



Evaluation of Method 5B at an Oil-Fired Boiler

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SECTION 1

INTRODUCTION

On June 28, 1979, the U.S. Environmental Protection Agency (EPA) issued an advance notice of proposed rulemaking to develop New Source Performance Standards (NSPS) for fossil-fuel-fired industrial steam generators.* Because these sources can emit significant amounts of condensible sulfates that even the best emission reduction systems are unable to control, particulate emissions measured by Method 5, which is capable of collecting condensible matter, could vary widely as a result of fuel sulfur content or process changes. For this reason, the EPA decided that condensible sulfates should not be included in particulate emission standards or measurements. Therefore, the test program undertaken by EPA to support development of the NSPS had two objectives: 1) to obtain background emission data, and 2) to evaluate sampling and analytical parameters designed to minimize collection of condensible sulfate materials from these sources. Background emission data have been collected at several coal-fired facilities and at one oil-fired facility by use of both the proposed Method 5B (to minimize collection of condensible sulfates) and Method 5.

* 44 FR 37632.

PEDCo Environmental, Inc., under contract to the Emission Measurement Branch of the EPA, conducted an atmospheric emission test program from February 7 through February 12, 1983, on the exhaust gases of a 400-MW oil-fired utility boiler. Testing was performed in an effort to determine the precision of proposed Method 5B and to evaluate the effect of sampling and analysis parameters on the collection of condensible sulfates.

All samples were collected by use of a four-train (quad) sampling system stationed at a single point in the exit gas stream. A total of 10 quad train tests were performed during the test series. Paired trains in the quad system consisted of similar sampling methods to allow within-run data comparisons as well as comparisons between different sampling methods.

So that method precision could be estimated, most of the samples were collected at Method 5B sampling conditions [filter and probe heated to 160°C (320°F)], designated as M5B.

Other sampling parameter studies have shown generally that 1) a higher sampling temperature can minimize collection of condensible matter, and 2) even a well-designed, well-constructed, and well-operated probe heating system can have cold spots where the gas temperature is lower than the desired monitored probe temperature. Consequently, several of the quad test runs were conducted with the probe heated to 204°C (400°F) in an effort to raise the temperature of any cold spots in the probe to approximately 160°C (320°F), the desired filter temperature. These samples were designated as M5B-P400.

Probe rinse and filter sample fractions collected by Methods 5B and 5B-P400 were subjected to a series of thermogravimetric analyses to assess sample weight loss as a function of heating temperature between ambient conditions and 316°C (600°F).

In addition, several samples (designated M5BW) were collected and analyzed by use of a modified version of Texas Air Control Board (TACB) Method 5W.* The method incorporates deionized water as the sample recovery solvent and a series of titrimetric and gravimetric analyses to measure water-soluble sulfates and subsequently derive the mass of nonwater-soluble sulfate particulate (particulate matter that does not include any water-soluble sulfates). The method was modified by sampling at 160°C (320°F) and measuring the water-soluble sulfates by ion chromatography (IC). These tests were conducted to determine the suitability of this method for fossil-fuel-fired steam generators. Previous studies^{1,2} have confirmed the suitability of Method 5W and the IC analysis modification for use on fluid catalytic cracking unit regenerators at petroleum refineries, which also can emit significant amounts of condensible sulfates.

The filterable portion of each sample train was followed by a modified EPA Method 8 impinger train; this permitted analysis of sulfur dioxide (SO₂) and condensible sulfate [as sulfuric acid (H₂SO₄)] that passed through the particulate filter. Flue gas temperature, moisture content, and composition [oxygen (O₂)

*Texas Air Control Board - Laboratory Division. Determination of Particulate in Stack Gases Containing Sulfur Dioxide. December 1979.

and carbon dioxide (CO₂) were measured in conjunction with the emission tests.

Ms. Jenna Sellers, the host plant's representative, recorded process data and provided assistance on site. Mr. Gary McAlister, the EPA Task Manager, and Mr. Andrew Kasprik, the utility company's representative, provided overall project coordination.

This report documents the activities and results of the test program. Section 2 briefly describes the process and operating conditions during the sampling periods. Section 3 describes the sampling site and the sampling and analytical plan. Section 4 presents the test results, which are then discussed in Section 5. Section 6 outlines quality assurance measures and audit results. The appendices contain computer output and example calculations (Appendix A), field data (Appendix B), analytical data (Appendix C), standard sampling and analytical procedures (Appendix D), calibration procedures and results (Appendix E), a quality assurance summary (Appendix F), a list of project participants (Appendix G), and process data (Appendix H).

SECTION 2

PROCESS OPERATION

The source tested in this program is a 400-MW fossil-fuel-fired utility boiler (designated Unit 2) located in the southeastern United States. The pressurized Foster Wheeler boiler, which was placed in service in 1969, generates steam at 17.9 MPa and 541°C (2590 psig and 1005°C). This unit normally fires a mixture of heavy oil and gas, but it was operated on 100 percent oil during the test program. Fly ash removed by the mechanical dust collectors is automatically reinjected into the furnace. Flue gases are exhausted through a 121-m (397-ft) stack. Typical oil burned in the boiler contains 2.4 percent sulfur and 300 to 400 ppm vanadium. No fuel additives are used at this facility.

Table 2-1 summarizes process conditions during the sampling periods. All tests were conducted at essentially the same boiler load (380-MW), as the load did not vary by more than ± 5 percent at any time during the sampling periods. A sudden loss of air flow occurred near the beginning of Run 4, but conditions stabilized in about 10 minutes. The condensate blowdown valve was opened during three runs because of high silica concentrations. None of these relatively minor process variations should affect the within-run data comparisons.

TABLE 2-1. PROCESS DATA SUMMARY

Run No.	Date (1983)	Time, 24-h	Gross load, MW		Stack monitor opacity range, %	Oxygen range at east economizer exit, %	Operation
			Range	Average			
1	2/7	0950-1150	Steady	380	21	0.9-1.0	Normal
2	2/7	1410-1610	Steady	380	22-25	0.8-1.1	Normal
3	2/8	0845-1045	Steady	380	18	0.7-0.8	Normal
4	2/8	1230-1430	Steady	380	22-30	0.6-1.2	a
5	2/11	0755-0925	365-378	375	18	0.7	b
6	2/11	1050-1220	Steady	380	24	0.4-0.5	CBD open ^c
7	2/11	1330-1500	Steady	380	20	0.6-0.7	CBD open ^c
8	2/11	1620-1650	Steady	375	18	0.8	Normal
9	2/12	0830-1000	Steady	385	20	0.6-0.7	Normal
10	2/12	1200-1330	Steady	385	20	0.6	Normal

^aAt 1250 hours there was a sudden loss of air flow. Conditions returned to normal in approximately 10 minutes.

^bAt 0820 hours the boiler pressure was decreased slightly and the condensate blowdown was opened because of high silica concentrations.

^cThe condensate blowdown was open because of high silica concentrations; boiler at full pressure.

Testing was not conducted on two days because the unit was operating at reduced load (approximately 200-MW) as a result of a malfunctioning condensate pump.

SECTION 3

SAMPLING AND ANALYTICAL PLAN

All samples were collected with a four-train (quad) sample system stationed at a single point in the exit gas stream. The sample methodology was developed and validated in previous studies.³ The ability of the four trains to sample simultaneously at essentially the same point in the gas stream (Figure 3-1) reduces the effect of spatial and temporal variations in the velocity and particulate profiles on the sampling results. It also permits a statistically significant number of samples to be taken in a short time. Further, because two of the four trains are identical for every run, within-train precision can be determined while the relationship of the different trains is being compared.

3.1 SAMPLE LOCATION

Testing took place in the east duct of Unit 2, as shown in Figures 3-2 and 3-3. Two existing 7.6-cm (3-in.) diameter ports were located 90 degrees apart in each of the horizontal ducts. A new 15-cm (6-in.) I.D. sampling port for the quad-train samples was installed in the side of the east duct above one of the existing smaller ports. All of the ports were located approximately 3 duct diameters downstream from the mechanical dust

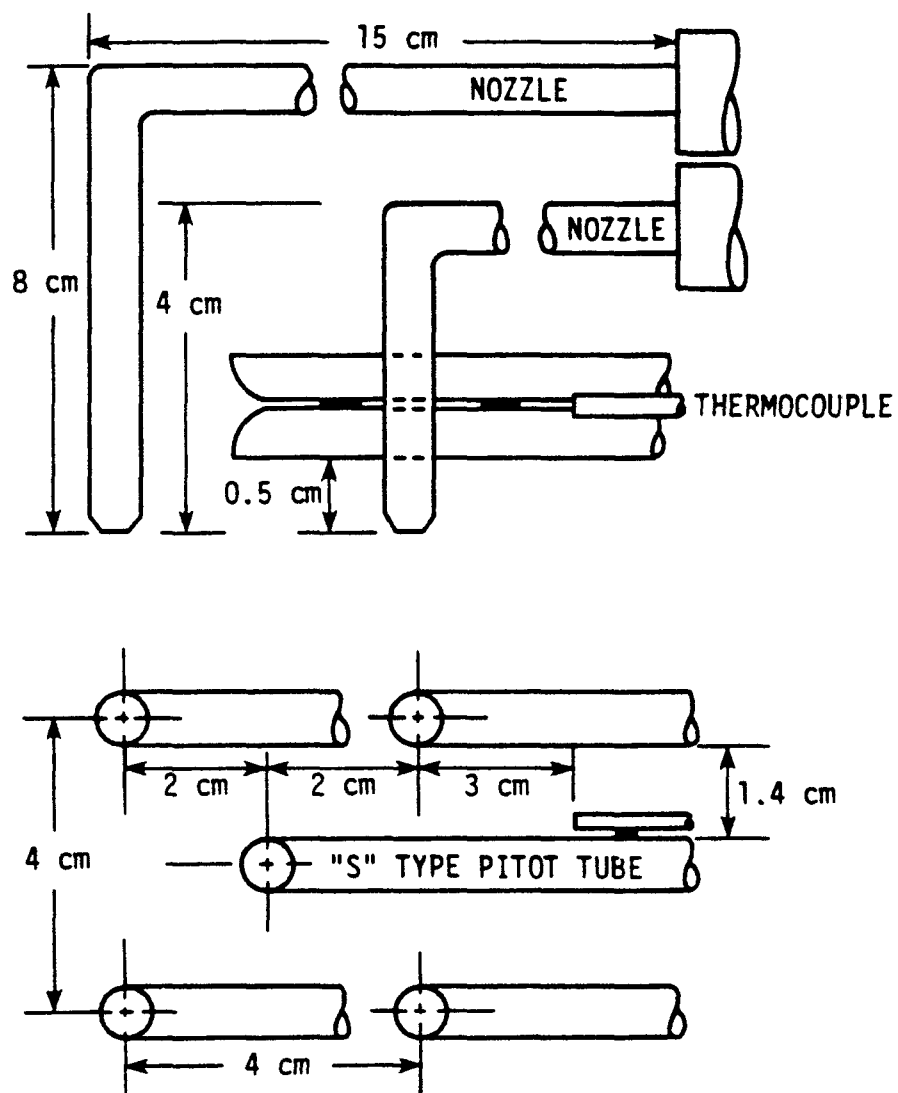


Figure 3-1. Four-train sampling system showing nozzle position.

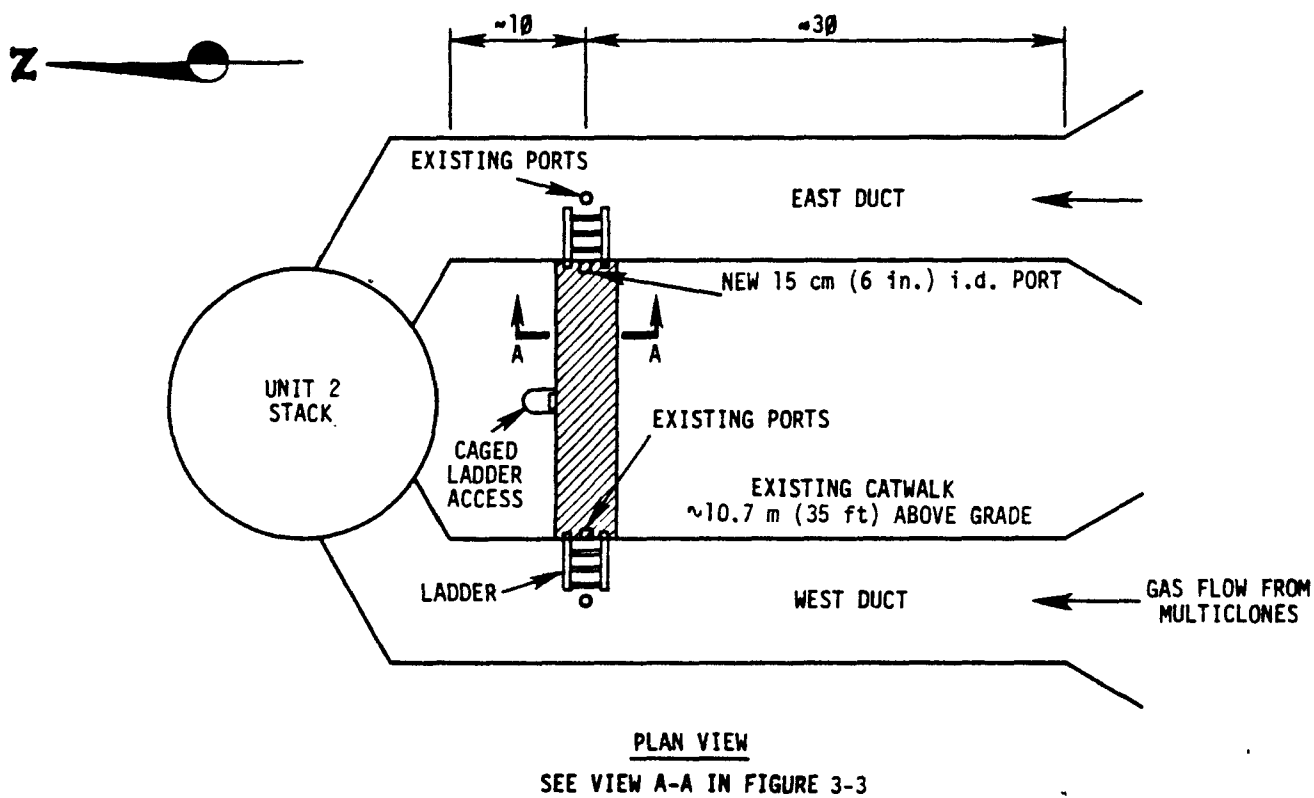


Figure 3-2. Sampling site.

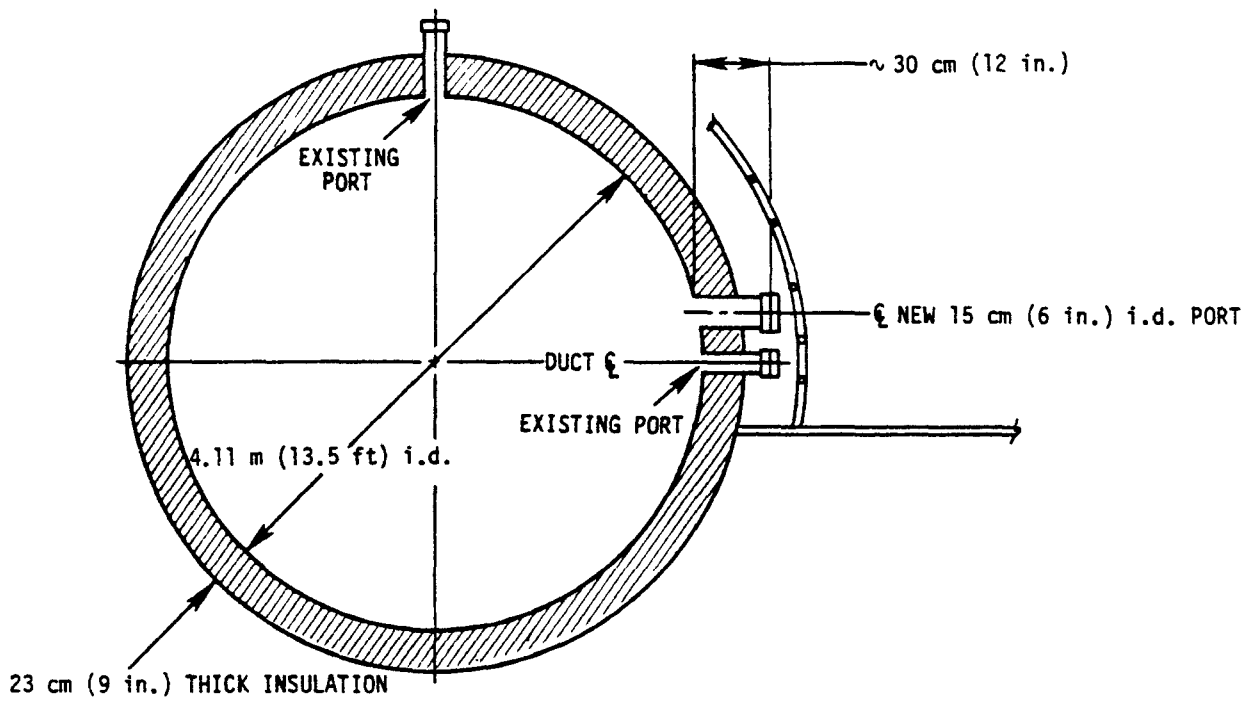
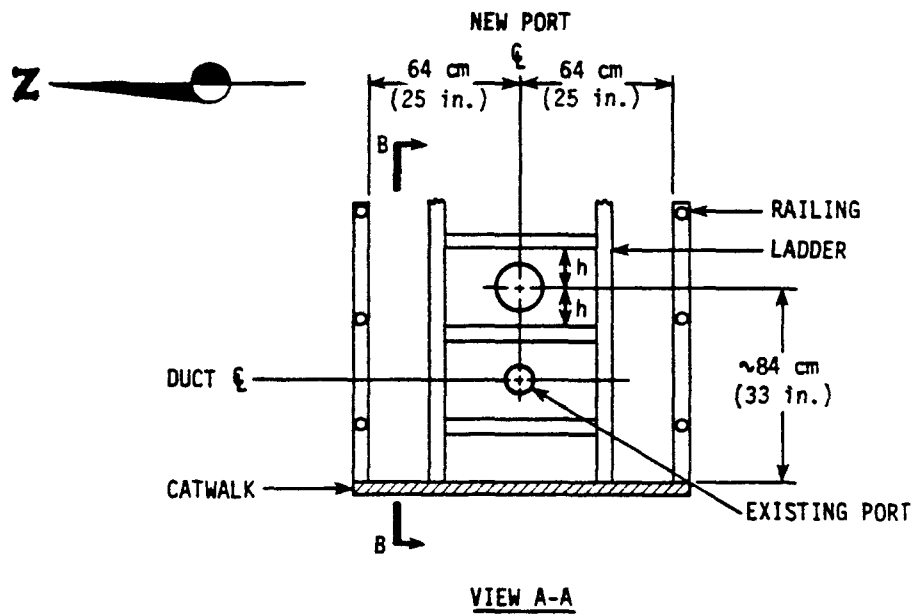


Figure 3-3. Location of sampling ports in east duct of Unit 2.

collector outlets and 1 duct diameter upstream of a 45-degree bend. Both ducts had an inside diameter of 4.11 m (13.5 ft) surrounded by a 23-cm (9-in.) thick layer of insulation.

3.2 SAMPLE METHODS

The four trains collected flue gas samples simultaneously from a single point in the gas stream. The nozzles of the four-train assembly (Figure 3-1) were positioned 64 cm (25 in.) from the stack wall for each test. The desired sample time was 120 minutes, and readings of stack flue gas and sampling train data were recorded for each train at 10-minute intervals. A single pitot tube and thermocouple located in the four-train nozzle arrangement was used to set isokinetic sample rates for each train. Sample rates were determined by use of programmable calculators. Prior to sampling, the velocity and temperature profile of the general sampling area was established to ensure that all four nozzles could be positioned at points of equal velocity to minimize spatial variations in emissions.

Table 3-1 presents the sample matrix performed during this test series. The particular conditions for each train are described briefly below:

- ° Method 5B - Designation M5B

Filterable particulate was collected by use of a probe and filter assembly heated to 160°C (320°F). Acetone was used to rinse all sample train components prior to the filter.

TABLE 3-1. SAMPLE MATRIX

Run No.	Sample Train No.	Sample method ^a		
		M5B 160°C (320°F)	M5B-P400 160°-204°C (320°-400°F)	M5BW 160°C (320°F)
1	1A			X
	1B			X
	1C	X		
	1D	X		
2	2A	X		
	2B	X		
	2C			X
	2D			X
3	3A	X		
	3B	X		
	3C		X	
	3D		X	
4	4A		X	
	4B		X	
	4C	X		
	4D	X		
5	5A	X		
	5B	X		
	5C	X		
	5D	X		
6	6A	X		
	6B	X		
	6C	X		
	6D	X		

(continued)

TABLE 3-1 (continued)

Run No.	Sample Train No.	Sample method ^a		
		M5B 160°C (320°F)	M5B-P400 160°-204°C (320°-400°F)	M5BW 160°C (320°F)
7	7A			X
	7B	X		
	7C			X
	7D	X		
8	8A	X		
	8B		X	
	8C	X		
	8D		X	
9	9A	X		
	9B	X		
	9C	X		
	9D	X		
10	10A	X		
	10B		X	
	10C	X		
	10D		X	

^aM5B - Probe and filter heated to 160°C.

M5B-P400 - Probe heated to 204°C; filter heated to 160°C.

M5BW - Probe and filter heated to 160°C; water rinse of nozzle, probe, and front filter holder glassware.

° Modified Method 5B - Designation M5B-P400

Filterable particulate was collected by use of a probe heated to 204°C (400°F) and a filter assembly heated to 160°C (320°F). Acetone was used to rinse all sample train components prior to the filter.

° Method 5BW - Designation M5BW

Filterable particulate was collected by use of a probe and filter assembly heated to 160°C (320°F). Deionized, distilled water was used to rinse all sample train components prior to the filter.

The purpose of heating the probe to 204°C while keeping the filter at 160°C was to raise the temperature of any cold spots in the probe to 160°C, and thereby minimize the quantity of condensible sulfates collected.

For each train, the probe and filter temperatures were set at the predetermined level and monitored throughout each test by the use of multiterminal digital indicators with the thermocouples located in the middle of each probe and immediately behind the Method 5 filter frits.

The back half of each sample train represented a modified Method 8 with five impingers. An unheated Method 5 filter assembly was inserted between the second and third impingers to preclude any sulfuric acid mist carryover. The contents of each impinger are listed below:

<u>Impinger</u>	<u>Contents - All Runs</u>
1	Empty
2	200 ml 80% IPA
3	100 ml 10% H ₂ O ₂
4	100 ml 10% H ₂ O ₂
5	400 grams silica gel

All the filters were Whatman Reeve Angel 934AH. The filters used in the Method 5 position were heated to 300°C prior to identification and tare weighing.

The flue gas moisture content of each sample train was determined gravimetrically by weighing each impinger before and after every test. In addition, a flue gas grab sample collected during each test was analyzed for oxygen (O₂) and carbon dioxide (CO₂) by use of an Orsat analyzer, as described in Method 3* of the Federal Register.

3.3 SAMPLE ANALYSIS

Table 3-2 presents the analytical matrix followed for this test program.

Thermogravimetric Analysis

Initially, the filter particulate catch was placed in a tared glass weighing dish, desiccated for 24 hours, and weighed to a constant weight.** The probe rinse fraction was transferred to a tared beaker, allowed to evaporate to dryness at ambient temperature and pressure, desiccated for 24 hours, and weighed to a constant weight. Because previous data have shown that samples containing a significant amount of sulfuric acid may not come to a constant weight, each sample received a maximum of three separate weighings. In any case, the lowest weight achieved was reported as the ambient weight.

* 40 CFR 60, Appendix A, Reference Method 3, July 1982.

** Criteria as specified in 40 CFR 60, Appendix A, Reference Method 5, July 1982.

TABLE 3-2. ANALYTICAL MATRIX

Run No.	Sample Train No.	Sample method	Thermogravimetric conditioning			Water soluble sulfate determination ^b
			Ambient → 160° → 232° → 316°C	Ambient → 232° → 316°C	Ambient → 316°C	
1	1A	M5BW				X
	1B	M5BW				X
	1C	M5B	X			
	1D	M5B	X			
2	2A	M5B	X (24)			
	2B	M5B	X (24)			
	2C	M5BW				X
	2D	M5BW				X
3	3A	M5B	X			
	3B	M5B	X			
	3C	M5B-P400	X			
	3D	M5B-P400	X			
4	4A	M5B-P400	X			
	4B	M5B-P400	X			
	4C	M5B	X			
	4D	M5B	X			
5	5A	M5B	X			
	5B	M5B	X			
	5C	M5B	X (24)			
	5D	M5B	X (24)			
6	6A	M5B		X (24)		
	6B	M5B		X (24)		
	6C	M5B		X		
	6D	M5B		X		

(continued)

TABLE 3-2 (continued)

Run No.	Sample Train No.	Sample method	Thermogravimetric conditioning			Water soluble sulfate determination ^b
			Ambient → 160° → 232° → 316°C	Ambient → 232° → 316°C	Ambient → 316°C	
7	7A	M5BW				X
	7B	M5B		X		
	7C	M5BW				X
	7D	M5B		X		
8	8A	M5B	X (24)			
	8B	M5B-P400	X			
	8C	M5B	X (24)			
	8D	M5B-P400	X			
9	9A	M5B			X (24)	
	9B	M5B			X (24)	
	9C	M5B			X	
	9D	M5B			X	
10	10A	M5B		X		
	10B	M5B-P400		X		
	10C	M5B		X		
	10D	M5B-P400		X		

^aThermogravimetric conditioning of probe rinse and filter fractions at indicated temperatures after initial desiccation and ambient weights were obtained. The designation (24) for selected samples indicates a heat period of 24 hours. All other samples were heat-conditioned for 6 hours.

^bIn this procedure, the mass of total water-soluble sulfates in the sample was determined and subtracted from the total sample mass.

Note: All back halves represent a modified Method 8, with analysis for sulfates as sulfuric acid and sulfur dioxide.

After this initial gravimetric analysis at ambient conditions, probe rinse and filter fractions were subjected to the sequence of heat treatments outlined in Table 3-2. The samples were heated in an oven at the specified temperature for either 6 or 24 hours, as indicated. Each sample fraction was cooled and desiccated for 24 hours after removal from the oven and then weighed to the nearest 0.1 mg. Each sample was then desiccated for an additional 3 hours and weighed to the nearest 0.1 mg. The lower weight obtained was reported.

Selected samples received additional heat treatments to evaluate sample stability. For these samples, a heat treatment was repeated at the same time and temperature condition until a stable weight was obtained prior to advancing to the next step of an analytical sequence. For this study, a stable weight was defined as a difference of no more than 5.0 mg or 10 percent of the net sample weight (whichever was greater) between successive treatments at the same conditions. The number of treatments required to achieve a stable weight was recorded for selected sample fractions up to a maximum of three treatments. The lowest weight achieved at a given treatment temperature was reported as the weight for that temperature condition. Filter and acetone blanks were treated in a similar manner as the actual samples.

Water-Soluble Sulfate Analysis

Sample Preparation--

Each sample fraction, including blanks, was handled and analyzed as follows:

Filter - The filter was cut into small pieces and placed in a 125-ml Erlenmeyer flask with a standard taper joint equipped with an air condenser. The shipping container was rinsed into the flask. About 50 ml of distilled water was added and gently refluxed for 6 to 8 hours. The solution was then cooled and diluted to exactly 250 ml with water in a volumetric flask. This was reserved for total soluble sulfate analysis, which is described below.

Probe Rinse - The probe wash was poured into a 250-ml volumetric flask. The sample bottle was rinsed with distilled water and the rinsings were added to the flask. The solution was then diluted to the mark with distilled water (or, if greater than 250 ml, the volume was measured). This solution was reserved for total soluble sulfate analysis, which is described below.

Total Soluble Sulfate Analysis--

A 15-ml aliquot* was drawn from the settled samples (filter and rinse) into separate sample containers with a clean, dry pipet (only solution was transferred, no solids; if necessary, a portion of the sample was centrifuged). The sulfate ion ($\text{SO}_4^{=}$) concentration in each aliquot was determined by ion chromatography (IC). A syringe was used to inject 1 ml of the aliquot into the 100- μ l sample loop of the IC, thereby flushing the loop with sample. The conductivity response of the sample was compared with the calibration curve to obtain the $\text{SO}_4^{=}$ concentration in mg/liter. Dilutions were prepared and reanalyzed if the initial response was out of the linear calibration range (i.e., greater than 15 mg/liter). Blank filter and water samples were prepared and analyzed in the same manner as the actual samples.

*The pipet is not rinsed. This is a deviation from normal procedures, but is necessary because the volume removed from the volumetric flask is required in the calculations.

Mass Determination--

Filter and Rinse Solution Preparation - The remaining contents of each volumetric flask (235 ml) were poured into separate tared 250-ml beakers, and the flask was rinsed with distilled water to transfer all particulate matter. The filter solution was in Beaker A and the rinse solution was in Beaker B. This solution was evaporated to approximately 100 ml at 105°C and allowed to cool before proceeding with the next analysis.

Filter and Rinse Solution Analysis - Five drops of phenolphthalein indicator were added to all the tared beakers. Concentrated NH_4OH was then added drop by drop until the solution turned pink. The samples were returned to the oven and evaporated to dryness at 105°C, then cooled in a desiccator and weighed to a constant weight. Results were reported to the nearest 0.1 mg. For this method, "constant weight" means a difference of no more than 0.5 mg or 1 percent of the total weight less beaker and/or filter tare, whichever is greater, between two consecutive weighings, with no less than 6 hours of desiccation time between weighings.

Calculations--

Nomenclature--

FP = weight of particulate* on the filter in Beaker A, mg

PRP = weight of probe rinse particulate* in Beaker B, mg

NWSSP = weight of nonwater-soluble sulfate particulate**, mg

AS_f = weight of ammonium sulfate in filter sample, mg

AS_{pr} = weight of AS in probe rinse sample, mg

V_{evap} = volume of solution evaporated in Beaker A (filter) or Beaker B (probe rinse), ml

C_{SO_4} = concentration of sulfate in filter or probe rinse solution aliquots, mg/liter

* Particulate with H_2SO_4 converted to $(\text{NH}_4)_2\text{SO}_4$.

** Particulate excluding water-soluble sulfates.

Equations--

$$FP(mg) = \text{gross weight Beaker A} - \text{tare weight Beaker A} - \text{filter tare weight} \quad \text{Eq. 1}$$

$$PRP(mg) = \text{Gross weight Beaker B} - \text{tare weight Beaker B} \quad \text{Eq. 2}$$

$$AS(mg) = C_{SO_4} (mg/liter) \times V_{\text{evap}} (ml) \times \frac{\text{liter}}{1000 \text{ ml}} \quad \text{Eq. 3}$$
$$\times 1.376 \left(\frac{mg \text{ AS}}{mg \text{ SO}_4} \right)$$

Mass of Nonwater-Soluble Sulfate Particulate

The sum of the particulate* collected on the filter (FP) and the particulate* collected in the probe rinse (PRP) is equal to the sum of nonwater-soluble sulfate particulate (NWSSP) and ammonium sulfate (AS) in both samples:

$$FP + PRP = NWSSP + AS_f + AS_{pr} \quad \text{Eq. 4}$$

The NWSSP can be found by rearranging the equation and substituting appropriate values determined by use of Equations 1, 2, and 3.

$$NWSSP = FP + PRP - AS_f - AS_{pr} \quad \text{Eq. 5}$$

Sulfuric Acid Mist Analysis

The amount of sulfuric acid that passed through the particulate filter was determined by analyzing the IPA solution recovered in the first two impingers and the backup filter. The volume of the sample solution was recorded, and the pH of the

* Particulate with H_2SO_4 converted to $(NH_4)_2SO_4$.

sample was determined. The sample volume was diluted to 500 ml with 80 percent IPA. A 100-ml aliquot of this solution was pipetted into a 250-ml Erlenmeyer flask with 2 to 3 drops of thorin indicator and titrated to a pink end point by using 0.0100 N barium perchlorate. If the end point color was not correct, the sample was passed through an ion exchange column and retitrated. A blank was titrated for each sample in the same manner.

Sulfur Dioxide Analysis

The hydrogen peroxide sample solution was diluted to 500 ml with deionized, distilled water. A 20-ml aliquot of this solution was pipetted into a 250-Erlenmeyer flask with 80 ml of 100 percent IPA and 2 to 3 drops of thorin indicator. The solution was then titrated to a pink end point by using 0.0100 N barium perchlorate. A blank was titrated in the same manner.

SECTION 4

SUMMARY OF TEST RESULTS

This section summarizes the results of the field sampling program. These results are presented to allow both within-run and between-run data comparisons, with emphasis on the thermogravimetric and water-soluble sulfate test results.

4.1 SAMPLE DATA

Table 4-1 summarizes pertinent sample data. All tests were conducted at a single point where the stack gas velocity profile was relatively flat. The actual probe and filter temperatures, stack temperature, and moisture content represent average values from each individual sample train. Gas composition data (O_2 and CO_2) are given in percent by volume on a dry basis. The isokinetic criteria defined in Reference Method 5* were met in almost every case, as indicated by the values shown in the far right-hand column. The isokinetic sampling rate for Run 3C reflects an adjustment for the post-test leak rate.

The sampling time for Runs 1 through 4 was 120 minutes; however, the sampling time for subsequent runs was shortened to make up for delays incurred during boiler condensate pump malfunctions. As indicated by the sample catch weights listed in

* 40 CFR 60, Appendix A, July 1982.

TABLE 4-1. SUMMARY OF SAMPLE CONDITIONS

Test No.	Date (1983) and time (24-h)	Train I.D.	Sample ^a type	Sample temperature, °C (°F)			Metered volume ^c dNm ³ (dscf)	Average stack temperature, °C (°F)	Moisture content, %	Average moisture, %	CO ₂ , %	O ₂ , %	Isokinetic sampling rate, %
				Probe		Filter ^b , actual							
				Desired	Actual								
1	2/7 0950-1150	1A	M5BW	160 (320)	162 (324)	161 (322)	1.940 (68.52)	153 (307)	11.3	11.3	13.4	2.4	103 104 99 104
		1B	M5BW	160 (320)	159 (318)	158 (317)	1.924 (67.93)		11.2				
		1C	M5B	160 (320)	158 (316)	161 (322)	1.820 (64.26)		11.5				
		1D	M5B	160 (320)	161 (321)	162 (324)	1.831 (64.66)		11.2				
2	2/7 1410-1610	2A	M5B	160 (320)	160 (319)	163 (325)	1.983 (70.04)	154 (310)	10.6	10.9	13.6	3.0	103 100 100 102
		2B	M5B	160 (320)	162 (324)	161 (322)	1.984 (70.07)		11.0				
		2C	M5BW	160 (320)	165 (328)	162 (324)	1.715 (60.56)		11.1				
		2D	M5BW	160 (320)	163 (307)	163 (325)	1.724 (60.88)		11.0				
3	2/8 0845-1045	3A	M5B	160 (320)	163 (326)	163 (326)	1.911 (67.50)	154 (310)	10.6	10.6	13.7	2.4	102 102 86 104
		3B ^d	M5B	160 (320)	162 (324)	166 (330)	1.891 (66.77)		10.6				
		3C ^d	M5B-P400	204 (400)	209 (407)	164 (327)	1.588 (56.09)		10.7				
		3D	M5B-P400	204 (400)	211 (412)	162 (324)	1.813 (64.02)		10.7				
4	2/8 1230-1430	4A	M5B-P400	204 (400)	209 (408)	167 (332)	1.973 (69.69)	159 (317)	10.7	10.8	13.6	2.3	100 102 99 102
		4B	M5B-P400	204 (400)	211 (412)	163 (325)	2.052 (72.47)		10.7				
		4C	M5B	160 (320)	164 (327)	163 (325)	1.727 (61.00)		10.8				
		4D	M5B	160 (320)	161 (321)	160 (319)	1.761 (62.19)		10.8				
5	2/11 0755-0925	5A	M5B	160 (320)	165 (329)	168 (334)	1.427 (50.39)	151 (304)	11.5	11.6	12.8	3.2	102 103 96 103
		5B	M5B	160 (320)	160 (319)	167 (332)	1.412 (49.88)		11.5				
		5C	M5B	160 (320)	161 (321)	164 (327)	1.311 (46.32)		11.8				
		5D	M5B	160 (320)	161 (322)	160 (319)	1.331 (46.99)		11.7				
6	2/11 1050-1220	6A	M5B	160 (320)	160 (319)	166 (330)	1.423 (50.26)	157 (314)	11.4	11.4	13.6	2.5	102 97 97 100
		6B	M5B	160 (320)	164 (326)	165 (329)	1.396 (49.31)		11.5				
		6C	M5B	160 (320)	161 (321)	161 (321)	1.211 (42.78)		11.5				
		6D	M5B	160 (320)	162 (324)	162 (324)	1.238 (43.72)		11.1				
7	2/11 1330-1500	7A	M5BW	160 (320)	167 (332)	166 (331)	1.411 (49.84)	159 (319)	11.3	11.2	13.4	2.6	101 102 98 106
		7B	M5B	160 (320)	161 (322)	166 (330)	1.396 (49.31)		11.1				
		7C	M5BW	160 (320)	161 (321)	159 (318)	1.339 (47.29)		11.4				
		7D	M5B	160 (320)	158 (317)	162 (323)	1.370 (48.40)		11.1				
8	2/11 1620-1650	8A	M5B	160 (320)	153 (307)	161 (321)	0.866 (30.59)	159 (319)	11.2	11.2	13.3	2.7	99 98 98 95
		8B	M5B-P400	204 (400)	207 (404)	166 (331)	0.829 (29.29)		11.3				
		8C	M5B	160 (320)	154 (309)	164 (327)	0.856 (30.22)		11.5				
		8D	M5B-P400	204 (400)	206 (403)	161 (321)	0.792 (27.99)		11.0				
9	2/12 0830-1000	9A	M5B	160 (320)	168 (335)	159 (318)	1.473 (52.00)	161 (321)	11.2	11.3	13.6	2.5	103 103 96 104
		9B	M5B	160 (320)	165 (328)	166 (331)	1.444 (50.99)		11.1				
		9C	M5B	160 (320)	161 (322)	160 (320)	1.348 (47.59)		11.6				
		9D	M5B	160 (320)	163 (326)	163 (326)	1.384 (48.86)		11.4				
10	2/12 1200-1330	10A	M5B	160 (320)	163 (325)	168 (335)	1.517 (53.59)	163 (326)	12.0	11.9	13.0	3.0	102 97 100 103
		10B	M5B-P400	204 (400)	210 (410)	170 (337)	1.491 (52.64)		11.5				
		10C	M5B	160 (320)	161 (322)	161 (321)	1.316 (46.48)		12.2				
		10D	M5B-P400	204 (400)	213 (415)	163 (325)	1.346 (47.52)		12.0				

^aM5B - Probe and filter heated to 160°C.

M5BW - Probe and filter heated to 160°C; water rinse of nozzle, probe, and filter holder.

M5B-P400 - Probe heated to 204°C; filter heated to 160°C.

^bAll desired filter temperatures were 160°C.^cSample volume in dry normal cubic meters (dNm³) at 20°C and 760 mmHg and in dry standard cubic feet (dscf) at 68°F and 29.92 in.Hg.^dThe sample volume, moisture content, and isokinetic sampling rate were adjusted to reflect a post-test leak rate of 0.06 cfm.

Table 4-2, an adequate amount of sample was still collected during the 90-minute runs. This was also true for Run 8, which was conducted with a larger nozzle size but stopped after approximately 30 minutes because the isokinetic sampling rate could not be maintained.

4.2 THERMOGRAVIMETRIC ANALYTICAL RESULTS

Table 4-2 presents the thermogravimetric analytical results. The filterable particulate values represent material collected in the sample probe and on the filter for each sample type (M5B, M5B-P400). All weights are reported in milligrams and sample concentrations in milligrams per dry normal cubic meter (mg/dNm^3).

The constant weight criteria described in Method 5* were achieved within two or three weighings during the ambient weighing on approximately 75 percent of the filter and probe rinse samples; however, the remaining samples did not meet the criteria after three weighings.

As previously noted, several selected samples were heat-conditioned at each temperature for either 6 or 24 hours (as indicated in the table) and then reheated at the same conditions until a stable weight was achieved prior to advancing to the next temperature in the analytical sequence. All samples were heated three times at 316°C (600°F). The stable weight criteria, which were defined as a difference of 5.0 mg or less between consecutive similar heat treatments (or 10 percent of the net sample

* 40 CFR 60, Appendix A, July 1982.

TABLE 4-2. SUMMARY OF THERMOGRAVIMETRIC ANALYTICAL RESULTS

Test No.	Train I.D.	Sample type	Filterable particulate following conditioning at indicated temperatures, °C (°F), mg							
			Ambient		160°C (320°F)		232°C (450°F)		316°C (600°F)	
			Probe	Filter	Probe	Filter	Probe	Filter	Probe	Filter
1	1A ^a	M5BW	-	-	-	-	-	-	-	-
	1B ^a	M5BW	-	-	-	-	-	-	-	-
	1C	M5B	125.8	210.9	102.3	181.3	98.1	168.0	62.4	132.4
	1D	M5B	110.2	199.1	95.0	170.6	90.6	160.4	84.1	142.0
2	2A ^b	M5B	161.0	228.7	141.3	196.6	136.4	190.2	41.2	181.0
	2B ^b	M5B	124.9	253.1	103.6	224.1	91.5	212.7	28.4	147.5
	2C ^a	M5BW	-	-	-	-	-	-	-	-
	2D ^a	M5BW	-	-	-	-	-	-	-	-
3	3A	M5B	119.7	237.2	108.7	202.4	103.6	194.6	77.4	173.7
	3B	M5B	149.2	227.4	137.1	195.3	131.6	185.5	81.7	160.0
	3C	M5B-P400	145.1	190.1	134.3	162.5	129.3	154.9	94.9	135.9
	3D	M5B-P400	106.5	244.9	96.4	217.9	93.8	206.5	60.5	185.2
4	4A	M5B-P400	173.6	225.3	165.7	203.4	162.7	195.0	117.3	174.2
	4B	M5B-P400	94.3	303.7	87.0	278.6	84.3	265.6	62.2	214.6
	4C	M5B	158.8	189.8	150.8	169.0	148.6	162.0	133.8	107.3
	4D	M5B	123.2	222.8	117.6	199.9	115.4	190.8	89.6	145.0
5	5A	M5B	75.6	159.9	64.0	137.2	56.4	129.0	39.3	113.3
	5B	M5B	71.1	159.8	58.3	137.7	53.6	129.2	32.4	87.6
	5C ^b	M5B	63.8	155.4	52.9	133.2	47.5	131.0	25.1	78.6
	5D ^b	M5B	64.9	153.0	51.1	132.4	43.8	129.9	20.6	92.7
6	6A ^b	M5B	69.4	159.9	-	-	41.9	140.9	20.3	107.2
	6B ^b	M5B	67.0	149.8	-	-	39.9	128.4	23.9	77.3
	6C	M5B	43.7	125.9	-	-	32.8	102.3	27.1	77.7
	6D	M5B	46.1	140.0	-	-	29.2	115.9	25.7	87.3
7	7A ^a	M5BW	-	-	-	-	-	-	-	-
	7B ^a	M5B	82.7	139.2	-	-	31.6	120.5	21.1	80.5
	7C ^a	M5BW	-	-	-	-	-	-	-	-
	7D	M5B	74.6	140.9	-	-	33.6	119.4	18.9	74.6

(continued)

TABLE 4-2 (continued)

Test No.	Train I.D.	Sample type	Filterable particulate following conditioning at indicated temperatures, °C (°F), mg							
			Ambient		160°C (320°F)		232°C (450°F)		316°C (600°F)	
			Probe	Filter	Probe	Filter	Probe	Filter	Probe	Filter
8	8A ^b	M5B	50.6	106.2	17.9	87.7	14.9	85.3	6.8	44.7
	8B	M5B-P400	23.8	87.7	12.5	75.4	10.3	69.0	6.5	52.6
	8C ^b	M5B	20.6	92.0	12.3	77.5	9.4	75.5	5.2	46.0
	8D	M5B-P400	21.6	83.9	10.5	74.8	8.6	65.6	5.8	49.9
9	9A ^b	M5B	84.9	168.0	-	-	-	-	19.3	98.2
	9B ^b	M5B	94.6	166.6	-	-	-	-	20.4	96.3
	9C	M5B	60.8	143.9	-	-	-	-	43.8	78.3
	9D	M5B	64.7	159.9	-	-	-	-	34.2	85.1
10	10A	M5B	108.8	151.8	-	-	72.8	130.3	50.5	107.3
	10B	M5B-P400	66.9	159.2	-	-	46.6	133.3	24.8	111.2
	10C	M5B	66.6	143.4	-	-	58.9	117.9	32.1	91.4
	10D	M5B-P400	64.8	149.0	-	-	53.1	128.5	24.5	100.2

^aM5BW samples were analyzed for total water soluble sulfates and particulate mass by modified Texas Air Board procedure described in Section 3 of this report.

^bHeated for 24 hours, all others heated for 6 hours.

weight, whichever was greater), were achieved in two treatments for selected samples heated at 160°C and 232°C. Several samples heated at 316°C for two treatments appeared to be stable according to the specified criteria, but others had significant weight losses, up to approximately 25 percent (50 mg) in one case. Note that this weight difference occurred between the first and second heat treatments at 316°C, not between two different temperatures. Because of this atypical behavior, all samples were heated a third time at 316°C, even if the stability criteria had been met after two treatments.

Table 4-3 presents the results of individual heatings at 316°C, including the sample weights after the last heating at 232°C as a reference. Approximately 25 percent of the samples did not meet the stability criteria after three heatings at 316°C. In some cases, samples that had met the criteria after two heatings failed to meet it after three heatings. There was no clear advantage to using a 24-h heating interval instead of a 6-h interval, based on the following observation: 14 of the 48 samples heated for 6-h intervals were classified unstable after three heatings at 316°C, and 5 of the 20 samples heated for 24-h intervals also were unstable.

Table 4-4 presents a comparison of total filterable particulate concentrations after heat conditioning at the indicated temperatures for the M5B and M5B-P400 samples. For reporting purposes, the results of similar sample types have been grouped together. The average concentration and standard deviation are

TABLE 4-3. NET SAMPLE WEIGHTS AFTER INDIVIDUAL HEAT TREATMENTS AT THE INDICATED TEMPERATURE

Run No.	Sample fraction ^a	Heating interval, h	Weight after last heating at 232°C (450°F), mg	Weight after indicated heating at 316°C (600°F), mg		
				First	Second	Third
1C	PR	6	98.1	82.7	69.9	62.4
1C	F	6	168.0	164.1	136.5	132.4
1D	PR	6	90.6	84.1	86.1	85.4
1D	F	6	160.4	144.1	142.0	142.5
3A	PR	6	103.6	96.2	95.2	77.4
3A	F	6	194.6	185.4	184.0	173.7
3B	PR	6	131.6	113.9	100.1	81.7
3B	F	6	185.5	183.7	176.9	160.0
3C	PR ^b	6	129.3	105.3	97.6	94.9
3C	F	6	154.9	140.7	139.8	135.9
3D	PR ^b	6	93.8	78.5	65.8	60.5
3D	F	6	206.5	197.3	186.9	185.2
4A	PR ^b	6	162.7	160.2	135.3	117.3
4A	F	6	195.0	181.6	175.3	174.2
4B	PR ^b	6	84.3	76.7	71.7	62.2
4B	F	6	265.6	248.2	236.3	214.6
4C	PR	6	148.6	139.4	135.5	133.8
4C	F	6	62.0	129.3	118.3	107.3
4D	PR	6	115.4	100.4	96.7	89.6
4D	F	6	190.8	161.9	148.1	145.0
5A	PR	6	56.4	54.5	45.0	39.3
5A	F	6	129.0	118.7	113.8	113.3
5B	PR	6	53.6	41.2	37.4	32.4
5B	F	6	129.2	89.8	87.6	88.2

(continued)

TABLE 4-3 (continued)

Run No.	Sample fraction ^a	Heating interval, h	Weight after last heating at 232°C (450°F), mg	Weight after indicated heating at 316°C (600°F), mg		
				First	Second	Third
6C	PR	6	32.8	28.9	31.2	27.1
6C	F	6	102.3	99.5	80.8	77.7
6D	PR	6	29.2	27.0	29.1	25.7
6D	F	6	115.9	103.9	97.5	87.3
7B	PR	6	31.6	26.7	24.2	21.1
7B	F	6	120.5	81.6	80.7	80.5
7D	PR	6	33.6	21.1	23.4	18.9
7D	F	6	119.4	83.5	75.1	74.6
8B	PR ^b	6	10.3	7.8	9.9	6.5
8B	F	6	69.0	53.4	52.6	53.7
8D	PR ^b	6	8.6	8.4	9.7	5.8
8D	F	6	65.6	62.4	54.2	49.9
9C	PR	6	c	46.6	44.7	43.8
9C	F	6	c	83.6	78.4	78.3
9D	PR	6	c	45.2	47.1	34.2
9D	F	6	c	90.9	85.3	85.1
10A	PR	6	72.8	58.1	59.7	50.5
10A	F	6	130.3	109.1	107.3	107.4
10B	PR ^b	6	46.6	40.2	28.3	24.8
10B	F	6	133.3	113.4	111.7	111.2
10C	PR	6	58.9	41.0	35.6	32.1
10C	F	6	117.9	96.3	91.4	91.4
10D	PR ^b	6	53.1	35.2	27.7	24.5
10D	F	6	128.5	113.5	100.5	100.2
2A	PR	24	136.1	57.7	51.2	41.2
2A	F	24	190.2	181.7	181.9	181.0
2B	PR	24	91.5	51.0	32.0	28.4
2B	F	24	213.1	201.7	151.8	147.5

(continued)

TABLE 4-3 (continued)

Run No.	Sample fraction ^a	Heating interval, h	Weight after last heating at 232°C (450°F), mg	Weight after indicated heating at 316°C (600°F), mg		
				First	Second	Third
5C	PR	24	47.5	34.7	25.6	25.1
5C	F	24	131.0	85.0	79.8	78.6
5D	PR	24	43.8	24.7	22.5	20.6
5D	F	24	129.9	114.0	105.4	92.7
6A	PR	24	41.9	35.3	34.2	20.3
6A	F	24	142.0	130.1	126.6	107.2
6B	PR	24	39.9	32.4	31.6	23.9
6B	F	24	128.4	81.2	77.3	77.5
8A	PR	24	14.9	7.8	6.8	7.4
8A	F	24	85.3	46.7	44.8	44.7
8C	PR	24	9.4	9.0	5.2	5.3
8C	F	24	75.5	48.7	47.3	46.0
9A	PR	24	c	26.2	20.6	19.3
9A	F	24	c	101.8	98.9	98.2
9B	PR	24	c	30.3	22.0	20.4
9B	F	24	c	99.5	97.2	96.3

^aPR = Probe rinse; F = Filter.

^bM5B-P400 run; all others are M5B runs.

^cSamples were not heated at 232°C.

TABLE 4-4. COMPARISON OF FILTERABLE PARTICULATE CONCENTRATION
AFTER HEAT CONDITIONING AT INDICATED TEMPERATURES^a

Run No.	Sample type	Ambient		160°C		232°C		316°C	
		Total weight, mg	Concentration, mg/dNm ³	Total weight, mg	Concentration, mg/dNm ³	Total weight, mg	Concentration, mg/dNm ³	Total weight, mg	Concentration, mg/dNm ³
1C	M5B	336.7	185.0	283.6	155.8	266.1	146.2	194.8	107.0
1D	M5B	309.3	168.9	265.6	145.1	251.0	137.0	226.1	123.5
2A ^b	M5B	389.7	196.5	337.9	170.4	326.6	164.7	222.2	112.0
2B ^b	M5B	378.0	190.5	327.7	165.2	304.2	153.3	175.9	88.7
3A	M5B	356.9	186.8	311.1	162.8	298.2	156.0	251.1	131.4
3B	M5B	376.6	199.2	332.4	175.8	317.1	167.7	241.7	127.8
4C	M5B	348.6	201.8	319.8	185.2	310.6	179.8	241.1	139.6
4D	M5B	346.0	196.5	317.5	180.3	306.2	173.9	234.6	133.2
5A	M5B	235.5	165.0	201.2	141.0	185.4	129.9	152.6	106.9
5B ^b	M5B	230.9	163.5	196.0	138.8	182.8	129.5	120.0	85.0
5C ^b	M5B	219.2	167.2	186.1	142.0	178.5	136.2	103.7	79.1
5D ^b	M5B	217.9	163.7	183.5	137.9	173.7	130.5	113.3	85.1
6A ^b	M5B	229.3	161.1	-	-	182.8	128.5	127.5	89.6
6B ^b	M5B	216.8	155.3	-	-	168.3	120.6	101.2	72.5
6C	M5B	169.6	140.0	-	-	135.1	111.6	104.8	86.5
6D	M5B	186.1	150.3	-	-	145.1	117.2	113.0	91.3
7B	M5B	221.9	159.0	-	-	152.1	109.0	101.6	72.8
7D	M5B	215.5	157.3	-	-	153.0	111.7	93.5	68.2
8A ^b	M5B	156.8	181.1	105.6	121.9	100.2	115.7	51.5	59.5
8C ^b	M5B	112.6	131.5	89.8	104.9	84.9	99.2	51.2	59.8
9A ^b	M5B	252.9	171.7	-	-	-	-	117.5	79.8
9B ^b	M5B	261.2	180.9	-	-	-	-	116.7	80.8
9C	M5B	204.7	151.8	-	-	-	-	122.1	90.6
9D	M5B	224.6	162.3	-	-	-	-	119.3	86.2

(continued)

TABLE 4-4 (continued)

Run No.	Sample type	Ambient		160°C		232°C		316°C	
		Total weight, mg	Concentration, mg/dNm ³	Total weight, mg	Concentration, mg/dNm ³	Total weight, mg	Concentration, mg/dNm ³	Total weight, mg	Concentration, mg/dNm ³
10A	M5B	260.6	171.8	-	-	203.1	133.9	157.8	104.0
10C	M5B	210.0	159.6	-	-	176.8	134.4	123.5	93.8
Average		169.9 $\sigma_d^c = 18.3$ N = 26		151.9 $\sigma = 23.0$ N = 14		135.7 $\sigma = 22.3$ N = 22		94.4 $\sigma = 22.5$ N = 26	
3C	M5B-P400	335.2	211.1	296.8	186.9	284.2	179.0	230.8	145.3
3D	M5B-P400	351.4	193.8	314.3	173.4	300.3	165.6	245.7	135.5
4A	M5B-P400	398.9	202.2	369.1	187.1	357.7	181.3	291.5	147.7
4B	M5B-P400	398.0	194.0	365.6	178.2	349.9	170.5	276.8	134.9
8B	M5B-P400	111.5	134.5	87.9	106.0	79.3	95.7	59.1	71.3
8D	M5B-P400	105.5	133.2	85.3	107.7	74.2	93.7	55.7	70.3
10B	M5B-P400	226.1	151.6	-	-	179.9	120.7	136.0	91.2
10D	M5B-P400	213.8	158.8	-	-	181.6	134.9	124.7	92.6
Average		172.4 $\sigma = 31.4$ N = 8		156.5 $\sigma = 38.8$ N = 6		142.7 $\sigma = 36.4$ N = 8		111.1 $\sigma = 33.1$ N = 8	

^aIncludes both filter and probe rinse fractions.

^bHeat conditioning intervals for these samples were 24 hours, all others were 6 hours.

^cStandard deviation with N-1 weighing for sample data.

^dNumber of data points.

given in mg/dNm^3 for all samples of a similar type and temperature. In addition, the number of data points at each temperature condition is shown. Figure 4-1 is a graphical representation of the average data.

Table 4-5 presents the statistical data for each set of grouped runs. Each group represents two runs of the same sample type conducted at the same time, except for run Groups 5, 6, and 9, which represent four similar samples. The M5B data are followed by the M5B-P400 data. Presented for each run group and temperature condition are the mean filterable particulate concentration, the standard deviation with N-1 weighting for sample data, and the relative standard deviation (RSD), which expresses the standard deviation as a percent of the mean concentration.

Table 4-6 summarizes the estimated precision for Methods 5B and 5B-P400 at each conditioning temperature. Method 5B precision data are presented on two bases; the first includes all available data (Runs 1 through 10), and the second includes only data from Runs 3, 4, 8, and 10 to allow a better comparison to within-run M5B-P400 data. The mean filterable concentrations were calculated by averaging grouped run values to weigh two- and four-run groups equally. The mean standard deviations were calculated by averaging standard deviation values for each set of grouped runs (from Table 4-5) to minimize the effect of temporal variation in emissions. In this way, the mean standard deviation of the grouped runs ($\bar{\sigma}$ in Table 4-6) more accurately reflects method precision than does the standard deviation of individual

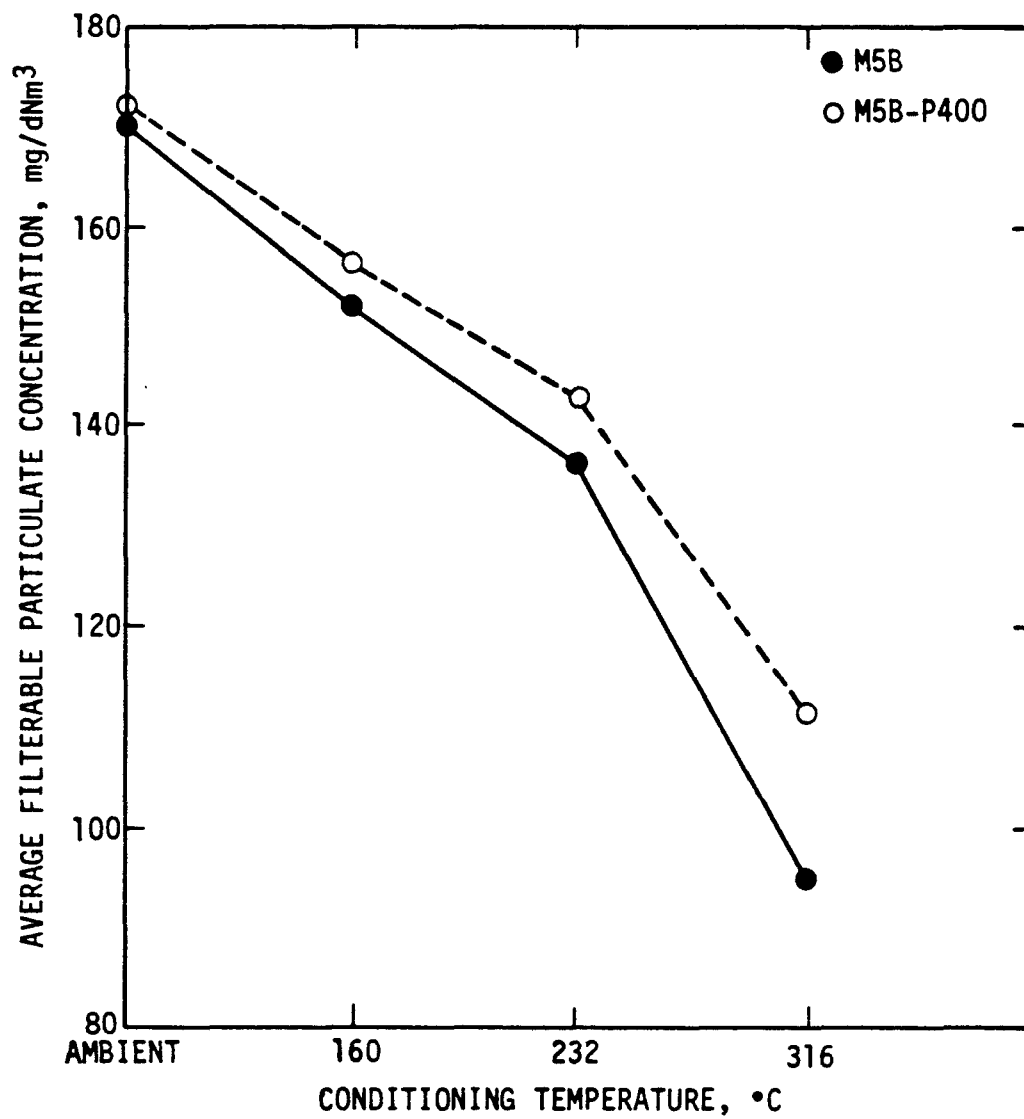


Figure 4-1. Average filterable particulate concentration for similar sample types after conditioning at indicated temperature.

TABLE 4-5. STATISTICAL DATA FOR GROUPED RUNS AFTER
CONDITIONING AT INDICATED TEMPERATURES

Run No.	Sample type	Ambient			160°C (320°F)			232°C (450°F)			316°C (600°F)		
		$\bar{x}$, ^a mg/dNm ³	σ , ^b mg/dNm ³	RSD, ^c %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %
1-C,D	M5B	177.0	11.4	6.4	150.4	7.6	5.1	141.6	6.5	4.6	115.3	11.6	10
2-A ^d ,B ^d	M5B	193.5	4.2	2.2	167.8	3.7	2.2	159.0	8.0	5.1	100.4	16.5	16
3-A,B	M5B	193.0	8.8	4.5	169.3	9.2	5.4	161.9	8.2	5.1	129.6	2.5	2.0
4-C,D	M5B	199.2	3.8	1.9	182.7	3.5	1.9	176.9	4.2	2.4	136.4	4.5	3.3
5-A ^d ,B ^d , C ^d ,D ^d	M5B	165.0	1.7	1.0	139.9	1.9	1.4	131.5	3.1	2.4	89.0	12.3	14
6-A ^d ,B ^d , C,D	M5B	151.7	8.9	5.9	-	-	-	119.4	7.1	5.9	85.0	8.6	10
7-B,D	M5B	158.1	1.2	0.7	-	-	-	110.3	1.9	1.7	70.5	3.2	4.5
8-A ^d ,C ^d	M5B	156.3	35.0	22	113.4	12.0	10.6	107.4	11.7	11	59.6	0.2	0.4
9-A ^d ,B ^d , C,D	M5B	166.7	12.5	7.5	-	-	-	-	-	-	84.3	5.0	6.0
10-A,C	M5B	165.7	8.6	5.2	-	-	-	134.1	0.3	0.2	98.9	7.2	7.3

(continued)

TABLE 4-5 (continued)

Run No.	Sample type	Ambient			160°C (320°F)			232°C (450°F)			316°C (600°F)		
		$\bar{x}$, ^a mg/dNm ³	σ , ^b mg/dNm ³	RSD, ^c %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %
3-C,D	M5B-P400	202.4	12.2	6.0	180.1	9.6	5.3	172.3	9.4	5.5	140.4	6.9	4.9
4-A,B	M5B-P400	198.1	5.8	2.9	182.6	6.3	3.4	175.9	7.6	4.3	141.3	9.1	6.4
8-B,D	M5B-P400	133.8	0.9	0.7	106.9	1.2	1.1	94.7	1.4	1.5	70.8	0.7	1.0
10-B,D	M5B-P400	155.2	5.1	3.3	-	-	-	127.8	10.1	7.9	91.9	1.0	1.1

^aMean filterable concentration.^bWithin-run standard deviation with N-1 weighting for sample data.^cRelative standard deviation is the standard deviation expressed as a percent of the mean concentration.^dSamples heated for 24-hour intervals; all others heated 6 hours.

TABLE 4-6. SUMMARY OF PRECISION ESTIMATES AFTER
CONDITIONING AT INDICATED TEMPERATURES

Run No.	Sample type	Ambient			160°C (320°F)			232°C (450°F)			316°C (600°F)		
		$\bar{x}$, ^a mg/dNm ³	σ , ^b mg/dNm ³	RSD, ^c %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %	$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %
1-10	M5B	172.6	9.6	5.6	153.9	6.3	4.1	138.0	5.7	4.1	96.9	7.2	7.4
		N ^d = 10			N = 6			N = 9			N = 10		
3,4, 8,10	M5B	178.5	14.1	7.9	155.2	8.2	5.3	145.1	6.1	4.2	106.1	3.6	3.4
		N = 4			N = 3			N = 4			N = 4		
3,4 8,10	M5B- P400	172.4	6.0	3.5	156.5	5.7	3.6	142.7	7.1	5.0	111.1	4.4	4.0
		N = 4			N = 3			N = 4			N = 4		

^aMean filterable concentration based on grouped run values.

^bMean standard deviation of grouped runs ($\frac{\sum \sigma_i}{N}$).

^cMean relative standard deviation (percent) calculated using the mean standard deviation and the mean filterable concentration of grouped runs.

