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# PROPERTIES OF AMMONIUM SULFATE, AMMONIUM BISULFATE, AND SULFUR DIOXIDE SOLUTIONS IN AMMONIA SCRUBBING PROCESSES



Office of Research and Development National Environmental Research Center U.S. Environmental Protection Agency Research Triangle Park N.C. 27771

# PROPERTIES OF AMMONIUM SULFATE, AMMONIUM BISULFATE, AND SULFUR DIOXIDE SOLUTIONS IN AMMONIA SCRUBBING PROCESSES

bу

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#### ABSTRACT

The report gives the results of a study that involved the collection of data that should be useful in evaluating pilot plant operation of an ammonia scrubber with an ammonium bisulfate regeneration system. The study determined: (1) the density, pH, and composition of saturated (NH $_4$ ) $_2$ SO $_4$  solutions at 50, 65, and 80°C; (2) the effects on density, pH, and composition of NH $_4$ HSO $_4$  addition to the solutions in (1); and (3) the solubility and the stripping rates of SO $_2$  in saturated solutions of ammonium sulfate containing ammonium bisulfate at 65°C and 80°C.

The solubility of  $(\mathrm{NH_4})_2\mathrm{SO}_4$  in water was determined and compared with accepted values: good agreement was found. Addition of  $\mathrm{NH_4HSO}_4$  to the saturated solutions lowered the solubility of  $(\mathrm{NH_4})_2\mathrm{SO}_4$ , decreased the pH, and increased the density. The solubility of  $\mathrm{SO}_2$  in saturated  $(\mathrm{NH_4})_2\mathrm{SO}_4$  decreased with increasing temperature and with increasing concentration of  $\mathrm{NH_4HSO}_4$ . For the system and conditions used in this experiment,  $\mathrm{SO}_2$  stripping rates were found to be first order with respect to concentration of  $\mathrm{SO}_2$  except when the pH rose above 2.6. The stripping rate is dependent on temperature,  $\mathrm{NH_4HSO}_4$  concentration, and almost certainly on sweep gas rate and agitation rate.

#### CONTENTS

Conclusions	
00110110115	1
Recommendations	2
Introduction	3
Background	3
Objectives	4
Procedure	5
Equipment	5
Materials	<b>5</b>
Experimental Methods	5
Discussion	8
Acknowledgements	13
References	14
Appendices	34
Appendix A - Lot Analysis of Chemicals Used	35
Appendix B - The Effects of $NH_4HSO_4$ on Density, pH, and Composition of Saturated Solutions of $(NH_4)_2SO_4$ at $80^{\circ}C$ ,	36
	Recommendations Introduction Background Objectives Procedure Equipment Materials Experimental Methods Discussion Acknowledgements References Appendices Appendix A - Lot Analysis of Chemicals Used Appendix B - The Effects of NH4HSO4 on Density, pH, and Composition of Saturated

#### FIGURES

No.		Page
1	NH <sub>3</sub> Scrubbing NH <sub>4</sub> HSO <sub>4</sub> Regeneration Process	15
2	Effect of NH <sub>4</sub> HSO <sub>4</sub> on Concentration of (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> in a Saturated SolutionGrams Per Liter	16
3	Effect of $NH_4HSO_4$ on Concentration of $(NH_4)_2SO_4$ in a Saturated SolutionMoles Per 100 Moles $H_2O$	17
4	Effect of $NH_4HSO_4$ on pH Reading of a Saturated $(NH_4)_2SO_4$ Solution	18
5	Effect of $\mathrm{NH_4HSO_4}$ on Density of a Saturated $\mathrm{(NH_4)_2SO_4}$ Solution	19
6	Absorption of $SO_2$ in Saturated (NH <sub>4</sub> ) $_2SO_4$ Solutions Containing NH $_4$ HSO $_4$ at 65°C	20
7	Abosrption of $SO_2^7$ in Saturated $(NH_4)_2SO_4$ Solutions Containing $NH_4HSO_4$ at $80^{\circ}C$	21
8	${\rm SO_2}$ Solubility in Saturated (NH <sub>4</sub> ) $_2{\rm SO_4}$ Solutions Containing NH $_4{\rm HSO_4}$	22
9	Stripping Rates for ${\rm SO_2}$ in Saturated ${\rm (NH_4)_2SO_4}$ Solutions Containing ${\rm NH_4HSO_4}$ at 65°C	23
10	Stripping Rates for ${\rm SO}_2$ in Saturated ${\rm (NH_4)}_2{\rm SO}_4$ Solutions Containing ${\rm NH}_4{\rm HSO}_4$ at ${\rm 80}^{\circ}{\rm C}$	24
11	SO <sub>2</sub> Stripping as a Function of SO <sub>2</sub> Concentration at 65°C	25
12	SO <sub>2</sub> Stripping as a Function of SO <sub>2</sub> Concentration at 80°C	26

#### TABLES

No.	,	Page
1	Density, pH, and Composition of Saturated Ammonium Sulfate Solutions at 50, 65, and 80°C	27
2	Effects of $\rm NH_4HSO_4$ on Density, pH, and Composition of Saturated $\rm (NH_4)_2SO_4$ Solutions at 50, 65, and 80°C	28
3	Absorption of $SO_2$ in Saturated $(NH_4)_2SO_4$ Solutions Containing $NH_4HSO_4$ at $65^{\circ}C$	. 29
4	Absorption of ${\rm SO_2}$ in Saturated ${\rm (NH_4)_2SO_4}$ Solutions Containing ${\rm NH_4HSO_4}$ at ${\rm 80^\circ C}$	30
5	Stripping Rates for ${\rm SO_2}$ in a Saturated ${\rm (NH_4)_2SO_4}$ Solution Containing ${\rm NH_4HSO_4}$ at 65°C	31
6	Stripping Rates for ${\rm SO_2}$ in a Saturated ${\rm (NH_4)_2SO_4}$ Solution Containing ${\rm NH_4HSO_4}$ at ${\rm 80^\circ C}$	32
7	Stripping Rate Constants	33

# Section I CONCLUSIONS

For the experimental conditions used:

- 1. The pH, density, and composition of saturated ammonium sulfate solutions determined at 50, 65, and 80°C are consistent with literature values.
- 2. Ammonium bisulfate addition to the above solutions lowered  $(NH_4)_2SO_4$  solubility, decreased pH, increased density, and lowered  $SO_2$  solubility.
- 3. The stripping rate of  $SO_2$  from  $(NH_4)_2SO_4$  solutions,  $-dSO_2/dt$ , was found to be a linear function of  $SO_2$  concentration for pH values below 2.6.

