Research and Development

EPA/600/S7-90/015 Jan. 1991

EPA

Project Summary

Costs for Advanced Coal Combustion Technologies

J.A. Martinez, G.C. Snow, and M. Maibodi

This project was undertaken to evaluate the development status of advanced coal combustion technologies and to prepare performance and economic models for their application to electric utility plants. The technologies addressed were atmospheric fluidized bed combustion (AFBC), pressurized fluidized bed combustion (PFBC), and integrated gasification combined cycle (IGCC). The development status was also reviewed for pulverized coal-fired boilers incorporating supercritical steam cycles. Although advanced combustion technologies are attractive due to decreased SO₂ and NO₃ emission characteristics and potentially higher generating efficiencies, full commercial readiness does not appear feasible before the mid to late 1990s. Capital cost estimates for a new plant at 500-MW ranged from \$1,250 to \$1,910/kW (in 1988 dollars) for the advanced technologies and from \$1,380 to \$1,810/kW for the conventional systems. Capital cost estimates for PFBC (turbocharged cycle) and conventional plants with add-on SO, and NO controls were within 4 % of the median cost (\$1,580/kW) of all of technologies evaluated. AFBC costs averaged 12% less than this median while integrated gasification combined cycle costs averaged 11% above the median. Potential capital cost savings for repowering an existing plant versus constructing a new facility at the same final capacity are between 10 and 40%.

This Project Summary was developed by EPA's Air and Energy Engineering Research Laboratory, Research Triangle Park, NC, to announce key findings of the research project that is fully documented in a separate report of the same title (see Project Report ordering information at back.)

Introduction

This report documents performance and economic models developed for advanced coal combustion and conventional power generation technologies. The models developed in this report are simplified to minimized computational time and data requirements, but they incorporate important parameters that have significant impacts on performance and costs. The models are based on recent information available from Electric Power Research Institute (EPRI) reports and other published sources. The sources of information are referenced in the report.

The advanced power generation technologies covered in the report include: atmospheric fluidized bed combustion (AFBC), pressurized fluidized bed combustion (PFBC), and integrated gasification combined cycle (IGCC). These technologies incorporate processes for removal of sulfur dioxide (SO₂), nitrogen oxides (NO_x), and particulate matter (PM).

The conventional power generation technology covered in the report is pulverized coal-fired (PC) plants. The economic model developed in this study for PC plants excludes the costs for flue gas desulfurization (FGD) and selective catalytic reduction (SCR) NO, controls. The costs for these control systems were drawn from other models and were combined with the PC base plant costs. The user has the option to include or exclude the cost of a baghouse for PM control. As such, the user of the model can add the desired control options to the uncontrolled PC boiler and compare the cost of a PC plant with those estimated for the advanced coal combustion technolo-



Table 1 describes the technologies covered in this study. The FGD configuration described has been considered as the EPA "base case" system. The SCR system is a hot-side, high-ash configuration, located upstream of the air heater. The nominal NO removal efficiency for this system is estimated at 75%. The advanced technologies-AFBC, PFBC, and IGCC—are near-term or first generation versions of each system. Both the AFBC and PFBC combustors are of the bubbling bed design. The PFBC reference plant is a turbocharged design and does not include a gas turbine generator for combined cycle electricity production. The IGCC reference plant utilizes an oxygen-blown, entrained-flow gasifier with cold gas cleanup prior to combustion turbine firing.

Although both conventional and advanced technologies have been evaluated in this study, direct economic comparisons are difficult for several reasons. First, a technology such as FGD is mature and fully commercialized with many vendors competing in the marketplace. Therefore, cost estimates for FGD systems are developed from a data base of actual installation and operating costs. In contrast, the advanced technologies, particularly PFBC and IGCC, are in relatively early stages of development with commercial service unlikely before the mid to late1990s. Cost estimates made during such early stages of development can significantly underpredict actual costs for the first commercial version of a new technology. However, costs for subsequent commercial installations often decline as improved versions of the technology are

T- -1 -- 1- --

built. Second, the cost effectiveness (cost to remove a given quantity of pollutant) is much easier to define for an add-on control such as FGD or SCR than for integrated technologies. To varying degrees, processes for removal of SO₂, NO_x, and PM are intrinsic to the basic designs of the advanced generating technologies. Finally, advanced technologies may offer significant capacity increases and increased fuels flexibility when retrofitting or repowering existing plants. These features also need to be considered when comparing technologies.

For each technology covered, the following information is presented:

- description of the technology,
- reference plant description defining the coverage of process equipment included in the cost models,
- system performance models relating to emission reduction,
- capital cost model,
- operating and maintenance cost model, and
- key technical issues discussion dealing with technical factors that will affect further development and use of the technology.

Summary and Results

Algorithms for the performance and economic models are presented in the report. These algorithms have also been incorporated in Version 4.0 of the Integrated Air Pollution Control System (IAPCS) cost model. Version 4.0 of IAPCS was used to generate the cost presented herein.

