



# Research and Development

ENVIRONMENTAL ASSESSMENT  
OF A COMMERCIAL BOILER FIRED WITH  
A COAL/WASTE PLASTIC MIXTURE  
Volume II. Data Supplement

## Prepared for

Office of Air Quality Planning and Standards

## Prepared by

Air and Energy Engineering Research  
Laboratory  
Research Triangle Park NC 27711

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ENVIRONMENTAL ASSESSMENT OF A COMMERCIAL BOILER  
FIRED WITH A COAL/WASTE PLASTIC MIXTURE

Volume II  
Data Supplement

By

R. DeRosier, H. I. Lips, and L. R. Waterland  
Acurex Corporation  
Energy & Environmental Division  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, California 94039

EPA Contract 68-02-3188

EPA Project Officer: Joseph A. McSorley  
Air and Energy Engineering Research Laboratory  
Research Triangle Park, North Carolina 27711

For

U.S. ENVIRONMENTAL PROTECTION AGENCY  
Office of Research and Development  
Washington, DC 20460

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## SECTION 1

### INTRODUCTION

The purpose of this data supplement is to document data in greater detail than was possible in Volume I (Technical Results) of this report. It is intended to provide sufficient detail for researchers to perform their own analysis of the data obtained. Readers are referred to the technical volume for objectives, description of source emission results, data interpretation, and conclusions.

The remaining sections of this data supplement contain the following information:

Section 2 -- Preliminary Tests and Equipment Calibration: stack velocity traverse and nozzle sizing calculations, equipment calibration records

Section 3 -- Boiler Operating Data: pressures, temperatures, and flowrates; efficiency calculations using the ASME heat loss method

Section 4 -- Sampling Data Sheets: continuous monitor data sheets; operating data tables for EPA Method 5/8 (for particulate mass emissions, SO<sub>2</sub> and SO<sub>3</sub> sampling), SASS (for trace element and semi- and nonvolatile organic sampling), HCl train, and VOST (for volatile organic sampling)

Section 5 -- Analytical Results: fuel and ash sample proximate and ultimate analyses; SASS particulate emissions; Method 5 particulate

emissions; Method 8 sulfur oxides emissions; HCl emissions; trace element emissions by spark source mass spectrometry (SSMS), atomic absorption spectroscopy (AAS), and other methods, and leachable anions analyses by ion chromatography; total chromatographable organic (TCO) and gravimetric (GRAV) results, determination of semivolatile organic priority pollutants by gas chromatography/mass spectrometry (GC/MS), infrared (IR) spectra of total sample extracts; liquid chromatography (LC) separation results with IR spectra of eluted fractions; analyses of VOST traps by GC/MS; N<sub>2</sub>O analyses by gas chromatography/electron capture detector; and biological assay reports.

SECTION 2  
PRELIMINARY TESTS AND EQUIPMENT CALIBRATION

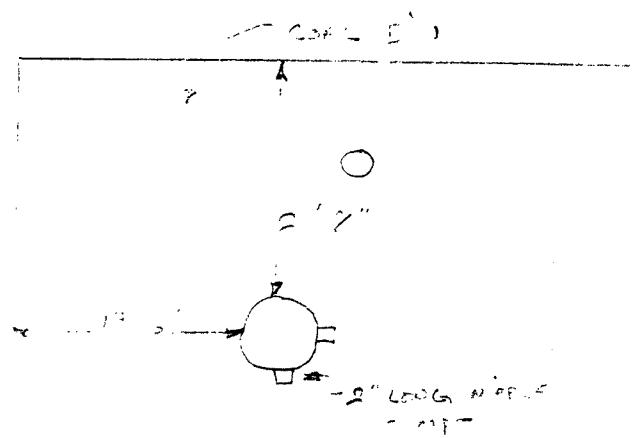
## TRAVERSE POINT LOCATION FOR CIRCULAR DUCTS

PLANT \_\_\_\_\_  
DATE \_\_\_\_\_  
SAMPLING LOCATION \_\_\_\_\_  
INSIDE OF FAR WALL TO  
OUTSIDE OF NIPPLE, (DISTANCE A) \_\_\_\_\_  
INSIDE OF NEAR WALL TO  
OUTSIDE OF NIPPLE, (DISTANCE B) \_\_\_\_\_  
STACK I.D., (DISTANCE A - DISTANCE B) \_\_\_\_\_  
NEAREST UPSTREAM DISTURBANCE \_\_\_\_\_  
NEAREST DOWNSTREAM DISTURBANCE \_\_\_\_\_  
CALCULATOR \_\_\_\_\_

## SCHEMATIC OF SAMPLING LOCATION

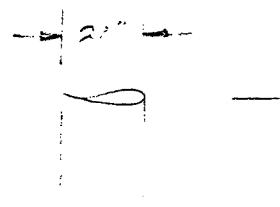
For  $\omega^2 = \omega_0^2$   $\omega = \sqrt{\omega_0^2 - \nu^2} = \sqrt{\omega_0^2 - \nu^2}$

$\omega = \sqrt{\omega_0^2 - \nu^2}$

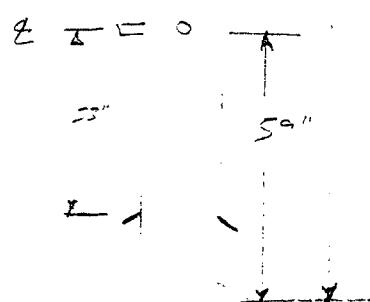


$$\omega = \sqrt{\frac{k}{m}}$$

$$= \sqrt{\frac{4000}{1}} = \sqrt{4000}$$



$$\omega' = \sqrt{\frac{k}{m + c^2/m}}$$



## PRELIMINARY VELOCITY TRAVERSE

PLANT Ex-12-2  
DATE 7-17-77  
LOCATION W. H. CO.  
STACK I.D. 210"  
BAROMETRIC PRESSURE, in. Hg 29.96  
STACK GAUGE PRESSURE, in. H<sub>2</sub>O -1.0  
OPERATORS C. E. C. S.

## SCHEMATIC OF TRAVERSE POINT LAYOUT

ISOKINETIC NOZZLE CALCULATION  
AND  
SAMPLING RATE CALCULATION

Plant ROCK CRAGGS      Performed by BARKER  
 Date JULY 6, 1983  
 Sample Location SAW HOUSE  
 Test No./Type - M58

$$N_d = \left( \frac{\Delta H}{K T_m \Delta P} \right)^{.25}$$

where:  $N_d$  = Nozzle diameter (inches)

|   |            |       |
|---|------------|-------|
| Average pressure differential across the orifice meter (in. H <sub>2</sub> O) | $\Delta H$ | 1.5   |
| Temperature stack gas, average (°F)   | $T_s$      | 275.8 |
| Temperature of gas meter, average (°F)  | $T_m$      | 70    |
| Stack gas velocity pressure (in H <sub>2</sub> O)                             | $\Delta P$ | 0.055 |
| $\left( \frac{(\_) (\_)^4}{(\_) (\_) + 460} \right)^{.25}$                    | $N_d$      | , 461 |

$$\Delta H = K (N_d)^4 \frac{T_m}{T_s} (\Delta P)$$

where:  $\Delta H$  = Pressure differential across the orifice meter (in H<sub>2</sub>O)

|  |            |       |
|--|------------|-------|
| Nozzle diameter, actual (inches)   | $N_d$      | , 387 |
| Temperature of gas meter (°F)  | $T_m$      |       |
| Temperature of stack gas (°F)  | $T_s$      |       |
| Stack gas velocity pressure (in H <sub>2</sub> O)                                | $\Delta P$ |       |
| $\left( (\_) (\_)^4 \left\{ \frac{(\_) + 460}{(\_) + 460} \right\} (\_) \right)$ | $\Delta H$ |       |
| Magic number <u>      </u> ( <u>      </u> ) <sup>4</sup>                        | $K(N_d)^4$ |       |

# ISOKINETIC SAMPLING WORKSHEET

Plant ROCKFACES  
 Date 7/7/83  
 Sample Location SAW HOUSE  
 Test No./Type I-M-5-8

Performed by BAKELIS

$$K = \frac{782.687 (C_p)^2 (1-B_{w0})^2 P_s M_d}{K_o^2 M_s P_m}$$

where: K = Constant of fixed and assumed parameters (dimensionless)

|  |          |   |
|--|----------|---|
| Pitot coefficient (dimensionless)  | $C_p$    | 1.300   |
| Water vapor in the gas stream<br>(proportion by volume)  | $B_{w0}$ | .075  |
| Absolute stack gas pressure (in. Hg)   | $P_s$    | -10   |
| Molecular weight, stack gas dry<br>(1b/1b-mole)  | $M_d$    | CO <sub>2</sub> 13<br>O <sub>2</sub> 7<br>N <sub>2</sub> 28 |
| Orifice coefficient (dimensionless)  | $K_o$    | 0.725   |
| Molecular weight, stack gas wet<br>(1b/1b-mole) $M_d(1-B_{w0}) + 18(B_{w0})$   | $M_s$    |   |
| Absolute meter pressure (in. Hg)   | $P_m$    | 25.24   |
| $\frac{782.687 (\underline{\hspace{1cm}})^2 (1-\underline{\hspace{1cm}})^2 (\underline{\hspace{1cm}}) (\underline{\hspace{1cm}})}{(\underline{\hspace{1cm}})^2 (\underline{\hspace{1cm}}) (\underline{\hspace{1cm}})}$ | K        | 841.373   |

# PRELIMINARY VELOCITY TRAVERSE

PLANT \_\_\_\_\_  
 DATE \_\_\_\_\_  
 LOCATION \_\_\_\_\_  
 STACK I.D. \_\_\_\_\_  
 BAROMETRIC PRESSURE, in. Hg \_\_\_\_\_  
 STACK GAUGE PRESSURE, in. H<sub>2</sub>O \_\_\_\_\_  
 OPERATORS \_\_\_\_\_

## SCHEMATIC OF TRAVERSE POINT LAYOUT

| TRAVERSE<br>POINT<br>NUMBER | VELOCITY<br>HEAD<br>( $\Delta p_s$ ), in. H <sub>2</sub> O | STACK<br>TEMPERATURE<br>(T <sub>s</sub> ), °F |
|-----------------------------|--|---|
|                             | 1.36   | 312   |
|                             | 1.20   | 322   |
|                             | 1.17   | 322   |
|                             | 0.95   | 316   |
|                             | 0.93   | 307   |
|                             | 1.02   | 274   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
|                             |  |   |
| AVERAGE                     | 0.0467   | 309.6   |

| TRAVERSE<br>POINT<br>NUMBER | VELOCITY<br>HEAD<br>( $\Delta p_s$ ), in. H <sub>2</sub> O | STACK<br>TEMPERATURE<br>(T <sub>s</sub> ), °F |
|-----------------------------|--|---|
| 1-                          | 2.77   | 321   |
| 1                           | 1.51   | 320   |
| 2                           | 1.19   | 324   |
| 3                           | 1.15   | 320   |
| 4                           | 1.17   | 321   |
| 5                           | 1.17   | 321   |
| 6                           | 1.17   | 321   |
| 7                           | 1.17   | 321   |
| 8                           | 1.17   | 321   |
| 9                           | 1.17   | 321   |
| 10                          | 1.17   | 321   |
| 11                          | 1.17   | 321   |
| 12                          | 1.17   | 321   |
| 13                          | 1.17   | 321   |
| 14                          | 1.17   | 321   |
| 15                          | 1.17   | 321   |
| 16                          | 1.17   | 321   |
| 17                          | 1.17   | 321   |
| 18                          | 1.17   | 321   |
| 19                          | 1.17   | 321   |
| 20                          | 1.17   | 321   |
| 21                          | 1.17   | 321   |
| 22                          | 1.17   | 321   |
| 23                          | 1.17   | 321   |
| 24                          | 1.17   | 321   |
| 25                          | 1.17   | 321   |
| 26                          | 1.17   | 321   |
| 27                          | 1.17   | 321   |
| 28                          | 1.17   | 321   |
| 29                          | 1.17   | 321   |
| 30                          | 1.17   | 321   |
| 31                          | 1.17   | 321   |
| 32                          | 1.17   | 321   |
| 33                          | 1.17   | 321   |
| 34                          | 1.17   | 321   |
| 35                          | 1.17   | 321   |
| 36                          | 1.17   | 321   |
| 37                          | 1.17   | 321   |
| 38                          | 1.17   | 321   |
| 39                          | 1.17   | 321   |
| 40                          | 1.17   | 321   |
| 41                          | 1.17   | 321   |
| 42                          | 1.17   | 321   |
| 43                          | 1.17   | 321   |
| 44                          | 1.17   | 321   |
| 45                          | 1.17   | 321   |
| 46                          | 1.17   | 321   |
| 47                          | 1.17   | 321   |
| 48                          | 1.17   | 321   |
| 49                          | 1.17   | 321   |
| 50                          | 1.17   | 321   |
| 51                          | 1.17   | 321   |
| 52                          | 1.17   | 321   |
| 53                          | 1.17   | 321   |
| 54                          | 1.17   | 321   |
| 55                          | 1.17   | 321   |
| 56                          | 1.17   | 321   |
| 57                          | 1.17   | 321   |
| 58                          | 1.17   | 321   |
| 59                          | 1.17   | 321   |
| 60                          | 1.17   | 321   |
| 61                          | 1.17   | 321   |
| 62                          | 1.17   | 321   |
| 63                          | 1.17   | 321   |
| 64                          | 1.17   | 321   |
| 65                          | 1.17   | 321   |
| 66                          | 1.17   | 321   |
| 67                          | 1.17   | 321   |
| 68                          | 1.17   | 321   |
| 69                          | 1.17   | 321   |
| 70                          | 1.17   | 321   |
| 71                          | 1.17   | 321   |
| 72                          | 1.17   | 321   |
| 73                          | 1.17   | 321   |
| 74                          | 1.17   | 321   |
| 75                          | 1.17   | 321   |
| 76                          | 1.17   | 321   |
| 77                          | 1.17   | 321   |
| 78                          | 1.17   | 321   |
| 79                          | 1.17   | 321   |
| 80                          | 1.17   | 321   |
| 81                          | 1.17   | 321   |
| 82                          | 1.17   | 321   |
| 83                          | 1.17   | 321   |
| 84                          | 1.17   | 321   |
| 85                          | 1.17   | 321   |
| 86                          | 1.17   | 321   |
| 87                          | 1.17   | 321   |
| 88                          | 1.17   | 321   |
| 89                          | 1.17   | 321   |
| 90                          | 1.17   | 321   |
| 91                          | 1.17   | 321   |
| 92                          | 1.17   | 321   |
| 93                          | 1.17   | 321   |
| 94                          | 1.17   | 321   |
| 95                          | 1.17   | 321   |
| 96                          | 1.17   | 321   |
| 97                          | 1.17   | 321   |
| 98                          | 1.17   | 321   |
| 99                          | 1.17   | 321   |
| 100                         | 1.17   | 321   |
| AVERAGE                     |  |   |