#### Section II

#### RECOMMENDATIONS

A valuable addition to the accomplishments listed in this report would be an investigation of the effects of agitation and gas flow rate on  $\mathrm{SO}_2$  stripping rates. It would be useful to know the effects of these variables on the first order stripping rate constant. Without these data, scale up is difficult. The usefulness of the rate data which are contained in this report is limited to qualitative work only.

Another area requiring investigation is the effect of ammonium bisulfate on the release rates from ammonium sulfite-sulfate solutions. These data would be of great benefit in studying acidifier kinetics in the ammonia scrubbing process.

# Section III INTRODUCTION

#### Background

The problem of stack gas desulfurization has received much attention in the past few years. As a result, modifications of NH $_3$  scrubbing of SO $_2$  with an NH $_4$ HSO $_4$  regeneration cycle are being investigated. The original work is described in Hixon and Miller patent No. 2,405,747.

This process essentially consists of scrubbing the flue gas stream with an  $NH_3$  and  $(NH_4)SO_4$  solution. The scrubber effluent is then acidified with  $NH_4HSO_4$  to release the greater portion of  $SO_2$ , stripped of the remaining  $SO_2$  in a stripper, neutralized with  $NH_3$ , and crystallized to yield solid  $(NH_4)_2SO_4$ . The solid  $(NH_4)_2SO_4$  is thermally decomposed to yield  $NH_4HSO_4$  and  $NH_3$  which are recycled back into the process (see Figure 1).

The reactions below describe the chemistry of the system.

#### Scrubber Reactions

$$NH_3 + H_2O + SO_2 \rightarrow NH_4HSO_3$$
  
 $NH_4HSO_3 + NH_3 \rightarrow (NH_4)_2SO_3$   
 $(NH_4)_2SO_3 + SO_2 + H_2O \rightarrow 2 NH_4HSO_4$ 

#### Regeneration Reactions

$$(NH_4)_2SO_3 + 2 NH_4HSO_4 \rightarrow 2(NH_4)_2SO_4 + SO_2 + + H_2O_3 + NH_4HSO_4 \rightarrow (NH_4)_2SO_4 + SO_2 + + H_2O_4$$
  
 $(NH_4)_2SO_4 \rightarrow NH_4HSO_4 + NH_3$   
Heat

#### **Objectives**

This study will be used as a basis to evaluate the results of the pilot plant operation. In particular, basic  $S0_2$  release rate data are needed to evaluate the effectiveness of the stripper and acidifier.

There were three objectives that this work was to meet in order to satisfy the need of the pilot plant project. First, measurements of the density, pH, and composition of saturated  $(NH_4)_2SO_4$  solutions were to be determined at 50, 65, and 80°C. Since the solutions throughout the process would be nearly saturated it is important to know these values. Also some of these data were available in the literature as a check on accuracy of the measurements. Second, the effects of addition of  $NH_4HSO_4$  on density, pH, and composition of these solutions were to be studied. These effects are important in the operation of the acidifier. Finally, the solubility and the stripping rates of  $SO_2$  in saturated solutions of  $(NH_4)_2SO_4$  containing incremental amounts of  $NH_4HSO_4$  were to be studied at 65 and 80°C. These data would yield the characteristics of the release of  $SO_2$  in the acidifier and in the stripper.

#### Section IV

#### **PROCEDURE**

#### Equipment

The reaction vessels in this experiment were 500 and 1000 ml, three-necked, round-bottom flasks. Agitation was supplied by a 6.25 cm. Teflon blade on a 0.95 cm. diameter glass rod powered by a Fisher Dyna Mix. The  $\rm SO_2$  and  $\rm N_2$  gas flow rates were measured by Brooks Rotameters. An Instrumentation Laboratories Model 245 pH meter (with a Beckman 39183 Combination Electrode) was used to measure pH. Density was measured by weighing the sample with a Sartorius analytical balance.

#### Materials

 $(\mathrm{NH_4})_2\mathrm{SO}_4$  was obtained from two suppliers: Matheson, Coleman, and Bell and Fisher Scientific. The latter was used for all  $\mathrm{SO}_2$  absorption and stripping rates; the former was used for the 50 and 65°C solubility data only. A comparison made between the salts failed to show a difference. The comparison results can be seen in Figures 2 through 5. The 65°C data in these figures were determined using each salt. Material from Matheson, Coleman, and Bell was used in procedure A and from Fisher Scientific in procedure B.  $\mathrm{NH_4HSO}_4$  was purchased from Fisher Scientific.  $\mathrm{N_2}$  and pure anhydrous  $\mathrm{SO}_2$  were supplied by Matheson Gas Products. Appendix A is a lot analysis of the solid chemicals used in these experiments.

#### Experimental Methods

The properties of  $(\mathrm{NH_4})_2\mathrm{SO_4}$  and  $\mathrm{NH_4HSO_4}$  solutions at 50 and 65°C were determined by a different method than the one used for the 80°C data. The change in procedure resulted from several factors, the most important of which was the inadequacy of the sampling technique used in the original method for temperatures above 65°C. A change in the determination of solution composition was made to increase the accuracy of readings at lower bisulfate concentrations. The change in suppliers of  $(\mathrm{NH_4})_2\mathrm{SO_4}$  was due to a greater than anticipated usage of the chemical.

For simplicity, procedure A for the 50 and 65°C data will be described in detail; changes made for the 80°C data, procedure B, will follow.

For procedure A (used for 50 and 65°C data), saturated  $(\mathrm{NH}_4)_2\mathrm{SO}_4$  solutions were prepared by placing 400 g of the reagent grade crystals and 320 ml of deoxygenated, deionized water into a three-necked flask. The solution was heated for 2 hours at 95°C and cooled to the desired temperature by adding ice to the bath as needed. After 20 minutes a sample of the solution was withdrawn with a standard 5 ml transfer pipet and drained into a tared vessel. The sample was weighed to determine density and analyzed by a barium perchlorate titration for  $\mathrm{SO}_4^=$  and the Kjeldal analysis for  $\mathrm{NH}_4$ . The pH was recorded at the time the sample was taken. The measurements made above were repeated on  $(\mathrm{NH}_4)_2\mathrm{SO}_4$  saturated solutions containing  $\mathrm{NH}_4\mathrm{HSO}_4$  which had been added incrementally. Twenty minutes was allowed for each portion of bisulfate to dissolve, and complete solution was verified by a non-changing pH response.