^dN = number of data points.

run concentrations (σ in Table 4-4). The mean relative standard deviation expresses the mean standard deviation as a percent of the mean concentration. The number of data points included in each calculation is shown for consideration in evaluating the precision estimates.

Table 4-7 presents the relative percent weight loss for the filter samples after conditioning at the indicated temperatures. Percent weight loss was calculated in two ways; 1) by use of the ambient weight as the initial weight basis, and 2) by use of the weight after conditioning at 160°C (320°F) as the initial weight basis. The results of similar sample types have been grouped together. Tables 4-8 and 4-9 present similar data for the probe rinse samples and the total filterable samples, respectively. Figure 4-2 is a graphical representation of the average weight loss data on an ambient weight basis. The graph points out two characteristics of the tabulated data: 1) the most significant weight loss occurred during heating at 316°C (600°F), and 2) the pattern of relative percent weight loss upon heating was similar for all samples.

Because the fuel oil fired during the tests was known to have a relatively high vanadium content (~400 ppm by weight), vanadyl sulfate (VO_2SO_4) was suspected to be one of the components in the particulate matter. A sample of pure vanadyl sulfate was placed in a tared beaker and subjected to a series of heat treatments in the same manner as probe rinse samples. The resultant weight loss data did not follow the same pattern as the samples

TABLE 4-7. RELATIVE PERCENT WEIGHT LOSS FOR FILTER
SAMPLES AFTER CONDITIONING AT INDICATED TEMPERATURES

Run No.	Sample type	Net filter weights, mg				Relative weight loss ^a , %				
		Amb.	160°C	232°C	316°C	From ambient to:			From 160°C to:	
						160°C	232°C	316°C	232°C	316°C
1C	M5B	210.9	181.3	168.0	132.4	14	20	37	7	27
1D	M5B	199.1	170.6	160.4	142.0	14	19	29	6	17
2A	M5B	228.7	196.6	190.2	181.0	14	17	21	3	8
2B	M5B	253.1	224.1	212.7	147.5	11	16	42	5	34
3A	M5B	237.2	202.4	194.6	173.7	15	18	27	4	14
3B	M5B	227.4	195.3	185.5	160.0	14	18	30	5	18
4C	M5B	189.8	169.0	162.0	107.3	11	15	43	4	37
4D	M5B	222.8	199.9	190.8	145.0	10	14	35	5	27
5A	M5B	159.9	137.2	129.0	113.3	14	19	29	6	17
5B ^b	M5B	159.8	137.7	129.2	87.6	14	19	45	6	36
5C ^b	M5B	155.4	133.2	131.0	78.6	14	16	49	2	41
5D ^b	M5B	153.0	132.4	129.9	92.7	13	15	39	2	30
6A ^b	M5B	159.9	-	140.9	107.2	-	12	33	-	-
6B ^b	M5B	149.8	-	128.4	77.3	-	14	48	-	-
6C	M5B	125.9	-	102.3	77.7	-	19	38	-	-
6D	M5B	140.0	-	115.9	87.3	-	17	38	-	-
7B	M5B	139.2	-	120.5	80.5	-	13	42	-	-
7D	M5B	140.9	-	119.4	74.6	-	15	47	-	-
8A ^b	M5B	106.2	87.7	85.3	44.7	17	20	58	3	49
8C ^b	M5B	92.0	77.5	75.5	46.0	16	18	50	3	41
9A ^b	M5B	168.0	-	-	98.2	-	-	42	-	-
9B ^b	M5B	166.6	-	-	96.3	-	-	42	-	-
9C	M5B	143.9	-	-	78.3	-	-	46	-	-
9D	M5B	159.9	-	-	85.1	-	-	47	-	-

(continued)

TABLE 4-7 (continued)

Run No.	Sample type	Net filter weights, mg				Relative weight loss ^a , %				
						From ambient to:			From 160°C to:	
		Amb.	160°C	232°C	316°C	160°C	232°C	316°C	232°C	316°C
10A	M5B	151.8	-	130.3	107.3	-	14	29	-	-
10C	M5B	143.4	-	117.9	91.4	-	18	36	-	-
M5B average		169.0	160.0	142.0	104.0	14	17	39	3	15
3C	M5B-P400	190.1	162.5	154.9	135.9	15	19	29	5	16
3D	M5B-P400	244.9	217.9	206.5	185.2	11	16	24	5	15
4A	M5B-P400	225.3	203.4	195.0	174.2	10	13	23	4	14
4B	M5B-P400	303.7	278.6	265.6	214.6	8	13	29	5	23
8B	M5B-P400	87.7	75.4	69.0	52.6	14	21	40	8	30
8D	M5B-P400	83.9	74.8	65.6	49.9	11	22	41	12	33
10B	M5B-P400	159.2	-	133.3	111.2	-	16	30	-	-
10D	M5B-P400	149.0	-	128.5	100.2	-	14	33	-	-
M5B-P400 average		180.0	169.0	152.0	128.0	11	17	31	5	17

^aWeight loss, % = $\frac{\text{Weight @ } T_1 - \text{Weight @ } T_2}{\text{Weight @ } T_1} \times 100$; where $T_1 < T_2$.

^bHeat conditioning intervals for these samples were 24 hours, all others were 6 hours.

TABLE 4-8. RELATIVE PERCENT WEIGHT LOSS FOR PROBE RINSE
SAMPLES AFTER CONDITIONING AT INDICATED TEMPERATURES

Run No.	Sample type	Net probe rinse weights, mg				Relative weight loss ^a , %				
						From ambient to:			From 160°C to:	
		Amb.	160°C	232°C	316°C	160°C	232°C	316°C	232°C	316°C
1C	M5B	125.8	102.3	98.1	62.4	19	22	50	4	39
1D	M5B	110.2	95.0	90.6	84.1	14	18	24	5	11
2A ^b	M5B	161.0	141.3	136.4	41.2	12	15	74	3	71
2B ^b	M5B	124.9	103.6	91.5	28.4	17	27	77	12	73
3A	M5B	119.7	108.7	103.6	77.4	9	13	35	5	29
3B	M5B	149.2	137.1	131.6	81.7	8	12	45	4	40
4C	M5B	158.8	150.8	148.6	133.8	5	6	16	1	11
4D	M5B	123.2	117.6	115.4	89.6	5	6	27	2	24
5A	M5B	75.6	64.0	56.4	39.3	15	25	48	12	39
5B ^b	M5B	71.1	58.3	53.6	32.4	18	25	54	8	44
5C ^b	M5B	63.8	52.9	47.5	25.1	17	26	61	10	53
5D ^b	M5B	64.9	51.1	43.8	20.6	21	33	68	14	60
6A ^b	M5B	69.4	-	41.9	20.3	-	40	71	-	-
6B ^b	M5B	67.0	-	39.9	23.9	-	40	64	-	-
6C	M5B	43.7	-	32.8	27.1	-	25	38	-	-
6D	M5B	46.1	-	29.2	25.7	-	37	44	-	-
7B	M5B	82.7	-	31.6	21.1	-	62	74	-	-
7D	M5B	74.6	-	33.6	18.9	-	55	75	-	-
8A ^b	M5B	50.6	17.9	14.9	6.8	65	71	87	17	62
8C ^b	M5B	20.6	12.3	9.4	5.2	40	54	75	24	58
9A ^b	M5B	84.9	-	-	19.3	-	-	77	-	-
9B ^b	M5B	94.6	-	-	20.4	-	-	78	-	-
9C	M5B	60.8	-	-	43.8	-	-	28	-	-
9D	M5B	64.7	-	-	34.2	-	-	47	-	-

(continued)

TABLE 4-8 (continued)

Run No.	Sample type	Net probe rinse weights, mg				Relative weight loss ^a , %				
						From ambient to:			From 160°C to:	
		Amb.	160°C	232°C	316°C	160°C	232°C	316°C	232°C	316°C
10A	M5B	108.8	-	72.8	50.5	-	33	54	-	-
10C	M5B	66.6	-	58.9	32.1	-	12	52	-	-
M5B average		88	87	67	41	19	30	56	5	24
3C	M5B-P400	145.1	134.3	129.3	94.9	7	11	35	4	29
3D	M5B-P400	106.5	96.4	93.8	60.5	9	12	43	3	37
4A	M5B-P400	173.6	165.7	162.7	117.3	5	6	32	2	29
4B	M5B-P400	94.3	87.0	84.3	62.2	8	11	34	3	29
8B	M5B-P400	23.8	12.5	10.3	6.5	47	57	73	18	48
8D	M5B-P400	21.6	10.5	8.6	5.8	51	60	73	18	45
10B	M5B-P400	66.9	-	46.6	24.8	-	30	63	-	-
10D	M5B-P400	64.8	-	53.1	24.5	-	18	62	-	-
M5B-P400 average		87	84	74	50	21	26	52	6	27

^aWeight loss, % = $\frac{\text{Weight @ } T_1 - \text{Weight @ } T_2}{\text{Weight @ } T_1} \times 100$; where $T_1 < T_2$.

^bHeat conditioning intervals for these samples were 24 hours, all others were 6 hours.

TABLE 4-9. RELATIVE PERCENT WEIGHT LOSS FOR TOTAL FILTERABLE PARTICULATE SAMPLES AFTER CONDITIONING AT INDICATED TEMPERATURES

Run No.	Sample type	Total net weights, mg				Relative weight loss ^a , %				
		Amb.	160°C	232°C	316°C	From ambient to:			From 160°C to:	
						160°C	232°C	316°C	232°C	316°C
1C	M5B	336.7	283.6	266.1	194.8	16	21	42	6	31
1D	M5B	309.3	265.6	251.0	226.1	14	19	27	5	15
2A ^b	M5B	389.7	337.9	326.6	222.2	13	16	43	3	34
2B ^b	M5B	378.0	327.7	304.2	175.9	13	20	53	7	46
3A	M5B	356.9	311.1	298.2	251.1	13	16	30	4	19
3B	M5B	376.6	332.4	317.1	241.7	12	16	36	5	27
4C	M5B	348.6	319.8	310.6	241.1	8	11	31	3	25
4D	M5B	346.0	317.5	306.2	234.6	8	12	32	4	26
5A	M5B	235.5	201.2	185.4	152.6	15	21	35	8	24
5B ^d	M5B	230.9	196.0	182.8	120.0	15	21	48	7	39
5C ^d	M5B	219.2	186.1	178.5	103.7	15	19	53	4	44
5D ^b	M5B	217.9	183.5	173.7	113.3	16	20	48	5	38
6A ^b	M5B	229.3	-	182.8	127.5	-	20	44	-	-
6B ^b	M5B	216.8	-	168.3	101.2	-	22	53	-	-
6C	M5B	169.6	-	135.1	104.8	-	20	38	-	-
6D	M5B	186.1	-	145.1	113.0	-	22	39	-	-
7B	M5B	221.9	-	152.1	101.6	-	31	54	-	-
7D	M5B	215.5	-	153.0	93.5	-	29	57	-	-
8A ^b	M5B	156.8	105.6	100.2	51.5	33	36	67	5	51
8C ^b	M5B	112.6	89.8	84.9	51.2	20	25	55	5	43
9A ^b	M5B	252.9	-	-	117.5	-	-	54	-	-
9B ^b	M5B	261.2	-	-	116.7	-	-	55	-	-
9C	M5B	204.7	-	-	122.1	-	-	40	-	-
9D	M5B	224.6	-	-	119.3	-	-	47	-	-

(continued)

TABLE 4-9 (continued)

Run No.	Sample type	Total net weights, mg				Relative weight loss ^a , %				
						From ambient to:			From 160°C to:	
		Amb.	160°C	232°C	316°C	160°C	232°C	316°C	232°C	316°C
10A	M5B	260.6	-	203.1	157.8	-	22	39	-	-
10C	M5B	210.0	-	176.8	123.5	-	16	41	-	-
M5B average		256	247	209	145	15	21	45	3	18
3C	M5B-P400	335.2	296.8	284.2	230.8	11	15	31	4	22
3D	M5B-P400	351.4	314.3	300.3	245.7	11	15	30	4	22
4A	M5B-P400	398.9	369.1	357.7	291.5	7	10	27	3	21
4B	M5B-P400	398.0	365.6	349.9	276.8	8	12	30	4	24
8B	M5B-P400	111.5	87.9	79.3	59.1	21	29	47	10	33
8D	M5B-P400	105.5	85.3	74.2	55.7	19	30	47	13	35
10B	M5B-P400	226.1	-	179.9	136.0	-	20	40	-	-
10D	M5B-P400	213.8	-	181.6	124.7	-	15	42	-	-
M5B-P400 average		268	253	226	178	13	18	37	5	20

$$^a \text{Weight loss, \%} = \frac{\text{Weight @ } T_1 - \text{Weight @ } T_2}{\text{Weight @ } T_1} \times 100; \text{ where } T_1 < T_2.$$

^bHeat conditioning intervals for these samples were 24 hours, all others were 6 hours.

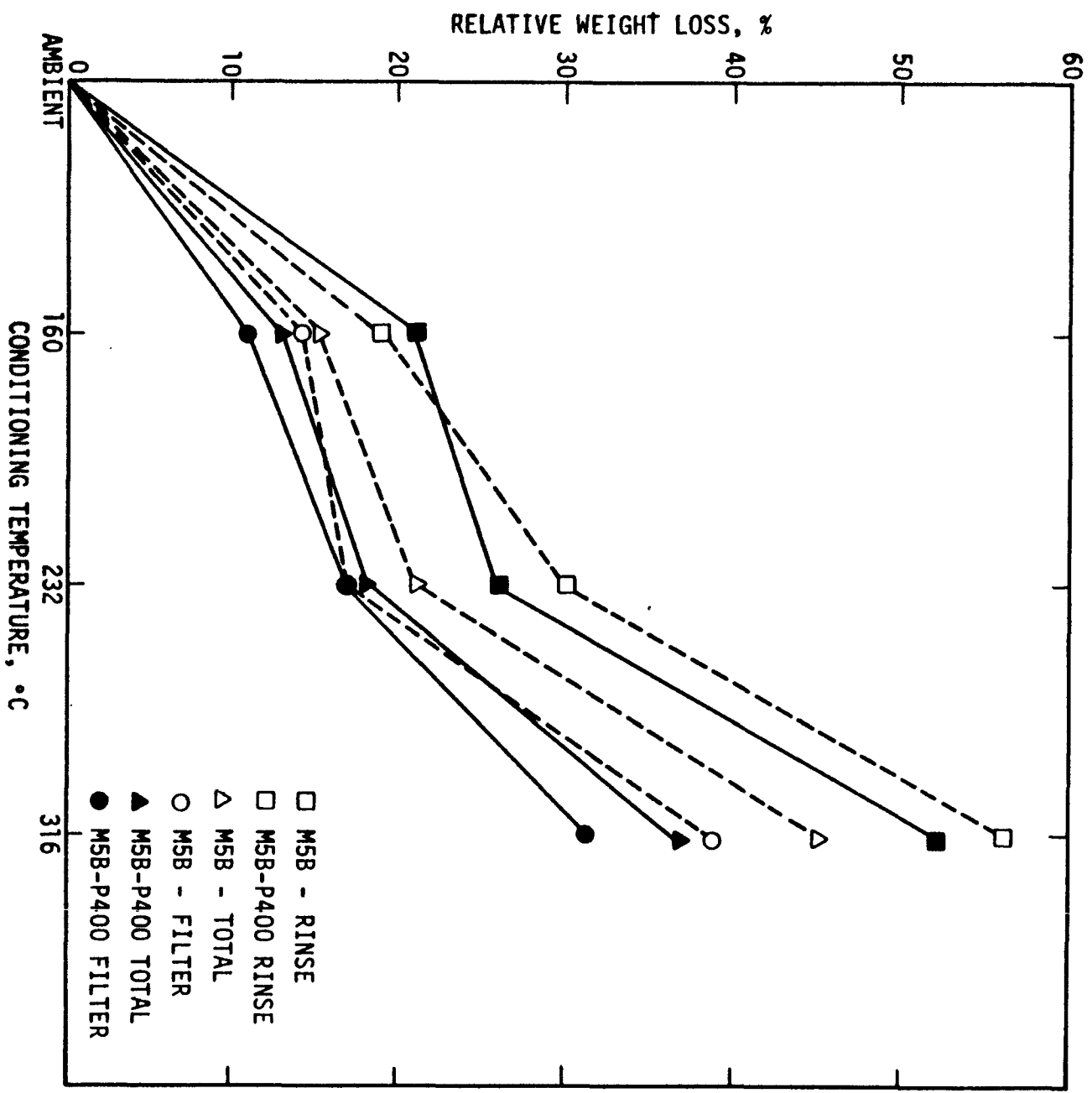


Figure 4-2. Average relative percent weight loss after conditioning at indicated temperatures - ambient weight basis.

in this report, but typified other thermogravimetric analyses that show that the most significant weight loss occurs upon the initial heating at 160°C (320°C).

The filter and probe rinse samples underwent a series of changes in appearance before and during thermogravimetric analysis. Upon recovery in the field, all filters were described as having a green coating. Some filters also had black spots or granular particulate matter. Prior to being desiccated in the laboratory, the filters were described generally as having black specks or black shining spots with a green perimeter. Some filters also had green specks. One filter had a light green glossy surface. During the heatings at 316°C the particulate on the filters turned gradually to a yellow-colored material. The probe rinse samples were basically dark initially, but after heating at 316°C, some of the probe rinse beakers contained some yellow powder along with a black granular particulate matter.

Vanadyl sulfate ($\text{VOSO}_4 \cdot n\text{H}_2\text{O}$) is a brilliant blue; upon heating at 160°C it turned a dull bluish green; upon heating at 316°C it gradually changed to a greenish yellow.

4.3 WATER-SOLUBLE SULFATE ANALYTICAL DATA

Table 4-10 summarizes the nonwater-soluble sulfate particulate (NWSSP) results of the Method 5BW tests. Since particulate matter cannot be determined gravimetrically in the presence of sulfuric acid because of the inexact amount of water retained by the acid, the method is designed to convert the acid to a non-hygroscopic, nonvolatile product, in this case ammonium sulfate.

TABLE 4-10. SUMMARY OF NONWATER-SOLUBLE SULFATE PARTICULATE RESULTS^a

Run No.	Weight, mg			Total filterable concentration, mg/dNm ³	Statistical data for gaseous runs			Comparison grouped within-runs M5B samples after heating to 316°C	
	Filter	Probe rinse	Total		$\bar{x}$, mg/dNm ³	σ , mg/dNm ³	RSD, %	Run No.	$\bar{x}$, mg/dNm ³
1A	74.5	85.8	160.3	82.6	84.6	2.8	3.3	1C, 1D	115.3
1B	83.9	82.7	166.6	86.6					
2C	94.4	83.5	177.9	103.7	104.4	0.9	0.9	2A, 2B	100.4 ^b
2D	98.7	82.3	181.0	105.0					
7A	28.8	53.3	82.1	58.2	60.8	3.7	6.2	7B, 7D	70.5
7C	33.3	51.7	85.0	63.5					
Average = 83.3						Average = 95.4			

^aNWSSP results of the Method 5BW tests using Texas Air Board procedures modified by the use of ion chromatography to measure water-soluble sulfate concentrations.

^bThe samples for Runs 2A and 2B had a higher relative weight loss than similar samples during the heatings at 316°C.

The acid is measured as water-soluble sulfate and converted to ammonium sulfate. The weight of ammonium sulfate formed is subtracted from the total weight of ammonium sulfate and NWSSP (particulate excluding water-soluble sulfates). Results of within-run Method 5B samples are presented for comparison.

As shown in Table 4-10, the average Method 5BW results were lower than the Method 5B results for samples that had been heated to 316°C (600°F). Method precisions were comparable.

The difference in results between the two methods indicates that the Method 5B samples contain water-soluble sulfates that are not easily volatilized by heating at 316°C. It may be possible to identify any cations associated with the residual sulfate by analyzing water extracts of the samples by ion chromatography. Another approach would consist of heating several samples to a higher temperature to determine additional weight loss and stability.

4.4 METHOD 8 ANALYTICAL RESULTS

Table 4-11 presents the results of back-half analyses for sulfates as H_2SO_4 and SO_2 . As expected, the H_2SO_4 data show a higher degree of variability than the SO_2 data, which show a high degree of precision. There is no apparent difference in the H_2SO_4 data between the two methods.

TABLE 4-11. SUMMARY OF BACK-HALF ANALYSES

Test No.	Train I.D.	Sample type	H ₂ SO ₄ ^a		SO ₂ ^b	
			mg	mg/dNm ³	mg	mg/dNm ³
1	1A	M5BW	66.2	34.1	7224	3720
	1B	M5BW	62.6	32.5	7055	3670
	1C	M5B	58.9	32.4	6652	3650
	1D	M5B	58.5	32.0	6467	3530
2	2A	M5B	36.6	18.5	7135	3600
	2B	M5B	29.7	15.0	7678	3870
	2C	M5BW	44.0	25.7	6376	3720
	2D	M5BW	24.2	14.0	6427	3730
3	3A	M5B	49.3	25.8	7124	3730
	3B	M5B	49.3	26.1	7031	3720
	3C	M5B-P400	58.9	37.1	5827	3670
	3D	M5B-P400	53.4	29.4	6797	3750
4	4A	M5B-P400	25.9	13.1	7362	3731
	4B	M5B-P400	24.8	12.1	7678	3740
	4C	M5B	24.8	14.4	6667	3860
	4D	M5B	18.8	10.7	6703	3810
5	5A	M5B	35.5	24.9	5398	3780
	5B	M5B	36.8	26.1	5301	3750
	5C	M5B	28.6	21.8	5008	3820
	5D	M5B	29.8	22.4	5059	3800
6	6A	M5B	38.0	26.7	5278	3710
	6B	M5B	36.5	26.1	5144	3680
	6C	M5B	53.0	43.8	4546	3750
	6D	M5B	24.6	19.9	4518	3650
7	7A	M5BW	52.4	37.1	5087	3610
	7B	M5B	42.6	30.5	5026	3600
	7C	M5BW	47.6	35.5	4800	3580
	7D	M5B	53.6	39.1	4955	3620

(continued)

TABLE 4-11 (continued)

Test No.	Train I.D.	Sample type	H ₂ SO ₄ ^a		SO ₂ ^b	
			mg	mg/dNm ³	mg	mg/dNm ³
8	8A	M5B	31.9	36.8	3037	3510
	8B	M5B-P400	62.8	75.8	2967	3580
	8C	M5B	71.6	83.6	3062	3580
	8D	M5B-P400	46.8	59.1	2763	3490
9	9A	M5B	102.1	69.3	5266	3580
	9B	M5B	84.3	75.8	5198	3580
	9C	M5B	104.1	77.2	4928	3660
	9D	M5B	99.9	72.2	5001	3610
10	10A	M5B	77.5	51.1	5465	3600
	10B	M5B-P400	81.9	54.9	5121	3430
	10C	M5B	92.8	70.5	4834	3670
	10D	M5B-P400	70.7	52.5	4916	3650

^aSulfate analysis (as H₂SO₄) per Method 8 (40 CFR 60, Appendix A, July 1, 1981) of IPA impinger contents, back-half filter, and rinse.

^bSO₂ analysis per Method 8 of peroxide impinger contents and rinse.

SECTION 5

DISCUSSION OF TEST RESULTS

The data both differ and agree with previous studies that characterize condensible sulfate bias of particulate measurements at source emission streams containing sulfur oxides.^{2,4,5,6} These studies have shown that sample temperature is a parameter that significantly affects the retention of condensible material in the front half of the standard Method 5 sample train. In this case, condensible matter is defined as probe rinse/filter residue that can be removed by heating. Sulfate species will most likely exist in sources containing sulfur oxides. Water-soluble sulfate can exist in these sources in many different chemical forms. Sulfuric acid (H_2SO_4) is the most common form, but salts of ammonium, sodium, or other cations are also possible. Because exit gas streams from boilers are known to contain sulfur trioxide and sulfur dioxide, sulfuric acid is the most probable form of water-soluble sulfate. Vanadyl sulfate also can be formed during the combustion of high-vanadium residual fuel oils, although the precise effect of this compound on measurements of particulate matter is not completely known.

Data presented in Tables 4-2 and 4-4 show that the use of a higher probe sample temperature did not have a significant effect on the measurement of particulate emissions from this source.

The M5B samples collected at 160°C (320°F) were expected to have a higher particulate catch in the probe rinse than the M5B-P400 samples, which were collected at a probe temperature of 204°C (400°F) and a filter temperature of 160°C; however, this effect was not exhibited. The M5B filterable particulate concentration averaged 170 mg/dNm³ at ambient conditions and compared very well with the M5B-P400 average of 172 mg/dNm³.

Data presented in Table 4-3 show that samples were atypically unstable (according to specified criteria) between heat treatments at the higher temperatures. The variability in weight loss between samples at the same temperature suggests that 316°C may be close to the reaction or decomposition temperature of materials present in the samples.

Effects of analytical temperature are shown graphically in Figure 4-1. The average M5B and M5B-P400 particulate concentrations are similar at each of the three stages of heat conditioning from 160°C (320°F) through 316°C (600°F). The M5B sample concentrations averaged 152, 136, and 94 mg/dNm³ after conditioning at 160°, 232°, and 316°C, respectively. Corresponding results of the M5B-P400 runs at these three temperatures were 156, 143, and 111 mg/dNm³. These data differ from results presented in previous studies in that the most significant sample weight loss normally occurs during the initial heat treatment at 160°C, with subsequent decreasing losses (i.e., the slope of the concentration versus temperature curve becomes flatter). The sample in this study showed a relatively small percent weight loss until they were heated to 316°C, which results in a steeper curve.

An examination of within-run samples (as presented in Table 4-6) shows a closer comparison between the two methods. For Runs 3, 4, 8, and 10, the M5B sample concentrations averaged 155, 145, and 106 mg/dNm³ after conditioning at 160°, 232°, and 316°C, respectively. Corresponding results of the M5B-P400 runs at these three temperatures were 156, 143, and 111 mg/dNm³. The apparent increasing difference between the two methods at higher temperatures is probably related to the increasing instability of the samples.

Weight loss data presented in Tables 4-7 through 4-9 and Figure 4-2 show that both probe rinse and filter samples of each method type lost significant percentages of their ambient weights upon heating, although individual samples varied greatly. The M5B and M5B-P400 filter samples had average weight losses of 39 and 31 percent after thermal treatment at 316°C. This close comparison was expected because the sample filtration temperatures were both 160°C. These percentage weight losses correspond to approximately 65 and 52 mg, respectively.

The M5B and M5B-P400 probe rinse samples had average weight losses of 56 and 52 percent after thermal treatment at 316°C. These percentages correspond to approximately 47 and 37 mg, respectively.

The sample weight loss curve shown in Figure 4-2 begins to flatten out between 160°C and 232°C in a manner similar to previous studies. The abrupt departure from expected behavior at a temperature of 316°C supports the possibility of being close to a reaction temperature of components in the particulate matter.

Statistical data for grouped runs in Tables 4-5 and 4-6 show the precision estimates for Methods 5B and M5B-P400. For a given group of two or four runs, the within-run precision generally worsened between the heat treatments at 232° and 316°C, probably as a result of increased instability of the samples. The mean standard deviation for all 10 M5B run groups was 9.6 mg/dNm³ at ambient conditions, which corresponds to a relative standard deviation (RSD) of 5.6 percent. The four M5B-P400 run groups had a mean standard deviation of 6.0 mg/dNm³ and a corresponding RSD of 3.5 percent at ambient conditions.

The mean standard deviation for the six M5B run groups heated to 160°C was 6.3 mg/dNm³, with a corresponding RSD of 4.1 percent, which indicated a slight improvement over results at ambient conditions. For the three M5B-P400 run groups heated to 160°C, the mean standard deviation and RSD were 5.7 mg/dNm³ and 3.6 percent, respectively.

Precision data for the nine M5B run groups heated to 232°C included a mean standard deviation of 5.7 mg/dNm³ and an RSD of 4.1 percent. For the four M5B-P400 run groups, the average standard deviation and RSD were 7.1 mg/dNm³ and 5.0 percent, respectively.

Precision data for the 10 M5B groups heated to 316°C included a mean standard deviation of 7.2 mg/dNm³ and an RSD of 7.4 percent. For the four M5B-P400 samples, the mean standard deviation and RSD were 4.4 mg/dNm³ and 4.0 percent, respectively.

All of these statistical results indicate a high degree of precision for the majority of samples.

Results of the six M5BW samples and within-run M5B samples presented in Table 4-10 show the disparity between the two methods. The reported nonwater-soluble sulfate particulate (NWSSP) values represent particulate concentrations corrected for water-soluble sulfates determined by ion chromatography (IC). The average NWSSP concentration (83.3 mg/dNm^3) is significantly lower than the average particulate concentration of the within-run M5B samples heated to 316°C (95.4 mg/dNm^3).

A maximum bias of 6 percent (low) could be introduced to the NWSSP value determined by the IC analytical procedure if all of the collected particulate was water-soluble. This is because the aliquot removed for IC analysis is equal to 6 percent of the sample, and the NWSSP result is not corrected for particulate in the aliquot that is water-soluble and nonsulfate. The actual amount of bias is independent of the water-soluble sulfate, but depends on the makeup of the NWSSP. The NWSSP can consist of nonwater-soluble particulate (NWSP) and water-soluble particulate that is not sulfate (WSPNS). Extreme examples of these types of materials would be sand (NWSP) and sodium chloride (WSPNS). If the NWSSP consisted of 75 percent sand and 25 percent salt, the NWSSP results reported from the use of the IC procedure would be biased low by 1.5 percent (6 percent of the WSPNS). For most boiler exhaust gases, the amount of WSPNS in the particulate and the resultant bias to the reported NWSSP should be relatively low.

These NWSSP results indicate that a portion of the water-soluble sulfate initially present in the ambient samples either is not sulfuric acid or it effectively prevents sulfuric acid from being released upon heating to 316°C. It is possible that vanadium present in the fuel oil is responsible for the atypical weight loss results.

As a test for residual sulfates or determination of interfering cations, several of the M5B samples that have been heated to 316°C can be extracted with water for subsequent analysis by IC. Additionally, several of the remaining M5B samples can be heated to 400°C to determine if any additional weight loss is observed.

SECTION 6

QUALITY ASSURANCE

Because the goal of testing is to produce representative emission results, quality assurance is one of the main facets of stack sampling. Quality assurance guidelines provide the detailed procedures and actions necessary for defining and producing acceptable data. Four such documents were used in this test program to ensure the collection of acceptable data and to provide a definition of unacceptable data. These documents are 1) the Source-Specific Test Plan prepared by PEDCo and reviewed by Emission Measurement Branch; 2) the EPA Quality Assurance Handbook Volume III, EPA-600/4-77-027, 3) the PEDCo Environmental Emission Test Quality Assurance Plan, and 4) the PEDCo Environmental Laboratory Quality Assurance Plan. The last two, which are PEDCo's general guideline manuals, define the company's standard operating procedures and are followed by the emission testing groups and the laboratory groups.

Appendix F provides more detail on the quality assurance procedures, such as QA objectives; data reduction; quality control checks; performance and system audits; preventive maintenance; precision, accuracy, and completeness; corrective action; and quality assurance reports to management.

Relative to this specific test program, the following steps were taken to ensure that the testing and analytical procedures produced quality data.

- ° Calibration of all field sampling equipment. (Appendix E describes calibration guidelines in more detail.)
- ° Checks on train configuration and calculations.
- ° Onsite quality assurance checks such as leak checks on the sampling train, pitot tube, and Orsat line, and quality assurance checks of all test equipment prior to use.
- ° Use of designated analytical equipment and sampling reagents.

Table 6-1 lists the sampling equipment used for quad-train particulate and SO₂ testing as well as the calibration guidelines and limits. In addition to the pre- and post-test calibrations, a field audit was performed on the meter boxes used for the sampling. PEDCo constructed critical orifices for use in this audit. Figures 6-1a through 6-1d show audit runs for each dry gas meter used for testing. Figures 6-2a and 6-2b show thermocouple digital indicator audit runs. Figures 6-3a through 6-3d show thermometer and thermocouple audit data collected during pretest equipment checks.

Between runs, onsite preliminary calculation checks were performed to verify isokinetic sampling rates and to compare moisture contents and other parameters with expected values. These checks were used to ensure that the tests were conducted properly. An example isokinetic calculation sheet is shown in Figure 6-4.

TABLE 6-1. FIELD EQUIPMENT CALIBRATION

Equipment	I.D. No.	Calibrated against	Allowable error	Actual error	Within allowable limits	Comments
Meter boxes	FB-4 FB-5 FB-6 FB-7	Wet test meter	$Y \pm 0.02 Y$ $\Delta H \theta \pm 0.15$ ($Y \pm 0.05 Y$ post-test)	0.003 0.004 0.003 0.000	X X X X	$Y \pm 0.05 Y$ post-test
Pitot tubes	278 379	Standard pitot tube	See Appendix E		X X	
Digital indicators	124 125	Millivolt signals	0.5%	0.27% 0.11%	X X	
Thermocouples and stack thermometer	178 206	ASTM-2F or 3F	1.5%	1.0% 1.0%	X X	
Orsat analyzer	141	Standard gas	$\pm 0.5\%$	0.3%	X	
Impinger thermometers	447 448 449 450	ASTM-2F or 3F	$\pm 2^\circ\text{F}$	2°F 1.5°F 1.5°F 2.0°F	X X X X	
Balance	M-1	Type S weights	$\pm 0.5 \text{ g}$	0.27 g	X	
Barometer	229	NBS traceable barometer	$\pm 0.10 \text{ in.Hg}$ (0.20 post-test)	0.01 in.Hg	X	
Dry gas thermometers	FB-4 FB-5 FB-6 FB-7	ASTM-2F or 3F	$\pm 5^\circ\text{F}$	1.0°F 2.2°F 1.1°F 2.5°F	X X X X	Inlet and outlet averaged
Probe nozzles	1A 1B 1C 1D	Caliper	$D_n \pm 0.004 \text{ in.}$	0.002 0.001 0.001 0.003	X X X X	
	2A 2B 2C 2D			0.001 0.001 0.001 0.001	X X X X	
	8A 8B 8C 8D			0.002 0.002 0.000 0.002	X X X X	

AUDIT REPORT DRY GAS METER

DATE: 2/6/83

CLIENT: USERA

BAROMETRIC PRESSURE (P_{bar}): 30.2 in. Hg

METER BOX NO. FB 4 TRAIN D

ORIFICE NO. 21

PRETEST γ : 1.030

ORIFICE K FACTOR: 5.206×10^{-4}

AUDITOR: PR

Orifice manometer reading ΔH in H_2O	Dry gas meter reading V_i/V_f ft^3	Temperatures			Duration of run $\emptyset$ min
		Ambient T_{ai}/T_{af} $^{\circ}F$	Dry gas meter		
			Inlet T_{ii}/T_{if} $^{\circ}F$	Outlet T_{oi}/T_{of} $^{\circ}F$	
2.30	595.900	69	73	70	13 min 57 34 sec
	606.300	69	74	70	

Dry gas meter volume V_m ft^3	Average temperatures		V_{mstd} ft^3	V_{mact} ft^3	Audit γ	γ deviation %
	Ambient T_a $^{\circ}F$	Dry gas meter T_m $^{\circ}F$				
10.410	68	72	10.477	10.747	1.026	-0.4

V_{mstd}	V_{mact}
$\frac{(17.647)(V_m)(P_{bar} + \Delta H/13.6)}{(T_m + 460)}$	$\frac{(1203)(\emptyset)(K)(P_{bar})}{(T_a + 460)^{1/2}}$
10.477	10.747

Audit γ	γ deviation, %
$\frac{V_{mact}}{V_{mstd}}$	$\frac{(\gamma_{audit} - \gamma_{pre-test})(100\%)}{(\gamma_{audit})}$
1.026	-0.4%

Audit γ must be in the range, pre-test $\gamma \pm 0.05 \gamma$

Figure 6-1a. Audit report dry gas meter.

AUDIT REPORT DRY GAS METER

DATE: 2/6/83

CLIENT: USEPA

BAROMETRIC PRESSURE (P_{bar}): 30.2 in. Hg

METER BOX NO. FB-5 TRAIN C

ORIFICE NO. 5

PRETEST γ : 0.983

ORIFICE K FACTOR: 5.412×10^{-4}

AUDITOR: Paul Reimerman

Orifice manometer reading ΔH in H_2O	Dry gas meter reading V_i/V_f ft^3	Temperatures			Duration of run ϕ min
		Ambient T_{ai}/T_{af} $^{\circ}F$	Dry gas meter		
			Inlet T_{ii}/T_{if} $^{\circ}F$	Outlet T_{oi}/T_{of} $^{\circ}F$	
2.45	026.700	68	77	72	12 min 0.058 3.5 sec
	037.200	68	78	72	

Dry gas meter volume V_m ft^3	Average temperatures		V_{mstd} ft^3	V_{mact} ft^3	Audit γ	γ deviation %
	Ambient T_a $^{\circ}F$	Dry gas meter T_m $^{\circ}F$				
10.500	68	75	10.52	10.32	0.981	-0.2%

V_{mstd}	V_{mact}
$\frac{(17.647)(V_m)(P_{bar} + \Delta H/13.6)}{(T_m + 460)}$	$\frac{(1203)(\phi)(K)(P_{bar})}{(T_a + 460)^{1/2}}$
10.52	10.32

Audit γ	γ deviation, %
$\frac{V_{mact}}{V_{mstd}}$	$\frac{(\gamma_{audit} - \gamma_{pre-test})(100\%)}{(\gamma_{audit})}$
0.981	-0.2%

Audit γ must be in the range, pre-test $\gamma \pm 0.05 \gamma$

Figure 6-1b. Audit report dry gas meter.

AUDIT REPORT DRY GAS METER

DATE: 2/2/83
 BAROMETRIC PRESSURE (P_{bar}): 30.2 in. Hg
 ORIFICE NO. 3
 ORIFICE K FACTOR: 5.435 x 10⁻⁴

CLIENT: USEPA
 METER BOX NO. FB 6 Train B
 PRETEST γ : 0.960
 AUDITOR: Dr. R. R. R.

Orifice manometer reading ΔH in H ₂ O	Dry gas meter reading V_i/V_f ft ³	Temperatures			Duration of run $\emptyset$ min
		Ambient T_{ai}/T_{af} °F	Dry gas meter		
			Inlet T_{ii}/T_{if} °F	Outlet T_{oi}/T_{of} °F	
1.92	937.0	67	70	65	13.32
	948.800	67	72	65	

Dry gas meter volume V_m ft ³	Average temperatures		V_{mstd} ft ³	V_{mact} ft ³	Audit γ	γ deviation %
	Ambient T_a °F	Dry gas meter T_m °F				
11.800	67	69	11.94	11.46	0.960	0

V_{mstd}	V_{mact}
$\frac{(17.647)(V_m)(P_{bar} + \Delta H/13.6)}{(T_m + 460)}$	$\frac{(1203)(\emptyset)(K)(P_{bar})}{(T_a + 460)^{1/2}}$
11.94	11.46

Audit γ	γ deviation, %
$\frac{V_{mact}}{V_{mstd}}$	$\frac{(\gamma_{audit} - \gamma_{pre-test})(100\%)}{(\gamma_{audit})}$
0.960	0

Audit γ must be in the range, pre-test $\gamma \pm 0.05 \gamma$

Figure 6-1c. Audit report dry gas meter.

AUDIT REPORT DRY GAS METER

DATE: 2/6/83
 BAROMETRIC PRESSURE (P_{bar}): _____ in. Hg
 ORIFICE NO. 10
 ORIFICE K FACTOR: 4.189×10^{-7}

CLIENT: USEPA
 METER BOX NO. FB-7 TRAIN A
 PRETEST γ : 1.003
 AUDITOR: Paul Reinermann

Orifice manometer reading ΔH in H_2O	Dry gas meter reading V_i/V_f ft^3	Temperatures			Duration of run ϕ min
		Ambient T_{ai}/T_{af} $^{\circ}F$	Dry gas meter		
			Inlet T_{ii}/T_{if} $^{\circ}F$	Outlet T_{oi}/T_{of} $^{\circ}F$	
1.80	411.000	68	76	72	14.70
	422.200	69	77	72	

Dry gas meter volume V_m ft^3	Average temperatures		V_{mstd} ft^3	V_{mact} ft^3	Audit γ	γ deviation %
	Ambient T_a $^{\circ}F$	Dry gas meter T_m $^{\circ}F$				
1.20	68	74	11.23	11.13	0.991	-1.2%

V_{mstd}	V_{mact}
$\frac{(17.647)(V_m)(P_{bar} + \Delta H/13.6)}{(T_m + 460)}$	$\frac{(1203)(\phi)(K)(P_{bar})}{(T_a + 460)^{1/2}}$
11.227	11.13

Audit γ	γ deviation, %
$\frac{V_{mact}}{V_{mstd}}$	$\frac{(\gamma_{audit} - \gamma_{pre-test})(100\%)}{(\gamma_{audit})}$
0.991	-1.2%

Audit γ must be in the range, pre-test $\gamma \pm 0.05 \gamma$

Figure 6-1d. Audit report dry gas meter.

**THERMOCOUPLE DIGITAL INDICATOR
AUDIT DATA SHEET**

CCS 124

Date 2/6/83 Indicator No. TRAIN C+D ~~ENTER~~ Operator PR

Test Point No.	Millivolt signal*	Equivalent temperature, °F*	Digital indicator temperature reading, °F	Difference, %
1		32	29	0.6
2		102.2	93.7	0.6
3		451.1	448.2	0.3
4		1127	1127	0.0

ALL SWITCHES OKAY

$\overline{AVG} = 0.4$

Percent difference must be less than or equal to 0.5%.

Percent difference:

$$\frac{(\text{Equivalent temperature } ^\circ R - \text{Digital indicator temperature reading } ^\circ R)(100\%)}{(\text{Equivalent temperature } ^\circ R)}$$

Where $^\circ R = ^\circ F + 460^\circ F$

* These values are to be obtained from the calibration data sheet for the calibration device.

Figure 6-2a. Thermocouple digital indicator audit data sheet.

**THERMOCOUPLE DIGITAL INDICATOR
AUDIT DATA SHEET**

Date 2/6/83 Indicator No. 125 Operator PK
TRAINS A+B

Test Point No.	Millivolt signal*	Equivalent temperature, °F*	Digital indicator temperature reading, °F	Difference, %
1		32	33.2	0.2
2		102.2	102.3	0.0
3		451.1	451.1	0.0
4		1127	1128	0.0

ALL SWITCHES OKAY

AVG = 0.0

Percent difference must be less than or equal to 0.5%.

Percent difference:

$$\frac{(\text{Equivalent temperature } ^\circ\text{R} - \text{Digital indicator temperature reading } ^\circ\text{R})(100\%)}{(\text{Equivalent temperature } ^\circ\text{R})}$$

Where $^\circ\text{R} = ^\circ\text{F} + 460^\circ\text{F}$

* These values are to be obtained from the calibration data sheet for the calibration device.

Figure 6-2b. Thermocouple digital indicator audit data sheet.

ON-SITE AUDIT DATA SHEET

Audit Name: F13-7 TRH/A 2/6/83 Date: 2/6/83 Auditor: PR

Equipment	Reference	Reference Value	Value Determined	Deviation	Max. Allowable Deviation
Meter box inlet thermo.	ASTM-3F at ambient temp.	68	69	1	5°F
Meter box outlet thermo.	ASTM-3F at ambient temp.	68	68	0	5°F
Impinger #777	ASTM-3F at ambient temp.	68	62	6	2°F
Stack #178 thermometer or Thermocouple <i>Filter - Probe</i>	ASTM-3F at ambient temp.	96	92	4	7°F
	ASTM-3F at stack temp.	92	8792	5	See table
Orsat analyzer	% O ₂ in ambient air	20.8%			0.7%
Trip balance	IOLM std. weight				0.5 grams
Barometer	Corrected* NWS value				0.20 in. Hg

Reference temp. °F	32-140	141-273	274-406	407-540	541-673	674-760
Max. deviation °F	7	9	11	13	15	17

* Correction factor:

NWS value (in. Hg) - [Altitude (ft)/1000(ft/in. Hg)] + 0.74 in. Hg**

** 0.74 in. Hg is the nominal correction factor for the reference barometer against which the field barometer was calibrated.

If it is not feasible to perform the audit on any piece of equipment, record "N/A" in the space provided for the data.

Figure 6-3a. On-site audit data sheet.

ON-SITE AUDIT DATA SHEET

Audit Name: FB - 6 TRIN B Date: 2/6/83 Auditor: PR

Equipment	Reference	Reference Value	Value Determined	Deviation	Max. Allowable Deviation
Meter box inlet thermo.	ASTM-3F at ambient temp.	68	65	3	5°F
Meter box outlet thermo.	ASTM-3F at ambient temp.	68	66	2	5°F
Impinger #444 thermometer	ASTM-3F at ambient temp.	68	64	4	2°F
Stack #200 thermometer or Thermocouple	ASTM-3F at ambient temp.	88	91	3	7°F
	ASTM-3F at stack temp.	94	97	3	See table
Orsat analyzer	% O ₂ in ambient air	20.8%			0.7%
Trip balance	IOLM std. weight				0.5 grams
Barometer	Corrected* NWS value				0.20 in. Hg

Reference temp. °F	32-140	141-273	274-406	407-540	541-673	674-760
Max. deviation °F	7	9	11	13	15	17

* Correction factor:

$$\text{NWS value (in. Hg)} - [\text{Altitude (ft)} / 1000(\text{ft/in. Hg})] + 0.74 \text{ in. Hg}^{**}$$

** 0.74 in. Hg is the nominal correction factor for the reference barometer against which the field barometer was calibrated.

If it is not feasible to perform the audit on any piece of equipment, record "N/A" in the space provided for the data.

Figure 6-3b. On-site audit data sheet.

ON-SITE AUDIT DATA SHEET

Audit Name: FIB 5 TRKIN ~~C~~ Date: 2/6/83 Auditor: PR

Equipment	Reference	Reference Value	Value Determined	Deviation	Max. Allowable Deviation
Meter box inlet thermo.	ASTM-3F at ambient temp.	68	68	0	5°F
Meter box outlet thermo.	ASTM-3F at ambient temp.	68	69	1	5°F
Impinger #450 thermometer	ASTM-3F at ambient temp.	68	64	4	2°F
Stack thermometer or Thermocouple	ASTM-3F at ambient temp.				7°F
	ASTM-3F at stack temp.	96	98	4	See table
Orsat analyzer	% O ₂ in ambient air	20.8%			0.7%
Trip balance	IOLM std. weight				0.5 grams
Barometer	Corrected* NWS value				0.20 in. Hg

Reference temp. °F	32-140	141-273	274-406	407-540	541-673	674-760
Max. deviation °F	7	9	11	13	15	17

* Correction factor:

NWS value (in. Hg) - [Altitude (ft)/1000(ft/in. Hg)] + 0.74 in. Hg**

** 0.74 in. Hg is the nominal correction factor for the reference barometer against which the field barometer was calibrated.

If it is not feasible to perform the audit on any piece of equipment, record "N/A" in the space provided for the data.

Figure 6-3c. On-site audit data sheet.

ON-SITE AUDIT DATA SHEET

Audit Name: F3 + TRAIN D Date: 2/6/83 Auditor: PR

Equipment	Reference	Reference Value	Value Determined	Deviation	Max. Allowable Deviation
Meter box inlet thermo.	ASTM-3F at ambient temp.	68	66°F	2	5°F
Meter box outlet thermo.	ASTM-3F at ambient temp.	68	66°F	2	5°F
Impinger #448 thermometer	ASTM-3F at ambient temp.	68	62	6	2°F
Stack thermometer or Thermocouple	ASTM-3F at ambient temp.				7°F
	ASTM-3F at stack temp.	94	94	0	See table
Orsat analyzer	% O ₂ in ambient air	20.8%			0.7%
Trip balance	IOLM std. weight				0.5 grams
Barometer	Corrected* NWS value				0.20 in. Hg

Reference temp. °F	32-140	141-273	274-406	407-540	541-673	674-760
Max. deviation °F	7	9	11	13	15	17

* Correction factor:

NWS value (in. Hg) - [Altitude (ft)/1000(ft/in. Hg)] + 0.74 in. Hg**

** 0.74 in. Hg is the nominal correction factor for the reference barometer against which the field barometer was calibrated.

If it is not feasible to perform the audit on any piece of equipment, record "N/A" in the space provided for the data.

Figure 6-3d. On-site audit data sheet.

ISOKINETIC CALCULATION

SITE U.S. EPA

TEST NO. 4

		RUN 4A	RUN 4B	RUN 4C	RUN 4D
1. Volume of dry gas sampled corrected to standard conditions. Note: V must be corrected for leakage if any leakage rates exceed L_g. $V_{m, std} = 17.65 \times V_m \times Y \left[\frac{P_{bar} + \frac{\Delta H}{13.6}}{T_m} \right]$	V_m, ft^3	67.961	73.022	60.527	58.395
	Y	1.003	0.960	0.983	1.030
	$P_{bar}, in. Hg$	30.36	30.36	30.36	30.36
	$\Delta H, in. H_2O$	1.032	0.952	0.89	0.89
	$T_m, ^\circ R$	524.5	519.5	525.25	517.0
	$V_{m, std}, dscf$	69.814	72.481	60.83	62.365
Volume of water vapor at standard conditions, ft^3. $V_{w, std} = 0.04707 V_{lc}$	V_{lc}, g	177.7	184.4	156.3	159.4
	$V_{w, std}, ft^3$	8.36	8.68	7.36	7.52
Moisture content in stack gas. $B_{ws} = \frac{V_{w, std}}{V_{m, std} + V_{w, std}}$	B_{ws}	0.107	0.107	0.108	0.10
	$1 - B_{ws}$	0.893	0.893	0.892	0.895
Dry molecular weight of stack gas, lb/lb-mole. $M_d = 0.440 (\% CO_2) + 0.320 (\% O_2) + 0.280 (\% N_2 + \% CO)$	$\% CO_2$	13.6	13.6	13.6	13.6
	$\% CO_2$	2.3	2.3	2.3	2.3
	$\% N_2 + \% CO$	84.1	84.1	84.1	84.1
	$M_d, lb/lb-mole$	30.27	30.27	30.27	30.27
Molecular weight of stack gas. $M_s = M_d (1 - B_{ws}) + 18 B_{ws}$	$M_s, lb/lb-mole$	29.08	29.08	28.95	28.96
Stack velocity at stack conditions, fps. $V_s = 85.49 C_p \left(\text{avg. } \sqrt{\Delta P} \right) \sqrt{\frac{T_s}{P_s M_s}}$	$P_{static}, in. H_2O$	-0.6	0.6	0.6	0.6
	$P_s, in. Hg$	30.32	30.32	30.32	30.3
	$T_s, ^\circ R$	777.3	777.3	777.3	777
	$\sqrt{\Delta P}$	0.849	0.849	0.849	0.849
	C_p	0.84	0.84	0.84	0.84
	V_s, fps	57.24	57.24	57.37	57.36
Isokinetic variation $\% I = \frac{V_{m, std} \times T_s \times 17.32}{V_s \times D_n \times 0 \times P_s \times (1 - B_{ws})}$	$D_n, in.$	0.224	0.227	0.211	0.210
	$\theta, min.$	120	120	120	120
	$\% I$	100.7	101.8	98.8	102.0

Figure 6-4. Isokinetic calculations.

As a check on the reliability of the method used to analyze particulate samples, sets of filters that had been preweighed in the lab and acetone blanks were submitted for thermogravimetric analysis in a manner similar to the actual samples. Table 6-2 summarizes the results of blank filter and reagent analyses.

Audit solutions prepared by EPA were used to check the analytical procedures and reagents for SO₂ sampling analysis. Table 6-3 presents the results of this analytical audit. Table 6-4 summarizes the results of SO₂ reagent blank analyses. The audit test and blank analyses show that the analytical techniques were good.

Filter and deionized water blanks were analyzed to check the reliability of the analytical methods used to determine nonwater-soluble sulfate particulate. Table 6-5 presents the results of the blank reagent analyses.

The sampling equipment, reagents, and analytical procedures for this test series were in compliance with all necessary guidelines set forth for accurate test results as described in Volume III of the Quality Assurance Handbook.*

* Quality Assurance Handbook for Air Pollution Measurement Systems, Volume III, EPA-600/4-77-027b, August 1977.

TABLE 6-2. THERMOGRAVIMETRIC REAGENT BLANK ANALYSIS

Sample type	I.D. No.	Initial volume, ml	Net blank weight, mg			
			Ambient	160°C	232°C	316°C
Filter - (Whatman RA 934AH)	CT341	NA	0.2	-0.3	-0.1	0.2
	CT832	NA	0.3	NA	NA	0.3
Acetone	CT881	368	0.6	1.1	0.2	-0.3
Acetone	CT882	372	4.3	NA	NA	0.5

NA = Not applicable

TABLE 6-3. AUDIT REPORT SO₂ ANALYSIS

Plant USEPA PN Number 3530-15
 Date samples received 2-18-83 Date analyzed 3-1-83
 Samples analyzed by Craig Skel
 Reviewed by John Bennett Date of Review 3-2-83

Sample Number	mg SO ₂ /dscm Determined	Source of Sample	Accepted Value	% Difference
#1805 Lot 8480 (CT493)	1134.2	T. Wagner	1143.4	-0.6%
#1808 Lot 8480 (CT494)	376.5	T. Wagner	381.3	-1.3%

(continued)

TABLE 6-3 (continued)

Plant WFF PN Number 113 15
 Date samples received 5 18 83 Date analyzed 8 3 83
 Samples analyzed by George Smith
 Reviewed by Tim B. [unclear] JPL Date of Review 8 5 83

Sample Number	mg SO ₂ /dscm Determined	Source of Sample	Accepted Value	% Difference
114.3 #115	1140.7	T. Wagner	1140.1	+ 0.5 %
114.4 #116	317.5	T. Wagner	381.3	+ 4.2 %

TABLE 6-4. SO₂ REAGENT BLANK ANALYSES

Sample type	I.D. No.	Net blank weight, mg	
		as SO ₂	as H ₂ SO ₄
80% IPA	CT944	-	<0.3
80% IPA/Filter	CT943	-	<0.2
10% Hydrogen peroxide	CT991	<0.3	-
	CT992	<0.3	-
Water	CT901	<0.3	-
	CT902	<0.2	-

TABLE 6-5. NONWATER-SOLUBLE SULFATE PARTICULATE
REAGENT BLANK ANALYSIS

Sample type	I.D. No.	Net weight of particulate plus ammonium sulfate, mg	C _{SO₄} ^a , mg/liter	V _{evap} , ml	NWSSP blank weight, mg
Filter	CT889	2.8	1.98	235	2.2
Acetone	CT901	0.8	<1.00	305	0.8
Filter	CT890	1.1	1.91	235	0.5
Acetone	CT902	1.3	<1.00	215	1.3
Filter	CT883	3.6	1.89	235	3.0
Acetone	CT897	3.1	1.55	235	2.6
Filter	CT898	2.8	<1.00	235	2.8
Acetone	CT899	2.7	<1.00	235	2.7
Acetone	CT900	3.1	2.24	235	2.4

^aA 15-ml aliquot was removed from sample for ion chromatography analysis.

SECTION 7

REFERENCES

1. PEDCo Environmental, Inc. Laboratory Evaluation Report - Analytical Method for Determining the Particulate Weight of EPA Method 5 Exclusive of Water-Soluble Particulate. Method Development and Testing for FCCU Regenerators. EPA Contract No. 68-02-3546, Work Assignment No. 14. October 1982.
2. PEDCo Environmental, Inc. Emission Test Report. Method Development and Testing for FCCU Regenerators. EPA Contract No. 68-02-3546, Work Assignment No. 14. December 1982.
3. Mitchell, W. J., and M. R. Midgett. A Means to Evaluate the Performance of Stationary Source Test Methods. Environmental Science and Technology, 10:85-88, 1976.
4. Oldaker, G. B. Condensibile Particulate and Its Impacts on Particulate Measurements. Draft Report, EPA Contract No. 68-01-4148, Task No. 69. May 1980.
5. Peters, E. T., and J. W. Adams. Sulfur Dioxide Interaction With Filters Used for Method 5 Stack Sampling. In: Workshop Proceedings on Primary Sulfate Emissions From Combustion Sources, Volume I - Measurement Technology. EPA-600/9-78-020a, 1978. pp. 199-202.
6. Cushing, K. W. Particulate Sampling in Process Streams in the Presence of Sulfur Dioxide. In: Workshop Proceedings on Primary Sulfate Emissions From Combustion Sources, Volume I - Measurement Technology. EPA-600/9-78-020a, 1978. pp. 202-227.

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APPENDIX A

COMPUTER PRINTOUTS AND EXAMPLE CALCULATIONS

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/07/83
RUN NUMBER 1AM5BW

SAMPLE TYPE PARTIC S03 S02
OPERATOR PR RA
AMBIENT TEMP.(DEG.F) 63.
BAR.PRESS.(IN.HG) 30.06
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531017
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TURE COEFF. .84
THERM. NO.
LEAKAGE .000 CFM @ 10.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE 1A : I.D. .223
ASSUMED MOISTURE 10.0
SAMPLE BOX NUMBER
METER BOX NUMBER F87
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1161.9

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
				-----				-----				
				DESIRED ACTUAL				INLET OUTLET				
INIT	0	950	436.809									
	10.0	0	442.715	.710	1.08	1.08	305.	63.	62.	4.0	330.	49.
	20.0	0	448.212	.710	1.08	1.08	306.	64.	62.	4.0	319.	49.
	30.0	0	453.974	.710	1.08	1.08	307.	67.	62.	4.5	330.	49.
	40.0	0	459.541	.650	.99	.99	305.	70.	62.	5.0	332.	47.
	50.0	0	464.999	.650	.98	.98	307.	72.	62.	6.0	310.	47.
	60.0	0	471.123	.680	1.03	1.03	308.	72.	62.	6.0	311.	49.
	70.0	0	476.434	.680	1.03	1.03	309.	74.	64.	6.5	319.	48.
	80.0	0	482.099	.680	1.03	1.08	307.	74.	64.	6.5	317.	48.
	90.0	0	487.859	.700	1.06	1.06	309.	74.	65.	7.5	325.	48.
	100.0	0	493.419	.650	.98	.98	308.	74.	65.	8.0	328.	48.
	110.0	0	498.932	.650	.98	.98	308.	73.	66.	8.0	328.	48.
	120.0	1150	504.527	.650	.98	.98	308.	74.	65.	8.5	315.	51.
TOTALS	120.0		67.718									
AVERAGE					1.02	1.03	307.	71.	63.	6.2	322.	48.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA

TEST 1A5BN UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/07/83	02/07/83

TB	TIME-START	950	950
TF	TIME-FINISH	1150	1150
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.223 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.03 IN-H2O	26.1 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	67.718 CU-FT	1.918 CU-M
TM	AVERAGE GAS METER TEMP	67.2 F	19.5 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	68.519 SCF	1.940 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	184.9	184.9
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.703 SCF	.246 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.27	11.27
FMD	MOLE FRACTION DRY GAS	.887	.887
PCO2	PERCENT CO2 BY VOL., DRY	13.35	13.35
PO2	PERCENT O2 BY VOL., DRY	2.45	2.45
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.20	84.20
MD	MOLECULAR WT-DRY STACK GAS	30.23	30.23

A-3

MWS	MOLECULAR WT-STACK GAS	28.86		28.86	
PB	BAROMETRIC PRESSURE	30.06	IN-HG	763.52	MM-HG
PSI	STATIC PRES OF STACK GAS	-.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.02	IN-HG	762.40	MM-HG
TS	AVERAGE STACK TEMP	307.	F	153.	C
VS	AVG STACK GAS VELOCITY	55.6	FPS	16.9	MPS
AS	STACK AREA	20612.	SQ-IN	13.29A	SQ-M
QSSD	STACK FLOW RATE, DRY*	17546932.	SCFH	496877.	SCMH
QS	ACTUAL STACK FLOW RATE	28644928.	ACFH	811139.	ACMH
ISO	PERCENT ISOKINETIC	103.0		103.0	
MN	AMBIENT PARTICULATE MG. EPA 5	100.0		100.0	
CS	AMBIENT PARTICULATE	.0225	GR/DSCF*	51.545	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.1AM5BW

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 67.718 * 1.003 * (30.06 + 1.029 / 13.6)}{(67. + 460.)} = 68.519 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 185. = 8.70 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 8.70}{68.519 + 8.70} = 11.27 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.3}{100.} = .887$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.35*44/100) + (2.4*32/100) + ((84.2+ .0) * 28/100 = 30.23$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO/100)) + 18. * (BWO/100)$$

$$MWS = 30.23 * (1. - (11.27/100)) + 18. * (11.27/100) = 28.86$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 273.377 / (\text{SQRT}(28.86 * 30.02) * 12. = 55.59 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.59 * 20612. 3600/144 = 28644928. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28644928. * 30.02 * (1. - (11.27/100))}{(307. + 460.)} = 17546932. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (307. + 460.)) * ((0.002669 * 185.) + (67.718 * 1.003 * (30.06 + (1.029/13.6)) / (67. + 460.)))}{120. * 55.59 * 30.02 * .223 * .223} = 103.05 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 100.0 * 15.43 / 68.519 = .0225 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE PART 904 S02
OPERATOR PR RA
AMBIENT TEMP.(DEG.F) 63.
BAR.PRESS.(IN.HG) 30.06
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531016
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TURE COEFF. .84
THERM. NO.
LEAKAGE .012 CFM @ 11.0 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/07/83
RUN NUMBER 18M58W

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE 18 : I.D. .221
ASSUMED MOISTURE 10.0
SAMPLE BOX NUMBER
METER BOX NUMBER FB6
METER HEAD DIFF. 1.50

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 977.4

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					----- DESIRED ACTUAL	----- INLET OUTLET				
INIT	0	950	949.932							
	10.0	0	955.850	.710	.91	.91	305.	59.	60.	1.0 319. 46.
	20.0	0	961.680	.710	.91	.91	306.	59.	60.	1.0 310. 46.
	30.0	0	967.575	.710	.90	.90	307.	62.	60.	1.5 317. 46.
	40.0	0	973.272	.650	.83	.83	305.	64.	60.	1.0 320. 47.
	50.0	0	979.000	.650	.83	.83	307.	66.	60.	5.0 321. 47.
	60.0	0	985.015	.680	.87	.87	308.	67.	60.	6.0 313. 48.
	70.0	0	990.558	.680	.86	.86	309.	68.	60.	6.0 313. 47.
	80.0	0	996.418	.680	.87	.87	307.	68.	61.	6.5 308. 47.
	90.0	0	2.290	.700	.89	.89	309.	68.	60.	7.5 318. 47.
	100.0	0	8.000	.650	.83	.83	308.	68.	60.	7.5 319. 47.
	110.0	0	13.764	.650	.83	.83	308.	68.	60.	8.0 322. 47.
	120.0	1150	19.509	.650	.83	.83	308.	67.	60.	8.0 324. 57.
TOTALS AVERAGE	120.0		69.577		.86	.86	307.	65.	60.	4.9 317. 48.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA

TEST 18M5BW

UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/07/83	02/07/83

TB	TIME-START	950	950
TF	TIME-FINISH	1150	1150
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.86 IN-H2O	21.9 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	69.577 CU-FT	1.970 CU-M
TM	AVERAGE GAS METER TEMP	62.7 F	17.1 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	67.929 SCF	1.924 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	182.1	182.1
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.571 SCF	.243 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.20	11.20
FMD	MOLE FRACTION DRY GAS	.888	.888
PCO2	PERCENT CO2 BY VOL., DRY	13.35	13.35
PO2	PERCENT O2 BY VOL., DRY	2.45	2.45
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.20	84.20
MD	MOLECULAR WT-DRY STACK GAS	30.23	30.23

MWS	MOLECULAR WT-STACK GAS	28.86		28.86	
PB	BAROMETRIC PRESSURE	30.06	IN-HG	763.52	MM-HG
PSI	STATIC PRES OF STACK GAS	-.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.02	IN-HG	762.40	MM-HG
TS	AVERAGE STACK TEMP	307.	F	153.	C
VS	AVG STACK GAS VELOCITY	55.6	FPS	16.9	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17557520.	SCFH	497176.	SCMH
QS	ACTUAL STACK FLOW RATE	28640920.	ACFH	811025.	ACMH
ISO	PERCENT ISOKINETIC	104.0		104.0	
MN	AMBIENT PARTICULATE MG. EPA 5	100.0		100.0	
CS	AMBIENT PARTICULATE	.0227	GR/DSCF*	51.993	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.18M5BW

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 69.577 * .960 * (30.06 + .863 / 13.6)}{(63. + 460.)} = 67.929 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 182. = 8.57 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 8.57}{67.929 + 8.57} = 11.20 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.2}{100.} = .888$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.35 * 44 / 100) + (2.4 * 32 / 100) + ((84.2 + .0) * 28 / 100) = 30.23$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.23 * (1. - (11.20 / 100)) + 18. * (11.20 / 100) = 28.86$$

A-10

STACK GAS VELOCITY AT STACK CONDITIONS

DELP = SUM. OF THE SQRT(VH * (TS + 460.))