Example cost estimates are presented for newly constructed AFBC, PFBC, and IGCC plants as well as for new PC plants equipped with wet limestone FGD and SCR systems. These capital and operating cost estimates are based on early or near-term versions of the advanced technologies. As the advanced technologies are developed further, revised capital cost estimates may either increase or decrease. Revised annual operating cost estimates, however are likely to decrease as more efficient versions of the technologies are evaluated. Cost estimates are also presented for repowering existing PC plants with advanced coal combustion technologies. To compare the repowering approaches, cost estimates are presented for life extension and retrofit of existing PC plants. Equipment refurbishment and upgrade costs associated with a 20-year life extension were combined with retrofit FGD and SCR costs for existing

Status of Advanced Coal Combustion Technologies

Advanced coal combustion technologies have received considerable attention because of decreased SO₂ and NO_x emissions characteristics, potential improvements in overall generating efficiency, and the ability to increase generating capacity when repowering existing stations. Table 2 compares net plant generating efficiencies which are available currently or on a near-term basis against projected efficiency for mature or second generation configurations for the technologies considered. Cur-

Table 1. General Descriptions of the Technologies Considered

| Technol | gy Process Description |
|---------|---|
| FGD | Forced oxidation wet limestone with in-line steam reheat; spray tower type absorber modules with liquid/ gas ratio of 80 gpm/1000 acfm*; three modules are assumed for 200 and 500 MWe plants, and four modules are assumed for 1000 MWe plants; sludge disposal is by landfill. |
| SCR | Hot-side location between economizer and air heater; economizer bypass to maintain nominal catalyst temperature of 700 °F at low load operation; air heater modifications to resist impact of ammonia salt formation; vertical reactor vessels with fly ash hopper and handling systems; complete catalyst replacement at 3-year intervals. |
| AFBC | Bubbling bed combustor; limestone sorbent; overbed coal and limestone feed system; dry waste disposal by landfill. |
| PFBC | Bubbling bed combustor; dolomite sorbent; underbed coal and sorbent feed system; turbocharged cycle; dry waste disposal by landfill. |
| IGCC | Texaco entrained flow gasifier; oxygen blown; radiative and convective raw gas cooler; cold gas cleanup by Selexol acid gas removal; Claus sulfur recovery; SCOT tail gas treatment; turbine firing temperature 2200 °F. |

^{*}Readers more familiar with metric units may use the factors at the end of this Summary to convert to that system.

Table 2. Net Plant Generating Efficienciesa

| Technology C | Current or Near-Term Efficiency % | Mature Technology Projected Efficiency | % |
|-----------------------|--------------------------------------|---|---|
| Conventional PC/FGD | 33-35 | 35 | |
| Supercritical PC/FGD | . 39 | 41 | |
| AFBC | <i>34</i> | <i>35</i> | |
| PFBC (Turbocharged C) | rcle) 33 | <i>35</i> | |
| PFBC (Combined Cycle) |) 34 | 45 | |
| IGCC . | 34 | 40 | |

^aNet plant efficiency is the inverse of net plant heat rate times the conversion factor, 3413 Btu/kWh.

rent or near-term achievable efficiencies for advanced technologies show no improvement over conventional PC plants with FGD systems. However, projected efficiencies for mature (or second generation) versions of IGCC and PFBC are about 14-29% higher, respectively, than that achievable for the conventional system. Supercritical PC plants operate at steam cycle pressures above the critical pressure of water, but utilize an essentially conventional (low NO.) PC firing system and FGD scrubbers. Supercritical plants have been available in the U.S. since the late 1950s. However, due to materials-related reliability problems in the boiler superheater and reheater surfaces, main steam lines, and high pressure turbine valves, nozzle chambers, and casings, supercritical plants have not been fully commercialized. Near term net plant generating efficiencies of about 39% are based on the performance levels of the pre-NSPS Philadelphia Electric Company Eddystone No. 1 (Eddystone, Pennsylvania) and The Ohio Power Company Philo No. 6 (near Zanesville, Ohio) plants in the late 1950s and early 1960s. Proposed supercritical plant designs have efficiencies of about 41% or about 17-24% higher than current subcritical designs.

Advanced coal combustion technologies may also be used to repower existing steam electric plants. Repowering consists of substantial modification or replacement of the existing boiler. Where economically feasible, the existing steam turbine generator and the remaining balance-of-plant equipment is reused. In the combined cycle configurations of PFBC and IGCC, additional electricity is produced by a new gas turbine generator. Repowering cannot only provide a plant service life extension, but can also result in significant capacity increases without developing new greenfield power plant sites.

At their current status of development, however, advanced technologies may not be fully available for utility application until the mid to late 1990s. Significantly technical issues must be overcome before these technologies will fully penetrate the utility

market. These issues include materials limitations, process control, load following ability, hot gas cleanup, and secondary environmental impacts. Table 3 lists some of the major issues and provides time frame estimates of commercial availability for the technologies. The development issues and availability status of the advanced technologies are more fully discussed in the main report.

General Costing Assumptions

Assumptions used to estimate both constant and current 1988 dollars are shown in Table 4. EPRI's general cost procedures were used to incorporate inflation, cost of capital, and levelization of future expenses. Cost adjustments to account for the technical issues discussed above affecting further development and future use of each technology are not presented in this cost analysis.