For procedure B (used for the 80°C data), an insulated and heated automatic pipet replaced the standard pipet. An NaOH titration using formaldehyde to tie up  $\mathrm{NH_4}^+$  ions was used for the  $(\mathrm{NH_4})_2\mathrm{SO_4}$  determination.  $^4$ 

Solubility of  $\mathrm{SO}_2$  and the  $\mathrm{SO}_2$  stripping rates were determined in procedure B by preparing 1 liter of saturated  $(\mathrm{NH}_4)_2\mathrm{SO}_4$  in the same manner as for procedure A. Pure  $\mathrm{SO}_2$  was bubbled into the flask at a rate of 600 cm³/min through a fritted glass impinger immersed in the solution. Agitation was constant at 200 rpm. In order to take a liquid sample, agitation had to be stopped to allow settling of excess  $(\mathrm{NH}_4)_2\mathrm{SO}_4$  crystals. Thus, for this period gas flow was stopped, and the sample period was not included in the time measurement. Initially, and at each sample period, the pH, composition, and density were measured. The saturated  $\mathrm{SO}_2$  solution produced above was then stripped with  $\mathrm{N}_2$  gas at 1000 cm³/min and 200 rpm agitation. Samples were taken and analyzed using procedure B, and  $\mathrm{SO}_2$  concentrations were determined iodimetrically.  $^5$ 

The effects of  $\mathrm{NH_4HSO_4}$  on stripping and solubility of  $\mathrm{SO_2}$  were determined by making the same measurements on saturated sulfate solutions containing incremental amounts of  $\mathrm{NH_4HSO_4}$ .

A discussion of measurement accuracy follows. First the reading on the pH meter was accurate to  $\frac{1}{2}$  0.01 pH unit when tested against known standards. Density measurements were found to be within 0.005 g/ml of the correct value. This deviation was the maximum error found in several determinations of the density of distilled water. The accuracy of the analytical methods for composition was: for the most part good. Both of the methods for sulfate and sulfite analysis were found to be within 1% accuracy. The bisulfate analyses were accurate to within 1% except when  $SO_2$  analyses were also performed. In these cases the tests were only accurate to within 10 g/l. This effect is explained in the discussion.

#### Section V

#### DISCUSSION

Table 1 contains the properties of saturated  $(NH_4)_2SO_4$  solutions. The composition of the solutions agrees to within 1% of the values listed in the literature. Linke and Seidell list the solubility of  $(NH_A)_2SO_A$ in weight percent rather than grams per liter. Thus, to compare the Table 1 values with Linke and Seidell values, both the density and the concentration in Table 1 must be used. This situation indicates that the experimental values of both concentration and density are reliable. There is a question, however, as to the reliability of the pH reading. It should be pointed out that all pH's reported are instrument readings: no corrections were made for electrode processes as the correction factor was assumed negligible for the present work. For saturated solutions the pH drifted with time to lower values. Raising the temperature of the solution accelerated the pH drop. Information available from the lot analysis of the chemical indicated that the pH of a 5% solution would be in the range of 5.0 to 6.0 pH units. Freshly made saturated and 5% solutions fell into this pH range, but in both cases pH drifted to lower values according to the time-temperature history of the solution. It is thought that this drop in pH was due to thermal decomposition of  $(NH_4)_2SO_4$  to  $NH_4HSO_4$ . However, this has not been confirmed because the analysis for  $\mathrm{NH_4HS0_4}$  is not sensitive to such low concentrations.

The effects of  $\mathrm{NH_4HSO_4}$  addition can be noted from Table 2 and Figures 2-5. Figures 2 and 3 show that the addition of  $\mathrm{NH_4HSO_4}$  to saturated  $(\mathrm{NH_4})_2\mathrm{SO_4}$  solutions lowers the solubility of the latter salt in that solution. Figure 3 shows the data on a constant water basis. The major source of error in these data is the determination of low  $\mathrm{NH_4HSO_4}$  concentrations. In the 50 and 65°C data, this error resulted from taking a small difference between two large titrations. The 80°C readings using procedure B should be somewhat more reliable because they were determined by direct titration. The work for 50 and 65°C had already been completed when the analysis in procedure B was initiated.

A second effect, the pH lowering due to the acid nature of  $NH_4HSO_4$ , is shown in Figure 4. The pH lowering is independent of temperature. There are no data in the available literature with which a comparison can be made. The pH reading did not suffer from the same drift as noted above in the pure saturated solutions.

A third effect of  $\mathrm{NH_4HSO_4}$  on  $(\mathrm{NH_4})_2\mathrm{SO_4}$  solutions is the increase in density of the solution with the increase of  $\mathrm{NH_4HSO_4}$ . It appears from Figure 5 that the density of the saturated solutions is independent of temperature. One explanation of this is that the increase of salt concentration offsets the increase in volume.

Absorption rates for  $SO_2$  in  $(NH_4)_2SO_4$  and  $NH_4HSO_4$  solutions were measured to indicate when the solutions were reaching saturation. Thus, the end points of the curves in Figures 6 and 7 show solutions which are approximately saturated in  $SO_2$ . Figure 8 shows the decrease of the solubility of  $\mathrm{SO}_2$  in solution as the concentration of  $\mathrm{NH_4HSO}_4$  increases. Tables 3 through 6 show that the density measurements were unaffected by the concentration of  $SO_2$ . Although there is scatter in the data, these tables indicate that concentration of  ${\rm SO}_{2}$  has no effect on the concentration of  $(\mathrm{NH_4})_2\mathrm{SO_4}$  and  $\mathrm{NH_4HSO_4}$ . The scatter was produced by an analytical method which required taking differences among large numbers when  $\mathrm{SO}_2$  was present in the sample. For solutions having no  $\rm SO_2$  (those at zero time in Tables 3 through 6), the  $(NH_4)_2SO_4$  and  $NH_4HSO_4$  values were found from direct titrations and are more accurate. Stopping agitation and sweep gas apparently had no effect on the results. The pH did not change during the delay period, indicating no SO<sub>2</sub> evolution, and the experimental stripping curves matched derived, first-order curves closely enough to indicate absences of SO<sub>2</sub> evolution.

The stripping curves in Figures 9 and 10 were analyzed in greater detail than the absorption curves. The instantaneous rate was found at various points on the curves and plotted against the concentration of  ${\rm SO}_2$ 

as shown in Figures 11 and 12. The plots, which appear linear except at low concentrations of  $SO_2$  and  $NH_4HSO_4$  (pH values above 2.6), indicate that the first order differential equation below applies:

$$\frac{-dC}{dt} = kC \tag{1}$$

Where C is concentration of  $SO_2$ , g/l; k is the proportionality constant,  $min^{-1}$ ; and t is time, min. This equation can be integrated to find the concentration at any time which is given by

$$C = C_0 e^{-kt}$$
 (2)

where  $C_0$  is the initial concentration of  $SO_2$ , g/l; and e is the natural logarithm base. The rate constant k, which is the slope of the lines in Figures 11 and 12, is listed in Table 7 for various concentrations of  $NH_4HSO_4$  and temperatures. Using equation 2 and obtaining the constants from Figure 8 and Table 7, curves of concentration verus time can be generated and compared with curves in Figures 9 and 10. The agreement is good for all portions of the curve where equation 1 was valid or for portions below a pH of 2.6.