VS = 85.49 * CP * DELP / (SQRT(MWS * PS) * PNTS)

VS = 85.49 * .84 * 273.377 / (SQRT(28.86 * 30.02) * 12. = 55.58 FPS

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

QS = VS * AS * 3600/144

QS = 55.58 * 20612. 3600/144 = 28640920. ACFH

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

QSSD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)

QSSD = $\frac{17.647 * 28640920. * 30.02 * (1. - (11.20/100))}{(307. + 460.)}$ = 17557520. SCFH

PERCENT ISOKINETIC

ISO = (305.58*(TS+460.))*((0.002669*VLC)+(VM*Y*(PB+(PM/13.6))/(TM+460.)))/(TT*VS*PS*DN*DN)

ISO = $\frac{(305.58*(307.+460.))*((0.002669* 182.)+(69.577* .960*(30.06+(.863/13.6)))/(63.+460.))}{120. * 55.58 * 30.02 * .221 * .221}$ = 103.95 PERCENT

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

CS = 0.001 * MN * 15.43 / VMSTD

CS = 0.001 * 100.0 * 15.43 / 67.929 = .0227 GR/DSCF

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

SAMPLE TYPE M-5H
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 64.
BAR.PRESS.(IN.HG) 30.06
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531015
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .000 CFM @ 10.0 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/07/83
RUN NUMBER 1CM5B

PROBE LENGTH & TYPE 6FT GLASS
NOZZLE : I.D. .221
ASSUMED MOISTURE 10.0
SAMPLE BOX NUMBER
METER BOX NUMBER F85
METER HEAD DIFF. 1.84

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1174.2

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	950	53.396									
	10.0	1000	59.325	.710	1.09	1.10	305.	62.	62.	5.0	315.	51.
	20.0	1010	64.300	.710	1.09	1.09	306.	62.	62.	5.0	328.	52.
	30.0	1020	69.800	.710	1.09	1.09	307.	67.	62.	5.5	323.	52.
	40.0	1030	74.640	.650	1.00	1.00	305.	72.	63.	6.0	330.	49.
	50.0	1040	80.000	.650	1.00	1.00	307.	74.	64.	6.5	332.	49.
	60.0	1050	85.650	.680	1.04	1.00	308.	75.	64.	7.0	320.	48.
	70.0	1100	91.210	.680	1.04	1.00	309.	76.	65.	7.0	315.	49.
	80.0	1110	96.275	.680	1.04	1.00	307.	76.	66.	7.5	322.	49.
	90.0	1120	102.000	.700	1.07	1.10	309.	78.	66.	8.5	325.	50.
	100.0	1130	106.845	.650	.99	1.00	308.	76.	66.	9.0	317.	49.
	110.0	1140	113.071	.650	.99	1.00	308.	76.	66.	9.5	321.	50.
	120.0	1140	118.356	.650	.99	1.00	308.	77.	66.	9.5	317.	48.
TOTALS AVERAGE	120.0		64.960		1.04	1.03	307.	73.	64.	7.2	322.	50.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 1CM5B UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/07/83	02/07/83

TS	TIME-START	950	950
TF	TIME-FINISH	1140	1140
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.03 IN-H2O	26.2 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	64.960 CU-FT	1.839 CU-M
TM	AVERAGE GAS METER TEMP	68.5 F	20.3 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	64.260 SCF	1.820 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	177.0	177.0
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.331 SCF	.236 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.48	11.48
FMD	MOLE FRACTION DRY GAS	.885	.885
PCO2	PERCENT CO2 BY VOL., DRY	13.35	13.35
PO2	PERCENT O2 BY VOL., DRY	2.45	2.45
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.20	84.20
MD	MOLECULAR WT-DRY STACK GAS	30.23	30.23

A-13

MWS	MOLECULAR WT-STACK GAS	28.83		28.83	
PB	BAROMETRIC PRESSURE	30.06	IN-HG	763.52	MM-HG
PSI	STATIC PRES OF STACK GAS	-.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.02	IN-HG	762.40	MM-HG
TS	AVERAGE STACK TEMP	307.	F	153.	C
VS	AVG STACK GAS VELOCITY	55.6	FPS	17.0	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17513744.	SCFH	495937.	SCMH
QS	ACTUAL STACK FLOW RATE	28657476.	ACFH	811494.	ACMH
ISO	PERCENT ISOKINETIC	98.6		98.6	
MN	AMBIENT PARTICULATE MG, EPA 5	336.7		336.7	
CS	AMBIENT PARTICULATE	.0808	GR/DSCF*	185.052	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 1CMS8

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 64.960 * .983 * (30.06 + 1.032 / 13.6)}{(68. + 460.)} = 64.260 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 177. = 8.33 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 8.33}{64.260 + 8.33} = 11.48 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.5}{100.} = .885$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.35 * 44 / 100) + (2.4 * 32 / 100) + ((84.2 + .0) * 28 / 100) = 30.23$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.23 * (1. - (11.48 / 100)) + 18. * (11.48 / 100) = 28.83$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE } \sqrt{VM * (TS + 460.)}$$

$$VS = 85.49 * CP * DELP / (\sqrt{MWS * PS}) * PNTS)$$

$$VS = 85.49 * .84 * 273.377 / (\sqrt{28.83 * 30.02}) * 12. = 55.61 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.61 * 20612. 3600/144 = 28657476. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28657476. * 30.02 * (1. - (11.48/100))}{(307. + 460.)} = 17513744. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (307. + 460.)) * ((0.002669 * 177.) + (64.960 * .983 * (30.06 + (1.032/13.6)) / (68. + 460.)))}{120. * 55.61 * 30.02 * .221 * .221} = 98.59 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 336.7 * 15.43 / 64.260 = .0808 \text{ GR/DSCF}$$

FIELD DATA

PLANT
 SAMPLING LOCATION UNIT TWO EAST

SAMPLE TYPE M5B
 OPERATOR CLARKE
 AMBIENT TEMP.(DEG.F) 64.
 BAR.PRESS.(IN.HG) 30.06
 STATIC PRESS.(IN.H2O) -.60
 FILTER NUMBER(S) 3531014
 STACK INSIDE DIM.(IN) 162.00 .00
 PITOT TUBE COEFF. .84
 THERM. NO. 206
 LEAKAGE .000 CFM @ 8.0 IN.HG
 METER CALIB. FACTOR 1.030
 READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/07/83
 RUN NUMBER 1DM5B

PROBE LENGTH & TYPE 5 FT GLASS
 NOZZLE : I.D. .215
 ASSUMED MOISTURE 10.0
 SAMPLE BOX NUMBER
 METER BOX NUMBER FB4
 METER HEAD DIFF. 1.88

PROBE HEATER SETTING 320.
 HEATER BOX SETTING 320.

K FACTOR 1174.2

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL	INLET OUTLET					
INIT	0	950	622.701									
	10.0	1000	629.125	.710	1.09	1.10	305.	58.	60.	2.0	307.	49.
	20.0	1010	633.433	.710	1.09	1.10	306.	60.	59.	2.5	334.	50.
	30.0	1020	638.490	.710	1.09	1.09	307.	62.	59.	3.0	304.	50.
	40.0	1030	643.625	.650	1.00	1.00	305.	65.	60.	3.5	341.	48.
	50.0	1040	648.656	.650	1.00	1.00	307.	68.	60.	3.5	315.	48.
	60.0	1050	654.150	.680	1.04	1.00	308.	68.	60.	4.0	317.	48.
	70.0	1100	659.210	.680	1.04	1.00	309.	68.	62.	4.5	328.	49.
	80.0	1110	663.750	.680	1.04	1.00	307.	68.	62.	5.0	334.	51.
	90.0	1120	669.100	.700	1.07	1.10	309.	68.	62.	6.0	319.	50.
	100.0	1130	674.125	.650	.99	1.00	308.	67.	62.	6.5	319.	49.
	110.0	1140	679.815	.650	.99	1.00	308.	67.	62.	6.5	332.	48.
	120.0	1150	684.453	.650	.99	1.00	308.	66.	61.	7.0	336.	48.
TOTALS AVERAGE	120.0		61.752		1.04	1.03	307.	65.	61.	4.5	324.	49.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 10M50 UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/07/83	02/07/83

TB	TIME-START	950	950
TF	TIME-FINISH	1150	1150
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	1.030	1.030
DN	SAMPLING NOZZLE DIAMETER	.215 IN	5.5 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.03 IN-H2O	26.2 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	61.752 CU-FT	1.749 CU-M
TM	AVERAGE GAS METER TEMP	63.1 F	17.3 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	64.665 SCF	1.831 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	172.9	172.9
VMC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.138 SCF	.230 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.18	11.18
FMD	MOLE FRACTION DRY GAS	.888	.888
PCO2	PERCENT CO2 BY VOL., DRY	13.35	13.35
PO2	PERCENT O2 BY VOL., DRY	2.45	2.45
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.20	84.20
MD	MOLECULAR WT-DRY STACK GAS	30.23	30.23

MWS	MOLECULAR WT-STACK GAS	28.87		28.87	
PB	BAROMETRIC PRFSSURE	30.06	IN-HG	763.52	MM-HG
PSI	STATIC PRES OF STACK GAS	-6.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.02	IN-HG	762.40	MM-HG
TS	AVERAGE STACK TEMP	307.	F	153.	C
VS	AVG STACK GAS VFLOCITY	55.6	FPS	16.9	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17561684.	SCFH	497294.	SCMH
QS	ACTUAL STACK FLOW RATE	28639348.	ACFH	810981.	ACMH
ISO	PERCENT ISOKINETIC	104.5		104.5	
MN	AMBIENT PARTICULATE MG. EPA 5	309.3		309.3	
CS	AMBIENT PARTICULATE	.0738	GR/DSCF*	168.928	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 10M5R

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 61.752 * 1.030 * (30.06 + 1.033 / 13.6)}{(63. + 460.)} = 64.665 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 173. = 8.14 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 8.14}{64.665 + 8.14} = 11.18 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.2}{100.} = .888$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.35 * 44 / 100) + (2.4 * 32 / 100) + ((84.2 + .0) * 28 / 100) = 30.23$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.23 * (1. - (11.18 / 100)) + 18. * (11.18 / 100) = 28.87$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VM * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 273.377 / (\text{SQRT}(28.87 * 30.02) * 12. = 55.58 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.58 * 20612. 3600/144 = 28639348. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28639348. * 30.02 * (1. - (11.18/100))}{(307. + 460.)} = 17561684. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (307. + 460.)) * ((0.002669 * 173.) + (61.752 * 1.030 * (30.06 + (1.033/13.6)) / (63. + 460.)))}{120. * 55.58 * 30.02 * .215 * .215} = 104.54 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 309.3 * 15.43 / 64.665 = .0738 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE M5B 304 S02
OPERATOR PR RA
AMBIENT TEMP.(DEG.F) 65.
BAR.PRESS.(IN.HG) 30.07
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531013
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .000 CFM @ 10.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/07/83
RUN NUMBER 2AM5B

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE 2A : I.D. .224
ASSUMED MOISTURE 10.0
SAMPLE BOX NUMBER
METER BOX NUMBER FB
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1182.9

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1410	504.942									
	10.0	0	510.863	.700	1.08	1.08	305.	64.	63.	4.5	325.	48.
	20.0	0	516.599	.700	1.08	1.08	309.	66.	64.	4.5	303.	48.
	30.0	0	522.411	.700	1.08	1.08	309.	70.	64.	5.0	325.	48.
	40.0	0	528.144	.680	1.04	1.04	310.	73.	65.	5.5	330.	53.
	50.0	0	533.875	.680	1.04	1.04	310.	75.	66.	6.0	326.	53.
	60.0	0	539.638	.680	1.04	1.04	309.	76.	67.	6.5	332.	52.
	70.0	0	545.535	.710	1.09	1.09	310.	76.	67.	7.0	333.	52.
	80.0	0	551.392	.710	1.09	1.09	311.	77.	68.	7.5	320.	62.
	90.0	0	557.213	.710	1.09	1.09	311.	78.	68.	7.5	333.	62.
	100.0	0	563.067	.700	1.08	1.08	310.	79.	69.	8.0	320.	52.
	110.0	0	568.934	.700	1.08	1.08	311.	80.	70.	8.5	330.	53.
	120.0	0	574.595	.650	1.00	1.00	310.	82.	70.	8.5	324.	62.
TOTALS AVERAGE	120.0		69.653		1.07	1.07	310.	75.	67.	6.6	325.	54.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA

TEST 2AM58 UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/07/83	02/07/83

TR	TIME-START	1410	1410
TF	TIME-FINISH	0	0
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.224 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.07 IN-H2O	27.1 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	69.653 CU-FT	1.972 CU-M
TM	AVERAGE GAS METER TEMP	70.7 F	21.5 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	70.036 SCF	1.983 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	176.8	176.8
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.322 SCF	.236 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.62	10.62
FMD	MOLE FRACTION DRY GAS	.894	.894
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.95	2.95
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.45	83.45
MD	MOLECULAR WT-DRY STACK GAS	30.29	30.29

MWS	MOLECULAR WT-STACK GAS	28.99		28.99	
PB	BAROMETRIC PRESSURE	30.07	IN-HG	763.78	MM-HG
PSI	STATIC PRFS OF STACK GAS	-.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.03	IN-HG	762.66	MM-HG
TS	AVERAGE STACK TEMP	310.	F	154.	C
VS	AVG STACK GAS VFLOCITY	56.2	FPS	17.1	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17828276.	SCFH	504843.	SCMH
QS	ACTUAL STACK FLOW RATE	28970800.	ACFH	820366.	ACMH
ISO	PERCENT ISOKINETIC	102.7		102.7	
MN	AMBIENT PARTICULATE MG. EPA 5	389.7		389.7	
CS	AMBIENT PARTICULATE	.0859	GR/DSCF*	196.520	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 2AM5R

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 69.653 * 1.003 * (30.07 + 1.066 / 13.6)}{(71. + 460.)} = 70.036 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 177. = 8.32 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 8.32}{70.036 + 8.32} = 10.62 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 10.6}{100.} = .894$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.9 * 32 / 100) + ((83.4 + .0) * 28 / 100) = 30.29$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.29 * (1. - (10.62 / 100)) + 18. * (10.62 / 100) = 28.99$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 277.170 / (\text{SQRT}(28.99 * 30.03) * 12.) = 56.22 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 56.22 * 20612.3600/144 = 28970800. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 28970800. * 30.03 * (1. - (10.62/100))}{(310. + 460.)} = 17828276. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (310. + 460.)) * ((0.002669 * 177.) + (69.653 * 1.003 * (30.07 + (1.066/13.6)) / (71. + 460.)))}{120. * 56.22 * 30.03 * .224 * .224} = 102.74 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 389.7 * 15.43 / 70.036 = .0859 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE PMSB 304 302
OPERATOR PR RA
AMBIENT TEMP.(DEG.F) 65.
BAR.PRESS.(IN.HG) 30.07
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531017
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TURE COEFF. .84
THERM. NO. 117
LEAKAGE .020 CFM @ 13.0 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/07/83
RUN NUMBER 28M5B

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .227
ASSUMED MOISTURE 10.0
SAMPLE BOX NUMBER
METER BOX NUMBER F86
METER HEAD DIFF. 1.50

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1088.0

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					----- DESIRED ACTUAL					
					----- INLET OUTLET					
INIT	0	1410	19.804							
	10.0	0	26.053	.700	1.00	1.00	305.	59.	59.	48.
	20.0	0	32.238	.700	.99	.99	309.	60.	59.	48.
	30.0	0	38.421	.700	.99	.99	309.	65.	60.	48.
	40.0	0	44.544	.680	.96	.96	310.	68.	60.	49.
	50.0	0	50.624	.680	.96	.96	310.	69.	60.	49.
	60.0	0	56.790	.680	.96	.96	310.	70.	62.	53.
	70.0	0	63.104	.710	1.00	1.00	310.	70.	62.	53.
	80.0	0	69.366	.710	1.00	1.00	311.	70.	62.	59.
	90.0	0	75.637	.710	1.00	1.00	311.	70.	63.	59.
	100.0	0	81.936	.700	.99	.99	310.	71.	64.	53.
	110.0	0	88.211	.700	.99	.99	311.	72.	64.	53.
	120.0	0	94.225	.650	.92	.92	310.	72.	65.	59.
TOTALS AVERAGE	120.0		72.021		.98	.98	310.	68.	62.	53.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA

TEST 28M58 UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/07/83	02/07/83

TR	TIME-START	1410	1410
TF	TIME-FINISH	0	0
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.227 IN	5.8 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.98 IN-H2O	24.9 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	72.021 CU-FT	2.039 CU-M
TM	AVERAGE GAS METER TEMP	64.8 F	18.2 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	70.073 SCF	1.984 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	183.8	183.8
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.651 SCF	.245 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.99	10.99
FMD	MOLE FRACTION DRY GAS	.890	.890
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.95	2.95
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.45	83.45
MD	MOLECULAR WT-DRY STACK GAS	30.29	30.29

A-28

MWS	MOLECULAR WT-STACK GAS	28.94		28.94	
PB	BAROMETRIC PRESSURE	30.07	IN-HG	763.78	MM-HG
PSI	STATIC PRES OF STACK GAS	-.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.03	IN-HG	762.66	MM-HG
TS	AVERAGE STACK TEMP	310.	F	154.	C
VS	AVG STACK GAS VELOCITY	56.3	FPS	17.2	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17767612.	SCFH	503126.	SCMH
QS	ACTUAL STACK FLOW RATE	28995052.	ACFH	821053.	ACMH
ISO	PERCENT ISOKINETIC	100.4		100.4	
MN	AMBIENT PARTICULATE MG. EPA 5	378.0		378.0	
CS	AMBIENT PARTICULATE	.0832 GR/DSCF*		190.517	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 2BM5B

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PR + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 72.021 * .960 * (30.07 + .980 / 13.6)}{(65. + 460.)} = 70.073 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 184. = 8.65 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$RWO = (100. * VWC) / (VMSTD + VWC)$$

$$RWO = \frac{100. * 8.65}{70.073 + 8.65} = 10.99 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - RWO) / 100.$$

$$FMD = \frac{100. - 11.0}{100.} = .890$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.9 * 32 / 100) + ((83.4 + .0) * 28 / 100) = 30.29$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (RWO / 100)) + 18. * (RWO / 100)$$

$$MWS = 30.29 * (1. - (10.99 / 100)) + 18. * (10.99 / 100) = 28.94$$

STACK GAS VELOCITY AT STACK CONDITIONS

DELP = SUM. OF THE SQRT(VH * (TS + 460.))

VS = 85.49 * CP * DELP / (SQRT(MWS * PS) * PNTS)

VS = 85.49 * .84 * 277.185 / (SQRT(28.94 * 30.03) * 12. = 56.27 FPS

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

QS = VS * AS * 3600/144

QS = 56.27 * 20612. 3600/144 = 28995052. ACFH

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

QSSTD = 17.647 * QS * PS * (1. - (RWD/100)) / (TS + 460.)

QSSTD = $\frac{17.647 * 28995052. * 30.03 * (1. - (10.99/100))}{(310. + 460.)}$ = 17767612. SCFH

PERCENT ISOKINETIC

ISO = (305.58*(TS+460.))*((0.002669*VLC)+(VM*Y*(PB*(PM/13.6)))/(TM+460.)))/(TT*VS*PS*DN*DN)

ISO = $\frac{(305.58*(310.+460.))*((0.002669*184.)+(72.021*.960*(30.07*(.980/13.6)))/(65.+460.))}{120. * 56.27 * 30.03 * .227 * .227}$ = 100.44 PERCENT

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

CS = 0.001 * MN * 15.43 / VMSTD

CS = 0.001 * 378.0 * 15.43 / 70.073 = .0832 GR/DSCF

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/07/83
RUN NUMBER 2CM58W

SAMPLE TYPE MSBW
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 58.
BAR.PRESS.(IN.HG) 30.07
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531070
STACK INSIDE DTM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .001 CFM @ 7.0 IN.HG
METER CALIB. FACTOR .9A3
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : 1.0. .211
ASSUMED MOISTURE 10.0
SAMPLE BOX NUMBER
METER BOX NUMBER F85
METER HEAD DIFF. 1.84
PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.
K FACTOR 992.4

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					----- DESIRED ACTUAL					
					----- INLET OUTLET					
INIT	0	1410	118.570							
	10.0	1420	123.900	.700	.91	.91	305.	62.	62.	4.0
	20.0	1430	128.975	.700	.90	.90	309.	64.	62.	4.0
	30.0	1440	134.150	.700	.90	.90	309.	69.	63.	4.0
	40.0	1450	139.000	.680	.88	.88	310.	73.	64.	4.5
	50.0	1500	144.404	.680	.88	.88	310.	75.	65.	4.5
	60.0	1510	149.194	.680	.88	.88	309.	77.	68.	5.0
	70.0	1520	154.525	.710	.92	.92	310.	78.	67.	5.5
	80.0	1530	159.500	.710	.92	.92	311.	78.	68.	5.5
	90.0	1540	164.810	.710	.92	.92	311.	78.	68.	6.0
	100.0	1550	169.750	.700	.90	.90	310.	80.	69.	6.0
	110.0	1600	174.495	.700	.90	.90	311.	80.	70.	6.5
	120.0	1610	180.021	.650	.84	.84	310.	80.	70.	6.5
TOTALS AVERAGE	120.0		61.451		.90	.90	310.	75.	66.	5.2
									324.	54.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 2CM5BW

UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/07/83	02/07/83

TR	TIME-START	1410	1410
TF	TIME-FINISH	1610	1610
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.211 IN	5.4 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.90 IN-H2O	22.8 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	61.451 CU-FT	1.740 CU-M
TM	AVERAGE GAS METER TEMP	70.4 F	21.3 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	60.565 SCF	1.715 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILTCA GEL, ML.	160.1	160.1
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	7.536 SCF	.213 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.07	11.07
FMD	MOLE FRACTION DRY GAS	.889	.889
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.95	2.95
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.45	83.45
MD	MOLECULAR WT-DRY STACK GAS	30.29	30.29

MWS	MOLECULAR WT-STACK GAS	28.93		28.93	
PB	BAROMETRIC PRESSURE	30.07	IN-HG	763.78	MM-HG
PSI	STATIC PRES OF STACK GAS	-.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.03	IN-HG	762.66	MM-HG
TS	AVERAGE STACK TFMP	310.	F	154.	C
VS	AVG STACK GAS VELOCITY	56.3	FPS	17.2	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17756224.	SCFH	502803.	SCMH
QS	ACTUAL STACK FLOW RATE	28998200.	ACFH	821142.	ACMH
ISO	PERCENT ISOKINETIC	100.5		100.5	
MN	AMBIENT PARTICULATE MG. EPA 5	100.0		100.0	
CS	AMBIENT PARTICULATE	.0255	GR/DSCF*	58.314	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.2CM5BW

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 61.451 * .983 * (30.07 + .896 / 13.6)}{(70. + 460.)} = 60.565 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 160. = 7.54 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 7.54}{60.565 + 7.54} = 11.07 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.1}{100.} = .889$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * .44 / 100) + (2.9 * .32 / 100) + ((83.4 + .0) * .28 / 100) = 30.29$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.29 * (1. - (11.07 / 100)) + 18. * (11.07 / 100) = 28.93$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 277.170 / (\text{SQRT}(28.93 * 30.03) * 12.) = 56.27 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 56.27 * 20612.3600/144 = 28998200. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28998200. * 30.03 * (1. - (11.07/100))}{(310. + 460.)} = 17756224. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (310. + 460.)) * ((0.002669 * 160.) + (61.451 * .983 * (30.07 + (.896/13.6)) / (70. + 460.)))}{120. * 56.27 * 30.03 * .211 * .211} = 100.54 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 100.0 * 15.43 / 60.565 = .0255 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/07/83
RUN NUMBER 2DM5BW

SAMPLE TYPE M5BW
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 58.
BAR.PRESS.(IN.HG) 30.07
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531069
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .002 CFM @ 9.0 IN.HG
METER CALIB. FACTOR 1.030
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .210
ASSUMED MOISTURE 10.0
SAMPLE BOX NUMBER
METER BOX NUMBER F84
METER HEAD DIFF. 1.88
PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.
K FACTOR 992.4

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					----- DESIRED ACTUAL	----- INLET OUTLET				
INIT	0	1410	684.704							
	10.0	1420	689.725	.700	.91 .90	305.	62.	61.	5.0	317.
	20.0	1430	694.200	.700	.90 .90	309.	63.	61.	5.0	327.
	30.0	1440	699.800	.700	.90 .90	309.	65.	61.	5.0	312.
	40.0	1450	704.174	.680	.88 .88	310.	68.	62.	5.5	312.
	50.0	1500	709.097	.680	.88 .88	310.	69.	62.	6.0	331.
	60.0	1510	713.445	.680	.88 .88	309.	70.	64.	6.5	317.
	70.0	1520	718.999	.710	.92 .92	310.	70.	64.	7.0	313.
	80.0	1530	723.430	.710	.92 .92	311.	70.	64.	7.5	330.
	90.0	1540	728.811	.710	.92 .92	311.	70.	64.	8.0	326.
	100.0	1550	733.525	.700	.90 .90	310.	71.	66.	8.5	333.
	110.0	1600	737.990	.700	.90 .90	311.	71.	65.	9.0	342.
	120.0	1610	743.154	.650	.84 .84	310.	72.	66.	9.0	335.
TOTALS AVERAGE	120.0		58.450		.90 .89	310.	68.	63.	6.8	325.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 20M5BN

UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/07/83	02/07/83

TB	TIME-START	1410	1410
TF	TIME-FINISH	1610	1610
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	1.030	1.030
DN	SAMPLING NOZZLE DIAMETER	.210 IN	5.3 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.89 IN-H2O	22.7 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	58.450 CU-FT	1.655 CU-M
TM	AVERAGE GAS METER TEMP	65.9 F	18.8 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	60.883 SCF	1.724 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	160.0	160.0
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	7.531 SCF	.213 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.01	11.01
FMD	MOLE FRACTION DRY GAS	.890	.890
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.95	2.95
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.45	83.45
MD	MOLECULAR WT-DRY STACK GAS	30.29	30.29

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MWS	MOLECULAR WT-STACK GAS	28.94		28.94	
PB	BAROMETRIC PRESSURE	30.07	IN-HG	763.78	MM-HG
PSI	STATIC PRES OF STACK GAS	-1.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.03	IN-HG	762.66	MM-HG
TS	AVERAGE STACK TEMP	310.	F	154.	C
VS	AVG STACK GAS VELOCITY	56.3	FPS	17.2	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17765544.	SCFH	503067.	SCMH
QS	ACTUAL STACK FLOW RATE	28994660.	ACFH	821042.	ACMH
ISO	PERCENT ISOXINETIC	102.0		102.0	
MN	AMBIENT PARTICULATE MG. EPA 5	100.0		100.0	
CS	AMBIENT PARTICULATE	.0253	GR/DSCF*	58.010	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.2DM5BW

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 58.450 * 1.030 * (30.07 + .895 / 13.6)}{(66. + 460.)} = 60.883 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 160. = 7.53 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 7.53}{60.883 + 7.53} = 11.01 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.0}{100.} = .890$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.9 * 32 / 100) + ((83.4 + .0) * 28 / 100) = 30.29$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.29 * (1. - (11.01 / 100)) + 18. * (11.01 / 100) = 28.94$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VM * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 277.170 / (\text{SQRT}(28.94 * 30.03) * 12.) = 56.27 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 56.27 * 20612.3600/144 = 28994660. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (BWO/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 28994660. * 30.03 * (1. - (11.01/100))}{(310. + 460.)} = 17765544. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (310. + 460.)) * ((0.002669 * 160.) + (58.450 * 1.030 * (30.07 + (.895/13.6)) / (66. + 460.)))}{120. * 56.27 * 30.03 * .210 * .210} = 101.98 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 100.0 * 15.43 / 60.883 = .0253 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE PART 303 S04
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 45.
BAR.PRESS.(IN.HG) 30.34
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531010
STACK INSIDE DTM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .010 CFM @ 9.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/08/83
RUN NUMBER 3AM5B

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE 1A : I.D. .223
ASSUMED MOISTURE 11.1
SAMPLE BOX NUMBER
METER BOX NUMBER FB4
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1093.5

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	845	574.939									
	10.0	0	580.299	.650	.93	.93	303.	46.	45.	3.5	321.	43.
	20.0	0	585.673	.650	.93	.93	306.	48.	45.	4.0	324.	43.
	30.0	0	590.978	.650	.93	.93	308.	53.	46.	4.5	334.	45.
	40.0	0	596.377	.670	.95	.95	307.	56.	46.	5.0	316.	45.
	50.0	0	601.740	.670	.95	.95	309.	60.	48.	5.0	322.	45.
	60.0	0	607.148	.670	.95	.95	310.	62.	50.	5.5	336.	46.
	70.0	0	612.600	.680	.97	.97	310.	63.	51.	6.0	330.	37.
	80.0	0	617.950	.650	.92	.92	311.	64.	52.	6.5	327.	38.
	90.0	0	623.286	.650	.92	.92	311.	65.	53.	7.0	318.	39.
	100.0	0	628.650	.650	.92	.92	312.	66.	54.	7.0	330.	40.
	110.0	0	634.100	.680	.96	.96	313.	66.	55.	7.5	319.	40.
	120.0	1045	639.502	.680	.96	.96	314.	66.	56.	8.0	339.	45.
TOTALS AVERAGE	120.0		64.563		.94	.94	310.	60.	50.	5.8	326.	42.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 3AM5B UNIT 2 FAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/08/83	02/08/83

TB	TIME-START	845	845
TF	TIME-FINISH	1045	1045
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.223 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.94 IN-H2O	23.9 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	64.563 CU-FT	1.828 CU-M
TM	AVERAGE GAS METER TEMP	54.8 F	12.7 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	67.498 SCF	1.911 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	170.4	170.4
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.021 SCF	.227 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.62	10.62
FMD	MOLE FRACTION DRY GAS	.894	.894
PCO2	PERCENT CO2 BY VOL., DRY	13.70	13.70
PO2	PERCENT O2 BY VOL., DRY	2.35	2.35
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.95	83.95
MD	MOLECULAR WT-DRY STACK GAS	30.29	30.29

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MWS	MOLECULAR WT-STACK GAS	28.98		28.98	
PB	BAROMETRIC PRESSURE	30.34	IN-HG	770.64	MM-HG
PSI	STATIC PRES OF STACK GAS	-0.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.30	IN-HG	769.52	MM-HG
TS	AVERAGE STACK TFMP	310.	F	154.	C
VS	AVG STACK GAS VFLOCITY	54.7	FPS	16.7	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17509204.	SCFH	495808.	SCMH
QS	ACTUAL STACK FLOW RATE	28195776.	ACFH	798420.	ACMH
ISO	PERCENT ISOKINETIC	101.7		101.7	
MN	AMBIENT PARTICULATE MG. EPA 5	356.9		356.9	
CS	AMBIENT PARTICULATE	.0816	GR/DSCF*	186.744	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 3AM5R

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 64.563 * 1.003 * (30.34 + .941 / 13.6)}{(55. + 460.)} = 67.498 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 170. = 8.02 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 8.02}{67.498 + 8.02} = 10.62 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 10.6}{100.} = .894$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.70 * 44 / 100) + (2.3 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.29$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.29 * (1. - (10.62 / 100)) + 18. * (10.62 / 100) = 28.98$$

STACK GAS VELOCITY AT STACK CONDITIONS

DELP = SUM. OF THE SQRT(VH * (TS + 460.))

VS = 85.49 * CP * DELP / (SQRT(MWS * PS) * PNTS)

VS = 85.49 * .84 * 270.932 / (SQRT(28.98 * 30.30) * 12. = 54.72 FPS

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

QS = VS * AS * 3600/144

QS = 54.72 * 20612. 3600/144 = 28195776. ACFH

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

QSSD = 17.647 * QS * PS * (1. - (RWD/100)) / (TS + 460.)

QSSD =
$$\frac{17.647 * 28195776. * 30.30 * (1. - (10.62/100))}{(310. + 460.)} = 17509204. \text{ SCFH}$$

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PERCENT ISOKINETIC

ISO = (305.58*(TS+460.))*((0.002669*VLC)+(VM*Y*(PB+(PM/13.6))/(TM+460.)))/(TT*VS*PS*DN*DN)

ISO =
$$\frac{(305.58*(310.+460.))*((0.002669* 170.)+(64.563*1.003*(30.34+(.941/13.6)))/(55.+460.))}{120. * 54.72 * 30.30 * .223 * .223} = 101.73 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

CS = 0.001 * MN * 15.43 / VMSTD

CS = 0.001 * 356.9 * 15.43 / 67.498 = .0816 GR/DSCF

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE PART 303 S02
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 45.
BAR.PRESS.(IN.HG) 30.34
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531009
STACK INSIDE DTM.(IN) 162.00 .00
PITOT TURE COEFF. .84
THERM. NO.
LEAKAGE .013 CFM @ 9.5 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/08/83
RUN NUMBER 38M58

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE 18 : I.D. .221
ASSUMED MOISTURE 11.1
SAMPLE BOX NUMBER
METER BOX NUMBER F86
METER HEAD DIFF. 1.50

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 919.9

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	845	94.740									
	10.0	0	100.161	.650	.78	.78	303.	40.	42.	3.5	321.	43.
	20.0	0	105.596	.650	.78	.78	306.	42.	43.	3.5	328.	43.
	30.0	0	111.008	.650	.78	.78	308.	46.	43.	4.0	328.	45.
	40.0	0	116.514	.670	.80	.80	307.	51.	43.	4.5	329.	45.
	50.0	0	122.076	.670	.80	.80	309.	54.	44.	5.0	326.	45.
	60.0	0	127.593	.670	.80	.80	310.	56.	45.	5.5	332.	46.
	70.0	0	133.181	.680	.81	.81	310.	57.	46.	6.0	335.	39.
	80.0	0	138.664	.650	.77	.77	311.	57.	46.	6.0	339.	39.
	90.0	0	144.100	.650	.77	.77	311.	58.	48.	6.5	331.	40.
	100.0	0	149.581	.650	.77	.77	312.	59.	49.	7.0	337.	40.
	110.0	0	155.196	.680	.81	.68	312.	59.	50.	7.0	321.	40.
	120.0	1045	160.804	.680	.81	.81	314.	60.	50.	7.5	335.	43.
TOTALS AVERAGE	120.0		66.064		.79	.78	309.	53.	46.	5.5	330.	42.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 3BMSB UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/08/83	02/08/83

TB	TIME-START	845	845
TF	TIME-FINISH	1045	1045
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.78 IN-H2O	19.8 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	66.064 CU-FT	1.871 CU-M
TM	AVERAGE GAS METER TEMP	49.5 F	9.7 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	66.772 SCF	1.891 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	168.8	168.8
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	7.945 SCF	.225 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.63	10.63
FMD	MOLE FRACTION DRY GAS	.894	.894
PCO2	PERCENT CO2 BY VOL., DRY	13.70	13.70
PO2	PERCENT O2 BY VOL., DRY	2.35	2.35
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.95	83.95
MD	MOLECULAR WT-DRY STACK GAS	30.29	30.29

MWS	MOLECULAR WT-STACK GAS	28.98		28.98	
PB	BAROMETRIC PRFSSURE	30.34	IN-HG	770.64	MM-HG
PSI	STATIC PRES OF STACK GAS	-.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.30	IN-HG	769.52	MM-HG
TS	AVERAGE STACK TEMP	309.	F	154.	C
VS	AVG STACK GAS VELOCITY	54.7	FPS	16.7	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17508064.	SCFH	495776.	SCMH
QS	ACTUAL STACK FLOW RATE	28195020.	ACFH	798398.	ACMH
ISO	PERCENT ISOKINETIC	102.5		102.5	
MN	AMBIENT PARTICULATE MG. EPA 5	376.6		376.6	
CS	AMBIENT PARTICULATE	.0870 GR/DSCF*		199.195 MG/DSCM	

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 38M5B

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 66.064 * .960 * (30.34 + .779 / 13.6)}{(50. + 460.)} = 66.772 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 169. = 7.95 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 7.95}{66.772 + 7.95} = 10.63 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 10.6}{100.} = .894$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.70 * 44 / 100) + (2.3 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.29$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.29 * (1. - (10.63 / 100)) + 18. * (10.63 / 100) = 28.98$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 270.917 / (\text{SQRT}(28.98 * 30.30) * 12. = 54.72 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 54.72 * 20612.3600/144 = 28195020. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28195020. * 30.30 * (1. - (10.63/100))}{(309. + 460.)} = 17508064. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (309. + 460.)) * ((0.002669 * 169.) + (66.064 * .960 * (30.34 + (.779/13.6)) / (50. + 460.)))}{120. * 54.72 * 30.30 * .221 * .221} = 102.47 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 376.6 * 15.43 / 66.772 = .0870 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/08/83
RUN NUMBER 3CM58P

SAMPLE TYPE M5RP400
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 45.
BAR.PRESS.(IN.HG) 30.34
STATIC PRESS.(IN.H2O) -.60
FILTER NUMRER(S) 3531008
STACK INSIDE DTM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .060 CFM @ 7.0 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .221
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAC
METER BOX NUMBER FR5
METER HEAD DIFF. 1.84

PROBE HEATER SETTING 400.
HEATER BOX SETTING 320.

K FACTOR 1089.1

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	845	180.494									
	10.0	855	185.825	.650	.95	.93	303.	44.	46.	4.5	314.	42.
	20.0	905	190.865	.650	.92	.92	306.	47.	46.	5.0	320.	44.
	30.0	915	195.995	.650	.92	.92	308.	53.	46.	5.5	329.	46.
	40.0	925	201.050	.670	.95	.95	307.	58.	48.	5.0	323.	45.
	50.0	935	206.245	.670	.95	.95	309.	62.	50.	5.5	333.	46.
	60.0	945	211.499	.670	.95	.95	310.	64.	51.	6.0	330.	44.
	70.0	955	216.595	.680	.96	.96	310.	64.	52.	6.0	325.	42.
	80.0	1005	221.715	.650	.92	.92	311.	65.	54.	6.5	335.	38.
	90.0	1015	226.891	.650	.92	.92	311.	66.	54.	6.5	335.	39.
	100.0	1025	232.150	.650	.92	.92	312.	67.	55.	6.5	330.	40.
	110.0	1035	237.277	.680	.96	.96	313.	68.	56.	7.0	317.	41.
	120.0	1045	242.544	.680	.96	.96	314.	68.	56.	7.0	328.	44.
TOTALS AVERAGE	120.0		54.850		.94	.94	310.	61.	51.	5.9	327.	43.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 3CM58P

UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/08/83	02/08/83

TB	TIME-START	845	845
TF	TIME-FINISH	1045	1045
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.94 IN-H2O	23.8 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	54.850 CU-FT	1.553 CU-M
TM	AVERAGE GAS METER TEMP	55.8 F	13.2 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	56.091 SCF	1.588 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	143.4	143.4
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.750 SCF	.191 SCM
BW0	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.74	10.74
FMD	MOLE FRACTION DRY GAS	.893	.893
PCO2	PERCENT CO2 BY VOL., DRY	13.70	13.70
PO2	PERCENT O2 BY VOL., DRY	2.35	2.35
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.95	83.95
MD	MOLECULAR WT-DRY STACK GAS	30.29	30.29

MWS	MOLECULAR WT-STACK GAS	28.97		28.97	
PB	BAROMETRIC PRESSURE	30.34	IN-HG	770.64	MM-HG
PSI	STATIC PRES OF STACK GAS	-60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.30	IN-HG	769.52	MM-HG
TS	AVERAGE STACK TEMP	310.	F	154.	C
VS	AVG STACK GAS VFLOCITY	54.7	FPS	16.7	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17490092.	SCFH	495267.	SCMH
QS	ACTUAL STACK FLOW RATE	28202980.	ACFH	798624.	ACMH
ISO	PERCENT ISOKINETIC	86.2		86.2	
MN	AMBIENT PARTICULATE MG. EPA 5	335.2		335.2	
CS	AMBIENT PARTICULATE	.0922	GR/DSCF*	211.060	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.3CM5BP

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 54.850 * .983 * (30.34 + .938 / 13.6)}{(56. + 460.)} = 56.091 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VMC = .04707 * VLC$$

$$VMC = .04707 * 143. = 6.75 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VMC) / (VMSTD + VMC)$$

$$BWD = \frac{100. * 6.75}{56.091 + 6.75} = 10.74 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 10.7}{100.} = .893$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.70 * 44 / 100) + (2.3 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.29$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.29 * (1. - (10.74 / 100)) + 18. * (10.74 / 100) = 28.97$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 270.932 / (\text{SQRT}(28.97 * 30.30) * 12.) = 54.73 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 54.73 * 20612.3600/144 = 28202980. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28202980. * 30.30 * (1. - (10.74/100))}{(310. + 460.)} = 17490092. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (310. + 460.)) * ((0.002669 * 143.) + (54.850 * .983 * (30.34 + (.938/13.6)) / (56. + 460.)))}{120. * 54.73 * 30.30 * .221 * .221} = 86.17 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 335.2 * 15.43 / 56.091 = .0922 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

SAMPLE TYPE M58P400
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 45.
BAR.PRESS.(IN.HG) 30.34
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531004
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO.
LEAKAGE .002 CFM @ 6.0 IN.HG
METER CALIB. FACTOR 1.030
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/08/83
RUN NUMBER 30M58P

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .215
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAD
METER BOX NUMBER FB4
METER HEAD DIFF. 1.88

PROBE HEATER SETTING 400.
HEATER BOX SETTING 320.

K FACTOR 1089.1

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	845	743.598									
	10.0	855	748.454	.650	.93	.93	303.	42.	42.	2.0	314.	42.
	20.0	905	753.323	.650	.92	.92	306.	44.	42.	2.5	333.	42.
	30.0	915	758.195	.650	.92	.92	308.	49.	43.	2.5	311.	40.
	40.0	925	763.125	.670	.95	.95	307.	53.	44.	3.0	326.	44.
	50.0	935	768.125	.670	.95	.95	309.	56.	47.	3.5	334.	46.
	60.0	945	773.186	.670	.95	.95	310.	56.	47.	4.0	320.	42.
	70.0	955	777.999	.680	.96	.96	310.	57.	48.	4.5	319.	40.
	80.0	1005	782.935	.650	.92	.92	311.	57.	49.	4.5	336.	36.
	90.0	1015	787.855	.650	.92	.92	311.	58.	50.	5.0	313.	38.
	100.0	1025	792.690	.650	.92	.92	312.	58.	51.	5.0	328.	36.
	110.0	1035	797.725	.680	.96	.96	313.	59.	51.	5.5	329.	38.
	120.0	1045	802.746	.680	.96	.96	314.	60.	52.	6.0	319.	43.
TOTALS AVERAGE	120.0		59.148		.94	.94	310.	54.	47.	4.0	324.	41.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 3DM5BP

UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/08/83	02/08/83

TB	TIME-START	845	845
TF	TIME-FINISH	1045	1045
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	1.030	1.030
DN	SAMPLING NOZZLE DIAMETER	.215 IN	5.5 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.94 IN-H2O	23.8 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	59.148 CU-FT	1.675 CU-M
TM	AVERAGE GAS METER TEMP	50.6 F	10.3 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	64.025 SCF	1.813 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	163.5	163.5
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	7.696 SCF	.218 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.73	10.73
FMD	MOLE FRACTION DRY GAS	.893	.893
PCO2	PERCENT CO2 BY VOL., DRY	13.70	13.70
PO2	PERCENT O2 BY VOL., DRY	2.35	2.35
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.95	83.95
MD	MOLECULAR WT-DRY STACK GAS	30.29	30.29

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MWS	MOLECULAR WT-STACK GAS	28.97		28.97	
PB	BAROMETRIC PRESSURE	30.34	IN-HG	770.64	MM-HG
PSI	STATIC PRES OF STACK GAS	-0.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.30	IN-HG	769.52	MM-HG
TS	AVERAGE STACK TFMP	310.	F	154.	C
VS	AVG STACK GAS VELOCITY	54.7	FPS	16.7	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSD	STACK FLOW RATE, DRY*	17491792.	SCFH	495315.	SCMH
QS	ACTUAL STACK FLOW RATE	28202336.	ACFH	798606.	ACMH
ISO	PERCENT ISOKINETIC	103.9		103.9	
MN	AMBIENT PARTICULATE MG. EPA 5	351.4		351.4	
CS	AMBIENT PARTICULATE	.0647	GR/DSCF*	193.642	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.3DM5BP

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 59.148 * 1.030 * (30.34 + .938 / 13.6)}{(51. + 460.)} = 64.025 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 164. = 7.70 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 7.70}{64.025 + 7.70} = 10.73 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 10.7}{100.} = .893$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.70*44/100) + (2.3*32/100) + ((83.9+ .0) * 28/100) = 30.29$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO/100)) + 18. * (BWO/100)$$

$$MWS = 30.29 * (1. - (10.73/100)) + 18. * (10.73/100) = 28.97$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = 3111. OF THE SQRT(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (SQRT(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 270.932 / (SQRT(28.97 * 30.30) * 12. = 54.73 FPS$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 54.73 * 20612. 3600/144 = 28202336. ACFM$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28202336. * 30.30 * (1. - (10.73/100))}{(310. + 460.)} = 17491792. SCFH$$

PERCENT ISOKINETIC

$$ISO = (305.58*(TS+460.))*((0.002669*VLC)+(VM*Y*(PB+(PM/13.6))/(TM+460.)))/(TT*VS*PS*DN*DN)$$

$$ISO = \frac{(305.58*(310.+460.))*((0.002669*164.)+(59.148*1.030*(30.34+(.938/13.6))/(51.+460.)))}{120. * 54.73 * 30.30 * .215 * .215} = 103.91 PERCENT$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 351.4 * 15.43 / 64.025 = .0847 GR/DSCF$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE PART 303 S04
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 50.
BAR.PRESS.(IN.HG) 30.36
STATIC PRESS.(IN.H2O) -.60
FILTER NUMRER(S) 3530458
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THFRM. NO. 178
LEAKAGE .000 CFM @ 9.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/08/83
RUN NUMBER 4AM58P

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE 2A : I.D. .224
ASSUMED MOISTURE 11.1
SAMPLE BOX NUMBER
METER BOX NUMBER FB4
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 400.
HEATER BOX SETTING 320.

K FACTOR 1112.4

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TFMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1230	639.710									
	10.0	0	645.416	.720	1.03	1.03	314.	58.	56.	4.5	347.	50.
	20.0	0	651.047	.720	1.03	1.03	317.	60.	56.	4.5	318.	50.
	30.0	0	656.673	.720	1.03	1.03	318.	64.	57.	5.0	340.	51.
	40.0	0	662.447	.750	1.07	1.07	318.	68.	58.	5.5	327.	51.
	50.0	0	668.169	.750	1.07	1.07	317.	70.	60.	6.0	333.	51.
	60.0	0	673.838	.720	1.03	1.03	317.	71.	60.	6.0	341.	50.
	70.0	0	679.434	.720	1.03	1.03	317.	72.	61.	6.5	327.	50.
	80.0	0	685.020	.700	1.00	1.00	318.	73.	62.	6.5	338.	52.
	90.0	0	690.611	.700	1.00	1.00	318.	75.	63.	7.0	335.	52.
	100.0	0	696.309	.720	1.03	1.03	317.	76.	64.	7.5	335.	51.
	110.0	0	701.964	.720	1.03	1.03	318.	76.	65.	8.0	317.	51.
	120.0	1430	707.671	.720	1.03	1.03	319.	77.	66.	8.0	330.	51.
TOTALS AVERAGE	120.0		67.961		1.03	1.03	317.	70.	61.	6.3	332.	51.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 4AMS8P

UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/08/83	02/08/83

TB	TIME-START	1230	1230
TF	TIME-FINISH	1430	1430
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.224 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.03 IN-H2O	26.2 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	67.961 CU-FT	1.924 CU-M
TM	AVERAGE GAS METER TEMP	65.3 F	18.5 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	69.692 SCF	1.973 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	177.7	177.7
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.364 SCF	.237 SCM
BW0	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.72	10.72
FMD	MOLE FRACTION DRY GAS	.893	.893
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.30	2.30
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.10	84.10
MD	MOLECULAR WT-DRY STACK GAS	30.27	30.27

MWS	MOLECULAR WT-STACK GAS	28.95		28.95	
PB	BAROMETRIC PRESSURE	30.36	IN-HG	771.14	MM-HG
PSI	STATIC PRES OF STACK GAS	-0.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.32	IN-HG	770.02	MM-HG
TS	AVERAGE STACK TEMP	317.	F	159.	C
VS	AVG STACK GAS VELOCITY	57.4	FPS	17.5	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	18177220.	SCFH	514724.	SCMH
QS	ACTUAL STACK FLOW RATE	29581420.	ACFH	837657.	ACMH
ISO	PERCENT ISOKINETIC	100.3		100.3	
MN	AMBIENT PARTICULATE MG. EPA 5	398.9		398.9	
CS	AMBIENT PARTICULATE	.0883 GR/DSCF*		202.151	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.4AM5BP

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 67.961 * 1.003 * (30.36 + 1.032 / 13.6)}{(65. + 460.)} = 69.692 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VMC = .04707 * VLC$$

$$VMC = .04707 * 178. = 8.36 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VMC) / (VMSTD + VMC)$$

$$BWO = \frac{100. * 8.36}{69.692 + 8.36} = 10.72 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 10.7}{100.} = .893$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.3 * 32 / 100) + ((84.1 + .0) * 28 / 100) = 30.27$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.27 * (1. - (10.72 / 100)) + 18. * (10.72 / 100) = 28.95$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 284.204 / (\text{SQRT}(28.95 * 30.32) * 12.) = 57.41 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 57.41 * 20612.3600/144 = 29581420. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 29581420. * 30.32 * (1. - (10.72/100))}{(317. + 460.)} = 18177220. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * UN)$$

$$ISO = \frac{(305.58 * (317. + 460.)) * ((0.002669 * 178.) + (67.961 * 1.003 * (30.36 + (1.032/13.6)) / (65. + 460.)))}{120. * 57.41 * 30.32 * .224 * .224} = 100.27 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 398.9 * 15.43 / 69.692 = .0883 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/08/83
RUN NUMBER 48M5RP

SAMPLE TYPE PART 903 S04
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 50.
BAR.PRESS.(IN.HG) 30.36
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(9) 0002530
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO.
LEAKAGE .005 CFM @ 10.5 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE 2B : I.D. .227
ASSUMED MOISTURE 11.1
SAMPLE BOX NUMBER
METER BOX NUMBER FB6
METER HEAD DIFF. 1.50

PROBE HEATER SETTING 400.
HEATER BOX SETTING 320.

K FACTOR 1023.1

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1230	162.434									
	10.0	0	168.474	.720	.95	.95	314.	52.	52.	4.5	320.	48.
	20.0	0	174.553	.720	.95	.95	317.	52.	52.	4.5	324.	48.
	30.0	0	180.584	.720	.95	.95	318.	58.	52.	5.0	323.	50.
	40.0	0	186.800	.750	.99	.99	318.	61.	52.	5.5	322.	50.
	50.0	0	192.990	.750	.99	.99	317.	64.	54.	6.0	322.	51.
	60.0	0	199.064	.720	.95	.95	317.	65.	56.	6.5	324.	50.
	70.0	0	205.137	.720	.95	.95	317.	66.	56.	6.5	327.	50.
	80.0	0	211.094	.700	.92	.92	318.	66.	58.	7.0	328.	50.
	90.0	0	217.103	.700	.92	.92	318.	67.	59.	7.5	330.	51.
	100.0	0	223.214	.720	.95	.95	317.	68.	60.	7.5	323.	50.
	110.0	0	229.300	.720	.95	.95	318.	69.	60.	8.0	327.	50.
	120.0	1430	235.462	.720	.95	.95	319.	69.	60.	8.5	324.	50.
TOTALS AVERAGE	120.0		73.028		.95	.95	317.	63.	56.	6.4	325.	50.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 4BMSRP

UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/08/83	02/08/83

TR	TIME-START	1230	1230
TF	TIME-FINISH	1430	1430
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.227 IN	5.8 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.95 IN-H2O	24.2 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	73.028 CU-FT	2.064 CU-M
TM	AVERAGE GAS METER TEMP	59.5 F	15.3 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	72.468 SCF	2.052 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	184.4	184.4
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	8.680 SCF	.246 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.70	10.70
FMD	MOLE FRACTION DRY GAS	.893	.893
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.30	2.30
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.10	84.10
MD	MOLECULAR WT-DRY STACK GAS	30.27	30.27

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MWS	MOLECULAR WT-STACK GAS	28.96		28.96	
PR	BAROMETRIC PRESSURE	30.36	IN-HG	771.14	MM-HG
PSI	STATIC PRES OF STACK GAS	-1.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.32	IN-HG	770.02	MM-HG
TS	AVERAGE STACK TEMP	317.	F	159.	C
VS	AVG STACK GAS VELOCITY	57.4	FPS	17.5	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	18180460.	SCFH	514816.	SCMH
QS	ACTUAL STACK FLOW RATE	29580184.	ACFH	837622.	ACMH
ISO	PERCENT ISOKINETIC	101.5		101.5	
MN	AMBIENT PARTICULATE MG. EPA 5	398.0		398.0	
CS	AMBIENT PARTICULATE	.0847	GR/DSCF*	193.968	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.4RM5RP

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 73.028 * .960 * (30.36 + .952 / 13.6)}{(60. + 460.)} = 72.468 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 184. = 8.68 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 8.68}{72.468 + 8.68} = 10.70 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 10.7}{100.} = .893$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.3 * 32 / 100) + ((84.1 + .0) * 28 / 100) = 30.27$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.27 * (1. - (10.70 / 100)) + 18. * (10.70 / 100) = 28.96$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VM * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 284.204 / (\text{SQRT}(28.96 * 30.32) * 12.) = 57.40 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 57.40 * 20612.3600/144 = 29580184. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (BWO/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 29580184. * 30.32 * (1. - (10.70/100))}{(317. + 460.)} = 18180460. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * UN)$$

$$ISO = \frac{(305.58 * (317. + 460.)) * ((0.002669 * 184.) + (73.028 * .960 * (30.36 + (.952/13.6)) / (60. + 460.)))}{120. * 57.40 * 30.32 * .227 * .227} = 101.51 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 398.0 * 15.43 / 72.468 = .0847 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/08/83
RUN NUMBER 4CM5B

SAMPLE TYPE MSH
OPERATOR CLARKE
AMBIENT TEMP. (DEG.F) 60.
BAR. PRESS. (IN.HG) 30.36
STATIC PRESS. (IN.H2O) -.60
FILTER NUMBER(S) 3531066
STACK INSIDE DIM. (IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .000 CFM @ 7.0 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .211
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAR
METER BOX NUMBER
METER HEAD DIFF. 1.84

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 957.5

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1230	244.025									
	10.0	1240	249.129	.720	.89	.89	314.	57.	56.	4.0	331.	55.
	20.0	1250	254.111	.720	.89	.89	317.	58.	56.	4.0	316.	56.
	30.0	1300	259.195	.720	.89	.89	318.	64.	57.	4.0	324.	58.
	40.0	1310	264.300	.750	.92	.92	318.	68.	58.	4.5	326.	58.
	50.0	1320	269.444	.750	.92	.92	317.	70.	59.	4.5	325.	56.
	60.0	1330	274.500	.720	.89	.89	317.	72.	60.	5.0	326.	54.
	70.0	1340	279.525	.720	.89	.89	317.	73.	62.	5.0	324.	50.
	80.0	1350	284.465	.700	.86	.86	318.	74.	62.	5.0	325.	50.
	90.0	1400	289.425	.700	.86	.86	318.	74.	64.	5.5	324.	52.
	100.0	1410	294.504	.720	.89	.89	317.	75.	65.	6.0	323.	52.
	110.0	1420	299.622	.720	.89	.89	318.	75.	65.	6.0	326.	54.
	120.0	1430	304.732	.720	.89	.89	319.	76.	66.	6.5	328.	56.
TOTALS AVERAGE	120.0		60.707		.89	.89	317.	70.	61.	5.0	325.	54.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 4CM5B UNIT TWO EAST

ENGLISH UNITS

METRIC UNITS

TEST DATE

02/08/83

02/08/83

TR	TIME-START	1230	1230
TF	TIME-FINISH	1430	1430
TT	NET TIME OF TEST, MIN.	120.0	120.0
NP	NET SAMPLING POINTS	12	12
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.211 IN	5.4 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.89 IN-H2O	22.6 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	60.707 CU-FT	1.719 CU-M
TM	AVERAGE GAS METER TEMP	65.3 F	18.5 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	61.001 SCF	1.727 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	156.3	156.3
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	7.357 SCF	.208 SCM
BW0	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.76	10.76
FMD	MOLF FRACTION DRY GAS	.892	.892
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.30	2.30
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.10	84.10
MO	MOLECULAR WT-DRY STACK GAS	30.27	30.27

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MWS	MOLECULAR WT-STACK GAS	28.95		28.95	
PB	BAROMETRIC PRESSURE	30.36	IN-HG	771.14	MM-HG
PSI	STATIC PRES OF STACK GAS	-1.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.32	IN-HG	770.02	MM-HG
TS	AVERAGE STACK TEMP	317.	F	159.	C
VS	AVG STACK GAS VELOCITY	57.4	FPS	17.5	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	18169492.	SCFH	514506.	SCMH
QS	ACTUAL STACK FLOW RATE	29584348.	ACFH	837740.	ACMH
ISO	PERCENT ISOKINETIC	99.0		99.0	
MN	AMBIENT PARTICULATE MG. EPA 5	348.6		348.6	
CS	AMBIENT PARTICULATE	.0882 GR/DSCF*		201.831 MG/DSCM	

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 4C5R

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 60.707 * .983 * (30.36 + .890 / 13.6)}{(65. + 460.)} = 61.001 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 156. = 7.36 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$RWO = (100. * VWC) / (VMSTD + VWC)$$

$$RWO = \frac{100. * 7.36}{61.001 + 7.36} = 10.76 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - RWO) / 100.$$

$$FMD = \frac{100. - 10.8}{100.} = .892$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.3 * 32 / 100) + ((84.1 + .0) * 28 / 100) = 30.27$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (RWO / 100)) + 18. * (RWO / 100)$$

$$MWS = 30.27 * (1. - (10.76 / 100)) + 18. * (10.76 / 100) = 28.95$$

STACK GAS VELOCITY AT STACK CONDITIONS

$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$
 $VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNIS)$
 $VS = 85.49 * .84 * 284.204 / (\text{SQRT}(28.95 * 30.32) * 12.) = 57.41 \text{ FPS}$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$QS = VS * AS * 3600/144$
 $QS = 57.41 * 20612.3600/144 = 29584348. \text{ ACFH}$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$QSSTD = 17.647 * QS * PS * (1. - (RHO/100)) / (TS + 460.)$
 $QSSTD = \frac{17.647 * 29584348. * 30.32 * (1. - (10.76/100))}{(317. + 460.)} = 18169492. \text{ SCFH}$

A-7/6
PERCENT ISOKINETIC

$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$
 $ISO = \frac{(305.58 * (317. + 460.)) * ((0.002669 * 156.) + (60.707 * .983 * (30.36 + (.890/13.6)) / (65. + 460.)))}{120. * 57.41 * 30.32 * .211 * .211} = 98.96 \text{ PERCENT}$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$CS = 0.001 * MN * 15.43 / VMSTD$
 $CS = 0.001 * 348.6 * 15.43 / 61.001 = .0882 \text{ GR/DSCF}$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/08/83
RUN NUMBER 4DMSB

SAMPLE TYPE M5B
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.36
STATIC PRESS.(IN.H2O) -.60
FILTER NUMBER(S) 3531068
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .001 CFM @ 9.0 IN.HG
METER CALIB. FACTOR 1.030
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .210
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAD
METER BOX NUMBER
METER HEAD DIFF. 1.88

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 957.5

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL	INLET	OUTLET		
INIT	0	1230	802.979							
	10.0	1240	807.867	.720	.89	.89	314.	54.	54.	4.5 327.
	20.0	1250	812.715	.720	.89	.89	317.	55.	54.	5.0 317.
	30.0	1300	817.535	.720	.89	.89	318.	58.	54.	5.0 312.
	40.0	1310	822.475	.750	.92	.92	318.	60.	54.	6.0 322.
	50.0	1320	827.385	.750	.92	.92	317.	62.	56.	6.0 325.
	60.0	1330	832.265	.720	.89	.89	317.	63.	56.	6.5 312.
	70.0	1340	837.110	.720	.89	.89	317.	63.	57.	7.0 309.
	80.0	1350	841.925	.700	.86	.86	318.	64.	58.	7.0 320.
	90.0	1400	846.725	.700	.86	.86	318.	65.	58.	7.5 326.
	100.0	1410	851.621	.720	.89	.89	317.	66.	60.	8.0 310.
	110.0	1420	856.475	.720	.89	.89	318.	66.	60.	8.5 318.
	120.0	1430	861.373	.720	.89	.89	319.	66.	60.	9.0 327.
TOTALS AVERAGE	120.0		58.394		.89	.89	317.	62.	57.	6.7 319.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 4DM5B

UNIT TWO EAST

ENGLISH UNITS

MEIRIC UNITS

TEST DATE

02/08/83

02/08/83

TR TIME-START
TF TIME-FINISH

1230
1430

1230
1430

TT NET TIME OF TEST, MIN.

120.0

120.0

NP NET SAMPLING POINTS

12

12

Y METER CALIBRATION FACTOR

1.030

1.030

DN SAMPLING NOZZLE DIAMETER

.210 IN

5.3 MM

CP PITOT TUBE COEFFICIENT

.84

.84

PM AVERAGE ORIFICE PRESSURE
DROP

.89 IN-H2O

22.6 MM-H2O

VM VOLUME OF DRY GAS SAMPLED
AT METER CONDITIONS

58.394 CU-FT

1.654 CU-M

TM AVERAGE GAS METER TEMP

59.3 F

15.2 C

VMSTD VOLUME OF DRY GAS SAMPLED
AT STANDARD CONDITIONS*

62.187 SCF

1.761 SCM

VLC TOTAL H2O COLLECTED IN
IMPINGERS AND SILICA GEL, ML.

159.4

159.4

VWC VOLUME OF WATER VAPOR
AT STANDARD CONDITIONS*

7.503 SCF

.212 SCM

BWD PERCENT MOISTURE BY VOLUME
(CHECK AGAINST SATURATION
POINT HAS BEEN MADE.)