Process contingencies are used to address the uncertainty associated with developing technologies while project contingencies reflect the level of detail in estimating overall project cost. In developing detailed cost estimates for a technology, process contingencies are determined for each process area or section according to its development and commercialization status. For example, in an IGCC plant, the steam turbine generator section is typically assigned a process contingency at or near

Table 3. Development and Availability Status of Advanced Coal Combustion Technologies

| | | Estimated Commercial Availability | | | |
|---------------------------|--|-----------------------------------|-----------------------------------|--|--|
| Technology | Key Technical Issues | First Generation | Fully Mature Second Generation | | |
| Supercritical PC/FGD | Superheater materials limitations Main steam line creep and expansion failure Steam turbine erosion, creep, and expansion failure Load following and control Plant trip critical pressure letdown | 1962 | 1993 | | |
| AFBC (Bubbling Bed) | Modest combustion efficiency Poor limestone utilization Part-load efficiency and emissions control Solid waste production Potential N ₂ O emissions | 1989 | 1995 | | |
| PFBC | Erosion-corrosion of in- bed heat transfer surfaces Load following and control Solid waste production Alkali and halogen emissions Potential N ₂ O emis- sions | 1995 | 2000 | | |
| IGCC | Solid waste production from insitu sulfur capture High temperature S, N, PM, and alkali removal High temperature gas turbine development | 1988 | 1996 | | |

| Table 4. Economic Assumptions Used in Cost Analysis | | | | | | | |
|---|-----------------------------|----------------|---|--|--|--|--|
| Current Dollars | (1988) | | • | | | | |
| Weighted Cost o Inflation Rate | f Capital | 12.5% 6.0 | 1 1 | | | | |
| Carrying Charge Economic Life: | | 0.189 0.175 | (Retrofit, Repowered Plants) (New Plants) | | | | |
| Levelization Fact | tor | | | | | | |
| Economic Life: | 20 years 30 years | 1.57 1.75 | | | | | |
| Current Dollars | (1988) | | | | | | |
| Weighted Cost o Inflation Rate | f Capital | 6.1% 0% | | | | | |
| Carrying Charge | Factor | r | | | | | |
| Economic Life: | 20 years | 0.123 | (Retrofit, Repowered Plants) | | | | |
| | 30 years | 0.105 | (New Plants) | | | | |
| Levelization Fac Economic Life: | tor 20 years 30 years | 1.00 1.00 | • | | | | |
| Indirect Cost | | Case 1 | Case 2 | | | | |
| General Facilitie | | 10% | 10% | | | | |
| Engineering and | l Home Office Fees | 10% | 10% | | | | |
| Process Conting Project Contings | | 10% 30% | 0% 15% | | | | |
| Froject Continge | 3110103 | 0070 | . 1070 | | | | |

zero. However, given that hot gas cleanup systems have generally not progressed from pilot demonstration scale to full commercial status, a process contingency within the range of 20-35% is more appropriate for this section. A weighted average of the process area contingencies can then be expressed for the technology.

A range of contingency values was used in the present costing analysis to represent optimistic as well as conservative estimates. Weighted average contingencies are shown in the analyses for each technology rather than individual process area contingencies. Contingencies of 0% for process and 15% for project are appropriate for mature processes and detailed project cost estimates. Contingencies of 30% for project and 10% for process give more conservative cost estimates corresponding to increased process uncertainties and reduced detail in project cost estimating. In other work, EPA has used a 15% contingency factor for the FGD base case estimate. Contingencies inherent to the example cost estimates contained in the 1986 Technical Assessment Guide (TAG) are on the order of 18-20% for AFBC and IGCC and are >30% for PFBC. As more experience is gained in some of the process areas and with improved project costing, these factors may be refined. Contingency factors developed by EPRI following detailed engineering and risk analyses currently fall within the range of 15-20% for

AFBC, IGCC, and PFBC. Each technology in this study has been evaluated using contingency values representing both optimistic and conservative premises.

Table 5 presents coal characteristics for a midwestern bituminous coal used in the cost analysis. To be consistent with an EPRI study of FBC, a coal cost of \$2.00/106 Btu was used for a hypothetical Illinois coal. (Note: Actual fuel costs may differ from this assumed price, thus affecting the relative economic ranking between the technologies. Higher fuel costs will have a greater impact on total annual operating costs for low efficiency technologies as compared to technologies with high generating efficiencies. Table 6 presents unit costs for estimating operating and maintenance costs. Annual costs were estimated using a capacity factor of 0.65. Costs are reported for technologies firing 2 or 4% sulfur coal.

