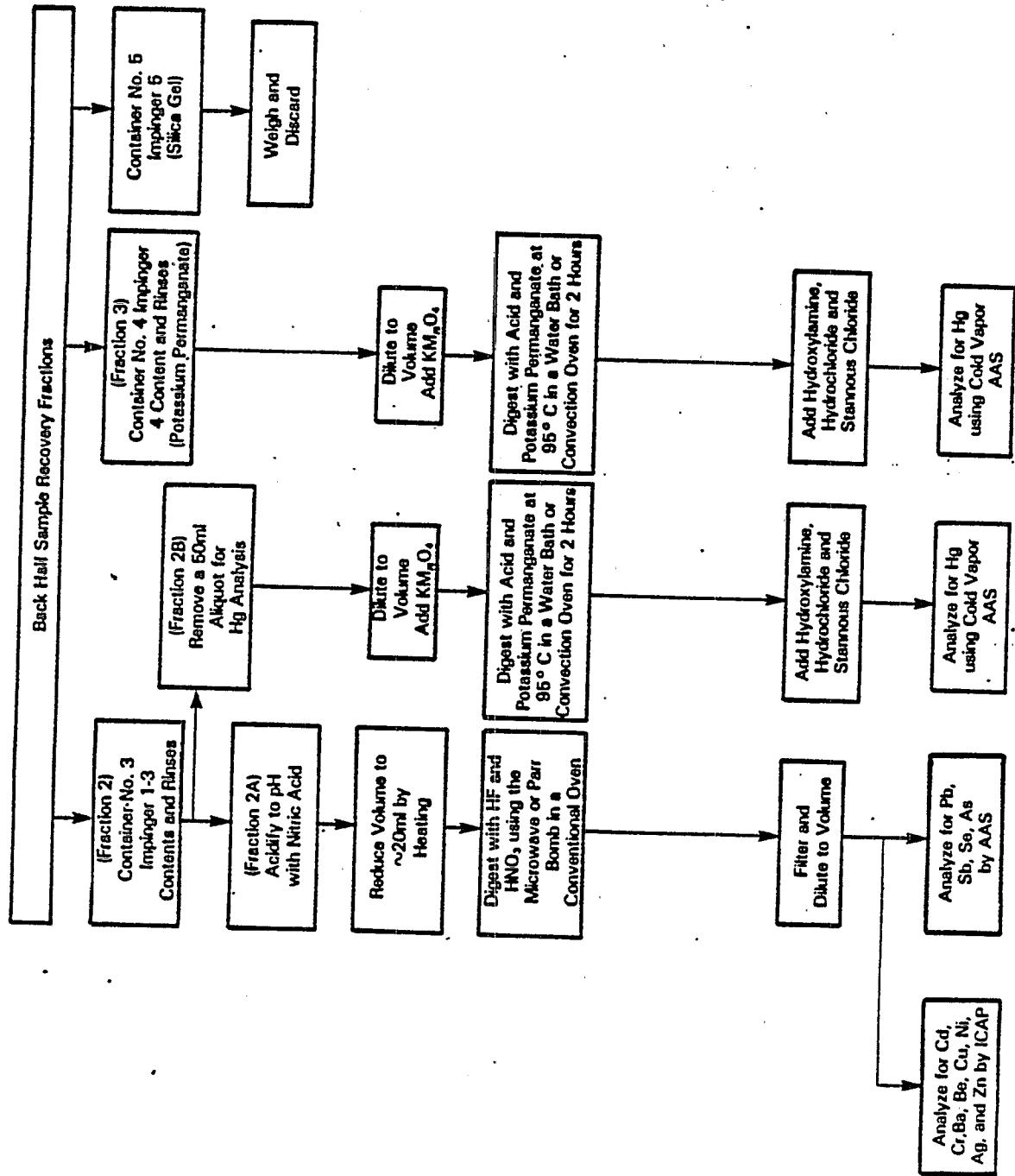


Figure 5-3. (Continued)

Digestion and analysis scheme for EMSL trace metal train components - back half.

that were essentially identical. Since December 1984 when the draft ASME/EPA method was prepared, many modifications have been incorporated, not all of which can be discussed in this brief section.

The sampling train is based on Method 5, but as shown in Figure 5-4, includes a condenser and XAD resin trap after the filter and before the impingers. The sampling train glassware, XAD resin, and filters are cleaned by baking, and rinsing with acetone and toluene prior to sampling. After sampling, the sampling train is recovered with acetone followed by methylene chloride and toluene rinses. The solvents should be of the highest grade available to prevent the introduction of chemical impurities which can interfere with the quantitative analytical determinations.

The state-of-the-art extraction scheme is shown in Figure 5-5. The extracted samples are analyzed by gas chromatography and mass spectroscopy (GC/MS). The typical organics available are summarized in Tables 5-1 and 5-2.

#### 5.4 VOLATILE ORGANIC SAMPLING TRAIN (VOST) METHOD

Sampling for volatile organic compounds (VOC) is conducted according to SW-846, Method 0030. The sorbent cartridges are analyzed according to SW-846, Method 5040. Specific compounds of interest, which typically vary depending on the test program, are listed in Table 5-3. A brief flow diagram of the VOST analysis is shown in Figure 5-6.<sup>5</sup>

The VOST is designed to collect volatile organic compounds with boiling points between 30°C and 100°C and has a flue gas detection limit of about 0.1 ug/m<sup>3</sup> for most compounds. A schematic diagram of the VOST is shown in Figure 5-7. The flue gas is sampled from the stack through a glass probe with a glass wool plug. The probe temperature is maintained above 300°F. The gas sample is then cooled to 68°F by a water-cooled condenser and passes through a pair of resin traps in series, a silica gel drying tube, a rotameter, a sampling pump, and a dry gas meter. The first resin trap contains Tenax and the second trap contains Tenax followed by petroleum-based charcoal.

A VOST run consists of collecting four pairs of traps, with each pair used for 20 minutes at a sample flow rate of 1 liter per minute. The

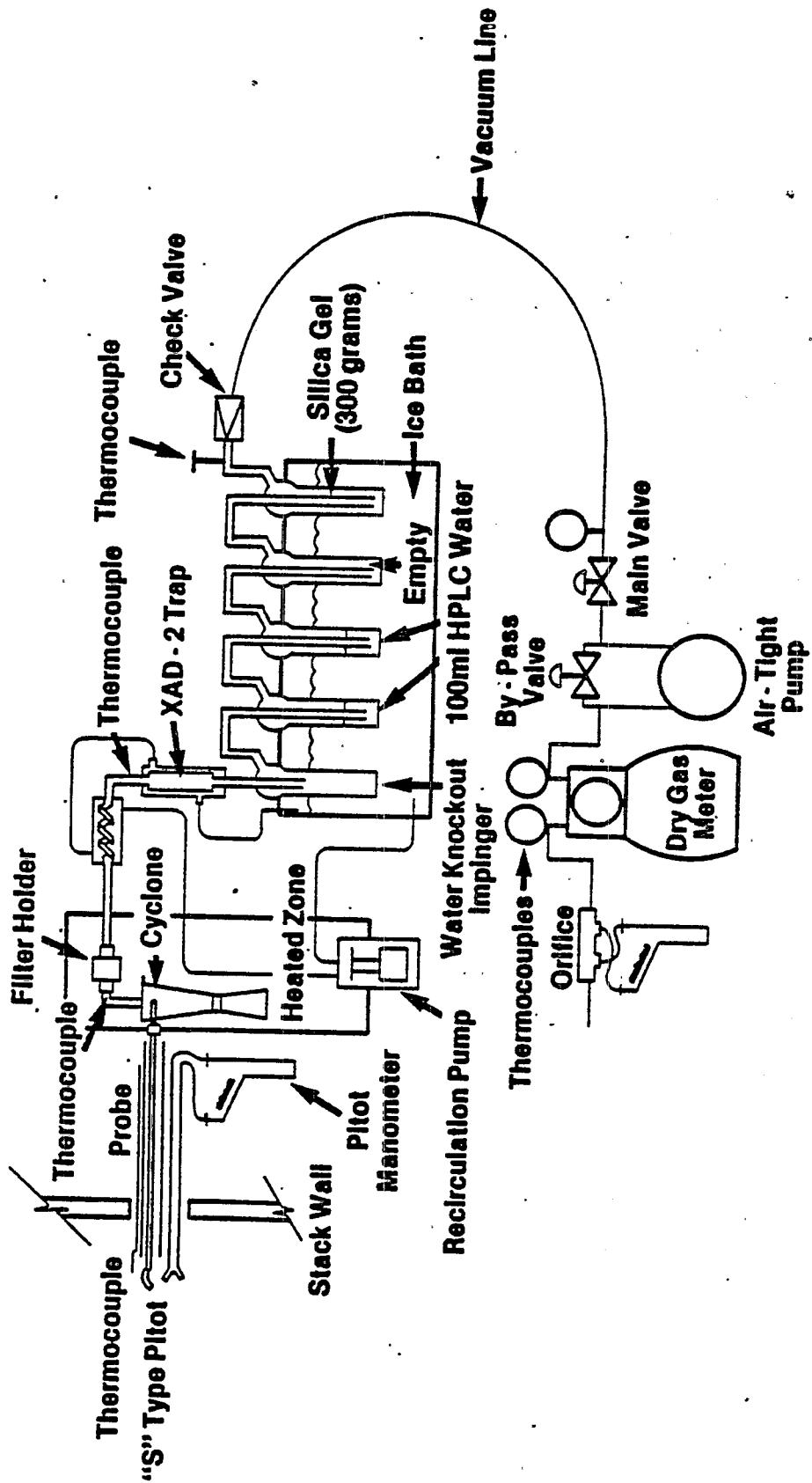


Figure 5-4. CDD/CDF/CB/CP/PCB/PAH sampling train configuration.