ISOKINETIC NOZZLE CALCULATION  
AND  
SAMPLING RATE CALCULATION

Plant Rock of Ages

Performed by Rakus

Date 7/8/83

Sample Location SAC Hall

Test No./Type 2 M-58

$$N_d = \left( \frac{\Delta H T_s}{K T_m \Delta P} \right)^{.25}$$

where:  $N_d$  = Nozzle diameter (inches)

|   |            |       |
|---|------------|-------|
| Average pressure differential across the orifice meter (in. H <sub>2</sub> O) | $\Delta H$ | 1.5   |
| Temperature stack gas, average (°F)   | $T_s$      | 300.2 |
| Temperature of gas meter, average (°F)  | $T_m$      | 80    |
| Stack gas velocity pressure (in H <sub>2</sub> O)                             | $\Delta P$ | .047  |
| $\left( \frac{(\_) (\_) + 460}{(\_) (\_) + 460 (\_)} \right)^{.25}$           | $N_d$      | .482  |

$$\Delta H = K (N_d)^4 \frac{T_m}{T_s} (\Delta P)$$

where:  $\Delta H$  = Pressure differential across the orifice meter (in H<sub>2</sub>O)

|   |            |       |
|---|------------|-------|
| Nozzle diameter, actual (inches)                          | $N_d$      | 1.387 |
| Temperature of gas meter (°F)                             | $T_m$      |       |
| Temperature of stack gas (°F)                             | $T_s$      |       |
| Stack gas velocity pressure (in H <sub>2</sub> O)         | $\Delta P$ |       |
| $(\_) (\_)^4 \left\{ \frac{+ 460}{+ 460} (\_) \right\}$   | $\Delta H$ |       |
| Magic number <u>839.439</u> ( <u>1.387</u> ) <sup>4</sup> | $K(N_d)^4$ | 18.34 |

# ISOKINETIC SAMPLING WORKSHEET

Plant RIDGE FARMES

Performed by Sarker

Date 7/8/83

Sample Location SMW A/C HOUSE

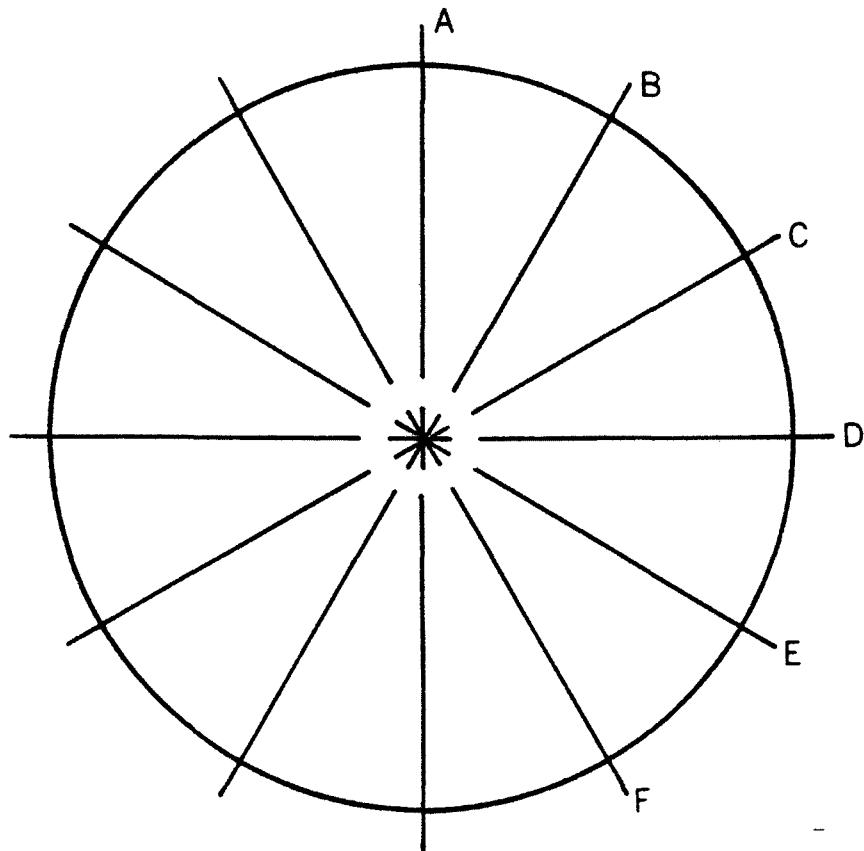
Test No./Type Z-N-58

$$K = \frac{782.687 (C_p)^2 (1-B_{wo})^2 P_s M_d}{K_o^2 M_s P_m}$$

where: K = Constant of fixed and assumed parameters (dimensionless)

|  |          |   |
|--|----------|---|
| Pitot coefficient (dimensionless)  | $C_p$    | ,800                                    |
| Water vapor in the gas stream<br>(proportion by volume)  | $B_{wo}$ | ,075                                    |
| Absolute stack gas pressure (in. Hg)   | $P_s$    | -,10                                    |
| Molecular weight, stack gas dry<br>(lb/lb-mole)  | $M_d$    | $CO_2 - 28$<br>$O_2 - 16$<br>$N_2 - 28$ |
| Orifice coefficient (dimensionless)  | $K_o$    | 1.02<br>,725                            |
| Molecular weight, stack gas wet<br>(lb/lb-mole) $M_d(1-B_{wo}) + 18(B_{wo})$   | $M_s$    |   |
| Absolute meter pressure (in. Hg)   | $P_m$    | 24.4                                    |
| $\frac{782.687 (\underline{\hspace{1cm}})^2 (1-\underline{\hspace{1cm}})^2 (\underline{\hspace{1cm}}) (\underline{\hspace{1cm}})}{(\underline{\hspace{1cm}})^2 (\underline{\hspace{1cm}}) (\underline{\hspace{1cm}})}$ | K        | 339.934                                 |

## NOZZLE MEASUREMENT



DIAMETER  
DIMENSION

A \_\_\_\_\_

B \_\_\_\_\_

C \_\_\_\_\_

D \_\_\_\_\_

E \_\_\_\_\_

F \_\_\_\_\_

AVG. \_\_\_\_\_

NOZZLE SERIAL  
\_\_\_\_\_

DATE  
\_\_\_\_\_

RECORDED BY  
\_\_\_\_\_

## CONTROL MODULE CALIBRATION

Module I.D. D-554  
Date 5-13 / 5-16-83

Barometric Pressure (in. Hg) 30.12 - 30.16  
Primary Meter I.D. \_\_\_\_\_

Ambient Temperature (°F) 70° - 67°  
Operator S.A. Smith

| Orifice Size              | Orifice Reading<br>ΔH<br>(in H <sub>2</sub> O) | Primary Meter Gas Volume<br>V <sub>p</sub><br>(ft <sup>3</sup> ) | Meter Box Gas Volume<br>V <sub>d</sub><br>(ft <sup>3</sup> ) | Temperature                |                             |                             |                            |                             |                             | Time<br>t<br>(min) | Meter Correction Factor<br>α | Orifice Coefficient<br>K <sub>0</sub> |  |  |  |
|---------------------------|--|--|--|----------------------------|-----------------------------|-----------------------------|----------------------------|-----------------------------|-----------------------------|--------------------|------------------------------|---------------------------------------|--|--|--|
|                           |  |  |  | Primary Meter              |                             |                             | Meter Box Meter            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  | Inlet T <sub>pi</sub> (°F) | Outlet T <sub>po</sub> (°F) | Average T <sub>p</sub> (°F) | Inlet T <sub>di</sub> (°F) | Outlet T <sub>do</sub> (°F) | Average T <sub>d</sub> (°F) |                    |                              |                                       |  |  |  |
| Small<br>Orifice<br>0.187 |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
| 2-12                      | .5   | 15.695   | 16.000   | 70 70 70 70                | 70°                         | 72 80 71 80                 | 75.8°                      | 37.6                        | 1.010                       | 0.753              |                              |                                       |  |  |  |
|                           | 1.0  | 14.195   | 14.615   | 70 70 70 70                | 70°                         | 80 83 80 81                 | 81°                        | 24.4                        | 1.011                       | 0.739              |                              |                                       |  |  |  |
|                           | 2.5  | 10.400   | 10.720   | 70 70 70 70                | 70°                         | 83 81 81 81                 | 83°                        | 11.9                        | 1.012                       | 0.701              |                              |                                       |  |  |  |
|                           | 4.0  | 18.710   | 19.190   | 67 67 67 67                | 67°                         | 79 83 73 76                 | 77.8°                      | 16.9                        | 1.015                       | 0.705              |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
| Large<br>Orifice<br>0.358 |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |
|                           |  |  |  |                            |                             |                             |                            |                             |                             |                    |                              |                                       |  |  |  |

$$\alpha = \frac{V_d \left( P_B + \frac{\Delta H}{T_{3.6}} \right) (T_p + 460)}{V_p (P_B) (T_d + 460)}$$

$$K_0 = \frac{V_p}{\alpha \sqrt{\frac{\Delta H (T_d + 460)}{P_B (28.96)}}}$$

| Orifice | Avg. α | Avg. K <sub>0</sub> |
|---------|--------|---------------------|
| Small   |        |                     |
| Medium  | 1.012  | 0.725               |
| Large   |        |                     |

Date 4/13/82

Time

Barometric Pressure 29.88

Ambient Temperature 19.5 °C

Orifice Meter

Orifice Magnehelic 81212 OB 59

Primary Calibration Meter 445598

Control Module D 555

Operators SCHOLTZ

Net Bulk Temperature

## METER CALIBRATION DATA

| Orifice<br>Manometer<br>ΔH <sub>ref</sub><br>(in. w.g.) | Orifice<br>Magnehelic<br>ΔH <sub>G</sub><br>(in. w.g.) | Primary<br>Meter<br>ΔH <sub>P</sub><br>(in. w.g.) | Dry Test<br>Meter<br>P <sub>dg</sub><br>(in. w.g.) | Gas Volume<br>Primary Meter<br>V <sub>p</sub><br>(ft. <sup>3</sup> ) | Gas Volume<br>Dry Test Meter<br>V <sub>d</sub><br>(ft. <sup>3</sup> ) | Temperature                    |                                 |                              |                                |                                 |                              | Time<br>t<br>(min.) | s   | E <sub>0</sub> |  |  |  |  |
|---|--|---|--|--|---|--------------------------------|---------------------------------|------------------------------|--------------------------------|---------------------------------|------------------------------|---------------------|-----|----------------|--|--|--|--|
|   |  |   |  |  |   | Primary Meter                  |                                 |                              | Dry Test Meter                 |                                 |                              |                     |     |                |  |  |  |  |
|   |  |   |  |  |   | Inlet,<br>T <sub>pt</sub> (°F) | Outlet,<br>T <sub>po</sub> (°F) | Avg.<br>T <sub>pa</sub> (°F) | Inlet,<br>T <sub>dt</sub> (°F) | Outlet,<br>T <sub>do</sub> (°F) | Avg.<br>T <sub>da</sub> (°F) |                     |     |                |  |  |  |  |
|   | 0.2  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 0.4  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
| #1  | 0.6  |   |  | 964.643  | 360.515   | 64                             | 63                              |                              | 73                             | 75                              |                              | 20 min              | 0.7 | sec            |  |  |  |  |
|   | 0.8  |   |  | 973.408  | 369.209   | 65                             | 64                              |                              | 74                             | 76                              |                              |                     |     |                |  |  |  |  |
|   | 1.0  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
| #2  | 1.2  |   |  | 974.081  | 369.838   | 64                             | 63                              |                              | 73                             | 74                              |                              | 20 min              | 0.2 | sec            |  |  |  |  |
|   | 1.4  |   |  | 936.255  | 382.256   | 64                             | 64                              |                              | 76                             | 75                              |                              |                     |     |                |  |  |  |  |
|   | 1.6  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
| #3  | 1.8  |   |  | -1002.675  | 398.885   | 64                             | 64                              |                              | 73                             | 75                              |                              | 20 min              | 0.9 | sec            |  |  |  |  |
|   | 2.0  |   |  | 917.839  | 414.273   | 62                             | 65                              |                              | 70                             | 71                              |                              |                     |     |                |  |  |  |  |
|   | 2.2  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
| #4  | 2.4  |   |  | 948.407  | 445.230   | 65                             | 65                              |                              | 70                             | 77                              |                              | 20 min              | 0.7 | sec            |  |  |  |  |
|   | 2.6  |   |  | 925.610  | 462.720   | 60                             | 60                              |                              | 60                             | 78                              |                              |                     |     |                |  |  |  |  |
|   | 2.8  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 3.0  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 3.2  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 3.4  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 3.6  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 3.8  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 4.0  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 4.2  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 4.4  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 4.6  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 4.8  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |
|   | 5.0  |   |  |  |   |                                |                                 |                              |                                |                                 |                              |                     |     |                |  |  |  |  |

Average

2-13

$$\gamma = 0.9908$$

$$K_0 = 0.7126$$

DATE 10-6-82

TIME 65 3

BAROMETRIC PRESSURE 30.18

AMBIENT TEMP 75°

TEST PAPER TIME 2-399 A

STANDARD PIPIE TUBE 31

**TEST SECTION LOCATION**

**OPERATORS**

**NOZZLE SIZE**

### NOZZLE-PITOT SPACING

### PITOT-TC SPACING

## PITOT TUBE CALIBRATION DATA

Average  $C_{p, \text{upper}}$  = 0.843

$$\text{Average } C_{p, \text{ lower}} = 0.834$$

DATE 10-6-85  
TIME 15:0  
BAROMETRIC PRESSURE 30.10  
AMBIENT TEMP 75°

TEST PITOT TUBE 3'-398 6  
STANDARD PITOT TUBE 3'  
TEST SECTION LOCATION  
OPERATORS JEO

NOZZLE SIZE  
NOZZLE-PITOT SPACING  
PITOT-TC SPACING

## PITOT TUBE CALIBRATION DATA

$$\text{Average } \bar{c}_{p, \text{ upper}} = 0.833$$

Average  $C_p$ , lower = 0.847

SECTION 3  
BOILER OPERATING DATA

| Time | Feedwater<br>flow<br>(total gal) | Feedwater<br>temperature<br>(°F) | Steam<br>pressure<br>(psig) | Fuel flow<br>(lb/hr<br>nominal<br>setting) | Comment                      |
|------|----------------------------------|----------------------------------|-----------------------------|--|------------------------------|
| 430  |                                  |                                  |                             |  | Start fuel feed, boiler on   |
| 625  | 20.0                             | --                               | --                          | --   |                              |
| 645  | 231.1                            | 60                               | 7                           | 300  |                              |
| 705  | 268.6                            | 60                               | 7                           | 300  |                              |
| 715  | 281.7                            | 60                               | 7                           | 300  |                              |
| 730  | 335.0                            | 58                               | 2                           | 300  |                              |
| 750  | 400.0                            | 56                               | 2                           | 300  |                              |
| 805  | 457.6                            | 56                               | 2                           | 300  |                              |
| 825  | 552.4                            | 56                               | 0                           | 300  | Increase feedwater flow      |
| 840  | 626.0                            | 56                               | 0                           | 300  |                              |
| 945  | 1,057.0                          | 56                               | 2                           | 300  |                              |
| 1000 | 1,151.0                          | 56                               | 2                           | 300  |                              |
| 1030 | 1,381.1                          | 56                               | 2                           | 300  |                              |
| 1100 | 1,550.0                          | 54                               | 1.5                         | 300  |                              |
| 1130 | 1,738.3                          | 56                               | 2                           | 300  |                              |
| 1145 | 1,846.0                          | 54                               | 2.5                         | 300  |                              |
| 1200 | 1,939.0                          | 55                               | 2.5                         | 300  | SASS start; Method 5/8 start |
| 1215 | 2,044.8                          | 54                               | 2                           | 300  |                              |
| 1230 | 2,148.0                          | 54                               | 2                           | 300  |                              |
| 1245 | 2,217.9                          | 54                               | 2.5                         | 300  |                              |
| 1300 | 2,311.2                          | 54                               | 3                           | 300  |                              |
| 1315 | 2,425.7                          | 54                               | 3                           | 300  | Method 5/8 stop              |
| 1330 | 2,515.7                          | 54                               | 2                           | 300  |                              |
| 1400 | 2,710.3                          | 54                               | 2                           | 300  |                              |
| 1415 | 2,795.1                          | 54                               | 2.5                         | 300  |                              |
| 1430 | 2,873.5                          | 54                               | 2                           | 300  |                              |
| 1445 | 2,970.1                          | 54                               | 1.5                         | 300  |                              |
| 1500 | 3,035.9                          | 54                               | 2                           | 300  |                              |
| 1515 | 3,120.2                          | 54                               | 2                           | 300  | HCl start                    |
| 1530 | 3,204.9                          | 54                               | 2.5                         | 300  |                              |
| 1545 | 3,243.8                          | 54                               | 3                           | 300  | HCl stop                     |
| 1600 | 3,387.8                          | 54                               | 3                           | 300  |                              |
| 1615 | 3,487.5                          | 54                               | 2                           | 300  |                              |
| 1630 | 3,562.1                          | 54                               | 2                           | 300  |                              |
| 1645 | 3,645.4                          | 54                               | 2                           | 300  | SASS stop                    |
| 1700 | 3,720.3                          | 54                               | 2                           | 300  |                              |
| 1715 | 3,802.0                          | 54                               | 2.5                         | 300  |                              |
| 1730 | 3,890.6                          | 54                               | 2                           | 300  | Terminate fuel flow          |