Equation 2 cannot be used in the general case because the dependency of k on temperature,  $NH_4HSO_4$  concentration, sweep gas rate, and agitation is not known.

The deviation in first order behavior above a 2.6 pH is not fully understood. One possible explanation of this phenomenon is that the dissolved  $SO_2$  exists in several forms as described by the following:

$$SO_2$$
 ·  $H_2O$   $\longrightarrow$   $H_2SO_3$   $\longrightarrow$   $H^+ + HSO_3^ \longrightarrow$   $2H^+ + SO_3^-$ 

According to this hypothesis the mass transfer of  $SO_2$  from the liquid phase to the gas phase is proportional to the concentration of  $SO_2$  \*  $H_2O$ , the driving force. At low pH readings: the  $H^+$  concentration is high,

the equilibrium is shifted to the left, and the  $SO_2$  present is almost exclusively in the hydrated form. Accordingly, the concentration of total  $SO_2$  which is determined analytically is an accurate measure of the true driving force. However, at higher pH values: the  $H^+$  concentration is lower, the equilibrium is shifted to the right, and the  $SO_2$  present is distributed among the several forms. In this case the total  $SO_2$  which is measured analytically is larger than the true driving force, the  $SO_2 \cdot H_2O$ . It is postulated that if only the  $SO_2 \cdot H_2O$  were measured at any time the first order behavior would be observed over the whole pH range.

#### Section VI

#### **ACKNOWLEDGEMENTS**

Assistance is gratefully acknowledge to L. I. Griffin for the original concept of this work, to J. H. Abbott for providing much helpful criticism and analysis, and to R. Grote for assistance with laboratory requirements.

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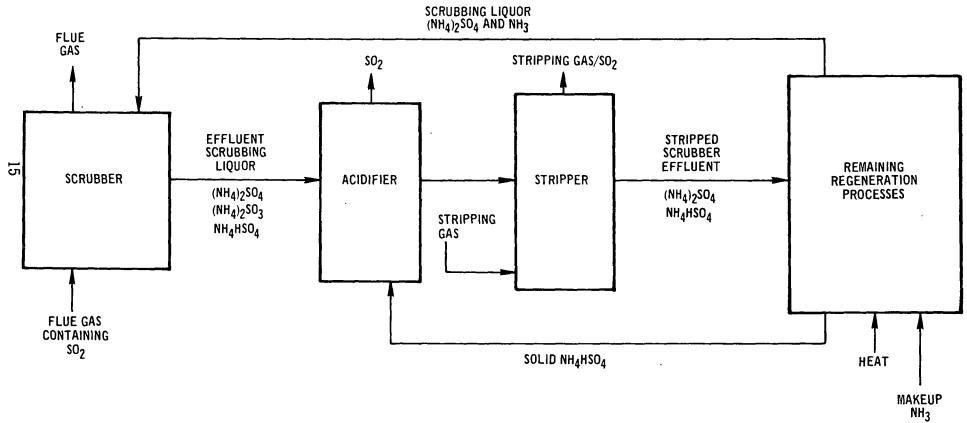


Figure 1. Ammonia scrubbing--ammonia bisulfate regeneration process.

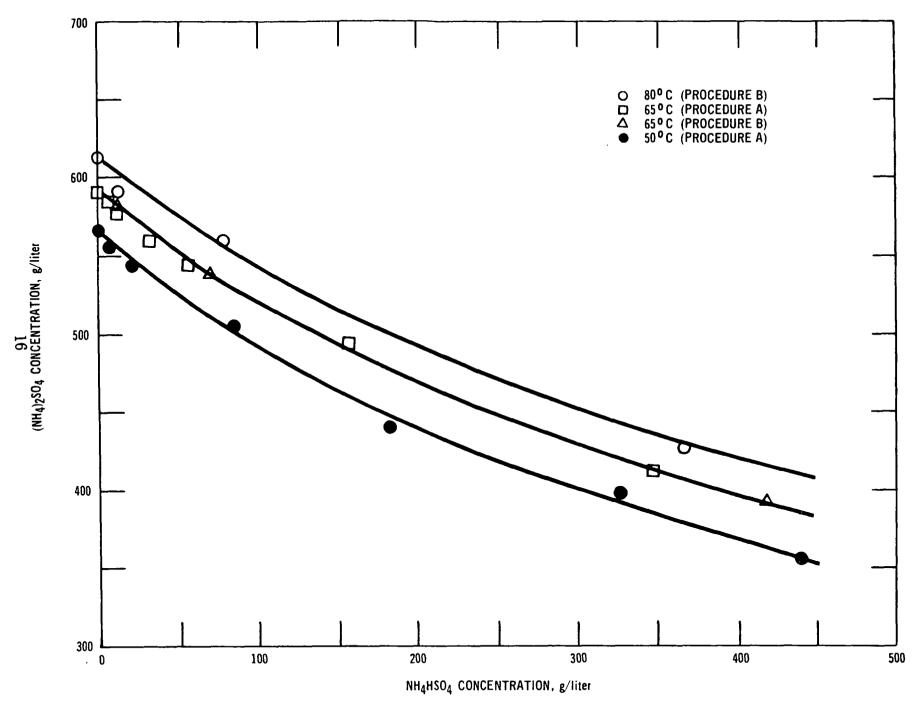


Figure 2. Effect of  $NH_4HSO_4$  on concentration of  $(NH_4)_2SO_4$  in a saturated solution.

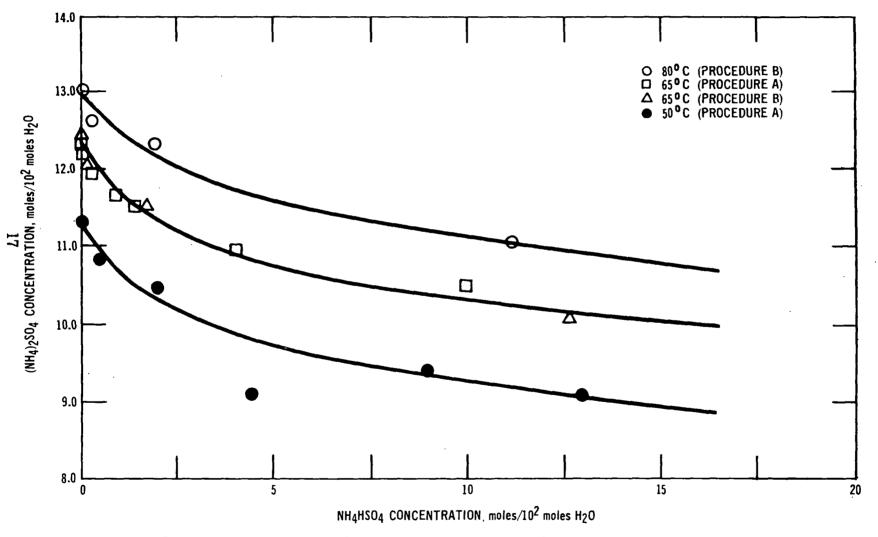


Figure 3. Effect of  $NH_4HSO_4$  on concentration of  $(NH_4)_2SO_4$  in a saturated solution.