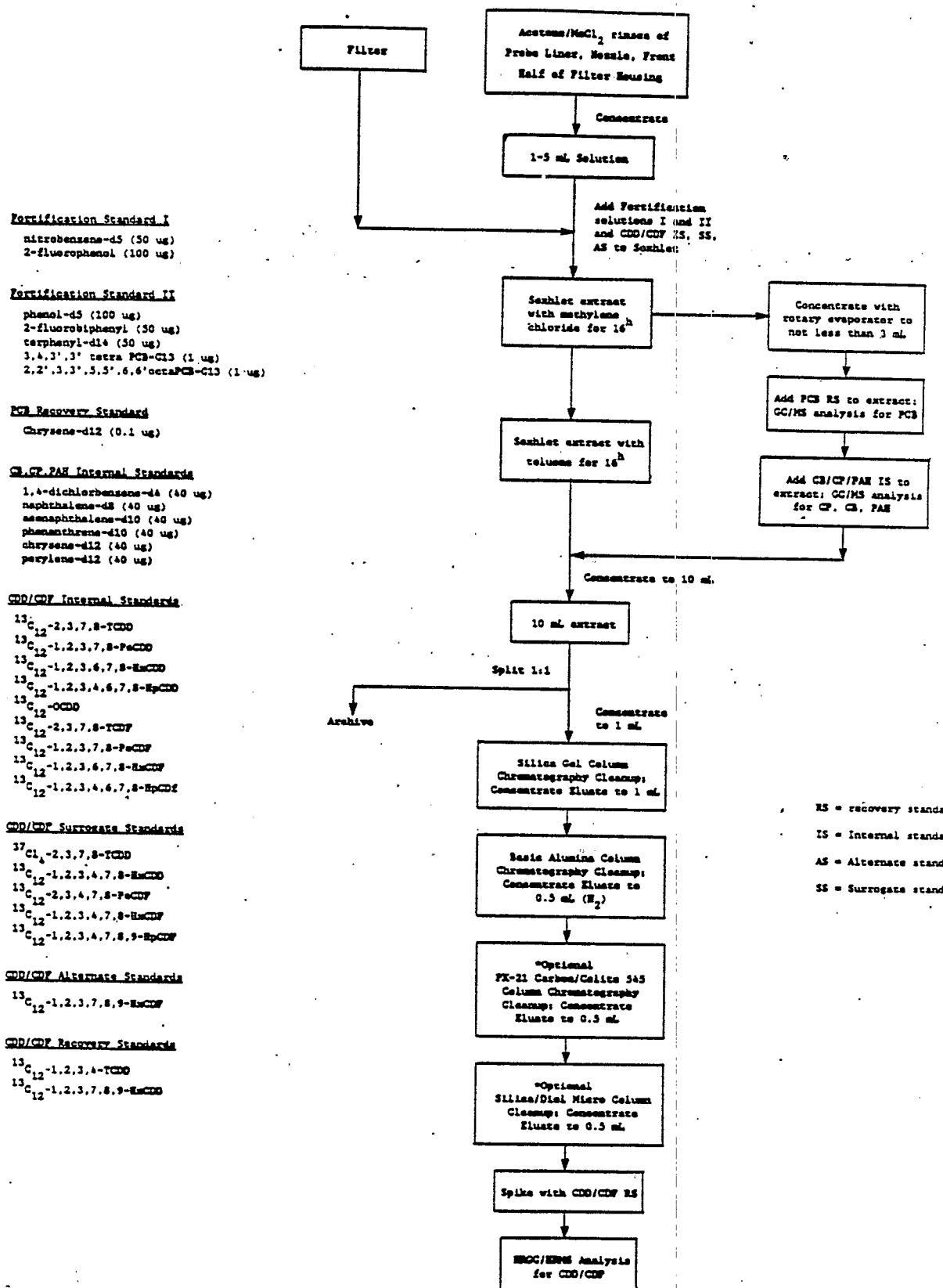


Figure 5-5. Extraction and analysis schematic for CDD/CDF/CB/CP/PCB/PAH flue gas samples.

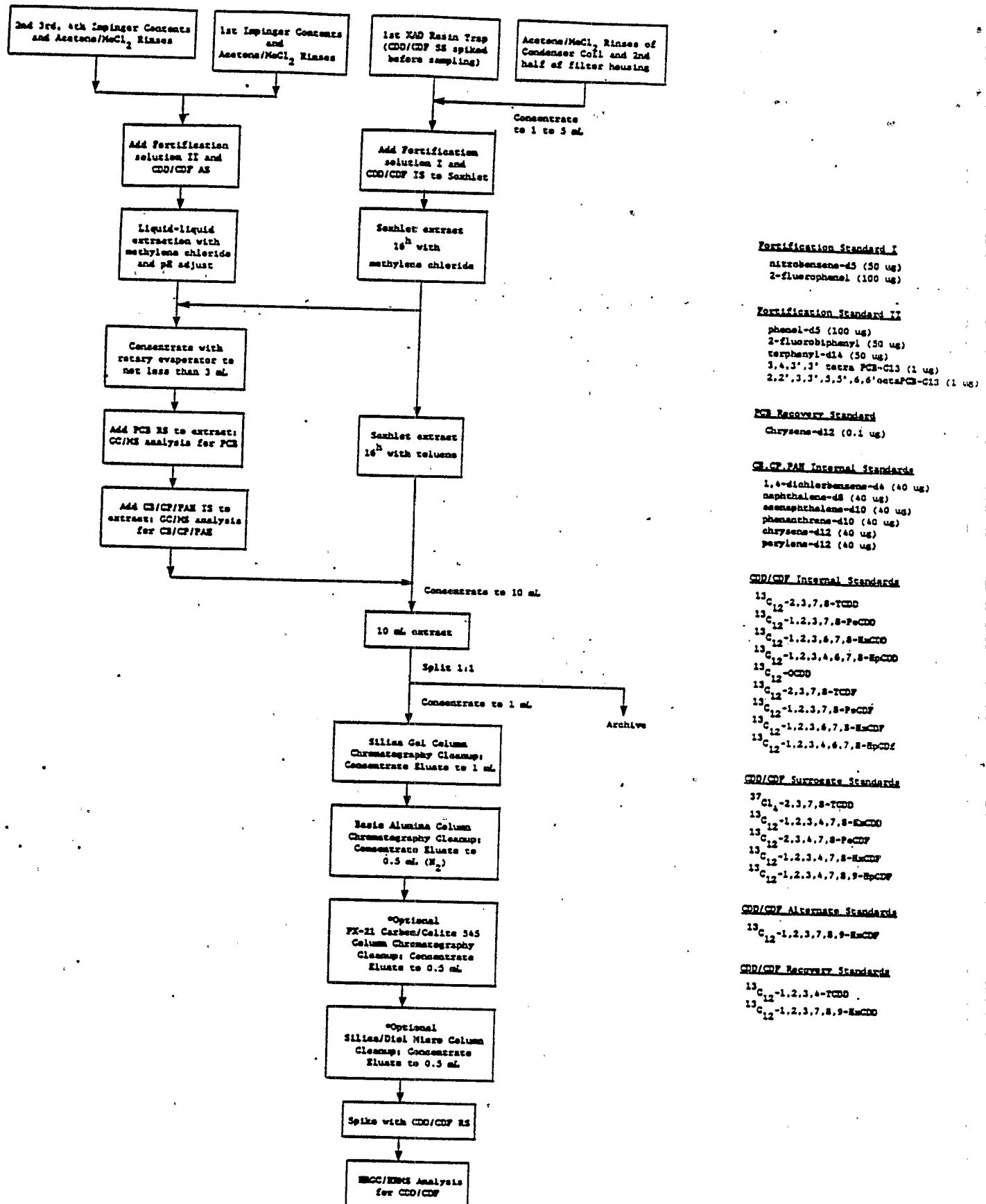


Figure 5-5. (Continued)

TABLE 5-1. TYPICAL CDD/CDF TARGET CONGENERS

---

DIOXINS

Total trichlorinated dibenzo-p-dioxins (TrCDD)  
2,3,7,8 tetrachlorodibenzo-p-dioxin (2,3,7,8 TCDD)  
Total tetrachlorinated dibenzo-p-dioxins (TCDD)  
1,2,3,7,8 pentachlorodibenzo-p-dioxin (1,2,3,7,8 PeCDD)  
Total pentachlorinated dibenzo-p-dioxins (PeCDD)  
1,2,3,4,7,8 hexachlorodibenzo-p-dioxin (1,2,3,4,7,8 HxCDD)  
1,2,3,6,7,8 hexachlorodibenzo-p-dioxin (1,2,3,6,7,8 HxCDD)  
1,2,3,7,8,9 hexachlorodibenzo-p-dioxin (1,2,3,7,8,9 HxCDD)  
Total hexachlorinated dibenzo-p-dioxins (HxCDD)  
1,2,3,4,6,7,8 heptachlorodibenzo-p-dioxin (1,2,3,4,6,7,8 HpCDD)  
Total heptachlorinated dibenzo-p-dioxins (HpCDD)  
Total octachlorinated dibenzo-p-dioxins (OCDD)

---

FURANS

Total trichlorinated dibenzofurans (TrCDF)  
2,3,7,8 tetrachlorodibenzofurans (2,3,7,8 TCDF)  
Total tetrachlorinated dibenzofurans (TCDF)  
1,2,3,7,8 pentachlorodibenzofuran (1,2,3,7,8 PeCDF)  
2,3,4,7,8 pentachlorodibenzofuran (2,3,4,7,8 PeCDF)  
Total pentachlorinated dibenzofurans (PeCDF)  
1,2,3,4,7,8 hexachlorodibenzofuran (1,2,3,4,7,8 HxCDF)  
1,2,3,6,7,8 hexachlorodibenzofuran (1,2,3,6,7,8 HxCDF)  
2,3,4,6,7,8 hexachlorodibenzofuran (2,3,4,6,7,8 HxCDF)  
1,2,3,7,8,9 hexachlorodibenzofuran (1,2,3,7,8,9 HxCDF)  
Total hexachlorinated dibenzofurans (HxCDF)  
1,2,3,4,6,7,8 heptachlorodibenzofuran (1,2,3,4,6,7,8 HpCDF)  
1,2,3,4,7,8,9 heptachlorodibenzofuran (1,2,3,4,7,8,9 HpCDF)  
Total heptachlorinated dibenzofurans (HpCDF)  
Total octachlorinated dibenzofurans (OCDF)

---

TABLE 5-2. TYPICAL CB, PCB, CP, AND PAH TARGET COMPOUNDS

Chlorobzenes

Total Dichlorobzenes  
 1,2-dichlorobenzene  
 1,3-dichlorobenzene  
 1,4-dichlorobenzene

Total Trichlorobzenes  
 1,2,4-trichlorobenzene  
 1,3,5-trichlorobenzene  
 1,2,3-trichlorobenzene

Total Tetrachlorobzenes  
 1,2,3,4-tetrachlorobenzene  
 1,2,3,5-tetrachlorobenzene  
 1,2,4,5-tetrachlorobenzene

Pentachlorobenzene

Hexachlorobenzene

Polychlorinated Biphenyls

Total Monochlorobiphenyls  
 2-chlorobiphenyl

Total Dichlorobiphenyls  
 2,3-dichlorobiphenyl

Total Trichlorobiphenyls  
 2,4,5-trichlorobiphenyl

Total Tetrachlorobiphenyls  
 2,2'4,6-tetrachlorobiphenyl

Total Pentachlorobiphenyls  
 2,2',3',4,5-pentachlorobiphenyl

Total Hexachlorobiphenyls  
 2,2'4,4,5,6'-hexachlorobiphenyl

Total Heptachlorobiphenyls  
 2,2'3,4,5',6,6-heptachlorobiphenyl

Total Octachlorobiphenyls  
 2,2',3,3',4,5',6,6'-octachloro-  
 biphenyl

Total nonachlorobiphenyls  
 2,2',3,3',4,4',5,6,6'-nonachloro-  
 biphenyl

Decachlorobiphenyl

Chlorophenols

2-chlorophenol  
 3-chlorophenol  
 4-chlorophenol

Total Dichlorophenols  
 2,3-dichlorophenol  
 2,4-dichlorophenol  
 2,5-dichlorophenol  
 2,6-dichlorophenol  
 3,4-dichlorophenol  
 3,5-dichlorophenol

Total Trichlorophenols  
 2,3,4-trichlorophenol  
 2,3,5-trichlorophenol  
 2,3,6-trichlorophenol  
 2,4,5-trichlorophenol  
 2,4,6-trichlorophenol

Total Tetrachlorophenols  
 2,3,4,6-tetrachlorophenol  
 2,3,5,6-tetrachlorophenol

(continued)

TABLE 5-2. (Continued)

Chlorophenols, (continued)

Pentachlorophenol  
4-chloro-3-methylphenol

Polynuclear Aromatic Hydrocarbons

1,4-Dichlorobenzene-d4  
Naphthalene-d8  
Acenaphthene-d10  
Acenaphthylene  
Acenaphthene  
Fluorene  
Phenanthrene-d10  
Phenanthrene  
Anthracene  
Fluoranthene  
Chrysene-d12  
Pyrene  
Benzo(a)anthracene  
Chrysene  
Perylene-d12  
Benzo(b)fluoranthene  
Benzo(k)fluoranthene  
Benzo(a)pyrene  
Indeno(1,2,3-cd)pyrene  
Dibenz(a;h)anthracene  
Benzo(g,h,i)perylene  
Benzo(e)pyrene  
Perylene

TABLE 5-3. TYPICAL TARGET VOC

Acetaldehyde	trans-1,2-Dichloroethene
Acrolein	1,1-Dichloroethylene
Acrylonitrile	Dichlorofluoromethane
Benzene	1,2-Dichloropropane
Bromodichloromethane	cis-1,3-Dichloropropene
Carbon Tetrachloride	trans-1,3-Dichloropropene
Chlorobenzene	Epoxyethane (ethylene oxide)
Chloroethane	1,2-Epoxypropane (propylene oxide)
2-Chloroethylvinyl ether	Ethylbenzene
Chloroform	Methylene Chloride
Chloromethane	2-Nitropropane
2-Chlorophenol <sup>a</sup>	PAN (Peroxyacetyl nitrate)
3-Chlorophenol <sup>a</sup>	Tetrachloroethene
4-Chlorophenol <sup>a</sup>	Toluene
Chloropropane	1,1,1-Trichloroethane
2-Chloropropane	1,1,2-Trichloroethane
Dibromochloromethane	Trichloroethene
1,1-Dichloroethane	Trichlorofluoromethane
1,2-Dichloroethane	1,1,2-Trichloropropane
4,2-Dichloroethane	Vinyl Chloride
1,1-Dichloroethene	

<sup>a</sup>Measured in chlorophenol analysis.