Total fuel fed = 3,094 lb. Collect 405 lb bottom ash, 12.5 lb cyclone hopper ash

ASME TEST FORM  
FOR ABBREVIATED EFFICIENCY TEST

SUMMARY SHEET

PTC 4.1-a(1964)

|  |        | TEST NO.                               | BOILER NO.  | DATE                                       |
|--|--------|--|---|--|
| CWTR OF PLANT  |        | LOCATION                               |   |  |
| TE. CONDUCTED BY   |        | OBJECTIVE OF TEST                      | DURATION  |  |
| BOILER, MAKE & TYPE  |        | RATED CAPACITY                         |   |  |
| STOKER, TYPE & SIZE  |        |  |   |  |
| PULVERIZER, TYPE & SIZE  |        | BURNER, TYPE & SIZE                    |   |  |
| FUEL USED  | MINE   | COUNTY                                 | STATE   | SIZE AS FIRED                              |
| PRESSURES & TEMPERATURES   |        |  |   |  |
| 1 STEAM PRESSURE IN BOILER DRUM  | psia   | 17.0                                   | COAL AS FIRED PROX. ANALYSIS                                      | % wt                                       |
| 2 STEAM PRESSURE AT S. H. OUTLET   | psia   |  | 37 MOISTURE   | 2.7  |
| 3 STEAM PRESSURE AT R. H. INLET  | psia   |  | 38 VOL MATTER   | 7.7  |
| 4 STEAM PRESSURE AT R. H. OUTLET   | psia   |  | 39 FIXED CARBON   | 57   |
| 5 STEAM TEMPERATURE AT S. H. OUTLET  | F      |  | 40 ASH  | 2.1  |
| 6 STEAM TEMPERATURE AT R. H. INLET   | F      |  | TOTAL   | 41 Btu per lb AS FIRED                     |
| 7 STEAM TEMPERATURE AT R.H. OUTLET   | F      |  | 41 Btu per lb AS FIRED  | 13   |
| 8 WATER TEMP. ENTERING (ECON.)(BOILER)                                       | F      | 54                                     | 42 ASH SOFT TEMP.* ASTM METHOD                                    |  |
| FUEL DATA  |        |  |   |  |
| 9 STEAM QUALITY % MOISTURE OR P. P. M.                                       |        | COAL OR OIL AS FIRED ULTIMATE ANALYSIS |   |  |
| 10 AIR TEMP. AROUND BOILER (AMBIENT)   | F      | 61                                     | 43 CARBON   | 54 CO                                      |
| 11 TEMP. AIR FOR COMBUSTION<br>(This is Reference Temperature) †             | F      | 62                                     | 44 HYDROGEN   | 55 CH <sub>4</sub> METHANE                 |
| 12 TEMPERATURE OF FUEL   | F      | 63                                     | 45 OXYGEN   | 56 C <sub>2</sub> H <sub>2</sub> ACETYLENE |
| 13 GAS TEMP. LEAVING (Boiler) (Econ.) (Air Htr.)                             | F      | 64                                     | 46 NITROGEN   | 57 C <sub>2</sub> H <sub>4</sub> ETHYLENE  |
| 14 GAS TEMP. ENTERING AH (If conditions to be corrected to guarantee)        | F      | 65                                     | 47 SULPHUR  | 58 C <sub>2</sub> H <sub>6</sub> ETHANE    |
| UNIT QUANTITIES  |        |  | 40 ASH  | 59 H <sub>2</sub> S                        |
| 15 ENTHALPY OF SAT. LIQUID (TOTAL HEAT)                                      | Btu/lb | 182.1                                  | 37 MOISTURE   | 60 CO <sub>2</sub>                         |
| 16 ENTHALPY OF (SATURATED) (SUPERHEATED) STM.                                | Btu/lb | 1153.2                                 | TOTAL   | TOTAL                                      |
| 17 ENTHALPY OF SAT. FEED TO (BOILER)<br>(ECON.)                              | Btu/lb | 22.1                                   | COAL PULVERIZATION  |  |
| 18 ENTHALPY OF REHEATED STEAM R. H. INLET                                    | Btu/lb |  | 48 GRINDABILITY INDEX*  | 62 DENSITY 68 F ATM. PRESS.                |
| 19 ENTHALPY OF REHEATED STEAM R. H.<br>OUTLET                                | Btu/lb |  | 49 FINENESS % THRU 50 M*  | 63 Btu PER CU FT                           |
| 20 HEAT ABS/LB OF STEAM (ITEM 16 - ITEM 17)                                  | Btu/lb | 1131.2                                 | 50 FINENESS % THRU 200 M*   | 41 Btu PER LB                              |
| 21 HEAT ABS/LB R.H. STEAM (ITEM 19 - ITEM 18)                                | Btu/lb |  | 64 INPUT-OUTPUT<br>EFFICIENCY OF UNIT %                           | ITEM 31 x 100<br>ITEM 29                   |
| 22 DRY REFUSE (ASH PIT + FLY ASH) PER LB<br>AS FIRED FUEL                    | lb/lb  | 3.4                                    | HEAT LOSS EFFICIENCY  |  |
| 23 Btu PER LB IN REFUSE (WEIGHTED AVERAGE)                                   | Btu/lb | 72.7                                   | 65 HEAT LOSS DUE TO DRY GAS                                       |  |
| 24 CARBON BURNED PER LB AS FIRED FUEL  | lb/lb  | 3.8                                    | 66 HEAT LOSS DUE TO MOISTURE IN FUEL                              |  |
| 25 DRY GAS PER LB AS FIRED FUEL BURNED                                       | lb/lb  | 1.7                                    | 67 HEAT LOSS DUE TO H <sub>2</sub> O FROM COMB. OF H <sub>2</sub> | 4.2  |
| HOURLY QUANTITIES  |        |  |   |  |
| 26 ACTUAL WATER EVAPORATED   | lb/hr  |  | 68 HEAT LOSS DUE TO COMBUST. IN REFUSE                            |  |
| 27 REHEAT STEAM FLOW   | lb/hr  |  | 69 HEAT LOSS DUE TO RADIATION                                     |  |
| 28 RATE OF FUEL FIRING (AS FIRED wt)   | lb/hr  |  | 70 UNMEASURED LOSSES  |  |
| 29 TOTAL HEAT INPUT (Item 28 x Item 41)<br>1000                              | kB/hr  |  | 71 TOTAL  |  |
| 30 HEAT OUTPUT IN BLOW-DOWN WATER  | kB/hr  |  | 72 EFFICIENCY = (100 - Item 71)                                   |  |
| 31 TOTAL HEAT (Item 26 x Item 20)+(Item 27 x Item 21)+Item 30<br>OUTPUT 1000 | kB/hr  |  |   |  |
| FLUE GAS ANAL. (BOILER)(ECON) (AIR HTR) OUTLET                               |        |  |   |  |
| 32 CO <sub>2</sub>   | % VOL  | 12.1                                   |   |  |
| 33 O <sub>2</sub>  | % VOL  | 7.1                                    |   |  |
| 34 CO  | % VOL  | 1.1                                    |   |  |
| 35 N <sub>2</sub> (BY DIFFERENCE)  | % VOL  | 5.1                                    |   |  |
| 36 EXCESS AIR  | %      | 2.7                                    |   |  |

\* Not Required for Efficiency Testing

3-4

† For Point of Measurement See Par. 7.2.8.1-PTC 4.1-1964

## CALCULATION SHEET

ASME TEST FORM  
FOR ABBREVIATED EFFICIENCY TEST

Revised September, 1965

| OWNER OF PLANT   | TEST NO.             | BOILER NO.                                      | DATE  |
|--|----------------------|---|---|
| 30 HEAT OUTPUT IN BOILER BLOW-DOWN WATER = LB OF WATER BLOW-DOWN PER HR X  |                      | [ ITEM 15    ITEM 17 ]<br>..... - .....<br>1000 | kg/hr   |
| 24 If impractical to weigh refuse, this item can be estimated as follows :<br><br>DRY REFUSE PER LB OF AS FIRED FUEL = $\frac{\% \text{ ASH IN AS FIRED COAL}}{100 - \% \text{ COMB. IN REFUSE SAMPLE}}$   |                      |   |   |
| 25 CARBON BURNED PER LB AS FIRED FUEL = $\frac{\text{ITEM 43}}{100} - \left[ \frac{\text{ITEM 22}}{14,500} \times \frac{\text{ITEM 23}}{14,500} \right] = \dots \dots$   |                      |   | NOTE: IF FLUE DUST & ASH PIT REFUSE DIFFER MATERIALLY IN COMBUSTIBLE CONTENT, THEY SHOULD BE ESTIMATED SEPARATELY. SEE SECTION 7, COMPUTATIONS. |
| 26 DRY GAS PER LB AS FIRED FUEL = $\frac{11\text{CO}_2 + 8\text{O}_2 + 7(\text{N}_2 + \text{CO})}{3(\text{CO}_2 + \text{CO})} \times (\text{LB CARBON BURNED PER LB AS FIRED FUEL} + \frac{3}{8} \text{S})$<br>BURNED .<br>= $11 \times \frac{\text{ITEM 32}}{14,500} + 8 \times \frac{\text{ITEM 33}}{14,500} + 7 \left( \frac{\text{ITEM 35}}{14,500} + \frac{\text{ITEM 34}}{14,500} \right) \times \left[ \frac{\text{ITEM 24}}{14,500} + \frac{\text{ITEM 47}}{14,500} \right] = \dots \dots$ |                      |   |   |
| 36 EXCESS AIR = $100 \times \frac{\text{O}_2 - \frac{\text{CO}}{2}}{.2682\text{N}_2 - (\text{O}_2 - \frac{\text{CO}}{2})} = 100 \times \frac{\text{ITEM 33} - \frac{\text{ITEM 34}}{2}}{.2682(\text{ITEM 35}) - (\text{ITEM 33} - \frac{\text{ITEM 34}}{2})} = \dots \dots$  |                      |   |   |
|  | HEAT LOSS EFFICIENCY | Btu/lb AS FIRED FUEL                            | $\frac{\text{LOSS}}{\text{HHV}} \times \frac{100}{100} =$<br>LOSS %   |
| 65 HEAT LOSS DUE TO DRY GAS = $\frac{\text{LB DRY GAS PER LB AS FIRED FUEL} \times C_p \times (\text{lg}_g - \text{lg}_{air})}{\text{Unit}} = \frac{\text{ITEM 25} \times 0.24 (\text{ITEM 13}) - (\text{ITEM 11})}{\dots \dots} = \dots \dots$  |                      |   | $\frac{65}{41} \times 100 = \dots \dots$  |
| 66 HEAT LOSS DUE TO MOISTURE IN FUEL = $\frac{\text{LB H}_2\text{O PER LB AS FIRED FUEL} \times [(\text{ENTHALPY OF VAPOR AT 1 PSIA & T GAS LG}) - (\text{ENTHALPY OF LIQUID AT T AIR})]}{\dots \dots} = \frac{\text{ITEM 37} \times [(\text{ENTHALPY OF VAPOR AT 1 PSIA & T ITEM 13}) - (\text{ENTHALPY OF LIQUID AT T ITEM 11})]}{100} = \dots \dots$  |                      |   | $\frac{66}{41} \times 100 = \dots \dots$  |
| 67 HEAT LOSS DUE TO H <sub>2</sub> O FROM COMB. OF H <sub>2</sub> = $9\text{H}_2 \times [(\text{ENTHALPY OF VAPOR AT 1 PSIA & T GAS LG}) - (\text{ENTHALPY OF LIQUID AT T AIR})]$<br>= $9 \times \frac{\text{ITEM 44}}{100} \times [(\text{ENTHALPY OF VAPOR AT 1 PSIA & T ITEM 13}) - (\text{ENTHALPY OF LIQUID AT T ITEM 11})] = \dots \dots$  |                      |   | $\frac{67}{41} \times 100 = \dots \dots$  |
| 68 HEAT LOSS DUE TO COMBUSTIBLE IN REFUSE = $\frac{\text{ITEM 22} \times \text{ITEM 23}}{\dots \dots \dots} = \dots \dots$   |                      |   | $\frac{68}{41} \times 100 = \dots \dots$  |
| 69 HEAT LOSS DUE TO RADIATION = $\frac{\text{TOTAL BTU RADIATION LOSS PER HR}}{\text{LB AS FIRED FUEL} - \text{ITEM 28}} = \dots \dots$  |                      |   | $\frac{69}{41} \times 100 = \dots \dots$  |
| 70 UNMEASURED LOSSES **  |                      |   | $\frac{70}{41} \times 100 = \dots \dots$  |
| 71 TOTAL   |                      |   |   |
| 2 EFFICIENCY = (100 - ITEM 71)   |                      |   | 77.3  |

† For rigorous determination of excess air see Appendix 9.2 - PTC 4.1-1964

\* If losses are not measured, use ABMA Standard Radiation Loss Chart, Fig. 8, PTC 4.1-1964

\*\* Unmeasured losses listed in PTC 4.1 but not tabulated above may be provided for by assigning a mutually agreed upon value for Item 70.