Table 7 presents design specifications for acid gas control used to estimate costs for each technology. For SO, control, 90% removal is assumed for AFBC, PFBC, and FGD; 95% removal is assumed for IGCC. For NO control, a NO emission limit of 0.6 lb/10⁶ Btu corresponding to the current New Source Performance Standard (NSPS) level, is assumed for AFBC plants and PC plants without SCR. For PC plants with SCR, the design NO removal efficiency is assumed to be 80%, corresponding to an emission level of 0.12 lb/106 Btu. Measured NO emissions from a large demonstration PFBC boiler ranged from 0.15 to 0.5 lb/ 106 Btu. In this study, an NO, emission level of 0.2 lb/106 Btu is assumed based on conceptual bubbling bed PFBC performance levels. The NO emission level of 0.27 lb/ 106 Btu for IGCC is based on the use of wet injection in the gas turbine for complying with the gas turbine NSPS limit (75 ppm at 15% dry O₂).

Table 5. Coal Characteristics and Prices Used in the Cost Analysis

| Coal Characteristics | | Midwestern Bituminous Coal | |
|-----------------------|--|--|---|
| Sulfur Conte | nt. % | 2.0 - 4.0 | |
| Ash Content. | % | 16 | |
| Carbon Cont | | <i>57.6</i> | |
| Heating Value, Btu/lb | | 10,100 | • |
| | | of the second se | |
| | e for Conventional Plants D. Btu/kWh | 10,060 | |
| | te for Conventional Plants GD and SCR. Btu/kWhª | 10,160 | |
| | te for AFBC, Btu/kWh | 10.000 | |
| | te for PFBC, Btu/kWh | 10.278 | |
| | te for IGCC, Btu/kWh | 9,280 | |
| Coal Price | \$/ton | 40.0 | |
| | \$/10° Btu | 2.00 | |

^{*}Assumes that SCR will increase the net heat rate by 1% over that of conventional plants with FGD.

Table 6. Unit Costs for Estimating Operating and Maintenance Costs (1988 Dollars)

| Item | Units | Value | |
|------------------------|-------------|--------------|--|
| Operating Labor | \$/man-hour | 21.40 | |
| Water | \$/1000 gal | 0.65 | |
| Limestone and Dolomite | \$/ton | <i>16.30</i> | |
| Waste Disposal | \$/ton | 10 | |
| Sulfur | \$/ton | <i>65</i> | |
| Ammonia | \$/ton | 150 | |
| SCR Catalyst | \$/ton | 20.300 | |
| Steam | \$/10° Btu | 7.00 | |

New Plant Costs

Tables 8 and 9 present the capital and annual costs of new AFBC, PFBC, and IGCC plants firing 2 and 4% sulfur bituminous coals, respectively. The costs are reported for 200-, 500-, and 1000-MW plant sizes.

For comparison with advanced coal combustion costs, costs are also reported in Tables 8 and 9 for newly constructed PC plants with wet limestone FGD and SCR systems. Costs for new wet limestone FGD and SCR systems were estimated from the IAPCS model. The SCR costs are based on a 3-year catalyst life. Tables 8 and 9 include operating costs of conventional plants with baghouses for PM control. Annual costs of FGD and FGD plus SCR were added to the new plant costs so that the annual conventional plant cost can be compared directly with those for advanced coal combustion technologies.

The cost effectiveness, or unit cost per ton of acid gas removed is also presented for each technology in Tables 8 and 9. The tons of acid gas removed were determined by applying advanced technology removal efficiencies to emissions of NO, and SO, from an uncontrolled PC plant at given plant sizes. For integrated techologies, FBC and IGCC, it is difficult to separate costs associated with acid gas control from the rest of the costs attributed to electrical generation. To estimate effective costs for acid gas control for new plants, annual costs (including annualized capital costs) for the conventional PC plant exclusive of FGD and SCR costs systems were subtracted from annual costs (including annualized capital costs) for a new AFBC, PFBC, and IGCC plant at the same plant size. This is represented by the following equation:

(Effective acid gas control costs)

=(Annual cost for advanced technology)

(Annual cost for PC plant without FGD and SCR)

For conventional PC boilers, the cost for acid gas control is simply the annual costs for FGD and SCR.

Figures 1, 2, and 3 show the capital costs, annual costs, and unit cost per ton of acid gas removed from Table 8 as a function of plant sized for the 2% sulfur coal, respectively. Only constant 1988 dollar costs estimates and 30% for project and 10% for process contingencies are presented in these figures.

Repowered Plant Costs

Tables 10 and 11 present the capital and annual costs of repowering AFBC, PFBC, and IGCC on existing plants firing 2 and 4% sulfur bituminous coals, respectively. These costs are based on repowered plant final net capacity and are reported for 200-, 500-, and 1000-MW plant sizes. Whereas plant capacity is assumed to remain unchanged for AFBC and turbocharged PFBC repowering, it is assumed that IGCC repowering results in a tripling of net plant output.Capital costs are based on reuse and refurbishment factors for each technology. They do not however, include the costs for replacement power during the construction outage.

For comparison with costs of repowering, costs are also reported in Tables 10 and 11 for life extension of an existing plant for 20 years of additional operation and retrofit of add-on wet limestone FGD and SCR systems and fabric filter PM control. Retrofit of FGD and SCR systems results in decreased operating efficiency which may derate the plant. This analysis assumes that an FGD retrofit gives a 3% capacity derate and the addition of an SCR system gives another 1% derate. The capital cost of life extension is \$214/kW, which is the average cost reported by EPRI without considering downtime costs. Costs for wet limestone FGD systems were estimated from the IAPCS model. Capital costs for FGD and SCR systems are based on retrofit factors of 1.5 and 1.34, respectively, as shown in Table 7.