## VOST ANALYSIS PROTOCOL

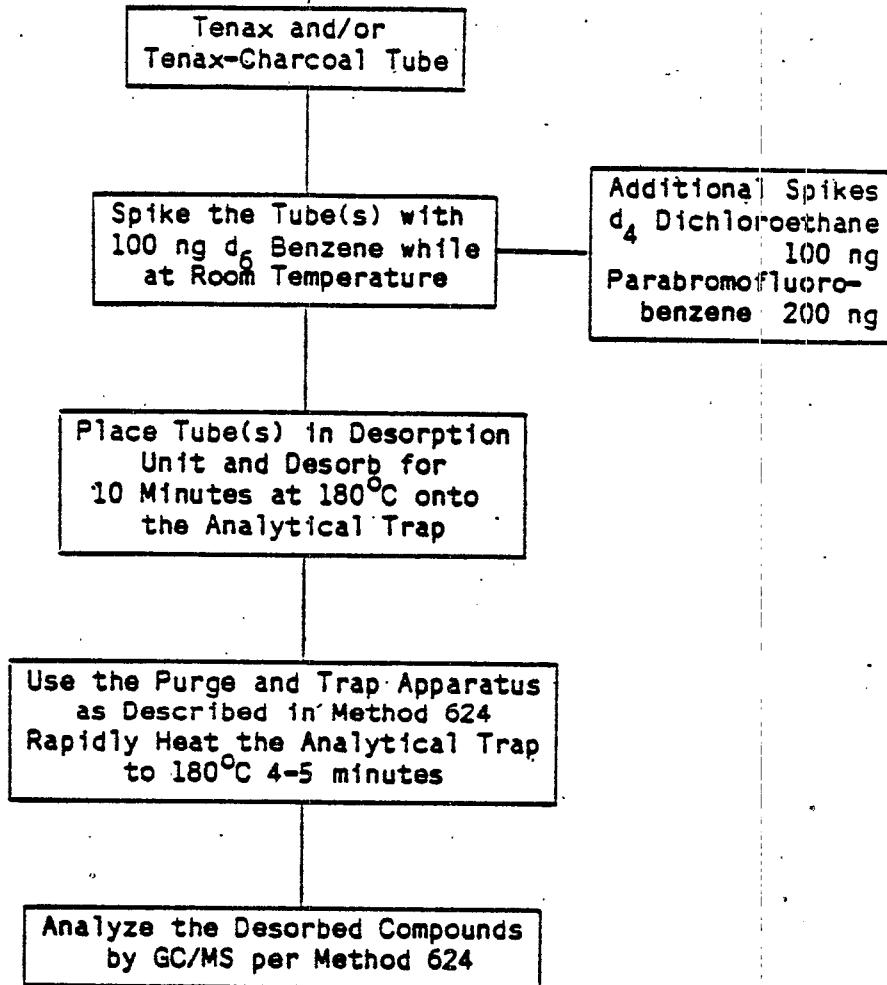


Figure 5-6. VOST analysis protocol.

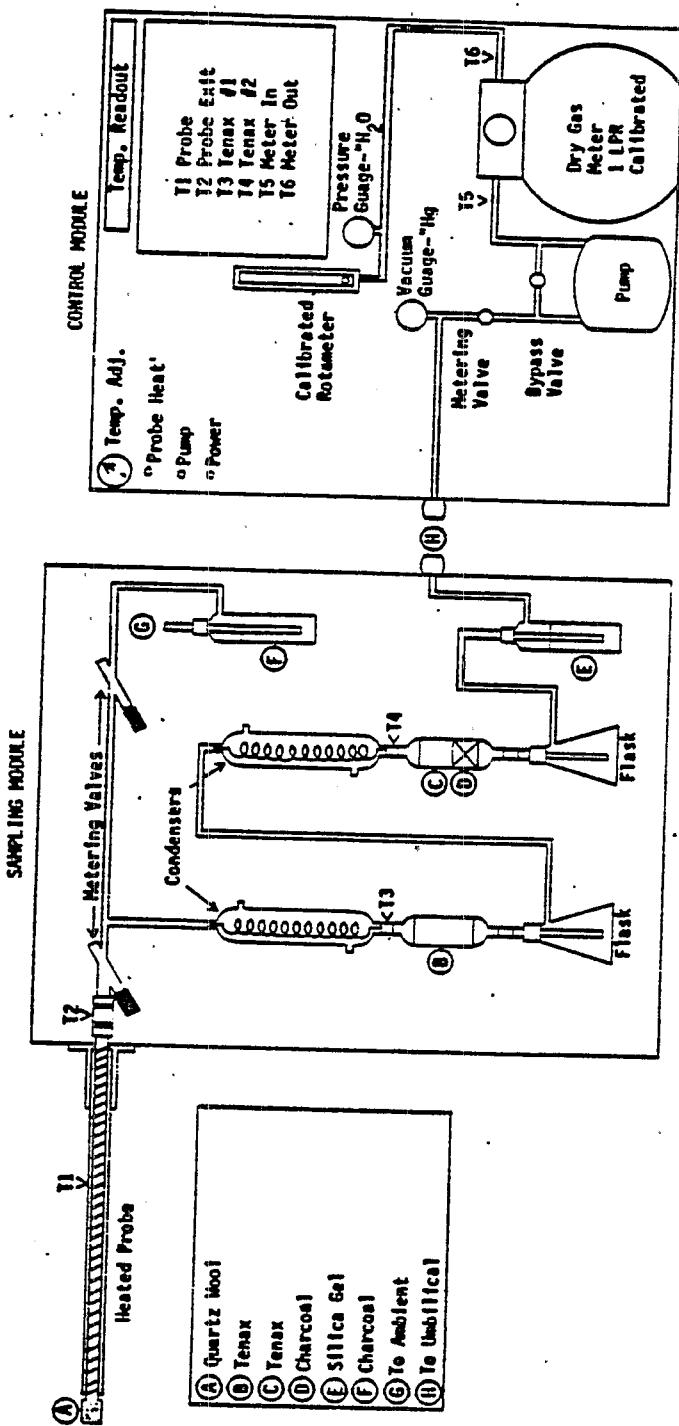


Figure 5-7. VOST sampling train configuration.

samples are collected at a fixed point representing average gas velocity. Since the target species are gaseous components of the flue gas, isokinetic sampling is not a consideration for this method.

#### 5.5 PARTICLE SIZE SEMIVOLATILE ORGANIC SOURCE ASSESSMENT SAMPLING SYSTEM (SASS)

Particulate matter and semivolatile organics are withdrawn at a constant rate near isokinetic conditions. Three heated stainless steel cyclones (10 um, 3 um and 1 um) and a final filter collect and separate the particulate matter. Since isokinetic sampling conditions are not guaranteed, this method is not used for compliance determinations.

A schematic of the sampling train is shown in Figure 5-8. After the cyclones and filter, the flue gas is cooled and organics are removed by a sorbent cartridge. Following the sorbent cartridge is a set of impingers which contain a nitric acid and peroxide mixture to condense moisture and remove metals. The analytical scheme for the train is presented in Figures 5-9, 5-10 and 5-11.<sup>6</sup>

#### 5.6 SLUDGE ANALYSES

Sludge samples are often analyzed for metals, moisture and volatile organics. The metals analyses are done according to SW-846, Method 3050 for digestion and Methods 6010, 7421 and 7060 for analysis. The analysis protocol is shown in Figure 5-12.

The volatile organic analysis follows SW-846, Method 8240. The analysis protocol is shown in Figure 5-13.