7-7-83

| Time | Feedwater<br>flow<br>(total gal) | Feedwater<br>temperature<br>(°F) | Steam<br>pressure<br>(psig) | Fuel flow<br>(lb/hr<br>nominal<br>setting) | Comment                        |
|------|----------------------------------|----------------------------------|-----------------------------|--|--------------------------------|
| 530  |                                  |                                  |                             |  | Start fuel feed, boiler on     |
| 830  | 4,733.5                          | 55                               | 2                           | 300  |                                |
| 845  | 4,799.4                          | 55                               | 2.5                         | 300  |                                |
| 900  | 4,860.9                          | 56                               | 2                           | 400  | SASS start; increase fuel flow |
| 915  | 4,924.8                          | 54                               | 3                           | 400  | Method 5/8-2 start             |
| 930  | 5,012.7                          | 54                               | 2                           | 400  |                                |
| 945  | 5,097.8                          | 55                               | 2.5                         | 400  |                                |
| 1000 | 5,185.3                          | 55                               | 2                           | 400  |                                |
| 1015 | 5,278.0                          | 54                               | 2.5                         | 400  |                                |
| 1030 | 5,363.0                          | 54                               | 3.5                         | 400  | Method 5/8-2 stop              |
| 1045 | 5,473.6                          | 54                               | 2.5                         | 400  |                                |
| 1100 | 5,555.1                          | 54                               | 4                           | 400  |                                |
| 1115 | 5,660.8                          | 54                               | 3                           | 400  |                                |
| 1130 | 5,785.9                          | 54                               | 3                           | 400  |                                |
| 1145 | 5,892.1                          | 55                               | 3.5                         | 400  | HC1-2 start                    |
| 1215 | 6,093.0                          | 55                               | 3                           | 400  | HC1-2 stop                     |
| 1230 | 6,196.4                          | 55                               | 3                           | 400  |                                |
| 1245 | 6,287.5                          | 55                               | 4                           | 400  |                                |
| 1300 | 6,391.6                          | 54                               | 4                           | 400  |                                |
| 1315 | 6,483.5                          | 54                               | 4                           | 400  |                                |
| 1330 | 6,603.1                          | 54                               | 4                           | 400  | HC1-3 start                    |
| 1345 | 6,708.1                          | 54                               | 3.5                         | 400  |                                |
| 1400 | 6,816.5                          | 54                               | 3.5                         | 400  | SASS stop, HC1-3 stop          |
| 1415 | 6,922.7                          | 54                               | 3.5                         | 400  |                                |
| 1430 | 7,003.8                          | 54                               | 3.5                         | 400  |                                |
| 1445 | 7,111.2                          | 54                               | 3                           | 400  |                                |
| 1500 | 7,237.2                          | 54                               | 4.5                         | 400  |                                |
| 1515 | 7,320.0                          | 54                               | 3.5                         | 400  |                                |
| 1530 | 7,417.7                          | 54                               | 4                           | 300  |                                |
| 1545 | 7,503.8                          | 54                               | 7                           | 200  | VOST start                     |
| 1600 | 7,585.2                          | 55                               | 7                           | 200  |                                |
| 1615 | 7,670.0                          | 55                               | 7.5                         | 200  | VOST stop                      |
| 1630 | 7,747.0                          | 54                               | 4.5                         | 200  | Method 5/8-3 start             |
| 1645 | 7,815.6                          | 56                               | 2                           | 200  |                                |
| 1700 | 7,887.0                          | 56                               | 1                           | 200  |                                |
| 1715 | 7,948.1                          | 57                               | 1                           | 200  |                                |
| 1730 | 7,976.1                          | 57                               | 1                           | 200  |                                |
| 1745 | 8,018.6                          | 57                               | (0.5)                       | 200  | Method 4/8-3 stop              |
| 1752 | 8,032.0                          | 57                               | 0                           | 200  | Terminate fuel flow            |

Total fuel feed = 2,976.5 lb = 2,489 lb coal + 487.5 lb PET. Collect 237.5 lb bottom ash, 8 lb cyclone hopper ash.

|                          |   |                     |            |   |                          |   |                    |
|--------------------------|---|---------------------|------------|---|--------------------------|---|--------------------|
| WATER OF PLANT           |   | TEST NO.            | BOILER NO. | DATE  |                          |   |                    |
| E. CONDUCTED BY          |   | LOCATION            |            |   |                          |   |                    |
| BOILER, MAKE & TYPE      |   | OBJECTIVE OF TEST   |            | DURATION  |                          |   |                    |
| TOKER, TYPE & SIZE       |   | RATED CAPACITY      |            |   |                          |   |                    |
| PULVERIZER, TYPE & SIZE  |   | BURNER, TYPE & SIZE |            |   |                          |   |                    |
| FUEL USED                |   | COUNTY              | STATE      | SIZE AS FIRED   |                          |   |                    |
| PRESSURES & TEMPERATURES |   |                     |            |   | FUEL DATA                |   |                    |
| 1                        | STEAM PRESSURE IN BOILER DRUM   | psia                | 17.7       | COAL AS FIRED<br>PROX. ANALYSIS                                   | % wt                     | OIL                                     |                    |
| 2                        | STEAM PRESSURE AT S. H. OUTLET  | psia                |            | 37 MOISTURE   | 51                       | FLASH POINT F*                          |                    |
| 3                        | STEAM PRESSURE AT R. H. INLET   | psia                |            | 38 VOL MATTER   | 52                       | Sp. Gravity Deg. API*                   |                    |
| 4                        | STEAM PRESSURE AT R. H. OUTLET  | psia                |            | 39 FIXED CARBON   | 53                       | VISCOSITY AT SSU*<br>BURNER SSF         |                    |
| 5                        | STEAM TEMPERATURE AT S. H. OUTLET   | F                   |            | 40 ASH  | 44                       | TOTAL HYDROGEN<br>% wt                  |                    |
| 6                        | STEAM TEMPERATURE AT R.H. INLET   | F                   |            | TOTAL   |                          | 41 Btu per lb                           |                    |
| 7                        | STEAM TEMPERATURE AT R.H. OUTLET  | F                   |            | 41 Btu per lb AS FIRED  | 37.2                     |   |                    |
| 8                        | WATER TEMP. ENTERING (ECON.) (BOILER)                                     | F                   | 55         | 42 ASH SOFT TEMP.*<br>ASTM METHOD                                 | GAS % VOL                |   |                    |
| 9                        | STEAM QUALITY % MOISTURE OR P.P.M.  |                     |            | COAL OR OIL AS FIRED<br>ULTIMATE ANALYSIS                         | 54                       | CO                                      |                    |
| 0                        | AIR TEMP. AROUND BOILER (AMBIENT)   | F                   | 63         | 43 CARBON   | 55                       | CH <sub>4</sub> METHANE                 |                    |
| 1                        | TEMP. AIR FOR COMBUSTION<br>(This is Reference Temperature) †             | F                   | 63         | 44 HYDROGEN   | 56                       | C <sub>2</sub> H <sub>2</sub> ACETYLENE |                    |
| 2                        | TEMPERATURE OF FUEL   | F                   |            | 45 OXYGEN   | 57                       | C <sub>2</sub> H <sub>4</sub> ETHYLENE  |                    |
| 3                        | GAS TEMP. LEAVING (Boiler) (Econ.) (Air Htr.)                             | F                   | 72         | 46 NITROGEN   | 58                       | C <sub>2</sub> H <sub>6</sub> ETHANE    |                    |
| 4                        | GAS TEMP. ENTERING AH (If conditions to be<br>corrected to guarantee)     | F                   |            | 47 SULPHUR  | 59                       | H <sub>2</sub> S                        |                    |
|                          | UNIT QUANTITIES   |                     |            | 40 ASH  | 60                       | CO <sub>2</sub>                         |                    |
| 5                        | ENTHALPY OF SAT. LIQUID (TOTAL HEAT)                                      | Btu/lb              | 18.0       | 37 MOISTURE   | 61                       | H <sub>2</sub> HYDROGEN                 |                    |
| 6                        | ENTHALPY OF (SATURATED) (SUPERHEATED)<br>STM.                             | Btu/lb              | 22.1       | TOTAL   |                          | TOTAL                                   |                    |
| 7                        | ENTHALPY OF SAT. FEED TO (BOILER)<br>(ECON.)                              | Btu/lb              | 23.1       | COAL PULVERIZATION  |                          | TOTAL HYDROGEN<br>% wt                  |                    |
| 8                        | ENTHALPY OF REHEATED STEAM R. H. INLET                                    | Btu/lb              |            | 48 GRINDABILITY<br>INDEX*   | 62                       | DENSITY 68 F<br>ATM. PRESS.             |                    |
| 9                        | ENTHALPY OF REHEATED STEAM R. H.<br>OUTLET                                | Btu/lb              |            | 49 FINENESS % THRU<br>50 M*                                       | 63                       | Btu PER CU FT                           |                    |
| 10                       | HEAT ABS/LB OF STEAM (ITEM 16 - ITEM 17)                                  | Btu/lb              | 113.2      | 50 FINENESS % THRU<br>200 M*                                      | 41                       | Btu PER LB                              |                    |
| 11                       | HEAT ABS/LB R. H. STEAM (ITEM 19 - ITEM 18)                               | Btu/lb              |            | 64 INPUT-OUTPUT<br>EFFICIENCY OF UNIT %                           | ITEM 31 x 100<br>ITEM 29 |   |                    |
| 12                       | DRY REFUSE (ASH PIT + FLY ASH) PER LB<br>AS FIRED FUEL                    | lb/lb               | 0.027      | HEAT LOSS EFFICIENCY  |                          | Btu/lb<br>A. F. FUEL                    | % of A. F.<br>FUEL |
| 13                       | Btu PER LB IN REFUSE (WEIGHTED AVERAGE)                                   | Btu/lb              | 19.4       | 65 HEAT LOSS DUE TO DRY GAS                                       |                          |   | 7.5                |
| 14                       | CARBON BURNED PER LB AS FIRED FUEL  | lb/lb               | 17.0       | 66 HEAT LOSS DUE TO MOISTURE IN FUEL                              |                          |   | 0.16               |
| 15                       | DRY GAS PER LB AS FIRED FUEL BURNED                                       | lb/lb               | 13.7       | 67 HEAT LOSS DUE TO H <sub>2</sub> O FROM COMB. OF H <sub>2</sub> |                          |   | -1.3               |
|                          | HOURLY QUANTITIES   |                     |            | 68 HEAT LOSS DUE TO COMBUST. IN REFUSE                            |                          |   |                    |
| 26                       | ACTUAL WATER EVAPORATED   | lb/hr               |            | 69 HEAT LOSS DUE TO RADIATION                                     |                          |   |                    |
| 27                       | REHEAT STEAM FLOW   | lb/hr               |            | 70 UNMEASURED LOSSES  |                          |   |                    |
| 28                       | RATE OF FUEL FIRING (AS FIRED wt)   | lb/hr               |            | 71 TOTAL  |                          |   |                    |
| 29                       | TOTAL HEAT INPUT (Item 28 x Item 41)<br>1000                              | kB/hr               |            | 72 EFFICIENCY = (100 - Item 71)                                   |                          |   | 71                 |
| 30                       | HEAT OUTPUT IN BLOW-DOWN WATER  | kB/hr               |            |   |                          |   |                    |
| 31                       | TOTAL HEAT (Item 26 x Item 20)+(Item 27 x Item 21)+Item 30<br>OUTPUT 1000 | kB/hr               |            |   |                          |   |                    |
|                          | FLUE GAS ANAL. (BOILER) (ECON) (AIR HTR) OUTLET                           |                     |            |   |                          |   |                    |
| 32                       | CO <sub>2</sub>   | % VOL               | 12.9       |   |                          |   |                    |
| 33                       | O <sub>2</sub>  | % VOL               | 5.2        |   |                          |   |                    |
| 34                       | CO  | % VOL               | 1.1        |   |                          |   |                    |
| 35                       | N <sub>2</sub> (BY DIFFERENCE)  | % VOL               | 1.1        |   |                          |   |                    |
| 36                       | EXCESS AIR  | %                   | 77         |   |                          |   |                    |

ASME TEST FORM  
CALCULATION SHEET FOR ABBREVIATED EFFICIENCY TEST Revised September, 1965

| OWNER OF PLANT |  | TEST NO. | BOILER NO.                                  | DATE  |
|----------------|--|----------|---|---|
| 30             | HEAT OUTPUT IN BOILER BLOW-DOWN WATER = LB OF WATER BLOW-DOWN PER HR X   |          | ITEM 15    ITEM 17<br>..... - .....<br>1000 | kB/hr<br>.....  |
| 24             | If impractical to weigh refuse, this item can be estimated as follows :<br><br>DRY REFUSE PER LB OF AS FIRED FUEL = $\frac{\% \text{ ASH IN AS FIRED COAL}}{100 - \% \text{ COMB. IN REFUSE SAMPLE}}$  |          |   | NOTE: IF FLUE DUST & ASH PIT REFUSE DIFFER MATERIALLY IN COMBUSTIBLE CONTENT, THEY SHOULD BE ESTIMATED SEPARATELY. SEE SECTION 7, COMPUTATIONS. |
| 25             | CARBON BURNED PER LB AS FIRED FUEL = $\frac{\text{ITEM 43}}{100} - \left[ \frac{\text{ITEM 22}}{14,500} \times \frac{\text{ITEM 23}}{14,500} \right] = \dots \dots$  |          |   |   |
| 26             | DRY GAS PER LB AS FIRED FUEL = $\frac{11\text{CO}_2 + 8\text{O}_2 + 7(\text{N}_2 + \text{CO})}{3(\text{CO}_2 + \text{CO})} \times (\text{LB CARBON BURNED PER LB AS FIRED FUEL} + \frac{3}{8})$<br>= $\frac{11 \times \text{ITEM 32} + 8 \times \text{ITEM 33}}{3 \times \text{ITEM 32}} + 7 \left( \frac{\text{ITEM 35}}{14,500} + \frac{\text{ITEM 34}}{14,500} \right) \times \left[ \frac{\text{ITEM 24}}{267} + \frac{\text{ITEM 47}}{267} \right] = \dots \dots$ |          |   |   |
| 36             | EXCESS AIR = $100 \times \frac{\text{O}_2 - \frac{\text{CO}}{2}}{.2682\text{N}_2 - (\text{O}_2 - \frac{\text{CO}}{2})} = 100 \times \frac{\text{ITEM 33} - \frac{\text{ITEM 34}}{2}}{.2682(\text{ITEM 35}) - (\text{ITEM 33} - \frac{\text{ITEM 34}}{2})} = \dots \dots$   |          |   |   |
| 65             | HEAT LOSS DUE TO DRY GAS FIRED FUEL = $\frac{\text{LB DRY GAS PER LB AS FIRED FUEL} \times C_p \times (\text{t}_{vg} - \text{t}_{air})}{\text{Unit}} = \frac{\text{ITEM 25} \times 0.24 (\text{ITEM 13}) - (\text{ITEM 11})}{\text{Unit}} = \dots \dots$   |          | BTU/lb AS FIRED FUEL                        | $\frac{\text{LOSS}}{\text{HHV}} \times 100 =$<br>$\frac{65}{41} \times 100 =$<br>.....  |
| 66             | HEAT LOSS DUE TO MOISTURE IN FUEL = $\frac{\text{LB H}_2\text{O PER LB AS FIRED FUEL} \times [(\text{ENTHALPY OF VAPOR AT 1 PSIA & T GAS LYG}) - (\text{ENTHALPY OF LIQUID AT T AIR})]}{100} = \frac{\text{ITEM 37} \times [(\text{ENTHALPY OF VAPOR AT 1 PSIA & T ITEM 13}) - (\text{ENTHALPY OF LIQUID AT T ITEM 11})]}{100} = \dots \dots$  |          |   | $\frac{66}{41} \times 100 =$<br>.....   |
| 67             | HEAT LOSS DUE TO H <sub>2</sub> O FROM COMB. OF H <sub>2</sub> = $9\text{H}_2 \times [(\text{ENTHALPY OF VAPOR AT 1 PSIA & T GAS LYG}) - (\text{ENTHALPY OF LIQUID AT T AIR})]$<br>= $9 \times \frac{\text{ITEM 44}}{100} \times [(\text{ENTHALPY OF VAPOR AT 1 PSIA & T ITEM 13}) - (\text{ENTHALPY OF LIQUID AT T ITEM 11})] = \dots \dots$  |          |   | $\frac{67}{41} \times 100 =$<br>.....   |
| 68             | HEAT LOSS DUE TO COMBUSTIBLE IN REFUSE = $\frac{\text{ITEM 22}}{\dots \dots} \times \frac{\text{ITEM 23}}{\dots \dots} = \dots \dots$  |          |   | $\frac{68}{41} \times 100 =$<br>.....   |
| 69             | HEAT LOSS DUE TO RADIATION = $\frac{\text{TOTAL BTU RADIATION LOSS PER HR}}{\text{LB AS FIRED FUEL} - \text{ITEM 28}} = \dots \dots$   |          |   | $\frac{69}{41} \times 100 =$<br>.....   |
| 70             | UNMEASURED LOSSES **   |          |   | $\frac{70}{41} \times 100 =$<br>.....   |
| 71             | TOTAL  |          |   | .....   |
| 2              | EFFICIENCY = $(100 - \text{ITEM 71})$  |          |   | .....   |

† For rigorous determination of excess air see Appendix 9.2 - PTC 4.1-1964

\* If losses are not measured, use ABMA Standard Radiation Loss Chart, Fig. 8, PTC 4.1-1964

\*\* Unmeasured losses listed in PTC 4.1 but not tabulated above may be provided for by assigning a mutually agreed upon value for Item 70.