Conclusions

Advanced coal combustion technologies are of interest due to decreased SO. and NO, emissions characteristics, potential improvements in overall generating efficiency, and the ability to increases generating capacity when repowering existing stations. Existing NSPS emission limits and proposed acid rain regulations are expected to be met by most AFBC, PFBC, and IGCC configurations. In addition, prevention of significant deterioration (PSD) requirements are expected to be satisfied under repowering scenarios. Projected net plant generating efficiencies for mature technology combined cycle configurations (IGCC and PFBC) are about 14-29% higher than for conventional PC boilers equipped with FGD scrubbers. Advanced supercritical PC/FGD designs have generating efficiencies comparable to those of mature IGCC plants but still about 8-9% below those of second generation PFBC designs.

At their current status of development, however, advanced technologies may not be fully available for utility application until the mid to late 1990s. Significant technical issues must be overcome before these technologies will fully penetrate the utility market. These issues include materials limitations, process control, load following ability, hot gas cleanup, and secondary

environmental impacts.

Capital cost estimates for a new plant at 500-MW ranged from \$1,250 to \$1,910/kW for advanced technologies and from \$1,390 to \$1,810/kW for conventional systems. Capital cost estimates for PFBC (turbocharged cycle) and conventional plants with add-on SO₂ and NO_x controls were within 4% of the median cost (\$1,580/kW) of all of technologies evaluated. AFBC costs averaged 12% less than this median while IGCC costs averaged 11% above the median. Potential capital cost savings for repowering an existing plant versus constructing a new facility at the same final capacity are between 10 and 40%.

Metric Conversion Factors

Readers more familiar with metric units may use the following factors to convert to that system:

| British | Multiplied by | Yields Metric |
|------------|---------------|---------------|
| Btu | 1.06 | kJ |
| Btu/lb | 2.33 | kJ/kg |
| cfm | 0.000472 | m³/s |
| ۰F | 5/9 (°F - 32) | °C |
| gal. | 0.00379 | m³ |
| gpm | 0.0000633 | m³/s |
| Ĭb/10° Btu | 0.430 | lb/GJ |
| ton | 907 | kg |

Table 7. Design Specifications for Acid Gas Control

| Design | Specifications | |
|--------|----------------|--|
| | | |

| Technologies | Evaluated a |
|--------------|-------------|
|--------------|-------------|

| | AFBC | PFBC | IGCC | PC/FGD/SCR | PC/FGD | |
|--|---|--|--|---|---|--|
| SO ₂ Control: | | i | | | | |
| - SO ₂ Removal % - SO ₃ Control Method - Sorbent Type - Ca/S Ratio - L/G Ratio - Stoichiometric Ratio - Retrolit Factor ^b | 90 in-situ limestone 3.1 NA NA NA | 90 in-situ dolomite 1.5 NA NA | 95 Selexol Process Selexol NA ° NA NA NA | 90 wet limestone FGD limestone NA 80 1.15 1.5 | 90 wet limestone FGD limestone NA 80 1.15 1.5 | |
| lO _x Control: | | | | | 4 | |
| - NO, Emissions, lb/10°Btu - NO, Control Method - NH,: NO, Ratio - SCR Space Velocity, 1/hr - SCR Catalyst Replacement, years - Retrofit Factor b | 0.6 in-situ NA NA NA NA | 0.2 in-situ NA NA NA NA | 0.27 wet injection NA NA NA NA | 0.12 SCFI 0.82 25,000 3 1.34 | O.6 NA NA NA NA NA | |

^{*} AFBC PFBC IGCC

New Plant Cost Estimates for Advanced Coal Combustion Technologies Firing 2% Sulfur Bituminous Coal^a Table 8.

| | Net Plant | | Annual Cost | s. mills/kW-h | Unit Cost per Ton of Acid Gas Removed, \$/ton ° | |
|-------------------------|-----------|-----------------------|--------------------|------------------|--|--------|
| Technology ^b | Capacity | Capital Costs | Constant | Current | Constant | Curren |
| | MW | \$/kW | \$ | \$ | \$ | \$ |
| | Case 1, I | Project Contingencies | = 15%, Process Col | ntingencies = 0% | · . | |
| AFBC | 200 | 1530 | 60 | 103 | 270 | 460 |
| | 500 | 1250 | 52 | 90 | 210 | 360 |
| | 1000 | 1080 | 48 | 82 | 180 | 300 |
| PFBC | 200 | 1800 | 68 | 116 | 580 | 1000 |
| | 500 | 1440 | 58 | 99 | 420 | 720 |
| | 1000 | 1220 | 52 | 89 | 320 | 560 |
| IGCC | 200 | 1890 | 65 | 112 | 470 | 800 |
| | 500 | 1540 | 55 | 95 | 310 | 540 |
| | 1000 | 1330 | 50 | 85 | 230 | 390 |
| PC/FGD/SCR | 200 | 1840 | 70 | 120 | 680 | 1150 |
| | 500 | 1490 | 61 | 104 | 550 | 940 |
| | 1000 | 1310 | 56 | 96 | 510 | 870 |
| PC/FGD | 200 | 1720 | 65 | 112 | 570 | 980 |
| | 500 | 1390 | 57 | 97 | 450 | 760 |
| | 1000 | 1122 | 52 | 89 | 400 | 680 |