10.77

10.77

FMD MOLE FRACTION DRY GAS

.892

.892

PCO2 PERCENT CO2 BY VOL., DRY

13.60

13.60

PO2 PERCENT O2 BY VOL., DRY

2.30

2.30

PCO PERCENT CO BY VOL., DRY

.00

.00

PN2 PERCENT N2 BY VOL., DRY

84.10

84.10

MD MOLECULAR WT-DRY STACK GAS

30.27

30.27

MWS	MOLECULAR WT-STACK GAS	28.95		28.95	
PB	BAROMETRIC PRESSURE	30.36	IN-HG	771.14	MM-HG
PSI	STATIC PRES OF STACK GAS	-6.60	IN-H2O	-15.24	MM-H2O
PS	STACK PRES, ABS.	30.32	IN-HG	770.02	MM-HG
TS	AVERAGE STACK TEMP	317.	F	159.	C
VS	AVG STACK GAS VELOCITY	57.4	FPS	17.5	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	18168904.	SCFH	514489.	SCMH
QS	ACTUAL STACK FLOW RATE	29584568.	ACFH	837746.	ACMH
ISO	PERCENT ISOKINETIC	101.9		101.9	
MN	AMBIENT PARTICULATE MG, EPA 5	346.0		346.0	
CS	AMBIENT PARTICULATE	.0858	GR/DSCF*	196.503	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 40M5R

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PH + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 58.394 * 1.030 * (30.36 + .890 / 13.6)}{(59. + 460.)} = 62.187 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 159. = 7.50 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 7.50}{62.187 + 7.50} = 10.77 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 10.8}{100.} = .892$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.3 * 32 / 100) + ((84.1 + .0) * 28 / 100) = 30.27$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.27 * (1. - (10.77 / 100)) + 18. * (10.77 / 100) = 28.95$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VM * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 284.204 / (\text{SQRT}(28.95 * 30.32) * 12.) = 57.41 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 57.41 * 20612.3600/144 = 29584568. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 29584568. * 30.32 * (1. - (10.77/100))}{(317. + 460.)} = 18168904. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (317. + 460.)) * ((0.002669 * 159.) + (58.394 * 1.030 * (30.36 + (.890/13.6)) / (59. + 460.)))}{120. * 57.41 * 30.32 * .210 * .210} = 101.85 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 346.0 * 15.43 / 62.187 = .0858 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE M5R
OPERATOR PR RA
AMBIENT TEMP. (DEG.F) 60.
BAR. PRESS. (IN.HG) 30.05
STATIC PRESS. (IN.H2O) -.80
FILTER NUMBER(S) 3531067
STACK INSIDE DTM. (IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .000 CFM @ 7.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/11/83
RUN NUMBER 5AM5R

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE 1A : I.D. .223
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER F84
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1116.0

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	755	708.102									
	10.0	805	713.796	.700	1.03	1.03	301.	63.	62.	4.0	327.	52.
	20.0	815	719.262	.650	.95	.95	303.	64.	62.	4.0	341.	52.
	30.0	825	724.692	.650	.95	.95	305.	68.	62.	4.0	377.	53.
	40.0	835	730.183	.650	.95	.95	305.	70.	62.	5.0	321.	53.
	50.0	845	735.892	.700	1.02	1.02	305.	73.	63.	5.5	330.	54.
	60.0	855	741.423	.650	.95	.95	304.	75.	64.	5.5	331.	54.
	70.0	905	746.950	.650	.95	.95	305.	77.	65.	6.0	330.	52.
	80.0	915	752.500	.650	.95	.95	304.	78.	66.	6.0	323.	52.
	90.0	925	757.988	.650	.95	.95	307.	79.	68.	6.5	324.	52.
TOTALS AVERAGE	90.0		49.886		.97	.97	304.	72.	64.	5.2	334.	53.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA

TEST 5AMSB UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83
TB	TIME-START	755	755
TF	TIME-FINISH	925	925
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.223 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.97 IN-H ₂ O	24.6 MM-H ₂ O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	49.886 CU-FT	1.413 CU-M
TM	AVERAGE GAS METER TEMP	67.8 F	19.9 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	50.388 SCF	1.427 SCM
VLC	TOTAL H ₂ O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	138.6	138.6
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.524 SCF	.185 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.46	11.46
FMD	MOLE FRACTION DRY GAS	.885	.885
PCO ₂	PERCENT CO ₂ BY VOL., DRY	12.80	12.80
PO ₂	PERCENT O ₂ BY VOL., DRY	3.25	3.25
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN ₂	PERCENT N ₂ BY VOL., DRY	83.95	83.95
MD	MOLECULAR WT-DRY STACK GAS	30.18	30.18

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MWS	MOLECULAR WT-STACK GAS	28.78		28.78	
PB	BAROMETRIC PRESSURE	30.05	IN-HG	763.27	MM-HG
PSI	STATIC PRES OF STACK GAS	- .80	IN-H2O	-20.32	MM-H2O
PS	STACK PRES, ABS.	29.99	IN-HG	761.78	MM-HG
TS	AVERAGE STACK TEMP	304.	F	151.	C
VS	AVG STACK GAS VELOCITY	54.9	FPS	16.7	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSD	STACK FLOW RATE, DRY*	17355016.	SCFH	491442.	SCMH
QS	ACTUAL STACK FLOW RATE	28308684.	ACFH	801617.	ACMH
ISO	PERCENT ISOKINETIC	102.2		102.2	
MN	AMBIENT PARTICULATE MG. EPA 5	235.5		235.5	
CS	AMBIENT PARTICULATE	.0721	GR/DSCF*	165.067	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 5AM5B

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PR + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 49.886 * 1.003 * (30.05 + .967 / 13.6)}{(68. + 460.)} = 50.388 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 139. = 6.52 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 6.52}{50.388 + 6.52} = 11.46 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.5}{100.} = .885$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (12.80 * 44 / 100) + (3.3 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.18$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.18 * (1. - (11.46 / 100)) + 18. * (11.46 / 100) = 28.78$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 202.286 / (\text{SQRT}(28.78 * 29.99) * 9.) = 54.94 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 54.94 * 20612.3600/144 = 28308684. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28308684. * 29.99 * (1. - (11.46/100))}{(304. + 460.)} = 17355016. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PR + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (304. + 460.)) * ((0.002669 * 139.) + (49.886 * 1.003 * (30.05 + (.967/13.6)) / (68. + 460.)))}{90. * 54.94 * 29.99 * .223 * .223} = 102.16 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 235.5 * 15.43 / 50.388 = .0721 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/11/83
RUN NUMBER 5HMSB

SAMPLE TYPE MSR
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 60.
RAP.PRESS.(IN.HG) 30.05
STATIC PRESS.(IN.H2O) -.80
FILTER NUMBER(S) 3531013
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TURE COEFF. .84
THERM. NO. 206
LEAKAGE .000 CFM @ 8.5 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE 1/8 : I.D. .221
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER FB6
METER HEAD DIFF. 1.50

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.
K FACTOR 938.8

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	755	236.455									
	10.0	805	242.410	.700	.86	.86	301.	56.	58.	4.0	322.	52.
	20.0	815	247.969	.650	.80	.80	303.	57.	58.	3.5	340.	52.
	30.0	825	253.558	.650	.80	.80	305.	62.	58.	4.0	332.	52.
	40.0	835	259.176	.650	.80	.80	305.	65.	59.	4.0	336.	53.
	50.0	845	265.000	.700	.86	.86	305.	67.	59.	4.0	337.	53.
	60.0	855	270.627	.650	.80	.80	304.	69.	60.	4.0	329.	55.
	70.0	905	276.234	.650	.80	.80	305.	70.	61.	5.5	333.	50.
	80.0	915	281.856	.650	.80	.80	304.	71.	62.	6.0	329.	50.
	90.0	925	287.555	.650	.80	.80	307.	72.	63.	6.0	327.	51.
TOTALS AVERAGE	90.0		51.100		.81	.81	304.	65.	60.	4.6	332.	52.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST SRM5B UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TB	TIME-START	755	755
TF	TIME-FINISH	925	925
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.81 IN-H2O	20.7 MM-H2O
8VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	51.100 CU-FT	1.447 CU-M
TM	AVERAGE GAS METER TEMP	62.6 F	17.0 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	49.876 SCF	1.412 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	137.2	137.2
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.458 SCF	.183 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.46	11.46
FMD	MOLE FRACTION DRY GAS	.885	.885
PCO2	PERCENT CO2 BY VOL., DRY	12.80	12.80
PO2	PERCENT O2 BY VOL., DRY	3.25	3.25
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.95	83.95
MD	MOLECULAR WT-DRY STACK GAS	30.18	30.18

MWS	MOLECULAR WT-STACK GAS	28.78		28.78	
PB	BAROMETRIC PRESSURE	30.05	IN-HG	763.27	MM-HG
PSI	STATIC PRES OF STACK GAS	- .80	IN-H2O	-20.32	MM-H2O
PS	STACK PRES, ABS.	29.99	IN-HG	761.78	MM-HG
TS	AVERAGE STACK TEMP	304.	F	151.	C
VS	AVG STACK GAS VELOCITY	54.9	FPS	16.7	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17354928.	SCFH	491440.	SCMH
QS	ACTUAL STACK FLOW RATE	28308716.	ACFH	801618.	ACMH
ISO	PERCENT ISOKINETIC	103.0		103.0	
MN	AMBIENT PARTICULATE MG. EPA 5	230.9		230.9	
CS	AMBIENT PARTICULATE	.0714	GR/DSCF*	163.503	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 58M58

UNIT 2 FAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 51.100 * .960 * (30.05 + .813 / 13.6)}{(63. + 460.)} = 49.876 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 137. = 6.46 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 6.46}{49.876 + 6.46} = 11.46 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.5}{100.} = .885$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (12.80 * 44 / 100) + (3.3 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.18$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.18 * (1. - (11.46 / 100)) + 18. * (11.46 / 100) = 28.78$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SIIM. OF THE SORT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SORT}(MWS * PS) * PNIS)$$

$$VS = 85.49 * .84 * 202.286 / (\text{SORT}(28.78 * 29.99) * 9.) = 54.94 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 54.94 * 20612.7600/144 = 28308716. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RW0/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28308716. * 29.99 * (1. - (11.46/100))}{(304. + 460.)} = 17354928. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (304. + 460.)) * ((0.002669 * 137.) + (51.100 * .960 * (30.05 + (.813/13.6)) / (63. + 460.)))}{90. * 54.94 * 29.99 * .221 * .221} = 102.96 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 230.9 * 15.43 / 49.876 = .0714 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

SAMPLE TYPE M5B
OPERATOR CLARKE
AMBIENT TEMP. (DEG.F) 60.
BAR. PRESS. (IN.HG) 30.05
STATIC PRESS. (IN.H2O) -.80
FILTER NUMBER(S) 3531124
STACK INSIDE DIM. (IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .000 CFM @ 11.0 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/11/83
RUN NUMBER 5CM5R

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .221
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAC
METER BOX NUMBER FR5
METER HEAD DIFF. 1.84

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1070.1

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRFD	ACTUAL		INLET	OUTLET			
INIT	0	755	306.333									
	10.0	805	311.845	.700	.98	.98	301.	62.	62.	5.0	327.	56.
	20.0	815	317.000	.650	.91	.91	303.	64.	62.	4.5	324.	54.
	30.0	825	322.180	.650	.91	.91	303.	70.	62.	5.0	322.	52.
	40.0	835	327.245	.650	.91	.91	303.	74.	63.	5.5	326.	54.
	50.0	845	332.630	.700	.98	.98	305.	77.	64.	6.0	329.	50.
	60.0	855	337.737	.650	.91	.91	304.	79.	69.	6.5	336.	50.
	70.0	905	342.945	.650	.91	.91	305.	80.	67.	6.5	336.	52.
	80.0	915	348.190	.650	.91	.91	304.	80.	68.	7.0	332.	50.
	90.0	925	353.282	.650	.91	.91	307.	81.	69.	7.0	312.	48.
TOTALS AVERAGE	90.0		46.949		.93	.93	304.	74.	65.	5.9	327.	52.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKF

TEST 5CM5B UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TB	TIME-START	755	755
TF	TIME-FINISH	925	925
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.93 IN-H2O	23.5 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	46.949 CU-FT	1.329 CU-M
TM	AVERAGE GAS METER TEMP	69.6 F	20.9 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	46.315 SCF	1.311 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	131.6	131.6
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.194 SCF	.175 SCM
BW0	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.80	11.80
FMD	MOLF FRACTION DRY GAS	.882	.882
PCO2	PERCENT CO2 BY VOL., DRY	12.80	12.80
PO2	PERCENT O2 BY VOL., DRY	3.25	3.25
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.95	83.95
MD	MOLECULAR WT-DRY STACK GAS	30.18	30.18

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MWS	MOLECULAR WT-STACK GAS	28.74		28.74	
PR	BAROMETRIC PRESSURE	30.05	IN-HG	763.27	MM-HG
PSI	STATIC PRES OF STACK GAS	- .80	IN-H2O	-20.32	MM-H2O
PS	STACK PRES, ABS.	29.99	IN-HG	761.78	MM-HG
TS	AVERAGE STACK TEMP	304.	F	151.	C
VS	AVG STACK GAS VELOCITY	55.0	FPS	16.8	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17306912.	SCFH	490080.	SCMH
QS	ACTUAL STACK FLOW RATE	28320512.	ACFH	801952.	ACMH
ISO	PERCENT ISOKINETIC	95.9		95.9	
MN	AMBIENT PARTICULATE MG. EPA 5	219.2		219.2	
CS	AMBIENT PARTICULATE	.0730 GR/DSCF*		167.153	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 5CM5B

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 46.949 * .983 * (30.05 + .926 / 13.6)}{(70. + 460.)} = 46.315 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 132. = 6.19 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$RWD = (100. * VWC) / (VMSTD + VWC)$$

$$RWD = \frac{100. * 6.19}{46.315 + 6.19} = 11.80 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - RWD) / 100.$$

$$FMD = \frac{100. - 11.8}{100.} = .882$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (12.80 * 44 / 100) + (3.3 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.18$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (RWD / 100)) + 18. * (RWD / 100)$$

$$MWS = 30.18 * (1. - (11.80 / 100)) + 18. * (11.80 / 100) = 28.74$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 202.227 / (\text{SQRT}(28.74 * 29.99) * 9.) = 54.96 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 54.96 * 20612.3600/144 = 28320512. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWD/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28320512. * 29.99 * (1. - (11.80/100))}{(304. + 460.)} = 17306912. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (304. + 460.)) * ((0.002669 * 132.) + (46.949 * .983 * (30.05 + (.926/13.6)) / (70. + 460.)))}{90. * 54.96 * 29.99 * .221 * .221} = 95.87 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 219.2 * 15.43 / 46.315 = .0730 \text{ GR/DSCF}$$

FIELD DATA

PLANT.
SAMPLING LOCATION UNIT TWO EAST

DATE 02/11/83
RUN NUMBER 50M5H

SAMPLE TYPE M5H
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.05
STATIC PRESS.(IN.H2O) -.80
FILTER NUMBER(S) 3531123
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .010 CFM @ 8.0 IN.HG
METER CALIB. FACTOR 1.030
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .215
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAD
METER BOX NUMBER FR4
METER HEAD DIFF. 1.88

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1070.1

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
A-97	INIT	0	755	863.797								
	10.0	805	868.940	.700	.98	.98	301.	58.	58.	2.5	311.	52.
	20.0	815	874.125	.650	.91	.91	303.	60.	58.	2.5	317.	52.
	30.0	825	878.910	.650	.91	.91	305.	66.	62.	3.0	322.	50.
	40.0	835	883.833	.650	.91	.91	305.	68.	60.	3.0	325.	50.
	50.0	845	889.000	.700	.98	.98	305.	70.	62.	3.5	321.	48.
	60.0	855	893.845	.650	.91	.91	304.	71.	62.	4.0	315.	52.
	70.0	905	898.939	.650	.91	.91	305.	72.	64.	4.0	319.	50.
	80.0	915	903.900	.650	.91	.91	304.	73.	66.	4.5	325.	52.
	90.0	925	908.861	.650	.91	.91	307.	74.	66.	5.0	314.	50.
TOTALS	90.0		45.064									
AVERAGE					.93	.93	304.	68.	62.	3.6	319.	51.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKF

TEST SDMSB UNIT TWO EAST

ENGLISH UNITS

METRIC UNITS

TEST DATE

02/11/83

02/11/83

TR
TF

TIME-START
TIME-FINISH

755
925

755
925

TT NET TIME OF TEST, MIN.

90.0

90.0

NP NET SAMPLING POINTS

9

9

Y METER CALIBRATION FACTOR

1.030

1.030

DN SAMPLING NOZZLE DIAMETER

.215 IN

5.5 MM

CP PITOT TUBE COEFFICIENT

.84

.84

PM AVERAGE ORIFICE PRESSURE
DROP

.93 IN-H2O

23.5 MM-H2O

VM VOLUME OF DRY GAS SAMPLED
AT METER CONDITIONS

45.064 CU-FT

1.276 CU-M

TM AVERAGE GAS METER TEMP

65.0 F

18.3 C

VMSTU VOLUME OF DRY GAS SAMPLED
AT STANDARD CONDITIONS*

46.990 SCF

1.331 SCM

VLC TOTAL H2O COLLECTED IN
IMPINGERS AND SILICA GEL, ML.

132.8

132.8

VWC VOLUME OF WATER VAPOR
AT STANDARD CONDITIONS*

6.251 SCF

.177 SCM

BWD PERCENT MOISTURE BY VOLUME
(CHECK AGAINST SATURATION
POINT HAS BEEN MADE.)

11.74

11.74

FMD MOLE FRACTION DRY GAS

.883

.883

PCO2 PERCENT CO2 BY VOL., DRY

12.80

12.80

PO2 PERCENT O2 BY VOL., DRY

3.25

3.25

PCO PERCENT CO BY VOL., DRY

.00

.00

PN2 PERCENT N2 BY VOL., DRY

83.95

83.95

MD MOLECULAR WT-DRY STACK GAS

30.18

30.18

A-98

MWS	MOLECULAR WT-STACK GAS	28.75		28.75	
PB	BAROMETRIC PRESSURE	30.05	IN-HG	763.27	MM-HG
PSI	STATIC PRES OF STACK GAS	-1.80	IN-H2O	-20.32	MM-H2O
PS	STACK PRES, ABS.	29.99	IN-HG	761.78	MM-HG
TS	AVERAGE STACK TEMP	304.	F	151.	C
VS	AVG STACK GAS VELOCITY	55.0	FPS	16.8	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17310776.	SCFH	490189.	SCMH
QS	ACTUAL STACK FLOW RATE	28325324.	ACFH	802088.	ACMH
ISO	PERCENT ISOKINETIC	102.8		102.8	
MN	AMBIENT PARTICULATE MG. EPA 5	217.9		217.9	
CS	AMBIENT PARTICULATE	.0716	GR/DSCF*	163.775	MG/DSCM

A-99

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 50M5R

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 45.064 * 1.030 * (30.05 + .926 / 13.6)}{(65. + 460.)} = 46.990 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 133. = 6.25 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$RWD = (100. * VWC) / (VMSTD + VWC)$$

$$RWD = \frac{100. * 6.25}{46.990 + 6.25} = 11.74 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - RWD) / 100.$$

$$FMD = \frac{100. - 11.7}{100.} = .883$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCU) * .28$$

$$MD = (12.80 * 44 / 100) + (3.3 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.18$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (RWD / 100)) + 18. * (RWD / 100)$$

$$MWS = 30.18 * (1. - (11.74 / 100)) + 18. * (11.74 / 100) = 28.75$$

A-100

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQR}(\text{VH} * (\text{TS} + 460.))$$

$$\text{VS} = 85.49 * \text{CP} * \text{DEL P} / (\text{SQR}(\text{MWS} * \text{PS}) * \text{PNTS})$$

$$\text{VS} = 85.49 * .84 * 202.286 / (\text{SQR}(28.75 * 29.99) * 9.) = 54.97 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$\text{QS} = \text{VS} * \text{AS} * 3600/144$$

$$\text{QS} = 54.97 * 20612.3600/144 = 28325324. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$\text{QSSTD} = 17.647 * \text{QS} * \text{PS} * (1. - (\text{BW0}/100)) / (\text{TS} + 460.)$$

$$\text{QSSTD} = \frac{17.647 * 28325324. * 29.99 * (1. - (11.74/100))}{(304. + 460.)} = 17310776. \text{ SCFH}$$

PERCENT ISOKINETIC

$$\text{ISO} = (305.58 * (\text{TS} + 460.)) * ((0.002669 * \text{VLC}) + (\text{VM} * \text{Y} * (\text{PR} + (\text{PM}/13.6)) / (\text{TM} + 460.))) / (\text{TT} * \text{VS} * \text{PS} * \text{DN} * \text{DN})$$

$$\text{ISO} = \frac{(305.58 * (304. + 460.)) * ((0.002669 * 133.) + (45.064 * 1.030 * (30.05 + (.926/13.6)) / (65. + 460.)))}{90. * 54.97 * 29.99 * .215 * .215} = 102.75 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$\text{CS} = 0.001 * \text{MN} * 15.43 / \text{VMSTD}$$

$$\text{CS} = 0.001 * 217.9 * 15.43 / 46.990 = .0716 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/11/83
RUN NUMBER 6AM5R

SAMPLE TYPE MSB
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.10
STATIC PRESS.(IN.H2O) .25
FILTER NUMBER(S) 3531061
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .000 CFM @ 8.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE 2A : I.D. .224
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER FB4
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1139.1

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRFD	ACTUAL	INLET OUTLET			
INIT	0	1050	758.131							
	10.0	1100	763.876	.700	1.03	1.03	311.	70.	68.	4.5 315. 66.
	20.0	1110	769.397	.650	.96	.96	313.	71.	68.	4.5 328. 60.
	30.0	1120	774.920	.650	.96	.96	313.	75.	68.	5.0 346. 60.
	40.0	1130	780.453	.650	.96	.96	315.	78.	69.	5.5 316. 60.
	50.0	1140	786.057	.670	.98	.98	316.	80.	70.	6.0 329. 60.
	60.0	1150	791.653	.670	.98	.98	314.	81.	71.	6.5 321. 60.
	70.0	1200	797.273	.670	.98	.98	316.	82.	72.	7.0 336. 59.
	80.0	1210	802.831	.650	.96	.96	315.	82.	72.	7.0 338. 62.
	90.0	1220	808.399	.650	.96	.96	317.	84.	73.	7.5 338. 62.
TOTALS AVERAGE	90.0		50.268		.97	.97	314.	78.	70.	5.9 330. 61.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 6AM58 UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TS	TIME-START	1050	1050
TF	TIME-FINISH	1220	1220
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.224 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.97 IN-H2O	24.8 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	50.268 CU-FT	1.423 CU-M
TM	AVERAGE GAS METER TEMP	74.1 F	23.4 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	50.261 SCF	1.423 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	137.6	137.6
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.477 SCF	.183 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.42	11.42
FMD	MOLE FRACTION DRY GAS	.886	.886
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.50	2.50
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.90	83.90
MD	MOLECULAR WT-DRY STACK GAS	30.28	30.28

MWS	MOLECULAR WT-STACK GAS	28.87		28.87	
PR	BAROMETRIC PRESSURE	30.10	IN-HG	764.54	MM-HG
PSI	STATIC PRES OF STACK GAS	.25	IN-H2O	6.35	MM-H2O
PS	STACK PRES, ABS.	30.12	IN-HG	765.01	MM-HG
TS	AVERAGE STACK TEMP	314.	F	157.	C
VS	AVG STACK GAS VELOCITY	55.1	FPS	16.8	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17274784.	SCFH	489170.	SCMH
QS	ACTUAL STACK FLOW RATE	28414632.	ACFH	804617.	ACMH
ISO	PERCENT ISOKINETIC	101.5		101.5	
MN	AMBIENT PARTICULATE MG. EPA 5	229.3		229.3	
CS	AMBIENT PARTICULATE	.0704	GR/DSCF*	161.127	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 6AM5H

UNIT 2 FAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 50.268 * 1.003 * (30.10 + .974 / 13.6)}{(74. + 460.)} = 50.261 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 138. = 6.48 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 6.48}{50.261 + 6.48} = 11.42 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.4}{100.} = .886$$

AVFRAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.5 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.28$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.28 * (1. - (11.42 / 100)) + 18. * (11.42 / 100) = 28.87$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VM * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 203.800 / (\text{SQRT}(28.87 * 30.12) * 9.) = 55.14 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.14 * 20612.3600/144 = 28414632. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28414632. * 30.12 * (1. - (11.42/100))}{(314. + 460.)} = 17274784. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PR + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (314. + 460.)) * ((0.002669 * 138.) + (50.268 * 1.003 * (30.10 * (.974/13.6)) / (74. + 460.)))}{90. * 55.14 * 30.12 * .224 * .224} = 101.46 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 229.3 * 15.43 / 50.261 = .0704 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/11/83
RUN NUMBER 68M5R

SAMPLE TYPE M5H
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.10
STATIC PRESS.(IN.H2O) .25
FILTER NUMBER(S) 3531062
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .000 CFM @ 8.5 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .227
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER
METER HEAD DIFF. 1.50
PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.
K FACTOR 941.3

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					----- DESIRED ACTUAL					
					----- INLET OUTLET					
INIT	0	1050	287.808							
	10.0	1100	293.165	.700	.85	.85	311.	63.	63.	4.0 319. 60.
	20.0	1110	299.214	.650	.79	.79	313.	64.	63.	4.0 335. 56.
	30.0	1120	304.890	.650	.79	.79	313.	68.	64.	4.5 332. 56.
	40.0	1130	310.472	.650	.79	.79	315.	72.	64.	4.5 319. 56.
	50.0	1140	316.167	.670	.81	.81	316.	74.	66.	5.0 329. 58.
	60.0	1150	321.872	.670	.81	.81	314.	75.	67.	6.0 332. 58.
	70.0	1200	327.592	.670	.81	.81	316.	76.	68.	6.0 326. 58.
	80.0	1210	333.200	.650	.79	.79	315.	77.	69.	6.5 330. 60.
	90.0	1220	338.850	.650	.79	.79	317.	77.	69.	7.0 336. 60.
TOTALS AVERAGE	90.0		51.042		.80	.80	314.	72.	66.	5.3 329. 58.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 68M58 UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83
TS	TIME-START	1050	1050
TF	TIME-FINISH	1220	1220
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.227 IN	5.8 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.80 IN-H2O	20.4 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	51.042 CU-FT	1.445 CU-M
TM	AVERAGE GAS METER TEMP	68.8 F	20.5 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	49.314 SCF	1.396 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	136.3	136.3
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.416 SCF	.182 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.51	11.51
FMD	MOLE FRACTION DRY GAS	.885	.885
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.50	2.50
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.90	83.90
MD	MOLECULAR WT-DRY STACK GAS	30.28	30.28

A-108

MWS	MOLECULAR WT-STACK GAS	28.86		28.86	
PB	BAROMETRIC PRESSURE	30.10	IN-HG	764.54	MM-HG
PSI	STATIC PRES OF STACK GAS	.25	IN-H2O	6.35	MM-H2O
PS	STACK PRES, ABS.	30.12	IN-HG	765.01	MM-HG
TS	AVERAGE STACK TEMP	314.	F	157.	C
VS	AVG STACK GAS VELOCITY	55.2	FPS	16.8	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17259472.	SCFH	498737.	SCMH
QS	ACTUAL STACK FLOW RATE	28420484.	ACFH	804783.	ACMH
ISO	PERCENT ISOKINETIC	97.0		97.0	
MN	AMBIENT PARTICULATE MG. EPA 5	216.8		216.8	
CS	AMBIENT PARTICULATE	.0678	GR/DSCF*	155.269	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 68M5H

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 51.042 * .960 * (30.10 + .803 / 13.6)}{(69. + 460.)} = 49.314 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 136. = 6.42 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$RWO = (100. * VWC) / (VMSTD + VWC)$$

$$RWO = \frac{100. * 6.42}{49.314 + 6.42} = 11.51 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - RWO) / 100.$$

$$FMD = \frac{100. - 11.5}{100.} = .885$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.5 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.28$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (RWO / 100)) + 18. * (RWO / 100)$$

$$MWS = 30.28 * (1. - (11.51 / 100)) + 18. * (11.51 / 100) = 28.86$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQR}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQR}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 203.800 / (\text{SQR}(28.86 * 30.12) * 9. = 55.15 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.15 * 20612.3600/144 = 28420484. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (RWD/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 28420484. * 30.12 * (1. - (11.51/100))}{(314. + 460.)} = 17259472. \text{ SCFH}$$

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PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (314. + 460.)) * ((0.002669 * 136.) + (51.042 * .960 * (30.10 + (.803/13.6)) / (69. + 460.)))}{90. * 55.15 * 30.12 * .227 * .227} = 97.02 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 216.8 * 15.43 / 49.314 = .0678 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

SAMPLE TYPE MSR
OPERATOR CLARKE
AMBIENT TEMP. (DEG.F) 60.
BAR. PRESS. (IN.HG) 30.10
STATIC PRESS. (IN.H2O) .25
FILTER NUMBER(S) 3531108
STACK INSIDE DIM. (IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .000 CFM @ .6 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/11/83
RUN NUMBER 6CM58
PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .211
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAC
METER BOX NUMBER FRS
METER HEAD DIFF. 1.84
PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.
K FACTOR 937.4

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1050	353.557									
	10.0	1100	358.565	.700	.85	.85	311.	68.	68.	3.5	313.	59.
	20.0	1110	363.343	.650	.79	.79	313.	70.	68.	3.5	320.	58.
	30.0	1120	368.650	.650	.79	.79	313.	74.	69.	4.0	319.	57.
	40.0	1130	373.500	.650	.79	.79	315.	80.	70.	4.0	322.	60.
	50.0	1140	378.300	.670	.81	.81	316.	82.	71.	4.5	316.	60.
	60.0	1150	382.780	.670	.81	.81	314.	84.	72.	4.5	326.	59.
	70.0	1200	387.625	.670	.81	.81	316.	84.	73.	5.0	323.	57.
	80.0	1210	392.655	.650	.79	.79	315.	85.	74.	5.0	327.	60.
	90.0	1220	397.318	.650	.78	.78	317.	86.	75.	5.5	326.	60.
TOTALS AVERAGE	90.0		43.761		.80	.80	314.	79.	71.	4.4	321.	59.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 6CM5B UNIT TWO EAST

ENGLISH UNITS

METRIC UNITS

TEST DATE

02/11/83

02/11/83

TS	TIME-START	1050	1050
TF	TIME-FINISH	1220	1220
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.211 IN	5.4 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.80 IN-H2O	20.4 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	43.761 CU-FT	1.239 CU-M
TM	AVERAGE GAS METER TEMP	75.2 F	24.0 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	42.780 SCF	1.211 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	117.7	117.7
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	5.540 SCF	.157 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.47	11.47
FMD	MOLE FRACTION DRY GAS	.885	.885
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.50	2.50
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.90	83.90
MD	MOLECULAR WT-DRY STACK GAS	30.28	30.28

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MWS	MOLECULAR WT-STACK GAS	28.87		28.87	
PR	BAROMETRIC PRESSURE	30.10	IN-HG	764.54	MM-HG
PSI	STATIC PRES OF STACK GAS	.25	IN-H2O	6.35	MM-H2O
PS	STACK PRES, ABS.	30.12	IN-HG	765.01	MM-HG
TS	AVERAGE STACK TEMP	314.	F	157.	C
VS	AVG STACK GAS VELOCITY	55.1	FPS	16.8	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17266852.	SCFH	488945.	SCMH
QS	ACTUAL STACK FLOW RATE	28417676.	ACFH	804703.	ACMH
ISO	PERCENT ISOKINETIC	97.4		97.4	
MN	AMBIENT PARTICULATE MG. EPA 5	169.6		169.6	
CS	AMBIENT PARTICULATE	.0612	GR/DSCF*	140.017	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 6CM5R

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PH + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 43.761 * .983 * (30.10 + .802 / 13.6)}{(75. + 460.)} = 42.780 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 118. = 5.54 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 5.54}{42.780 + 5.54} = 11.47 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.5}{100.} = .885$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.5 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.28$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.28 * (1. - (11.47 / 100)) + 18. * (11.47 / 100) = 28.87$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 203.800 / (\text{SQRT}(28.87 * 30.12) * 9. = 55.15 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.15 * 20612.3600/144 = 28417676. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWN/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28417676. * 30.12 * (1. - (11.47/100))}{(314. + 460.)} = 17266852. \text{ SCFH}$$

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PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (1T * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (314. + 460.)) * ((0.002669 * 118.) + (43.761 * .983 * (30.10 * (.802/13.6)) / (75. + 460.)))}{90. * 55.15 * 30.12 * .211 * .211} = 97.37 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 169.6 * 15.43 / 42.780 = .0612 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/11/83
RUN NUMBER 6DMSB

SAMPLE TYPE MSH
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.10
STATIC PRESS.(IN.H2O) .25
FILTER NUMBER(S) 3531090
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .015 CFM @ 7.0 IN.HG
METER CALIB. FACTOR 1.030
HEAD & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .210
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAU
METER BOX NUMBER FB4
METER HEAD DIFF. 1.88

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 937.4

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					----- DESIRED ACTUAL	----- INLET OUTLET				
INIT	0	1050	909.442							
A-117	10.0	1100	914.580	.700	.85 .85	311.	66. 65.	5.0	312.	62.
	20.0	1110	919.185	.650	.79 .79	313.	68. 66.	4.5	328.	60.
	30.0	1120	924.225	.650	.79 .79	313.	71. 66.	5.0	332.	58.
	40.0	1130	928.600	.650	.79 .79	315.	74. 68.	5.5	333.	61.
	50.0	1140	933.490	.670	.81 .81	316.	76. 69.	5.5	326.	60.
	60.0	1150	937.937	.670	.81 .81	314.	77. 70.	6.0	326.	59.
	70.0	1200	942.445	.670	.81 .81	316.	78. 71.	6.5	309.	58.
	80.0	1210	947.200	.650	.79 .79	315.	78. 71.	7.0	321.	59.
	90.0	1220	951.818	.650	.78 .78	317.	78. 72.	7.0	331.	60.
TOTALS AVERAGE	90.0		42.376		.80 .80	314.	74. 69.	5.8	324.	60.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 6DM5H UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83
TB	TIME-START	1050	1050
TF	TIME-FINISH	1220	1220
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	1.030	1.030
DN	SAMPLING NOZZLE DIAMETER	.210 IN	5.3 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.80 IN-H ₂ O	20.4 MM-H ₂ O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	42.376 CU-FT	1.200 CU-M
TM	AVERAGE GAS METER TEMP	71.3 F	21.9 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	43.720 SCF	1.238 SCM
VLC	TOTAL H ₂ O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	116.2	116.2
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	5.470 SCF	.155 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.12	11.12
FMD	MOLE FRACTION DRY GAS	.889	.889
PCO2	PERCENT CO ₂ BY VOL., DRY	13.60	13.60
PO2	PERCENT O ₂ BY VOL., DRY	2.50	2.50
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N ₂ BY VOL., DRY	83.90	83.90
MD	MOLECULAR WT-DRY STACK GAS	30.28	30.28

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MWS	MOLECULAR WT-STACK GAS	28.91		28.91	
PB	BAROMETRIC PRESSURE	30.10	IN-HG	764.54	MM-HG
PSI	STATIC PRES OF STACK GAS	.25	IN-H ₂ O	6.35	MM-H ₂ O
PS	STACK PRES, ABS.	30.12	IN-HG	765.01	MM-HG
TS	AVERAGE STACK TEMP	314.	F	157.	C
VS	AVG STACK GAS VELOCITY	55.1	FPS	16.8	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17321612.	SCFH	490496.	SCMH
QS	ACTUAL STACK FLOW RATE	28396772.	ACFH	804111.	ACMH
ISO	PERCENT ISOKINETIC	100.1		100.1	
MN	AMBIENT PARTICULATE MG. EPA 5	186.1		186.1	
CS	AMBIENT PARTICULATE	.0657 GR/DSCF*		150.336	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 6DM5H

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 42.376 * 1.030 * (30.10 + .802 / 13.6)}{(71. + 460.)} = 43.720 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 116. = 5.47 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 5.47}{43.720 + 5.47} = 11.12 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.1}{100.} = .889$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.5 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.28$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.28 * (1. - (11.12 / 100)) + 18. * (11.12 / 100) = 28.91$$

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STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE } \sqrt{VH * (TS + 460.)}$$

$$VS = 85.49 * CP * DEL P / (\sqrt{MWS * PS}) * PNTS)$$

$$VS = 85.49 * .84 * 203.800 / (\sqrt{28.91 * 30.12}) * 9. = 55.11 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.11 * 20612.3600/144 = 28396772. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (BW0/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 28396772. * 30.12 * (1. - (11.12/100))}{(314. + 460.)} = 17321612. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * UN)$$

$$ISO = \frac{(305.58 * (314. + 460.)) * ((0.002669 * 116.) + (42.376 * 1.030 * (30.10 + (.802/13.6)) / (71. + 460.)))}{90. * 55.11 * 30.12 * .210 * .210} = 100.14 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 186.1 * 15.43 / 43.720 = .0657 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE M5BW
OPERATOR PR RA JP
AMBIENT TEMP. (DEG.F) 65.
BAR. PRESS. (IN.HG) 30.11
STATIC PRESS. (IN.H2O) .20
FILTER NUMBER(S) 35310125
STACK INSIDE DTM. (IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .000 CFM @ 8.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/11/83
RUN NUMBER 7AM5HW

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .223
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER FR4
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.
K FACTOR 1129.5

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRFD	ACTUAL	INLET		OUTLET	
INIT	0	1330	808.703							
	10.0	1340	814.370	.670	.98	.98	315.	76.	74.	4.0 325.
	20.0	1350	819.924	.650	.94	.94	317.	79.	75.	4.0 343.
	30.0	1400	825.527	.670	.98	.98	318.	80.	75.	4.0 330.
	40.0	1410	831.125	.670	.98	.98	318.	83.	75.	4.5 318.
	50.0	1420	836.570	.640	.93	.93	318.	86.	78.	5.0 332.
	60.0	1430	842.295	.700	1.01	1.01	320.	87.	77.	6.0 323.
	70.0	1440	847.913	.670	.97	.97	320.	88.	77.	6.0 327.
	80.0	1450	853.352	.670	.97	.97	321.	88.	78.	6.5 338.
	90.0	1500	859.095	.670	.97	.97	321.	88.	79.	7.0 339.
TOTALS AVERAGE	90.0		50.392		.97	.97	319.	84.	76.	5.2 331.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 7AMSBN UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TS	TIME-START	1330	1330
TF	TIME-FINISH	1500	1500
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.223 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.97 IN-H ₂ O	24.6 MM-H ₂ O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	50.392 CU-FT	1.427 CU-M
TM	AVERAGE GAS METER TEMP	80.2 F	26.8 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	49.836 SCF	1.411 SCM
VLC	TOTAL H ₂ O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	134.9	134.9
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.350 SCF	.180 SCM
BW0	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.30	11.30
FMD	MOLE FRACTION DRY GAS	.887	.887
PCO ₂	PERCENT CO ₂ BY VOL., DRY	13.40	13.40
PO ₂	PERCENT O ₂ BY VOL., DRY	2.60	2.60
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN ₂	PERCENT N ₂ BY VOL., DRY	84.00	84.00
MD	MOLECULAR WT-DRY STACK GAS	30.25	30.25

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MWS	MOLECULAR WT-STACK GAS	28.86		28.86	
PB	BAROMETRIC PRESSURE	30.11	IN-HG	764.79	MM-HG
PSI	STATIC PRES OF STACK GAS	.20	IN-H2O	5.08	MM-H2O
PS	STACK PRES, ABS.	30.12	IN-HG	765.17	MM-HG
TS	AVERAGE STACK TEMP	319.	F	159.	C
VS	AVG STACK GAS VELOCITY	55.5	FPS	16.9	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17327652.	SCFH	490667.	SCMH
QS	ACTUAL STACK FLOW RATE	28614128.	ACFH	810266.	ACMH
ISO	PERCENT ISOKINETIC	101.2		101.2	
MN	AMBIENT PARTICULATE MG. EPA 5	100.0		100.0	
CS	AMBIENT PARTICULATE	.0310 GR/DSCF*		70.868	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.7AM5HW

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PH + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 50.392 * 1.003 * (30.11 + .970 / 13.6)}{(80. + 460.)} = 49.836 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 135. = 6.35 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 6.35}{49.836 + 6.35} = 11.30 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.3}{100.} = .887$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.40 * 44 / 100) + (2.6 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.25$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.25 * (1. - (11.30 / 100)) + 18. * (11.30 / 100) = 28.86$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 205.214 / (\text{SQRT}(28.86 * 30.12) * 9. = 55.53 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.53 * 20612.3600/144 = 28614128. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RHO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28614128. * 30.12 * (1. - (11.30/100))}{(319. + 460.)} = 17327652. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (319. + 460.)) * ((0.002669 * 135.) + (50.392 * 1.003 * (30.11 + (.970/13.6)) / (80. + 460.)))}{90. * 55.53 * 30.12 * .223 * .223} = 101.20 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 100.0 * 15.43 / 49.836 = .0310 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE M5B
OPERATOR PR RA JP
AMBIENT TEMP. (DEG.F) 65.
BAR. PRESS. (IN.HG) 30.11
STATIC PRESS. (IN.H2O) .20
FILTER NUMBER(S) 35310072
STACK INSIDE DIM. (IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .015 CFM @ 8.5 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/11/83
RUN NUMBER 78M5B

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .221
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER F86
METER HEAD DIFF. 1.50

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 950.2

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL	INLET		OUTLET	
INIT	0	1330	339.104							
	10.0	1340	344.847	.670	.82	.82	315.	69.	70.	4.0
	20.0	1350	350.452	.650	.79	.79	317.	70.	70.	3.5
	30.0	1400	356.187	.670	.82	.82	318.	73.	70.	4.0
	40.0	1410	361.878	.670	.82	.82	318.	76.	70.	4.5
	50.0	1420	367.536	.640	.78	.78	318.	78.	71.	4.5
	60.0	1430	373.376	.700	.85	.85	320.	79.	71.	6.0
	70.0	1440	379.100	.670	.82	.82	320.	80.	72.	5.5
	80.0	1450	384.671	.670	.82	.82	321.	80.	73.	6.0
	90.0	1500	390.580	.670	.82	.82	321.	80.	73.	6.5
TOTALS AVERAGE	90.0		51.476		.82	.82	319.	76.	71.	4.9
										330.
										60.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 7RM5B UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TR	TIME-START	1330	1330
TF	TIME-FINISH	1500	1500
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.82 IN-H2O	20.7 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	51.476 CU-FT	1.458 CU-M
TM	AVERAGE GAS METER TEMP	73.6 F	23.1 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	49.306 SCF	1.396 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	130.7	130.7
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.152 SCF	.174 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.09	11.09
FMD	MOLE FRACTION DRY GAS	.889	.889
PCO2	PERCENT CO2 BY VOL., DRY	13.40	13.40
PO2	PERCENT O2 BY VOL., DRY	2.60	2.60
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.00	84.00
MG	MOLECULAR WT-DRY STACK GAS	30.25	30.25

MWS	MOLECULAR WT-STACK GAS	28.89		28.89	
PR	BAROMETRIC PRESSURE	30.11	IN-HG	764.79	MM-HG
PSI	STATIC PRES OF STACK GAS	.20	IN-H2O	5.08	MM-H2O
PS	STACK PRES, ABS.	30.12	IN-HG	765.17	MM-HG
TS	AVERAGE STACK TEMP	319.	F	159.	C
VS	AVG STACK GAS VELOCITY	55.5	FPS	16.9	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17360644.	SCFH	491601.	SCMH
QS	ACTUAL STACK FLOW RATE	28601504.	ACFH	809909.	ACMH
ISO	PERCENT ISOKINETIC	101.7		101.7	
MN	AMBIENT PARTICULATE MG. EPA 5	221.9		221.9	
CS	AMBIENT PARTICULATE	.0694	GR/DSCF*	158.948	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 78M5R

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 51.476 * .960 * (30.11 + .816 / 13.6)}{(74. + 460.)} = 49.306 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 131. = 6.15 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 6.15}{49.306 + 6.15} = 11.09 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.1}{100.} = .889$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.40 * 44 / 100) + (2.6 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.25$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.25 * (1. - (11.09 / 100)) + 18. * (11.09 / 100) = 28.89$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 205.214 / (\text{SQRT}(28.89 * 30.12) * 9.) = 55.50 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.50 * 20612.3600/144 = 28601504. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (RWC/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 28601504. * 30.12 * (1. - (11.09/100))}{(319. + 460.)} = 17360644. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (319. + 460.)) * ((0.002669 * 131.) + (51.476 * .960 * (30.11 + (.816/13.6)) / (74. + 460.)))}{90. * 55.50 * 30.12 * .221 * .221} = 101.75 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 221.9 * 15.43 / 49.306 = .0694 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/11/83
RUN NUMBER 7CM58W

SAMPLE TYPE M5BW
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 65.
BAR.PRESS.(IN.HG) 30.11
STATIC PRESS.(IN.H2O) .20
FILTER NUMBER(S) 3531132
STACK INSIDE DTM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .000 CFM @ 7.0 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .221
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAC
METER BOX NUMBER FMS
METER HEAD DIFF. 1.84

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1156.2

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1330	397.594									
	10.0	1340	403.390	.670	1.00	1.00	315.	75.	74.	5.0	306.	58.
	20.0	1350	408.675	.650	.97	.97	317.	76.	74.	4.5	335.	60.
	30.0	1400	414.075	.670	1.00	1.00	318.	80.	74.	5.0	318.	58.
	40.0	1410	419.444	.670	1.00	1.00	318.	84.	74.	5.5	322.	54.
	50.0	1420	424.696	.640	.95	.95	318.	88.	75.	5.5	315.	56.
	60.0	1430	430.185	.700	1.04	1.04	320.	88.	76.	6.0	314.	58.
	70.0	1440	435.555	.670	.99	.99	320.	89.	78.	6.5	318.	60.
	80.0	1450	440.981	.670	.99	.99	321.	90.	78.	7.0	317.	62.
	90.0	1500	446.378	.670	.99	.99	321.	90.	80.	7.0	317.	62.
TOTALS AVERAGE	90.0		44.784		.99	.99	319.	84.	76.	5.8	318.	59.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKF

TEST 7CM5RW

UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TB	TIME-START	1330	1330
TF	TIME-FINISH	1500	1500
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.99 IN-H2O	25.2 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	48.784 CU-FT	1.381 CU-M
TM	AVERAGE GAS METER TEMP	80.2 F	26.8 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	47.286 SCF	1.339 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	128.9	128.9
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.067 SCF	.172 SCM
BW0	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.37	11.37
FMD	MOLE FRACTION DRY GAS	.886	.886
PCO2	PERCENT CO2 BY VOL., DRY	13.40	13.40
PO2	PERCENT O2 BY VOL., DRY	2.60	2.60
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.00	84.00
MD	MOLECULAR WT-DRY STACK GAS	30.25	30.25

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MWS	MOLECULAR WT-STACK GAS	28.86		28.86	
PB	BAROMETRIC PRESSURE	30.11	IN-HG	764.79	MM-HG
PSI	STATIC PRES OF STACK GAS	.20	IN-H2O	5.08	MM-H2O
PS	STACK PRES, ABS.	30.12	IN-HG	765.17	MM-HG
TS	AVERAGE STACK TEMP	319.	F	159.	C
VS	AVG STACK GAS VELOCITY	55.5	FPS	16.9	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17316460.	SCFH	490350.	SCMH
QS	ACTUAL STACK FLOW RATE	28618416.	ACFH	810388.	ACMH
ISO	PERCENT ISOKINETIC	97.8		97.8	
MN	AMBIENT PARTICULATE MG. EPA 5	100.0		100.0	
CS	AMBIENT PARTICULATE	.0326	GR/DSCF*	74.689	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.7CM5RW

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 48.784 * .983 * (30.11 + .992 / 13.6)}{(80. + 460.)} = 47.286 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VMC = .04707 * VLC$$

$$VMC = .04707 * 129. = 6.07 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VMC) / (VMSTD + VMC)$$

$$BWD = \frac{100. * 6.07}{47.286 + 6.07} = 11.37 \text{ PERCENT}$$

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MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.4}{100.} = .886$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.40 * 44 / 100) + (2.6 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.25$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.25 * (1. - (11.37 / 100)) + 18. * (11.37 / 100) = 28.86$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 205.214 / (\text{SQRT}(28.86 * 30.12) * 9. = 55.54 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.54 * 20612.3600/144 = 28618416. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (RWO/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 28618416. * 30.12 * (1. - (11.37/100))}{(319. + 460.)} = 17316460. \text{ SCFH}$$

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PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (319. + 460.)) * ((0.002669 * 129.) + (48.784 * .983 * (30.11 + (.992/13.6)) / (80. + 460.)))}{90. * 55.54 * 30.12 * .221 * .221} = 97.83 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 100.0 * 15.43 / 47.286 = .0326 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATTON UNIT TWO EAST

DATE 02/11/83
RUN NUMBER 70MSH

SAMPLE TYPE MSH
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 65.
BAR.PRESS.(IN.HG) 30.11
STATIC PRESS.(IN.H2O) .20
FILTER NUMBER(S) 3531131
STACK INSIDE DTM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .001 CFM @ 6.0 IN.HG
METER CALIB. FACTOR 1.030
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .215
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAD
METER BOX NUMBER FR4
METER HEAD DIFF. 1.88

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1156.2

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1330	952.183									
	10.0	1340	957.870	.670	1.00	1.00	315.	72.	70.	3.0	329.	58.
	20.0	1350	962.962	.650	.97	.97	317.	72.	70.	3.5	317.	54.
	30.0	1400	968.125	.670	1.00	1.00	318.	75.	71.	3.0	322.	52.
	40.0	1410	973.353	.670	1.00	1.00	318.	78.	72.	3.0	317.	50.
	50.0	1420	978.444	.640	.95	.95	318.	80.	72.	3.5	306.	54.
	60.0	1430	983.737	.700	1.04	1.04	320.	81.	74.	4.0	324.	60.
	70.0	1440	988.898	.670	.99	.99	320.	82.	74.	4.5	337.	61.
	80.0	1450	994.170	.670	.99	.99	321.	82.	74.	5.0	329.	60.
	90.0	1500	999.409	.670	.99	.99	321.	82.	75.	5.0	322.	62.
TOTALS AVERAGE	90.0		47.226		.99	.99	319.	78.	72.	3.8	323.	57.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 7DM5B

UNIT TWO EAST

ENGLISH UNITS

METRIC UNITS

TEST DATE

02/11/83

02/11/83

TB	TIME-START	1330	1330
TF	TIME-FINISH	1500	1500
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	1.030	1.030
DN	SAMPLING NOZZLE DIAMETER	.215 IN	5.5 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.99 IN-H2O	25.2 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	47.226 CU-FT	1.337 CU-M
TM	AVERAGE GAS METER TEMP	75.3 F	24.1 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	48.398 SCF	1.370 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	128.5	128.5
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.048 SCF	.171 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.11	11.11
FMD	MOLE FRACTION DRY GAS	.889	.889
PCO2	PERCENT CO2 BY VOL., DRY	13.40	13.40
PO2	PERCENT O2 BY VOL., DRY	2.60	2.60
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.00	84.00
MD	MOLECULAR WT-DRY STACK GAS	30.25	30.25

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MWS	MOLECULAR WT-STACK GAS	28.89		28.89	
PB	BAROMETRIC PRESSURE	30.11	IN-HG	764.79	MM-HG
PSI	STATIC PRES OF STACK GAS	.20	IN-H2O	5.08	MM-H2O
PS	STACK PRES, ABS.	30.12	IN-HG	765.17	MM-HG
TS	AVERAGE STACK TEMP	319.	F	159.	C
VS	AVG STACK GAS VELOCITY	55.5	FPS	16.9	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17358136.	SCFH	491530.	SCMH
QS	ACTUAL STACK FLOW RATE	28602468.	ACFH	809936.	ACMH
ISO	PERCENT ISOKINETIC	105.5		105.5	
MN	AMBIENT PARTICULATE MG. EPA 5	215.5		215.5	
CS	AMBIENT PARTICULATE	.0687	GR/DSCF*	157.259	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 7DM5B

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 47.226 * 1.030 * (30.11 + .992 / 13.6)}{(75. + 460.)} = 48.398 \text{ USCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 129. = 6.05 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWO = (100. * VWC) / (VMSTD + VWC)$$

$$BWO = \frac{100. * 6.05}{48.398 + 6.05} = 11.11 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWO) / 100.$$

$$FMD = \frac{100. - 11.1}{100.} = .889$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.40 * 44 / 100) + (2.6 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.25$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWO / 100)) + 18. * (BWO / 100)$$

$$MWS = 30.25 * (1. - (11.11 / 100)) + 18. * (11.11 / 100) = 28.89$$

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STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 205.214 / (\text{SQRT}(28.89 * 30.12) * 9.) = 55.51 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 55.51 * 20612.3600/144 = 28602468. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RHO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28602468. * 30.12 * (1. - (11.11/100))}{(319. + 460.)} = 17358136. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TI * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (319. + 460.)) * ((0.002669 * 129.) + (47.226 * 1.030 * (30.11 + (.992/13.6)) / (75. + 460.)))}{90. * 55.51 * 30.12 * .215 * .215} = 105.54 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 215.5 * 15.43 / 48.398 = .0687 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/11/83
RUN NUMBER 8AM58

SAMPLE TYPE M5B
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 70.
BAR.PRESS.(IN.HG) 30.08
STATIC PRESS.(IN.H2O) .02
FILTER NUMBER(S)
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .000 CFM @ 17.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .305
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER FB4
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 3986.7

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1620	860.601									
	10.0	0	871.024	.650	3.33	3.33	319.	76.	75.	9.0	311.	60.
	20.0	0	880.863	.620	3.18	3.18	318.	76.	74.	8.5	313.	62.
	30.0	0	890.491	.590	3.02	3.02	320.	79.	74.	9.0	319.	56.
	30.7	1650	891.157	.740	3.79	3.35	318.	81.	73.	15.0	320.	56.
TOTALS AVERAGE	30.7		30.556		3.33	3.22	319.	78.	74.	10.4	321.	59.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 8AM5B

UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TB	TIME-START	1620	1620
TF	TIME-FINISH	1650	1650
TT	NET TIME OF TEST, MIN.	30.7	30.7
NP	NET SAMPLING POINTS	4	4
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.305 IN	7.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	3.22 IN-H2O	81.8 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	30.556 CU-FT	.865 CU-M
TM	AVERAGE GAS METER TEMP	76.0 F	24.4 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	30.591 SCF	.866 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	81.6	81.6
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	3.841 SCF	.109 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.16	11.16
FMD	MOLE FRACTION DRY GAS	.888	.888
PCO2	PERCENT CO2 BY VOL., DRY	13.30	13.30
PO2	PERCENT O2 BY VOL., DRY	2.70	2.70
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.00	84.00
MD	MOLECULAR WT-DRY STACK GAS	30.24	30.24

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MWS	MOLECULAR WT-STACK GAS	28.87		28.87	
PB	BAROMETRIC PRESSURE	30.08	IN-HG	764.03	MM-HG
PSI	STATIC PRES OF STACK GAS	.02	IN-H2O	.51	MM-H2O
PS	STACK PRES, ABS.	30.08	IN-HG	764.07	MM-HG
TS	AVERAGE STACK TEMP	319.	F	159.	C
VS	AVG STACK GAS VELOCITY	54.8	FPS	16.7	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17093528.	SCFH	484037.	SCMH
QS	ACTUAL STACK FLOW RATE	28224616.	ACFH	799237.	ACMH
ISO	PERCENT ISOKINETIC	98.7		98.7	
MN	AMBIENT PARTICULATE MG. EPA 5	156.8		156.8	
CS	AMBIENT PARTICULATE	.0791	GR/DSCF*	181.031	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

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EXAMPLE PARTICULATE CALCULATIONS TEST NO. 8AM5R

UNIT 2 FAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 30.556 * 1.003 * (30.08 + 3.220 / 13.6)}{(76. + 460.)} = 30.591 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 82. = 3.84 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 3.84}{30.591 + 3.84} = 11.16 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.2}{100.} = .888$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.30 * 44 / 100) + (2.7 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.24$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.24 * (1. - (11.16 / 100)) + 18. * (11.16 / 100) = 28.87$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 89.911 / (\text{SQRT}(28.87 * 30.08) * 4. = 54.77 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 54.77 * 20612.3600/144 = 28224616. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 28224616. * 30.08 * (1. - (11.16/100))}{(319. + 460.)} = 17093528. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (319. + 460.)) * ((0.002669 * 82.) + (30.556 * 1.003 * (30.08 + (3.220/13.6)) / (76. + 460.)))}{31. * 54.77 * 30.08 * .305 * .305} = 98.68 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 156.4 * 15.43 / 30.591 = .0791 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/11/83
RUN NUMBER 88M58P

SAMPLE TYPE M58 P400
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 20.
BAR.PRESS.(IN.HG) 30.08
STATIC PRESS.(IN.H2O) .02
FILTER NUMBER(S)
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .013 CFM @ 23.0 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .307
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER FB6
METER HEAD DIFF. 1.50
PROBE HEATER SETTING 400.
HEATER BOX SETTING 320.
K FACTOR 3568.9

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1620	390.904									
	10.0	0	401.501	.650	2.98	2.98	319.	69.	71.	12.5	322.	60.
	20.0	0	411.562	.620	2.84	2.75	318.	69.	70.	13.5	350.	60.
	30.0	1650	421.136	.590	2.75	2.50	320.	69.	69.	14.0	320.	60.
TOTALS	30.0		30.232									
AVERAGE					2.86	2.74	319.	69.	70.	13.3	331.	60.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 88M5BP UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TB	TIME-START	1620	1620
TF	TIME-FINISH	1650	1650
TT	NET TIME OF TEST, MIN.	30.0	30.0
NP	NFT SAMPLING POINTS	3	3
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.307 IN	7.8 MM
CP	PILOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	2.74 IN-H2O	69.7 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	30.232 CU-FT	.856 CU-M
TM	AVERAGE GAS METER TEMP	69.5 F	20.8 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	29.290 SCF	.829 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	79.5	79.5
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	3.742 SCF	.106 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.33	11.33
FMD	MOLE FRACTION DRY GAS	.887	.887
PCO2	PERCENT CO2 BY VOL., DRY	13.30	13.30
PO2	PERCENT O2 BY VOL., DRY	2.70	2.70
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.00	84.00
MD	MOLECULAR WT-DRY STACK GAS	30.24	30.24

2-11-83

MWS	MOLECULAR WT-STACK GAS	28.85		28.85	
PR	BAROMETRIC PRESSURE	30.08	IN-HG	764.03	MM-HG
PSI	STATIC PRES OF STACK GAS	.02	IN-H2O	.51	MM-H2O
PS	STACK PRES, ABS.	30.08	IN-HG	764.07	MM-HG
TS	AVERAGE STACK TEMP	319.	F	159.	C
VS	AVG STACK GAS VELOCITY	53.6	FPS	16.3	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	16677352.	SCFH	472253.	SCMH
QS	ACTUAL STACK FLOW RATE	27600084.	ACFH	781552.	ACMH
ISO	PERCENT ISOKINETIC	97.8		97.8	
MN	AMBIENT PARTICULATE MG. EPA 5	111.5		111.5	
CS	AMBIENT PARTICULATE	.0587	GR/DSCF*	134.445	MG/DSCM

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* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 88M5BP

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 30.232 * .960 * (30.08 + 2.743 / 13.6)}{(70. + 460.)} = 29.290 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VMC = .04707 * VLC$$

$$VMC = .04707 * 80. = 3.74 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VMC) / (VMSTD + VMC)$$

$$BWD = \frac{100. * 3.74}{29.290 + 3.74} = 11.33 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.3}{100.} = .887$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.30 * 44 / 100) + (2.7 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.24$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.24 * (1. - (11.33 / 100)) + 18. * (11.33 / 100) = 28.85$$

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STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VM * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 65.917 / (\text{SQRT}(28.85 * 30.08) * 3.) = 53.56 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 53.56 * 20612.3600/144 = 27600084. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 27600084. * 30.08 * (1. - (11.33/100))}{(319. + 460.)} = 16677352. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PR + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (319. + 460.)) * ((0.002669 * 80.) + (30.232 * .960 * (30.08 + (2.743/13.6)) / (70. + 460.)))}{30. * 53.56 * 30.08 * .307 * .307} = 97.82 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 111.5 * 15.43 / 29.290 = .0587 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/11/83
RUN NUMBER ACM58

SAMPLE TYPE M58
OPERATOR CLARKE
AMBIENT TEMP. (DEG.F) 70.
BAR. PRESS. (IN.HG) 30.08
STATIC PRESS. (IN.H2O) .02
FILTER NUMBER(S)
STACK INSIDE DIM. (IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .001 CFM @ 15.0 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .305
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAC
METER BOX NUMBER F85
METER HEAD DIFF. 1.84

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 4473.6

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1620	446.569									
	10.0	1630	457.000	.650	3.73	3.73	319.	74.	75.	8.0	340.	62.
	20.0	1640	467.350	.620	3.57	3.57	318.	76.	74.	9.0	332.	58.
	30.0	1650	477.100	.590	3.38	3.38	320.	79.	74.	10.5	305.	58.
	30.8	1651	477.329	.740	4.26	4.26	318.	81.	74.	12.5	329.	50.
TOTALS	30.8		30.760									
AVERAGE					3.74	3.74	319.	78.	74.	10.0	327.	57.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 8CM58 UNIT TWO EAST

ENGLISH UNITS

METRIC UNITS

TEST DATE

02/11/83

02/11/83

TB TIME-START

1620

1620

TF TIME-FINISH

1651

1651

TT NET TIME OF TEST, MIN.

30.8

30.8

NP NET SAMPLING POINTS

4

4

Y METER CALIBRATION FACTOR

.983

.983

DN SAMPLING NOZZLE DIAMETER

.305 IN

7.7 MM

CP PITOT TUBE COEFFICIENT

.84

.84

PM AVERAGE ORIFICE PRESSURE
DROP

3.74 IN-H2O

94.9 MM-H2O

VM VOLUME OF DRY GAS SAMPLED
AT METER CONDITIONS

30.760 CU-FT

.871 CU-M

TM AVERAGE GAS METER TEMP

75.9 F

24.4 C

VMSTD VOLUME OF DRY GAS SAMPLED
AT STANDARD CONDITIONS*

30.225 SCF

.856 SCM

VLC TOTAL H2O COLLECTED IN
IMPINGERS AND SILICA GEL, ML.

83.6

83.6

VWC VOLUME OF WATER VAPOR
AT STANDARD CONDITIONS*

3.935 SCF

.111 SCM

BWO PERCENT MOISTURE BY VOLUME
(CHECK AGAINST SATURATION
POINT HAS BEEN MADE.)

11.52

11.52

FMD MOLE FRACTION DRY GAS

.885

.885

PCO2 PERCENT CO2 BY VOL., DRY

13.30

13.30

PO2 PERCENT O2 BY VOL., DRY

2.70

2.70

PCO PERCENT CO BY VOL., DRY

.00

.00

PN2 PERCENT N2 BY VOL., DRY

84.00

84.00

MD MOLECULAR WT-DRY STACK GAS

30.24

30.24

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MWS	MOLEFCULAR WT-STACK GAS	28.83		28.83	
PB	BAROMETRIC PRESSURE	30.08	IN-HG	764.03	MM-HG
PSI	STATIC PRES OF STACK GAS	.02	IN-H2O	.51	MM-H2O
PS	STACK PRES, ABS.	30.08	IN-HG	764.07	MM-HG
TS	AVERAGE STACK TEMP	319.	F	159.	C
VS	AVG STACK GAS VELOCITY	54.8	FPS	16.7	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17036632.	SCFH	482426.	SCMH
QS	ACTUAL STACK FLOW RATE	28246420.	ACFH	799854.	ACMH
ISO	PERCENT ISOKINETIC	97.5		97.5	
MN	AMBIENT PARTICULATE MG. EPA 5	112.6		112.6	
CS	AMBIENT PARTICULATE	.0575	GR/DSCF*	131.571	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 8CM5H

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 30.760 * .983 * (30.08 + 3.735 / 13.6)}{(76. + 460.)} = 30.225 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VIC$$

$$VWC = .04707 * 84. = 3.94 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 3.94}{30.225 + 3.94} = 11.52 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.5}{100.} = .885$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.30 * 44 / 100) + (2.7 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.24$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.24 * (1. - (11.52 / 100)) + 18. * (11.52 / 100) = 28.83$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNIS)$$

$$VS = 85.49 * .84 * 89.911 / (\text{SQRT}(28.83 * 30.08) * 4. = 54.82 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 54.82 * 20612.3600/144 = 28246420. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (RWD/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 28246420. * 30.08 * (1. - (11.52/100))}{(319. + 460.)} = 17036632. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * UN)$$

$$ISO = \frac{(305.58 * (319. + 460.)) * ((0.002669 * 84.) + (30.760 * .983 * (30.08 + (3.735/13.6)) / (76. + 460.)))}{31. * 54.82 * 30.08 * .305 * .305} = 97.51 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 112.6 * 15.43 / 30.225 = .0575 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/11/83
RUN NUMBER 8DM5BP

SAMPLE TYPE MSH-P400
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 70.
BAR.PRESS.(IN.HG) 30.08
STATIC PRESS.(IN.H2O) .02
FILTER NUMBER(S)
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .016 CFM @ 18.0 IN.HG
METER CALIB. FACTOR 1.030
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .304
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER Q40
METER BOX NUMBER FR4
METER HEAD DIFF. 1.88

PROBE HEATER SETTING 400.
HEATER BOX SETTING 320.