SECTION 4  
SAMPLING DATA SHEETS

4.1 CONTINUOUS MONITOR EMISSION DATA

4.2 FIELD DATA SHEETS FOR EPA METHOD 5/8, SASS, HC1, AND VOST TRAINS

#### 4.1 CONTINUOUS MONITOR EMISSION DATA

Plant Plant 1Location Amarillo, TexasDate 7-1-83

## CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Instrument<br>Van<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | Heated Sample Line Analysis (Wet) |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |             |                          |                          |                       |                        |           |             |               |                                  |
|--------------------------|--------------------------------|-----|--|--|-----------------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|-------------|---------------|----------------------------------|
|                          | WBT                            | DBT |  |  | NO <sup>a</sup><br>(ppm)          | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) | CO<br>(ppm) | TUHC<br>(ppm) | Sample Gas<br>Temperatur<br>(°F) |
|                          |                                |     |  |  |                                   |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |           |             |               |                                  |
| 1150                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 6.5                      | 11.5                     | 4.5                   | 16                     |           |             |               |                                  |
| 1155                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 6.6                      | 12.5                     | 4.6                   | 17                     |           |             |               |                                  |
| 1200                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 6.7                      | 12.5                     | 4.7                   | 17                     |           |             |               |                                  |
| 1205                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 7.0                      | 17.5                     | 4.6                   | 17                     |           |             |               |                                  |
| 1210                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 205         | 7.5                      | 16                       | 4.0                   | 17                     |           |             |               |                                  |
| 1215                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 205         | 7.5                      | 17                       | 4.0                   | 17                     |           |             |               |                                  |
| 1220                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 7.5                      | 12.5                     | 4.7                   | 17                     |           |             |               |                                  |
| 1225                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 6.7                      | 12.5                     | 4.6                   | 17                     |           |             |               |                                  |
| 1230                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 6.5                      | 12.5                     | 4.5                   | 17                     |           |             |               |                                  |
| 1235                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 7.0                      | 17.5                     | 4.6                   | 17                     |           |             |               |                                  |
| 1240                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 7.5                      | 17.5                     | 4.6                   | 17                     |           |             |               |                                  |
| 1245                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 7.5                      | 17.5                     | 4.6                   | 17                     |           |             |               |                                  |
| 1250                     |                                |     | 75                                       |  |                                   |  |                                       |                                       |                                       |                                   |  | 210         | 7.5                      | 17.5                     | 4.6                   | 17                     |           |             |               |                                  |

<sup>a</sup>NO = direct sample measurement (no conversion)<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

<sup>d</sup>NO<sub>2</sub> = NO<sub>x</sub> - NO

<sup>e</sup>NH<sub>3</sub> = (NO<sub>x</sub> + NH<sub>3</sub>) - NO<sub>x</sub>

Notes:

Plant 66-1  
 Location Sainte-Juste P.W.  
 Date 1-6-85

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |             |                          |                          |                       |                        |           |             |               |                                   |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|-------------|---------------|-----------------------------------|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) | CO<br>(ppm) | TUHC<br>(ppm) | Sample Gas<br>Temperature<br>(°F) |
|                          |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |           |             |               |                                   |
| 1255                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 155         | 148                      | 2.1                      | 8.3                   | 6.5                    | 6         |             |               |                                   |
| 1300                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 155         | 143                      | 2.4                      | 7.3                   | 9.5                    | 6         |             |               |                                   |
| 1305                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 160         | 140                      | 2.6                      | 10.0                  | 10.0                   | 6         |             |               |                                   |
| 1310                     |                                |     |                                    |  | 155  | 145                      |  |                                       |                                       |                                       |                                   |  | 155         | 6.5                      | 11.1                     | 17.0                  | 5                      |           |             |               |                                   |
| 1315                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 215         | 6.5                      | 11.2                     | 17.0                  | 1                      |           |             |               |                                   |
| 1320                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 210         | 6.5                      | 11.1                     | 18                    | 11                     |           |             |               |                                   |
| 1325                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 205         | 7.0                      | 12.2                     | 17.5                  | 12                     |           |             |               |                                   |
| 1330                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 195         | 6.5                      | 12.5                     | 18.0                  | 11                     |           |             |               |                                   |
| 1335                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 170         | 5.9                      | 6.5                      | 12.6                  | 17.0                   | 9         |             |               |                                   |
| 1340                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 165         | 6.5                      | 12.6                     | 17.0                  | 19                     |           |             |               |                                   |
| 1345                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 165         | 6.8                      | 12.2                     | 17.0                  | 6                      |           |             |               |                                   |
| 1350                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 170         | 6.5                      | 12.7                     | 20.0                  | 16                     |           |             |               |                                   |
| 1355                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 170         | 7.0                      | 12.7                     | 20.0                  | 12                     |           |             |               |                                   |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

<sup>d</sup>NO<sub>2</sub> = NO<sub>x</sub> - NO

<sup>e</sup>NH<sub>3</sub> = (NO<sub>x</sub> + NH<sub>3</sub>) - NO<sub>x</sub>

Notes:

Plant Kellogg's  
 Location Saskatoon, Alberta  
 Date 7-6-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       | Cold Sample Line Analysis (Dry)   |  |             |                          |                          |                       |                        |           |             |               |                                  |  |  |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|-------------|---------------|----------------------------------|--|--|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) | CO<br>(ppm) | TUHC<br>(ppm) | Sample Ga<br>Temperature<br>(°F) |  |  |
|                          |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |           |             |               |                                  |  |  |
| 1400                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  | 6.5         | 124                      |                          | 310                   | 10                     |           |             |               |                                  |  |  |
| 1405                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  | 6.0         | 134                      |                          | 310                   | 8                      |           |             |               |                                  |  |  |
| 1410                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 205  | 6.0         | 132                      |                          | 310                   | 10                     |           |             |               |                                  |  |  |
| 1415                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 210  | 6.3         | 134                      |                          | 310                   | 10                     |           |             |               |                                  |  |  |
| 1420                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 145  | 6.7         | 11.3                     |                          | 300                   | 12                     |           |             |               |                                  |  |  |
| 1425                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  | 7.2         | 11.6                     |                          | 300                   | 12                     |           |             |               |                                  |  |  |
| 1430                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 195  | 7.5         | 10.9                     |                          | 300                   | 13                     |           |             |               |                                  |  |  |
| 1435                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 190  | 8.5         | 10.1                     |                          | 200                   | 15                     |           |             |               |                                  |  |  |
| 1440                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 195  | 7.2         | 9.7                      |                          | 210                   | 14                     |           |             |               |                                  |  |  |
| 1445                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 175  | 9.1         | 9.7                      |                          | 200                   | 14                     |           |             |               |                                  |  |  |
| 1450                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 190  | 7.5         | 10.3                     |                          | 200                   | 13                     |           |             |               |                                  |  |  |
| 1455                     |                                |     |                                    |  | .  |                          |  |                                       |                                       |                                       |                                   | 200  | 7.8         | 10.6                     |                          | 190                   | 11                     |           |             |               |                                  |  |  |
| 1500                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  | 7.0         | 11.5                     |                          | 170                   | 11                     |           |             |               |                                  |  |  |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$\text{d} \text{NO}_2 = \text{NO}_x - \text{NO}$$

$$\text{e} \text{NH}_3 = (\text{NO}_x + \text{NH}_3) - \text{NO}_x$$

Notes:

Plant Piedmont  
 Location Sacramento River  
 Date 1-6-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       | Cold Sample Line Analysis (Dry)   |  |             |                          |                          |                       |                        |           |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) |
| 1505                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  |             | 70                       | 116                      |                       | 160                    | 11        |
| 1510                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  |             | 70                       | 116                      |                       | 170                    | 13        |
| 1515                     |                                |     |                                    |  | STACK  |                          |  |                                       |                                       |                                       |                                   | 130  |             | 117                      | 6.5                      |                       | 110                    | 1         |
| 1520                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 110  |             | 121                      | 6.5                      |                       | 100                    | 0         |
| 1525                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 130  |             | 125                      | 6.1                      |                       | 100                    | 0         |
| 1530                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 130  |             | 126                      | 6.3                      |                       | 90                     | 0         |
| 1535                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 130  |             | 125                      | 6.3                      |                       | 90                     | 0         |
| 1540                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 130  |             | 123                      | 6.5                      |                       | 90                     | 0         |
| 1545                     |                                |     |                                    |  | HOTLINE (10 min)                                     |                          |  |                                       |                                       |                                       |                                   | 6.2  | 125         | 150                      | 7                        |                       |                        |           |
| 1550                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 170  |             | 6.2                      | 12.5                     |                       | 150                    | 1         |
| 1555                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 170  |             | 6.1                      | 12.9                     |                       | 150                    | 0         |
| 1600                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 160  |             | 6.6                      | 12.5                     |                       | 150                    | 3         |
| 1605                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  |             | 6.5                      | 12.3                     |                       | 150                    |           |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

<sup>d</sup>NO<sub>2</sub> = NO<sub>x</sub> - NO

<sup>e</sup>NH<sub>3</sub> = (NO<sub>x</sub> + NH<sub>3</sub>) - NO<sub>x</sub>

Notes:

Plant Kure Refinery  
 Location Sulfur House Building  
 Date 7-6-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       | Cold Sample Line Analysis (Dry)   |  |             |                          |                          |                       |                        |           |             |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|-------------|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) | CO<br>(ppm) |
| 1610                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 185         | 6.7                      | 12.7                     | 15.0                  | 8.7                    |           |             |
| 1615                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 185         | 7.2                      | 12.2                     | 16.0                  | 7.7                    |           |             |
| 1620                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 185         | 7.4                      | 12.1                     | 16.0                  | 11.1                   |           |             |
| 1625                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 195         | 6.9                      | 12.3                     | 17.0                  | 11.3                   |           |             |
| 1630                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200         | 6.5                      | 12.3                     | 18.0                  | 11.1                   |           |             |
| 1635                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200         | 7.0                      | 11.9                     | 17.0                  |                        |           |             |
| 1640                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200         | 7.3                      | 11.5                     | 17.0                  |                        |           |             |
| 1645                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 210         | 7.5                      | 11.2                     | 22.0                  |                        |           |             |
| 1650                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 210         | 7.3                      | 11.4                     | 23.0                  |                        |           |             |
| 1655                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 210         | 7.2                      | 11.5                     | 23.0                  |                        |           |             |
| 1700                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 210         | 7.0                      | 11.6                     | 21.0                  |                        |           |             |
| 1705                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |           |             |
| 1710                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |           |             |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$d_{NO_2} = NO_x - NO$$

$$e_{NH_3} = (NO_x + NH_3) - NO_x$$

Notes:

Plant Kiln of 4 yrs  
 Location Sun House Boiler  
 Date 7-7-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |                     |                          |                          |                       |                        |             |             |               |                                   |  |  |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|---------------------|--------------------------|--------------------------|-----------------------|------------------------|-------------|-------------|---------------|-----------------------------------|--|--|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm)         | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(ppm) | CO<br>(ppm) | TUHC<br>(ppm) | Sample Gas<br>Temperature<br>(°F) |  |  |
|                          |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |                     |                          |                          |                       |                        |             |             |               |                                   |  |  |
| 0900                     |                                |     | 28.60                              |  |  |                          |  |                                       |                                       |                                       |                                   |  | 165                 |                          | 105                      | 3.2                   |                        | 230         | 3           |               |                                   |  |  |
| 0905                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200                 |                          | 76                       | 11.1                  |                        | 210         | 3           |               |                                   |  |  |
| 0910                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 100                 |                          | 7.0                      | 11.1                  |                        | 200         | 3           |               |                                   |  |  |
| 0915                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 165                 |                          | 6.1                      | 12.2                  |                        | 200         | 3           |               |                                   |  |  |
| 0920                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 210                 |                          | 6.5                      | 12.0                  |                        | 210         | 3           |               |                                   |  |  |
| 0925                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200                 |                          | 6.6                      | 11.5                  |                        | 200         | 3           |               |                                   |  |  |
| 0930                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | *145                |                          | 6.3                      | 11.1                  |                        | 260         | 3           |               |                                   |  |  |
| 0935                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 190                 |                          | 6.0                      | 12.6                  |                        | 230         | 3           |               |                                   |  |  |
| 0940                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200                 |                          | 6.4                      | 12.0                  |                        | 170         | 3           |               |                                   |  |  |
| 0945                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200                 |                          | 6.7                      | 11.4                  |                        | 165         | 3           |               |                                   |  |  |
| 0950                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200                 |                          | 7.1                      | 11.0                  |                        | 165         | 3           |               |                                   |  |  |
| 0955                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | *7.000 (transition) |                          | 165                      | 10.1                  | 7.3                    | 125         | 3           |               |                                   |  |  |
| 1000                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 165                 |                          | 28                       | 1.4                   |                        | 70          | 2           |               |                                   |  |  |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$\begin{aligned} d_{NO_2} &= NO_x - NO \\ e_{NH_3} &= (NO_x + NH_3) - NO_x \end{aligned}$$

Notes:

Plant Richart  
 Location Sawdust Boiler  
 Date 7-1-63

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |             |                          |                          |                       |                        |           |             |               |                                  |  |  |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|-------------|---------------|----------------------------------|--|--|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) | CO<br>(ppm) | TUHC<br>(ppm) | Sample Gas<br>Temperatur<br>(°F) |  |  |
|                          |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |           |             |               |                                  |  |  |
| 1005                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 160  |             | 88                       | 8.2                      |                       | 70                     | 76.2      |             |               |                                  |  |  |
| 1010                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 160  |             | 87                       | 8.4                      |                       | 55                     | 8         |             |               |                                  |  |  |
| 1015                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 160  |             | 83                       | 8.9                      |                       | 60                     | 1         |             |               |                                  |  |  |
| 1020                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 175  |             | 79                       | 9.2                      |                       | 50                     | 1         |             |               |                                  |  |  |
| 1025                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 195  |             | 73                       | 9.9                      |                       | 65                     | 1         |             |               |                                  |  |  |
| 1030                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  |             | 5.1                      | 12.6                     |                       | 100                    | 3         |             |               |                                  |  |  |
| 1035                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 195  | 195         | 6.3                      | 11.60                    |                       | 25                     | 3         |             |               |                                  |  |  |
| 1040                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 195  |             | 6.3                      | 12.0                     |                       | 75                     | 3         |             |               |                                  |  |  |
| 1045                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 195  |             | 6.3                      | 11.9                     |                       | 75                     | 3         |             |               |                                  |  |  |
| 1050                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 200  |             | 5.4                      | 12.9                     |                       | 95                     | 2         |             |               |                                  |  |  |
| 1055                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 195  |             | 4.5                      | 13.3                     |                       | 105                    | 1         |             |               |                                  |  |  |
| 1100                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 155  |             | 6.0                      | 11.1                     |                       | 70                     | 1         |             |               |                                  |  |  |
| 1105                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 115  |             | 7.4                      | 9.3                      |                       | 55                     | 2         |             |               |                                  |  |  |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$\text{d}_{\text{NO}_2} = \text{NO}_x - \text{NO}$$

$$\text{e}_{\text{NH}_3} = (\text{NO}_x + \text{NH}_3) - \text{NO}_x$$

Notes:

Plant Rock of Ages  
 Location S. 3rd Street, Galesburg  
 Date 1-2-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |                       |                          |                          |                       |                        |           |             |               |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-----------------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|-------------|---------------|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm)           | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) | CO<br>(ppm) | TUHC<br>(ppm) |
|                          |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |                       |                          |                          |                       |                        |           |             |               |
| 1110                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 135                   |                          | 6.8                      | 16.1                  |                        | 45        | 1           |               |
| 1115                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 120                   |                          | 7.8                      | 8.8                   |                        | 26        | 2           |               |
| 1120                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 120                   |                          | 7.8                      | 8.7                   |                        | 15        | 2           |               |
| 1125                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | <i>Changed filter</i> |                          |                          |                       |                        |           |             |               |
| 1130                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | "                     | "                        |                          |                       |                        |           |             |               |
| 1135                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 135                   |                          | 6.7                      | 13.4                  |                        | 76        | 3           |               |
| 1140                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 135                   |                          | 4.2                      | 13.1                  |                        | 35        | 3           |               |
| 1145                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 135                   |                          | 3.2                      | 14.3                  |                        | 15        | 2           |               |
| 1150                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 100                   |                          | 3.7                      | 14.5                  |                        | 65        | 2           |               |
| 1155                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 100                   |                          | 3.6                      | 14.6                  |                        | 72        | 2           |               |
| 1200                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 125                   |                          | 4.3                      | 13.8                  |                        | 85        | 2           |               |
| 1205                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 140                   |                          | 4.3                      | 13.6                  |                        | 75        | 2           |               |
| 1210                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  | 175                   |                          | 4.4                      | 13.6                  |                        | 72        | 2           |               |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$d_{NO_2} = NO_x - NO$$

$$e_{NH_3} = (NO_x + NH_3) - NO_x$$

Notes:

Plant Koch Refinery  
 Location Gas House Boiler  
 Date 7-2-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |             |                          |                          |                       |                        |           |             |               |                                   |  |
|--------------------------|--------------------------------|-----|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|-------------|---------------|-----------------------------------|--|
|                          | WBT                            | DBT |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) | CO<br>(ppm) | TUHC<br>(ppm) | Sample Gas<br>Temperature<br>(°F) |  |
|                          |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |           |             |               |                                   |  |
| 1215                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 205         | 4.0                      | 14.1                     | 75                    | 2                      |           |             |               |                                   |  |
| 1220                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 200         | 3.5                      | 14.7                     | 170                   | 2                      |           |             |               |                                   |  |
| 1225                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 190         | 3.1                      | 14.4                     | 130                   | 3                      |           |             |               |                                   |  |
| 1230                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 176         | 2.6                      | 15.8                     | 245                   | 4                      |           |             |               |                                   |  |
| 1235                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 95          | 2.4                      | 14.6                     | 1120                  | 3                      |           |             |               |                                   |  |
| 1240                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 190         | 3.2                      | 15.1                     | 105                   | 3                      |           |             |               |                                   |  |
| 1245                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 202         | 3.4                      | 14.6                     | 100                   | 3                      |           |             |               |                                   |  |
| 1250                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 175         | 3.1                      | 15.0                     | 135                   | 2                      |           |             |               |                                   |  |
| 1255                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 185         | 3.8                      | 14.3                     | 125                   | 2                      |           |             |               |                                   |  |
| 1300                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 195         | 3.6                      | 14.2                     | 115                   | 2                      |           |             |               |                                   |  |
| 1305                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 205         | 3.8                      | 14.1                     | 90                    | 3                      |           |             |               |                                   |  |
| 1310                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 175         | 4.0                      | 13.9                     | 70                    | 2                      |           |             |               |                                   |  |
| 1315                     |                                |     |  |  | 57                       | 104  | 72                                    | 4.05                                  | 15.77                                 | 20                                | 2000   | 1271        | 8                        |                          |                       |                        |           |             |               |                                   |  |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$\text{d} \text{NO}_2 = \text{NO}_x - \text{NO}$$

$$\text{e} \text{NH}_3 = (\text{NO}_x + \text{NH}_3) - \text{NO}_x$$

Notes:

Plant Rock of Ages  
 Location Sawdust Boiler  
 Date 7-1-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |             |                          |                          |                       |                        |           |             |
|--------------------------|--------------------------------|-----|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|-------------|
|                          |                                |     |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) | CO<br>(ppm) |
|                          | WBT                            | DBT |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |           |             |
| 1320                     |                                |     |  |  |                          | 57.0C  | 10.0                                  |                                       |                                       |                                   |  | 150         |                          | 9.6                      | 5.6                   | 4.0                    | 3         |             |
| 1325                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 115         |                          | 9.6                      | 5.8                   | 2.5                    | 3         |             |
| 1330                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 95          |                          | 9.5                      | 5.6                   | 3.5                    | 3         |             |
| 1335                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 90          |                          | 10.0                     | 4.9                   | 0.7                    | 4         |             |
| 1340                     |                                |     |  |  |                          | Boiler Duct  | 14.0                                  |                                       |                                       |                                   |  | 115         |                          | 3.4                      | 13.8                  | 2.0                    | 1.5       |             |
| 1345                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 115         |                          | 3.5                      | 13.4                  | 1.5                    | 4.0       |             |
| 1350                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 110         |                          | 4.0                      | 12.8                  | 1.0                    | 3.8       |             |
| 1355                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 115         |                          | 4.1                      | 12.5                  | 1.5                    | 3.8       |             |
| 1400                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 115         |                          | 3.4                      | 13.3                  | 1.0                    | 2.0       |             |
| 1405                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 110         |                          | 3.5                      | 13.2                  | 1.0                    | 1.5       |             |
| 1410                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 105         |                          | 3.4                      | 13.5                  | 1.5                    | 1.2       |             |
| 1415                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 100         |                          | 3.5                      | 13.5                  | 2.0                    | 0.9       |             |
| 1420                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  | 100         |                          | 3.2                      | 13.7                  | 4.55                   | 1.2       |             |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$d_{NO_2} = NO_x - NO$$

$$e_{NH_3} = (NO_x + NH_3) - NO_x$$

Notes:

Plant Rock of Ages  
 Location Secondary Boiler  
 Date 7-1-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       | Cold Sample Line Analysis (Dry)   |  |             |                          |                          |                       |                        |           |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-----------|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(%) |
| 1425                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 175  | 3.4         | 14.1                     |                          | 425                   | 13                     |           |
| 1430                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 185  | 3.4         | 14.7                     |                          | 375                   | 1                      |           |
| 1435                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 175  | 3.1         | 14.4                     |                          | 520                   | 10                     |           |
| 1440                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 175  | 2.9         | 14.4                     |                          | 220                   | 19                     |           |
| 1445                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 182  | 4.1         | 13.7                     |                          | 265                   | 6                      |           |
| 1450                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 180  | 3.1         | 14.7                     |                          | 265                   | 4                      |           |
| 1455                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 190  | 2.5         | 15.0                     |                          | 235                   | 3                      |           |
| 1500                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 190  | 2.5         | 15.0                     |                          | 285                   | 3                      |           |
| 1505                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 195  | 3.0         | 14.0                     |                          | 215                   | 2                      |           |
| 1510                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 190  | 3.9         | 13.1                     |                          | 175                   | 3                      |           |
| 1515                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 190  | 4.1         | 12.9                     |                          | 205                   | 3                      |           |
| 1520                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 180  | 4.0         | 12.9                     |                          | 195                   | 3                      |           |
| 1525                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 185  | 3.9         | 12.8                     |                          | 200                   | 3                      |           |

<sup>a</sup>NO = direct sample measurement (no conversion)

<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter

<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$\text{d}_{\text{NO}_2} = \text{NO}_x - \text{NO}$$

$$\text{e}_{\text{NH}_3} = (\text{NO}_x + \text{NH}_3) - \text{NO}_x$$

Notes:

Plant Kick of Stages  
 Location Sew 2111 Boiler  
 Date 7-1-83

CONTINUOUS MONITOR FIELD DATA

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Barometric<br>Pressure<br>(in. Hg) | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |             |                          |                          |                       |                        |             |             |               |                                   |  |  |
|--------------------------|--------------------------------|-----|------------------------------------|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-------------|-------------|---------------|-----------------------------------|--|--|
|                          | WBT                            | DBT |                                    |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(ppm) | CO<br>(ppm) | TUHC<br>(ppm) | Sample Gas<br>Temperature<br>(°F) |  |  |
|                          |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |             |               |                                   |  |  |
| 1530                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 185  | 3.2         | 13.3                     | 195                      | 4                     |                        |             |             |               |                                   |  |  |
| 1535                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 165  | 3.6         | 12.2                     | 125                      | 4                     |                        |             |             |               |                                   |  |  |
| 1540                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 100  | 2.4         | 13.2                     | 105                      | 15                    |                        |             |             |               |                                   |  |  |
| 1545                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 110  | 3.1         | 12.6                     | 565                      | 22                    |                        |             |             |               |                                   |  |  |
| 1550                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 115  | 2.9         | 13.3                     | 630                      | 15                    |                        |             |             |               |                                   |  |  |
| 1555                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 135  | 3.6         | 13.3                     | 335                      | 4                     |                        |             |             |               |                                   |  |  |
| 1600                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   | 175  | 5.1         | 12.1                     | 170                      | 0                     |                        |             |             |               |                                   |  |  |
| 1605                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |             |               |                                   |  |  |
| 1610                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |             |               |                                   |  |  |
| 1615                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |             |               |                                   |  |  |
| 1620                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |             |               |                                   |  |  |
| 1625                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |             |               |                                   |  |  |
| 1630                     |                                |     |                                    |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |             |               |                                   |  |  |

$$^a \text{NO} = \text{direct sample measurement (no conversion)}$$

<sup>a</sup>

<sup>b</sup>

$$\text{^bNO}_x + \text{NH}_3 = \text{sample path through stainless steel converter}$$

<sup>c</sup>

<sup>d</sup>

$$\text{^dNO}_2 = \text{NO}_x - \text{NO}$$

<sup>e</sup>

$$\text{^eNH}_3 = (\text{NO}_x + \text{NH}_3) - \text{NO}_x$$

Notes:

DATA

## CONTINUOUS MONITOR FIELD DATA

Plant \_\_\_\_\_

Location \_\_\_\_\_

Date \_\_\_\_\_

| Time<br>(24-hr<br>clock) | Ambient<br>Temperature<br>(°F) |     | Instrument<br>Van<br>Temperature<br>(°F) | Heated Sample Line Analysis (Wet)                    |                          |  |                                       |                                       |                                       |                                   | Cold Sample Line Analysis (Dry)                      |             |                          |                          |                       |                        |             |               |                                   |  |
|--------------------------|--------------------------------|-----|--|--|--------------------------|--|---------------------------------------|---------------------------------------|---------------------------------------|-----------------------------------|--|-------------|--------------------------|--------------------------|-----------------------|------------------------|-------------|---------------|-----------------------------------|--|
|                          | WBT                            | DBT |  | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO <sup>a</sup><br>(ppm) | NO <sub>x</sub> +NH <sub>3</sub> <sup>b</sup><br>(ppm) | NO <sub>x</sub> <sup>c</sup><br>(ppm) | NO <sub>2</sub> <sup>d</sup><br>(ppm) | NH <sub>3</sub> <sup>e</sup><br>(ppm) | Sample Gas<br>Temperature<br>(°F) | Sample<br>Location<br>Specify:<br>Inlet or<br>Outlet | NO<br>(ppm) | NO <sub>x</sub><br>(ppm) | NO <sub>2</sub><br>(ppm) | O <sub>2</sub><br>(%) | CO <sub>2</sub><br>(%) | CO<br>(ppm) | TUHC<br>(ppm) | Sample Gas<br>Temperature<br>(°F) |  |
|                          |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |               |                                   |  |
| 1635                     |                                |     |  |  | 1010                     | 0.174  | -                                     | 1.182                                 | 1010                                  | 1010                              |  |             |                          |                          |                       |                        |             |               |                                   |  |
| 1640                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   | 145  |             | 2.8                      | 9.2                      |                       |                        | 140         |               |                                   |  |
| 1645                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   | 140  |             | 2.8                      | 8.8                      |                       |                        | 210         |               |                                   |  |
| 1650                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   | 140  |             | 3.1                      | 8.6                      |                       |                        | 225         |               |                                   |  |
| 1655                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   | 146  |             | 8.7                      | 8.7                      |                       |                        | 225         |               |                                   |  |
| 1700                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   | 150  |             | 8.4                      | 8.3                      |                       |                        |             |               |                                   |  |
| 1705                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   | 135  |             |                          |                          |                       |                        |             |               |                                   |  |
| 1710                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |               |                                   |  |
| 1715                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |               |                                   |  |
| 1720                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |               |                                   |  |
| 1725                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |               |                                   |  |
| 1730                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |               |                                   |  |
| 1735                     |                                |     |  |  |                          |  |                                       |                                       |                                       |                                   |  |             |                          |                          |                       |                        |             |               |                                   |  |

<sup>a</sup>NO = direct sample measurement (no conversion)<sup>b</sup>NO<sub>x</sub> + NH<sub>3</sub> = sample path through stainless steel converter<sup>c</sup>NO<sub>x</sub> = sample path through molybdenum converter

$$\text{dNO}_2 = \text{NO}_x - \text{NO}$$

$$\text{eNH}_3 = (\text{NO}_x + \text{NH}_3) - \text{NO}_x$$

Notes:

#### 4.2 FIELD DATA SHEETS FOR EPA METHOD 5/8, SASS, HC1, AND VOST TRAINS

## FIELD DATA

Page / of 2

Plant Clock of God

Date 7-6-78

Sample Location (e.g., House)

Sample Type 11-512

**Run Number**

**Operator** V. Gandy

Ambient Temperature  $\sim 60^{\circ}\text{F}$

Barometric Pressure 29.2

Static Pressure, ( $H_2O$ ) - 10

Filter Number(s) 96-26(a)

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Leak Check: Initial at  $\frac{15}{12}$ " Hg, .05 CFM  
Final at  $\frac{12}{12}$ " Hg, .025 CFM

Pitot Leak Check: ok

Probe Length and Type 5' PTC

Nozzel Size & I.D. 3/8"