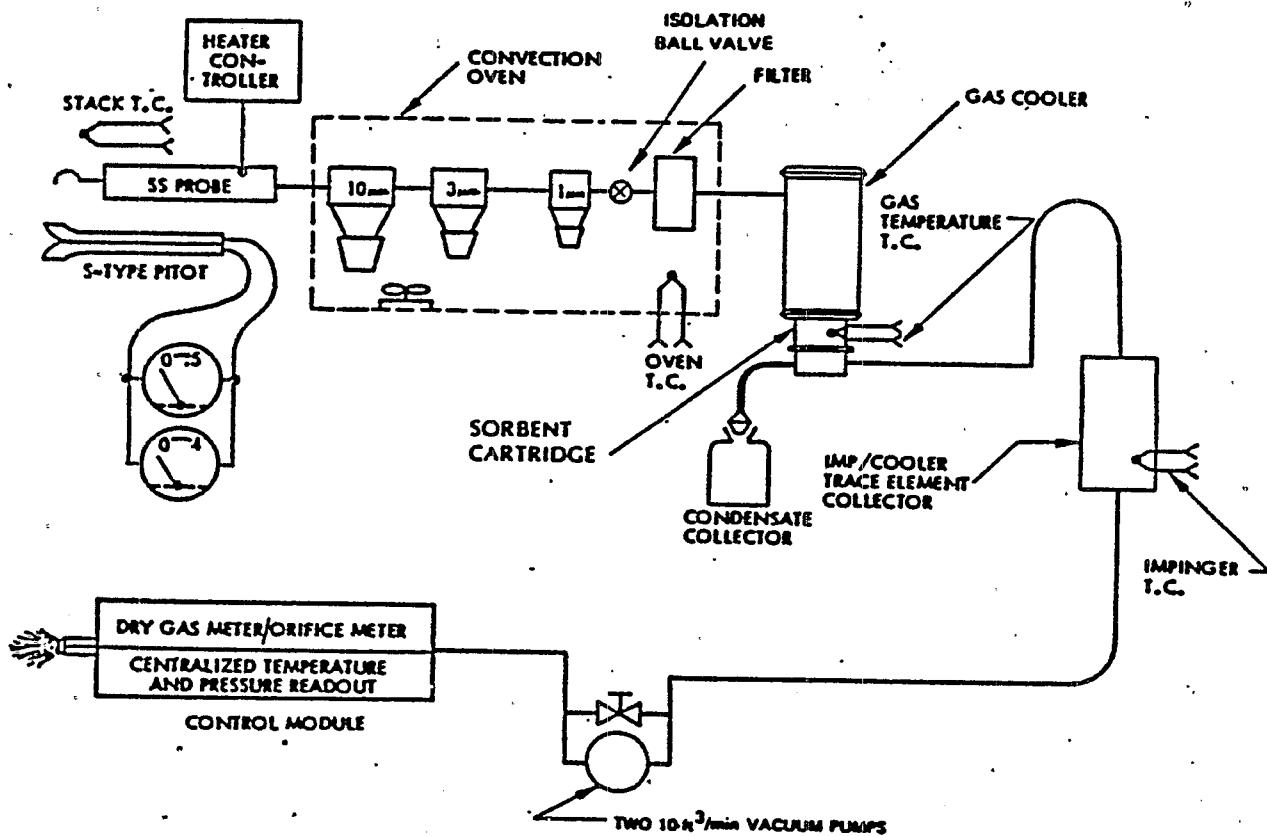
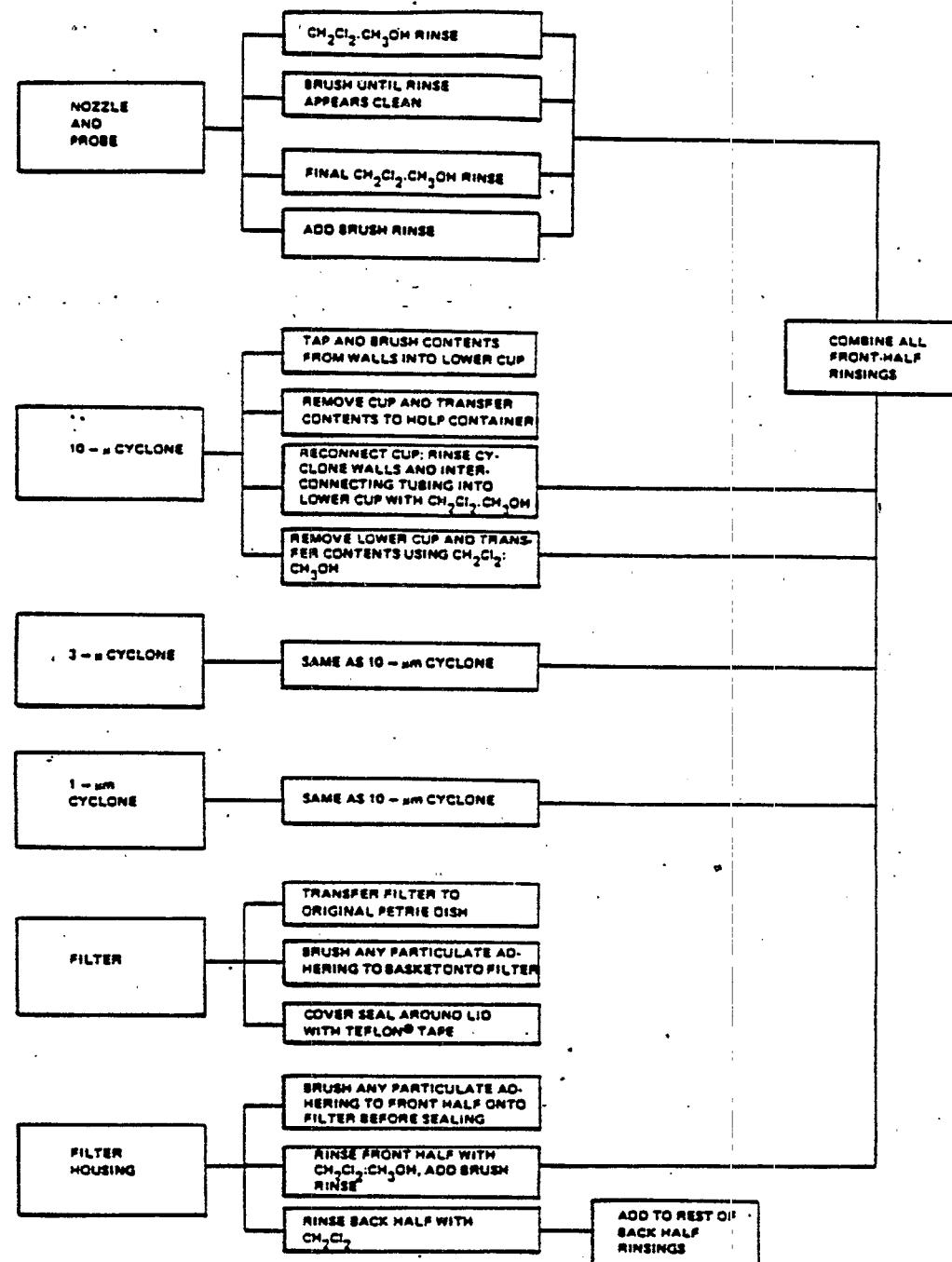


Figure 5-8. SASS sample diagram.

Source: IERL Procedures Manual: Level 1  
Environmental Assessment Second Edition, EPA-600/7-78-201



NOTES: ALL CH<sub>2</sub>Cl<sub>2</sub>:CH<sub>3</sub>OH MIXTURES ARE 50:50 V/V.  
 ALL CONTAINERS FOR SAMPLES FOR ORGANIC ANALYSIS MUST BE GLASS.  
 USE TEFLON® OR GLASS WASH BOTTLES; TEFLON® IS PREFERRED.

Figure 5-9. SASS sample handling and transfer: nozzle, probe, cyclones and filter.

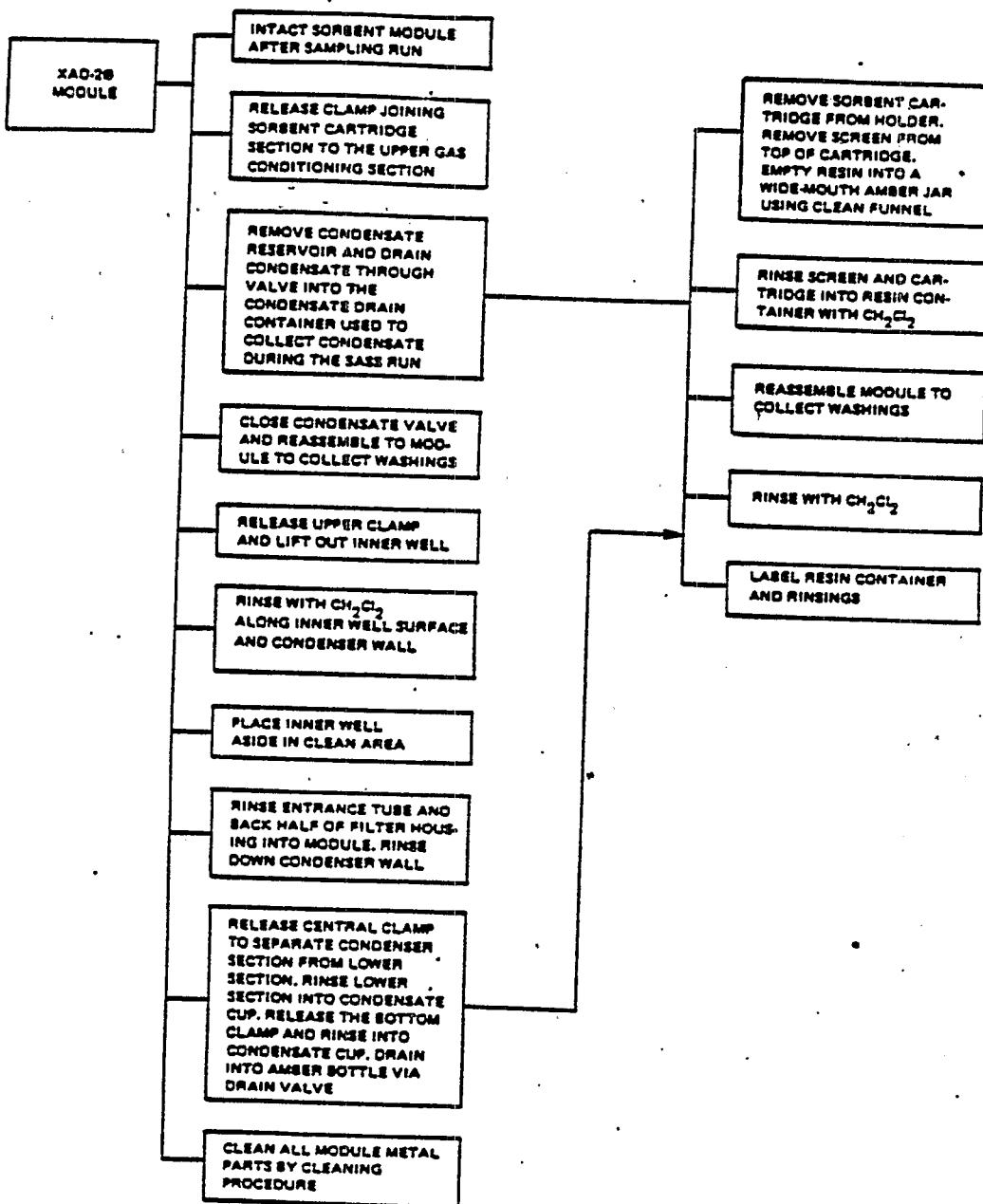
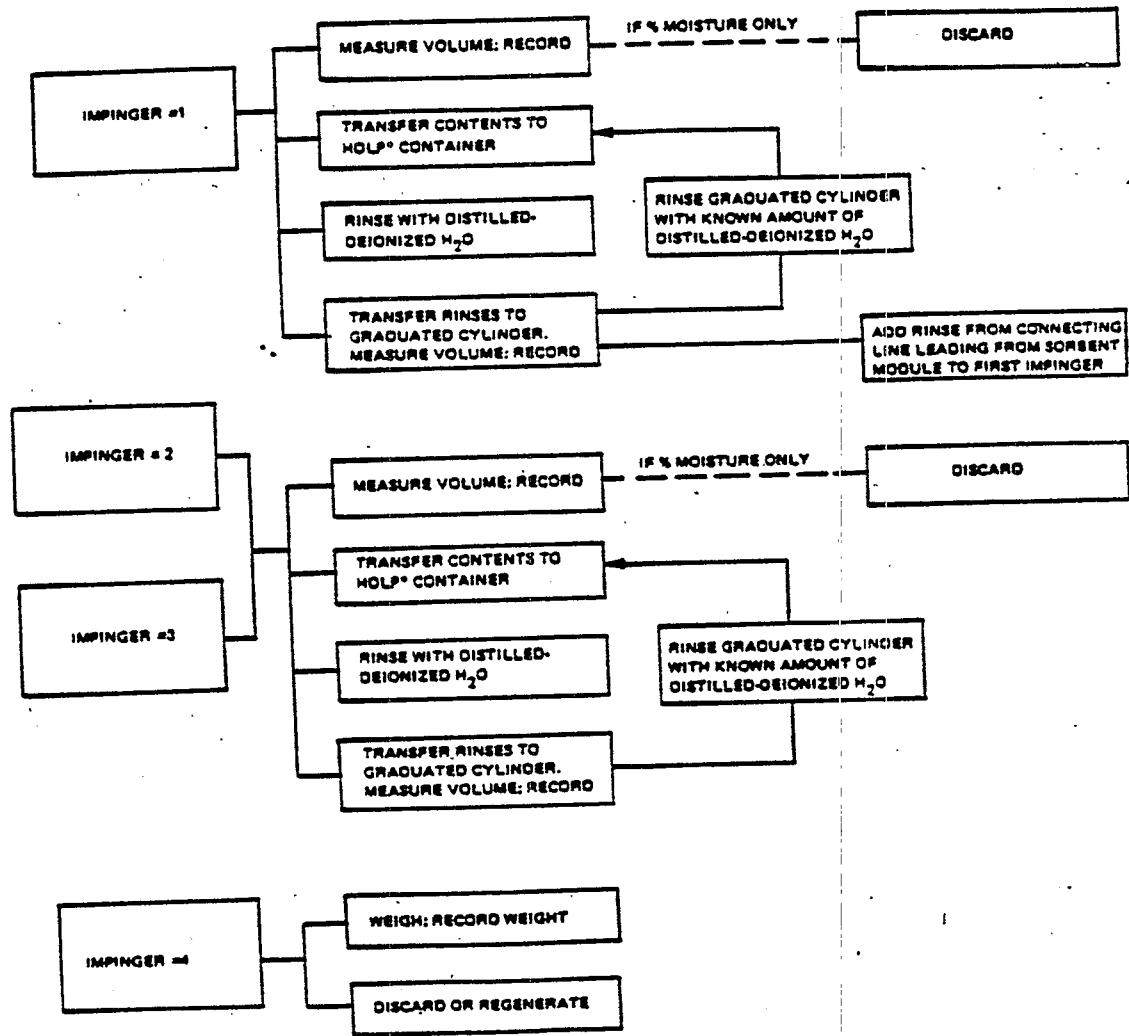


Figure 5-10. SASS sample handling and transfer: organic module section.