(Continued)

atmospheric fluidized bed combustion.
pressurized fluidized bed combustion.
integrated gasification combined cycle.
pulverized coal-fired plant.
flue gas desulfurization.
selective catalytic reduction. PC FGD SCR

For estimating new plant costs, retrofit factor is 1.0. For estimating repowered AFBC, PFBC, and IGCC costs, costs of new plants were adjusted using the reuse and refurbishment factor approach discussed in this report.

*NA = Not applicable.

| Table 8. (Con | tinued) | | | | | er Ton of Acid |
|---------------------------------------|-----------------------------|------------------------|-------------------------------|--------------------------------|----------------------------|---------------------------------|
| Technology ^b | Net Plant Capacity MW | Capital Costs \$/kW | Annual Cost Constant \$ | s, mills/kW-h Current \$ | Gas Remo Constant \$ | oved, \$/ton ° Current \$ |
| · · · · · · · · · · · · · · · · · · · | Case 2, i | Project Contingencies | = 30%, Process Co | ntingencies = 10% | | |
| AFBC | 200 | 1860 | 67 | 115 | 310 | 530 |
| | 500 | 1510 | 58 | 99 | 240 | 410 |
| | 1000 | 1300 | 53 | 91 | 190 | 330 |
| PFBC | 200 | 2190 | 76 | 130 | 670 | 1150 |
| | 500 | 1750 | 64 | 110 | 490 | 830 |
| | 1000 | 1470 | 58 | 98 | 370 | 630 |
| IGCC | 200 | 2300 | 74 | 127 | 580 | 990 |
| | 500 | 1880 | 63 | 107 | 400 | 680 |
| | 1000 | 1610 | 56 | 96 | 300 | 520 |
| PC/FGD/SCR | 200 | 2150 | 75 | 128 | 750 | 1280 |
| | 500 | 1750 | 65 | 110 | 600 | 1030 |
| | 1000 | 1540 | 59 | 101 | 550 | 940 |
| PC/FGD | 200 | 2070 | 73 | 125 | 640 | 1100 |
| | 500 | 1670 | 63 | 107 | 490 | 840 |
| | 1000 | 1460 | 57 ' | 98 | 440 | 750 |

Cost are in 1988 dollars.

AFBC = atmospheric fluidized bed combustion.

PFBC = pressurized fluidized bed combustion.

IGCC = integrated gasification combined cycle.

PC/FGD/SCR = pulverized-coal plant with wet limestone flue gas desulfurization and selective catalytic reduction.

PC/FGD = PC plant with wet limestone FGD.

Tons of acid gas removed = sum of the tons of SO₂ and NO_x removed.

Hypothetical acid gas control cost = annual cost for advanced technologies - annual cost for PC plant without FGD and SCR.

Table 9. New Plant Cost Estimates for Advanced Coal Combustion Technologies Firing 4% Sulfur Bituminous Coal ^a

| | Net Plant | | Annual Costs, mills/kW-h | | Unit Cost per Ton of Acid Gas Removed, \$/ton ° | |
|-------------------------|--------------------|------------------------|--------------------------|-----------------|--|--------------|
| Technology ^b | Capacity MW | Capital Costs \$/kW | Constant \$ | Current \$ | Constant (| Curren \$ |
| | Case 1, | Project Contingencie | s = 15%, Process Cont | ringencies = 0% | | |
| AFBC | 200 500 1000 | 1260 | 63 10 55 9 51 8 | 5 19 | 90 330 | |
| PFBC | 200 500 1000 | | 70 12 60 10 54 9 | 3 30 | 00 510 | |
| IGCC | 200 500 1000 | 1570 | 65 11 55 9 50 8 | 5 17 | 70 290 | |
| PC/FGD/SCR | 200 500 1000 | 1480 | 69 11 60 10 55 9 | 2 35 | 50 470 | |
| PC/FGD | 200 500 1000 | 1380 | 64 11 56 9 52 8 | 6 28 | 30 470 | |

(Continued)

AFBC = atmospheric fluidized bed combustion.