Pitot Coefficient & I.D. 0.800

Assumed Moisture \_\_\_\_\_ .07

**Molecular Weight, Dry, ( $M_d$ )**

Meter Box Number WAPP - 1

Meter Coefficient .7

$$\alpha \text{ Factor} \underline{\quad 1.013 \quad}$$

$$\Delta H = K(N_d)^4 \left( \frac{T_m}{T_s} \right) (P)$$

## SASS Condensate

Total Volume 54.1

| Traverse Point Number | Sampling Time, min | Clock Time (24-hr) Clock | Gas Meter Reading ( $V_m$ ), ft <sup>3</sup> | Velocity Head ( $4P_s$ ), in. H <sub>2</sub> O | Orifice Pressure Differential ( $\Delta H$ ), in. H <sub>2</sub> O | Temperature of |        |      |       |       |          | Pump Vacuum in. Hg | Avg. $\sqrt{4P}$ |     |       |  |
|-----------------------|--------------------|--------------------------|--|--|--|----------------|--------|------|-------|-------|----------|--------------------|------------------|-----|-------|--|
|                       |                    |                          |  |  |  | Gas Meter      |        |      | Stack | Probe | Impinger | Organic Module     | Gas Meter        |     |       |  |
|                       |                    |                          |  |  |  | Desired        | Actual | Oven |       |       |          |                    | In               | Out |       |  |
|                       | 0                  | 1100                     | Init. 593.941                                |  |  |                |        |      |       |       |          |                    |                  |     |       |  |
| A-1                   |                    |                          | 596.1  | 0.855  | .71  | .71            | .67    |      | 62    |       | 170      | 61                 | 61               | 61  | 0.247 |  |
| 2                     | 12                 |                          | 596.87                                       | 1.055  | .72  | .72            | .74    |      | 55    |       | 120      | 61                 | 61               | 61  | 0.247 |  |
| 3                     | 17                 |                          | 601.49                                       | 1.055  | .71  | .71            | .71    |      | 56    |       | 21       | 61                 | 61               | 61  | 0.247 |  |
| 4                     | 28                 |                          | 607.97                                       | 1.055  | .72  | .72            | 261    |      | 54    |       | 195      | 61                 | 61               | 61  | 0.247 |  |
| 5                     | 35                 |                          | 616.27                                       | 1.055  | .61  | .61            | 275    |      | 53    |       | 145      | 70                 | 61               | 61  | 0.247 |  |
| 6                     | 43                 |                          | 604.015                                      | 0.85   | .61  | .61            | 261    |      | 51    |       | 145      | 70                 | 70               | 61  | 0.247 |  |
| 7                     | 50                 |                          | 610.66175<br>611.612                         | 1.07   | .62  | .62            | 261    |      | —     |       | 21       | 61                 | 61               | 61  | 0.247 |  |
| 8                     | 57                 |                          | 614.11                                       | 0.7  | .71  | .71            | 261    |      | 51    |       | 21       | 70                 | 70               | 61  | 0.247 |  |
| 9                     | 67                 |                          | 614.73                                       | 1.05   | .61  | .61            | 261    |      | 51    |       | 125      | 70                 | 70               | 61  | 0.247 |  |

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Run No. 1-1-1-1-1

Date 7/20-22

Sampling Location 7th Avenue

#### Comments:

## FIELD DATA

Page 1 of 1

Plant Rock NE F-55  
Date 7-6-83  
Sample Location Saw Horse  
Sample Type SAC  
Run Number 1  
Operator P.W. KAUFMAN  
Ambient Temperature \_\_\_\_\_  
Barometric Pressure 28.24  
Static Pressure, ( $H_2O$ ) - .10  
Filter Number(s) \_\_\_\_\_

Leak Check: Initial at 18" Hg, .03 CFM O.M. + 1 MP  
Final at 10" Hg, .05 CFM ed.m. + 1 MP  
Pitot Leak Check: N/A

Probe Length and Type 3 Standard  
Nozzel Size & I.D. 1.40  
Pitot Coefficient & I.D. .82  
Assumed Moisture 7.5%  
Molecular Weight, Dry, ( $M_d$ ) \_\_\_\_\_  
Meter Box Number 216  
Meter Coefficient 3.514  
 $\alpha$  Factor 0.93  
 $K = \frac{DIA}{A}$   
 $K(N_d)^4 = \text{_____} \times (\text{____})^4 = \text{_____}$   
 $4H = K(N_d)^4 \left( \frac{T_m}{T_s} \right) (P)$

| Traverse Point Number | Clock Time (24-hr) Clock<br>Sampling Time, min | Gas Meter Reading ( $V_m$ ), ft <sup>3</sup> | Velocity Head ( $\Delta P_s$ ), in. H <sub>2</sub> O | Orifice Pressure Differential ( $\Delta H$ ), in. H <sub>2</sub> O | Temperature °F |        |       |       |          |                | Pump Vacuum in. Hg | Avg. $\sqrt{\Delta P}$ |     |    |  |
|-----------------------|--|--|--|--|----------------|--------|-------|-------|----------|----------------|--------------------|------------------------|-----|----|--|
|                       |  |  |  |  | Desired        | Actual | Stack | Probe | Impinger | Organic Module | Oven               | Gas Meter              |     |    |  |
|                       |  |  |  |  |                |        |       |       |          |                |                    | In                     | Out |    |  |
| 0                     | 1149   | Init. 787.726                                |  |  |                |        |       |       |          |                |                    |                        |     |    |  |
| 10                    |  | 825.61                                       | .05  | 2.14   | 2.1            | 259    | 396   |       |          | 60             | 405                | 55                     | 55  | 15 |  |
| 20                    |  | 765.0  | .05  | 2.14   | 2.1            | 281    | 376   |       |          | 56             | 402                | 51                     | 55  | 15 |  |
| 30                    |  | 903.01                                       | .045   | 2.15   | 2.0            | 216    | 365   |       |          | 58             | 401                | 71                     | 66  | 15 |  |
| 40                    |  | 941.85                                       | .045   | 2.15   | 2.1            | 270    | 382   |       |          | 57             | 399                | 73                     | 67  | 15 |  |
| 50                    |  | 980.7  | .055   | 2.15   | 2.1            | 223    | 405   |       |          | 56             | 405                | 57                     | 61  | 14 |  |
| 60                    |  | 1028.9                                       | .05  | 2.15   | 2.1            | 279    | 406   |       |          | 57             | 400                | 52                     | 46  | 15 |  |
| 70                    |  | 89.1   |  | 2.17   | 2.0            | 268    | 371   |       |          | 56             | 397                | 76                     | 57  | 17 |  |
| 80                    |  |  |  | 2.17   | 2.1            | 251    | 416   |       |          | 51             | 411                | 71                     | 61  | 17 |  |
| 90                    |  |  |  |  | 2.1            |        |       |       |          | 51             | 411                | 71                     | 61  | 17 |  |

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Comments: 40 min. 50% E. 100% 82 p. intact 12.87

245

192.884

2012

626

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Run No. \_\_\_\_\_

Date 7/18/83

Sampling Location East Bay Area

### **Comments:**

'ICAL DATA

Plant Rock of Ages Sample No. 5455 - 1  
Sampling Location 7735.61 Run No. 1  
Recovered By \_\_\_\_\_ Recovery Date 7/16/73 Run Date 7/16/73  
Comments \_\_\_\_\_  
Analyst Responsible \_\_\_\_\_  
Calculations and Report Reviewed By \_\_\_\_\_ Report Date \_\_\_\_\_

| FILTERS USED |          | CYCLONES         |                             |
|--------------|----------|------------------|-----------------------------|
| No.          |          | Used<br>(yes/no) | Pretared Container<br>(No.) |
| _____        | _____    | _____            | _____                       |
| _____        | 10 $\mu$ | _____            | _____                       |
| _____        | 3 $\mu$  | _____            | _____                       |
| _____        | 1 $\mu$  | _____            | _____                       |

| IMPIINGER VOLUMES         |         |         |                    |
|---------------------------|---------|---------|--------------------|
|                           | Initial | Final   |                    |
| First ( $H_2O_2$ )        | 500 ml  | 540 ml  |                    |
| Second ( $APS + AgNO_3$ ) | 500 ml  | 458 ml  |                    |
| Third ( $APS + AgNO_3$ )  | 500 ml  | 504 ml  |                    |
| TOTALS                    | 1500 ml | 1502 ml | Gain <u>0.2 ml</u> |

| SILICA GEL WEIGHTS |                |                 |                     |
|--------------------|----------------|-----------------|---------------------|
|                    | Initial        | Final           |                     |
|                    | <u>800.0 g</u> | <u>956.0 g</u>  |                     |
|                    | <u>800.0 g</u> | <u>931.7 g</u>  |                     |
|                    | <u>g</u>       | <u>g</u>        |                     |
| TOTALS             | <u>16000 g</u> | <u>1887.7 g</u> | Gain <u>287.7 g</u> |

| CONDENSATE   |       |    |                     |
|--|-------|----|---------------------|
| TOTAL VOLUME COLLECTED                             |       |    |                     |
| Volume Neat  | _____ | ml | _____ ml            |
| Volume Extracted                                   | _____ | ml | _____ ml            |
| Volume $CH_2Cl_2$ Extract ( $3 \times$ <u>ml</u> ) | _____ | ml | _____ ml            |
| Extracted Condensate: pH Neat                      | _____ |    |                     |
| Amount 96% $HNO_3$ added                           | _____ |    |                     |
| pH Final   | _____ |    | _____               |
|  |       |    | TOTAL GAIN _____ ml |

## FIELD DATA

Page \_\_\_\_\_ of \_\_\_\_\_

Plant Flock of Fish  
Date 7-6-77  
Sample Location Tuna Hill  
Sample Type FCL  
Run Number 1  
Operator C.R.  
Ambient Temperature 55.6  
Barometric Pressure 28.5.21  
Static Pressure, (H<sub>2</sub>O) -10  
Filter Number(s) N/A

Leak Check: Initial at 13 " Hg, .013 CFM  
Final at 5 " Hg, .008 CFM  
Pitot Leak Check:

Pitot Leak Check:

**SASS Condensate**

Probe Length and Type 5 ft.  
 Nozzel Size & I.D. 1/4"  
 Pitot Coefficient & I.D. 1.822  
 Assumed Moisture 0.675  
 Molecular Weight, Dry, ( $M_d$ ) 16.0  
 Meter Box Number D554-1118P1  
 Meter Coefficient 1725  
 $\alpha$  Factor 1.012  
 $K = \frac{3413.13}{}$   
 $K(N_d)^4 = \underline{\quad} \times (\underline{\quad})^4 = \underline{\quad}$   
 $\Delta H = K(N_d)^4 \left( \frac{T_m}{T_s} \right) (P)$

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**Comments:**

## ISOKINETIC CALCULATIONS - USEPA: M/5 BASIS

ROCK OF AGES - NO. 1

| RUN NUMBER               | 1-SASS  | 1-M5/8  | 1-HCL   |
|--------------------------|---------|---------|---------|
| DATE OF TEST             | 7-6-83  | 7-6-83  | 7-6-83  |
| OPERATOR                 | PWK     | VB      | VB      |
| METER VOLUME, CF         | 992.884 | 30.22   | 16.145  |
| METER COEF               | 0.973   | 1.012   | 1.012   |
| BAROMETRIC PRES, HG      | 28.24   | 28.24   | 28.21   |
| DELTA H, IN H2O          | 2.012   | 0.703   | 0.74    |
| METER TEMP, DEG F        | 68.6    | 69.5    | 64.8    |
| STACK TEMP, DEG F        | 274.3   | 295.3   | 279     |
| CONDENSATE, ML           | 964.7   | 54.1    | 11.3    |
| PERCENT CO2              | 7.1     | 7.1     | 7.1     |
| PERCENT O2               | 12.2    | 12.2    | 12.2    |
| PERCENT CO               | 0       | 0       | 0       |
| PERCENT N2               | 80.7    | 80.7    | 80.7    |
| STATIC PRES, IN H2O      | -0.1    | -0.1    | -0.1    |
| PITOT COEF               | 0.79    | 0.79    | 0       |
| SQRT DELTA P, IN H2O     | 0.234   | 0.231   | 0       |
| STACK AREA, SQ FT        | 2.405   | 2.405   | 0       |
| NOZZLE DIAM, IN          | 1.24    | 0.387   | 0       |
| TEST TIME, MIN           | 260     | 60      | 30      |
| MASS PARTICULATE, G      | 0       | 0       | 0       |
| F-FACTOR, DSCF/MBTU      | 0       |         |         |
| VOLUME, DSCF             | 967.246 | 28.161  | 15.165  |
| WATER VAPOR, SCF         | 45.408  | 2.546   | 0.532   |
| PERCENT MOISTURE         | 0.045   | 0.083   | 0.034   |
| MOLECULAR WT DRY, LB/LB  | 29.624  | 29.624  | 29.624  |
| MOLECULAR WT WET, LB/LB  | 29.10   | 28.66   | 29.23   |
| STACK PRES, IN HG        | 28.23   | 28.23   | 28.20   |
| STACK VELOCITY, FT/SEC   | 14.34   | 15.07   | 0.00    |
| MASS FLOW, DSCFM         | 1,397   | 1,316   | 0       |
| MASS FLOW, ACFM          | 2,156   | 2,175   | 0       |
| PERCENT EXCESS AIR       |         |         |         |
| PERCENT ISOKINETIC       | 76.421  | 105.109 | #DIV/0! |
| GRAIN LOADING, GR/DSCF   | 0.00000 | 0.00000 | 0.00000 |
| GRAIN LOADING, GR/ACF    | 0.00000 | 0.00000 | 0.00000 |
| EMISSION RATE, LB/HR-STD | 0.00000 | 0.00000 | 0.00000 |
| EMISSION RATE, LB/MBTU   |         |         |         |

Plant \_\_\_\_\_  
Date \_\_\_\_\_  
Sample Location \_\_\_\_\_  
Sample Type \_\_\_\_\_  
Run Number \_\_\_\_\_  
Operator \_\_\_\_\_  
Ambient Temperature \_\_\_\_\_  
Barometric Pressure \_\_\_\_\_  
Static Pressure, (H<sub>2</sub>O) \_\_\_\_\_  
Filter Number(s) \_\_\_\_\_

Leak Check: Initial at 15" Hg, .021 CFM  
Final at 11" Hg, .013 CFM  
Pitot Leak Check: i

Pitot Leak Check: ✓

Pitot Leak Check: \_\_\_\_\_ ✓

| Impinger Volumes |       |          |
|------------------|-------|----------|
| Initial          | Final | Net Gain |
| 501.9            | 501.8 | -14.9    |
| 538.4            | 570.0 | 31.6     |
| 538.6            | 551.3 | 12.7     |
|                  |       |          |
|                  |       |          |
|                  |       |          |
|                  |       |          |
|                  |       |          |
| Silica Gel       |       |          |
| 141.10           | 161.4 | 14.3     |

Probe Length and Type \_\_\_\_\_  
 Nozzel Size & I.D. \_\_\_\_\_  
 Pitot Coefficient & I.D. \_\_\_\_\_  
 Assumed Moisture \_\_\_\_\_  
 Molecular Weight, Dry, ( $M_d$ ) \_\_\_\_\_  
 Meter Box Number \_\_\_\_\_  
 Meter Coefficient \_\_\_\_\_  
 $\alpha$  Factor \_\_\_\_\_  
 $K = \frac{837}{K(Nd)^4} = \frac{837}{8.37 \times (1.38)^4} = 18.374$   
 $\Delta H = K(Nd)^4 \left( \frac{T_m}{T_s} \right) (P)$