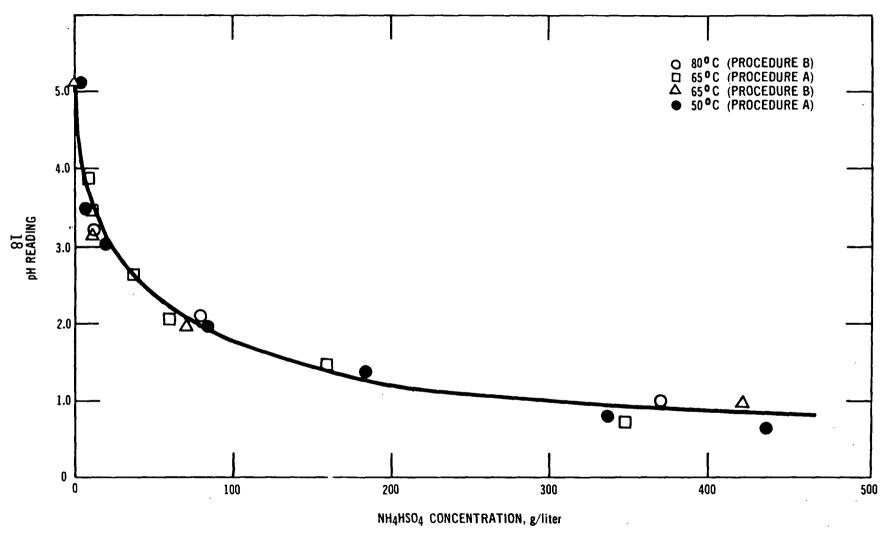


Figure 4. Effect of  $NH_4HSO_4$  on pH reading of a saturated  $(NH_4)_2SO_4$  solution.

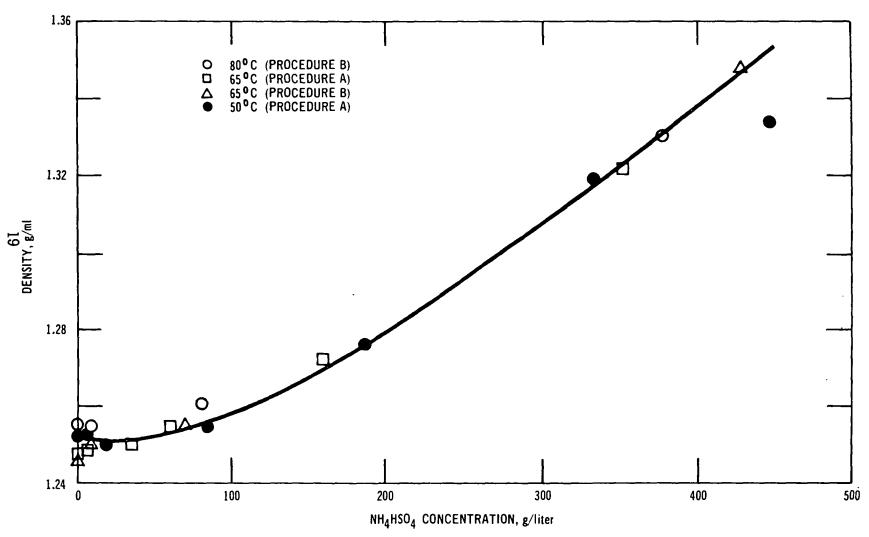


Figure 5. Effect of  $NH_4HSO_4$  on the density of a saturated  $(NH_4)_2SO_4$  solution.

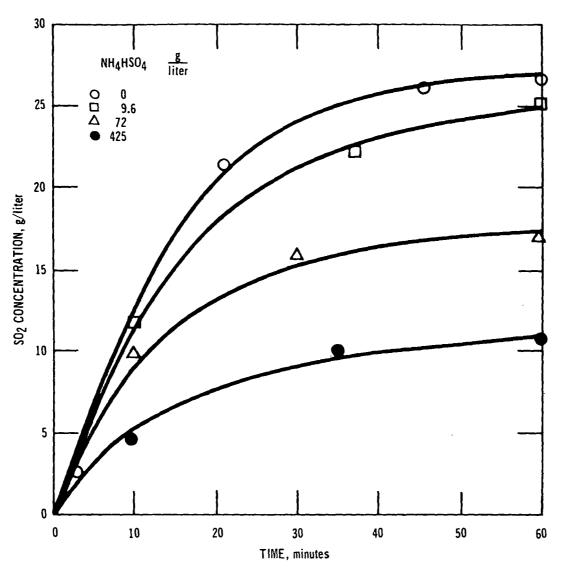


Figure 6. Absorption of  $SO_2$  in saturated (NH<sub>4</sub>)<sub>2</sub> $SO_4$  solutions containing NH<sub>4</sub>HSO<sub>4</sub> at 65° C.

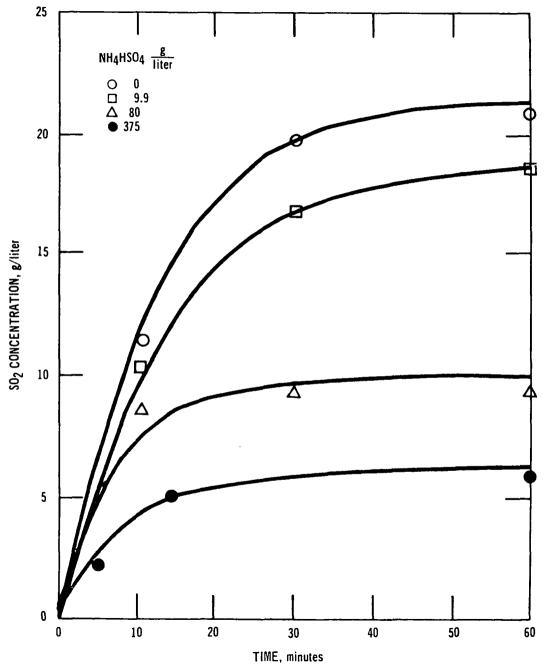


Figure 7. Absorption of  $SO_2$  in saturated (NH<sub>4</sub>)<sub>2</sub> $SO_4$  solutions containing NH<sub>4</sub>HSO<sub>4</sub> at 80° C.