\*HDPE = HIGH-DENSITY LINEAR POLYETHYLENE.

Figure 5-11. SASS sample handling and transfer: impinger train.

## METALS IN SLUDGE ANALYSIS PROTOCOL

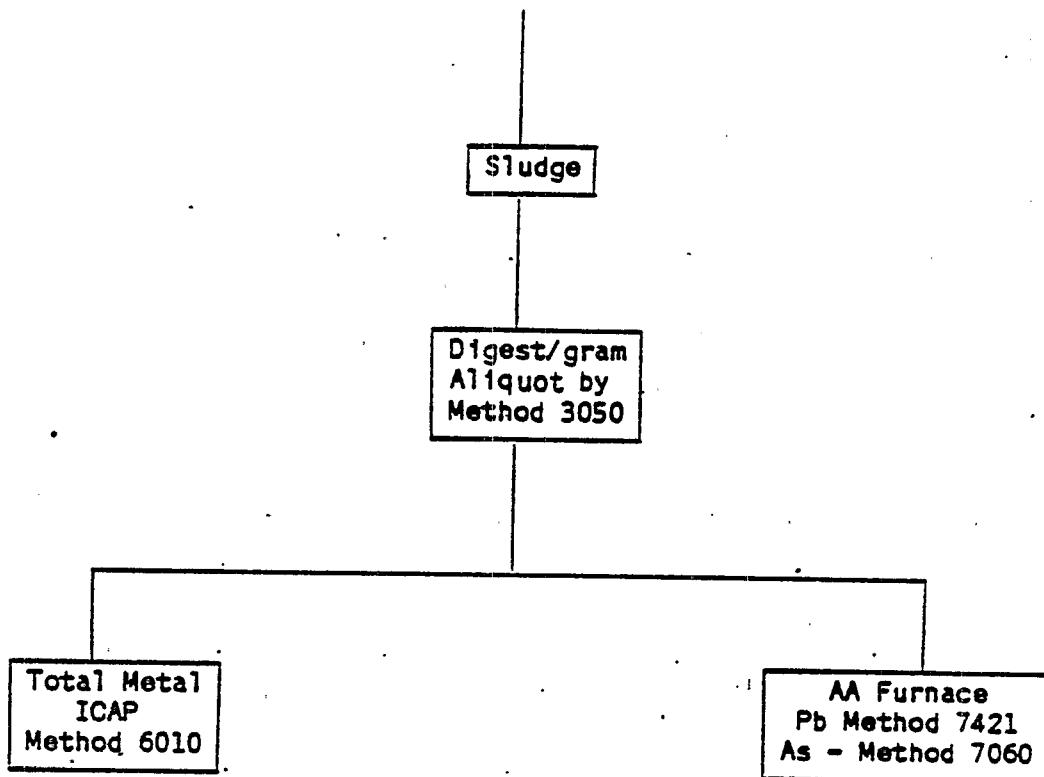


Figure 5-12. Analysis protocol for metals in sludge.

METHOD 8240 - VOLATILE ORGANICS

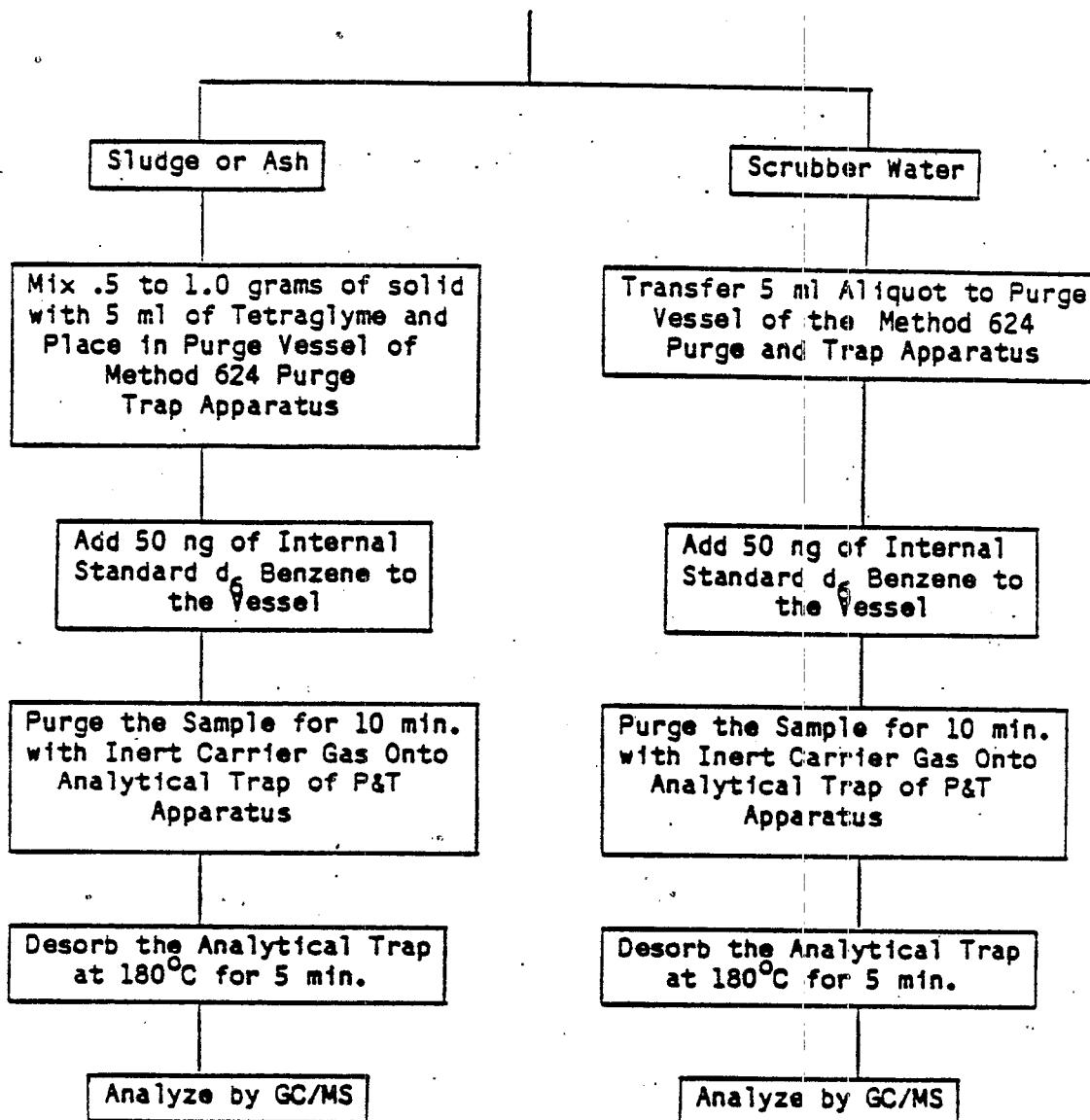
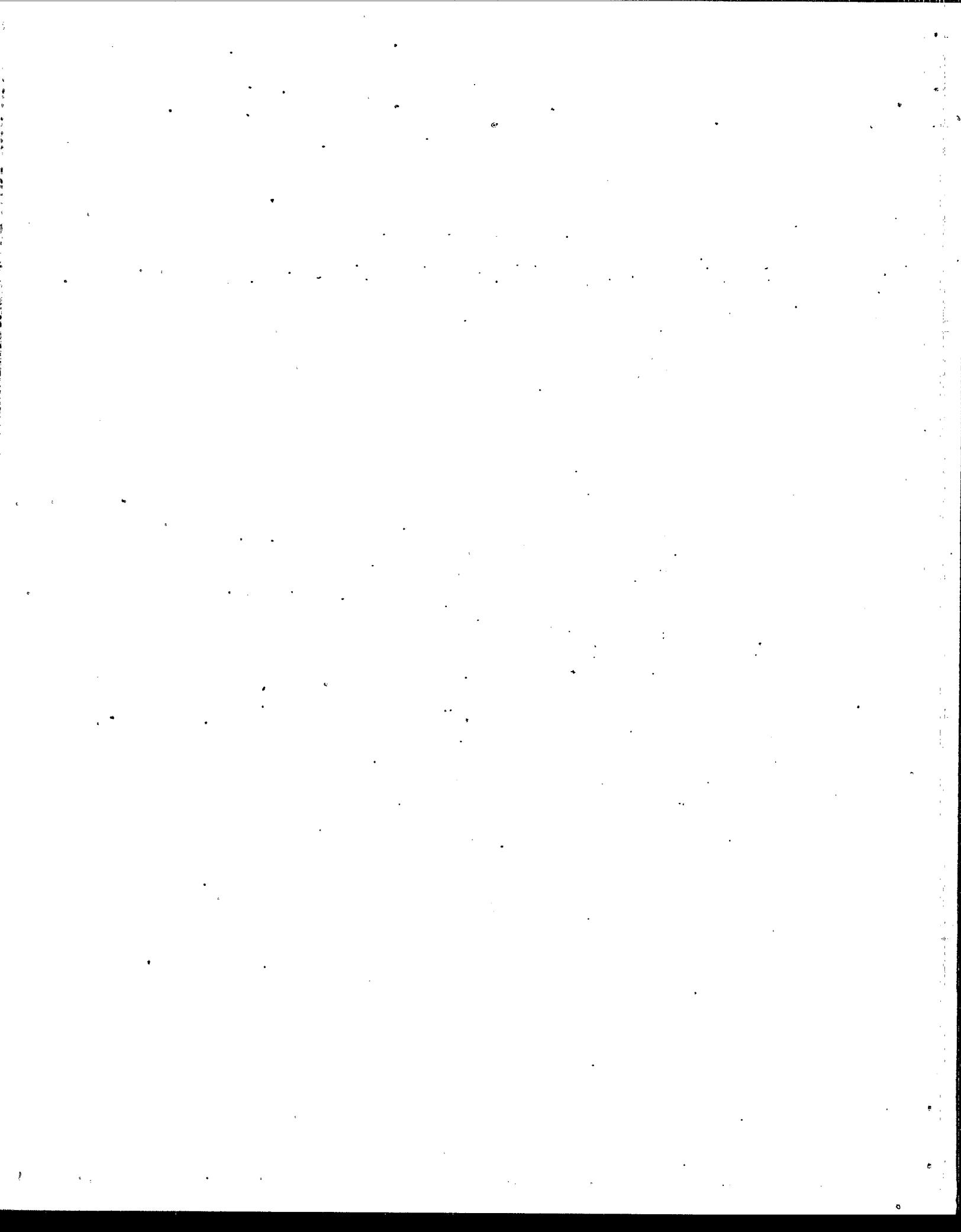
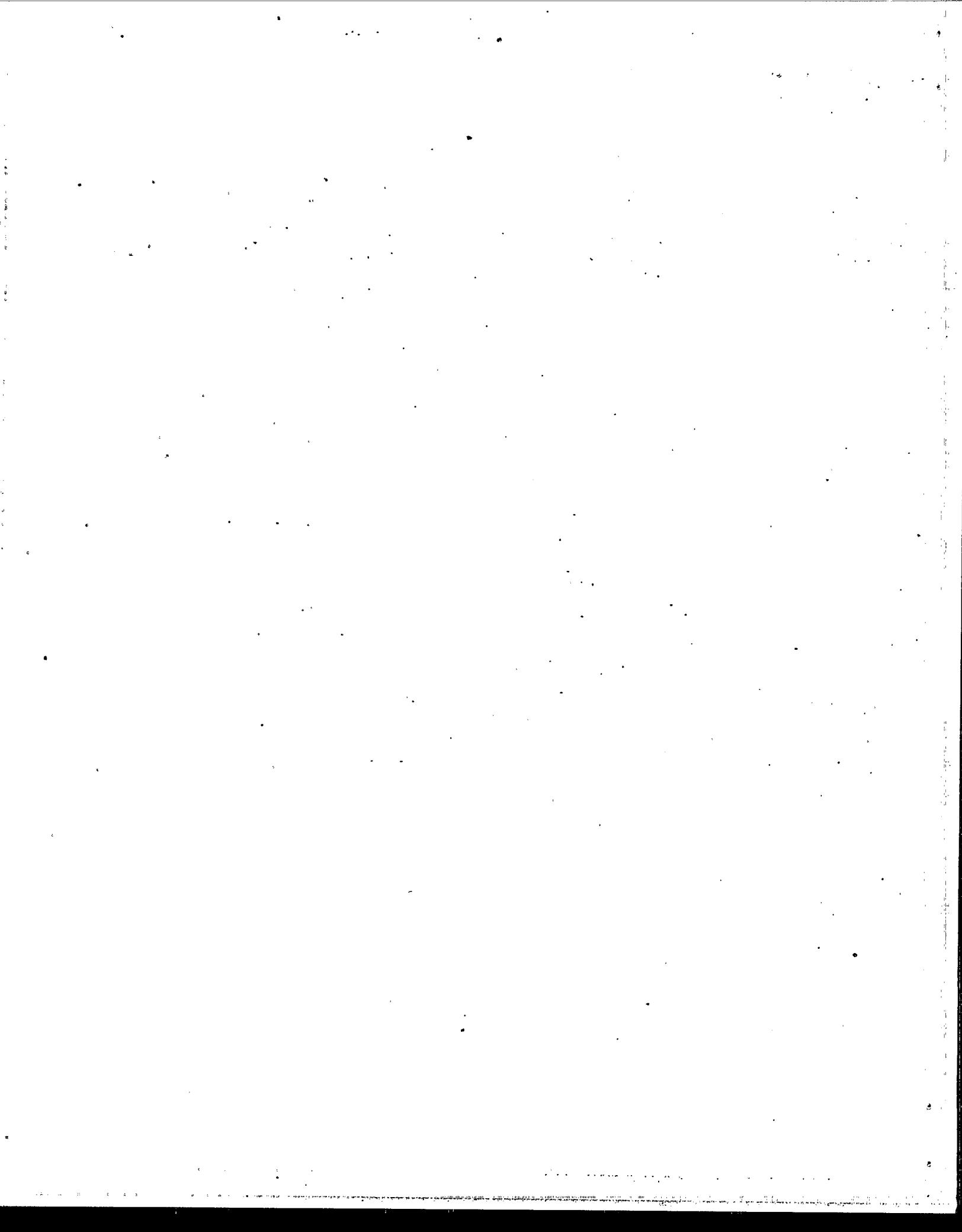