K FACTOR 4473.6

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRFD	ACTUAL		INLET	OUTLET			
INIT	0	1620	999.812									
	10.0	1630	9.222	.650	3.73	3.73	319.	70.	70.	13.0	331.	62.
	20.0	1640	18.500	.620	3.57	3.30	318.	70.	70.	16.5	337.	64.
	30.0	1650	26.727	.590	3.38	2.70	320.	71.	69.	17.0	295.	64.
TOTALS	30.0		26.915									
AVERAGE					3.56	3.24	319.	70.	70.	15.5	321.	63.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 80M58P UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/11/83	02/11/83

TB	TIME-START	1620	1620
TF	TIME-FINISH	1650	1650
TT	NET TIME OF TEST, MIN.	30.0	30.0
NP	NET SAMPLING POINTS	3	3
Y	METER CALIBRATION FACTOR	1.030	1.030
DN	SAMPLING NOZZLE DIAMETER	.304 IN	7.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	3.24 IN-H2O	82.4 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	26.915 CU-FT	.762 CU-M
TM	AVERAGE GAS METER TEMP	70.0 F	21.1 C
VMST0	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	27.986 SCF	.792 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILTCA GEL, ML.	73.3	73.3
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	3.450 SCF	.098 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	10.98	10.98
FMD	MOLE FRACTION DRY GAS	.890	.890
PCO2	PERCENT CO2 BY VOL., DRY	13.30	13.30
PO2	PERCENT O2 BY VOL., DRY	2.70	2.70
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.00	84.00
MD	MOLECULAR WT-DRY STACK GAS	30.24	30.24

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MWS	MOLECULAR WT-STACK GAS	28.89		28.89	
PB	BAROMETRIC PRESSURE	30.08	IN-HG	764.03	MM-HG
PSI	STATIC PRES OF STACK GAS	.02	IN-H2O	.51	MM-H2O
PS	STACK PRES, ABS.	30.08	IN-HG	764.07	MM-HG
TS	AVERAGE STACK TEMP	319.	F	159.	C
VS	AVG STACK GAS VELOCITY	53.5	FPS	16.3	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	16731224.	SCFH	473778.	SCMH
QS	ACTUAL STACK FLOW RATE	27579440.	ACFH	780967.	ACMH
ISO	PERCENT ISOKINETIC	95.0		95.0	
MN	AMBIENT PARTICULATE MG. EPA 5	105.5		105.5	
CS	AMBIENT PARTICULATE	.0582	GR/DSCF*	133.141	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 80M5HP

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 26.915 * 1.030 * (30.08 + 3.243 / 13.6)}{(70. + 460.)} = 27.986 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 73. = 3.45 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 3.45}{27.986 + 3.45} = 10.98 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 10.98}{100.} = .890$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.30 * 44 / 100) + (2.7 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.24$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.24 * (1. - (10.98 / 100)) + 18. * (10.98 / 100) = 28.89$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 65.917 / (\text{SQRT}(28.89 * 30.08) * 3. = 53.52 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 53.52 * 20612.3600/144 = 27579440. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 27579440. * 30.08 * (1. - (10.98/100))}{(319. + 460.)} = 16731224. \text{ SCFH}$$

A-161 PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (319. + 460.)) * ((0.002669 * 73.) + (26.915 * 1.030 * (30.08 + (3.243/13.6)) / (70. + 460.)))}{30. * 53.52 * 30.08 * .304 * .304} = 95.01 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 105.5 * 15.43 / 27.986 = .0582 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

SAMPLE TYPE MSB
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.27
STATIC PRESS.(IN.H2O) -.40
FILTER NUMBER(S) 3531106
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .002 CFM @ 9.0 IN.HG
METER CALIB. FACTOR 1.003
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/12/83
RUN NUMBER 9AM58

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .223
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER FR4
METER HEAD DIFF. 1.72

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1126.6

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	830	891.537									
	10.0	840	897.300	.720	1.05	1.05	313.	63.	62.	4.0	320.	49.
	20.0	850	902.930	.690	1.00	1.00	319.	64.	62.	4.0	334.	49.
	30.0	900	908.540	.690	1.00	1.00	321.	67.	62.	4.5	338.	49.
	40.0	910	914.173	.690	1.00	1.00	321.	70.	63.	5.0	334.	50.
	50.0	920	919.851	.690	1.00	1.00	322.	72.	63.	5.5	315.	50.
	60.0	930	925.513	.700	1.01	1.01	323.	74.	64.	6.0	314.	51.
	70.0	940	931.174	.700	1.01	1.01	324.	76.	65.	7.0	307.	53.
	80.0	950	936.885	.710	1.02	1.02	324.	76.	66.	7.5	305.	55.
	90.0	1000	942.595	.710	1.02	1.02	324.	77.	66.	8.0	295.	55.
TOTALS AVERAGE	90.0		51.058		1.01	1.01	321.	71.	64.	5.7	318.	51.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 9AM5B UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/12/83	02/12/83

TB	TIME-START	830	830
TF	TIME-FINISH	1000	1000
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.223 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.01 IN-H2O	25.7 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	51.058 CU-FT	1.446 CU-M
TM	AVERAGE GAS METER TEMP	67.3 F	19.6 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	52.003 SCF	1.473 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	139.7	139.7
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.576 SCF	.186 SCM
BW0	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.23	11.23
FMD	MOLE FRACTION DRY GAS	.888	.888
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.50	2.50
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.90	83.90
MD	MOLECULAR WT-DRY STACK GAS	30.28	30.28

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MWS	MOLECULAR WT-STACK GAS	28.90		28.90	
PB	BAROMETRIC PRESSURE	30.27	IN-HG	768.86	MM-HG
PSI	STATIC PRFS OF STACK GAS	-.40	IN-H2O	-10.16	MM-H2O
PS	STACK PRES, ABS.	30.24	IN-HG	768.11	MM-HG
TS	AVERAGE STACK TFMP	321.	F	161.	C
VS	AVG STACK GAS VELOCITY	56.8	FPS	17.3	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17750968.	SCFH	502654.	SCMH
QS	ACTUAL STACK FLOW RATE	29271616.	ACFH	828884.	ACMH
ISO	PERCENT ISOKINETIC	103.1		103.1	
MN	AMBIENT PARTICULATE MG. EPA 5	252.9		252.9	
CS	AMBIENT PARTICULATE	.0750 GR/DSCF*		171.757	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 9AMSR

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 51.058 * 1.003 * (30.27 + 1.012 / 13.6)}{(67. + 460.)} = 52.003 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 140. = 6.58 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 6.58}{52.003 + 6.58} = 11.23 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.2}{100.} = .888$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCU) * .28$$

$$MD = (13.60 * 44/100) + (2.5 * 32/100) + ((83.9 + .0) * 28/100) = 30.28$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD/100)) + 18. * (BWD/100)$$

$$MWS = 30.28 * (1. - (11.23/100)) + 18. * (11.23/100) = 28.90$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 210.457 / (\text{SQRT}(28.90 * 30.24) * 9. = 56.81 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 56.81 * 20612. 3600/144 = 29271616. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 29271616. * 30.24 * (1. - (11.23/100))}{(321. + 460.)} = 17750968. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.5 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (IT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (321. + 460.)) * ((0.002669 * 140.) + (51.058 * 1.003 * (30.27 + (1.012/13.6)) / (67. + 460.)))}{90. * 56.81 * 30.24 * .223 * .223} = 103.08 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 252.9 * 15.43 / 52.003 = .0750 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/12/83
RUN NUMBER 98MSB

SAMPLE TYPE MSB
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.27
STATIC PRESS.(IN.H2O) -.40
FILTER NUMBER(S) 3531105
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .012 CFM @ 8.5 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .221
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER FB6
METER HEAD DIFF. 1.50

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 947.8

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	830	421.579									
	10.0	840	427.397	.720	.88	.88	313.	57.	59.	4.0	322.	48.
	20.0	850	433.125	.690	.84	.84	319.	59.	59.	4.0	330.	48.
	30.0	900	438.857	.690	.84	.84	321.	62.	59.	4.5	327.	49.
	40.0	910	444.600	.690	.84	.84	321.	66.	60.	4.5	328.	50.
	50.0	920	450.337	.690	.84	.84	322.	68.	60.	5.0	334.	50.
	60.0	930	456.100	.700	.85	.85	323.	70.	61.	6.0	334.	50.
	70.0	940	461.983	.700	.85	.85	323.	70.	62.	6.5	336.	51.
	80.0	950	467.683	.710	.86	.86	324.	71.	62.	7.5	338.	52.
	90.0	1000	473.504	.710	.86	.86	324.	71.	64.	7.5	332.	52.
TOTALS AVERAGE	90.0		51.925		.85	.85	321.	66.	61.	5.5	331.	50.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 9RM5H UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/12/83	02/12/83

TS	TIME-START	830	830
TF	TIME-FINISH	1000	1000
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.960	.960
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PILOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.85 IN-H2O	21.6 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	51.925 CU-FT	1.470 CU-M
TM	AVERAGE GAS METER TEMP	63.3 F	17.4 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	50.986 SCF	1.444 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	135.4	135.4
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.373 SCF	.180 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.11	11.11
FMD	MOLE FRACTION DRY GAS	.889	.889
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.50	2.50
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.90	83.90
MD	MOLECULAR WT-DRY STACK GAS	30.28	30.28

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MWS	MOLECULAR WT-STACK GAS	28.91		28.91	
PR	BAROMETRIC PRESSURE	30.27	IN-HG	768.86	MM-HG
PSI	STATIC PRES OF STACK GAS	- .40	IN-H2O	-10.16	MM-H2O
PS	STACK PRES, ABS.	30.24	IN-HG	768.11	MM-HG
TS	AVERAGE STACK TEMP	321.	F	161.	C
VS	AVG STACK GAS VELOCITY	56.8	FPS	17.3	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17770760.	SCFH	503215.	SCMH
QS	ACTUAL STACK FLOW RATE	29262440.	ACFH	828625.	ACMH
ISO	PERCENT ISOKINETIC	102.8		102.8	
MN	AMBIENT PARTICULATE MG. EPA 5	261.2		261.2	
CS	AMBIENT PARTICULATE	.0790 GR/DSCF*		180.933	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 98MSR

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 51.925 * .960 * (30.27 + .851 / 13.6)}{(63. + 460.)} = 50.986 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VMC = .04707 * VLC$$

$$VMC = .04707 * 135. = 6.37 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$RWO = (100. * VMC) / (VMSTD + VMC)$$

$$RWO = \frac{100. * 6.37}{50.986 + 6.37} = 11.11 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - RWO) / 100.$$

$$FMD = \frac{100. - 11.1}{100.} = .889$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.5 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.28$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (RWO / 100)) + 18. * (RWO / 100)$$

$$MWS = 30.28 * (1. - (11.11 / 100)) + 18. * (11.11 / 100) = 28.91$$

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STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 210.402 / (\text{SQRT}(28.91 * 30.24) * 9. = 56.79 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 56.79 * 20612.3600/144 = 29262440. \text{ ACFM}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWD/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 29262440. * 30.24 * (1. - (11.11/100))}{(321. + 460.)} = 17770760. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (321. + 460.)) * ((0.002669 * 135.) + (51.925 * .960 * (30.27 + (.851/13.6)) / (63. + 460.)))}{90. * 56.79 * 30.24 * .221 * .221} = 102.79 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 261.2 * 15.43 / 50.986 = .0790 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/12/83
RUN NUMBER 9CM5R

SAMPLE TYPE MSH
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.27
STATIC PRESS.(IN.H2O) -.40
FILTER NUMBER(S) 3531104
STACK INSIDE DTM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .000 CFM @ 8.0 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .221
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAC
METER BOX NUMBER F85
METER HEAD DIFF. 1.84

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1134.0

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	830	477.734									
	10.0	840	482.700	.720	1.06	1.06	313.	65.	64.	4.5	328.	53.
	20.0	850	488.160	.690	1.00	1.00	319.	66.	64.	5.5	317.	54.
	30.0	900	493.440	.690	1.00	1.00	321.	70.	60.	5.5	317.	53.
	40.0	910	498.775	.690	1.00	1.00	321.	76.	66.	6.0	321.	50.
	50.0	920	504.110	.690	1.00	1.00	322.	78.	66.	6.5	322.	50.
	60.0	930	509.666	.700	1.01	1.01	323.	81.	69.	7.0	317.	52.
	70.0	940	515.015	.700	1.01	1.01	324.	82.	70.	7.5	322.	54.
	80.0	950	520.480	.710	1.03	1.03	324.	84.	71.	8.0	320.	54.
	90.0	1000	525.793	.710	1.03	1.03	324.	85.	72.	8.0	317.	54.
TOTALS AVERAGE	90.0		48.059		1.02	1.02	321.	76.	67.	6.5	320.	53.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 9CM5B UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/12/83	02/12/83

TB	TIME-START	830	830
TF	TIME-FINISH	1000	1000
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.221 IN	5.6 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.02 IN-H2O	25.4 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	48.059 CU-FT	1.361 CU-M
TM	AVERAGE GAS METER TEMP	71.6 F	22.0 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	47.587 SCF	1.348 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	133.1	133.1
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.265 SCF	.177 SCM
BWO	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.63	11.63
FMD	MOLE FRACTION DRY GAS	.884	.884
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.50	2.50
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.90	83.90
MD	MOLECULAR WT-DRY STACK GAS	30.28	30.28

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MWS	MOLECULAR WT-STACK GAS	28.85		28.85	
PB	BAROMETRIC PRESSURE	30.27	IN-HG	768.86	MM-HG
PSI	STATIC PRES OF STACK GAS	-0.40	IN-H2O	-10.16	MM-H2O
PS	STACK PRES, ABS.	30.24	IN-HG	768.11	MM-HG
TS	AVERAGE STACK TEMP	321.	F	161.	C
VS	AVG STACK GAS VELOCITY	56.9	FPS	17.3	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	17684652.	SCFH	500776.	SCMH
QS	ACTUAL STACK FLOW RATE	29297040.	ACFH	829604.	ACMH
ISO	PERCENT ISOKINETIC	96.4		96.4	
MN	AMBIENT PARTICULATE MG. EPA 5	204.7		204.7	
CS	AMBIENT PARTICULATE	.0664	GR/DSCF*	151.924	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 9C5R

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 48.059 * .983 * (30.27 + 1.016 / 13.6)}{(72. + 460.)} = 47.587 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 133. = 6.27 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 6.27}{47.587 + 6.27} = 11.63 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.6}{100.} = .884$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.60 * 44 / 100) + (2.5 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.28$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.28 * (1. - (11.63 / 100)) + 18. * (11.63 / 100) = 28.85$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VM * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 210.457 / (\text{SQRT}(28.85 * 30.24) * 9.) = 56.85 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 56.85 * 20612.3600/144 = 29297040. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 29297040. * 30.24 * (1. - (11.63/100))}{(321. + 460.)} = 17684652. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (IT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (321. + 460.)) * ((0.002669 * 133.) + (48.059 * .983 * (30.27 + (1.016/13.6)) / (72. + 460.)))}{90. * 56.85 * 30.24 * .221 * .221} = 96.40 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 204.7 * 15.43 / 47.587 = .0664 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/12/83
RUN NUMBER 90M58

SAMPLE TYPE MSH
OPERATOR CLARKE
AMBIENT TEMP. (DEG.F) 60.
BAR. PRESS. (IN.HG) 30.27
STATIC PRESS. (IN.H2O) -.40
FILTER NUMBER(S) 3531103
STACK INSIDE DIM. (IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 206
LEAKAGE .000 CFM @ 5.0 IN.HG
METER CALIB. FACTOR 1.030
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .215
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAD
METER BOX NUMBER FR4
METER HEAD DIFF. 1.88

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.

K FACTOR 1134.0

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)	STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)	PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL	INLET	OUTLET		
INIT	0	830	27.215							
	10.0	840	31.819	.720	1.06	1.06	313.	59.	59.	3.0 320. 54.
	20.0	850	37.300	.690	1.00	1.00	319.	60.	60.	3.0 331. 53.
	30.0	900	42.380	.690	1.00	1.00	321.	64.	60.	3.0 325. 52.
	40.0	910	47.620	.690	1.00	1.00	321.	68.	60.	3.5 327. 50.
	50.0	920	52.815	.690	1.00	1.00	322.	70.	62.	4.0 321. 50.
	60.0	930	58.138	.700	1.01	1.01	323.	73.	63.	4.5 318. 48.
	70.0	940	63.425	.700	1.01	1.01	324.	74.	64.	4.5 322. 48.
	80.0	950	68.560	.710	1.03	1.03	324.	74.	65.	5.0 330. 52.
	90.0	1000	73.756	.710	1.03	1.03	324.	75.	66.	5.0 336. 56.
TOTALS AVERAGE	90.0		46.541		1.02	1.02	321.	69.	62.	3.9 326. 51.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 9DM58 UNIT TWO EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/12/83	02/12/83

TB	TIME-START	830	830
TF	TIME-FINISH	1000	1000
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	1.030	1.030
DN	SAMPLING NOZZLE DIAMETER	.215 IN	5.5 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.02 IN-H2O	25.8 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	46.541 CU-FT	1.318 CU-M
TM	AVERAGE GAS METER TEMP	65.3 F	18.5 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	48.864 SCF	1.384 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	133.5	133.5
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.284 SCF	.178 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.39	11.39
FMD	MOLE FRACTION DRY GAS	.886	.886
PCO2	PERCENT CO2 BY VOL., DRY	13.60	13.60
PO2	PERCENT O2 BY VOL., DRY	2.50	2.50
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	83.90	83.90
MD	MOLECULAR WT-DRY STACK GAS	30.28	30.28

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MWS	MOLECULAR WT-STACK GAS	28.88		28.88	
PB	BAROMETRIC PRESSURE	30.27	IN-HG	768.86	MM-HG
PSI	STATIC PRES OF STACK GAS	-1.40	IN-H2O	-10.16	MM-H2O
PS	STACK PRES, ABS.	30.24	IN-HG	768.11	MM-HG
TS	AVERAGE STACK TEMP	321.	F	161.	C
VS	AVG STACK GAS VELOCITY	56.8	FPS	17.3	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	17723520.	SCFH	501877.	SCMH
QS	ACTUAL STACK FLOW RATE	29282136.	ACFH	829182.	ACMH
ISO	PERCENT ISOKINETIC	104.4		104.4	
MN	AMBIENT PARTICULATE MG. EPA 5	224.6		224.6	
CS	AMBIENT PARTICULATE	.0709	GR/DSCF*	162.335	MG/DSCM

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* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO. 9DMSH

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PH + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 46.541 * 1.030 * (30.27 + 1.016 / 13.6)}{(65. + 460.)} = 48.864 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 134. = 6.28 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 6.28}{48.864 + 6.28} = 11.39 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.4}{100.} = .886$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCU) * .28$$

$$MD = (13.60 * 44 / 100) + (2.5 * 32 / 100) + ((83.9 + .0) * 28 / 100) = 30.28$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.28 * (1. - (11.39 / 100)) + 18. * (11.39 / 100) = 28.88$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$\Delta ELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * \Delta ELP / (\text{SQRT}(MWS * PS) * PNIS)$$

$$VS = 85.49 * .84 * 210.457 / (\text{SQRT}(28.88 * 30.24) * 9.) = 56.83 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 56.83 * 20612.3600/144 = 29282136. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 29282136. * 30.24 * (1. - (11.39/100))}{(321. + 460.)} = 17723520. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PH + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (321. + 460.)) * ((0.002669 * 134.) + (46.541 * 1.030 * (30.27 + (1.016/13.6)) / (65. + 460.)))}{90. * 56.83 * 30.24 * .215 * .215} = 104.36 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 224.6 * 15.43 / 48.864 = .0709 \text{ GR/DSCF}$$

FIELD DATA

PLANT	SAMPLING LOCATION	UNIT 2 EAST
1	2	3
4	5	6
7	8	9
10	11	12
13	14	15
16	17	18
19	20	21
22	23	24
25	26	27
28	29	30
31	32	33
34	35	36
37	38	39
40	41	42
43	44	45
46	47	48
49	50	51
52	53	54
55	56	57
58	59	60
61	62	63
64	65	66
67	68	69
70	71	72
73	74	75
76	77	78
79	80	81
82	83	84
85	86	87
88	89	90
91	92	93
94	95	96
97	98	99
100	101	102
103	104	105
106	107	108
109	110	111
112	113	114
115	116	117
118	119	120
121	122	123
124	125	126
127	128	129
130	131	132
133	134	135
136	137	138
139	140	141
142	143	144
145	146	147
148	149	150
151	152	153
154	155	156
157	158	159
160	161	162
163	164	165
166	167	168
169	170	171
172	173	174
175	176	177
178	179	180
181	182	183
184	185	186
187	188	189
190	191	192
193	194	195
196	197	198
199	200	201
202	203	204
205	206	207
208	209	210
211	212	213
214	215	216
217	218	219
220	221	222
223	224	225
226	227	228
229	230	231
232	233	234
235	236	237
238	239	240
241	242	243
244	245	246
247	248	249
250	251	252
253	254	255
256	257	258
259	260	261
262	263	264
265	266	267
268	269	270
271	272	273
274	275	276
277	278	279
280	281	282
283	284	285
286	287	288
289	290	291
292	293	294
295	296	297
298	299	300
301	302	303
304	305	306
307	308	309
310	311	312
313	314	315
316	317	318
319	320	321
322	323	324
325	326	327
328	329	330
331	332	333
334	335	336
337	338	339
340	341	342
343	344	345
346	347	348
349	350	351
352	353	354
355	356	357
358	359	360
361	362	363
364	365	366
3		

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SAMPLE TYPE          M5B
OPERATOR            PR RA JP
AMBIFNT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG)    30.27
STATIC PRESS.(IN.H2O) -.40
FILTER NUMBER(S)      3531028
STACK INSIDE DIM.(IN) 162.00      .00
PITOT TUBE COEFF.     .84
THERM. NO.           178
LEAKAGE              .000 CFM @ 8.5 IN.HG
METER CALIB. FACTOR  1.003
READ & RECORD DATA EVERY 10.0 MINUTES

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DATE	02/12/83
RUN NUMBER	10AM58
PROBE LENGTH & TYPE	5 FT GLASS
NOZZLE : I.D.	.224
ASSUMED MOISTURE	11.0
SAMPLE BOX NUMBER	
METER BOX NUMBER	FB4
METER HEAD DIFF.	1.72
PROBE HEATER SETTING	320.
HEATER BOX SETTING	320.
K FACTOR	1141.5

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H ₂ O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H ₂ O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1200	942.801									
	10.0	1210	949.150	.850	1.24	1.24	325.	67.	65.	5.0	342.	50.
	20.0	1220	955.100	.770	1.12	1.12	326.	69.	65.	5.0	327.	50.
	30.0	1230	961.038	.770	1.12	1.12	326.	72.	65.	5.5	340.	50.
	40.0	1240	966.760	.750	1.09	1.09	326.	77.	66.	6.0	331.	51.
	50.0	1250	972.650	.750	1.09	1.09	325.	81.	67.	6.0	336.	51.
	60.0	1300	978.444	.730	1.06	1.06	326.	81.	69.	7.0	337.	53.
	70.0	1310	984.250	.730	1.06	1.06	327.	81.	69.	7.5	326.	53.
	80.0	1320	990.061	.730	1.06	1.06	327.	81.	70.	8.0	337.	54.
	90.0	1330	995.879	.730	1.06	1.06	328.	82.	71.	8.5	327.	54.
TOTALS AVERAGE	90.0		53.078		1.10	1.10	326.	77.	67.	6.5	334.	52.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 10AM58

UNIT 2 EAST

		ENGLISH UNITS	METRIC UNITS
TEST DATE		02/12/83	02/12/83

TB	TIME-START	1200	1200
TF	TIME-FINISH	1330	1330
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	1.003	1.003
DN	SAMPLING NOZZLE DIAMETER	.224 IN	5.7 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	1.10 IN-H2O	27.9 MM-H2O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	53.078 CU-FT	1.503 CU-M
TM	AVERAGE GAS METER TEMP	72.1 F	22.3 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	53.587 SCF	1.517 SCM
VLC	TOTAL H2O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	154.9	154.9
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	7.291 SCF	.206 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	11.98	11.98
FMD	MOLE FRACTION DRY GAS	.880	.880
PCO2	PERCENT CO2 BY VOL., DRY	13.00	13.00
PO2	PERCENT O2 BY VOL., DRY	3.00	3.00
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN2	PERCENT N2 BY VOL., DRY	84.00	84.00
MD	MOLECULAR WT-DRY STACK GAS	30.20	30.20

MWS	MOLFCULAR WT-STACK GAS	28.74		28.74	
PB	BAROMETRIC PRESSURE	30.27	IN-HG	768.86	MM-HG
PSI	STATIC PRES OF STACK GAS	-.40	IN-H2O	-10.16	MM-H2O
PS	STACK PRES, ABS.	30.24	IN-HG	768.11	MM-HG
TS	AVERAGE STACK TEMP	326.	F	163.	C
VS	AVG STACK GAS VFLCITY	59.4	FPS	18.1	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	18286776.	SCFH	517827.	SCMH
QS	ACTUAL STACK FLOW RATE	30607220.	ACFH	866705.	ACMH
ISO	PERCENT ISOKINETIC	102.2		102.2	
MN	AMBIENT PARTICULATE MG. EPA 5	260.6		260.6	
CS	AMBIENT PARTICULATE	.0750	GR/DSCF*	171.757	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.10AM5R

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 53.078 * 1.003 * (30.27 + 1.100 / 13.6)}{(72. + 460.)} = 53.587 \text{ NSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VMC = .04707 * VLC$$

$$VMC = .04707 * 155. = 7.29 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VMC) / (VMSTD + VMC)$$

$$BWD = \frac{100. * 7.29}{53.587 + 7.29} = 11.98 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.98}{100.} = .880$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.00 * 44 / 100) + (3.0 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.20$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.20 * (1. - (11.98 / 100)) + 18. * (11.98 / 100) = 28.74$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 219.453 / (\text{SQRT}(28.74 * 30.24) * 9.) = 59.40 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 59.40 * 20612.3600/144 = 30607220. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSD = \frac{17.647 * 30607220. * 30.24 * (1. - (11.98/100))}{(326. + 460.)} = 18286776. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (326. + 460.)) * ((0.002669 * 155.) + (53.078 * 1.003 * (30.27 + (1.100/13.6)) / (72. + 460.)))}{90. * 59.40 * 30.24 * .224 * .224} = 102.19 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 260.6 * 15.43 / 53.587 = .0750 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT 2 EAST

DATE 02/12/83
RIIN NUMBR 10BM5P

SAMPLE TYPE M58 P400
OPERATOR PR RA JP
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.27
STATIC PRESS.(IN.H2O) -.40
FILTER NUMBER(S) 3531027
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .055 CFM @ 12.0 IN.HG
METER CALIB. FACTOR .960
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .227
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER
METER BOX NUMBER FB6
METER HEAD DIFF. 1.50

PROBE HEATER SETTING 400.
HEATER BOX SETTING 320.

K FACTOR 948.6

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TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRFD	ACTUAL		INLFT	OUTLFT			
INIT	0	1200	473.751									
	10.0	1210	480.096	.850	1.03	1.03	325.	61.	62.	4.0	331.	50.
	20.0	1220	486.187	.770	.93	.93	326.	62.	63.	4.0	345.	50.
	30.0	1230	492.168	.770	.93	.93	326.	66.	63.	4.0	342.	52.
	40.0	1240	498.125	.750	.90	.90	326.	70.	63.	4.0	334.	52.
	50.0	1250	504.061	.750	.90	.90	325.	73.	64.	4.5	335.	53.
	60.0	1300	509.993	.730	.88	.88	326.	74.	65.	4.5	334.	53.
	70.0	1310	515.870	.730	.88	.88	327.	74.	65.	4.5	338.	54.
	80.0	1320	521.792	.730	.88	.88	327.	74.	66.	4.5	339.	55.
	90.0	1330	527.726	.730	.88	.88	328.	74.	66.	6.5	339.	57.
TOTALS	90.0		53.975									
AVERAGE					.91	.91	326.	70.	64.	4.5	337.	53.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

PR RA JP

TEST 10BM5P

UNIT 2 EAST

ENGLISH UNITS

METRIC UNITS

TEST DATE

02/12/83

02/12/83

TS TIME-START
TF TIME-FINISH

1200
1330

1200
1330

TT NET TIME OF TEST, MIN.

90.0

90.0

NP NET SAMPLING POINTS

9

9

Y METER CALIBRATION FACTOR

.960

.960

DN SAMPLING NOZZLE DIAMETER

.227 IN

5.8 MM

CP PITOT TUBE COEFFICIENT

.84

.84

PM AVERAGE ORIFICE PRESSURE
DROP

.91 IN-H2O

23.2 MM-H2O

VM VOLUME OF DRY GAS SAMPLED
AT METER CONDITIONS

53.975 CU-FT

1.528 CU-M

TM AVERAGE GAS METER TEMP

66.9 F

19.4 C

VMSTD VOLUME OF DRY GAS SAMPLED
AT STANDARD CONDITIONS*

52.643 SCF

1.491 SCM

VLC TOTAL H2O COLLECTED IN
IMPINGERS AND SILICA GEL, ML.

145.6

145.6

VWC VOLUME OF WATER VAPOR
AT STANDARD CONDITIONS*

6.853 SCF

.194 SCM

BWD PERCENT MOISTURE BY VOLUME
(CHECK AGAINST SATURATION
POINT HAS BEEN MADE.)

11.52

11.52

FMD MOLE FRACTION DRY GAS

.885

.885

PCO2 PERCENT CO2 BY VOL., DRY

13.00

13.00

PO2 PERCENT O2 BY VOL., DRY

3.00

3.00

PCO PERCENT CO BY VOL., DRY

.00

.00

PN2 PERCENT N2 BY VOL., DRY

84.00

84.00

MD MOLECULAR WT-DRY STACK GAS

30.20

30.20

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MWS	MOLECULAR WT-STACK GAS	28.79		28.79	
PR	BAROMETRIC PRESSURE	30.27	IN-HG	768.86	MM-HG
PSI	STATIC PRES OF STACK GAS	-1.40	IN-H2O	-10.16	MM-H2O
PS	STACK PRES, ABS.	30.24	IN-HG	768.11	MM-HG
TS	AVERAGE STACK TFMP	326.	F	163.	C
VS	AVG STACK GAS VFLOCITY	59.3	FPS	18.1	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSSTD	STACK FLOW RATE, DRY*	18364048.	SCFH	520015.	SCMH
QS	ACTUAL STACK FLOW RATE	30577524.	ACFH	865864.	ACMH
ISO	PERCENT ISOKINETIC	97.3		97.3	
MN	AMBIENT PARTICULATE MG. EPA 5	226.1		226.1	
CS	AMBIENT PARTICULATE	.0663	GR/DSCF*	151.688	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.10RM5P

UNIT 2 EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 53.975 * .960 * (30.27 + .912 / 13.6)}{(67. + 460.)} = 52.643 \text{ NSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 146. = 6.85 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 6.85}{52.643 + 6.85} = 11.52 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 11.5}{100.} = .885$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.00 * 44 / 100) + (3.0 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.20$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.20 * (1. - (11.52 / 100)) + 18. * (11.52 / 100) = 28.79$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM. OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 219.453 / (\text{SQRT}(28.79 * 30.24) * 9. = 59.34 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 59.34 * 20612. * 3600/144 = 30577524. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (RWO/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 30577524. * 30.24 * (1. - (11.52/100))}{(326. + 460.)} = 18364048. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PR + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (326. + 460.)) * ((0.002669 * 146.) + (53.975 * .960 * (30.27 + (.912/13.6)) / (67. + 460.)))}{90. * 59.34 * 30.24 * .227 * .227} = 97.34 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 226.1 * 15.43 / 52.643 = .0663 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

SAMPLE TYPE MSB
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.27
STATIC PRESS.(IN.H2O) -.40
FILTER NUMBER(S) 3531089
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .000 CFM @ 6.0 IN.HG
METER CALIB. FACTOR .983
READ & RECORD DATA EVERY 10.0 MINUTES

DATE 02/12/83
RUN NUMBER 10CM5B

PROBE LENGTH & TYPE 6 FT GLASS
NOZZLE : I.D. .211
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAC
METER BOX NUMBER FB5
METER HEAD DIFF. 1.84

PROBE HEATER SETTING 320.
HEATER BOX SETTING 320.
K FACTOR 994.9

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1200	526.000									
	10.0	1210	531.595	.850	1.08	1.08	325.	60.	68.	4.0	317.	50.
	20.0	1220	536.820	.770	.98	.98	326.	68.	68.	4.0	337.	48.
	30.0	1230	542.160	.770	.98	.98	326.	72.	68.	4.5	314.	48.
	40.0	1240	547.370	.750	.95	.95	328.	78.	68.	4.5	317.	50.
	50.0	1250	552.600	.750	.95	.95	325.	82.	70.	5.0	319.	54.
	60.0	1300	557.810	.730	.92	.92	326.	84.	71.	5.0	319.	52.
	70.0	1310	562.989	.730	.92	.92	327.	85.	72.	5.5	321.	56.
	80.0	1320	567.925	.730	.92	.92	327.	86.	72.	6.0	322.	58.
	90.0	1330	573.155	.730	.92	.92	328.	86.	73.	6.0	323.	60.
TOTALS AVERAGE	90.0		47.155		.96	.96	326.	78.	70.	4.9	321.	53.

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PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 10CM5B

UNIT TWO EAST

ENGLISH UNITS

METRIC UNITS

TEST DATE

02/12/83

02/12/83

TB	TIME-START	1200	1200
TF	TIME-FINISH	1330	1330
TT	NET TIME OF TEST, MIN.	90.0	90.0
NP	NET SAMPLING POINTS	9	9
Y	METER CALIBRATION FACTOR	.983	.983
DN	SAMPLING NOZZLE DIAMETER	.211 IN	5.4 MM
CP	PITOT TUBE COEFFICIENT	.84	.84
PM	AVERAGE ORIFICE PRESSURE DROP	.96 IN-H ₂ O	24.3 MM-H ₂ O
VM	VOLUME OF DRY GAS SAMPLED AT METER CONDITIONS	47.155 CU-FT	1.335 CU-M
TM	AVERAGE GAS METER TEMP	73.9 F	23.3 C
VMSTD	VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS*	46.481 SCF	1.316 SCM
VLC	TOTAL H ₂ O COLLECTED IN IMPINGERS AND SILICA GEL, ML.	137.4	137.4
VWC	VOLUME OF WATER VAPOR AT STANDARD CONDITIONS*	6.467 SCF	.183 SCM
BWD	PERCENT MOISTURE BY VOLUME (CHECK AGAINST SATURATION POINT HAS BEEN MADE.)	12.21	12.21
FMD	MOLE FRACTION DRY GAS	.878	.878
PCO ₂	PERCENT CO ₂ BY VOL., DRY	13.00	13.00
PO ₂	PERCENT O ₂ BY VOL., DRY	3.00	3.00
PCO	PERCENT CO BY VOL., DRY	.00	.00
PN ₂	PERCENT N ₂ BY VOL., DRY	84.00	84.00
MD	MOLECULAR WT-DRY STACK GAS	30.20	30.20

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MWS	MOLECULAR WT-STACK GAS	28.71		28.71	
PB	BAROMETRIC PRESSURE	30.27	IN-HG	768.86	MM-HG
PSI	STATIC PRES OF STACK GAS	-.40	IN-H2O	-10.16	MM-H2O
PS	STACK PRES, ABS.	30.24	IN-HG	768.11	MM-HG
TS	AVERAGE STACK TEMP	326.	F	164.	C
VS	AVG STACK GAS VELOCITY	59.4	FPS	18.1	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	18244000.	SCFH	516615.	SCMH
QS	ACTUAL STACK FLOW RATE	30626964.	ACFH	867264.	ACMH
ISO	PERCENT ISOKINETIC	100.1		100.1	
MN	AMBIENT PARTICULATE MG, EPA 5	210.0		210.0	
CS	AMBIENT PARTICULATE	.0697	GR/DSCF*	159.564	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.10C5H

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PR + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 47.155 * .983 * (30.27 + .95H / 13.6)}{(74. + 460.)} = 46.481 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VWC = .04707 * VLC$$

$$VWC = .04707 * 137. = 6.47 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VWC) / (VMSTD + VWC)$$

$$BWD = \frac{100. * 6.47}{46.481 + 6.47} = 12.21 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 12.2}{100.} = .878$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.00*44/100) + (3.0*32/100) + ((84.0+ .0) * 28/100) = 30.20$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD/100)) + 18. * (BWD/100)$$

$$MWS = 30.20 * (1. - (12.21/100)) + 18. * (12.21/100) = 28.71$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DELP = \text{SUM. OF THE SQRT}(VM * (TS + 460.))$$

$$VS = 85.49 * CP * DELP / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 219.484 / (\text{SQRT}(28.71 * 30.24) * 9.) = 59.44 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 59.44 * 20612.3600/144 = 30626984. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 30626984. * 30.24 * (1. - (12.21/100))}{(326. + 460.)} = 18244000. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PB + (PM/13.6)) / (TM + 460.))) / (TT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (326. + 460.)) * ((0.002669 * 137.) + (47.155 * .983 * (30.27 + (.958/13.6)) / (74. + 460.)))}{90. * 59.44 * 30.24 * .211 * .211} = 100.13 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 210.0 * 15.43 / 46.481 = .0697 \text{ GR/DSCF}$$

FIELD DATA

PLANT
SAMPLING LOCATION UNIT TWO EAST

DATE 02/12/83
RUN NUMBER 10DM5P

SAMPLE TYPE M5H P400
OPERATOR CLARKE
AMBIENT TEMP.(DEG.F) 60.
BAR.PRESS.(IN.HG) 30.27
STATIC PRESS.(IN.H2O) -.40
FILTER NUMBER(S) 3531088
STACK INSIDE DIM.(IN) 162.00 .00
PITOT TUBE COEFF. .84
THERM. NO. 178
LEAKAGE .010 CFM @ 9.0 IN.HG
METER CALIB. FACTOR 1.030
READ & RECORD DATA EVERY 10.0 MINUTES

PROBE LENGTH & TYPE 5 FT GLASS
NOZZLE : I.D. .210
ASSUMED MOISTURE 11.0
SAMPLE BOX NUMBER QAD
METER BOX NUMBER FR4
METER HEAD DIFF. 1.88

PROBE HEATER SETTING 400.
HEATER BOX SETTING 320.

K FACTOR 994.9

TRAVERSE POINT NO.	SAMPLE TIME (MIN.)	CLOCK TIME (24-HR CLOCK)	GAS METER READING (CU.FT.)	VELOCITY HEAD (IN.H2O)	ORIFICE PRESSURE DIFFERENTIAL (IN.H2O)		STACK TEMP (DEG.F)	DRY GAS METER TEMP (DEG.F)		PUMP VACUUM (IN.HG)	SAMPLE BOX TEMP (DEG.F)	IMPINGER TEMP (DEG.F)
					DESIRED	ACTUAL		INLET	OUTLET			
INIT	0	1200	74.879									
	10.0	1210	80.200	.850	1.08	1.08	325.	64.	63.	5.0	342.	48.
	20.0	1220	85.290	.770	.98	.98	326.	66.	64.	5.5	326.	48.
	30.0	1230	90.428	.770	.98	.98	326.	68.	64.	6.0	329.	50.
	40.0	1240	95.500	.750	.95	.95	328.	72.	65.	6.8	330.	52.
	50.0	1250	100.600	.750	.95	.95	325.	74.	66.	7.0	321.	54.
	60.0	1300	105.525	.730	.92	.92	326.	75.	67.	7.5	324.	52.
	70.0	1310	110.500	.730	.92	.92	327.	76.	68.	8.0	309.	56.
	80.0	1320	115.580	.730	.92	.92	327.	76.	68.	8.5	320.	58.
	90.0	1330	120.457	.730	.92	.92	328.	76.	68.	9.0	326.	60.
TOTALS AVERAGE	90.0		45.578		.96	.96	326.	72.	66.	7.0	325.	53.

PARTICULATE FIELD DATA & RESULTS TABULATION

PLANT- NAME AND ADDRESS

TEST TEAM LEADER

CLARKE

TEST 10DM5P

UNIT TWO EAST

ENGLISH UNITS

METRIC UNITS

TEST DATE

02/12/83

02/12/83

TR TIME-START
TF TIME-FINISH

1200
1330

1200
1330

TT NET TIME OF TEST, MIN.

90.0

90.0

NP NET SAMPLING POINTS

9

9

Y METER CALIBRATION FACTOR

1.030

1.030

DN SAMPLING NOZZLE DIAMETER

.210 IN

5.3 MM

CP PITOT TUBE COEFFICIENT

.84

.84

PM AVERAGE ORIFICE PRESSURE
DROP

.96 IN-H2O

24.3 MM-H2O

VM VOLUME OF DRY GAS SAMPLED
AT METER CONDITIONS

45.578 CU-FT

1.291 CU-M

TM AVERAGE GAS METER TFMP

68.9 F

20.5 C

VMSTD VOLUME OF DRY GAS SAMPLED
AT STANDARD CONDITIONS*

47.525 SCF

1.346 SCM

VLC TOTAL H2O COLLECTED IN
IMPINGERS AND SILICA GEL, ML.

137.5

137.5

VWC VOLUME OF WATER VAPOR
AT STANDARD CONDITIONS*

6.472 SCF

.183 SCM

BWO PERCENT MOISTURE BY VOLUME
(CHECK AGAINST SATURATION
POINT HAS BEEN MADE.)

11.99

11.99

FMD MOLE FRACTION DRY GAS

.880

.880

PCO2 PERCENT CO2 BY VOL., DRY

13.00

13.00

PO2 PERCENT O2 BY VOL., DRY

3.00

3.00

PCO PERCENT CO BY VOL., DRY

.00

.00

PN2 PERCENT N2 BY VOL., DRY

84.00

84.00

MD MOLECULAR WT-DRY STACK GAS

30.20

30.20

A-198

MWS	MOLECULAR WT-STACK GAS	28.74		28.74	
PB	BAROMETRIC PRESSURE	30.27	IN-HG	768.86	MM-HG
PSI	STATIC PRES OF STACK GAS	-.40	IN-H2O	-10.16	MM-H2O
PS	STACK PRES, ABS.	30.24	IN-HG	768.11	MM-HG
TS	AVERAGE STACK TEMP	326.	F	164.	C
VS	AVG STACK GAS VELOCITY	59.4	FPS	18.1	MPS
AS	STACK AREA	20612.	SQ-IN	13.298	SQ-M
QSTD	STACK FLOW RATE, DRY*	18282604.	SCFH	517709.	SCMH
QS	ACTUAL STACK FLOW RATE	30612136.	ACFH	866844.	ACMH
ISO	PERCENT ISOKINETIC	103.1		103.1	
MN	AMBIENT PARTICULATE MG. EPA 5	213.8		213.8	
CS	AMBIENT PARTICULATE	.0694	GR/DSCF*	158.885	MG/DSCM

* 68 DEG F, 29.92 IN.HG.

EXAMPLE PARTICULATE CALCULATIONS TEST NO.100M5P

UNIT TWO EAST

VOLUME OF DRY GAS SAMPLED AT STANDARD CONDITIONS

$$VMSTD = (17.647 * VM * Y * (PB + PM / 13.6)) / (TM + 460.)$$

$$VMSTD = \frac{17.647 * 45.578 * 1.030 * (30.27 + .958 / 13.6)}{(69. + 460.)} = 47.525 \text{ DSCF}$$

VOLUME OF WATER VAPOR AT STANDARD CONDITIONS

$$VMC = .04707 * VLC$$

$$VMC = .04707 * 138. = 6.47 \text{ SCF}$$

PERCENT MOISTURE IN STACK GAS

$$BWD = (100. * VMC) / (VMSTD + VMC)$$

$$BWD = \frac{100. * 6.47}{47.525 + 6.47} = 11.99 \text{ PERCENT}$$

MOLE FRACTION OF DRY STACK GAS

$$FMD = (100. - BWD) / 100.$$

$$FMD = \frac{100. - 12.0}{100.} = .880$$

AVERAGE MOLECULAR WEIGHT OF DRY STACK GAS

$$MD = (PCO2 * .44) + (PO2 * .32) + (PN2 + PCO) * .28$$

$$MD = (13.00 * 44 / 100) + (3.0 * 32 / 100) + ((84.0 + .0) * 28 / 100) = 30.20$$

MOLECULAR WEIGHT OF STACK GAS

$$MWS = MD * (1. - (BWD / 100)) + 18. * (BWD / 100)$$

$$MWS = 30.20 * (1. - (11.99 / 100)) + 18. * (11.99 / 100) = 28.74$$

STACK GAS VELOCITY AT STACK CONDITIONS

$$DEL P = \text{SUM, OF THE SQRT}(VH * (TS + 460.))$$

$$VS = 85.49 * CP * DEL P / (\text{SQRT}(MWS * PS) * PNTS)$$

$$VS = 85.49 * .84 * 219.484 / (\text{SQRT}(28.74 * 30.24) * 9.) = 59.41 \text{ FPS}$$

STACK GAS VOLUMETRIC FLOW AT STACK CONDITIONS

$$QS = VS * AS * 3600/144$$

$$QS = 59.41 * 20612.3600/144 = 30612136. \text{ ACFH}$$

STACK GAS VOLUMETRIC FLOW AT STANDARD CONDITIONS

$$QSSTD = 17.647 * QS * PS * (1. - (BWD/100)) / (TS + 460.)$$

$$QSSTD = \frac{17.647 * 30612136. * 30.24 * (1. - (11.99/100))}{(326. + 460.)} = 18282604. \text{ SCFH}$$

PERCENT ISOKINETIC

$$ISO = (305.58 * (TS + 460.)) * ((0.002669 * VLC) + (VM * Y * (PR + (PM/13.6)) / (TM + 460.))) / (IT * VS * PS * DN * DN)$$

$$ISO = \frac{(305.58 * (326. + 460.)) * ((0.002669 * 138.) + (45.578 * 1.030 * (30.27 + (.958/13.6)) / (69. + 460.)))}{90. * 59.41 * 30.24 * .210 * .210} = 103.14 \text{ PERCENT}$$

PARTICULATE LOADING -- EPA METHOD 5 (AT STANDARD CONDITIONS)

$$CS = 0.001 * MN * 15.43 / VMSTD$$

$$CS = 0.001 * 213.8 * 15.43 / 47.525 = .0694 \text{ GR/DSCF}$$

END OF PROGRAM
:EOJ
CPU SEC. = 109. ELAPSED MIN. = 3. FRI, MAR 18, 1983, 12:27 PM

APPENDIX B
FIELD DATA

PLANT & CITY																																DATE		SAMPLING LOCATION																SAMPLE TYPE																													
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																2/7/83		PART 2 TEST																PARTIC SP3 SP2																													

[illegible][illegible]

DI-125

[illegible]

PLANT & CITY																																								DATE				SAMPLING LOCATION																				SAMPLE TYPE															
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																	2/17/83				1241T 21E11ST																				PPT								PPT														

[illegible][illegible][illegible]

1-C

[illegible]

Pre test @ 15" OK

[illegible]

* PRUBENANT SHORTED OUT
Rat at 3:15 on 10/14

1-D

[illegible]

Protest @ 15" O L

[illegible]

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/7/83
 Sample location Boiler #2 Recovery date 2/7/83
 Run number 1A M5 BW Recovered by DO/DS
 Particulate sample type _____ M5 _____ M5-320 _____ M5-450 ☒ M5W-320
 Particulate filter number 3531017 ✓
 Particulate filter sample I.D. 4313 B ✓
 Probe rinse H₂O I.D. 4313 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half between imp #2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>632.3</u> g	<u>629.6</u> g	<u>620.0</u> g	<u>616.9</u> g	<u>872.6</u> g
Initial wt	<u>502.1</u> g	<u>669.3</u> g	<u>599.9</u> g	<u>597.0</u> g	<u>828.1</u> g
Net wt	<u>130.2</u> g	<u>-39.7</u> g	<u>30.1</u> g	<u>19.9</u> g	<u>44.5</u> g
Total moisture	<u>184.9</u> g				<u>80</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4313 A ✓
 IPA IMP. CONTAINER I.D. 4314 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4315 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ✓
 H₂O₂ 4302 A ✓
 H₂O 4304 A ✓
 Acetone 4301 A ✓

Samples stored and locked _____

Remarks Filter Blank #3531026, I.D. 4301 B ✓
PROBE RINSE BLANK - CONT. NO. 4305 A ✓
Rinse - H₂O

LABORATORY CUSTODY

Received by Thomas Chute Date 15 Feb 1983
 Remarks Reg # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/7/83
 Sample location Boyer #2 Recovery date 2/7/83
 Run number 1BM5BW Recovered by 20/25
 Particulate sample type _____ M5 _____ M5-320 _____ M5-450 ☒ M5W-320
 Particulate filter number 3531016 ✓
 Particulate filter sample I.D. 4316 B ✓
 Probe rinse H₂O I.D. 4316 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half between imp. #2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>634.6</u> g	<u>622.7</u> g	<u>634.9</u> g	<u>624.5</u> g	<u>857.3</u> g
Initial wt	<u>503.9</u> g	<u>664.9</u> g	<u>603.6</u> g	<u>603.3</u> g	<u>816.2</u> g
Net wt	<u>130.7</u> g	<u>-42.2</u> g	<u>31.3</u> g	<u>21.2</u> g	<u>41.1</u> g
Total moisture	<u>192.1</u> g				<u>90</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4316 A ✓
 IPA IMP. CONTAINER I.D. 4317 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4318 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ✓
 H₂O₂ 4302 A ✓
 H₂O 4304 A ✓
 Acetone 4301 A ✓

Samples stored and locked _____

Remarks Filter blank #3531026, ID. 4301B ✓
Probe Rinse Blank - CONT ID 4306 A ✓
Rinse H₂O

LABORATORY CUSTODY

Received by Louis White Date 15 Feb - 1983
 Remarks leg #4061

Plant _____ Sample date 2/7/83
Sample location Boyer No. 2 Recovery date 2/7/83
Run number 1CM5B Recovered by DE/DS
Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
Particulate filter number 3531015 ✓
Particulate filter sample I.D. 4319B ✓
Probe rinse Acetone I.D. 4319A ✓
Purge train 20 min (check when completed) ☒
Location of filter in back half between imp #2 + 3

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>604.5</u> g	<u>631.7</u> g	<u>569.1</u> g	<u>629.2</u> g	<u>888.9</u> g
Initial wt	<u>481.4</u> g	<u>666.3</u> g	<u>537.8</u> g	<u>609.3</u> g	<u>857.6</u> g
Net wt	<u>123.1</u> g	<u>-34.6</u> g	<u>31.3</u> g	<u>19.9</u> g	<u>37.3</u> g
	Total moisture			<u>177.0</u> g	<u>90</u> % spent

PROBE RINSE CONTAINER I.D.	<u>4319A ✓</u>	
IPA IMP. CONTAINER I.D.	<u>4320A ✓</u>	LIQUID LEVEL MARKED <u>✓</u>
H ₂ O ₂ IMP. CONTAINER I.D.	<u>4321A ✓</u>	LIQUID LEVEL MARKED <u>✓</u>
BLANK CONTAINER(S) I.D.		LIQUID LEVEL MARKED
IPA	<u>4303A ✓</u>	<u>✓</u>
H ₂ O ₂	<u>4302A ✓</u>	<u>✓</u>
H ₂ O	<u>4304A ✓</u>	<u>✓</u>
Acetone	<u>4301A ✓</u>	<u>✓</u>

Remarks Filter Blank #3531026; ID. 4301B ✓
Probe Rinse Blank - CONT. ID. 4307A ✓
Rinse - Acetone

Received by Thomas Thiele Date 15 Feb 1983
Remarks Reg. # 406

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/7/83
Sample location Boxer No. 20 Recovery date 2/7/83
Run number 1DM5B Recovered by DA/DS
Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
Particulate filter number 3531014 ✓
Particulate filter sample I.D. 4322B ✓
Probe rinse Acetone I.D. 4322A ✓
Purge train 20 min (check when completed) ☒
Location of filter in back half Between imp #2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>616.9</u> g	<u>631.2</u> g	<u>630.3</u> g	<u>616.5</u> g	<u>869.7</u> g
Initial wt	<u>495.1</u> g	<u>667.9</u> g	<u>597.4</u> g	<u>598.2</u> g	<u>833.1</u> g
Net wt	<u>121.8</u> g	<u>-36.7</u> g	<u>32.9</u> g	<u>18.3</u> g	<u>36.6</u> g
	Total moisture			<u>172.9</u> g	<u>80</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D.	<u>4322A ✓</u>	
IPA IMP. CONTAINER I.D.	<u>4323A ✓</u>	LIQUID LEVEL MARKED <u>✓</u>
H ₂ O ₂ IMP. CONTAINER I.D.	<u>4324A ✓</u>	LIQUID LEVEL MARKED <u>✓</u>
BLANK CONTAINER(S) I.D.		LIQUID LEVEL MARKED
IPA	<u>4303A ✓</u>	<u>✓</u>
H ₂ O ₂	<u>4302A ✓</u>	<u>✓</u>
H ₂ O	<u>4304A ✓</u>	<u>✓</u>
Acetone	<u>4301A ✓</u>	<u>✓</u>

Samples stored and locked _____
Remarks F. Net Went # 3531026, I.D. 4301B ✓
PROBE RINSE BOWL - CONT. I.D. 4308A ✓
RINSE - ACETONE

LABORATORY CUSTODY

Received by James White Date 15 Feb. 1983
Remarks pg. # 4061



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2.7.83 TEST NO 1-ABCD
SAMPLING TIME (24-hr CLOCK) 1145
SAMPLING LOCATION Boiler #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSA
AMBIENT TEMPERATURE 70
OPERATOR WJ
ORSAT LEAK CHECKED ✓

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.4	13.4	13.3	13.3			13.35	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	15.8	2.4	15.8	2.5			2.45	32/100	
CO(NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)							284.2	28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

PLANT & CITY	DATE	SAMPLING LOCATION																								SAMPLE TYPE																	
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18
	2/27/83	PINKET P. BASIN																								MSB, SPH, SP2																	

PT-278

TC - 178

DI-125

LEAK CHECKS Pitot - good
OASAT - good

[illegible]

Protokoll 12.10.12

[illegible]

14

MOISTURE

RECOVERED SAMPLE

Samples stored and locked

Probe Rinse Blank - Cont ID 4309 A L

ПИРАТЕ-АКТОРЪ

LABORATORY CUSTODY

Remarks REG # 4061

File A - green coat, heavy

Plant _____ Sample date 2/2/83
Sample location Bay No. 2 Recovery date 2/2+P/83
Run number 2CM5BW Recovered by DO/DS
Particulate sample type _____ M5 _____ M5-320 _____ M5-450 ☒ M5W-320
Particulate filter number 3531070 ✓
Particulate filter sample I.D. 4331B ✓
Probe rinse H₂O I.D. 4331A ✓
Purge train 20 min (check when completed) _____ ✓
Location of filter in back half bet. imp. 2+3

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>597.5</u> g	<u>623.2</u> g	<u>637.6</u> g	<u>609.1</u> g	<u>867.4</u> g
Initial wt	<u>483.3</u> g	<u>670.2</u> g	<u>604.2</u> g	<u>589.1</u> g	<u>827.9</u> g
Net wt	<u>114.2</u> g	<u>-47.0</u> g	<u>33.4</u> g	<u>20.0</u> g	<u>39.5</u> g
	Total moisture			<u>160.1</u> g	<u>80</u> % spent

PROBE RINSE CONTAINER I.D.	<u>4331 A</u> ✓	
IPA IMP. CONTAINER I.D.	<u>4332 A</u> ✓	LIQUID LEVEL MARKED <u>✓</u>
H ₂ O ₂ IMP. CONTAINER I.D.	<u>4333 A</u> ✓	LIQUID LEVEL MARKED <u>✓</u>
BLANK CONTAINER(S) I.D.		LIQUID LEVEL MARKED
IPA	<u>4303 A</u> ✓	<u>✓</u>
H ₂ O ₂	<u>4302 A</u> ✓	<u>✓</u>
H ₂ O	<u>4304 A</u> ✓	<u>✓</u>
Acetone	<u>4301 A</u> ✓	<u>✓</u>

Remarks FINER BANK #3531026, I.D. 4301B
PROBE RINSE BANK - CONT. I.D. - 4311A ✓
RINSE - H₂O

Received by Marie D'Amico Date 15 Feb-1982
Remarks pc # 4061

Slender - green coat, heavy

* Approx 20 ml acetone in probe tube

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/7/83
 Sample location Boyer #2 Recovery date 2/7+8/83
 Run number 2DM5BW Recovered by DO/DS
 Particulate sample type _____ M5 _____ M5-320 _____ M5-450 ☒ M5W-320
 Particulate filter number 3531069 ✓
 Particulate filter sample I.D. 4334 B ✓
 Probe rinse H₂O I.D. 4334 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>571.1</u> g	<u>615.9</u> g	<u>572.5</u> g	<u>645.9</u> g	<u>871.5</u> g
Initial wt	<u>465.0</u> g	<u>659.2</u> g	<u>541.1</u> g	<u>621.5</u> g	<u>830.1</u> g
Net wt	<u>106.1</u> g	<u>-43.3</u> g	<u>31.4</u> g	<u>24.4</u> g	<u>41.4</u> g
Total moisture	<u>160.0</u> g				<u>90</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4334 A ✓
 IPA IMP. CONTAINER I.D. 4335 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4336 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ✓
 H₂O₂ 4302 A ✓
 H₂O 4304 A ✓
 Acetone 4301 A ✓

Samples stored and locked _____

Remarks Filter Blank # 3531026, I.D. 43013 ✓
Probe Rinse Blank - Cont. I.D. 4312 A ✓
RINSE-H₂O

LABORATORY CUSTODY

Received by Sharon White Date 15 Feb 1983
 Remarks plg # 4CE1

Filter - green coat, heavy



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2.7.83 TEST NO 2 - ABCD
SAMPLING TIME (24-hr CLOCK) _____
SAMPLING LOCATION Boiler #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSAT
AMBIENT TEMPERATURE _____
OPERATOR _____
ORSAT LEAK CHECKED ✓

COMMENTS:

GRAB Sample @ 1600

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb 'lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.6	13.6	13.6	13.6			13.6	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	16.6	3.0	16.5	2.9			2.95	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

PLANT & CITY	DATE	SAMPLING LOCATION	SAMPLE TYPE
	30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80		
	2/18/83	UNIT 3 EAST	PART 503 1504

[illegible][illegible]

PT-379

DI-125

OP- 999

or sat good - no leaks
pitot good no leaks

[illegible]

PLANT & CITY	EMISSION TESTING FIELD DATA																																			
	DATE		SAMPLING LOCATION																								SAMPLE TYPE									
	24	25	26	27	28	29	30	01	02	03	04	05	06	07	08	09	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29
	12/18/83		UNIT 2 GAS																								PART 1503, 1302									

BUN NO.	OPERATOR								Amb. TEMP (°F)	BAR. PRESS. (IN. Hg.)	STATIC PRESS. (IN. H ₂ O)	FILTER NUMBER(S)	STACK INSIDE DIMEN. (INCHES)	PITOT TUBE CØ	THERM NO.	PAGE
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75																
3BM5B	V.R. RA J.P.								45	303#	-60	3 5 3 1 9 0 9	V 6 2	0 8 4		10 F

[illegible]

LEAK CHECK, tot tube good
orsat - good.

[illegible]

3 C

$$7.16 + 379$$
$$6.17999$$

Protect@26"ok

4. 554

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/8/83
 Sample location Boiler #2 Recovery date 2/8/83
 Run number 3A M5 B Recovered by NO, DA
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531010 ☒
 Particulate filter sample I.D. 4338 B ☒
 Probe rinse Acetone I.D. 4338 A ☒
 Purge train 20 min (check when completed) ☒
 Location of filter in back half between imp's 2+3.

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>626.5</u> g	<u>642.7</u> g	<u>630.6</u> g	<u>606.7</u> g	<u>P35.5</u> g
Initial wt	<u>505.7</u> g	<u>676.0</u> g	<u>600.0</u> g	<u>591.6</u> g	<u>P00.3</u> g
Net wt	<u>120.8</u> g	<u>-33.3</u> g	<u>30.6</u> g	<u>17.1</u> g	<u>35.2</u> g
Total moisture	<u>170.4</u> g				<u>P5</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4338 A ☒
 IPA IMP. CONTAINER I.D. 4339 A ☒ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4340 A ☒ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ☒
 H₂O₂ 4302 A ☒
 H₂O 4304 A ☒
 Acetone 4301 A ☒

Samples stored and locked _____
 Remarks _____

LABORATORY CUSTODY

Received by Lionel White Date 15 Feb 1983
 Remarks reg. # 4061

Killer - green coat, heavy

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/8/83
 Sample location Boiler #2 Recovery date 2/8/83
 Run number 3B M5 B Recovered by AD, AD
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531009 ✓
 Particulate filter sample I.D. 4331 B 4341 B ✓
 Probe rinse Acetone I.D. 4341 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half BETWEEN imp's 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>630.4</u> g	<u>630.8</u> g	<u>634.2</u> g	<u>622.7</u> g	<u>856.4</u> g
Initial wt	<u>506.9</u> g	<u>671.2</u> g	<u>604.2</u> g	<u>602.7</u> g	<u>820.7</u> g
Net wt	<u>123.5</u> g	<u>-40.4</u> g	<u>30.0</u> g	<u>20.0</u> g	<u>35.7</u> g
Total moisture	<u>168.8</u> g				<u>85</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4341 A ✓
 IPA IMP. CONTAINER I.D. 4342 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4343 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ✓ ☒
 H₂O₂ 4302 A ✓ ☒
 H₂O 4304 A ✓ ☒
 Acetone 4301 A ✓ ☒

Samples stored and locked _____

Remarks _____

LABORATORY CUSTODY

Received by James White Date 15 Feb. 1983

Remarks Acq. # 4061

Filter - green coat, heavy

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/8/83
 Sample location Boiler #2 Recovery date 2/8/83
 Run number 3C M5B - P400 Recovered by DB/DS
 Particulate sample type _____ M5 ☒ M5-320 P400 ~~M5-450~~ _____ M5W
 Particulate filter number 353/00P ✓
 Particulate filter sample I.D. 4344B ✓
 Probe rinse Acetone I.D. 4344A ✓
 Purge train 20 min (check when completed) _____ ✓
 Location of filter in back half Between imp's 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>590.0</u> g	<u>641.8</u> g	<u>563.7</u> g	<u>624.2</u> g	<u>881.4</u> g
Initial wt	<u>483.4</u> g	<u>662.1</u> g	<u>545.1</u> g	<u>610.5</u> g	<u>851.6</u> g
Net wt	<u>106.6</u> g	<u>-25.3</u> g	<u>18.6</u> g	<u>13.7</u> g	<u>29.8</u> g
Total moisture	<u>143.4</u> g				<u>55</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4344A ✓
 IPA IMP. CONTAINER I.D. 4345A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4346A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303A ✓ ☒
 H₂O₂ 4302A ✓ ☒
 H₂O 4304A ✓ ☒
 Acetone 4301A ✓ ☒

Samples stored and locked _____
 Remarks _____

LABORATORY CUSTODY

Received by Donis White Date 15-Feb. 1983
 Remarks Reg # 4061

Filter - green coat, heavy

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/8/83
 Sample location Boiler #2 Recovery date 2/8/83
 Run number 3DM5B-P400 Recovered by DO/DS
 Particulate sample type M5 ☒ M5-320 P400 ~~M5-450~~ M5W
 Particulate filter number 3531007 ☒
 Particulate filter sample I.D. 4347B ☒
 Probe rinse Acetone I.D. 4347A ☒
 Purge train 20 min (check when completed) ☒
 Location of filter in back half between imp's 2+3.