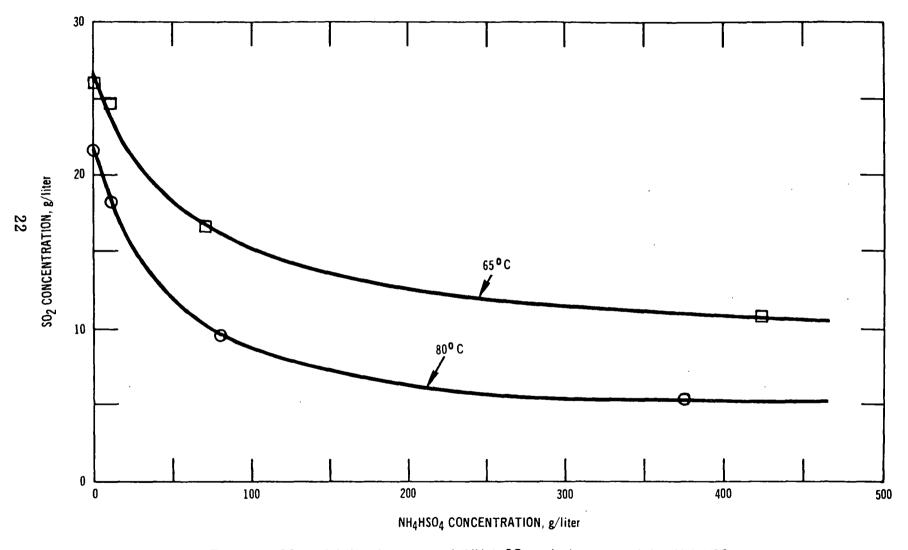


Figure 8.  $\mathrm{SO}_2$  solubility in saturated (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> solutions containing NH<sub>4</sub>HSO<sub>4</sub>.

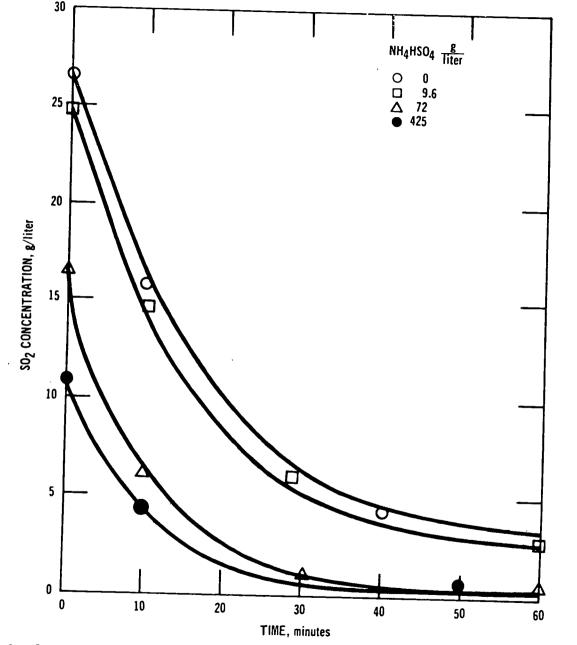


Figure 9. Stripping rates for  $SO_2$  in saturated (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> solutions containing NH<sub>4</sub>HSO<sub>4</sub> at 65 $^{\circ}$  C.

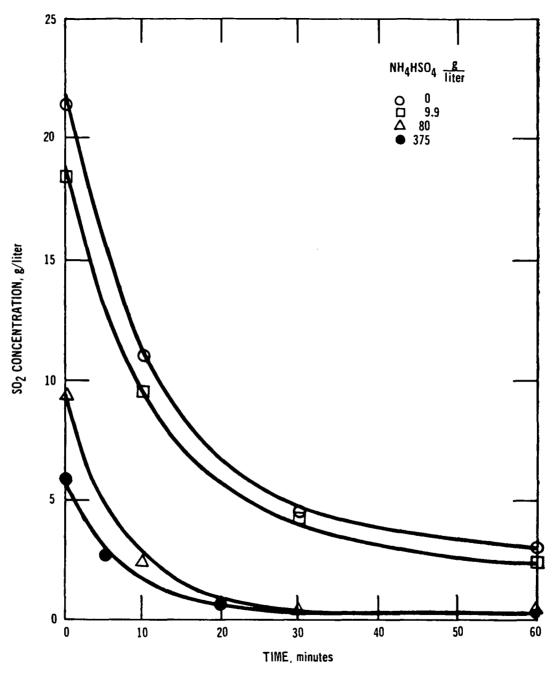


Figure 10. Stripping rates for  $SO_2$  in saturated (NH<sub>4</sub>)<sub>2</sub>SO<sub>4</sub> solutions containing NH<sub>4</sub>HSO<sub>4</sub> at  $80^{\circ}$  C.

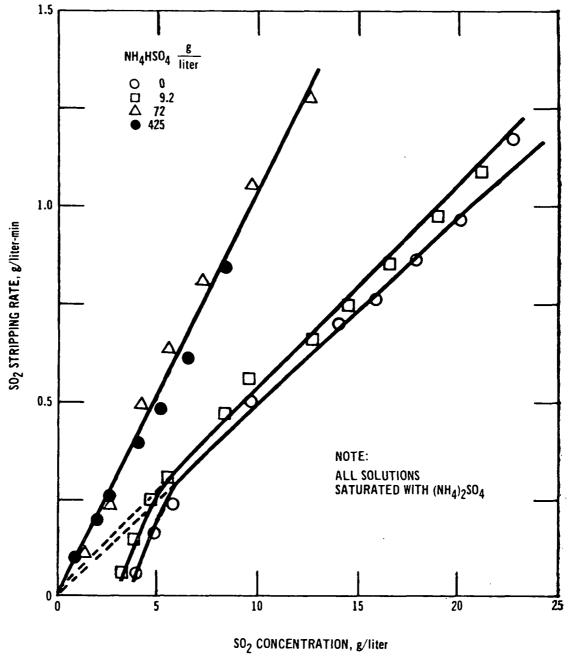


Figure 11.  $SO_2$  stripping as a function of  $SO_2$  concentration at 65  $^{\rm 0}$  C.