Figure 5-13. Analysis protocol for volatile organics in solids wastes.



## 5.6 REFERENCES

1. Method 5 - Determination of Particulate Emissions from Stationary Sources. 40 CFR Ch. 1, Part 60, Appendix A, Method 5. July 1, 1988.
2. Draft - Methodology for the Determination of Trace Metal Emissions in Exhaust Gases from Stationary Source Combustion Processes. U.S. Environmental Protection Agency. Research Triangle Park, N.C.
3. Sampling for the Determination of Chlorinated Organic Compounds in Stack Emissions - Draft. American Society of Mechanical Engineers and the U.S. Environmental Protection Agency. December 31, 1984.
4. Analytical Procedures to Assay Stack Effluent Samples and Residual Combustion Products for Polychlorinated PCDD and PCDF - Draft. American Society of Mechanical Engineers and the U.S. Environmental Protection Agency. December 31, 1984. Revised by Triangle Laboratories - February 1989.
5. Volatile Organic Sampling Train. SW-846, Method 0030. Revision 0. September 1986.
6. Modified Method 5 Train and Source Assessment Sampling System Operator's Manual. Schlichenrieder, Lynn M., et al. (Arthur D. Little, Inc.). U.S. Environmental Protection Agency. Research Triangle Park, North Carolina. February 1985.



**APPENDIX A**  
**U.S. SEWAGE SLUDGE INCINERATORS**

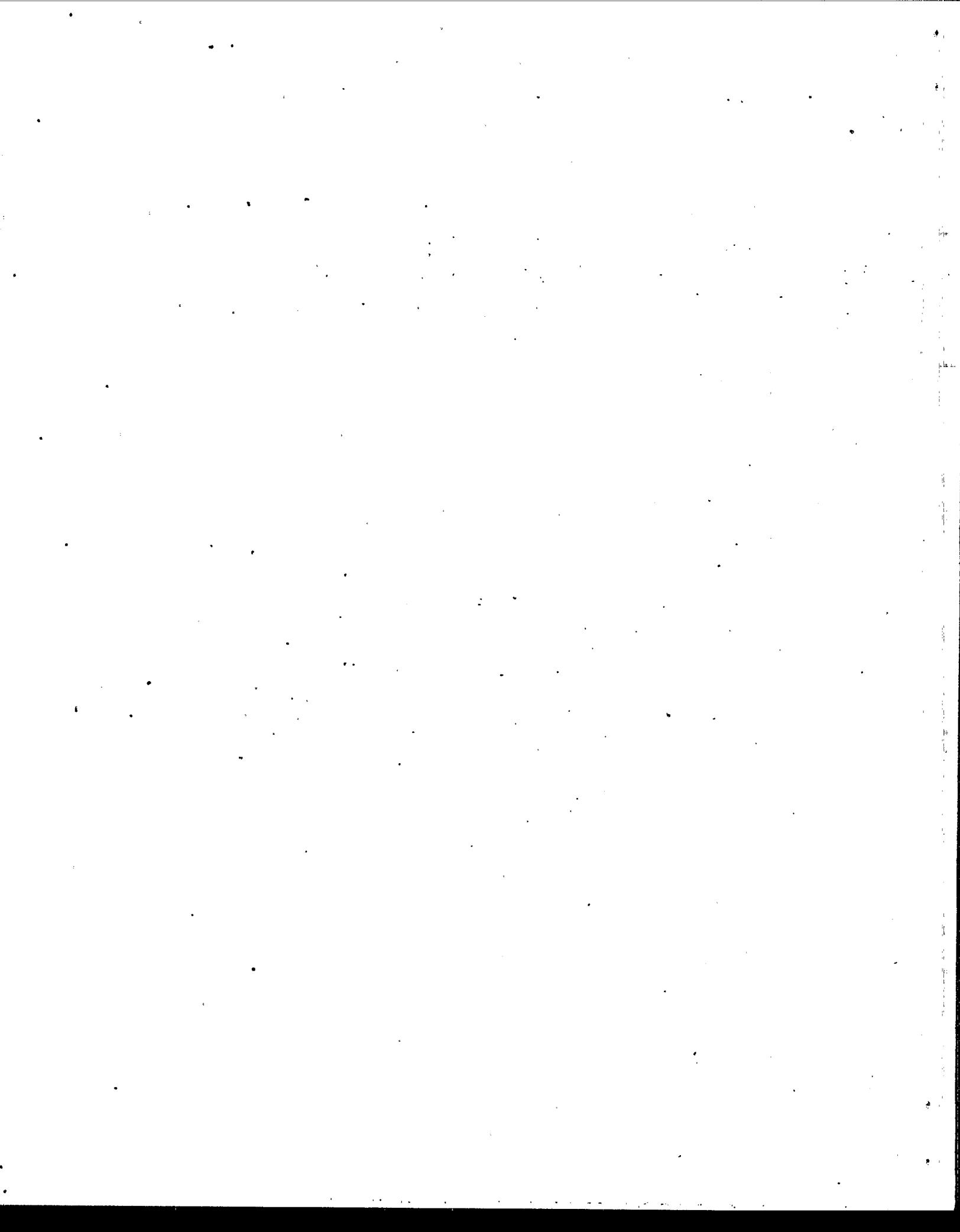


TABLE A-1. U.S. SEWAGE SLUDGE INCINERATORS SORTED BY STATE AND TYPE<sup>1</sup>

Facility	city	state	Type <sup>2</sup>	Number of units	Total capacity (dry tpd)	Unit capacity (dry tpd)	Start-up date	Control device(s)
Anchorage	AK	MH	1	1.1	1.1	NA	NA	Impingement
Wrangell	AK	EL	1	0.2	0.2	NA	NA	Venturi <sup>1</sup>
Petersburg	AK	EL	NA	NA	NA	NA	NA	NA
Martinez	CA	MH	NA	NA	NA	NA	NA	NA
Redwood City	CA	MH	NA	NA	NA	NA	NA	NA
Yosemite	CA	MH	1	3.4	3.4	NA	NA	Venturi/Impingement
Yosemite National Park	CA	MH	1	4.9	4.9	NA	NA	Venturi/Impingement
San Mateo	CA	MH	1	0.8	0.8	NA	NA	Impingement
Lake Arrowhead	CA	MH	1	4.8	4.8	NA	NA	Scrubber (type unknown)
Palo Alto	CA	MH	2	6	3.0	NA	NA	Impingement
Truckee	CA	MH	NA	NA	NA	NA	NA	NA
Walnut Creek	CA	MH	2	44	22.0	NA	NA	NA
Sacramento	CA	MH	1	7.2	7.2	NA	NA	NA
Barstow	CA	FB	1	2.5	2.5	NA	NA	Spray Chamber
Cromwell	CT	MH	1	12.5	12.5	NA	NA	Net Cyclone
New Haven	CT	MH	1	29.2	29.2	NA	NA	Venturi <sup>1</sup>
Willimantic	CT	MH	NA	NA	NA	NA	NA	Impingement
Hartford	CT	MH	3	336	112.0	NA	NA	Scrubber (type unknown)
New London	CT	MH	2	51.8	25.9	NA	NA	Impingement
Waterbury	CT	MH	1	6.5	6.5	NA	NA	Venturi <sup>1</sup>
Norwalk	CT	FB	2	36	36.0	NA	NA	Venturi <sup>1</sup>
Cromwell	CT	FB	1	NA	NA	1989	NA	NA
West Haven	CT	FB	2	NA	NA	NA	NA	1967/86
Stamford	CT	R/S	1	94.7	94.7	NA	NA	Electrostatic Precipitator
New Canaan	CT	R/S	1	38.9	38.9	NA	NA	Venturi <sup>1</sup>
Jacksonville	FL	MH	1	28.4	28.4	NA	NA	Venturi/Impingement
Pensacola WATP	FL	MH	1	NA	NA	NA	NA	NA
Marletta	GA	MH	2	19.8	19.8	NA	NA	Venturi/Impingement
Atlanta (Bolton Rd)	GA	MH	2	129.6	64.8	NA	NA	Venturi/Impingement
Savannah	GA	MH	2	12	6.0	NA	NA	Venturi Impingement
Atlanta (Utoy)	GA	MH	1	8.1	8.1	NA	NA	Venturi <sup>1</sup>
R.M. Clayton WATP	GA	MH	NA	NA	NA	NA	NA	Scrubber (type unknown)

TABLE A-1. (Continued)