| Table 9. | (Continued) |
|----------|-------------|

| | Net Plant Capacity Capital Costs | | Anı Cons | nual Costs, mills/kW-h tant Current | G | Unit Cost per Ton of Acid Gas Removed, \$/ton ° Constant Current | | |
|-------------------------|-------------------------------------|------------------------|---------------|--|-----|--|--|--|
| Technology ^b | MW | \$/kW | \$ | sant Current \$ | \$ | \$ | | |
| | Case 2 | 2, Project Contingenci | es = 30%, Pro | ocess Contingencies = | 10% | | | |
| AFBC | 200 | 1870 | 70 | 120 | 240 | 420 | | |
| | 500 | 1520 | 61 | 104 | 210 | 350 | | |
| | 1000 | 1310 | 56 | 96 | 180 | 310 | | |
| PFBC | 200 | 2200 | 78 | 134 | 430 | 740 | | |
| | 500 | 1750 | 67 | 114 | 330 | 570 | | |
| | 1000 | 1480 | 60 | 102 | 270 | 460 | | |
| IGCC | 200 | 2340 | 74 | 127 | 320 | 550 | | |
| | 500 | 1910 | 63 | 107 | 220 | 380 | | |
| | 1000 | 1640 | 56 | 96 | 160 | 280 | | |
| PC/FGD/SCR | 200 | 2230 | 80 | 136 | 460 | 790 | | |
| | 500 | 1810 | 69 | 113 | 380 | 650 | | |
| | 1000 | 1590 | 63. | 108 | 350 | 600 | | |
| PC/FGD | 200 | 2090 | 75 | 128 | 370 | 640 | | |
| | 500 | 1690 | 64 | 110 | 300 | 510 | | |
| | 1000 | 1480 | 59 | 101 | 270 | 460 | | |

Costs are in 1988 dollars.

AFBC = atmospheric fluidized bed combustion.

PFBC = pressurized fluidized bed combustion.

IGCC = integrated gasification combined cycle.

PC/FGD/SCR = pulverized-coal plant with wet limestone flue gas desulfurization and selective catalytic reduction.

PC/FGD = PC plant with wet limestone FGD.

Tons of acid gas removed = sum of the tons of SO₂ and NO₂ removed.

Hypothetical acid gas control cost = annual cost for advanced technologies - annual cost for PC plantwithout FGD and SCR.

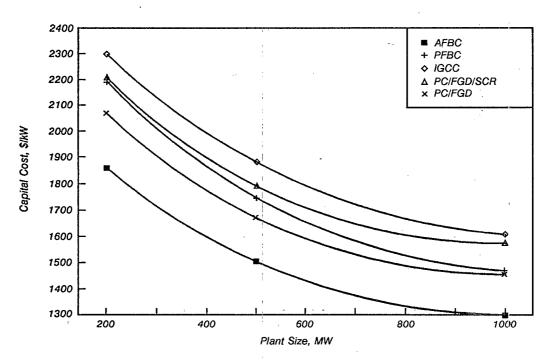


Figure 1. Capital costs for new plants as a function of size for plants using 2% sulfur coal (in constant 1988 dollars).

Contingencies of 30% for project and 10% for process are assumed.

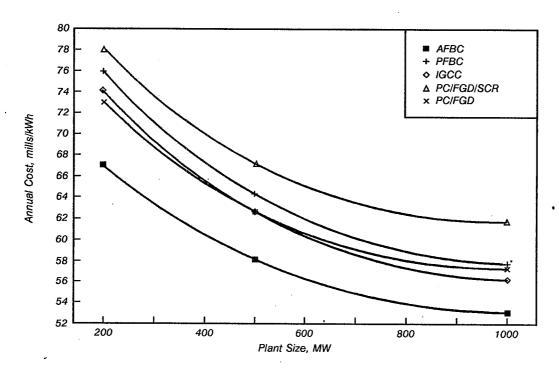


Figure 2. Annual costs for new plants as a function of size for plants using 2% sulfur coal (in constant 1988 dollars). Contingencies of 30% for project and 10% for process are assumed.

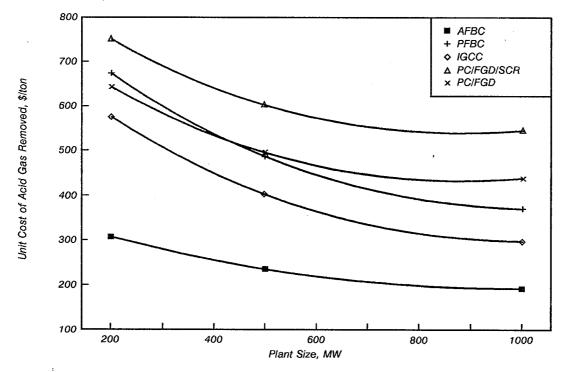


Figure 3. Unit cost of acid gas removed as a function of size for plants using 2% sulfur coal (in constant 1988 dollars). Contingencies of 30% for project and 10% for process are assumed.