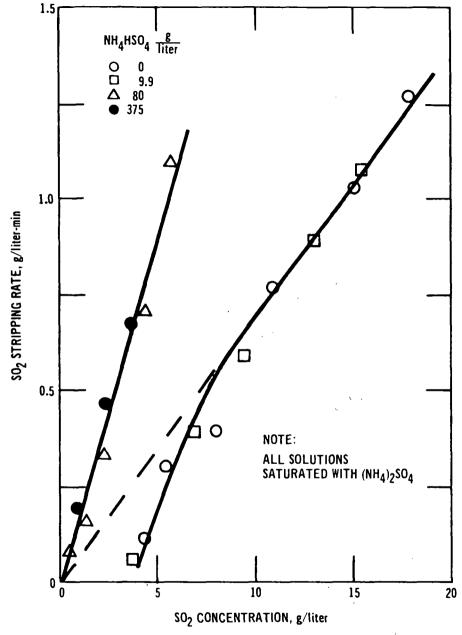


Figure 12.  $SO_2$  stripping as a function of  $SO_2$  concentration at  $80^{\circ}$  C.

Table 1. DENSITY, pH, AND COMPOSITION OF SATURATED  $(NH_4)_2SO_4$  SOLUTIONS AT 50, 65, AND 80°C

Temperature	Conc (N	H <sub>4</sub> ) <sub>2</sub> S0 <sub>4</sub>	Density	рН
°C	g/1	moles/100 moles H <sub>2</sub> 0	g/cm <sup>3</sup>	Reading
50	570	11.4	1.254	5.18
65	596	12.4	1.251	5.10
80	616	13.1	1.256	5.17

Table 2. EFFECTS OF  $\rm NH_4HSO_4$  ON DENSITY, pH, AND COMPOSITION OF SATURATED  $\rm (NH_4)_2SO_4$  SOLUTIONS AT 50, 65, and 80°C

Conc (N	H <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub>	Conc NH	4 <sup>HS0</sup> 4	pH	Density
grams liter	moles 100 moles H <sub>2</sub> 0	grams Titer	moles 100 moles H <sub>2</sub> 0	Reading	grams cm <sup>3</sup>
		Resul	ts at 50°C (Proced	ure A)	
570	17.4	0	0	5.18	1.254
561	11.1	6	0.14	3.51	1.255
547	10.9	20	0.46	3.05	1.250
509	10.5	85	2.01	2.00	1.255
442	9.2	185	4.37	1.39	1.276
402	9.4	332	8.87	0.82	1.320
358	9.1	441	12.9	0.64	1.334
		Resul	ts at 65°C (Proced	ure A)	
596	12.4	0	0	5.10	1.251
590	12.3	5	0.12	3.85	1.248
579	12.0	10	0.24	3.50	1.247
562	11.7	35	0.84	2.66	1.250
548	11.6	60	1.45	2.09	1.255
498	11.0	160	4.07	1.50	1.273
414	10.5	352	9.91	0.74	1.322
		Resul	ts at 65°C (Proced	ure B)	
596	12.5	0	0	5.18	1.245
584	12.1	9.6	0.23	3.11	1.251
544	11.6	72.0	1.76	2.00	1.251
394	10.1	425.0	12.55	0,98	1.349
		Resul	ts at 80°C (Proced	ure B)	
616	13.1	0	0	5.17	1.255
597	12.7	9.9	0.25	3.11	1.254
565	12.4	80.0	2.0	2.13	1.261
430	11.1	375.0	11.1	1.05	1.331

Table 3. ABSORPTION OF  $\mathrm{SO}_2$  IN SATURATED  $\mathrm{(NH_4)_2SO_4}$  SOLUTIONS CONTAINING  $\mathrm{NH_4HSO_4}$  AT 65°C

Time min	pH Reading	Density g/cm <sup>3</sup>	SO <sub>2</sub> g/1	(NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> g/1	NH <sub>4</sub> HSO <sub>4</sub> g/1
		Concentration NH <sub>4</sub> HS	O <sub>4</sub> = O grams/liter		
0	5.18	1.245	0	586	0
3	3.25	1,246	2.5	580	0
21	2.62	1.244	21.2	586	0
45	2.53	1.247	26.0	590	0
60	2.52	1.250	26.4	583	0
	***	Concentration NH <sub>4</sub> HS	O <sub>4</sub> = 9.6 grams/lite	r	······································
0	3.11	1,251	0	584	9.6
19	2.64	1.250	12.1	582	5.7
35	2.37	1.256	22.6	593	4.5
60	2.31	1.255	24.8	586	3.5
		Concentration NH <sub>4</sub> HS	$0_4 = 72 \text{ grams/liter}$	•	
0	2.00	1,256	0	544	72.0
10	1.91	1.257	10.2	543	70.0
30	1,87	1.257	15.7	547	63.0
60	1.87	1.260	16.5	554	61.0
		Concentration NH <sub>4</sub> HS	0 <sub>4</sub> = 425 grams/lite	r	
0	0.98	1.349	0	394	425.0
10	0.95	1.350	4.6	394	418.0
35	0.94	1.352	9.6	391	405.0
60	0.93	1.351	10.9	396	415.0

Table 4. ABSORPTION OF  ${\rm SO_2}$  IN SATURATED  ${\rm (NH_4)_2SO_4}$  SOLUTIONS CONTAINING  ${\rm NH_4HSO_4}$  at  ${\rm 80^{\circ}C}$ 

Time min	pH Reading	Density g/cm <sup>3</sup>	50 <sub>2</sub> g/1	(NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> g/1	NH <sub>4</sub> HSO <sub>2</sub> g/1
		Concentration NH <sub>4</sub> H	ISO <sub>4</sub> = 0 grams/lit	er	
0	5.17	1.255	0	616	0
10	2.91	1.256	11.4	608	0
30	2.68	1.259	19.7	611	0
60	2.66	1.258	21.3	610	0
		Concentration NH <sub>4</sub> H	1SO <sub>4</sub> = 9.9 grams/1	iter	· <del>- · · · · · · · · · · · · · · · · · · </del>
0	3.11	1.254	0	585	9.9
10	2.66	1.260	10.3	582	3.7
30	2.54	1.258	16.8	609	11.5
60	2.50	1.259	18.4	598	8.1
<del></del>		Concentration NH <sub>4</sub> H	ISO <sub>4</sub> = 80 grams/li	ter	
0	2.13	1.261	0	565	80.0
15	2.10	1.267	8.6	562	76.0
35	2.09	1.266	9.4	564	84.0
55	2.08	1.270	9.4	566	80.0
		Concentration NH <sub>4</sub> H	ISO <sub>4</sub> = 375 grams/1	iter	
0	1.05	1.331	0	430	375.0
5	1.06	1.329	2.2	436	372.0
15	1.05	1.335	5.0	440	364.0
60	1.04	1.333	5.9	435	382.0