Facility	City	State	Type*	Number of units	Total capacity (dry tpd)	Unit capacity (dry tpd)	Start-up date	Control device(s)
Gainesville		GA	EL	2	5.5	2.8		Venturi
Decatur		GA	EL	2	44.8	22.4		Venturi/Impingement
Honolulu WTP		HI	HH	NA	NA	NA		Venturi/Impingement
San Island WTP		HI	HH	2	25.9	13.0		Venturi/Impingement
Oahu		HI	HH	NA	NA	NA		NA
Cedar Rapids WPCF		IA	HH	1	24.3	24.3		Venturi/Impingement
Davenport		IA	HH	1	35.6	35.6		Venturi/Impingement
Dubuque		IA	FB	2	56	28.0	1970	Venturi
Decatur SIP		IL	HH	NA	NA	NA		NA
Indianapolis		IN	HH	8	362.9	45.4		Wet Cyclone
Johnson County		IA	HH	NA	NA	NA		NA
Shawnee Mission		KA	HH	1	17.8	17.8		Scrubber (type unknown)
Kansas City		KA	FB	2	40	20	1967	Venturi
Kansas City		KA	FB	1	18	18.0	1980	Venturi
Kenton County		KY	HH	NA	NA	NA		NA
Cynthiana		KY	EL	NA	NA	NA		NA
New Orleans		LA	HH	1	30	30.0	1966	Wet Cyclone
Lake Charles		LA	HH	NA	NA	NA		NA
Lake Charles		LA	HH	NA	NA	NA		NA
Algiers		LA	HH	NA	NA	NA		NA
New Orleans West Bank STP		LA	FB	1	41	41.0	1980	Venturi
Lake Charles-Plant B		LA	HH	NA	NA	NA		NA
East Bank STP #1		LA	HH	NA	NA	NA		NA
Lake Charles-Plant C		LA	HH	NA	NA	NA		NA
Lake Charles		LA	HH	1	6	6.0		NA
East Bank STP #2		LA	FB	1	41	41.0	1980	Venturi
Hatchitoches		LA	FB	1	NA	NA		NA
Lynn		MA	HH	NA	NA	NA		NA
Fitchburg East WTP		MA	HH	1	38.9	38.9		Impingement
Chicopee		MA	HH	1	7.2	7.2		Venturi/Impingement
Upper Blackstone WTP		MA	HH	3	35.1	11.7		Impingement
New Bedford WTP		MA	HH	1	16.2	16.2		Impingement
Fall River		MA	HH	NA	NA	NA		NA
Chicopee		MA	HH	1	7.2	7.2		Venturi/Impingement
Attleboro Advanced WTP		MA	HH	NA	NA	NA		Venturi/Impingement
Greater Lawrence SD WTP		MA	HH	2	90.8	45.4		Packed Tower
Annapolis City STP		MD	HH	NA	NA	NA		NA

TABLE A-1. (Continued)

Facility	City	State	Type <sup>a</sup>	Number of units	Total capacity (dry tpd)	Unit capacity (dry tpd)	Start-up date	Control device(s)
Cox Creek WWTP	Riviera Beach	HD	NA	NA	NA	NA	NA	NA
Patapsco	Baltimore	HD	MM	.3	98.4	32.8	NA	NA
Ocean City	Ocean City	HD	FB	2	8	4.0	1969/86	Venturi/Impingement
Wyandotte SIP	Wayne County	MI	MM	4	243.2	60.8	NA	NA
Trenton WWTP	Trenton	MI	MM	NA	NA	NA	NA	NA
Ann Arbor	Ann Arbor	MI	MM	1	54	54.0	NA	scrubber (type unknown)
Lansing WWTP	Lansing	MI	MM	NA	NA	NA	NA	NA
Warren	Warren	MI	MM	1	25.9	25.9	NA	Wet Cyclone/Impingement
Ohiozzo WWTP	Okosso	MI	MM	NA	NA	NA	NA	NA
Detroit (1)	Detroit	MI	MM	6	408	68.0	NA	Venturi/Impingement
Pontiac SIP	Pontiac	MI	MM	1	64.8	64.8	NA	scrubber (type unknown)
Detroit (2)	Detroit	MI	MM	8	673.8	84.2	NA	Impingement
Grand Rapids	Grand Rapids	MI	MM	1	32.4	32.4	NA	Venturi
Kalamazoo WWTP	Kalamazoo	MI	MM	1	48	48.0	NA	Venturi/Impingement
Niles WWTP	Niles	MI	MM	NA	NA	NA	NA	NA
East Lansing	East Lansing	MI	MM	2	32.4	16.2	NA	scrubber (type unknown)
Ypsilanti	Ypsilanti	MI	MM	1	54	54.0	NA	Venturi
Battle Creek	Battle Creek	MI	MM	NA	NA	NA	NA	NA
Bay City	Bay City	MI	MM	1	3.2	3.2	NA	scrubber (type unknown)
Port Huron	Port Huron	MI	FB	1	7.6	7.6	1974	Venturi/Impingement
Bay County	Bay County	MI	EL	NA	NA	NA	NA	NA
St. Paul	St. Paul	MM	6	777.6	129.6	NA	NA	Venturi/Impingement
Seneca IP	Seneca IP	MM	2	19.4	9.7	NA	NA	Venturi/Impingement
Duluth	Duluth	NN	R/S	2	34	17.0	NA	Venturi
Kansas City	Kansas City	HO	MM	1	45.4	45.4	NA	scrubber (type unknown)
St. Louis (Lennay STP)	St. Louis	HO	MM	4	145.8	36.5	NA	Venturi/Impingement
St. Louis (Bissell Point STP)	Independence	HO	HO	5	324	64.8	NA	Wet Cyclone
Independence	Little Blue Valley	HO	FB	1	9.7	9.7	1979	Venturi/Impingement
Little Blue Valley	Greensboro	NC	MM	1	NA	NA	1989	NA
Greensboro	Rocky Mount	NC	MM	1	7.5	7.5	NA	Venturi/Impingement
Rocky Mount	Shelby	NC	FB	1	16.2	16.2	1966	Impingement
Shelby	Manchester	NH	MM	NA	NA	NA	NA	Venturi

TABLE A-1. (Continued)

Facility	City	State	Type*	Number of units	Total capacity (dry tpd)	Unit capacity (dry tpd)	Start-up date	Control device(s)
Lebanon WWT								
Herrimack WWT	Lebanon	NH	HH	1	7.2	7.2	NA	Venturi/Impingement
Stony Brook RSA STP #1	Herrimack	NH	HH	NA	NA	NA	NA	Venturi
Rockaway Valley	Princeton	NJ	HH	2	39.5	19.8	NA	Venturi/Impingement
Atlantic City	Parsippany-Troy Hills	NJ	HH	NA	NA	NA	NA	NA
Parsippany	Atlantic City	NJ	HH	1	25.9	25.9	NA	Venturi/Impingement
Wayne	Parsippany	NJ	HH	2	77.8	38.9	NA	Uncontrolled
Mountain View Sewer Authority	Wayne	NJ	HH	2	96	48.0	NA	Scrubber (type unknown)
West Side STP	Wayne Township	NJ	HH	NA	NA	NA	NA	NA
Two Bridges	Jersey City	NJ	HH	1	13.8	13.8	NA	Venturi
NW Bergen County Utilities	Lincoln Park	NJ	FB	1	66	66	1979	Venturi/Impingement
Somerset Raritan Valley Authority	Waldwick	NJ	FB	1	18	18.0	1970	Venturi
Gloucester Township	Bridgewater	NJ	FB	1	14	14.0	1972	Venturi/Impingement
Bayshore Regional Sewer Authority	Blackwood	NJ	FB	1	9.6	9.6	1985	Venturi/Impingement
Douglas County SID #1 WWT	Union Beach	NJ	FB	1	30	30.0	1974	Venturi/Impingement
Round Hill	Zephyr Cove	NV	FB	1	5	5.0	1985	Venturi/Impingement
West STP	Douglas County	NV	FB	2	9.0	4.5	1966/84	Scrubber (type unknown)
Frank E. Van Lare WTP	Oswego	NY	HH	NA	NA	NA	NA	NA
Anherst	Rochester	NY	HH	2	72	36.0	NA	Scrubber (type unknown)
Gates Chitt Ogden STP	Anherst	NY	HH	NA	NA	NA	NA	Venturi/Impingement
Auburn	Rochester	NY	HH	2	36	18.0	NA	Scrubber (type unknown)
New Rochelle SD STP	Auburn	NY	HH	1	40.5	40.5	NA	Scrubber (type unknown)
Orangetown DPW	New Rochelle	NY	HH	NA	NA	NA	NA	NA
Hamaroneck	Orangetown	NY	HH	1	16.8	16.8	NA	Venturi/Impingement
Disposal District No. 15	Mamaroneck	NY	HH	NA	NA	NA	NA	NA
Niagra County	Southampton	NY	HH	NA	NA	NA	NA	NA
Two Mile Creek STP	Niagra County	NY	HH	NA	NA	NA	NA	Scrubber (type unknown)
Rochester (NW Quad)	Tonawanda	NY	HH	NA	NA	NA	NA	Scrubber (type unknown)
Watertown	Rochester	NY	HH	2	48	24.0	NA	Impingement
Albany (North)	Watertown	NY	HH	1	21	21.0	NA	Scrubber (type unknown)
Port Chester SDSTP	Albany	NY	HH	2	129.6	64.8	NA	NA
Birds Island STP	Port Chester	NY	HH	3	183.6	61.2	NA	NA
Dunkirk STP	Buffalo	NY	HH	NA	NA	NA	NA	Venturi
	Dunkirk	NY	HH	NA	NA	NA	NA	NA

TABLE A-1. (Continued)

Facility	City	State	Type*	Number of units	Total capacity (dry tpd)	Unit capacity (dry tpd)	Start-up date	Control devices
East STP	Oswego	NY	MH	NA	NA	NA	NA	Impingement
Albany (South)	Albany	NY	MH	2	91.8	45.9	NA	NA
NW Quadrant TP	Greece	NY	MH	NA	NA	NA	NA	Scrubber (type unknown)
Schenectady STP	Schenectady	NY	MH	1	140	140.0	NA	Scrubber (type unknown)
Beacon WPCP	Beacon	NY	MH	1	9.7	9.7	NA	NA
Saratoga	Saratoga	NY	FB	1	NA	NA	NA	Scrubber (type unknown)
Watertown	Watertown	NY	FB	1	NA	NA	NA	NA
Arlington	Arlington	NY	FB	1	8.4	8.4	NA	Scrubber (type unknown)
Port Washington	Port Washington	NY	FB	1	NA	NA	1968	NA
Oneida County	Oneida County	NY	FB	3	60	20.0	1972/87	Venturi
Erie County	Erie County	NY	FB	2	288	144.0	NA	Venturi/Impingement
Little Falls	Little Falls	NY	FB	1	3.9	3.9	NA	Venturi
Glens Falls	Glens Falls	NY	FB	1	NA	NA	NA	NA
Buffalo	Buffalo	NY	FB	1	43.2	21.6	1981	Venturi/Packed Tower
Bath	Bath	NY	R/S	1	NA	NA	NA	NA
New York	New York	NY	R/S	1	25	25.0	NA	Electrostatic Precipitator
Akron	Akron	OH	MH	4	38.8	9.7	NA	Venturi/Impingement
Cleveland	Cleveland	OH	MH	4	259.2	64.8	1979	Venturi/Impingement
Columbus	Columbus	OH	MH	1	38.9	38.9	NA	Venturi
Canton	Canton	OH	MH	2	50	25	NA	Impingement
Cincinnati	Cincinnati	OH	MH	4	168.4	42.1	NA	Impingement
Cleveland	Cleveland	OH	MH	2	194.4	97.2	1982	Impingement
Euclid WTP	Euclid	OH	MH	2	21.6	10.8	NA	Scrubber (type unknown)
Little Miami WTP	Cincinnati	OH	MH	3	NA	NA	NA	Venturi/Impingement
Willoughby-Eastlake WTP	Willoughby	OH	MH	1	21	21	1974	Scrubber / Tray
Youngstown WTP	Youngstown	OH	MH	1	40.5	40.5	NA	Spray Chamber
Lorain	Lorain	OH	FB	1	NA	NA	NA	NA
Tigard	Tigard	OR	MH	3	15	15	NA	Venturi/Impingement
Franklin	Franklin	OH	R/S	NA	NA	NA	NA	NA
Ambridge	Ambridge	PA	MH	NA	NA	NA	NA	NA
York	York	PA	MH	2	38.8	19.4	NA	Scrubber (type unknown)
Bridgeport	Bridgeport	PA	MH	NA	NA	NA	NA	NA