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>613.3</u> g	<u>639.0</u> g	<u>626.4</u> g	<u>622.8</u> g	<u>PP6.7</u> g
Initial wt	<u>492.6</u> g	<u>672.8</u> g	<u>594.6</u> g	<u>604.6</u> g	<u>P55.1</u> g
Net wt	<u>115.7</u> g	<u>-33.8</u> g	<u>31.8</u> g	<u>18.2</u> g	<u>31.6</u> g
Total moisture	<u>163.5</u> g				<u>60</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4347A ☒
 IPA IMP. CONTAINER I.D. 4348A ☒ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4349A ☒ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303A ☒
 H₂O₂ 4302A ☒
 H₂O 4304A ☒
 Acetone 4301A ☒

Samples stored and locked _____
 Remarks _____

LABORATORY CUSTODY

Received by Louis White Date 15 Feb. 1983
 Remarks Fig # 4061

Filter - green coat w/ black, heavy



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2.8.83 TEST NO 3
SAMPLING TIME (24-hr CLOCK) 1040
SAMPLING LOCATION Boiler #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSAT
AMBIENT TEMPERATURE 60
OPERATOR D. Schuff
ORSAT LEAK CHECKED ✓

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb/lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.6	13.6	13.8	13.8			13.7	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	16.0	2.4	16.1	2.3			2.35	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

PLANT & CITY																																DATE		SAMPLING LOCATION																SAMPLE TYPE																													
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																12/8/83		UNIT 2 EAST																PART 503 504																													

RUN NO.				OPERATOR																AMB. TEMP. (°F)	BAR. PRESS. (IN. HG)	STATIC PRESS. (IN. H ₂ O)	FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)								PITOT TUBE C _p	THERM. NO.	PAGE																														
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
G.A.M.S.I.A.P.				R.R. R.A. P.R.																50	31.0	3.6	13513P458																163								084	178	10 F																														

PROBE LENGTH AND TYPE																			NOZZLE,		H ₂ O, (\$)	SAMPLE BOX NO	METER BOX NO	METER Δ H Ø	METER CAL. FACTOR V	LEAK CHECK		K FACTOR	C FACTOR	PROBE HEAT SET	BOX HEAT SET	REF. Δ P	RECORD DATA MIN																																														
																			I.D.	NO.						IN. HG	CFM																																																				
8	9	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
1	S	E	T																4	3	4								1	1	1			F	B	4	1	7	2	1	2	0	3	1	9	0	0	0	1	1	1	1	1	2	4	A	1	1	7	0	0	3	2	9	A	1	1	1	0	0									

DI-125
OP-948

pitot tube no leaks
orint no leaks

[illegible]

EMISSION TESTING FIELD DATA																																																																															
PLANT & CITY																				DATE				SAMPLING LOCATION												SAMPLE TYPE																																											
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																				12/18/83				UNIT 2 EAST												PLANT SPB 151014																																											

RUN NO.				OPERATOR																AMB TEMP (°F)		BAR. PRESS. (IN. Hg)		STATIC PRESS. (IN. H ₂ O)		FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)								PILOT TUBE C _D		THEM NO.		PAGE																										
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	
4	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
4	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
4	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
4	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
4	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
4	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74						

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7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57
TRAVERSE POINT NUMBER				CLOCK TIME (24 hr CLOCK)		GAS METER READING (V _m), ft ³		VELOCITY HEAD (Δp ₀), in. H ₂ O		ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H ₂ O		STACK TEMPERATURE (T _s), °F		DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg		SAMPLE BOX TEMPERATURE °F		IMPINGER TEMPERATURE °F																														
												INLET (T _{m in}), °F		OUTLET (T _{m out}), °F				F		P																														
0				1230		162.434				DESIRED		ACTUAL																																						
10.						168.474		0.72		0.95		0.95		314		52		52		4.5		320		409		24.49																								
20.						174.553		0.72		0.95		0.95		317		52		52		4.5		324		420		48																								
30.						180.584		0.72		0.95		0.95		318		58		52		5.0		323		402		50																								
40.						186.800		0.7275		0.99		0.99		318		61		52		5.5		322		464		50																								
50.						192.990		0.75		0.99		0.99		317		64		54		6.0		322		402		51																								
60.						199.064		0.72		0.95		0.95		317		65		56		6.5		324		407		50																								
70.						205.137		0.72		0.95		0.95		317		66		56		6.5		327		407		50																								
80.						211.094		0.70		0.92		0.92		318		66		58		7.0		328		417		50																								
90.						217.103		0.70		0.92		0.92		318		67		59		7.5		330		419		51																								
100.						223.214		0.72		0.95		0.95		317		68		60		7.5		323		420		50																								
110.						229.300		0.72		0.95		0.95		318		69		60		8.0		327		418		50																								
120.				1430		235.462		0.72		0.95		0.95		319		69		60		8.5		324		414		50																								
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PLANT & CITY																																	DATE		SAMPLING LOCATION																SAMPLE TYPE																												
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																	02/08/83		4411T T44 EAST																M5B																												

RUN NO.			OPERATOR																												AMB TEMP (°F)		BAR. PRESS. (IN. Hg)		STATIC PRESS (IN. H ₂ O)		FILTER NUMBER(S)										STACK INSIDE DIMEN. (INCHES)						PITOT TUBE C _D		THERM NO.		PAGE																						
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
JC-1758						K. CHARNEY																												60		30.36		-10.6		353, 1266										162						ea178		10 F																					

Pilot
278

[illegible]

.211 gm

[illegible]

60.527

29

65.25

PLANT & CITY																																	DATE			SAMPLING LOCATION																					SAMPLE TYPE																						
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																	92/98/83			4 W/IT 1749 1545 IT																					17568																						

RUN NO.					OPERATOR																												AMB TEMP (°F)	BAR. PRESS. (IN. Hg)	STATIC PRESS (IN. H ₂ O)	FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)								PITOT TUBE Cp	THERM NO.	PAGE																	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
141458					CKIAIRKE																												60	30.36	10.61	353, 10.62																1624									219/78	01																	

[illegible][illegible]

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/8/83
 Sample location Biller #2 Recovery date 2/8+9/83
 Run number 4 AMSB P400 Recovered by DA/DS
 Particulate sample type M5 ☒ M5-320 P400 ~~M5-450~~ M5W
 Particulate filter number 3530458 3530458 ✓
 Particulate filter sample I.D. 43522 B ✓
 Probe rinse Acetone I.D. 43521 ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half between imp's 2+3.

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>619.5</u> g	<u>634.6</u> g	<u>644.7</u> g	<u>615.8</u> g	<u>867.1</u> g
Initial wt	<u>494.3</u> g	<u>672.0</u> g	<u>612.3</u> g	<u>596.8</u> g	<u>828.6</u> g
Net wt	<u>125.2</u> g	<u>-37.4</u> g	<u>32.4</u> g	<u>19.0</u> g	<u>38.5</u> g
Total moisture	<u>177.7</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D.	<u>4352 A</u> ✓	
IPA IMP. CONTAINER I.D.	<u>4353 A</u> ✓	LIQUID LEVEL MARKED ☒
H ₂ O ₂ IMP. CONTAINER I.D.	<u>4354 A</u> ✓	LIQUID LEVEL MARKED ☒
BLANK CONTAINER(S) I.D.		LIQUID LEVEL MARKED
IPA	<u>4303 A</u> ✓	☒
H ₂ O ₂	<u>4302 A</u> ✓	☒
H ₂ O	<u>4304 A</u> ✓	☒
Acetone	<u>4301 A</u> ✓	☒

Samples stored and locked _____

Remarks _____

LABORATORY CUSTODY

Received by Donna White Date 15 Feb 1983

Remarks reg #4061

Filter - green coat, heavy

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/8/83
 Sample location Bulk #2 Recovery date 2/8/10/83
 Run number 4B M5B P400 Recovered by DA/DS
 Particulate sample type _____ M5 ☒ M5-320 P400 ~~M5-450~~ _____ M5W
 Particulate filter number 0002530 ✓
 Particulate filter sample I.D. 4355B ✓
 Probe rinse Acetone I.D. 4355A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half between imp's 2+3.

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>620.4</u> g	<u>622.4</u> g	<u>621.5</u> g	<u>646.7</u> g	<u>864.9</u> g
Initial wt	<u>490.5</u> g	<u>671.3</u> g	<u>584.7</u> g	<u>624.5</u> g	<u>820.5</u> g
Net wt	<u>129.9</u> g	<u>-48.9</u> g	<u>36.8</u> g	<u>22.2</u> g	<u>44.4</u> g
Total moisture	<u>184.4</u> g				<u>50</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4355A ✓
 IPA IMP. CONTAINER I.D. 4356A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4357A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303A ✓ ☒
 H₂O₂ 4302A ✓ ☒
 H₂O 4304A ✓ ☒
 Acetone 4301A ✓ ☒

Samples stored and locked _____
 Remarks _____

LABORATORY CUSTODY

Received by Donna White Date 15 Feb 1983
 Remarks req # 4061

green coat, heavy, w/ black mostly around edge

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/8/83
 Sample location Boiler #2 Recovery date 2/8+10/83
 Run number 4C M5B Recovered by DO/PS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531066 ✓
 Particulate filter sample I.D. 4958 B ✓
 Probe rinse Acetone I.D. 4358 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half Between imp's 2+3.

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>610.2</u> g	<u>624.6</u> g	<u>623.8</u> g	<u>630.5</u> g	<u>1229.5</u> g
Initial wt	<u>498.6</u> g	<u>664.0</u> g	<u>591.4</u> g	<u>610.5</u> g	<u>797.8</u> g
Net wt	<u>111.6</u> g	<u>-39.4</u> g	<u>32.4</u> g	<u>20.0</u> g	<u>31.7</u> g
Total moisture	<u>156.3</u> g				<u>35</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4358 A ✓
 IPA IMP. CONTAINER I.D. 4359 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4360 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ✓ ☒
 H₂O₂ 4302 A ✓ ☒
 H₂O 4304 A ✓ ☒
 Acetone 4301 A ✓ ☒

Samples stored and locked _____
 Remarks _____

LABORATORY CUSTODY

Received by Adrian White Date 15 Feb 1983
 Remarks pcg # 4061

Filter - green coat, heavy

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/8/83
 Sample location Bldg #2 Recovery date 2/8+10/83
 Run number 4D M5B Recovered by DO/PS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531068 ☒
 Particulate filter sample I.D. 4361 B ☒
 Probe rinse Acetone I.D. 4361 A ☒
 Purge train 20 min (check when completed) ☒
 Location of filter in back half between imps 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>577.8</u> g	<u>623.0</u> g	<u>584.4</u> g	<u>642.1</u> g	<u>173.5</u> g
Initial wt	<u>468.0</u> g	<u>665.4</u> g	<u>552.6</u> g	<u>620.9</u> g	<u>834.5</u> g
Net wt	<u>109.8</u> g	<u>-42.4</u> g	<u>31.8</u> g	<u>21.2</u> g	<u>39.0</u> g
Total moisture	<u>159.4</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4361 A ☒
 IPA IMP. CONTAINER I.D. 4362 A ☒ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4363 A ☒ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ☒
 H₂O₂ 4302 A ☒
 H₂O 4304 A ☒
 Acetone 4301 A ☒

Samples stored and locked _____
 Remarks Acetone probe rinse blank #4350A ☒

LABORATORY CUSTODY

Received by Shirley White Date 15 Feb. 1983
 Remarks reg #4061

Filter - green coat, heavy, w/ some black



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2.8.83 TEST NO. 04 BAG A
SAMPLING TIME (24-hr CLOCK) 1420
SAMPLING LOCATION Boiler #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSAT
AMBIENT TEMPERATURE 70
OPERATOR A. Schepel
ORSAT LEAK CHECKED ✓

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb/lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.6	13.6	13.6	13.6			13.6	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	15.9	2.3	15.9	2.3			2.3	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2.8.83 TEST NO. 4 Bag B
SAMPLING TIME (24-hr CLOCK) 1430
SAMPLING LOCATION Bailer #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSA
AMBIENT TEMPERATURE 70
OPERATOR D. Schiffel
ORSAT LEAK CHECKED _____

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M_d , lb/lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.6	13.6	13.6	13.6			12.8 13.6	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	15.9	2.3	15.9	2.3			2.3	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

PLANT & CITY																																	DATE		SAMPLING LOCATION																SAMPLE TYPE																												
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
7																																	2/11/8		UNIT 2 EAST																MSB																												

PROBE LENGTH AND TYPE																				NOZZLE				H ₂ O (\$)	SAMPLE BOX NO	METER BOX NO	METER Δ H Ø	METER CAL. FACTOR V	LEAK CHECK		K FACTOR	C FACTOR	PROBE HEAT SET	BOX HEAT SET	REF. AP	RECORD DATA MINS																																																															
																				I.D.	NO.								IN. HG	CFM																																																																					
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
5 FT. 64.6151																				0223				1A				1P				F64				172				0003				700000				VX100				A A A				320				320				A A A				100																															

DT-125
OP-999

pitot tube no leaks
output no leaks IF-#447

[illegible]

PLANT & CITY																																								DATE				SAMPLING LOCATION																				SAMPLE TYPE															
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																	2/11/83				UNIT 2 EAST																				MSB																						

RUN NO.					OPERATOR																												AMB. TEMP (°F)		BAR. PRESS. (IN. Hg)		STATIC PRESS. (IN. H ₂ O)		FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)				PITOT TUBE CO		THE RM NO.		PAGE																	
0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
58458					PR RA NP																												60.3		30.5		780		3531913																162								084206		10 F 1															

[illegible]

IT - #449

[illegible]

5-C

RUN NO.		OPERATOR																												AMB. TEMP (°F)		BAR. PRESS. (IN. HG)		STATIC PRESS (IN. H ₂ O)		FILTER NUMBER(S)										STACK INSIDE DIMEN. (INCHES)				PITOT TUBE Cp		THERM NO.		PAGE																																													
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
5C-158		CLARK																												60.5		30.5		-10.8		3531124										162				89		206		101																																													

[illegible]

Patent @ 15

ITC#
450

[illegible]

46 949

5-D

448

15.0

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Bayer No. 2 Recovery date 2/11/83
 Run number 5A MSB Recovered by DB/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531067 ✓
 Particulate filter sample I.D. 4364 B ✓
 Probe rinse Acetone I.D. 4364 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half left, dup 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>596.4</u> g	<u>644.9</u> g	<u>625.2</u> g	<u>611.2</u> g	<u>856.1</u> g
Initial wt	<u>504.9</u> g	<u>675.9</u> g	<u>597.0</u> g	<u>595.4</u> g	<u>822.0</u> g
Net wt	<u>91.5</u> g	<u>-31.0</u> g	<u>28.2</u> g	<u>15.8</u> g	<u>34.1</u> g
Total moisture	<u>138.6</u> g				<u>35</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4364 A ✓
 IPA IMP. CONTAINER I.D. 4365 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4366 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ✓
 H₂O₂ 4302 A ✓
 H₂O 4304 A ✓
 Acetone 4301 A ✓

Samples stored and locked _____
 Remarks Filter - green coat, medium

LABORATORY CUSTODY

Received by Sharon White Date 15 Feb 1983
 Remarks reg # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Bayer #2 Recovery date 2/11/83
 Run number SBMSB Recovered by DB/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W _____
 Particulate filter number 353101F-353101B ✓
 Particulate filter sample I.D. 4367B ✓
 Probe rinse McDane I.D. 4367A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half Ext. Imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>596.4</u> g	<u>637.0</u> g	<u>642.1</u> g	<u>617.6</u> g	<u>PP4.3</u> g
Initial wt	<u>507.5</u> g	<u>669.5</u> g	<u>610.8</u> g	<u>599.9</u> g	<u>852.6</u> g
Net wt	<u>88.9</u> g	<u>-32.5</u> g	<u>31.3</u> g	<u>17.8</u> g	<u>31.7</u> g
Total moisture	<u>137.2</u> g				<u>25</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4367A ✓
 IPA IMP. CONTAINER I.D. 4368A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4369A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303A ✓ ☒
 H₂O₂ 4302A ✓ ☒
 H₂O 4304A ✓ ☒
 Acetone 4301A ✓ ☒

Samples stored and locked _____
 Remarks Filter - green coat, medium

LABORATORY CUSTODY

Received by Shania White Date 15 Feb 1983
 Remarks reg # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Bayer #2 Recovery date 2/11/83
 Run number 5CMSB Recovered by DB/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531124 ✓
 Particulate filter sample I.D. 4370 B ✓
 Probe rinse Acetone I.D. 4370 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. dry 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>572.8</u> g	<u>622.0</u> g	<u>577.2</u> g	<u>626.9</u> g	<u>884.6</u> g
Initial wt	<u>485.4</u> g	<u>665.9</u> g	<u>546.1</u> g	<u>609.1</u> g	<u>845.4</u> g
Net wt	<u>87.4</u> g	<u>-43.9</u> g	<u>31.1</u> g	<u>17.8</u> g	<u>39.2</u> g
Total moisture	<u>131.6</u> g				<u>25</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4370 A ✓
 IPA IMP. CONTAINER I.D. 4371 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4372 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ✓
 H₂O₂ 4302 A ✓
 H₂O 4304 A ✓
 Acetone 4301 A ✓

Samples stored and locked _____
 Remarks Filter - green coat, medium

LABORATORY CUSTODY

Received by James White Date 15 Feb-1983
 Remarks Reg # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Boxer No. 2 Recovery date 2/11/83
 Run number 5DM5B Recovered by D8/DS
 Particulate sample type M5 ☒ M5-320 M5-450 M5W
 Particulate filter number 3531123 ✓
 Particulate filter sample I.D. 4373 B ✓
 Probe rinse Acetone I.D. 4373 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>586.8</u> g	<u>632.9</u> g	<u>631.8</u> g	<u>612.6</u> g	<u>163.8</u> g
Initial wt	<u>498.9</u> g	<u>673.7</u> g	<u>599.6</u> g	<u>595.5</u> g	<u>827.4</u> g
Net wt	<u>87.9</u> g	<u>-40.8</u> g	<u>32.2</u> g	<u>17.1</u> g	<u>36.4</u> g
Total moisture	<u>132.8</u> g				<u>30</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4373 A ✓
 IPA IMP. CONTAINER I.D. 4374 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4375 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4303 A ✓ ☒
 H₂O₂ 4302 A ✓ ☒
 H₂O 4304 A ✓ ☒
 Acetone 4301 A ✓ ☒

Samples stored and locked _____
 Remarks Filter green coat, medium

LABORATORY CUSTODY

Received by Lionie White Date 15 Feb. 1983
 Remarks reg. # 4061



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2.11.83 TEST NO. 05
SAMPLING TIME (24-hr CLOCK) 1500
SAMPLING LOCATION Boiler #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSAT
AMBIENT TEMPERATURE 70
OPERATOR AD
ORSAT LEAK CHECKED ☒

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb/lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	12.8	12.8	12.8	12.8			12.8	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	16.0	3.2	16.1	3.3			3.25	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

EMISSION TESTING FIELD DATA

PLANT & CITY																																		DATE		SAMPLING LOCATION																SAMPLE TYPE																											
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																		3/11/83		UNIT 2 EAST																MSB																											

2/11/83

MAY 2 EAST

MSB

RUN NO.			OPERATOR																															
AMT. TEMP. (°F)			BAR. PRESS. (IN. HG)			STATIC PRESS. (IN. H ₂ O)			FILTER NUMBER(S)										STACK INSIDE DIMEN. (INCHES)										PITOT TUBE CP		THERM. NO.		PAGE	
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35

PROBE LENGTH AND TYPE																			NOZZLE				H ₂ O (#)	SAMPLE BOX NO	METER BOX NO	METER Δ H Ø	METER CAL. FACTOR V	LEAK CHECK		K FACTOR	C FACTOR	PROBE HEAT SET		BOX HEAT SET	REF. Δ P	RECORD DATA MIN																																											
																			I.D.	NO.	IN. HG	CFM						HEAT SET	HEAT SET																																																		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
51 FT 16149 SS																			2234	2A	11P	FBH	172	1003	180	9999	11133	1	A	1	320	3219	A	1	10																																												

H ₂ O. (%)																																		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35

pilot tube no leaks
ORSAT no leaks

PT-278
DI-125
OP-998
IT-447

TRAVERSE POINT NUMBER			CLOCK TIME (24 hr CLOCK)		GAS METER READING (V _m), ft ³		VELOCITY HEAD (Δp _v), in. H ₂ O		ORIFICE PRESSURE DIFFERENTIAL (ΔH), in. H ₂ O		STACK TEMPERATURE (T _s), °F		DRY GAS METER TEMPERATURE		PUMP VACUUM, in. Hg		SAMPLE BOX TEMPERATURE °F		IMPINGER TEMPERATURE °F																																																													
SAMPLING TIME, min			0		1050		758.131		DESTROYED		ACTUAL		INLET (T _{in}), °F		OUTLET (T _{out}), °F		F		P																																																													
7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57																														
10.	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57																																	
20.	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
30.	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100										
40.	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100																				
50.	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100																														
60.	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100																																								
70.	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100																																																		
80.	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100																																																												
90.	91	92	93	94	95	96	97	98	99	100																																																																						

PLANT & CITY																																DATE		SAMPLING LOCATION																																SAMPLE TYPE															
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80		
																																2/11/83		UNIT 3 EAST																																MSB															

RUN NO.	OPERATOR	AIR TEMP. (°F)	BAR. PRESS. (IN. Hg.)	STATIC PRESS. (IN. H ₂ O)	FILTER NUMBER(S)	STACK INSIDE DIMEN. (INCHES)	PITOT TUBE Cp	THERM. NO.	PAGE
0 1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75									
6855A	PR RA J.P.	160	31.0 ± .10	± .25	3 F-3110 b7	16.2	.94	178	V.O.F. 1

[illegible]

IT-449

[illegible]

6c

RUN NO.				OPERATOR																AMB. TEMP. (°F)		BAR. PRESS. (IN. Hg)		STATIC PRESS. (IN. H ₂ O)		FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)				PITOT TUBE C _p		THERM. NO.		PAGE																													
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
SG-MES				CLARK																60		30.0		+0.25		5135V102																167						89172		10 F																													

PROBE LENGTH AND TYPE																		NOZZLE		H ₂ O (#)	SAMPLE BOX NO	METER BOX NO	METER Δ H O	METER CAL. FACTOR V	LEAK CHECK		K FACTOR	C FACTOR	PROBE HEAT SET	BOX HEAT SET	REF. Δ P	RECORD DATA RHS																																																										
																		I.D.	NO.						IN. No	CFM																																																																
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80												
1	6	157	GLASS															211										11A	QIA	FIB	184						2983									60	004								9374									824	324																	10								

Protest @ 15' 01K

[illegible]

FLTR
322

43.761

77

5.35

6-D

PROBE LENGTH AND TYPE																			NOZZLE		H.O. (%)	SAMPLE BOX NO	METER BOX NO	METER Δ H O	METER CAL. FACTOR V	LEAK CHECK		K FACTOR	C FACTOR	PROBE HEAT SET	BOX HEAT SET	REF. Δ P	RECORD DATA MINS																																																								
																			I.D.	NO.						IN. HG	CFM																																																														
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90
5 FT GLASS																			219		11	34	35	100	1030	30 0.15		9.379		320	329		10																																																								

Photo 16 "OK"

[illegible]

531

Plant _____ Sample date 2/11/83
Sample location Bayer No. 2 Recovery date 2/11/83
Run number CAMSB Recovered by DO/S
Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
Particulate filter number 3531061 ✓
Particulate filter sample I.D. 4380 B ✓
Probe rinse Acetone I.D. 4380 A ✓
Purge train 20 min (check when completed) ☒
Location of filter in back half bet. dry. 2+3

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>584.8</u> g	<u>636.9</u> g	<u>645.2</u> g	<u>615.9</u> g	<u>922.3</u> g
Initial wt	<u>497.8</u> g	<u>674.8</u> g	<u>615.1</u> g	<u>598.2</u> g	<u>881.6</u> g
Net wt	<u>87.0</u> g	<u>-37.9</u> g	<u>30.1</u> g	<u>17.7</u> g	<u>40.7</u> g
		Total moisture	<u>137.6</u> g		<u>45</u> % spent

PROBE RINSE CONTAINER I.D.	<u>4380 A ✓</u>	
IPA IMP. CONTAINER I.D.	<u>4381 A ✓</u>	LIQUID LEVEL MARKED <u>✓</u>
H ₂ O ₂ IMP. CONTAINER I.D.	<u>4382 A ✓</u>	LIQUID LEVEL MARKED <u>✓</u>
BLANK CONTAINER(S) I.D.		LIQUID LEVEL MARKED
IPA	<u>4377 A ✓</u>	<u>✓</u>
H ₂ O ₂	<u>4378 A ✓</u>	<u>✓</u>
H ₂ O	<u>4379 A ✓</u>	<u>✓</u>
Acetone	<u>4376 A ✓</u>	<u>✓</u>

Samples stored and locked _____
Remarks Filter - green coat, medium

Received by Sam White Date 15 Feb 1983
Remarks Reg # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Bay #2 Recovery date 2/11/83
 Run number 6BM5B Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531062 ✓
 Particulate filter sample I.D. 4384 B ✓
 Probe rinse Acetone I.D. 4384 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>580.7</u> g	<u>631.9</u> g	<u>627.8</u> g	<u>635.5</u> g	<u>865.4</u> g
Initial wt	<u>492.6</u> g	<u>669.1</u> g	<u>594.4</u> g	<u>618.6</u> g	<u>830.3</u> g
Net wt	<u>88.1</u> g	<u>-37.2</u> g	<u>33.4</u> g	<u>16.9</u> g	<u>35.1</u> g
Total moisture	<u>136.3</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4384 A ✓
 IPA IMP. CONTAINER I.D. 4385 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4386 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377 A ✓
 H₂O₂ 4378 A ✓
 H₂O 4379 A ✓
 Acetone 4376 A ✓

Samples stored and locked _____
 Remarks Filter - green coat, medium

LABORATORY CUSTODY

Received by Thomas White Date 15 Feb 1983
 Remarks bag #4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Bayer #2 Recovery date 2/11/83
 Run number 6C M5B Recovered by DB/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 353110P
 Particulate filter sample I.D. 4387 B ✓
 Probe rinse Acetone I.D. 4387 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>576.5</u> g	<u>631.0</u> g	<u>619.5</u> g	<u>621.8</u> g	<u>827.5</u> g
Initial wt	<u>498.5</u> g	<u>660.7</u> g	<u>592.6</u> g	<u>606.3</u> g	<u>800.5</u> g
Net wt	<u>78.0</u> g	<u>-29.7</u> g	<u>26.9</u> g	<u>15.5</u> g	<u>27.0</u> g
Total moisture	<u>112.7</u> g				<u>20</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4387 A ✓
 IPA IMP. CONTAINER I.D. 4388 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4389 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377 A ✓
 H₂O₂ 4378 A ✓
 H₂O 4379 A ✓
 Acetone 4376 A ✓

Samples stored and locked _____
 Remarks Filter-green coat, medium

LABORATORY CUSTODY

Received by Louis White Date 15 Feb 1983
 Remarks Reg # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Boyer #7 Recovery date 2/11/83
 Run number 6DM5B Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531096 ☒
 Particulate filter sample I.D. 4390 B ☒
 Probe rinse Acetone I.D. 4390 A ☒
 Purge train 20 min (check when completed) _____
 Location of filter in back half bet. Imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>543.8</u> g	<u>628.6</u> g	<u>581.2</u> g	<u>623.6</u> g	<u>852.3</u> g
Initial wt	<u>468.8</u> g	<u>663.5</u> g	<u>553.1</u> g	<u>607.4</u> g	<u>820.5</u> g
Net wt	<u>75.0</u> g	<u>-34.9</u> g	<u>28.1</u> g	<u>16.2</u> g	<u>31.8</u> g
Total moisture	<u>116.2</u> g				<u>35</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4390 A ☒
 IPA IMP. CONTAINER I.D. 4391 A ☒ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4392 A ☒ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377 A ☒
 H₂O₂ 4378 A ☒
 H₂O 4379 A ☒
 Acetone 4376 A ☒

Samples stored and locked _____
 Remarks Filter - green coat, medium
- Filter holder broken before recovery - no loss resulting

LABORATORY CUSTODY

Received by James White Date 15 Feb-1983
 Remarks Reg. # 4061



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2-11-83 TEST NO 06
SAMPLING TIME (24-hr CLOCK) 1230
SAMPLING LOCATION Bailer #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSAT
AMBIENT TEMPERATURE 70
OPERATOR DF
ORSAT LEAK CHECKED ✓

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M_d , lb lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.6	13.6	13.6	13.6			13.6	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	16.1	2.5	16.1	2.5			2.5	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

7-A

PT 379
DI 125
IT 449

PT 379
DI 125
IT 449

PT 379
DI 125
IT 449

[illegible]

PLANT & CITY																																	DATE		SAMPLING LOCATION																												SAMPLE TYPE																
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																	2/11/83		MAYITI REASIT																												MAYITI																

7-B

RUN NO.					OPERATOR																				AMB. TEMP. (°F)		BAR. PRESS. (IN. HG)		STATIC PRESS. (IN. H ₂ O)		FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)				PITOT TUBE C _D		THERM NO.		PAGE																			
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75
70450					P.B. R.A. V.A.																				65		30.11		7.20		315310073																142				28.4		2.96		10 F 1																			

PT-379

DI-125

IT-447

OP - 999

PROBE LENGTH AND TYPE																			NOZZLE,		H ₂ O, (#)	SAMPLE BOX NO	METER BOX NO.	METER A H O	METER CAL. FACTOR V	LEAK CHECK		K FACTOR	C FACTOR	PROBE HEAT SET	BOX HEAT SET	REF. ΔP	RECORD DATA MINS																																														
																			I.D.	NO.						IN. HG	CFM																																																				
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
No RTI GAS																			9236		14P	146	1519	92619	850	0.115	1.592			329	3219																																																

pitot tube no leaks
or sat no leaks

[illegible]

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Bailer No. 20 Recovery date 2/11/83
 Run number 7A MSBW Recovered by DO/DS
 Particulate sample type _____ M5 _____ M5-320 _____ M5-450 ☒ M5W 320
 Particulate filter number 353/125 ✓
 Particulate filter sample I.D. 4394 B ✓
 Probe rinse H₂O I.D. 4394A
 Purge train 20 min (check when completed) _____
 Location of filter in back half between 2nd + 3rd Imps

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>588.3</u> g	<u>641.6</u> g	<u>626.5</u> g	<u>608.9</u> g	<u>808.2</u> g
Initial wt	<u>505.0</u> g	<u>673.9</u> g	<u>597.2</u> g	<u>592.2</u> g	<u>770.3</u> g
Net wt	<u>83.3</u> g	<u>-32.3</u> g	<u>29.3</u> g	<u>16.7</u> g	<u>32.9</u> g
Total moisture	<u>134.9</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4394 A ✓
 IPA IMP. CONTAINER I.D. 4395 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4396 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377 A ✓
 H₂O₂ 4378 A ✓
 H₂O 4379 A ✓
 Acetone 4376 A ~A ✓

Samples stored and locked _____

Remarks Filter - green/grey coat, medium

LABORATORY CUSTODY

Received by Thomas White Date 15 Feb 1983

Remarks Fig # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Boiler No. 2^U Recovery date 2/11/83
 Run number 7 B MSB Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531072 ✓
 Particulate filter sample I.D. 4397 B ✓
 Probe rinse Acetone I.D. 4397 A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half Between 2nd + 3rd stages

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>585.2</u> g	<u>681.7</u> g	<u>648.8</u> g	<u>612.8</u> g	<u>156.8</u> g
Initial wt	<u>507.2</u> g	<u>669.4</u> g	<u>615.8</u> g	<u>595.4</u> g	<u>816.8</u> g
Net wt	<u>78.0</u> g	<u>-37.7</u> g	<u>33.0</u> g	<u>17.4</u> g	<u>40.0</u> g
Total moisture	<u>130.7</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4397 A ✓
 IPA IMP. CONTAINER I.D. 4398 A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4399 A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377 A ✓ ☒
 H₂O₂ 4378 A ✓ ☒
 H₂O 4379 A ✓ ☒
 Acetone 4376 A ✓ ☒

Samples stored and locked _____

Remarks Filter - green/gray coat, medium

LABORATORY CUSTODY

Received by Lonic White Date 15 Feb 1983
 Remarks Ref # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Boiler #2 Recovery date 2/11/83
 Run number 71 M5 BW Recovered by DO/DS
 Particulate sample type _____ M5 _____ M5-320 _____ M5-450 ☒ M5W-320
 Particulate filter number 3531132 ✓
 Particulate filter sample I.D. 4400B ✓
 Probe rinse H₂O I.D. 4400A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half Between 2nd + 3rd Imp's

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>566.7</u> g	<u>635.2</u> g	<u>573.6</u> g	<u>626.4</u> g	<u>886.8</u> g
Initial wt	<u>483.6</u> g	<u>666.4</u> g	<u>542.9</u> g	<u>609.4</u> g	<u>857.5</u> g
Net wt	<u>83.1</u> g	<u>-31.2</u> g	<u>30.7</u> g	<u>17.0</u> g	<u>29.3</u> g
Total moisture	<u>129.9</u> g				<u>30</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4400A ✓
 IPA IMP. CONTAINER I.D. 4401A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4402A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓ ☒
 H₂O₂ 4378A ✓ ☒
 H₂O 4379A ✓ ☒
 Acetone 4376A n/a ☒

Samples stored and locked _____

Remarks Finer - gray/green coat, medium

LABORATORY CUSTODY

Received by _____

Date _____

Remarks reg # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Boiler No 2 Recovery date 2/11/83
 Run number 7 DMS B Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 353/121 ✓
 Particulate filter sample I.D. 4403B ✓
 Probe rinse Acetone I.D. 4403B ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half between 2nd + 3rd Tap's.

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>581.4</u> g	<u>637.5</u> g	<u>632.5</u> g	<u>614.0</u> g	<u>844.3</u> g
Initial wt	<u>497.8</u> g	<u>620.1</u> g	<u>601.5</u> g	<u>597.8</u> g	<u>814.0</u> g
Net wt	<u>83.6</u> g	<u>-82.6</u> g	<u>31.0</u> g	<u>16.2</u> g	<u>30.3</u> g
Total moisture	<u>128.5</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4403A ✓
 IPA IMP. CONTAINER I.D. 4404A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4405A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓ ☒
 H₂O₂ 4378A ✓ ☒
 H₂O 4379A ✓ ☒
 Acetone 4376A ✓ ☒

Samples stored and locked _____
 Remarks Filter - green coat, medium

LABORATORY CUSTODY

Received by Lana White Date 15 Feb 1983
 Remarks rec # 4061



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2. 11. 83 TEST NO. 70
SAMPLING TIME (24-hr CLOCK) 1505
SAMPLING LOCATION Boiler #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSAT
AMBIENT TEMPERATURE 70
OPERATOR D. Schiffel
ORSAT LEAK CHECKED ✓

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.4	13.4	13.4	13.4			13.4	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	16.0	2.6	16.0	2.6			2.6	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

PLANT & CITY																																	DATE			SAMPLING LOCATION																								SAMPLE TYPE																			
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																	2/11/83			PLANT 13 KASIT																								MISB																			

RUN NO.				OPERATOR																AMB. TEMP. (°F)		BAR. PRESS. (IN. HG)		STATIC PRESS. (IN. H ₂ O)		FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)								PITOT TUBE CP		THERM NO.		PAGE																									
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
84153				PR RO JP																70		30.9		F.92																		162								086		200		10 F																									

[illegible]

PT-228
DJ-125
IT 447

pitot tubes no leaks
oxygen no leaks

[illegible]

B-C

RUN NO.		OPERATOR																								AMB TEMP (°F)		BAR. PRESS. (IN. Hg)		STATIC PRESS (IN. H ₂ O)		FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)				PIVOT TUBE C _D		THEORY NO.		PAGE																		
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75
EC-1518					G4A444																								72.3		29.8		0.0		162																162				162		162		162															

PROBE LENGTH AND TYPE																			NOZZLE		H ₂ O		SAMPLE		METER		METER		METER CAL.		LEAK CHECK		K FACTOR		C FACTOR		PROBE HEAT SET		BOB HEAT SET		REF. AD		RECORD DATA																																				
																			I.D.		NO.		PSI		BOX NO.		BOX NO.		Δ H D		FACTOR V		IN. HG		CFM																																												
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
K5 FTI GLASS																			SPSI				114		OAK FRS		1.84		0.9183		15.0		201		44.736				520		529				10																																		

Printed @ 15" O/K

- * Probe heat off for new summer bread.

8-D

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QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Ba Ter No. 2nd Recovery date 2/12/83
 Run number FAMSB Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531122 ✓
 Particulate filter sample I.D. 4406B ✓
 Probe rinse Acetone I.D. 4406A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2 + 3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>538.2</u> g	<u>647.9</u> g	<u>629.5</u> g	<u>617.3</u> g	<u>831.8</u> g
Initial wt	<u>495.2</u> g	<u>672.7</u> g	<u>605.3</u> g	<u>603.3</u> g	<u>806.6</u> g
Net wt	<u>43.0</u> g	<u>-24.8</u> g	<u>24.2</u> g	<u>14.0</u> g	<u>25.2</u> g
Total moisture	<u>81.6</u> g				<u>30</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4406A ✓
 IPA IMP. CONTAINER I.D. 4407A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4408A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓
 H₂O₂ 4378A ✓
 H₂O 4379A ✓
 Acetone 4376A ✓

Samples stored and locked _____

Remarks Filter - 1/2 gray, medium / 1/2 green, light.

LABORATORY CUSTODY

Received by Lorrie White Date 15 Feb. 1983
 Remarks log # 4001

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/11/83
 Sample location Boyer No. 2 Recovery date 2/12/83
 Run number PBM5BP400 Recovered by JO/DS
 Particulate sample type _____ M5 / M5-320-~~700~~ M5-450 _____ M5W
 Particulate filter number 3831121 ✓
 Particulate filter sample I.D. 4409B ✓
 Probe rinse Acetone I.D. 4409A ✓
 Purge train 20 min (check when completed) /
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>531.9</u> g	<u>642.0</u> g	<u>618.8</u> g	<u>634.2</u> g	<u>893.0</u> g
Initial wt	<u>491.0</u> g	<u>671.3</u> g	<u>590.2</u> g	<u>620.9</u> g	<u>867.0</u> g
Net wt	<u>40.9</u> g	<u>-29.3</u> g	<u>28.6</u> g	<u>13.3</u> g	<u>26.0</u> g
Total moisture	<u>79.5</u> g				<u>55</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4409A ✓
 IPA IMP. CONTAINER I.D. 4410A ✓ LIQUID LEVEL MARKED /
 H₂O₂ IMP. CONTAINER I.D. 4411A ✓ LIQUID LEVEL MARKED /
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓
 H₂O₂ 4378A ✓
 H₂O 4379A ✓
 Acetone 4376A ✓

Samples stored and locked _____
 Remarks Filter - green coat, medium

LABORATORY CUSTODY

Received by Shirley White Date 15 Feb. 1983
 Remarks pg. #406

Plant _____ Sample date 2/11/83
Sample location Bay Area No. 2 Recovery date 2/12/83
Run number ACMSB Recovered by DO/DS
Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
Particulate filter number 353/120 ✓
Particulate filter sample I.D. 44/2B ✓
Probe rinse Acidine I.D. 44/2A ✓
Purge train 20 min (check when completed) ☒
Location of filter in back half bet. Imp. 2+3

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>539.5</u> g	<u>632.1</u> g	<u>613.4</u> g	<u>631.3</u> g	<u>790.9</u> g
Initial wt	<u>498.6</u> g	<u>660.6</u> g	<u>586.2</u> g	<u>615.1</u> g	<u>768.1</u> g
Net wt	<u>40.9</u> g	<u>-28.5</u> g	<u>27.2</u> g	<u>16.2</u> g	<u>22.8</u> g
		Total moisture	<u>83.6</u> g		65 % spent

PROBE RINSE CONTAINER I.D.	<u>4412A</u> ✓	
IPA IMP. CONTAINER I.D.	<u>4413A</u> ✓	LIQUID LEVEL MARKED ✓
H ₂ O ₂ IMP. CONTAINER I.D.	<u>4414A</u> ✓	LIQUID LEVEL MARKED ✓
BLANK CONTAINER(S) I.D.		LIQUID LEVEL MARKED
IPA	<u>4377A</u> ✓	✓
H ₂ O ₂	<u>4378A</u> ✓	✓
H ₂ O	<u>4379A</u> ✓	✓
Acetone	<u>4376A</u> ✓	✓

Remarks Filler - green coat, medium

Received by Glenn White Date 15 Feb. 1983
Remarks ply #4001

Plant _____ Sample date 2/11/83
Sample location Bayer No. 2 Recovery date 2/12/83
Run number 8DM5BP400 Recovered by DO/DS
Particulate sample type _____ M5 ☒ M5-320 P400 M5-450 _____ M5W
Particulate filter number 3531107 ✓
Particulate filter sample I.D. 4415B ✓
Probe rinse Acetone I.D. 4415A ✓
Purge train 20 min (check when completed) _____
Location of filter in back half bet. imp 2+3

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>504.1</u> g	<u>630.2</u> g	<u>571.2</u> g	<u>633.0</u> g	<u>835.8</u> g
Initial wt	<u>467.1</u> g	<u>663.5</u> g	<u>544.3</u> g	<u>617.5</u> g	<u>808.6</u> g
Net wt	<u>37.0</u> g	<u>323.3</u> g	<u>226.9</u> g	<u>15.5</u> g	<u>27.2</u> g
	Total moisture			<u>73.3</u> g	<u>75</u> % spent

PROBE RINSE CONTAINER I.D.	<u>4415A</u> ✓	
IPA IMP. CONTAINER I.D.	<u>4416A</u> ✓	LIQUID LEVEL MARKED ✓
H ₂ O ₂ IMP. CONTAINER I.D.	<u>4417A</u> ✓	LIQUID LEVEL MARKED ✓
BLANK CONTAINER(S) I.D.		LIQUID LEVEL MARKED
IPA	<u>4377A</u> ✓	<u> </u> ✓
H ₂ O ₂	<u>4378A</u> ✓	<u> </u> ✓
H ₂ O	<u>4379A</u> ✓	<u> </u> ✓
Acetone	<u>4376A</u> ✓	<u> </u> ✓

Filter - green coat, medium

15 Feb. 1983

reg # 406'



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2.11.83 TEST NO 8
SAMPLING TIME (24-hr CLOCK) 1725
SAMPLING LOCATION BD:TER #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSAT
AMBIENT TEMPERATURE 70
OPERATOR D. Schipper
ORSAT LEAK CHECKED ✓

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb/lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.3	13.3	13.3	13.3			13.3	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	16.0	2.7	16.0	2.7			2.7	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

PLANT & CITY																																	DATE		SAMPLING LOCATION																				SAMPLE TYPE																								
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
																																	12/12/83		KIMITE 12 EAST																				MSIB																								

RUN NO.		OPERATOR																												AMB TEMP (°F)	BAR. PRESS. (IN. Hg)	STATIC PRESS. (IN. H ₂ O)	FILTER NUMBER(S)																STACK INSIDE DIMEN. (INCHES)								PITOT TUBE Cp	THERM NO.	PAGE																				
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
94M5B1		P4 RA JP																												60	30.27	14.0	3531109																163									284208	40 F																				

PROBE LENGTH AND TYPE																			NOZZLE		H ₂ O (#)	SAMPLE BOX NO	METER BOX NO.	METER Δ H Ø	METER CAL. FACTOR V	LEAK CHECK		K FACTOR	C FACTOR	PROBE HEAT SET	BOX HEAT SET	REF. Δ P	RECORD DATA MINS																																														
																			I.D.	NO.						IN. HG	CFM																																																				
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80
5.5 FT. BL455																			9223		1110		1584	172	1.993	9000.02		11/12166	A 1	324	324	A 1	19																																														

PT-379
DI-125
OP-999
IT-447

plot no leaks
ursat no leaks

[illegible]

A 837 1012 2A+2 781.2 ~~4210~~ 531.6

9-c

P. 64
379

P. 64
379

Protecte 15"

48.059

531.6

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/12/83
 Sample location Bayer No. 2 Recovery date 2/12/83
 Run number 9A MSB Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531/06 ✓
 Particulate filter sample I.D. 4418B ✓
 Probe rinse Acetone I.D. 4418A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>594.9</u> g	<u>638.1</u> g	<u>610.5</u> g	<u>619.5</u> g	<u>856.0</u> g
Initial wt	<u>505.3</u> g	<u>675.0</u> g	<u>585.6</u> g	<u>600.8</u> g	<u>807.5</u> g
Net wt	<u>89.5</u> g	<u>-36.9</u> g	<u>24.9</u> g	<u>18.7</u> g	<u>43.5</u> g
Total moisture	<u>139.7</u> g				<u>50</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4418A ✓
 IPA IMP. CONTAINER I.D. 4419A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4420A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓
 H₂O₂ 4378A ✓
 H₂O 4379A ✓
 Acetone 4376A ✓

Samples stored and locked _____
 Remarks Filter - green coat, medium (dark)

Received by Donna White LABORATORY CUSTODY Date 15 Feb. 1983
 Remarks leg # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/12/83
 Sample location Bay No. 2 Recovery date 2/12/83
 Run number 9BM5B Recovered by DO/DS
 Particulate sample type M5 ☒ M5-320 M5-450 M5W
 Particulate filter number 3531/05 ☒
 Particulate filter sample I.D. 4421 B ☒
 Probe rinse Acetone I.D. 4421 A ☒
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2 & 3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>595.1</u> g	<u>631.8</u> g	<u>643.9</u> g	<u>614.7</u> g	<u>924.9</u> g
Initial wt	<u>507.1</u> g	<u>669.5</u> g	<u>612.0</u> g	<u>596.7</u> g	<u>789.7</u> g
Net wt	<u>88.0</u> g	<u>-37.7</u> g	<u>31.9</u> g	<u>18.0</u> g	<u>35.2</u> g
Total moisture	<u>135.4</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4421 A ☒
 IPA IMP. CONTAINER I.D. 4422 A LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4423 A LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377 A ☒
 H₂O₂ 4378 A ☒
 H₂O 4379 A ☒
 Acetone 4376 A ☒

Samples stored and locked _____
 Remarks Filder - green coat (f), medium

LABORATORY CUSTODY

Received by Monica White Date 15 Feb 1983
 Remarks leg. #4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/12/83
 Sample location Bayer No. 2 Recovery date 2/12/83
 Run number 9CMSB Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531104 ✓
 Particulate filter sample I.D. 4424B ✓
 Probe rinse Acetone I.D. 4424A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>571.3</u> g	<u>622.6</u> g	<u>574.0</u> g	<u>628.7</u> g	<u>165.6</u> g
Initial wt	<u>484.6</u> g	<u>666.8</u> g	<u>542.1</u> g	<u>610.7</u> g	<u>129.9</u> g
Net wt	<u>86.7</u> g	<u>-39.2</u> g	<u>31.9</u> g	<u>18.0</u> g	<u>35.7</u> g
Total moisture	<u>132.1</u> g				<u>35</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4424A ✓
 IPA IMP. CONTAINER I.D. 4425A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4426A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓ ☒
 H₂O₂ 4378A ✓ ☒
 H₂O 4379A ✓ ☒
 Acetone 4376A ✓ ☒

Samples stored and locked _____
 Remarks Filter - green coat, medium

LABORATORY CUSTODY

Received by Louis White Date 15 Feb. 1983
 Remarks accy - # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/12/83
 Sample location Bayer No. 2 Recovery date 2/12/83
 Run number 9DMSB Recovered by DO/S
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 3531103 ✓
 Particulate filter sample I.D. 4427B ✓
 Probe rinse Acetone I.D. 4427A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>583.9</u> g	<u>630.3</u> g	<u>619.5</u> g	<u>629.1</u> g	<u>832.9</u> g
Initial wt	<u>498.5</u> g	<u>670.9</u> g	<u>588.8</u> g	<u>608.8</u> g	<u>800.2</u> g
Net wt	<u>85.4</u> g	<u>-40.6</u> g	<u>30.7</u> g	<u>20.3</u> g	<u>32.7</u> g
Total moisture	<u>133.5</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4427A ✓
 IPA IMP. CONTAINER I.D. 4428A LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4429A LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓
 H₂O₂ 4378A ✓
 H₂O 4379A ✓
 Acetone 4376A ✓

Samples stored and locked _____
 Remarks Filter - green coat, medium, some black around edges

LABORATORY CUSTODY

Received by Shonda White Date 15 Feb 1983
 Remarks Reg #4061



COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.6	13.6	13.6	13.6			13.6	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	16.1	2.5	16.1	2.5			2.5	32/100	
CO(NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
								TOTAL	

B-84

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/12/83
 Sample location Boyer #02 Recovery date 2/12/83
 Run number 10A M5B Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320 _____ M5-450 _____ M5W
 Particulate filter number 353102F
 Particulate filter sample I.D. 4431B
 Probe rinse Acetone I.D. 4431A
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>594.1</u> g	<u>644.6</u> g	<u>644.8</u> g	<u>617.2</u> g	<u>853.9</u> g
Initial wt	<u>497.6</u> g	<u>677.0</u> g	<u>613.2</u> g	<u>598.0</u> g	<u>813.9</u> g
Net wt	<u>?</u> g	<u>-32.4</u> g	<u>31.6</u> g	<u>?</u> g	<u>?</u> g
Total moisture	<u>15.5</u> g				<u>40</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4431A
 IPA IMP. CONTAINER I.D. 4432A LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4433A LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ☒
 H₂O₂ 4378A ☒
 H₂O 4379A ☒
 Acetone 4376A ☒

Samples stored and locked _____
 Remarks Filter - gray/green, medium

LABORATORY CUSTODY

Received by Lorrie White Date 15 Feb 1983
 Remarks key # 4001 acetone probe used # 4431A sealed & transferred

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 2/12/83
 Sample location Boyer #2 Recovery date 2/12/83
 Run number 10BMSBP400 Recovered by JA/PS
 Particulate sample type _____ M5 ☒ M5-320 7400 M5-450 _____ M5W _____
 Particulate filter number 3531027 ✓
 Particulate filter sample I.D. 4434B ✓
 Probe rinse Acetone I.D. 4434A ✓
 Purge train 20 min (check when completed) ☒
 Location of filter in back half bet. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>587.5</u> g	<u>634.2</u> g	<u>623.9</u> g	<u>642.6</u> g	<u>850.3</u> g
Initial wt	<u>492.7</u> g	<u>670.8</u> g	<u>590.5</u> g	<u>624.1</u> g	<u>814.8</u> g
Net wt	<u>94.8</u> g	<u>-36.6</u> g	<u>33.4</u> g	<u>118.5</u> g	<u>35.5</u> g
Total moisture	<u>12.1</u> g				<u>35</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4434A ✓
 IPA IMP. CONTAINER I.D. 4435A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4436A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓
 H₂O₂ 4378A ✓
 H₂O 4379A ✓
 Acetone 4376A ✓

Samples stored and locked _____

Remarks Filter - green w/ black around edges, medium

LABORATORY CUSTODY

Received by Louise D'Amico Date 15 Feb 1983

Remarks reg. # 4061

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant Sample date 2/12/83
 Sample location Boiler #2 Recovery date 2/12/83
 Run number 10 C M5B Recovered by DA/DS
 Particulate sample type M5 ✓ M5-320 M5-450 M5W
 Particulate filter number 35310F9
 Particulate filter sample I.D. 4437B
 Probe rinse Acetone I.D. 4437A
 Purge train 20 min (check when completed) ✓
 Location of filter in back half bot. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>589.8</u> g	<u>629.5</u> g	<u>624.9</u> g	<u>628.9</u> g	<u>849.9</u> g
Initial wt	<u>501.3</u> g	<u>662.2</u> g	<u>591.1</u> g	<u>610.4</u> g	<u>820.6</u> g
Net wt	<u>88.5</u> g	<u>67.3</u> g	<u>33.8</u> g	<u>118.5</u> g	<u>29.3</u> g
Total moisture	<u> </u> g				<u>30</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4437A ✓
 IPA IMP. CONTAINER I.D. 4437A ✓ LIQUID LEVEL MARKED ✓
 H₂O₂ IMP. CONTAINER I.D. 4437A ✓ LIQUID LEVEL MARKED ✓
 BLANK CONTAINER(S) I.D. LIQUID LEVEL MARKED

IPA	<u>4377A</u> ✓	<u> </u>
H ₂ O ₂	<u>4377A</u> ✓	<u> </u>
H ₂ O	<u>4377A</u> ✓	<u> </u>
Acetone	<u>4377A</u> ✓	<u> </u>

Samples stored and locked
 Remarks Killer green, medium w/ black edges

LABORATORY CUSTODY

Received by Alexis White Date 15 Feb 1983
 Remarks pg #4061 acetone probe rinse # 4437 located in
Inventory

QUAD TRAIN SAMPLE RECOVERY AND INTEGRITY SHEET

Plant _____ Sample date 1/12/83
 Sample location Boyer Pb 2 Recovery date 2/12/83
 Run number 10DH5BP400 Recovered by DO/DS
 Particulate sample type _____ M5 ☒ M5-320-P400 _____ M5-450 _____ M5W _____
 Particulate filter number 353108 ✓
 Particulate filter sample I.D. 4440B ✓
 Probe rinse Acetone I.D. 4440A ✓
 Purge train 20 min (check when completed) _____
 Location of filter in back half bot. imp. 2+3

MOISTURE

	1st impinger	2nd impinger	3rd impinger	4th impinger	Silica gel
Final wt	<u>555.3</u> g	<u>625.5</u> g	<u>559.7</u> g	<u>653.4</u> g	<u>876.8</u> g
Initial wt	<u>470.4</u> g	<u>663.4</u> g	<u>530.3</u> g	<u>629.8</u> g	<u>839.3</u> g
Net wt	<u>84.9</u> g	<u>62.1</u> g	<u>29.4</u> g	<u>223.6</u> g	<u>37.5</u> g
Total moisture	<u>127.5</u> g				<u>80</u> % spent

RECOVERED SAMPLE

PROBE RINSE CONTAINER I.D. 4440A ✓
 IPA IMP. CONTAINER I.D. 4441A ✓ LIQUID LEVEL MARKED ☒
 H₂O₂ IMP. CONTAINER I.D. 4442A ✓ LIQUID LEVEL MARKED ☒
 BLANK CONTAINER(S) I.D. _____ LIQUID LEVEL MARKED _____
 IPA 4377A ✓ ☒
 H₂O₂ 4378A ✓ ☒
 H₂O 4379A ✓ ☒
 Acetone 4376A ✓ ☒

Samples stored and locked _____
 Remarks Filter - green, medium, w/ black edges

LABORATORY CUSTODY

Received by Alma White Date 15 Feb 1983
 Remarks 100g # 4061



DRY MOLECULAR WEIGHT DETERMINATION

PLANT _____
DATE 2-12-83 TEST NO 10
SAMPLING TIME (24-hr CLOCK) 1330
SAMPLING LOCATION Boiler #2
SAMPLE TYPE (BAG, INTEGRATED, CONTINUOUS) BAG
ANALYTICAL METHOD ORSAT
AMBIENT TEMPERATURE 60
OPERATOR D. Schaffel
ORSAT LEAK CHECKED ✓

COMMENTS:

RUN GAS	1		2		3		AVERAGE NET VOLUME	MULTIPLIER	MOLECULAR WEIGHT OF STACK GAS (DRY BASIS) M _d , lb lb-mole
	ACTUAL READING	NET	ACTUAL READING	NET	ACTUAL READING	NET			
CO ₂	13.0	13.0	13.0	13.0			13.0	44/100	
O ₂ (NET IS ACTUAL O ₂ READING MINUS ACTUAL CO ₂ READING)	16.0	3.0	16.0	3.0			3.0	32/100	
CO (NET IS ACTUAL CO READING MINUS ACTUAL O ₂ READING)								28/100	
N ₂ (NET IS 100 MINUS ACTUAL CO READING)								28/100	
TOTAL									

APPENDIX C
LABORATORY RESULTS

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 1CM5B ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (ρ_a) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 542 ✓	1CM5B ✓	4319A ✓	385 ✓	104289.2 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓ ✓
Filter	CT 797 ✓	1CM5B ✓	4319B ✓	Filter # 3531015 ✓	331.0 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F, 6 hours cool, weigh	Number of treatments	Heat to 450°F, 6 hours cool, weigh	Number of treatments	Heat to 600°F, 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	11 ✓	1 ✓	0.2 ✓	1 ✓	-0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 542 ✓	1258 ✓	102.3 ✓	1 ✓	98.1 ✓	1 ✓	62.4 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	-0.3 ✓	1 ✓	-0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 797 ✓	2109 ✓	181.3 ✓	1 ✓	1680 ✓	2 ✓	132.4 ✓	3 ✓
Total particulate		336.7 ✓	283.6 ✓		266.1 ✓		194.8 ✓	

Remarks _____

T.J.N.

Data reviewed by Dea Bennett 4/21/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 1DM15B ✓
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (ρ_a) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank -	4301H -	368 ✓	998.1.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 843 ✓	1DM15B ✓	4322A ✓	355 ✓	102016.6 ✓
Filter blank	CT 831 ✓	Blank -	4316B ✓	F.Her * 3031063 -	335.6 -
Filter	CT 798 ✓	1DM15B ✓	4322B ✓	F.Her * 3031014 ✓	328.5 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	-0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 843 ✓	110.2 ✓	90.0 ✓	1 ✓	90.6 ✓	1 ✓	84.1 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	-0.3 ✓	1 ✓	-0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 798 ✓	199.1 ✓	170.6 ✓	1 ✓	160.4 ✓	2 ✓	142.0 ✓	3 ✓
Total particulate		309.3 ✓	265.6 ✓		251.0 ✓		226.1 ✓	

Remarks _____ T.J.R.

Data reviewed by John B. Smith 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 2 H115 B ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 844 ✓	2 H115 B ✓	4325A ✓	395 ✓	110012.0 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 799 ✓	2 H115 B ✓	4325B ✓	Filter # 3531013 ✓	330.8 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 24 hours cool, weigh	Number of treatments	Heat to 450°F 24 hours cool, weigh	Number of treatments	Heat to 600°F 24 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 844 ✓	161.0 ✓	141.3 ✓	2 ✓	136.4 ✓	2 ✓	41.2 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓						
Filter	CT 799 ✓	228.7 ✓	196.6 ✓	2 ✓	190.2 ✓	2 ✓	181.0 ✓	3 ✓
Total particulate		359.7 ✓	337.9 ✓		326.6 ✓		222.2 ✓	

Remarks _____

Data reviewed by John Bennett 4/2/83

T.J.M.

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 2B1115B ✓
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 845 ✓	2B115B ✓	4328A ✓	362 ✓	98640.0 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 800 ✓	2B115B ✓	4328B ✓	Filter # 3531071 ✓	327.9 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 24 hours cool, weigh ✓	Number of treatments	Heat to 450°F 24 hours cool, weigh ✓	Number of treatments	Heat to 600°F 24 hours cool, weigh ✓	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 845 ✓	124.9 ✓	103.6 ✓	2 ✓	91.5 ✓	2 ✓	28.4 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓						
Filter	CT 800 ✓	253.1 ✓	224.1 ✓	2 ✓	212.7 ✓	2 ✓	147.5 ✓	3 ✓
Total particulate		375.0 ✓	327.7 ✓		304.2 ✓		175.9 ✓	

Remarks _____ T.P.R.

Data reviewed by Deia Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 3H1115B
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 -	Blank -	4301H -	368 -	99881.3 -
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 846 ✓	3H115B ✓	4338H ✓	364 ✓	107426.3 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B -	F.H. # 3531063 ✓	335.6 ✓
Filter	CT 801 ✓	3H115B ✓	4338B ✓	F.H. # 3531010 ✓	330.4 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 -	0.6 /	1.1 -	1 /	0.2 /	1 /	-0.3 -	3 -
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 846 ✓	119.7 ✓	108.7 ✓	1 /	103.6 ✓	1 /	77.4 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 /	-0.3 -	1 -	-0.1 /	2 -	0.2 /	3 -
Filter	CT 801 ✓	237.2 ✓	202.4 ✓	1 -	194.6 ✓	2 ✓	173.7 ✓	3 ✓
Total particulate		356.9 /	311.1 /		298.2 ✓		251.1 ✓	

Remarks _____ T.J.R.

Data reviewed by Jane Bennett 4/21/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 3B1115 B ✓
Sample location Bowler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	9981.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 847 ✓	3B1115 B ✓	4341A ✓	385 ✓	98393.6 ✓
Filter blank	CT 831 ✓	Blank ✓	4316 B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 802 ✓	3B1115 B ✓	4341B ✓	Filter # 3531009 ✓	329.2 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	-0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 847 ✓	149.2 ✓	137.1 ✓	1 ✓	131.6 ✓	1 ✓	81.7 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	-0.3 ✓	1 ✓	-0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 802 ✓	227.4 ✓	195.3 ✓	1 ✓	185.5 ✓	2 ✓	160.0 ✓	3 ✓
Total particulate		376.6 ✓	332.4 ✓		317.1 ✓		241.7 ✓	

Remarks _____ T.J.N.
Data reviewed by John Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 3C115B P400 ✓
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301H ✓	308 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 848 ✓	3C115B P400 ✓	4344H ✓	405 ✓	104307.2 ✓
Filter blank	CT 831 ✓	Blank ✓	4376B ✓	F.Her* 3531063 ✓	335.6 ✓
Filter	CT 803 ✓	3C115B P410 ✓	4344B ✓	F.Her* 3531008 ✓	332.8 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	-0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 848 ✓	145.111 ✓	134.311 ✓	1 ✓	129.311 ✓	1 ✓	94.911 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	0.3 ✓	1 ✓	-0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 803 ✓	190.111 ✓	162.511 ✓	1 ✓	154.911 ✓	2 ✓	135.911 ✓	3 ✓
Total particulate		335.2 ✓	296.8 ✓		284.2 ✓		230.8 ✓	

Remarks _____ T.J.N.

Data reviewed by John Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 3DM15B-P400
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881	Blank	4301H	368	99881.3
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 849	3DM15B-P400	4347H	430	105588.7
Filter blank	CT 831	Blank	4316B	Filter* 3531007	335.6
Filter	CT 804	3DM15B-P400	4347B	Filter* 3531007	329.0

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881	0.6	1.1	1	0.2	1	-0.3	3
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 849	106.5	96.4	1	93.8	1	60.5	3
Filter blank	CT 831	0.2	-0.3	1	-0.1	2	0.2	3
Filter	CT 804	244.9	217.9	1	206.5	2	185.2	3
Total particulate		351.4	314.3		300.3		245.7	

Remarks _____ T.J.R.

Data reviewed by Jada Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 4H115B P-100
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 850 ✓	4H115B P400 ✓	4352A ✓	465 ✓	105368.4 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter * 3531063 ✓	335.6 ✓
Filter	CT 805 ✓	4H115B P400 ✓	4352B ✓	Filter * 3530158 ✓	359.5 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	0.3 ✓	2 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 850 ✓	173.6 ✓	165.7 ✓	1 ✓	162.7 ✓	1 ✓	117.3 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	0.3 ✓	1 ✓	0.1 ✓	2 ✓	0.2 ✓	2 ✓
Filter	CT 805 ✓	225.3 ✓	203.4 ✓	1 ✓	195.0 ✓	2 ✓	174.2 ✓	3 ✓
Total particulate		398.9 ✓	369.1 ✓		357.7 ✓		291.5 ✓	

Remarks _____ T.J.W.

Data reviewed by Dea Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 4-B1113B-P400
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 881 ✓	4-B1113B-P400 ✓	4355A ✓	352 ✓	116968.7 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3031003 ✓	335.6 ✓
Filter	CT 806 ✓	4-B1113B-P400 ✓	4355B ✓	Filter # 0002530 ✓	304.2 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 881 ✓	94.3 ✓	810 ✓	1 ✓	84.3 ✓	1 ✓	122 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	0.3 ✓	1 ✓	0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 806 ✓	303.7 ✓	215.6 ✓	1 ✓	215.6 ✓	2 ✓	214.6 ✓	3 ✓
Total particulate		398.0 ✓	362.6 ✓		349.9 ✓		276.8 ✓	

Remarks _____ T.J.H.

Data reviewed by Jela Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 40115 B
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 852 ✓	40115 B ✓	4358A ✓	368 ✓	107257.0 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter * 3531063 ✓	335.6 ✓
Filter	CT 801 ✓	40115 B ✓	4358B ✓	Filter * 3531066 ✓	3418 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	0.3 ✓	2 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 852 ✓	158.8 ✓	150.8 ✓	1 ✓	148.6 ✓	1 ✓	133.8 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	0.3 ✓	1 ✓	0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 801 ✓	189.8 ✓	169.0 ✓	1 ✓	162.0 ✓	2 ✓	116.2 ✓	3 ✓
Total particulate		348.6 ✓	319.8 ✓		310.6 ✓		250.0 ✓	

Remarks _____ T.J.N.

Data reviewed by John Bennett 4/31/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 4D115 B
 Sample location Baker No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881	Blank	4301H	368	99881.3
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 853	4D115B	4361H	274	106917.1
Filter blank	CT 831	Blank	4316 B	F. Her * 3531063	335.6
Filter	CT 808	4D115B	4361 B	F. Her * 3531068	328.2

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 1/2 hours cool, weigh	Number of treatments	Heat to 450°F 1/2 hours cool, weigh	Number of treatments	Heat to 600°F 1/2 hours cool, weigh	Number of treatments
Acetone blank	CT 881	0.6	1.1	1	0.2	1	-0.3	3
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 853	123.2	117.6	1	115.4	1	89.6	3
Filter blank	CT 831	0.2	0.3	1	-0.1	2	0.2	2
Filter	CT 808	222.8	199.9	1	190.8	2	145.0	3
Total particulate		346.0	317.5		306.2		234.6	

Remarks _____

Data reviewed by John Kennell 4/21/83

T.J.H.

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 5H115B ✓
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 854 ✓	5H115B ✓	4364A ✓	320 ✓	101482.4 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 809 ✓	5H115B ✓	4364B ✓	Filter # 3531067 ✓	339.2 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	-0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 854 ✓	75.6 ✓	64.0 ✓	1 ✓	56.4 ✓	1 ✓	39.3 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	-0.3 ✓	1 ✓	-0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 809 ✓	159.9 ✓	137.2 ✓	1 ✓	129.0 ✓	2 ✓	113.3 ✓	3 ✓
Total particulate		235.5 ✓	201.2 ✓		185.4 ✓		152.6 ✓	

Remarks 7.72Data reviewed by John Bennett 4/21/03

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 5B115B ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 855 ✓	5B115B ✓	4361A ✓	295 ✓	105728.4 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	F. Her # 3231063 ✓	335.6 ✓
Filter	CT 810 ✓	5B115B ✓	4367B ✓	F. Her # 3231018 ✓	338.4 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	0.1 ✓	1 ✓	0.2 ✓	1 ✓	-0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 855 ✓	71.1 ✓	58.3 ✓	1 ✓	53.6 ✓	1 ✓	32.4 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	0.3 ✓	1 ✓	0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 810 ✓	152.8 ✓	137.7 ✓	1 ✓	129.2 ✓	2 ✓	87.6 ✓	3 ✓
Total particulate		230.9 ✓	196.0 ✓		182.8 ✓		120.0 ✓	

Remarks _____ T2A.
Data reviewed by John Bennett 4/21/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 5C115B ✓
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (ρ_a) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99EB1.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 856 ✓	5C115B ✓	4370A ✓	340 ✓ ✓	104608.6 ✓ ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 811 ✓	5C115B ✓	4370B ✓	Filter # 3531124 ✓ ✓	329.6 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 2 1/2 hours cool, weigh	Number of treatments	Heat to 450°F 2 1/2 hours cool, weigh	Number of treatments	Heat to 600°F 2 1/2 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 856 ✓	63.8 ✓ ✓	52.9 ✓ ✓	2 ✓ ✓	47.5 ✓ ✓	2 ✓ ✓	25.1 ✓ ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓						
Filter	CT 811 ✓	155.4 ✓ ✓	133.2 ✓ ✓	2 ✓ ✓	131.0 ✓ ✓	2 ✓ ✓	78.6 ✓ ✓	3 ✓
Total particulate		219.2 ✓ ✓	186.1 ✓ ✓		178.5 ✓ ✓		103.7 ✓ ✓	

Remarks _____ T.J.W.