Table 5. STRIPPING RATES FOR  ${\rm SO_2}$  IN A SATURATED  ${\rm (NH_4)_2SO_4}$  SOLUTION CONTAINING  ${\rm NH_4HSO_4}$  AT 65°C

Time min	pH Reading	Density g/cm <sup>3</sup>	SO <sub>2</sub> g/1	(NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> g/1	NH <sub>4</sub> HSO <sub>4</sub> g/1
		Concentration NH <sub>4</sub> H	1SO <sub>4</sub> = 0 grams/1	iter	
0	2.52	1.250	26.4	583	0
10	2.70	1.274	15.8	586	0
40	3.10	1.244	4.2	580	0
		Concentration NH <sub>4</sub> H	1SO <sub>4</sub> = 9.6 grams	/liter	
0	2.31	1.255	24.8	586	3.5
10	2.54	1.253	14.6	582	5.7
28	2.76	1.253	5.8	586	5.7
52	2.94	1.251	3.0	587	3.5
		Concentration NH <sub>4</sub> H	150 <sub>4</sub> = 72 grams/	liter	
0	1.87	1.260	. 16.5	554	61.0
10	1.93	1,258	5.9	547	73.0
30	1.95	1.255	0.9	548	75.0
60	1.97	1.256	0.5	548	70.0
		Concentration NH <sub>4</sub> H	1SO <sub>4</sub> = 425 grams	/liter	
0	0.93	1.348	10.9	396	415
10	0.95	1.350	4.5	394	420
50	0.96	1.347	0.5	396	430

Table 6. STRIPPING RATES FOR  ${\rm SO_2}$  IN SATURATED  ${\rm (NH_4)_2SO_4}$  SOLUTIONS CONTAINING  ${\rm NH_4HSO_4}$  AT  ${\rm 80^{\circ}C}$ 

Time min	pH Reading	Density g/cm <sup>3</sup>	S0 <sub>2</sub> g/1	(NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> g/1	NH <sub>4</sub> HSO <sub>4</sub> g/1
		Concentration NH			<u>97 '</u>
0	2.66	1.258	21.3	610	0
10	2.96	1.258	10.9	610	0
30	3.27	1.255	4.5	613	0
60	3.54	1.255	2.9	611	0
		Concentration NH	4 <sup>HSO</sup> 4 = 9.9 gra	ams/liter	
0	2,50	1,259	18.4	598	8.1
10	2.71	1,258	9.5	580	5.3
30	2.86	1.254	4.2	607	11.3
60	2.99	1.254	2.5	600	7.5
		Concentration NH	4HSO <sub>4</sub> = 80 gran	ns/liter	
0	2.08	1.270	9.4	566	80.0
10	2.11	1.267	2.3	563	80.0
30	2.12	1.267	0.3	564	86.0
60	2.12	1.267	0.3	568	83.0
		Concentration NH	$_{4}^{HSO}_{4} = 375 \text{ gra}$	ams/liter	
0	1.04	1.351	5.9	435	382.0
5	1.05	1.355	2.6	425	386.0
20	1.06	1.360	0.7	434	372.0
60	1.08	1.359	0.4	430	372.0

Table 7. STRIPPING RATE CONSTANTS

Temperature C°	Conc NH <sub>4</sub> HSO <sub>4</sub> g/1	Rate Constant min <sup>-1</sup>
65	0	0.049
65	9.6	0.053
65	72	0.110
65	425	0.110
80	0	0.070
80	9.9	0.070
80	80	0.180
80	375	0.180

# Section VIII APPENDICES

Appendix		Page
Α	Lot Analysis of Chemicals Used	30
В	The Effects of NH <sub>4</sub> HSO <sub>4</sub> on Density, pH, and Composition of Saturated Solutions of	31
	(NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub> at 80°C Using Procedure A	

#### Appendix A

#### LOT ANALYSIS OF CHEMICALS USED

Α.	Ammonium Sulfate, (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub>
	Manufacturer - Matheson, Coleman, and Bell
	Maximum Impurities & Specifications
	Arsenic
	Chloride
	Heavy metals (as Pb)
	Insoluble matter
	Iron
	Nitrate
	pH of a 5% solution
	Phosphate
	Residue after ignition
В.	Ammonium Bisulfate, NH <sub>4</sub> HSO <sub>4</sub>
	Manufacturer - Fisher Scientific Company
	Maximum Impurities
	Chloride
	Iron
	Non-volatile matter
	Other heavy metals (as Pb)
	Chloride

Appendix B THE EFFECTS OF  ${\rm NH_4HSO_4}$  ON DENSITY, pH, AND COMPOSITION OF SATURATED SOLUTIONS OF  ${\rm (NH_4)_2SO_4}$  AT 80°C USING PROCEDURE  ${\rm A}^{\rm a}$ 

Conc (NH <sub>4</sub> ) <sub>2</sub> SO <sub>4</sub>		Conc NH4HSO4			Density	
grams	moles	grams	moles	1	g/cm <sup>3</sup>	
liter	100 moles H <sub>2</sub> 0	liter	100 moles H <sub>2</sub> 0	рН		
Run Number 1						
610	13.0	0	0	4.00	1.249	
396	12.6	` 6	0.15	3.86	1.248	
565	11.6	18	0.42	3.55	1.250	
530	10.7	44	1.00	2.95	1.252	
535	11.44	80	1.96	2.22	1.253	
423	9.69	252	6.62	1,50	1.270	
Run Number 2						
607	13.0	0	. 0	4.02	1.250	
530	10.6	40	0.92	2.91	1.249	
495	9.91	78	1.79	2.61	1.254	
366	9.90	407	12.6	1.47	1.277	
310	9.05	538	18.0	0.98	1.314	

These data are believed incorrect but are included for completeness.

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16. Abstracts The report gives results of a study involving	g data that can be used to evaluate					
pilot-plant operation of an NH3 scrubber with NH4HS	04 regeneration. It determined					
the density, pH, and composition of saturated (NH4)2	SO4 solutions at 50, 65, and					
80°C; effects on density, pH, and composition of add	ing NH4HSO4 to the above sol-					
utions; and the solubility and stripping rates of SO2 is	n saturated solutions of (NH4)2SO4					
containing NH4HSO4 at 65 and 80°C. (NH4)2SO4 solu						
ably with accepted values. Adding NH4HSO4 to the go	tunated solutions lowered (NUA)?					
ably with accepted values. Adding NH4HSO4 to the saturated solutions lowered (NH4)2-						
SO4 solubility, decreased pH, and increased density. SO2 solubility in saturated						
(NH4)2SO4 decreased with both increasing temperature and increasing NH4HSO4						
concentration. SO2 stripping rates were found to be						
concentration except when the pH rose above 2.6. Str	ripping rate depends on temper-					
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