(Continued)

TABLE A-1. (Continued)

Facility	City	State	Type <sup>a</sup>	Number of units	Total capacity (dry tpd)	Unit capacity (dry tpd)	Start-up date	Control device(s)
Erie	Willow Grove	PA	MH	2	135	67.5	NA	Electrostatic Precipitator
Upper Moreland-Hatboro TP	Johnstown	PA	MH	1	8.1	8.1	NA	NA
City of Johnstown	Pittsburgh	PA	MH	1	NA	NA	NA	Uncontrolled
Alcosan WTP	Chester	PA	MH	2	19.4	9.7	NA	Scrubber (type unknown)
Delcore-Chester STP	Appolo	PA	MH	7	136.1	19.4	NA	Scrubber (type unknown)
Kiski Valley WPCA	Harrisstown	PA	MH	NA	NA	NA	NA	Scrubber (type unknown)
E. Harrisstown Plymouth TP	Lemoine Boro	PA	MH	NA	NA	NA	NA	NA
Cumberland City	Wilkes-Barre	PA	MH	1	32.4	32.4	NA	Scrubber (type unknown)
Duryea	Duryea	PA	MH	1	25.9	25.9	NA	NA
Lower Lackawanna STP	Old Forge	PA	MH	NA	NA	NA	NA	Scrubber (type unknown)
Hazfield Township STP	Colmar	PA	MH	1	5.7	5.7	NA	Scrubber (type unknown)
Hershey	Hershey	PA	MH	1	40.5	40.5	NA	Impingement
Tyrone	Tyrone	PA	FB	1	5.1	5.1	NA	NA
Upper Glyndedd	North Wales	PA	FB	1	1.1	1.1	1973	Scrubber (type unknown)
Hazelton	West Hazelton	PA	FB	1	4.5	4.5	NA	Venturi
Trout Run WPCF	Upper Marion Township	PA	FB	1	NA	NA	NA	Impingement
Harrisburg	Harrisburg	PA	R/S	2	135.4	67.7	NA	Electrostatic Precipitator
Cranston	Cranston	RI	MH	2	20.4	10.2	NA	Venturi/Impingement
Providence	Providence	RI	MH	2	NA	NA	NA	Venturi
Columbia	Columbia	SC	MH	2	8.2	4.1	NA	scrubber (type unknown)
Charleston	Charleston	SC	MH	1	32.4	32.4	NA	scrubber (type unknown)
North Charleston	North Charleston	SC	FB	1	NA	NA	NA	NA
Central WTP	Nashville	TN	MH	2	92	46.0	NA	Scrubber (type unknown)
Charleston	Bristol	TN	MH	1	16.2	16.2	NA	Venturi/Impingement
Maryville	Maryville	TN	MH	1	13	13.0	NA	Scrubber (type unknown)
Newport	Newport	TN	MH	1	7.8	7.8	NA	NA
Fairfax	Fairfax	VA	MH	2	64.8	32.4	NA	Scrubber (type unknown)
Alexandria STP	Alexandria	VA	MH	2	NA	NA	NA	Net Cyclone
Williamsburg WPCF	Williamsburg	VA	MH	2	55.7	27.8	NA	NA
Fairfax (Lower Potomac STP)	Fairfax	VA	MH	2	90.8	45.4	NA	Venturi/Impingement
Potomac River STP	Woodbridge	VA	MH	NA	NA	NA	NA	Impingement
Boat Harbor WPCF	Newport News	VA	MH	2	33.7	16.9	NA	Venturi/Impingement

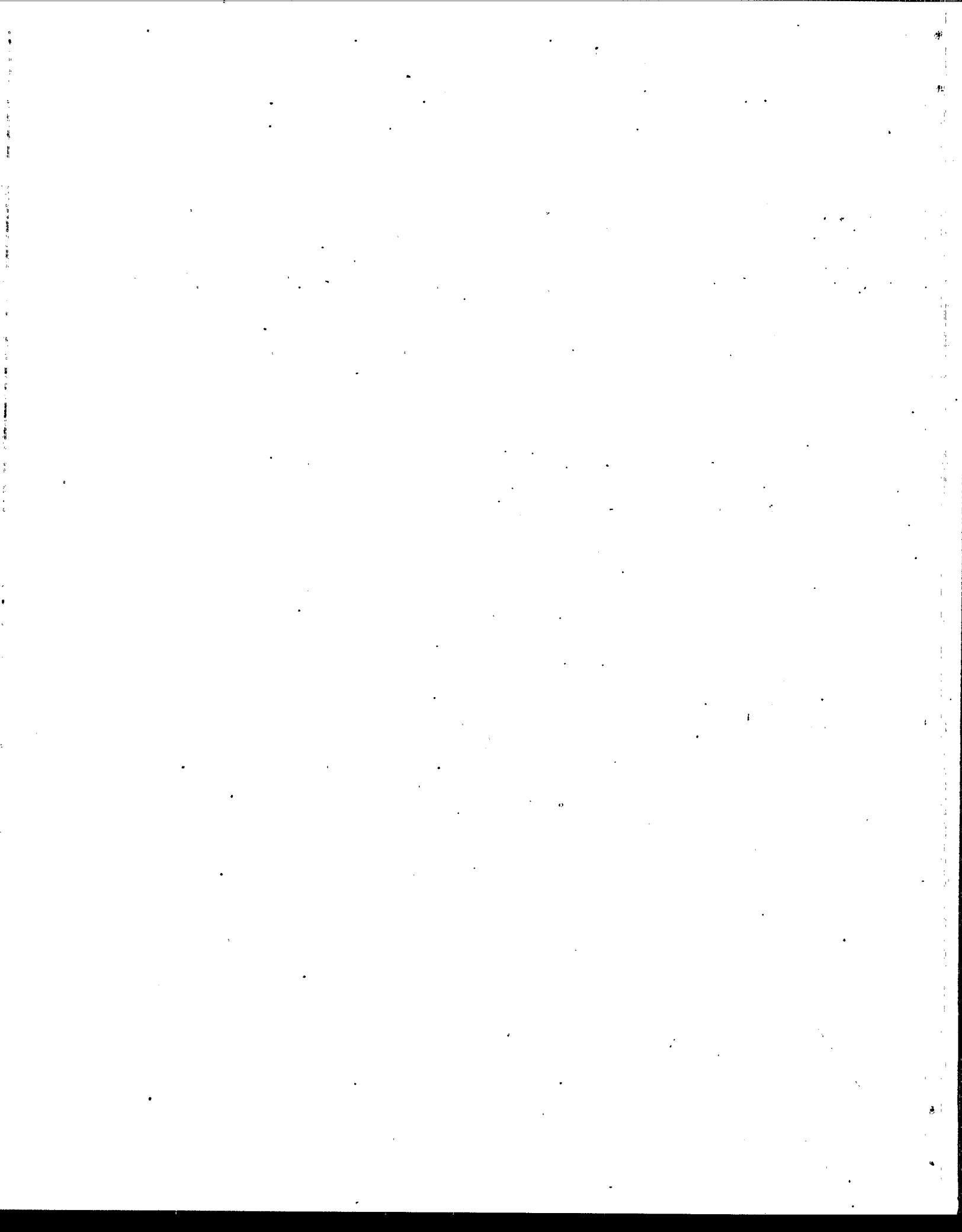
TABLE A-1. (continued)

Facility	City	State	Type*	Number of units	Total capacity (dry tpd)	Unit capacity (dry tpd)	Start-up date	Control device(s)
Arlington COMPCP	Arlington	VA	MH	2	34.8	17.4	NA	Venturi/Impingement
Hopewell	Hopewell	VA	MH	2	8.1	8.1	NA	Scrubber (type unknown)
Army Base WTP (Hampton Rds.)	Norfolk	VA	MH	2	25.5	12.8	NA	Venturi/Impingement
Lamberts Point WPCF	Norfolk	VA	MH	2	57.9	29.0	NA	Venturi/Impingement
Chesapeake-Eлизabeth WPCF	Virginia Beach	VA	MH	2	22.8	11.4	NA	Venturi/Impingement
Vancouver	Vancouver	WA	MH	1	34	34.0	NA	Scrubber (type unknown)
Edmonds	Edmonds	WA	FB	1	1.6	1.6	NA	Scrubber (type unknown)
Lynnwood	Lynnwood	WA	FB	1	0.7	0.7	NA	Scrubber (type unknown)
Brookfield	Brookfield	WI	MH	1	3.9	3.9	NA	Impingement
Green Bay WTP	Green Bay	WI	MH	2	87.5	87.5	NA	Scrubber (type unknown)
Milwaukee	Milwaukee	WI	MH	1	7.1	7.1	NA	Scrubber (type unknown)
Clarksburg STP	Clarksburg	WV	MH	NA	NA	NA	NA	NA
Huntington	Huntington	WV	FB	1	NA	NA	1989	NA

Note: NA Means Information Not Available.

\*As of May 31, 1989.

Type Key: MH=Multiple Hearth; FB=Fluidized Bed; EL=Electric; R/S=Refuse/Sludge.



# TECHNICAL REPORT DATA

*(Please read Instructions on the reverse before completing)*

1. REPORT NO.	2.	3. RECIPIENT'S ACCESSION NO.
EPA-405/2-90-009		
4. TITLE AND SUBTITLE  <i>Locating And Estimating Air Toxics Emissions From Sewage Sludge Incinerators</i>		5. REPORT DATE  <i>May 1990</i>
7. AUTHOR(S)		8. PERFORMING ORGANIZATION CODE  <i>90-203-080-83-02</i>
9. PERFORMING ORGANIZATION NAME AND ADDRESS  <i>Radian Corporation Post Office Box 13000 Research Triangle Park, NC 27709</i>		10. PROGRAM ELEMENT NO.
		11. CONTRACT/GANT NO.  <i>68-02-4392, Work Assignment 52 &amp; 83</i>
12. SPONSORING AGENCY NAME AND ADDRESS  <i>U.S. Environmental Protection Agency OAR, OAQPS, AQMD, NPPB, PCS (MD-15) Research Triangle Park, NC 27711</i>		13. TYPE OF REPORT AND PERIOD COVERED  <i>Final, 3/89 - 11/89</i>
15. SUPPLEMENTARY NOTES  <i>EPA Project Officer: William B. Kuykendal</i>		14. SPONSORING AGENCY CODE
16. ABSTRACT This document is intended to assist groups interested in inventing air emissions of various potentially toxic substances from sewage sludge incinerators. Its intended audience includes Federal, State and local air pollution personnel. The document presents information on the process description of the various types of sewage sludge incinerators and their air pollution control equipment. Emission factors are presented for each major type of sewage sludge incinerators for the following: metals including arsenics, beryllium, cadmium, chromium, and nickel; and organics including chlorinated dibenzo-p-dioxins, dibenzofurans, benzene, chlorinated benzene, and phenol.		
17. KEY WORDS AND DOCUMENT ANALYSIS		
a. DESCRIPTORS  <i>Sewage Sludge Incineration Air Toxics Emissions Emission Factors</i>	b. Identifiers/Open ended terms	c. COSATI Field/Group
18. DISTRIBUTION STATEMENT  <i>Unlimited</i>		19. SECURITY CLASS (This Report)  <i>Unclassified</i>
		21. NO OF PAGES  <i>79</i>
20. SECURITY CLASS (This page)  <i>Unclassified</i>		22. PRICE