Data reviewed by Eda Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 5 DM5B ✓
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 857 ✓	5 DM5B ✓	4373A ✓	331 ✓ ✓	104102.9 ✓ ✓
Filter blank	CT 831 ✓	Blank ✓	4316 B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 812 ✓	5 DM5B ✓	4373 B ✓	Filter # 3531123 ✓	330.4 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 24 hours cool, weigh	Number of treatments	Heat to 450°F 24 hours cool, weigh	Number of treatments	Heat to 600°F 24 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 857 ✓	64.9 ✓	54.1 ✓	2 ✓	43.8 ✓	2 ✓	20.6 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓						
Filter	CT 812 ✓	153.0 ✓	132.4 ✓	2 ✓	129.9 ✓	2 ✓	92.7 ✓	3 ✓
Total particulate		217.9 ✓	183.5 ✓		173.7 ✓		113.3 ✓	

Remarks _____ T.G.N.

Data reviewed by Ella Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 6A1115B ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 858 ✓	6A1115B ✓	4380A ✓	24.2 ✓	104461.2 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 813 ✓	6A1115B ✓	4380B ✓	Filter # 3531061 ✓	329.6 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F hours cool, weigh	Number of treatments	Heat to 450°F 24 hours cool, weigh	Number of treatments	Heat to 600°F 24 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 858 ✓	69.4 ✓			41.9 ✓	2 ✓	20.3 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓						
Filter	CT 813 ✓	159.9 ✓			140.9 ✓	2 ✓	101.2 ✓	3 ✓
Total particulate		229.3 ✓			182.8 ✓		127.5 ✓	

Remarks _____ T.J.R.
Data reviewed by Jada Plummer 4/21/13

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 6B1115B ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301H ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 859 ✓	6B1115B ✓	4384H ✓	228 ✓ ✓	107409.6 ✓ ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 814 ✓	6B1115B ✓	4384B ✓	Filter # 3531062 ✓ ✓	339.1 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F - cool, weigh	Number of treatments	Heat to 450°F 24 hours cool, weigh	Number of treatments	Heat to 600°F 24 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 859 ✓	62.0 ✓			39.9 ✓	2 ✓ ✓	23.9 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓						
Filter	CT 814 ✓	149.8 ✓ ✓			128.4 ✓ ✓	2 ✓ ✓	77.3 ✓	3 ✓
Total particulate		216.8 ✓			168.3 ✓		101.2 ✓	

Remarks _____
Data reviewed by John Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 66115B
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 860 ✓	66115B ✓	4387A ✓	244 ✓ ✓	106081.5 ✓ ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 815 ✓	66115B ✓	4387B ✓	Filter # 3531108 ✓ ✓	313.3 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F hours cool, weigh	Number of treatments	Heat to 450°F 6 hours, cool, weigh	Number of treatments	Heat to 600°F 6 hours, cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓			0.2 ✓	1 ✓	-0.3 ✓	2 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 860 ✓	43.7 ✓ ✓			32.8 ✓ ✓	1 ✓ ✓	27.1 ✓ ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓			-0.1 ✓	2 ✓	0.2 ✓	2 ✓
Filter	CT 815 ✓	125.9 ✓ ✓			102.3 ✓ ✓	2 ✓ ✓	77.7 ✓ ✓	3 ✓
Total particulate		169.6 ✓ ✓			135.1 ✓ ✓		104.8 ✓ ✓	

Remarks _____ T.J.N.

Data reviewed by Ida Bennett 4/21/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 6.DMSB ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (ρa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881	Blank	4301A	368	99881.3
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 861 ✓	6.DMSB ✓	4390A ✓	255 ✓	103295.9 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 816 ✓	6.DMSB ✓	4390B ✓	Filter # 3531036 ✓	322.0 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881	0.6			0.2	1	-0.3	3
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 861 ✓	46.1 ✓			29.2 ✓	1 ✓	25.7 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓			-0.1 ✓	2 ✓	0.2 ✓	2 ✓
Filter	CT 816 ✓	140.0 ✓			115.9 ✓	2 ✓	87.3 ✓	3 ✓
Total particulate		186.1 ✓			145.1 ✓		113.0 ✓	

Remarks _____ T.J.R.

Data reviewed by John Bennett 4/21/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 7BM5B ✓
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881	Blank	4301A	368	99881.3
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 862	7BM5B	4397A	251	105067.3
Filter blank	CT 831	Blank	4316B	F. Her # 3531063	335.6
Filter	CT 817	7BM5B	4397B	F. Her # 3531072	333.2

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881	0.6			0.2	1	-0.3	2
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 862	82.7			31.6	1	21.1	3
Filter blank	CT 831	0.2			0.1	2	0.2	2
Filter	CT 817	139.2			120.5	2	80.5	3
Total particulate		221.9			152.1		101.6	

Remarks _____ T. J. R.
 Data reviewed by Mr. Bennett 4/21/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 7DM5B ✓
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 -	Blank -	4301A -	368 -	99881.3 -
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 863 ✓	7DM5B ✓	4403A ✓	285 ✓ ✓	104028.3 ✓ ✓
Filter blank	CT 831 ✓	Blank -	4316B -	Filter # 3531063 -	335.6 -
Filter	CT 818 ✓	7DM5B ✓	4403B ✓	Filter # 3531131 ✓ ✓	335.4 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours ✓ cool, weigh	Number of treatments
Acetone blank	CT 881 -	0.6 ✓			0.2 -	1 -	-0.3 -	3 -
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 863 ✓	74.6 ✓ ✓			33.6 ✓ ✓	1 ✓ ✓	18.9 ✓ ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓			-0.1 -	2 -	0.2 -	3 -
Filter	CT 818 ✓	140.9 ✓			119.4 ✓ ✓	2 ✓ ✓	74.6 ✓ ✓	3 ✓
Total particulate		215.5 ✓ ✓			153.0 ✓ ✓		93.5 ✓ ✓	

Remarks _____ 1.22Data reviewed by Jela Blum 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. SHMSB ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 864 ✓	SHMSB ✓	4406A ✓	310 ✓ ✓	102105.2 ✓ ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	F. Hc. # 3531063 ✓	335.6 ✓
Filter	CT 819 ✓	SHMSB ✓	4406B ✓	F. Hc. # 3531122 ✓ ✓	332.4 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 24 hours, cool, weigh	Number of treatments	Heat to 450°F 24 hours, cool, weigh	Number of treatments	Heat to 600°F 24 hours, cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 864 ✓	50.6 ✓	17.9 ✓	2 ✓	14.9 ✓	2 ✓	6.8 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓						
Filter	CT 819 ✓	106.2 ✓ ✓	87.7 ✓ ✓	2 ✓ ✓	85.3 ✓ ✓	2 ✓ ✓	44.7 ✓ ✓	3 ✓
Total particulate		156.8 ✓	105.6 ✓		100.2 ✓		51.5 ✓	

Remarks _____ T.J.N.

Data reviewed by John Kuntz 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. SBM5B P400
 Sample location Boiler No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 865 ✓	SBM5B-P400 ✓	4409A ✓	232 ✓	1043445 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 820 ✓	SBM5B P400 ✓	4409B ✓	Filter # 3531121 ✓	329.8 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	-0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 865 ✓	23.8 ✓	12.5 ✓	1 ✓	10.3 ✓	1 ✓	6.5 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	-0.3 ✓	1 ✓	-0.1 ✓	2 ✓	0.2 ✓	2 ✓
Filter	CT 820 ✓	87.7 ✓	75.4 ✓	1 ✓	69.0 ✓	2 ✓	52.6 ✓	3 ✓
Total particulate		111.5 ✓	87.9 ✓		79.3 ✓		59.1 ✓	

Remarks _____ T.J.R.

Data reviewed by Jean Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 8C115B ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (ρ_a) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881	Blank	4301A	308	99881.3
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 866 ✓	8C115B ✓	4412A ✓	252 ✓ ✓	110329.7 ✓ ✓
Filter blank	CT 831	Blank	4316B	Filter* 3531063	335.6
Filter	CT 821 ✓	8C115B ✓	4412B ✓	Filter* 3531120 ✓ ✓	333.7 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 24 hours cool, weigh	Number of treatments	Heat to 450°F 24 hours cool, weigh	Number of treatments	Heat to 600°F 24 hours cool, weigh	Number of treatments
Acetone blank	CT 881	0.6						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 866 ✓	20.6 ✓	12.3 ✓	2 ✓	9.4 ✓	2 ✓	5.2 ✓	3 ✓
Filter blank	CT 831 ✓	0.2						
Filter	CT 821 ✓	92.0 ✓	77.5 ✓	2 ✓	75.5 ✓	2 ✓	46.0 ✓	3
Total particulate		112.6	89.8		84.9		51.2	

Remarks _____ T.J.N.

Data reviewed by John Bennett 4/31/13

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. SDMSB P400 ✓
 Sample location Beller No. 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 867 ✓	SDMSB P400 ✓	4415A ✓	304 ✓ ✓	106748.4 ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	F.Her * 3531063 ✓	335.6 ✓
Filter	CT 822 ✓	SDMSB-P400 ✓	4415B ✓	F.Her * 3531107 ✓ ✓	331.6 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F 6 hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓	1.1 ✓	1 ✓	0.2 ✓	1 ✓	-0.3 ✓	2 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 867 ✓	21.6 ✓	10.5 ✓	1 ✓	8.6 ✓	1 ✓	5.8 ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓	-0.3 ✓	1 ✓	-0.1 ✓	2 ✓	0.2 ✓	3 ✓
Filter	CT 822 ✓	83.9 ✓	74.8 ✓	1 ✓	65.6 ✓	2 ✓	49.9 ✓	3 ✓
Total particulate		105.5 ✓	85.3 ✓		74.2 ✓		55.7 ✓	

Remarks _____ T.J.R.

Data reviewed by Jola Bennett 4/21/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 9AM5B ✓
 Sample location Boiler No 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 882 ✓	Blank ✓	4376A ✓	372 ✓	101576.8 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 868 ✓	9AM5B ✓	4418A ✓	265 ✓	106277.6 ✓
Filter blank	CT 832 ✓	Blank ✓	4393B ✓	Filter # 3531126 ✓	336.4 ✓
Filter	CT 823 ✓	9AM5B ✓	4418B ✓	Filter # 3531106 ✓	332.0 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F — hours — cool, weigh	Number of treatments	Heat to 450°F — hours — cool, weigh	Number of treatments	Heat to 600°F 24 hours — cool, weigh	Number of treatments
Acetone blank	CT 882 ✓	4.3 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 868 ✓	84.9 ✓					193 ✓	3 ✓
Filter blank	CT 832 ✓	0.3 ✓						
Filter	CT 823 ✓	108.0 ✓					98.2 ✓	3 ✓
Total particulate		252.9 ✓					117.5 ✓	

Remarks T.J.N.Data reviewed by Jana Bennett 4/21/13

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

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THERMOGRAVIMETRIC PARTICULATE ANALYSIS

PN 3530-15

Plant _____ Run No. 9B1115B ✓
 Sample location Boiler No 2 Analyst KRM
 Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 882	Blank ✓	4376A ✓	372 ✓	101576.8 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 869 ✓	9B1115B ✓	4421A ✓	284 ✓	104351.5 ✓
Filter blank	CT 832 ✓	Blank ✓	4393B ✓	Filter# 3531126 ✓	336.4 ✓
Filter	CT 824 ✓	9B1115B ✓	4421B ✓	Filter# 3531105 ✓	327.3 ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F — hours — cool, weigh	Number of treatments	Heat to 450°F — hours — cool, weigh	Number of treatments	Heat to 600°F 24 hours — cool, weigh	Number of treatments
Acetone blank	CT 882 ✓	4.3 ✓						
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 869 ✓	946 ✓					20.4 ✓	3 ✓
Filter blank	CT 832 ✓	0.3 ✓						
Filter	CT 824 ✓	166.6 ✓					96.3 ✓	3 ✓
Total particulate		261.2 ✓					116.7 ✓	

Remarks _____ T.J.R.
 Data reviewed by Ila Bennett 4/2/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 9C1115 B
Sample location Boiler No 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 882 ✓	Blank ✓	4376 A ✓	372 ✓	101576.8 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 870 ✓	9C1115 B ✓	4424 A ✓	338 ✓ ✓	107964.2 ✓ ✓
Filter blank	CT 832 ✓	Blank ✓	4393 B ✓	Filter # 3531126 ✓	336.4 ✓
Filter	CT 825 ✓	9C1115 B ✓	4424 B ✓	Filter # 3531104 ✓ ✓	327.6 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F — hours — cool, weigh	Number of treatments	Heat to 450°F — hours — cool, weigh	Number of treatments	Heat to 600°F 6 hours — cool, weigh	Number of treatments
Acetone blank	CT 882 ✓	4.3 ✓					0.5 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 870 ✓	60.8 ✓ 1					43.8 ✓	3 ✓
Filter blank	CT 832 ✓	0.3 ✓					0.3 ✓	3 ✓
Filter	CT 825 ✓	143.9 ✓ 1					78.3 ✓ ✓	3 ✓
Total particulate		204.7 ✓ 1					122.1 ✓ 1	

Remarks _____ 7.2.2.

Data reviewed by Jada Bennett 4/21/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 9D1115B
Sample location Boiler No 2 Analyst KRM
Relative humidity 55% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 882 ✓	Blank ✓	4376A ✓	372 ✓	101576.8 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 871 ✓	9D1115B ✓	4427A ✓	270 ✓✓	107199.7 ✓✓
Filter blank	CT 832 ✓	Blank ✓	4393B ✓	F. Hcr # 3531126 ✓	336.4 ✓
Filter	CT 826 ✓	9D1115B ✓	4427B ✓	F. Hcr # 3531103 ✓✓	343.6 ✓✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F — hours — cool, weigh	Number of treatments	Heat to 450°F — hours — cool, weigh	Number of treatments	Heat to 600°F — 6 hours — cool, weigh	Number of treatments
Acetone blank	CT 882 ✓	4.3 ✓					0.5 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 871 ✓	61.7 ✓✓					34.2 ✓✓	3 ✓
Filter blank	CT 832 ✓	0.3 ✓					0.3 ✓	3 ✓
Filter	CT 826 ✓	159.9 ✓✓					85.1 ✓✓	3 ✓
Total particulate		224.6 ✓✓					119.3 ✓✓	

Remarks _____ TGN.
Data reviewed by John Bennett 4/20/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 10AM15B ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 872 ✓	10AM15B ✓	4431A ✓	252 ✓ ✓	108913.8 ✓ ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 827 ✓	10AM15B ✓	4431B ✓	Filter # 3531028 ✓ ✓	327.6 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓			0.2 ✓	1 ✓	-0.3 ✓	2 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 872 ✓	108.8 ✓ ✓			72.8 ✓ ✓	1 ✓ ✓	50.5 ✓ ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓			-0.1 ✓	2 ✓	0.2 ✓	2 ✓
Filter	CT 827 ✓	151.8 ✓ ✓			130.3 ✓ ✓	2 ✓ ✓	107.3 ✓ ✓	3 ✓
Total particulate		260.6 ✓			203.1 ✓		157.8 ✓	

Remarks _____ T.J.R.

Data reviewed by John Bennett 4/30/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 10 BmsB P400 ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 -	Blank -	4301A -	368	998.1.3 -
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 873 ✓	10 BmsB P400 ✓	4434A -	262 ✓	1026.0.2 ✓
Filter blank	CT 831 -	Blank -	4316B -	Filter # 3531063 ✓	335.6 ✓
Filter	CT 828 ✓	10 BmsB P400 ✓	4434B ✓	Filter # 3531027 ✓✓	325.5 ✓✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F - hours - cool, weigh	Number of treatments	Heat to 450°F - 6 hours - cool, weigh	Number of treatments	Heat to 600°F - 6 hours - cool, weigh	Number of treatments
Acetone blank	CT 881 -	0.6 ✓			0.2 -	1 -	-0.3 ✓	3 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 873 ✓	66.9 ✓✓			46.6 ✓✓	1 ✓✓	24.8 ✓✓	3 ✓
Filter blank	CT 831 -	0.2 ✓			0.1 ✓	2 -	0.2 -	2 -
Filter	CT 828 ✓	159.2 ✓✓			133.3 ✓✓	2 ✓✓	111.2 ✓✓	3 ✓
Total particulate		226.1 ✓✓			179.9 ✓✓		136.0 ✓✓	

Remarks _____ T.J.R.

Data reviewed by Donna H. 4/3/83

* These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 10C115B ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 -	Blank -	4301A -	368 -	99EB1.3 -
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 874 ✓	10C115B ✓	4437A ✓	280 ✓ ✓	106295.7 ✓ ✓
Filter blank	CT 831 -	Blank -	4316B -	F. Her * 3531063 -	335.6 -
Filter	CT 829 ✓	10C115B ✓	4437B ✓	F. Her * 3531089 ✓ ✓	335.7 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F - hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 -	0.6 ✓			0.2 ✓	1 ✓	0.3 ✓	2 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 874 ✓	66.6 ✓			58.9 ✓ ✓	1 ✓ ✓	32.1 ✓ ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓			-0.1 ✓	2 ✓	0.2 ✓	2 ✓
Filter	CT 829 ✓	143.4 ✓			117.9 ✓ ✓	2 ✓ ✓	91.4 ✓ ✓	3 ✓
Total particulate		210.0 ✓			176.8 ✓ ✓		123.5 ✓ ✓	

Remarks _____ T.J.R.

Data reviewed by Jela Bennett 4/2/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

THERMOGRAVIMETRIC PARTICULATE ANALYSIS
PN 3530-15

Plant _____ Run No. 10 DMSB P400 ✓
Sample location Boiler No. 2 Analyst KRM
Relative humidity 50% Density of acetone (pa) .7908 (g/ml)

Sample type	Lab No.	Sample I.D.	Container No.	Initial Vol. (ml)	Tare Wt. (mg)
Acetone blank	CT 881 ✓	Blank ✓	4301A ✓	368 ✓	99881.3 ✓
Acetone blank (2)					
Acetone blank (3)					
Acetone rinse	CT 875 ✓	10DMSB P400 ✓	4440A ✓	293 ✓ ✓	105517.2 ✓ ✓
Filter blank	CT 831 ✓	Blank ✓	4316B ✓	Filter # 3531063 ✓	335.6 ✓
Filter	CT 830 ✓	10DMSB P400 ✓	4440B ✓	Filter # 3531058 ✓ ✓	332.1 ✓ ✓

Analysis results (mg)*

Sample type	Lab No.	Initial wt. (ambient)	Heat to 320°F - hours cool, weigh	Number of treatments	Heat to 450°F 6 hours cool, weigh	Number of treatments	Heat to 600°F 6 hours cool, weigh	Number of treatments
Acetone blank	CT 881 ✓	0.6 ✓			0.2 ✓	1 ✓	-0.3 ✓	2 ✓
Acetone blank (2)								
Acetone blank (3)								
Acetone rinse	CT 875 ✓	648 ✓ ✓			531 ✓ ✓ ✓	1 ✓ ✓	245 ✓ ✓	3 ✓
Filter blank	CT 831 ✓	0.2 ✓			-0.1 ✓	2 ✓	0.2 ✓	2 ✓
Filter	CT 830 ✓	149.0 ✓ ✓			128.5 ✓ ✓	2 ✓ ✓	100.2 ✓ ✓	3 ✓
Total particulate		213.8 ✓ ✓			181.6 ✓ ✓		121.7 ✓ ✓	

Remarks _____ T.J.N.

Data reviewed by Dea Bennett 4/21/83

*These are net weights (gross wt. avg. minus tare wt.) without blank subtraction.

LABORATORY REPORT

PN 3530-15

Hydrogen Peroxide Impinger Solutions

<u>Run No.</u>	<u>PEDCo No.</u>	<u>Total sample volume, ml</u>	<u>SO₂ total mg</u>
1AM5BW	CT 951	420	7224
1BM5BW	CT 952	397	7055
1CM5B	CT 953	400	6652
1DM5B	CT 954	404	6467
2AM5B	CT 955	400	7135
2BM5B	CT 956	393	7678
2CM5BW	CT 957	410	6376
2DM5BW	CT 958	424	6427
3AM5B	CT 959	490	7124
3BM5B	CT 960	403	7031
3CM5BP400	CT 961	343	5827
3DM5BP400	CT 962	394	6797
4AM5BP400	CT 963	435	7362
4BM5BP400	CT 964	408	7678
4CM5B	CT 965	397	6667
4DM5B	CT 966	460	6703
5AM5B	CT 967	403	5398
5BM5B	CT 968	415	5301
5CM5B	CT 969	433	5008
5DM5B	CT 970	445	5059
6AM5B	CT 971	410	5278
6BM5B	CT 972	480	5144
6CM5B	CT 973	446	4546
6DM5B	CT 974	449	4518
7AM5BW	CT 975	432	5087
7BM5B	CT 976	418	5026
7CM5BW	CT 977	415	4800

LABORATORY REPORT

PN 3530-15

Hydrogen Peroxide Impinger Solutions

<u>Run No.</u>	<u>PEDCo No.</u>	<u>Total sample volume, ml</u>	<u>SO₂ total mg</u>
7DM5B	CT 978	397	4955
8AM5B	CT 979	428	3037
8BM5BP400	CT 980	455	2967
8CM5B	CT 981	438	3062
8DM5BP400	CT 982	445	2763
9AM5B	CT 983	405	5266
9BM5B	CT 984	430	5198
9CM5B	CT 985	392	4928
9DM5B	CT 986	416	5001
10AM5B	CT 987	412	5465
10BM5BP400	CT 988	404	5121
10CM5B	CT 989	443	4834
10DM5BP400	CT 990	418	4916
10% H ₂ O ₂ Blank, Runs 1-5	CT 991	305	<0.3
10% H ₂ O ₂ Blank, Runs 6-10	CT 992	308	<0.3
Water Blank, Runs 1-5	CT 901	320	<0.3
Water Blank, Runs 6-10	CT 902	230	<0.2

T.S. 24
3/19/83

RUN NO. -----	LAB NO. -----	SAMPLE VOL. -----	ML TITRANT -----	MG H2SO4 -----
1AM5BW	CT903	489	5.4	66.2
1BM5BW	CT904	485	5.15	62.6
1CM5B	CT905	500	4.7	58.9
1BM5B	CT906	519	4.5	58.5
2AM5B	CT907	479	3.05	36.6
2BM5B	CT908	493	2.4	29.7
2CM5BW	CT909	475	3.7	44.0
2DM5BW	CT910	513	1.9	24.4
2DM5BW	CT910R	513	1.87	24.0
3AM5B	CT911	525	3.75	49.3
3AM5B	CT911R	525	3.75	49.3
3BM5B	CT912	504	3.9	49.3
3BM5B	CT912R	504	3.9	49.3
3CM5BP400	CT913	490	4.8	58.9
3DM5BP400	CT914	496	4.3	53.4
4AM5BP400	CT915	493	2.1	25.9
4BM5BP400	CT916	495	2	24.8
4CM5B	CT917	495	2	24.8
4DM5B	CT918	510	1.5	19.2
4DM5B	CT918R	510	1.43	18.3
5AM5B	CT919	465	3.05	35.5
5BM5B	CT920	474	3.1	36.8
5CM5B	CT921	457	2.5	28.6
5DM5B	CT922	458	2.6	29.8
5DM5B	CT922R	458	2.6	29.8
6AM5B	CT923	474	3.2	38.0
6BM5B	CT924	463	3.15	36.5
6CM5B	CT925	475	4.45	53.0
6DM5B	CT926	465	2.12	24.7
6DM5B	CT926R	465	2.1	24.5
7AM5BW	CT927	455	4.6	52.4
7BM5B	CT928	430	3.95	42.6
7CM5BW	CT929	458	4.15	47.6
7DM5B	CT930	460	4.65	53.6
8AM5B	CT931	439	2.9	31.9
8AM5B	CT931R	439	2.9	31.9
8BM5BP400	CT932	458	5.45	62.6
8BM5BP400	CT932R	458	5.5	63.1
8CM5B	CT933	417	6.85	71.6
8DM5BP400	CT934	424	4.4	46.8
9AM5B	CT935	485	8.4	102.1
9BM5B	CT936	467	7.2	84.3
9CM5B	CT937	454	9.15	104.1
9DM5B	CT938	495	8.05	99.9
10AM5B	CT939	552	5.6	77.5
10BM5BP400	CT940	554	5.9	81.9
10CM5B	CT941	529	7	92.8
10DM5BP400	CT942	508	5.55	70.7
10DM5BP400	CT942R	508	5.55	70.7
80% IPA/FLT-BLK	CT943	297	< .05	< 0.2
80% IPA	CT944	348	< .05	< 0.3

NORMALITY OF TITRANT= .01022 ✓

LABORATORY REPORT

PN 3530-15

APRIL 20, 1983

Run No.	Lab No.	Ambient weight, mg	Total particulate M5W, mg	C _{SO₄} , mg/liter	V _{evap} , ml	NWSSP, mg
1AM5BW-PR	CT891	-	120.0	112.8	293	74.5
1AM5BW-F	CT883	228.9	224.0	427.4	235	85.8
1BM5BW-PR	CT892	-	132.3	120.8	291	83.9
1BM5BW-F	CT884	221.1	218.3	419.6	235	82.7
2CM5BW-PR	CT893	-	120.0	51.08	365	94.4
2CM5BW-F	CT885	188.8	187.1	320.4	235	83.5
2DM5BW-PR	CT894	-	137.2	84.24	332	98.7
2DM5BW-F	CT886	191.6	190.5	334.6	235	82.3
7AM5BW-PR	CT895	-	95.8	152.2	320	28.8
7AM5BW-F	CT887	148.4	155.5	316.1	235	53.3
7CM5BW-PR	CT896	-	93.1	111.7	389	33.3
7CM5BW-F	CT888	146.8	154.7	318.5	235	51.7
Blank-PR	CT901	-	0.8	<1.00	305	0.8
Blank-F	CT889	0.3	2.8	1.98	235	2.2
Blank-PR	CT902	-	1.3	<1.00	215	1.3
Blank-F	CT890	0.2	1.1	1.91	235	0.5
Blank-F	CT833	0.1	3.6	1.89	235	3.0
1A-PR-Blank	CT897	-	3.1	1.55	235	2.6
1B-PR-Blank	CT898	-	2.8	<1.00	235	2.8
2C-PR-Blank	CT899	-	2.7	<1.00	235	2.7
2D-PR-Blank	CT900	-	3.1	2.24	235	2.4

Reviewed by Thomas J. Hajos

PEDCO ENVIRONMENTAL, INC.
11499 CHESTER ROAD
CINCINNATI, OHIO 45246

LABORATORY ANALYSIS REPORT

CLIENT: USEPA

PROJECT NO: 3530-15

REQUISITION:

RECEIVED:

ATTENTION:

SAMPLED BY:

REPORTED: 5/17/83

VANADYL HEAT TREATMENTS

SAMPLE ID	BLANK	#1	#2	#3	#4
PARAMETER					
AMBIENT W. MG	0.0	143.3	175.9	171.5	109.2
160°C. 6 HR. MG	0.0	96.7	120.3	126.5	74.6
# OF TREATMENTS	2	2	2	2	2
232°C. 6 HR. MG	-0.1	83.3	102.4	100.7	63.8
# OF TREATMENTS	2	2	2	2	2
316°C. 6 HR. MG	0.0	80.3	99.3	97.6	61.3
# OF TREATMENTS	3	3	3	3	

SAMPLE ID	PERCENT WEIGHT LOSS AFTER HEATING @:		
	160°C	232°C	316°C
1	33	42	44
2	32	42	44
3	26	41	43
4	32	42	44
AVG	31	42	44

QUESTIONS CONCERNING ANALYTICAL
RESULTS SHOULD BE REFERRED TO
IDA J. BENNETT

APPROVED BY: *IDA J. Bennett*

APPENDIX D
SAMPLING AND ANALYTICAL PROCEDURES

SAMPLING AND ANALYTICAL PROCEDURES

A four-train (quad) sampling system was used in this test program. This system allowed four samples to be collected simultaneously at essentially the same point in the gas stream. Each individual sampling train consisted of a Method 5* fronthalf and a Method 8* backhalf. Method 5 sampling procedures were used for all tests, except as noted.

SAMPLING APPARATUS

The sampling train(s) used in these tests met design specifications established by the Federal EPA and was assembled by PEDCo personnel. Each train, set up as shown in Figure D-1, consisted of:

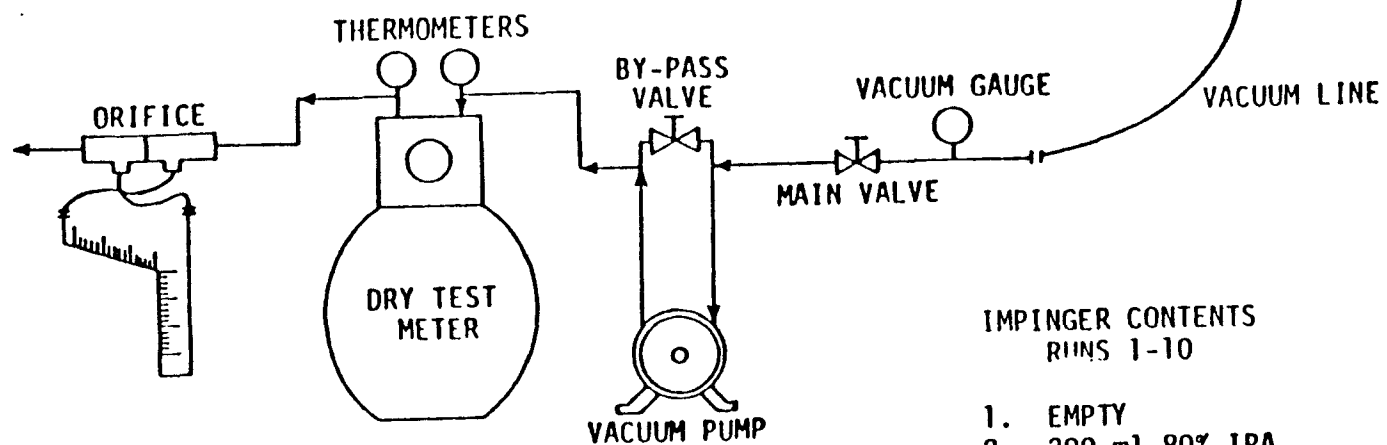
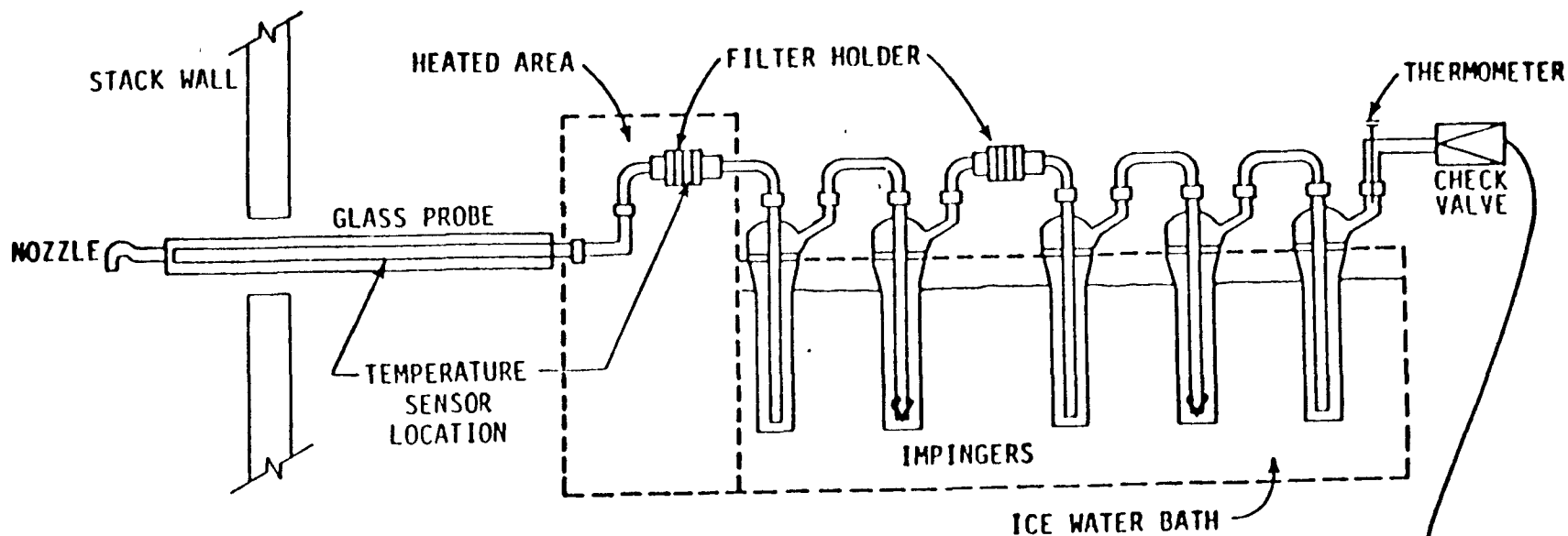
Nozzle - Stainless steel (316) with sharp, tapered leading edge and accurately measured round opening.

Probe - Borosilicate glass with a heating system capable of maintaining the desired gas temperature at the exit end during sampling.

Filter Holder - Pyrex glass with heating system capable of maintaining a filter temperature at desired levels.

Impingers - Five impingers connected in series with glass ball joints. The first, fourth, and fifth impingers were of the Greenburg-Smith design, modified by replacing the tip with a 1/2 inch I.D. glass tube extending to 1/2 inch from the bottom of the flask.

* 40 CFR 60, Appendix A, July 1981.



IMPINGER CONTENTS
RINS 1-10

1. EMPTY
2. 200 ml 80% IPA
3. 100 ml 10% H_2O_2
4. 100 ml 10% H_2O_2
5. 400 g SILICA GEL

Figure D-1. Methods 5 and 8 sampling train schematic.

Back-Half Filter Holder - Unheated Pyrex glass inserted between the second and third impingers to prevent carryover of any sulfuric acid mist.

Metering System - Vacuum guage, leak-free pump, thermometers capable of measuring temperature to within 5°F, calibrated dry gas meter, and related equipment to maintain an isokinetic sampling rate and to determine sample volume.

A single pitot-tube and thermocouple located as shown in Figure D-2 were used to measure stack gas velocity. Equipment consisted of:

Pitot Tube - Type S pitot tube that met all geometry standards was attached to the probe system to monitor stack gas velocity pressure.

Temperature Gauge - A Chromel/Alumel Type-K thermocouple (or equivalent) was attached to the pitot tube, in an interference-free arrangement, to monitor stack gas temperature within 5°F by the use of a digital indicator.

Draft Gauge - An inclined manometer made by Dwyer with a readability of 0.01 inch H₂O in the 0 to 1 inch range was used.

Barometer - Aneroid type to measure atmospheric pressures to within ± 0.1 inch Hg.

Probe and filter temperatures were monitored using multi-terminal digital indicators with thermocouple leads located in the middle of each probe and immediately behind the Method 5 filter frits. Rheostat devices were used to control individual probe temperatures. Filter temperatures were maintained at the desired level by the use of individual temperature controllers.

SAMPLING PROCEDURE

After selecting the sampling site, the stack pressure, temperature, molecular weight, moisture content, and range of

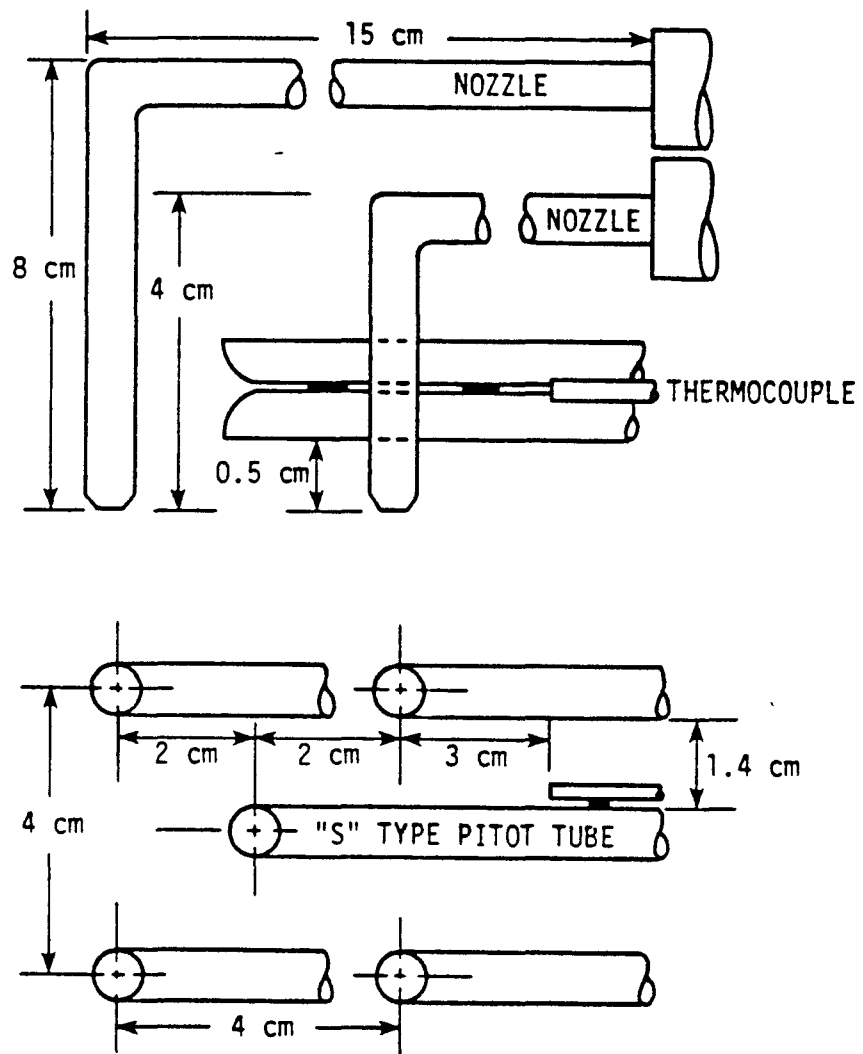


Figure D-2. Four-train sampling system showing nozzle, pitot tube, and thermocouple position.

velocity head in the general sampling area were measured according to procedures described in the Federal Register.^{*} A single sampling point located approximately 0.6 m from the stack wall was selected to allow all four nozzles to be positioned at points of equal velocity.

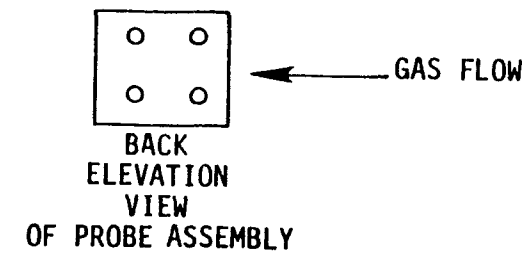
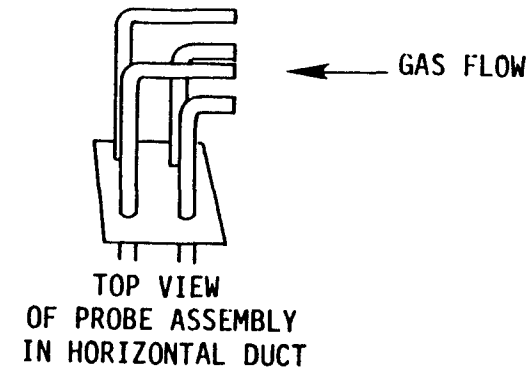
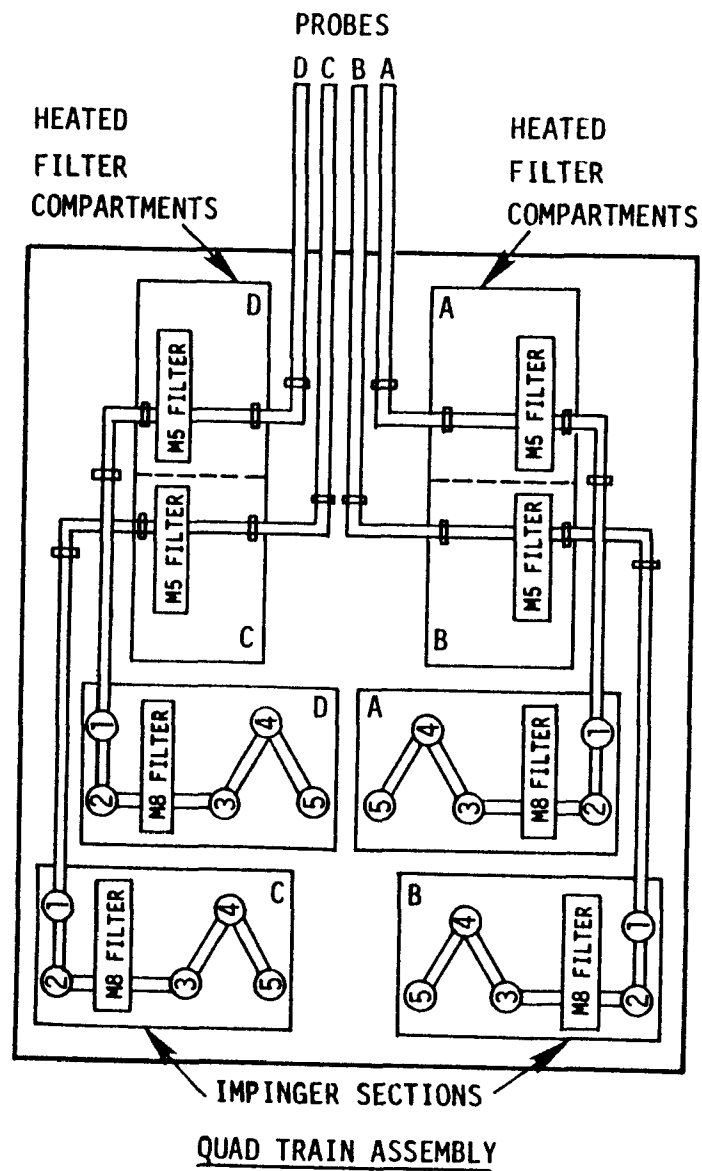
Individual sampling train components were assembled and labeled. Glass fiber filters^{**} (3-in. diameter) used in the Method 5 position were heated to 315°C prior to identification and tare weighing to the nearest 0.1 mg on an analytical balance. Each sample train had a Method 8 backhalf, modified by adding a fifth impinger behind the filter to minimize evaporation loss of IPA by additional cooling of the hot sample gas prior to its contacting the IPA. An unheated glass fiber filter^{**} assembly was inserted between the second and third impingers to preclude any sulfuric acid mist carryover. The contents of each impinger was as follows:

<u>Impinger</u>	<u>Contents - All Runs</u>
1	Empty
2	200-ml 80% IPA
3	100-ml 10% H ₂ O ₂
4	100-ml 10% H ₂ O ₂
5	400-grams silica gel

The sampling train subassemblies (probes, filter holders, impingers) were transported to the test site and assembled in the quad train configuration as shown in Figure D-3. The sampling trains were leak checked at the sampling site prior to each test

^{*} 40 CFR 60, Appendix A, Reference Methods 2, 3, and 4, July 1, 1981.

^{**} Whatman RA 934AH.



PROBE AND NOZZLE ORIENTATION

Figure D-3. Quad train configuration.

run by plugging the inlet to the nozzle and pulling a 15 inch Hg vacuum, and at the conclusion of the test by plugging the inlet to the nozzle and pulling a vacuum equal to the highest vacuum reached during the test run.

The pitot tube and lines were leak checked at the test site prior to each test run. The check was made by blowing into the impact opening of the pitot tube until 3 or more inches of water were recorded on the manometer and then capping the impact opening and holding it for 15 seconds to assure it was leak free. The static pressure side of the pitot tube was leak checked using the same procedure, except suction was used to obtain the 3 inch H₂O manometer reading. Crushed ice was placed around the impingers to keep the temperature of the gases leaving the last impinger at 20°C or less. For each train, the probe and filter were preheated to the desired temperature prior to sampling and maintained at that temperature throughout the run. The particular conditions for each type of train were:

Method 5B (Designated M5B) - probe and filter assembly heated to 160°C (320°F).

Modified Method 5B (Designated M5B-P400) - probe heated to 204°C (400°F) to minimize cold spots and filter assembly heated to 160°C (320°F).

Method 5BW (Designated M5BW) - probe and filter assembly heated to 160°C (320°F).

During sampling, stack gas and sampling train data were recorded at 10-minute intervals and when significant changes in stack flow conditions occurred. Isokinetic sampling rates were

set throughout the sampling period with the aid of a programmable calculator. All sampling data were recorded on the Particulate Field Data Sheet.

SAMPLE RECOVERY

The components of the quad train sample system were labeled and disassembled at the stack for transport to the sample clean-up/setup area. The filter and probe assemblies were recovered as follows:

- ° All filters were carefully removed from the filter holder and placed in a petri dish. These filters were sealed and labeled for shipment.
- ° For Methods 5B and M5B-P400, loose particulate from all sample exposed surfaces prior to the filter and acetone washings were placed in a polyethylene container, sealed, and labeled. For Method 5BW, deionized, distilled water was used for the probe rinse. Particulate was removed from the nozzle and probe with a nylon brush. The liquid level was marked after each container was sealed.

The impinger section of each sample train (modified Method 8) was removed from its ice bath and purged with ambient air for 15 minutes before recovering the contents. The long glass connector between the front filter holder and first impinger was not purged.

The contents were recovered as follows:

- ° After gravimetric weighing, the contents of the first and second impingers (condensate and 80 percent IPA) were placed in a polyethylene container. The impingers and connecting glassware between the front and backhalf filter were rinsed with 80 percent IPA and the rinse was added to the container along with the backhalf filter. The containers were then sealed, labeled, and the liquid level marked.

- ° After gravimetric weighing, the contents of the third and fourth impingers (10 percent H_2O_2) were placed in a polyethylene container. The impingers and connecting glassware were rinsed with deionized, distilled water and the rinse was added to the container. The containers were then sealed, labeled, and the liquid level marked.
- ° The color of the silica gel was noted on the sample recovery sheet and the net weight gain determined gravimetrically.

Blank samples were taken for each new batch (or a minimum of two) of the following reagents: acetone; deionized, distilled water; 80 percent IPA; 10 percent H_2O_2 ; and a filter. In addition, each probe was rinsed prior to initial use with either water or acetone (depending on method type), and these rinses were retained for probe rinse blank analysis.

SAMPLE LABELING

The sample label identifies the test run number, sample train, and each component of the individual train. The run numbers are consecutive from 1 to 10. Since each run consists of four single trains, each train was identified by a letter A, B, C, or D.

The last item of the label identifies the sample method and the component of the recovered sample. For example, identification No. 1C M5B-IPA indicates Test Run 1, Sample Train C, Method 5B sample method at 160°C (320°F) and the IPA impinger contents and rinse. Another example is 4A M5B-P400-Probe indicating Test Run 4, Sample Train A, Modified Method 5B sample method (filter at 160°C and probe at 204°C), and the probe rinse fraction.

SAMPLE RECEIPT AND CHAIN OF CUSTODY

Every sample entering the lab for analysis was assigned a unique alphanumeric identity on a Sample Receipt and Record Sheet (log). In the sample log-in book, this number was correlated with sample identification label and with the number of the analysis requisition form. A copy of the analysis requisition was kept with the samples and later with the raw data.

The samples remained in a locked sample storage room until removed for analysis. Transfer was documented on a Sample Control Record which is maintained by the sample custodian. The Sample Control Record documents all custody changes which occur in the laboratory and each procedure performed on the sample.

Release of samples requires notation of the Sample Control Record and verification of information and sample container condition. If the sample is to be transferred between two persons (i.e., two analysts), the transfer must take place through the sample custodian. In other words, the sample will be returned to the sample custodian and reissued.

SAMPLE ANALYSIS

Particulate Analysis

Initially, the filter particulate catch was placed in a tared glass weighing dish, desiccated for 24 hours, and weighed to the nearest 0.1 mg until a constant weight was achieved. The probe rinse fraction was transferred to a tared beaker and evaporated to dryness at ambient temperature and pressure, desiccated

for 24 hours, and weighed to the nearest 0.1 mg until a constant weight was achieved.

For this study a constant weight was defined as a difference of no more than 0.5 mg or 1 percent of the net weight, whichever was greater, between successive weighings, with at least 6 hours of desiccation between weighings. This is the same definition as for Method 5. Because previous data have shown that samples containing a significant amount of sulfuric acid may not come to a constant weight, each sample received a maximum of three separate weighings. In any case, the lowest weight achieved was reported as the ambient weight.

After this initial gravimetric analysis at ambient conditions, probe rinse and filter fractions were subjected to the sequence of heat treatments as outlined in the analytical matrix (Table 3-2). The samples were heated in an oven at the specified temperature for either 6 or 24 hours as indicated. Each sample fraction was cooled and desiccated for 24 hours after removal from the oven and weighed to the nearest 0.1 mg. Each sample was desiccated from an additional 3 hours and weighed to the nearest 0.1 mg. The lower weight achieved was reported.

Selected samples received additional heat treatments in order to evaluate sample stability. Prior to advancing to the next step of an analytical sequence, a heat treatment was repeated at the same time and temperature condition until a stable weight was obtained for these selected samples. For this study a stable weight was defined as a difference of no more than 5.0 mg

or 10 percent of the net sample weight, whichever was greater, between successive treatments at the same conditions. The number of treatments required to achieve a stable weight was recorded for each sample fraction up to a maximum of three treatments. The lowest weight achieved at a given treatment temperature was reported as the weight for that temperature condition. Filter and acetone blanks were treated in a similar manner as the samples.

Water-Soluble Sulfate Determination

Each sample fraction plus blanks were handled and analyzed as follows:

- ° Filter - The filter was cut into small pieces and placed in a 125-ml Erlenmeyer flask with a standard type joint equipped with an air condenser. The contents of the shipping container were rinsed into the flask. About 50 ml of distilled water was added and the contents gently refluxed for 6 to 8 hours. The solution was then cooled and diluted with water to exactly 250 ml in a volumetric flask. This solution was reserved for total soluble sulfate analysis, which is described below.
- ° Probe Rinse - The probe wash was poured into a 250 ml volumetric flask. The sample bottle was rinsed with distilled water and the rinsings were added to the flask. The solution was then diluted to the mark with distilled water (or, if greater than 250 ml, the volume was measured). This solution was reserved for total soluble sulfate analysis, which is described below.

Total Soluble Sulfate--

A 15-ml aliquot* was drawn from the settled samples (filter and rinse) into separate sample containers with a clean, dry pipet (only solution was transferred--no solid; if necessary, a portion of the sample was centrifuged). The sulfate ion ($\text{SO}_4^{=}$)

*The pipet is not rinsed. This deviation from normal procedures is necessary because the volume removed from the volumetric flask is required in the calculations.

concentration in each aliquot was determined by ion chromatography (IC). A syringe was used to inject 1 ml of the aliquot into the 100- μ l sample loop of the IC, thereby flushing the loop with sample. The conductivity response of the sample was compared with the calibration curve to obtain $\text{SO}_4^{=}$ concentration in mg/liter. Dilutions were prepared and reanalyzed if the initial response was out of the linear calibration range (i.e., greater than 15 mg/liter). Blank filter and water samples were prepared and analyzed in the same manner as the actual samples.

Mass Determination--

Filter and Rinse Solution Preparation - The remaining contents of each volumetric flask (235 ml) were poured into separate tared 250-ml beakers, and the flask was rinsed with distilled water to transfer all particulate matter. The filter solution was in Beaker A and the rinse solution was in Beaker B. These solutions were evaporated to approximately 100 ml at 105°C and allowed to cool before the next analysis was made.

Filter and Rinse Solution Analysis - Five drops of phenolphthalein indicator were added to all the tared beakers. Concentrated NH_4OH was then added drop by drop until the solution turned⁴ pink. The samples were returned to the oven and evaporated to dryness at 105°C, then cooled in a desiccator and weighed to a constant weight. Results were reported to the nearest 0.1 mg. For this method, "constant weight" means a difference of no more than 0.5 mg or 1 percent of the total weight less beaker and/or filter tare, whichever is greater, between two consecutive weighings, with no less than 6 hours of desiccation time between weighings.

Calculations--

Nomenclature--

FP = weight of particulate* on the filter in Beaker A,
mg

PRP = weight of probe rinse particulate* in Beaker B, mg

* Particulate with H_2SO_4 converted to $(\text{NH}_4)_2\text{SO}_4$.

NWSSP = weight of nonwater-soluble sulfate particulate*,
mg

AS_f = weight of ammonium sulfate in filter sample, mg

AS_{pr} = weight of AS in probe rinse sample, mg

V_{evap} = volume of solution evaporated in Beaker A (filter)
or Beaker B (probe rinse), ml

C_{SO₄} = concentration of sulfate in filter or probe rinse
solution aliquots, mg/liter

Equations--

$$FP(\text{mg}) = \text{gross weight Beaker A} - \text{tare weight Beaker A} - \text{filter tare weight} \quad \text{Eq. 1}$$

$$PRP(\text{mg}) = \text{gross weight Beaker B} - \text{tare weight Beaker B} \quad \text{Eq. 2}$$

$$AS(\text{mg}) = C_{SO_4} (\text{mg/liter}) \times V_{\text{evap}} (\text{ml}) \times \frac{\text{liter}}{1000 \text{ ml}} \quad \text{Eq. 3}$$
$$\times 1.376 \left(\frac{\text{mg AS}}{\text{mg SO}_4} \right)$$

Mass of Nonwater-Soluble Sulfate Particulate

The sum of the particulate** collected on the filter (FP) and the particulate* collected in the probe rinse (PRP) is equal to the sum of nonwater-soluble sulfate particulate (NWSSP) and ammonium sulfate (AS) in both samples:

$$FP + PRP = NWSSP + AS_f + AS_{pr} \quad \text{Eq. 4}$$

The NWSSP can be found by rearranging the equation and substituting appropriate values determined using Equations 1, 2, and 3.

$$NWSSP = FP + PRP - AS_f - AS_{pr} \quad \text{Eq. 5}$$

* Particulate excluding water-soluble sulfates.

** Particulate with H₂SO₄ converted to (NH₄)₂SO₄.

Sulfuric Acid Mist Analysis

The volume of the sample solution was recorded and the pH of the sample determined. The sample volume was diluted to 500 ml with 80 percent IPA. A 100 ml aliquot of this solution was pipetted into a 250 ml Erlenmeyer flask with 2 to 3 drops of thorin indicator and titrated to a pink end point using 0.0100 N barium perchlorate. If the end point color was not correct, the sample was passed through an ion exchange resin and retitrated. A blank was titrated for each sample in the same manner.

Sulfur Dioxide Analysis

The sample was diluted to 500 ml with deionized, distilled water. A 20 ml aliquot of this solution was pipetted into a 250 Erlenmeyer flask with 80 ml of 100 percent IPA and 2 to 3 drops thorin indicator. The solution was then titrated to a pink end point using 0.0100 N barium perchlorate. A blank was titrated in the same manner.

APPENDIX E
CALIBRATION PROCEDURES AND RESULTS

CALIBRATION PROCEDURES AND RESULTS

All of the equipment used was calibrated according to the procedures outlined in Maintenance, Calibration, and Operation of Isokinetic Source-Sampling Equipment.*

NOZZLE DIAMETER

The nozzles were calibrated by making three separate measurements using different inside diameters and calculating the average. If a deviation of more than 0.004 inches was found the nozzle was either discarded or reamed out and remeasured. A micrometer was used for measuring. These calibration data are shown in Figures E-1a and b.

PITOT TUBE CALIBRATION

The pitot tubes used in sampling were constructed by PEDCo Environmental and met all requirements of Method 2, Section 4.1 of the Federal Register.** Therefore, a baseline coefficient of 0.84 was assigned to each pitot tube. See Figures E-2 and E-3 for alignment requirements of Method 2, and Figures E-4a and b for actual inspection data of the pitot tubes used during the test program.

* Office of Air Programs Publication No. APTD-0576.

** 40 CFR 60, Appendix A, Reference Method 2, July 1981.

Date 2/6/83

Calibrated by D8/DS

Nozzle identification number	D ₁ , in.	D ₂ , in.	D ₃ , in.	ΔD, in.	D _{avg}
1A	.222	.223	.224	.002	.223
1B	.222	.221	.221	.001	.221
1C	.221	.221	.220	.001	.221
1D	.214	.217	.214	.003	.215
2A	.223	.224	.224	.001	.224
2B	.226	.227	.227	.001	.227
2C	.211	.211	.212	.001	.211
2D	.209	.210	.210	.001	.210

where:

D_{1,2,3}, = nozzle diameter measured on a different diameter, in.
Tolerance = measure within 0.001 in.

ΔD = maximum difference in any two measurements, in.
Tolerance = 0.004 in.

D_{avg} = average of D₁, D₂, and D₃.

Figure E-1a. Nozzle calibration data.

Date 2.11.83

Calibrated by D. Schffel

Nozzle identification number	D ₁ , in.	D ₂ , in.	D ₃ , in.	ΔD, in.	D _{avg}
B A	.306	.304	.305	.002	.305
B B	.308	.306	.306	.002	.307
B C	.305	.305	.305	.000	.305
B D	.304	.303	.305	.002	.304
For Runs 8 + 10					

where:

D_{1,2,3}, = nozzle diameter measured on a different diameter, in.
Tolerance = measure within 0.001 in.

ΔD = maximum difference in any two measurements, in.
Tolerance = 0.004 in.

D_{avg} = average of D₁, D₂, and D₃.

Figure E-1b. Nozzle calibration data.

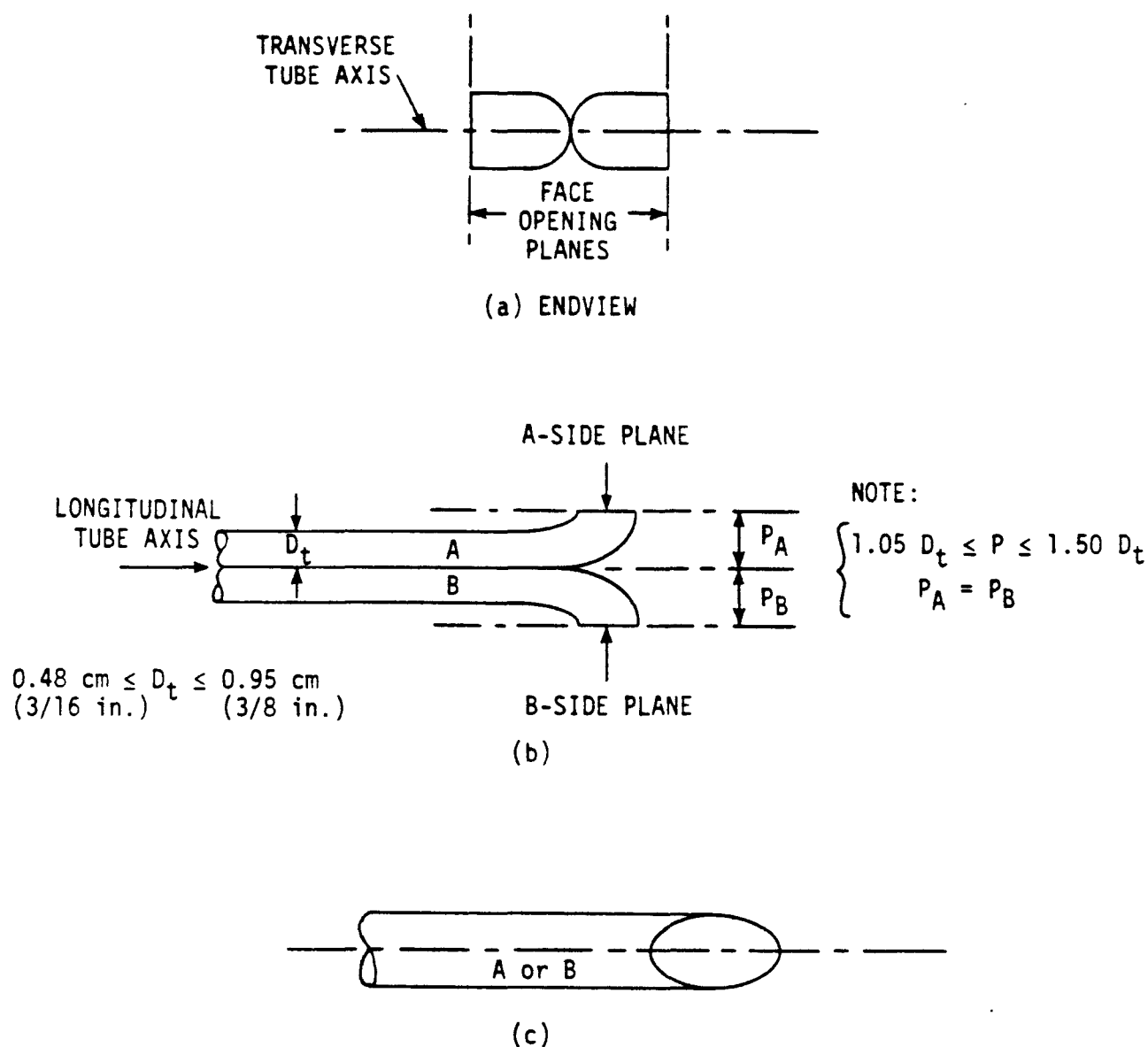


Figure E-2. Properly constructed Type S pitot tube, shown in: (a) end view; face opening planes perpendicular to transverse axis; (b) top view; face opening planes parallel to longitudinal axis; (c) side view; both legs of equal length and centerlines coincident, when viewed from both sides. Baseline coefficient values of 0.84 may be assigned to pitot tubes constructed this way.

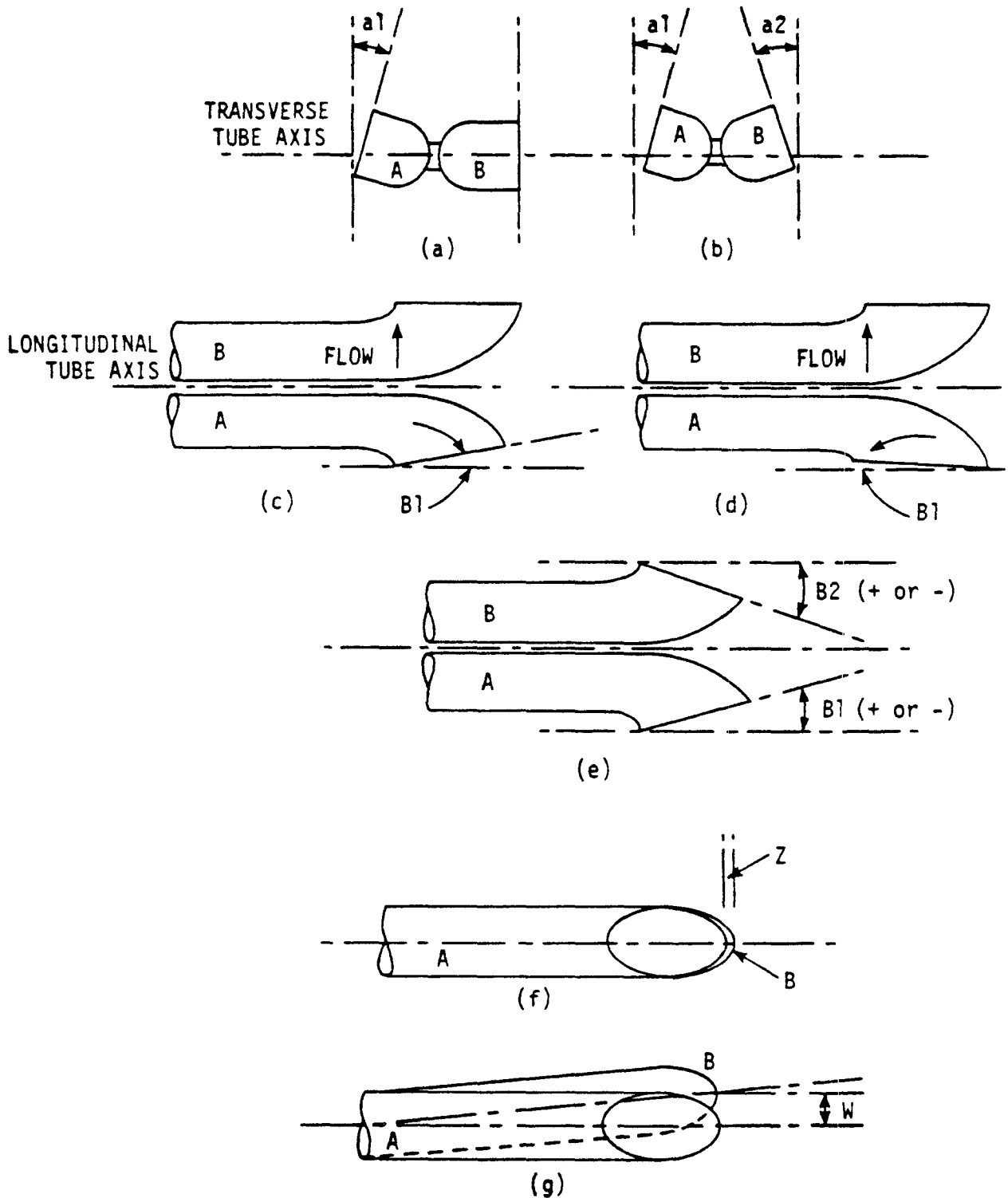


Figure E-3. Types of face-opening misalignment that can result from field use or improper construction of Type S pitot tubes. These will not affect C_p so long as a_1 and $a_2 < 10^\circ$, B_1 and $B_2 < 5^\circ$, $z < 0.32$ (1/8 in.) and $w < 0.08$ cm (1/32 in.).