| | Base Net | Final Net | | Annual Costs, mills/kW-h | | |
|-------------------------|----------------------|------------------------|------------------------|--------------------------|------------------|--|
| Technology ^b | Plant Capacity MW | Plant Capacity ° MW | Capital Costs \$/kW | Constant \$ \$ | Current \$ | |
| | Case 1, F | Project Contingencies | = 15%, Process Cont | ingencies = 0% | | |
| AFBC | 200 500 1000 | 200 500 1000 | 790 660 590 | 46 42 39 | 72 65 61 | |
| PFBC | 200 500 1000 | 200 500 1000 | 1190 950 810 | 58 50 45 | 90 78 71 | |
| IGCC | 70 170 330 | 200 500 1000 | 1710 1400 1210 | 67 56 51 | 104 88 79 | |
| PC/FGD/SCR * | 208 520 1040 | 200 500 1000 | 630 540 510 | 45 40 39 | 70 63 61 | |
| PC/FGD | 206 515 1030 | 200 500 1000 | 490 420 400 | 40 36 34 | 62 56 53 | |
| | Case 2, I | Project Contingencies | = 30%, Process Cont | tingencies = 10% | | |
| AFBC | 200 500 1000 | 200 500 1000 | 950 800 710 | 50 45 42 | 78 70 66 | |
| PFBC | 200 500 1000 | 200 500 1000 | 1440 1150 970 | 64 55 49 | 100 85 77 | |
| IGCC | 70 170 330 | 200 500 1000 | 2080 1700 1470 | 76 64 57 | 118 100 89 | |
| PC/FGD/SCR | 208 520 1040 | 200 500 1000 | 700 570 550 | 47 42 34 | 73 66 53 | |
| PC/FGD | 206 515 1030 | 200 500 1000 | 540 450 420 | 41 37 35 | 64 57 55 | |

^{*} Costs are in 1988 dollars.

* AFBC = atmospheric fluidized bed combustion.

PFBC = pressurized fluidized bed combustion.

IGCC = integrated gasification combined cycle.

PC/FGD/SCR = pulverized-coal plant with wet limestone flue gas desulfurization and selective catalytic reduction.

PC/FGD = PC plant with wet limestone FGD.

* Station generating capacity is unchanged for simple cycle AFBC and PFBC repowering. Repowering with combined cycle IGCC results in an approximate tripling of capacity. Retrofit with FGD and SCR results in a capacity derate.

| | Base Net | Plant Cost Estimates Final Net | | Annual Costs | mills/kW-h | |
|-------------------------|----------------------|--------------------------------|------------------------|-----------------|------------------|---|
| Technology ^b | Plant Capacity MW | Plant Capacity ° MW | Capital Costs \$/kW | Constant \$ | Current \$ \$ | |
| | | | | | | |
| | Case 1, P | Project Contingencies | = 15%, Process Cont | ingencies = 0% | | |
| AFBC | 200 500 1000 | 200 500 1000 | 800 670 600 | 49 44 42 | 76 69 65 | |
| PFBC | 200 500 1000 | 200 500 1000 | 1200 960 810 | 60 52 48 | 94 81 74 | |
| IGCC | 70 170 330 | 200 500 1000 | 1750 1420 1230 | 67 56 51 | 104. 88 79 | |
| PC/FGD/SCR | 208 520 1040 | 200 500 1000 | 690 590 550 | 47 42 40 | 73 66 63 | |
| PC/FGD | 206 515 1030 | 200 500 1000 | 550 470 430 | 41 37 36 | 64 58 56 | |
| | Case 2. F | Proiect Contingencies | = 30%, Process Cont | ingencies = 10% | | • |
| AFBC | 200 500 1000 | 200 500 1000 | 960 810 720 | 53 48 45 | 83 75 70 | |
| PFBC | 200 500 1000 | 200 500 1000 | 1440 1150 980 | 66 57 52 | 103 89 81 | |
| IGCC | 70 170 330 | 200 500 1000 | 2120 1730 1490 | 76 64 57 | 119 100 89 | |
| PC/FGD/SCR | 208 520 1040 | 200 500 1000 | 770 640 590 | 49 44 42 | 76 68 65 | |
| PC/FGD | 206 515 1030 | 200 500 1000 | 610 510 470 | 43 38 37 | 67 60 57 | |

^a Costs are in 1988 dollars.

^b AFBC = atmospheric fluidized bed combustion.

PFBC = pressurized fluidized bed combustion.

IGCC = integrated gasification combined cycle.

PC/FGD/SCR = pulverized-coal plant with wet limestone flue gas desulfurization and selective catalytic reduction.

PC/FGD = PC plant with wet limestone FGD.

^c Station generating capacity is unchanged for simple cycle AFBC and PFBC repowering. Repowering with combined cycle IGCC results in an approximate tripling of capacity. Retrofit with FGD and SCR results in a capacity derate.

J. Martinez, G. Snow, and M. Maibodi are with Radian Corp., Research Triangle Park,

Norman Kaplan is the EPA Project Officer (see below).

The complete report, entitled "Costs for Advanced Coal Combustion Technologies,"
(Order No. PB 90-255 688/AS; Cost: \$23.00, subject to change) will be available only from:

National Technical Information Service

National Technical Information Service
5285 Port Royal Road
Springfield, VA 22161
Telephone: 703-487-4650
The EPA Project Officer can be contacted at:
Air and Energy Engineering Research Laboratory
U.S. Environmental Protection Agency
Research Triangle Park, NC 27711

United States Environmental Protection Agency

Center for Environmental Research Information Cincinnati, OH 45268

BULK RATE POSTAGE & FEES PAID EPA PERMIT NO. G-35

Official Business Penalty for Private Use \$300

EPA/600/S7-90/015