Pitot Tube No. 278 Date 1/7/62 Inspector B. Armstrong

α_1 Degrees	α_2 Degrees	β_1 Degrees	β_2 Degrees
20	1.0	0.0	2.0
<10°	<10°	<5°	<5°

D_t Inches	P Inches	1.05 D_t Inches	1.50 D_t Inches
0.375	0.962	0.394	0.563
$0.185 \leq P_t < 0.380$	-	-	-

γ Degrees	ϕ Degrees	$P_{\sin(\gamma)}$ Inches	$P_{\sin(\phi)}$ Inches
1.0	0.0	0.017	0.000
-	-	<0.125	<0.03125

P_1 Inches	P_2 Inches	$ P_1 - P_2 $ Inches	Meet specifications
0.600	0.462	0.038	yes
$1.05 D_t < P_1 < 1.50 D_t$	$1.05 D_t < P_2 < 1.50 D_t$		

Lower line in each table is limits for meeting specifications.

Figure E-4a. Pitot tube inspection data sheet.

Pitot Tube No. 379 Date 2/1/83 Inspector P. Autenrieth

α_1 Degrees	α_2 Degrees	β_1 Degrees	β_2 Degrees
4°	5°	3.5°	1.5°
<10°	<10°	<5°	<5°

D_t Inches	P Inches	1.05 D_t Inches	1.50 D_t Inches
.375	1.070	.343	.562
$0.185 \leq P_t < 0.380$	-	-	-

γ Degrees	ϕ Degrees	$P_{\sin(\gamma)}$ Inches	$P_{\sin(\phi)}$ Inches
5.5°	1.5°	.0952	.0261
-	-	<0.125	<0.03125

P_1 Inches	P_2 Inches	$ P_1 - P_2 $ Inches	Meet specifications
5.10	5.10	0.0	yes
$1.05 D_t < P_1 < 1.50 D_t$	$1.05 D_t < P_2 < 1.50 D_t$	≤ 0.010	

Lower line in each table is limits for meeting specifications.

Figure E-4b. Pitot tube inspection data sheet.

DRY GAS METER AND ORIFICE METER

Figure E-5 was the set-up used for the initial and post-test calibration. A wet test meter with a 2-cubic-feet-per-minute capacity and ± 1 percent accuracy was used. The pump was run for approximately 15 minutes at an orifice manometer setting of 0.5 inch of water to heat up the pump and wet the interior surface of the wet test meter. The information on Figure E-6 (example calculation sheet) was gathered for the initial calibration and then, the ratio of accuracy of the wet test meter to the dry test meter, and the ΔH_0 were calculated.

POST-TEST METER CALIBRATION CHECK

A post-test meter calibration check was made on the meter box used during the test to check its accuracy against its last calibration check. This post-test calibration must be within ± 5 percent of the initial calibration. The initial calibration was performed as described in APTD-0576. The post-test calibration was performed using the same method as the initial calibration. Three calibration runs were made using the average orifice setting obtained during each test run and with the vacuum set at the average value obtained during each test run. After running the post-test calibration check all three runs were within the ± 5 percent range allowed by the Federal Register.*

The initial and post-test meter box calibration data are presented in Figures E-7a through h.

* 40 CFR 60, Appendix A, Reference Method 2, July 1981.

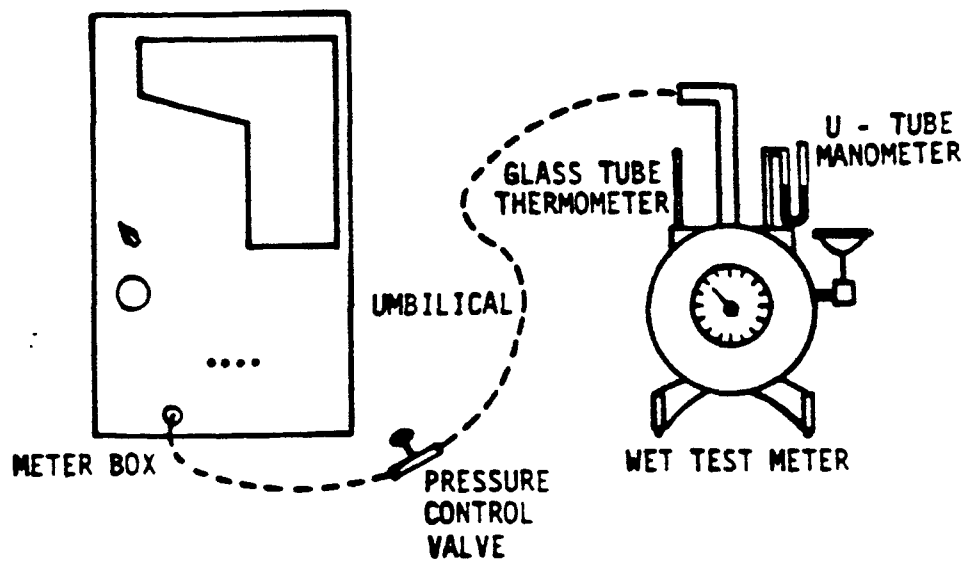


Figure E-5. Calibration setup.

DATE _____ METER BOX NO. _____

BAROMETRIC PRESSURE, P_b = _____ in. Hg. DRY GAS METER NO. _____

Orifice manometer setting ΔH in. H_2O	Gas volume wet test meter V_w ft ³	Gas volume dry gas meter V_d ft ³	Wet test		Dry gas meter		Time θ , min	γ	$\Delta H\theta$
			Meter t_w °F	Inlet t_{di} °F	outlet t_{dn} °F	Average t_d °F			
0.5	5								
1.0	5								
1.5	10								
2.0	10								
3.0	10								
4.0	10								

Average _____

ΔH	$\frac{\Delta H}{13.6}$	γ	$\Delta H\theta$
		$\frac{V_w P_b (t_d + 460)}{V_d (P_b + \frac{\Delta H}{13.6}) (t_w + 460)}$	$\frac{0.0317 \Delta H}{P_b (t_d + 460)} \left[\frac{(t_w + 460) \theta}{V_w} \right]^2$
0.5	0.0368		
1.0	0.0737		
1.5	0.110		
2.0	0.147		
3.0	0.221		
4.0	0.294		

γ = Ratio of accuracy of wet test meter to dry test meter. Tolerance = + 0.01
 $\Delta H\theta$ = Orifice of pressure differential that gives 0.75 cfm of air at 70°F and 29.92 inches of mercury, in H_2O . Tolerance = +0.15.

Figure E-6. Calibration data sheet.

DATE: FEBRUARY 1, 1983METER BOX NO. FB#4CALIBRATOR: James E. FitzgeraldBAROMETRIC PRESSURE (P_b) 29.27 in. Hg

Leak Checks:

- Positive (minimum 5 in. H₂O):- Negative (within 3 in. Hg of absolute): 2.00 cfm 27.5 in. Hg

Not to exceed 0.005 cfm.

Orifice manometer setting ΔH in H ₂ O	Volume wet test meter V_w ft ³	Volume dry gas meter V_d ft ³	Temperatures				Duration of test θ min	Vacuum setting in Hg	γ	ΔH in H ₂ O
			Wet test meter T_w °F	Dry gas meter		Average T_d °F				
				Inlet T_i °F	Outlet T_o °F					
0.5	5.0	445.698 451.502	72 72	76 78	76 76	76.5	12 ^{28.6} / ₆₀	8.5	1.0352	1.790
1.0	5.0	451.065 455.917	72 72	75 77	76 76	77.25	8 ^{53.9} / ₆₀	10.5	1.0248	1.808
1.5	10.0	451.112 465.969	72 71	78 77	76 76	77.25	14 ^{54.1} / ₆₀	10.0	1.0300	1.896
2.0	10.0	466.304 474.177	71 70.5	79 80	76 75	77.5	13 ^{7.8} / ₆₀	10.5	1.0288	1.957
3.0	10.0	476.626 481.424	70.5 70.5	80 80	75 76	77.75	10 ^{33.8} / ₆₀	10.0	1.0269	1.896
4.0	10.0	486.874 476.689	70.5 70.5	80 80	75 76	77.75	9 ^{13.7} / ₆₀	10.0	1.0247	1.927
Average									1.030	1.88

γ must not deviate by more than ± 0.02 γ .
 ΔH must not deviate by more than 0.15 in H₂O.

 γ must not deviate by more than ± 0.02 . ΔH must not deviate by more than 0.15 in H₂O.

ΔH	γ			ΔH	
	$\frac{(V_w)(P_b)(T_d + 460)}{(V_d)(P_b + \Delta H/13.6)(T_w + 460)}$			$\frac{(0.0317)(\Delta H)}{(P_b)(T_d + 460)} \left[\frac{(T_w + 460)(\theta)^2}{(V_w)} \right]$	
0.5	$\frac{(5.0)(29.27)(534.5)}{(4.864)(29.31)(532.0)}$			$\frac{(0.0317)(0.5)}{(29.27)(534.5)} \left[\frac{(532.0)(12.48)^2}{5.0} \right]$	
1.0	$\frac{(5.0)(29.27)(537.25)}{(4.892)(29.34)(532.0)}$			$\frac{(0.0317)(1.0)}{(29.27)(537.25)} \left[\frac{(532.0)(8.90)^2}{5.0} \right]$	
1.5	$\frac{(10.0)(29.27)(537.25)}{(9.277)(29.38)(534.5)}$			$\frac{(0.0317)(1.5)}{(29.27)(537.25)} \left[\frac{(531.5)(14.55)^2}{10.0} \right]$	
2.0	$\frac{(10.0)(29.27)(537.5)}{(9.793)(29.42)(530.75)}$			$\frac{(0.0317)(2.0)}{(29.27)(537.5)} \left[\frac{(537.5)(13.13)^2}{10.0} \right]$	
3.0	$\frac{(10.0)(29.27)(537.75)}{(9.793)(29.49)(530.5)}$			$\frac{(0.0317)(3.0)}{(29.27)(537.75)} \left[\frac{(530.5)(10.50)^2}{10.0} \right]$	
4.0	$\frac{(10.0)(29.27)(537.75)}{(9.715)(29.56)(530.5)}$			$\frac{(0.0317)(4.0)}{(29.27)(537.75)} \left[\frac{(530.5)(7.22)^2}{10.0} \right]$	

Figure E-7a. Particulate sampling meter box initial calibration.

DATE: 2/16/83METER BOX NO. FB-4BAROMETRIC PRESSURE (P_{bar}): 29.44 in. HgPRETEST γ : 1.030 $\Delta H\theta$: 1.28

PLANT: _____

PROJECT NO. 3530-15PROJECT MANAGER: S. PRASADCALIBRATOR: R. J. TESZKEG-22

Orifice manometer setting * ΔH in. H ₂ O	Wet test meter volume V_w ft ³	Dry gas meter volume V_d ft ³	Temperatures				Vacuum setting ** in. Hg	Duration of run θ min	γ	$\Delta H\theta$
			Wet test meter T_w °F	Inlet T_{di} °F	Dry gas meter Outlet T_{di} °F	Average T_d °F				
		129.315	73	77	73					
1.0	11	140.048	73	80	76	76.5	10	19 ⁴² / ₆₀	1.029	1.25
		140.048	73	80	76					
1.0	11	150.822	73	81	76	78.25	10	19 ⁵² / ₆₀	1.028	1.25
		150.822	73	81	76					
1.0	12	162.620	73	81	78	79	10	21 ⁴³ / ₆₀	1.026	1.76
Post-test average***									1.027	1.82

γ	$\Delta H\theta$
$\left(\frac{V_w}{V_d} \right) \left(\frac{P_{bar}}{P_{bar} + \Delta H/13.6} \right) \left(\frac{T_d + 460}{T_w + 460} \right)$	$\left(\frac{0.0317}{P_{bar}} \right) \left(\frac{\Delta H}{T_d + 460} \right) \left[\frac{(T_w + 460)(\theta)}{V_w} \right]^2$
$\left(\frac{10.733}{11.000} \right) \left(\frac{29.44}{29.51} \right) \left(\frac{536.5}{533} \right)$	$\left(\frac{0.0317}{29.44} \right) \left(\frac{1.0}{536.5} \right) \left[\frac{(533)(19.8)}{11.000} \right]^2$
$\left(\frac{10.774}{11.798} \right) \left(\frac{29.44}{29.51} \right) \left(\frac{538.25}{539} \right)$	$\left(\frac{0.0317}{29.44} \right) \left(\frac{1.0}{538.25} \right) \left[\frac{(533)(21.71)}{12.000} \right]^2$

*To be the average ΔH used during the test series.

**To be the highest vacuum used during the test series.

***Post-test γ must be within the range, pre-test $\gamma \pm 0.05\gamma$ Post-test $\Delta H\theta$ must be within the range, pre-test $\Delta H\theta \pm 0.15$

Figure E-7b. Particulate sampling meter box post-test calibration.

DATE: FEBRUARY 1, 1983
 CALIBRATOR: Michael J. Feltz

METER BOX NO. 1375
 BAROMETRIC PRESSURE (P_b) 29.53 in. Hg

Leak Checks:

Positive (minimum 5 in. H₂O): 0.001 cfm
 Negative (within 3 in. Hg of absolute): 25 in. Hg
 *Not to exceed 0.005 cfm.

Orifice manometer setting ΔH in H_2O	Volume wet test meter V_w ft^3	Volume dry gas meter V_d ft^3	Temperatures				Duration of test θ min	Vacuum setting in Hg	γ	ΔH_0 in H_2O
			Wet test meter T_w $^{\circ}F$	Dry gas meter						
				Inlet T_i $^{\circ}F$	Outlet T_o $^{\circ}F$	Average T_d $^{\circ}F$				
0.5	5.0	73.60 92.51	73	90 92	83 83	88.0	12.41 6.0	10.0	0.955	1.806
1.0	5.0	75.23 76.415	73	92 93	84 84	88.25	9.53 6.0	9.5	0.932	1.742
1.5	10.0	75.82 76.131	73	92 95	83 84	88.5	14.41 6.0	9.2	0.952	1.812
2.0	10.0	77.73 77.157	73	95 96	84 85	90.0	12.52 6.0	11.0	0.930	1.837
3.0	10.0	77.70 78.147	73	96 98	85 85	91.0	10.34 6.0	10.0	0.930	1.855
4.0	10.0	78.63 79.072	73	97 99	85 85	91.25	9.14 6.0	11.0	0.928	1.893
Average									0.933	1.84

γ must not deviate by more than $\pm 0.02 \gamma$.
 ΔH_0 must not deviate by more than 0.15 in H_2O .

γ must not deviate by more than +0.02 γ.
 ΔH₀ must not deviate by more than 0.15 in H₂O.

ΔH	γ			ΔH ₀		
	(V _w)	(P _b)	(T _d + 460)	(0.0317) (ΔH)	(T _w + 460) (θ) ²	(V _w)
0.5	(5.0)	(29.53)	(548.5)	(0.0317) (0.5)	(533.0) (12.74) ²	(5.0)
1.0	(5.0)	(29.53)	(548.25)	(0.0317) (1.0)	(533.0) (19.12) ²	(5.0)
1.5	(10.0)	(29.53)	(548.5)	(0.0317) (1.5)	(533.0) (14.74) ²	(10.0)
2.0	(10.0)	(29.53)	(550.0)	(0.0317) (2.0)	(533.0) (12.87) ²	(10.0)
3.0	(10.0)	(29.53)	(551.0)	(0.0317) (3.0)	(533.0) (10.57) ²	(10.0)
4.0	(10.0)	(29.53)	(551.25)	(0.0317) (4.0)	(533.0) (9.75) ²	(10.0)

Figure E-7c. Particulate sampling meter box initial calibration.

DATE: 2/15/83
 BAROMETRIC PRESSURE (P_{bar}): 29.46 in. Hg
 PLANT: _____
 PROJECT MANAGER: J. PROHASCA

METER BOX NO. FB-5
 PRETEST Y: 983 $\Delta H\theta$: 1.84
 PROJECT NO. 3530-15
 CALIBRATOR: R. ANTISBARGER

Orifice manometer setting * ΔH in. H ₂ O	Wet test meter volume V_w ft ³	Dry gas meter volume V_d ft ³	Temperatures				Vacuum setting ** in. Hg	Duration of run ϕ min	γ	$\Delta H\phi$
			Wet test meter T_w °F	Dry gas meter						
				Inlet T_{di} °F	Outlet T_{di} °F	Average T_d °F				
1.0	11 11	588.580	73	80	72	77.5	10	19 $\frac{36}{60}$	0.9885	1.806
		599.775	73	84	74					
1.0	10	599.775	73	84	74	80.0	10	17 $\frac{43}{60}$	0.9844	1.794
		610.037	73	86	76					
1.0	10	610.037	73	86	76	82.25	10	17 $\frac{53}{60}$	0.9870	1.802
		620.320	73	89	78					
Post-test average***									0.987	1.80

γ	$\Delta H\theta$
$\left(\frac{V_w}{V_d} \right) (P_{bar} + \Delta H/13.6) (T_d + 460)$	$\left(\frac{(0.0317)(\Delta H)}{(P_{bar})(T_d + 460)} \right) \left[\frac{(T_w + 460)(\theta)}{V_w} \right]^2$
$\left(\frac{11.0}{11.195} \right) (29.46) (537.5)$	$\left(\frac{0.0317(1.0)}{(29.46)(537.5)} \right) \left[\frac{(533.0)(19.60)}{11.0} \right]^2$
$\left(\frac{10.0}{10.262} \right) (29.46) (540.0)$	$\left(\frac{0.0317(1.0)}{(29.46)(540.0)} \right) \left[\frac{(533.0)(17.80)}{10.0} \right]^2$
$\left(\frac{10.0}{10.283} \right) (29.46) (542.25)$	$\left(\frac{0.0317(1.0)}{(29.46)(542.25)} \right) \left[\frac{(533.0)(17.88)}{10.0} \right]^2$

- *To be the average ΔH used during the test series.
 **To be the highest vacuum used during the test series.
 ***Post-test γ must be within the range, pre-test $\gamma \pm 0.05\gamma$
 Post-test $\Delta H\theta$ must be within the range, pre-test $\Delta H\theta \pm 0.15$

Figure E-7d. Particulate sampling meter box post-test calibration.

DATE: 11.5.82 METER BOX NO. FB-6
 CALIBRATOR: D. J. J. J. J. BAROMETRIC PRESSURE (P_b) 29.66 in. Hg

Leak Checks:

Positive (minimum 5 in. H₂O): ✓

Negative (within 3 in. Hg of absolute): 0.000 cfm 2.7 in. Hg

*Not to exceed 0.005 cfm.

Orifice manometer setting ΔH in H ₂ O	Volume wet test meter V_w ft ³	Volume dry gas meter V_d ft ³	Temperatures				Duration of test θ min	Vacuum setting in Hg	γ	$\Delta H\theta$ in H ₂ O
			Wet test meter T_w °F	Dry gas meter						
				Inlet T_i °F	Outlet T_o °F	Average T_d °F				
0.5	10	659.520 661.900	75 75	76 80	74 76	76.5	22 ³⁶	10.0	.965	1.456
1.0	10	672.000 682.443	75 75	80 83	76 76	78.75	16 ¹⁴	10.0	.962	1.471
1.5	10	688.100 698.613	75 75	83 86	76 78	80.75	13 ¹⁸	8.5	.958	1.501
2.0	10	701.000 711.531	75 75	86 86	78 79	82.25	11 ³²	11.0	.957	1.500
3.0	10	715.303 725.808	75 75	86 87	80 80	83.25	9 ²⁵	9.0	.959	1.515
4.0	10	730.103 742.597	75 75	88 88	80 80	84.0	8 ¹⁴	7.0	.960	1.524
Average									.960	1.50

γ must not deviate by more than $\pm 0.02 \gamma$.
 $\Delta H\theta$ must not deviate by more than ± 0.15 in H₂O.

γ must not deviate by more than +0.02 γ .

$\Delta H\theta$ must not deviate by more than 0.15 in H₂O.

ΔH	γ		$\Delta H\theta$	
	$\frac{(V_w)(P_b)(T_d + 460)}{(V_d)(P_b + \Delta H/13.6)(T_w + 460)}$		$\frac{(0.0317)(\Delta H)}{(P_b)(T_d + 460)} \left[\frac{(T_w + 460)(\theta)}{(V_w)} \right]^2$	
0.5	$\frac{(10)(29.66)(536.5)}{(10.38)(29.70)(535)}$		$\frac{(0.0317)(0.5)}{(29.66)(536.5)} \left[\frac{(535)(22.6)}{(10)} \right]^2$	
1.0	$\frac{(10)(29.66)(538.75)}{(10.443)(29.73)(535)}$		$\frac{(0.0317)(1.0)}{(29.66)(538.75)} \left[\frac{(535)(16.14)}{(10)} \right]^2$	
1.5	$\frac{(10)(29.66)(540.75)}{(10.513)(29.77)(535)}$		$\frac{(0.0317)(1.5)}{(29.66)(540.75)} \left[\frac{(535)(13.18)}{(10)} \right]^2$	
2.0	$\frac{(10)(29.66)(542.25)}{(10.529)(29.81)(535)}$		$\frac{(0.0317)(2.0)}{(29.66)(542.25)} \left[\frac{(535)(11.32)}{(10)} \right]^2$	
3.0	$\frac{(10)(29.66)(543.25)}{(10.505)(29.88)(535)}$		$\frac{(0.0317)(3.0)}{(29.66)(543.25)} \left[\frac{(535)(9.25)}{(10)} \right]^2$	
4.0	$\frac{(10)(29.66)(544)}{(10.494)(29.95)(535)}$		$\frac{(0.0317)(4.0)}{(29.66)(544)} \left[\frac{(535)(8.14)}{(10)} \right]^2$	

Figure E-7e. Particulate sampling meter box initial calibration.

DATE: 2/15/83METER BOX NO. FB-6BAROMETRIC PRESSURE (P_{bar}): 29.46 in. HgPRETEST Y: 960 $\Delta H\theta$: 1.50

PLANT: _____

PROJECT NO. 3530-15PROJECT MANAGER: J. PROHASKACALIBRATOR: 2 ANTISBERGER

Orifice manometer setting * ΔH in. H ₂ O	Wet test meter volume V_w ft ³	Dry gas meter volume V_d ft ³	Temperatures				Vacuum setting ** in. Hg	Duration of run θ min	Y	$\Delta H\theta$
			Wet test meter T_w °F	Dry gas meter						
				Inlet T_{di} °F	Outlet T_{di} °F	Average T_d °F				
1.0	10	537.28	73	72	67		16.01 60	10	0.9531	1.477
		545.186	73	75	70	71.0				
1.0	10	545.186	73	75	70		15.59 60	10	0.9752	1.462
		558.430	73	78	72	73.75				
1.0	10	558.430	73	78	72		16.03 60	10	0.9614	1.470
		568.355	73	79	73	75.5				
Post-test average***									0.963	1.47

Y	$\Delta H\theta$
$(\frac{V_w}{V_d})(\frac{P_{bar}}{P_{bar} + \Delta H/13.6})(\frac{T_d + 460}{T_w + 460})$	$(0.0317)(\Delta H) \left[\frac{(T_w + 460)(\theta)}{V_w} \right]^2$
$(\frac{10.0}{10.428})(\frac{29.46}{29.53})(\frac{531.0}{533.0})$	$(0.0317)(1.0) \left[\frac{533.0(16.02)}{10.0} \right]^2$
$(\frac{10.0}{10.244})(\frac{29.46}{29.53})(\frac{533.75}{533.0})$	$(0.0317)(1.0) \left[\frac{533.0(15.98)}{10.0} \right]^2$
$(\frac{10.0}{10.425})(\frac{29.46}{29.53})(\frac{535.5}{533.0})$	$(0.0317)(1.0) \left[\frac{533.0(16.05)}{10.0} \right]^2$

*To be the average ΔH used during the test series.

**To be the highest vacuum used during the test series.

***Post-test Y must be within the range, pre-test Y $\pm 0.05Y$ Post-test $\Delta H\theta$ must be within the range, pre-test $\Delta H\theta \pm 0.15$

Figure E-7f. Particulate sampling meter box post-test calibration.

DATE: JANUARY 31, 1983METER BOX NO. FB#7CALIBRATOR: Shane E. FitzgeraldBAROMETRIC PRESSURE (P_b) 29.55 in. Hg

Leak Checks:

Positive (minimum 5 in. H₂O): OKNegative (within 3 in. Hg of absolute): 0.000 cfm 26.5 in. Hg

*Not to exceed 0.005 cfm.

Orifice manometer setting ΔH in H_2O	Volume wet test meter V_w ft^3	Volume dry gas meter V_d ft^3	Temperatures				Duration of test θ min	Vacuum setting in Hg	γ	ΔH_e in H_2O
			Wet test meter T_w $^{\circ}F$	Dry gas meter						
				Inlet T_1 $^{\circ}F$	Outlet T_2 $^{\circ}F$	Average T_d $^{\circ}F$				
0.5	6.0	35.665 32.173	73 73	92 92	82 83	87.25	14 $\frac{25.4}{60}$	8.5	1.0077	1.522
1.0	5.0	324.763 319.567	73 73	91 92	83 83	87.25	8 $\frac{47.2}{60}$	8.0	1.0034	1.719
1.5	10.0	335.154 340.376	73 73	92 94	83 83	88.0	14 $\frac{15.6}{60}$	10.0	1.0021	1.706
2.0	11.0	340.666 351.731	73 73	94 97	84 84	89.75	13 $\frac{45.5}{60}$	10.0	1.0021	1.733
3.0	10.0	352.245 362.538	73 73	96 98	84 85	90.75	10 $\frac{14.2}{60}$	10.5	1.0014	1.739
4.0	10.0	363.052 373.284	73 73	98 99	85 85	91.75	8 $\frac{59.0}{60}$	10.5	0.9997	1.750
Average									1.003	1.72

γ must not deviate by more than $\pm 0.02 \gamma$.
 ΔH_e must not deviate by more than 0.15 in H₂O.

ΔH	γ			ΔH_e		
	$\left(\frac{V_w}{V_d} \right)$	$\left(\frac{P_b}{P_b + \Delta H / 13.6} \right)$	$(T_d + 460)$	$(0.0317) \left(\frac{\Delta H}{P_b} \right)$	$(T_d + 460)$	$\left[\frac{(T_w + 460)(\theta)^2}{(V_w)} \right]$
0.5	$\left(\frac{6.0}{6.105} \right)$	$\left(\frac{29.55}{29.62} \right)$	(547.25)	$(0.0317) \left(\frac{0.5}{29.55} \right)$	(547.25)	$\left[\frac{(533.0)(14.49)^2}{6.0} \right]$
1.0	$\left(\frac{5.0}{5.104} \right)$	$\left(\frac{29.55}{29.65} \right)$	(547.25)	$(0.0317) \left(\frac{1.0}{29.55} \right)$	(547.25)	$\left[\frac{(533.0)(8.79)^2}{5.0} \right]$
1.5	$\left(\frac{10.0}{10.222} \right)$	$\left(\frac{29.55}{29.69} \right)$	(545.0)	$(0.0317) \left(\frac{1.5}{29.55} \right)$	(548.0)	$\left[\frac{(533.0)(14.31)^2}{10.0} \right]$
2.0	$\left(\frac{11.0}{11.265} \right)$	$\left(\frac{29.55}{29.73} \right)$	(547.75)	$(0.0317) \left(\frac{2.0}{29.55} \right)$	(547.75)	$\left[\frac{(533.0)(13.76)^2}{11.0} \right]$
3.0	$\left(\frac{10.0}{10.242} \right)$	$\left(\frac{29.55}{29.80} \right)$	(550.75)	$(0.0317) \left(\frac{3.0}{29.55} \right)$	(550.75)	$\left[\frac{(533.0)(10.24)^2}{10.0} \right]$
4.0	$\left(\frac{10.0}{10.252} \right)$	$\left(\frac{29.55}{29.87} \right)$	(551.75)	$(0.0317) \left(\frac{4.0}{29.55} \right)$	(551.75)	$\left[\frac{(533.0)(8.75)^2}{10.0} \right]$

Figure E-7g. Particulate sampling meter box initial calibration.

DATE: 2/16/83METER BOX NO. FR-7BAROMETRIC PRESSURE (P_{bar}): 29.44 in. HgPRETEST γ : 1.003 $\Delta H\theta$: 1.72

PLANT: _____

PROJECT NO. 3530-15PROJECT MANAGER: J PROHASKACALIBRATOR: T. ANTISBERGER

Orifice manometer setting * ΔH in. H ₂ O	Wet test meter volume V_w ft ³	Dry gas meter volume V_d ft ³	Temperatures				Vacuum setting ** in. Hg	Duration of run θ min	γ	$\Delta H\theta$	
			Wet test meter T_w °F	Dry gas meter							
				Inlet T_{di} °F	Outlet T_{di} °F	Average T_d °F					
		002.013	73	77	73						
1.0	10	012.110	73	82	74	76.5	10	17 $\frac{24}{60}$	1.0045	1.726	
		012.110	73	77	74						
1.0	10	022.134	73	82	76	77.25	10	17 $\frac{16}{60}$	1.003	1.696	
		022.134	73	82	76						
1.0	14	036.255	73	88	78	81	10	24 $\frac{19}{60}$	1.004	1.70	
Post-test average***										1.0005	1.707

γ	$\Delta H\theta$
$\left(\frac{V_w}{V_d} \right) \left(\frac{P_{bar}}{P_{bar} + \Delta H/13.6} \right) \left(\frac{T_d + 460}{T_w + 460} \right)$	$\frac{(0.0317)(\Delta H)}{(P_{bar})(T_d + 460)} \left[\frac{(T_w + 460)(\theta)}{V_w} \right]^2$
$\frac{(10.000)(29.44)(536.5)}{(10.097)(29.51)(533)}$	$\frac{(0.0317)(1.0)}{(29.44)(536.5)} \left[\frac{(533)(17.4)}{10.000} \right]^2$
$\frac{(10.000)(29.44)(537.25)}{(10.024)(29.51)(533)}$	$\frac{(0.0317)(1.0)}{(29.44)(537.25)} \left[\frac{(533)(17.26)}{10.000} \right]^2$
$\frac{(14.000)(29.44)(541)}{(14.121)(29.51)(533)}$	$\frac{(0.0317)(1.0)}{(29.44)(541)} \left[\frac{(533)(24.31)}{14.000} \right]^2$

*To be the average ΔH used during the test series.

**To be the highest vacuum used during the test series.

***Post-test γ must be within the range, pre-test $\gamma \pm 0.05\gamma$ Post-test $\Delta H\theta$ must be within the range, pre-test $\Delta H\theta \pm 0.15$

Figure E-7h. Particulate sampling meter box post-test calibration.

THERMOCOUPLES

Thermocouples were calibrated by comparison against an ASTM-2F thermometer at approximately 32°F, ambient temperature, 100°F, and 500°F. The thermocouples read within 1.5 percent of the reference thermometer throughout the entire range when expressed in degrees Rankine. If a thermocouple did not read within 1.5 percent, a correction formula based on a least squares analysis of the data was utilized. The correction formula corrected the data to within 1.5 percent. Each thermocouple was checked at ambient temperature at the test site to verify the calibration. Calibration data are presented in Figures E-8a and b.

DIGITAL INDICATOR FOR THERMOCOUPLE READOUT

A digital indicator was calibrated by feeding a series of millivolt signals to the input, and comparing the indicator reading with the reading the signal should have generated. Error did not exceed 0.5 percent when the temperatures were expressed in degrees Rankine. Calibration data are shown in Figures E-9a and b.

DRY GAS THERMOMETERS

The dry gas thermometers were calibrated by comparison against an ASTM-2F thermometer at approximately 32°F, at ambient temperature, and at approximately 110°F. The thermometers agreed within 5°F of the reference thermometer. The impinger thermometers were calibrated by comparison against ASTM-2F thermometer at approximately 32°F and ambient temperature. Calibration data are included in Figures E-10a through d and E-11a through d.

Date: 6/3/80 Thermocouple No.: 178
 Ambient temperature: 72 °F Barometric pressure: 29.35 " Hg.
 Calibrator: D. Armstrong Reference: Thermocouple #139

Reference point No.	Source,* (specify)	Reference thermometer temperature, °F***	Thermocouple temperature, °F	Difference, %**
1	2	72 (72)	71	0.19
2	1	38 (39)	39	0.00
3	3	95 (94)	95	-0.18
4	3	445 (429)	455	-2.92

Correction factor****: Slope: 0.9335 Intercept: 4.5

Reference point No.	Reference thermometer temperature, °F	Corrected thermocouple temperature, °F	Difference, %**
1	72	71	0.19
2	39	41	-0.40
3	94	93	0.18
4	429	429	0.00

Critical test points are 32°, 100°, and 500°.

*Source: 1) Ice bath
 2) Ambient
 3) Furnace

**Percent difference

$$\frac{\text{Reference temp. } ^\circ\text{F} - \text{thermocouple temp. } ^\circ\text{F}}{(\text{Reference temp. } ^\circ\text{F} + 460^\circ\text{F})} \times 100.$$

Each percent difference must be less than or equal to 1.5%.

***Reference thermometer must be ASTM.

****Correction factor must be determined if any percent difference is >1.5%.

Figure E-8a. Thermocouple calibration data sheet.

Date: 5/13/80 Thermocouple No.: 206
 Ambient temperature: 73 °F Barometric pressure: 29.24 " Hg
 Calibrator: Jim Iversen Reference: ASTM-2F

Reference point No.	Source,* (specify)	Reference thermometer temperature, °F***	Thermocouple temperature, °F	Difference, %**
1	2	73	75	-0.38
2	1	35	34	0.20
3	3	118	111	1.21
4	3	455	434	1.15

Correction factor****: Slope: _____ Intercept: _____

Reference point No.	Reference thermometer temperature, °F	Corrected thermocouple temperature, °F	Difference, %**

Critical test points are 32°, 100°, and 500°.

*Source: 1) Ice bath
 2) Ambient
 3) Furnace

**Percent difference

$$\frac{\text{Reference temp. } ^\circ\text{F} - \text{thermocouple temp. } ^\circ\text{F}}{(\text{Reference temp. } ^\circ\text{F} + 460^\circ\text{F})} \times 100\%$$

Each percent difference must be less than or equal to 1.5%.

***Reference thermometer must be ASTM.

****Correction factor must be determined if any percent difference is >1.5%.

Figure E-8b. Thermocouple calibration data sheet.

Date Nov. 15, 1952 Indicator No. #124 Operator David R. Fitzgerald

Test Point No.	Millivolt signal*	Equivalent temperature, °F*	Digital indicator temperature reading, °F	Difference, %
0	**	76	73.8	0.41%
1		32.0	30.6	0.28%
2		102.2	100.1	0.37%
3		451.1	450.1	0.11%
4		1127.0	1129.5	0.16%

Percent difference must be less than or equal to 0.5%.

Percent difference:

$$\frac{(\text{Equivalent temperature } ^\circ\text{R} - \text{Digital indicator temperature reading } ^\circ\text{R})(100\%)}{(\text{Equivalent temperature } ^\circ\text{R})}$$

Where $^\circ\text{R} = ^\circ\text{F} + 460^\circ\text{F}$

*See thermocouple digital indicator calibration verification device calibration for these values.

**This point is ambient temperature. The device is off and therefore is supplying no signal other than ambient temperature.

Figure E-9a. Thermocouple digital indicator calibration data sheet.

Date Nov. 18, 1982 Indicator No. #125 Operator Charles E. Fitzgerald

Test Point No.	Millivolt signal*	Equivalent temperature, °F*	Digital indicator temperature reading, °F	Difference, %
0	**	75	74.4	0.11%
1		32.0	31.6	0.08%
2		102.2	100.9	0.23%
3		451.1	449.9	0.13%
4		1127.0	1127.3	-0.02%

Percent difference must be less than or equal to 0.5%.

Percent difference:

$$\frac{(\text{Equivalent temperature } ^\circ\text{R} - \text{Digital indicator temperature reading } ^\circ\text{R})(100\%)}{(\text{Equivalent temperature } ^\circ\text{R})}$$

Where $^\circ\text{R} = ^\circ\text{F} + 460^\circ\text{F}$

*See thermocouple digital indicator calibration verification device calibration for these values.

**This point is ambient temperature. The device is off and therefore is supplying no signal other than ambient temperature.

Figure E-9b. Thermocouple digital indicator calibration data sheet.

Date: 6/10/80 Meter Box No.: FB-4

Calibrator: B. Armstrong Reference: ASTM-2F

Inlet

Reference point No.	Source *	Reference thermometer temperature, °F	Dry gas thermometer temperature, °F	Difference, °F**
1	2	72.0	72	0.0
2	1	32.7	32	0.7
3	3	117.0	114	3.0

Outlet

Reference point No.	Source *	Reference thermometer temperature, °F	Dry gas thermometer temperature, °F	Difference, °F**
1	2	72.0	73	1.0
2	1	32.7	34	1.3
3	3	116.0	115	1.0

*Source: 1) Ice bath
2) Ambient
3) Water bath

**Difference must be less than or equal to $\pm 5^{\circ}\text{F}$.

Figure E-10a. Dry gas thermometer calibration data sheet.

Date: 6/10/80 Meter Box No.: FB-5

Calibrator: B. Armstrong Reference: ASTM-2F

Inlet

Reference point No.	Source *	Reference thermometer temperature, °F	Dry gas thermometer temperature, °F	Difference, °F**
1	2	72.0	76	4.0
2	1	32.7	35	2.3
3	3	108.0	106	2.0

Outlet

Reference point No.	Source *	Reference thermometer temperature, °F	Dry gas thermometer temperature, °F	Difference, °F**
1	2	72.0	73	1.0
2	1	32.7	34	1.3
3	3	117.5	115	2.5

*Source: 1) Ice bath
2) Ambient
3) Water bath

**Difference must be less than or equal to $\pm 5^{\circ}\text{F}$.

Figure E-10b. Dry gas thermometer calibration data sheet.

Date: 6/10/80Meter Box No.: FB-6Calibrator: B. ArmstrongReference: ASTM-2F

Inlet

Reference point No.	Source *	Reference thermometer temperature, °F	Dry gas thermometer temperature, °F	Difference, °F**
1	2	72.0	72	0.0
2	1	32.7	32	0.7
3	3	115.0	114	1.0

Outlet

Reference point No.	Source *	Reference thermometer temperature, °F	Dry gas thermometer temperature, °F	Difference, °F**
1	2	72.0	73	1.0
2	1	32.7	32	0.7
3	3	119.0	116	3.0

*Source: 1) Ice bath
2) Ambient
3) Water bath

**Difference must be less than or equal to $\pm 5^{\circ}\text{F}$.

Figure E-10c. Dry gas thermometer calibration data sheet.

Date: 6/11/80 Meter Box No.: FB-7

Calibrator: B. Armstrong Reference: ASTM-2F

Inlet

Reference point No.	Source *	Reference thermometer temperature, °F	Dry gas thermometer temperature, °F	Difference, °F**
1	2	72.0	76	4.0
2	1	33.5	38	4.5
3	3	119.0	117	2.0

Outlet

Reference point No.	Source *	Reference thermometer temperature, °F	Dry gas thermometer temperature, °F	Difference, °F**
1	2	72.0	72	0.0
2	1	37.3	37	0.3
3	3	117.0	113	4.0

*Source: 1) Ice bath
2) Ambient
3) Water bath

**Difference must be less than or equal to $\pm 5^{\circ}\text{F}$.

Figure E-10d. Dry gas thermometer calibration data sheet.

Date: 12/16/82 Thermometer No.: #447
 Ambient temperature: 75° °F Impinger: ✓ NO_x:
 Calibrator: R. ANTISBERGER Reference: ASTM-3F

Reference point No.	Source *	Reference thermometer temperature, °F	Thermometer temperature, °F	Difference, °F**
1	2	75°	73°	2°
2	1	34°	32°	2°

*Source: 1) Ice Bath
 2) Ambient

**Difference must be less than $\pm 2^{\circ}\text{F}$ at both points

Figure E-11a. Thermometer calibration data sheet.

Date: 12/16/82 Thermometer No.: #448
 Ambient temperature: 75° °F Impinger: ✓ NO_x:
 Calibrator: R. ANTESBERGER Reference: ASTM-3 F

Reference point No.	Source *	Reference thermometer temperature, °F	Thermometer temperature, °F	Difference, °F**
1	2	<u>75°</u>	<u>73°</u>	<u>2°</u>
2	1	<u>34°</u>	<u>33°</u>	<u>1°</u>

*Source: 1) Ice Bath
 2) Ambient

**Difference must be less than ±2°F at both points

Figure E-11b. Thermometer calibration data sheet.

Date: 12/16/20 Thermometer No.: #449
 Ambient temperature: 75° °F Impinger: ✓ NO_x:
 Calibrator: E. Antares, Inc. Reference: ASTM-31

Reference point No.	Source *	Reference thermometer temperature, °F	Thermometer temperature, °F	Difference, °F**
1	2	75°	74°	1°
2	1	37°	32°	2°

*Source: 1) Ice Bath
 2) Ambient

**Difference must be less than $\pm 2^{\circ}\text{F}$ at both points

Figure E-11c. Thermometer calibration data sheet.

Date: 12/16/82 Thermometer No.: # 450
 Ambient temperature: 75° °F Impinger: ✓ NO_x:
 Calibrator: Z. ANTISBERGER Reference: ASIM-3F

Reference point No.	Source *	Reference thermometer temperature, °F	Thermometer temperature, °F	Difference, °F**
1	2	75°	77°	2°
2	1	34°	36°	2°

*Source: 1) Ice Bath
 2) Ambient

**Difference must be less than $\pm 2^{\circ}\text{F}$ at both points

Figure E-11d. Thermometer calibration data sheet.

BALANCE

The Mettler electronic balance was calibrated by comparison with Class-S standard weights and agreed within 0.5 g. Calibration data are shown in Figure E-12.

BAROMETER

The field barometer was calibrated to within 0.1 in.Hg of an NBS-traceable mercury-in-glass barometer before each test series. The field barometer was checked against the mercury-in-glass barometer after each test series to determine if it read within 0.2 in.Hg. If it did not reading within 0.2 in.Hg, a correction factor was determined. Calibration data are included in Figure E-13.

ORSAT ANALYZER

The orsat analyzer was calibrated before each test series by determining the percentages of carbon dioxide and oxygen in a calibration gas containing known percentages of each. The analyzer read within 0.5 percent of the known value for each gas. Calibration data are shown in Figures E-14a through c.

Balance No.	Date	Calibrator	Mass determined for					
			5 g 200	Error	50 g 500	Error	100 g 1000	Error
M-1*	12/7/82	D. Osterhout	200.1	+0.1	500.2	+0.2	1000.4	+0.4
M-1*	2/7/83	D. Schiffel	199.8	-0.2	499.5	-0.5	50g 499	-0.1

Error must not exceed 0.5 grams at each point.

* Balance was also calibrated by manufacturer on 10/6/82.

Figure E-12. Trip balance calibration data sheet.

BAROMETER NO.	#317	#226	#229	#317	#227		
PRETEST	5250 Waterbury	5261 D.F. Goodrich	3630-5 USEPA	5202 Medical Center	ATC DOWA		
BAROMETER READING	29.62	29.51	28.70	29.45	29.64		
REFERENCE BAROMETER READING	29.62	29.52	28.68	29.49	29.64		
DIFFERENCE*	0.00	0.01	0.02	0.03	.00		
DATE	1-27-83	1-29-83	2-2-83	2-10-83	2-18-83		
CALIBRATOR	J-I	MDF	MDF	Self	RMA		

POST-TEST

BAROMETER READING	29.45	29.09	29.60				
REFERENCE BAROMETER READING	29.40	29.06	29.59				
DIFFERENCE**	.05	0.03	.01				
DATE	2-10-83	2-3-83	2-18-83				
CALIBRATOR	MDF	Self	Self				

*Barometer is adjusted so that difference does not exceed 0.05 in. Hg.

**Barometer is not adjusted. If difference exceed 0.10 in. Hg, inform project manager immediately.

Figure E-13. Barometer calibration log.

Reference Gas: AGA Burdox
 Cylinder No. 112704
 Invoice No. 0382088
 Lab Ref. No. VII:46-23

Orsat No.: 141 Gas (circle one): O₂ (CO₂) CO

Calibrator	Date	Value Det.
D. Schaff	10-11-82	4.8
P. AUESBERGER	11/20/82	4.7
P. AUESBERGER	12/3/82	4.6
W. G. [unclear]	2-7-83	4.5

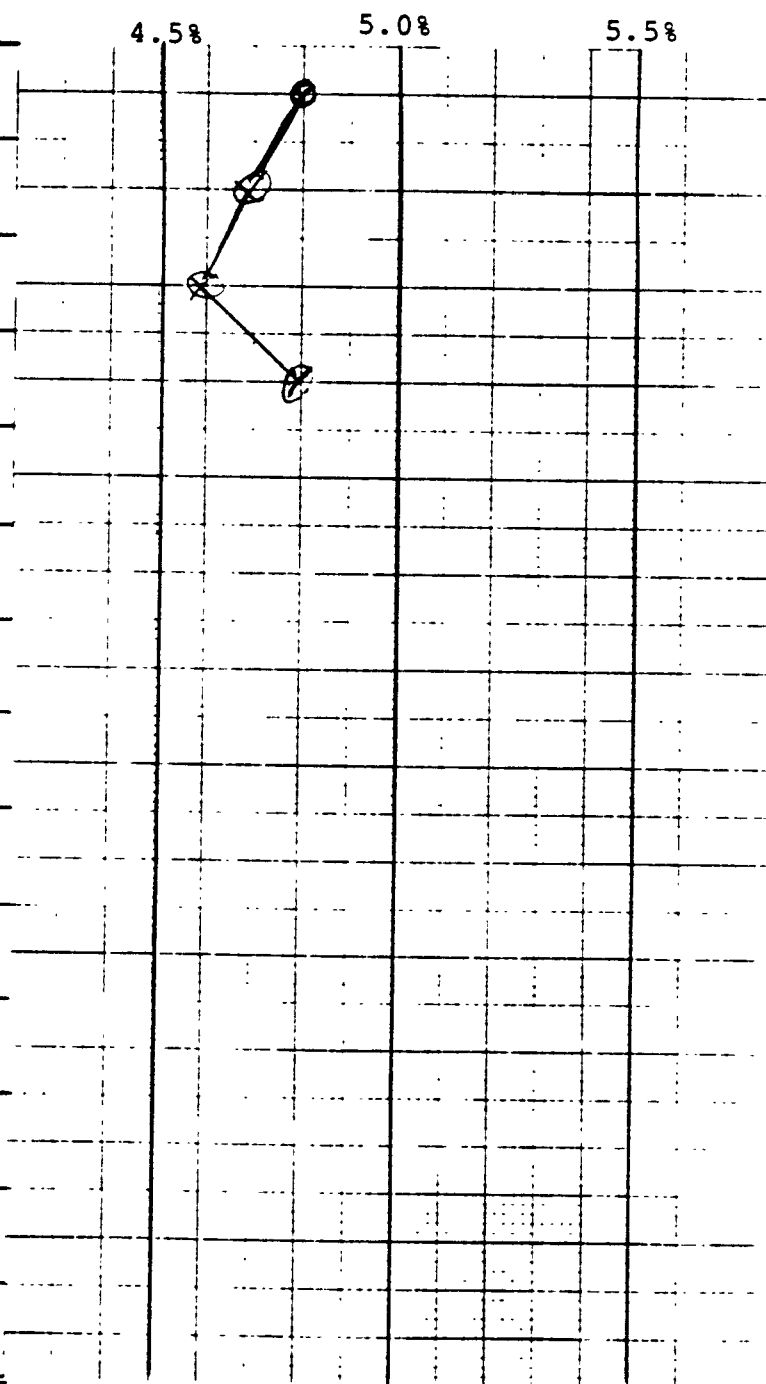


Figure E-14a. Orsat calibration data sheet - CO₂.

Reference Gas: AGA Burdox
 Cylinder No. 112704
 Invoice No. 0382088
 Lab Ref. No. VII:46-23

Orsat No.: 21 Gas (circle one): O₂ CO₂ CO

Calibrator	Date	Value Det.
K. Schaff	10-11-82	4.8
P. Antezberger	11/20/82	5.4
P. Antezberger	12/23/82	4.6
C. G. H. K.	2-2-83	5.2

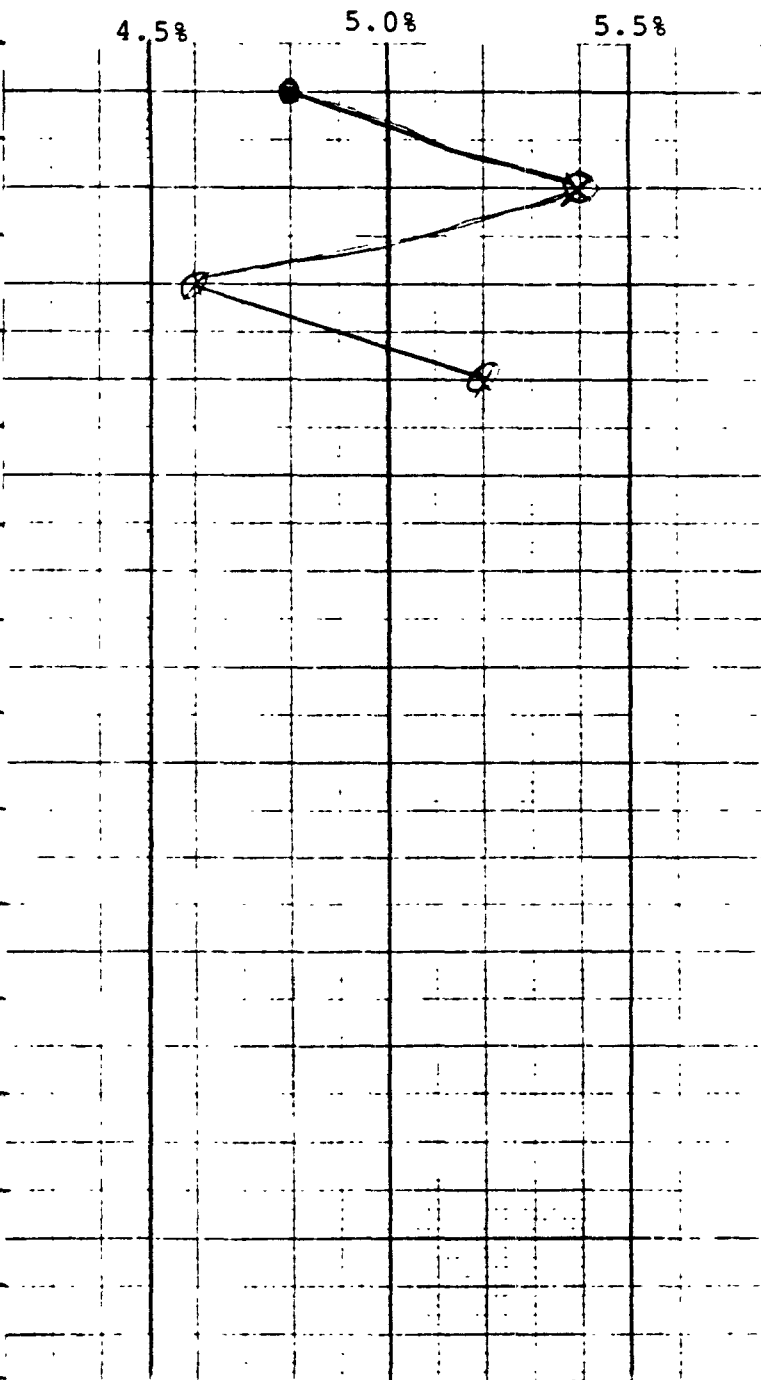


Figure E-14b. Orsat calibration data sheet - O₂.

Orsat No.: 121 Gas (circle one): O₂ CO₂ (CO)

[illegible]

E-37

APPENDIX F
QUALITY ASSURANCE SUMMARY

QUALITY ASSURANCE

The following summary addresses the general steps taken to insure data quality and accuracy for any given emission test project.

PROJECT ORGANIZATION AND RESPONSIBILITIES

The project organization and responsibilities of the project team are generally defined in the test plan. Specific responsibilities for this field test are shown in Appendix G, Project Participants.

QUALITY ASSURANCE OBJECTIVE

The primary objective of this program is to refine sampling and analytical techniques of EPA Proposed Method 5B (or develop a new method) that will minimize the collection of condensible sulfate materials in the measurement of particulate emissions from fossil fuel-fired boilers and to evaluate method precision. Therefore, all procedures used in the collection and analysis of emission samples were as outlined in applicable EPA reference methods, where applicable. The sample methodology used for this project (quad train - single point) has been previously validated specifically for research and methods development type projects.

Test results were presented in several units to allow for their comparison with data from other organizations wishing access to the data summary.

DATA REDUCTION, VALIDATION, AND REPORTING

Data reduction and reporting provide one of the greatest potential sources of system error. To help minimize this source of error, PEDCo performs most test method calculations by use of a validated computer program. In addition, hand calculation on standard computer cards to allow accurate input of data into the computer by individuals unfamiliar with testing procedures. The data printout is then validated by comparison with the field and analytical data sheets. In addition, hand calculation checks generally are made to validate the computer output. Other data validations are made whenever possible.

PERFORMANCE AND SYSTEM AUDITS AND FREQUENCY

When feasible, PEDCo performs both performance and system audits. Three types of performance audits were performed for this test program. All dry gas meter systems were audited for accuracy in the field by the use of a critical orifice. In addition, the analytical procedure for sulfur dioxide was audited for accuracy by the use of audit samples supplied by EPA prior to sample analysis. Also, onsite calculations were used to check the completeness and accuracy of the particulate test data.

The PEDCo Project Director was on-site February 11 and performed a general system audit as an internal evaluation of

sampling personnel and equipment. The EMB Task Manager was also on-site during the major portion of the test series and performed a separate system audit.

SPECIFIC ROUTINE PROCEDURES USED TO ASSESS DATA PRECISION, ACCURACY, AND COMPLETENESS

Because the precision of the standard EPA reference methods used had previously been determined, no further attempt was made to assess data precision. These precision results are summarized in "The EPA Program for the Standardization of Stationary Source Emission Test Methodology, A Review," EPA-600/4-76-044. Precision estimates were calculated for within-run M5B and M5B-P400 samples using standard statistical analysis procedures. The mean concentration and standard deviation (with N-1 weightings for sample data) were determined for each group of similar runs. The standard deviations were expressed as a percentage of the mean concentration for comparison purposes (called the relative standard deviation).

Three audit procedures were used to determine accuracy. Accuracy audit procedures used for the dry gas meter and sulfur dioxide, analysis are the standardized written procedures used by the EPA Quality Assurance Division program. The procedure for determining data completeness is the same as that for New Source Performance Standards, as documented in the Code of Federal Registers 40 CFR 60, Section 60.8

INTERNAL QUALITY CONTROL CHECKS

Several internal quality control checks are usually made for each test. Normally, most of these checks deal with the field sampling analysis. For this test series, control samples for the sulfur dioxide analytical procedures were analyzed. Also, filter and reagent blanks were returned to the laboratory for gravimetric analysis. A quality control check of both the initial and final weighing was thus provided. Results of the control sample checks are included in Section 6. Blanks were analyzed according to procedures used for the M5BW and IC analytical work.

CORRECTIVE ACTION

PEDCo has two methods for corrective action. The first involves the use of control limits, such as audit sample results, control sample results, and calibration results. When any of these limits show that the integrity of the data is questionable the procedure is repeated, additional data are collected, or the data are rejected. The second method involves the use of red tags. Whenever any piece of equipment is suspected of producing unacceptable data, the entire apparatus or malfunctioning component is replaced and a red tag is placed on the item. That piece of equipment is then rejected until its ability to perform its function correctly is verified by the proper individuals. The use of numerous control limits and the red tagging system reduces the amount of unacceptable data and provides a system by which to track and correct items and procedures that show an unusually high occurrence of unacceptability.

PREVENTIVE MAINTENANCE PROCEDURES AND SCHEDULES

PEDCo has a very comprehensive preventive maintenance program. Many of the major components of test equipment have pre-test checklists. These checklists ensure that all functions are checked and action is taken to repair or replace any part that shows probability of malfunction. The checks are made before every field test series, however, only the control console (meter box) check are recorded. Even though PEDCo's preventive maintenance program and schedule are not in writing, our commitment of three full-time experienced persons for the express purpose of equipment construction, preparation, calibration, and maintenance has created a program based on experience and skill that cannot be matched by a written guideline.

QUALITY ASSURANCE REPORTS TO MANAGEMENT

The standard quality assurance procedures used in this test program generated sufficient documentation to indicate the data quality. All evidence of the execution of the quality assurance guidelines is reviewed by management. In addition, during weekly meetings of all PEDCo's EMB task managers and project managers, all aspects of the project are discussed including the quality assurance of each task. No written report results from this meeting because all interested parties are verbally apprised of the situation during each meeting.

Two other reports are made to managements, which are not EMB task related. PEDCo's emission test and laboratory groups participants in all national audits by EPA's Quality Assurance Division, and PEDCo's quality assurance coordinator, Tom Wagner, makes several independent checks for management.

APPENDIX G
PROJECT PARTICIPANTS AND SAMPLE LOG

TABLE G-1. FIELD TEST CREW AND RESPONSIBILITIES

Name	Title	Field test assignment
J. Prohaska	Project Manager	Coordinate test activity; sample train setup and disassembly
P. Clarke	Engineer	Site leader; particulate tests meter reader quad train
P. Reinermann	Engineer	Particulate tests meter reader quad train
R. Antesberger	Technician	Assist at sample site; quad train assembly and disassembly
D. Osterhout	Engineer	Site leader; clean up area; setup and recover sample trains
D. Scheffel	Technician	Setup and recover sample trains; Orsat analysis
W. DeWees	Project Director	System audit
G. McAlister	EPA Task Manager	Monitor test performance
J. Sellers	Plant contact	Coordinate plant activities; provide general on-site assistance; record process data
A. Kasprik	Company contact	Project coordination

TABLE G-2. SAMPLE LOG

Date (1983)	Activities
February 5-6	Sample site and equipment setup. All initial measurements were obtained. Sample recovery and setup area organized.
February 7-8	Two test runs were performed daily.
February 9-10	No tests were performed. Boiler operated at reduced load because of malfunctioning condensate pump.
February 11	Four test runs were performed. System audit conducted.
February 12	Two test runs were performed. Packed equipment and left site.

APPENDIX H
PROCESS DATA

Date 2-7-83

Run No. 1

POD No. 2

Heller

PLANT OPERATIONAL DATA

PEDC. Test

Time	10 am	11:10 am
Used	379	378
Number of Oil Burners	18	18
Opacity Monitor (6 min. average)	21%	21%
Oil Temp. to Burners (°F.)	260°	260°

	E	W		
Oxygen at Economizer Exit (%)	Teledyne .9	.5	.9	.8
	Barley .9	.4	1.0	.5
Combustibles (%)	0	0	0	0
Carbon Monoxide (ppm)	not available			

Remarks

3

PEDC. Test

7-11-5

Ther...

PEDC. Test

7. 2.2×10^{-10} LOSS OF AIR LIGHT + ENDSCHNITT - 0.5 1.5 - 1.0 1.5

Date 6-11-52

Run No. 5

DOC No. 2

PLANT OPERATIONAL DATA

PEDC. Test

[illegible]

Results

H-6

ACC No. 2

PLANT OPERATIONAL DATA

PEDC. Test

[illegible]

References

Date 11-72

Run No. 71

PCC No. 2

PLANT OPERATIONAL DATA

PEDC. Test

[illegible]

REMARKS 1. 2. 3. 4. 5. 6. 7. 8. 9. 10. 11. 12.

Run No. 5

Vol. 2

PEDC. Test

Part 1: _____

Date _____

Run No. _____

PEDC No. 2

PLANT OPERATIONAL DATA

PEDC Test

Time	7:00	9:35		
Load	325	380		
Number of Oil Burners		18		
Opacity Monitor (6 min. average)	50%	20%		
Oil Temp. to Burners (°F.)	250	259		
Oxygen at Economizer Exit (%)	7	5	5	5
Combustibles (%)		0	0	
Carbon Monoxide (ppm)				
Remarks				

Run No. _____

100. 2.

PEDC. Test

Facts

Sheet 2,1

POWER RESOURCES LABORATORY
9250 W FLAGLER STREET
PO BOX 529100
MIAMI, FLORIDA 33152

ANALYSIS OF FUEL OIL FIRED
JANUARY 1982

DATE SAMPLE RECEIVED AT LABORATORY	1/20/82
API GRAVITY	13.2
DENSITY, LB/GAL	8.144
DENSITY, LB/BL	342.048
HEAT OF COMBUSTION, B/LB	18300
HEAT OF COMBUSTION, B/GAL	149000
HEAT OF COMBUSTION, MB/BL	6259
WATER, % BY VOLUME	0.40
SEDIMENT, % BY WEIGHT	0.01
SULFUR, % BY WEIGHT	2.30
SULFUR DIOXIDE EQUIVALENT, LB/MT	2.51
ASH, % BY WEIGHT	0.10
PARTICULATE EQUIVALENT, LB/MT	0.06
Vanadium IN ASH AS V2O5, % BY WEIGHT	67.
Vanadium IN OIL AS V2O5, PPM	700.
Vanadium IN OIL AS V, PPM	392.
VISCOSITY, SSF AT 122 F	225
ASPHALTENES, % BY WEIGHT	7.5

ANALYSIS CERTIFIED BY

JANUARY 27, 1982

D. Knutson

ORIGINAL TO: E G JONES
COPIES TO: L L WILLIAMS
E F GILBERT
A D SCHMITT
C D HENDERSON

Figure H-1. Typical fuel oil analysis.

TECHNICAL REPORT DATA
(Please read Instructions on the reverse before completing)

1. REPORT NO. EPA-450/3-84-007	2.	3. RECIPIENT'S ACCESSION NO.
4. TITLE AND SUBTITLE Evaluation of Method 5B at an Oil-Fired Boiler	5. REPORT DATE January 1984	6. PERFORMING ORGANIZATION CODE
7. AUTHOR(S) John Prohaska	8. PERFORMING ORGANIZATION REPORT NO.	
9. PERFORMING ORGANIZATION NAME AND ADDRESS PEDCo Environmental, Inc. 11499 Chester Road, Post Office Box 46100 Cincinnati, Ohio 45246 - 0100	10. PROGRAM ELEMENT NO.	11. CONTRACT/GRANT NO.
12. SPONSORING AGENCY NAME AND ADDRESS Emission Measurement Branch Emission Standards and Engineering Division U.S. Environmental Protection Agency Research Triangle Park, N.C. 27711	13. TYPE OF REPORT AND PERIOD COVERED	14. SPONSORING AGENCY CODE EPA/200/400
15. SUPPLEMENTARY NOTES		

16. ABSTRACT

This report describes the development and evaluation of Method 5B at an oil-fired boiler. Different sampling and analysis techniques for measuring nonsulfuric acid particulate matter were compared and evaluated. Statistical analyses of the results comparing the precision of the different techniques are presented.

KEY WORDS AND DOCUMENT ANALYSIS

DESCRIPTORS	b. IDENTIFIERS/OPEN ENDED TERMS	c. COSATI Field/Group
		13 B
17. DISTRIBUTION STATEMENT	19. SECURITY CLASS (This Report)	21. NO. OF PAGES 499
	20. SECURITY CLASS (This page)	22. PRICE