SASS Condensate \_\_\_\_\_  
Total Volume 24.3

### Total Volume

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| Traverse Point Number | Clock Time<br>(24-hr)<br>Clock | Gas Meter<br>Reading<br>(V <sub>m</sub> ), ft <sup>3</sup> | Velocity<br>Head<br>(ΔP <sub>s</sub> ),<br>in. H <sub>2</sub> O | Orifice Pressure<br>Differential<br>(ΔH), in. H <sub>2</sub> O | Temperature of        |         |        |       |       |          | Pump<br>Vacuum<br>in. Hg | Avg.<br>ΔP |    |     |  |
|-----------------------|--------------------------------|--|---|--|-----------------------|---------|--------|-------|-------|----------|--------------------------|------------|----|-----|--|
|                       |                                |  |   |  |                       |         |        |       |       |          |                          |            |    |     |  |
|                       |                                |  |   |  | Sampling<br>Time, min | Desired | Actual | Stack | Probe | Impinger | Organic<br>Module        | Oven       | In | Out |  |
|                       |                                | Init. 648.735  |   |  |                       |         |        |       |       |          |                          |            |    |     |  |
| 1-1                   | 5                              | 651.53   | .07   | .90  | .90                   | 338     |        | 74    |       |          | 250                      | 53         | 56 | 7   |  |
| 2                     | 10                             | 653.815  | .095  | .58  | .53                   | 338     |        | 79    |       |          | 250                      | 56         | 56 | 5   |  |
| 3                     | 15                             | 656.40   | .06   | .76  | .76                   | 351     |        | 76    |       |          | 250                      | 86         | 86 | 6   |  |
| 4                     | 20                             | 658.78   | .05   | .64  | .64                   | 338     |        | 76    |       |          | 247                      | 86         | 85 | 5   |  |
| 5                     | 25                             | 661.11   | .05   | .65  | .64                   | 327     |        | 73    |       |          | 249                      | 86         | 83 | 5   |  |
| 6                     | 30                             | 663.437  | .05   | .66  | .66                   | 325     |        | 76    |       |          | 247                      | 87         | 87 | 5   |  |
|                       | *                              | 0935   |   |  |                       |         |        |       |       |          |                          |            |    |     |  |
| A-1                   | 35                             | 666.35   | .07   | .92  | .92                   | 319     |        | 71    |       |          | 84                       | 57         | 57 | 7   |  |
| A-2                   | 40                             | 669.18   | .07   | .93  | .93                   | 332     |        | 69    |       |          | 213                      | 99         | 98 | 7   |  |

#### Comments:

\* changed ports

Run No. -

Date \_\_\_\_\_

Sampling Location \_\_\_\_\_

#### **Comments:**

Plant West. of Big  
Date 7/1/03  
Sample Location 5m House  
Sample Type CASS  
Run Number # 2  
Operator ZDZ  
Ambient Temperature -70  
Barometric Pressure 28.64  
Static Pressure, ( $H_2O$ ) -0.10  
Filter Number(s) \_\_\_\_\_

Leak Check: Initial at \_\_\_\_ " Hg, 0.35 CFM  
Final at \_\_\_\_ " Hg, 0.20 CFM  
Pitot Leak Check:

#### Pitot Leak Check:

## SASS Condensate

Probe Length and Type 3 ft  
 Nozzle Size & I.D. 1/2 in.  
 Pitot Coefficient & I.D. 0.7000 82  
 Assumed Moisture 7.5%  
 Molecular Weight, Dry, ( $M_d$ ) 28  
 Meter Box Number 4  
 Meter Coefficient 3.514  
 $\alpha$  Factor 0.973  
 $K = \frac{1}{4}$   
 $K(N_d)^4 = \underline{\quad} \times (\underline{\quad})^4 = \underline{\quad}$   
 $\Delta H = K(N_d)^4 \left( \frac{T_m}{T_s} \right) (P)$

$$\Delta H = T_a * .004$$

| Traverse Point Number | Clock Time<br>(24-hr)<br>Clock | Gas Meter<br>Reading<br>(V <sub>m</sub> ), ft <sup>3</sup> | Velocity<br>Head<br>(4P <sub>s</sub> ),<br>in. H <sub>2</sub> O | Orifice Pressure<br>Differential<br>(ΔH), in. H <sub>2</sub> O | Temperature Of |        |       |       |          |                   |      | Pump<br>Vacuum<br>in. Hg | Avg.<br>$\sqrt{4P}$ |    |
|-----------------------|--------------------------------|--|---|--|----------------|--------|-------|-------|----------|-------------------|------|--------------------------|---------------------|----|
|                       |                                |  |   |  |                |        | Stack | Probe | Impinger | Organic<br>Module | Oven | Gas Meter                |                     |    |
|                       |                                |  |   |  | Desired        | Actual |       |       |          |                   |      | In                       | Out                 |    |
| 0                     | 09105                          | Init. 7834670  |   |  |                |        |       |       |          |                   |      |                          |                     |    |
| 10                    | 0915                           | 3220   | .065  | 2.23   | 3.2            | 279    | 410   |       |          | 70                | 411  | 93                       | 95                  | 15 |
| 20                    | 0925                           | 360.0  | .07   | 2.23   | 2.1            | 292    | 410   |       |          | 69                | 410  | 103                      | 98                  | 15 |
| 30                    | 0935                           | 897.9  | .065  | 2.23   | 2.1            | 296    | 408   |       |          | 68                | 412  | 114                      | 106                 | 15 |
| 40                    | 0945                           | 936.2  | .065  | 2.28   | 2.2            | 311    | 416   |       |          | 67                | 414  | 118                      | 109                 | 19 |
| 50                    | 0952                           | 974.5  | .065  | 2.28   | 2.0            | 292    | 405   |       |          | 67                | 414  | 109                      | 109                 | 19 |
| 60                    | 1002                           | 012.6  | .06   | 2.23   | 2.0            | 289    | 411   |       |          | 61                | 415  | 114                      | 107                 | 19 |
| 70                    | 1012                           | 0419.3   | .065  | 2.28   | 2.0            | 269    | 41    |       |          | 61                | 418  | 113                      | 107                 | 19 |
| 80                    | 1021                           | 095.8  | .06   | 2.28   | 1.9            | 305    | 409   |       |          | 63                | 421  | 113                      | 108                 | 19 |
| 90                    | 1032                           | -  | .06   | 2.28   | 1.85           | 298    | 404   |       |          | 63                | 422  | 115                      | 115                 | 20 |

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Comments: SIG8 AT MN40 TO CHANGE FROM PORT A TO **PORT B**

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| Traverse Point Number | Clock Time<br>(24-hr) Clock | Sampling Time, min | Gas Meter Reading ( $V_m$ ), ft <sup>3</sup> | Velocity Head ( $\Delta P_s$ ), in. H <sub>2</sub> O | Orifice Pressure Differential ( $\Delta H$ ), in. H <sub>2</sub> O | Temperature of |        |       |       |          | Pump Vacuum in. Hg | Avg. $\sqrt{V_p}$ |           |     |  |
|-----------------------|-----------------------------|--------------------|--|--|--|----------------|--------|-------|-------|----------|--------------------|-------------------|-----------|-----|--|
|                       |                             |                    |  |  |  | Desired        | Actual | Stack | Probe | Impinger | Organic Module     | Oven              | Gas Meter |     |  |
|                       | 103.2                       | 4.0                | Init.  |  |  |                |        |       |       |          |                    |                   | In        | Out |  |
|                       | 100                         | 156.5              | .055   | 2.28   | 1.8  | 303            | 405    |       |       | 65       | 412                | 113               | 111       | 20  |  |
|                       | 110                         | 190.637            | .055   | 2.28   | 1.7  | 321            | 405    |       |       | 68       | 419                | 109               | 109       | 20  |  |
|                       | 120                         | 230.5              | .06  | 2.24   | 2.25   | 283            | 391    |       |       | 70       | 412                | 99                | 103       | 15  |  |
|                       | 130                         | 269.5              | .06  | 2.24   | 2.25   | 292            | 391    |       |       | 67       | 415                | 114               | 106       | 15  |  |
|                       | 140                         | 306.7              | .06  | 2.24   | 2.1  | 295            | 402    |       |       | 67       | 417                | 117               | 109       | 15  |  |
|                       | 150                         | 344.8              | .065   | 2.29   | 2.1  | 290            | 414    |       |       | 71       | 420                | 113               | 112       | 19  |  |
|                       | 160                         | 382.2              | .065   | 2.29   | 1.9  | 295            | 390    |       |       | 71       | 412                | 111               | 111       | 19  |  |
|                       | 170                         | 418.4              | .07  | 2.29   | 1.9  | 288            | 406    |       |       | 72       | 413                | 111               | 102       | 20  |  |
|                       | 180                         | 453.2              | .065   | 2.39   | 1.8  | 390            | 402    |       |       | 75       | 402                | 105               | 107       | 20  |  |
| RESTART 12:55         | 190                         | 492.3              | .06  | 2.26   | 2.2  | 397            | 405    |       |       | 71       | 409                | 106               | 103       | 15  |  |
|                       | 200                         | 530.8              | .06  | 2.26   | 2.1  | 292            | 395    |       |       | 71       | 410                | 103               | 103       | 15  |  |
|                       | 210                         | 568.5              | .065   | 2.26   | 2.1  | 280            | 401    |       |       | 68       | 411                | 103               | 107       | 19  |  |
|                       | 220                         | 606.0              | .065   | 2.28   | 2.0  | 292            | 414    |       |       | 71       | 414                | 105               | 106       | 19  |  |
|                       | 230                         | 641.5              | .065   | 2.28   | 1.9  | 272            | 399    |       |       | 73       | 410                | 105               | 105       | 19  |  |
|                       | 240                         | 676.2              | .065   | 2.26   | 1.8  | 257            | 400    |       |       | 73       | 415                | 104               | 104       | 20  |  |
|                       | 250                         | 710.6              | .065   | 2.26   | 1.7  | 271            | 402    |       |       | 71       | 417                | 103               | 106       | 20  |  |
|                       | 260                         | 743.509            | .065   | 2.26   | 1.7  | 275            | 415    |       |       | 71       | 414                | 106               | 105       | 20  |  |

Run No. 2-SASS

Date 7-7-83

Sampling Location SAW HOLE

Comments: STOP AT M.N. 110 TO CHANGE FILTER & SILICA GEL. RESTART 110.5  
 STOP AT M.N. 180 TO CHANGE FILTER & SILICA GEL. RESTART 12:55  
 Final 10% clock entries from 04-0101  
 P.D.A. entries 04-0101

## SASS ANALYTICAL DATA

Plant Rock of Ages Sample No. SASS-2  
 Sampling Location \_\_\_\_\_ Run No. 2  
 Recovered By \_\_\_\_\_ Recovery Date 7/7/83 Run Date 7/7/83  
 Comments \_\_\_\_\_  
 Analyst Responsible \_\_\_\_\_  
 Calculations and Report Reviewed By \_\_\_\_\_ Report Date \_\_\_\_\_

| FILTERS USED |            | CYCLONES                  |                             |
|--------------|------------|---------------------------|-----------------------------|
| No.          |            | Used<br>(yes/no)          | Pretared Container<br>(No.) |
|              | <u>380</u> |                           |                             |
|              | <u>357</u> |                           |                             |
|              | <u>346</u> | <u>10<math>\mu</math></u> |                             |
|              |            | <u>3<math>\mu</math></u>  |                             |
|              |            | <u>1<math>\mu</math></u>  |                             |

| IMPINGER VOLUMES          |               |                 |         |
|---------------------------|---------------|-----------------|---------|
|                           | Initial       | Final           |         |
| First ( $H_2O_2$ )        | <u>500</u> ml | <u>570.0</u> ml |         |
| Second ( $APS + AgNO_3$ ) | <u>500</u> ml | <u>452.6</u> ml |         |
| Third ( $APS + AgNO_3$ )  | <u>500</u> ml | <u>405.0</u> ml |         |
| TOTALS                    | ml            | ml              | Gain ml |

| SILICA GEL WEIGHTS |                |                |        |
|--------------------|----------------|----------------|--------|
|                    | Initial        | Final          |        |
|                    | <u>800.0</u> g | <u>989.9</u> g |        |
|                    | <u>800.0</u> g | <u>998.8</u> g |        |
|                    | <u>800.0</u> g | <u>914.2</u> g |        |
| TOTALS             | g              | g              | Gain g |

| CONDENSATE                                 |  |    |  |
|--|--|----|--|
| TOTAL VOLUME COLLECTED                     |  |    |  |
| Volume Neat                                |  | ml |  |
| Volume Extracted                           |  | ml |  |
| Volume $CH_2Cl_2$ Extract ( $3 \times$ ml) |  | ml |  |
| Extracted Condensate: pH Neat              |  |    |  |
| Amount 96% $ENo_3$ added                   |  |    |  |
| pH Final                                   |  |    |  |
| TOTAL GAIN                                 |  | ml |  |

Plant ROCKFORDNES  
Date 7/7/93  
Sample Location SKILL HOUSE  
Sample Type H2L  
Run Number 62  
Operator BORHUS  
Ambient Temperature 75  
Barometric Pressure 30.0  
Static Pressure, ( $H_2O$ ) -10  
Filter Number(s) N/A

Leak Check: Initial at 12" Hg, .003 CFM  
Final at 12" Hg, .010 CFM  
Pitot leak Check:

Pitot Leak Check: Pass

| Impinger Volumes |       |          |
|------------------|-------|----------|
| Initial          | Final | Net Gain |
| 100              | 190   | -10      |
|                  |       |          |
|                  |       |          |
|                  |       |          |
|                  |       |          |
|                  |       |          |
| Silica Gel       |       |          |
| 56.78            | 53.20 | 4.52     |

Probe Length and Type 5 ft. ext.  
 Nozzel Size & I.D. .387  
 Pitot Coefficient & I.D. .6500  
 Assumed Moisture .075  
 Molecular Weight, Dry, ( $M_d$ )  
 Meter Box Number NAPP - 02,54  
 Meter Coefficient .1785  
 $\alpha$  Factor 0.012  
 $K = \frac{4411.373}{(N_d)^4}$   
 $K(N_d)^4 = \underline{\quad} \times (\underline{\quad})^4 = \underline{18.873}$   
 $\Delta H = K(N_d)^4 \left( \frac{T_m}{T_s} \right) (P)$

SASS Condensate \_\_\_\_\_  
Total Volume - 58

## ISOKINETIC CALCULATIONS - USEPA: M/5 BASIS

## ROCK OF AGES - NO. 2

| RUN NUMBER               | 2-SASS<br>7-7-83<br>PWK | 2-M5/8<br>7-7-83<br>VB | 2-HCL<br>7-7-83<br>VB |
|--------------------------|-------------------------|------------------------|-----------------------|
| METER VOLUME, CF         | 960.049                 | 31.853                 | 14.871                |
| METER COEF               | 0.973                   | 1.012                  | 1.012                 |
| BAROMETRIC PRES, HG      | 28.6                    | 28.6                   | 28.6                  |
| DELTA H, IN H2O          | 1.988                   | 0.813                  | 0.74                  |
| METER TEMP, DEG F        | 107.7                   | 90                     | 94.5                  |
| STACK TEMP, DEG F        | 290.5                   | 329                    | 324.7                 |
| CONDENSATE, ML           | 1097.9                  | 39.2                   | 15.7                  |
| PERCENT CO2              | 7.5                     | 7.5                    | 7.5                   |
| PERCENT O2               | 8.8                     | 8.8                    | 8.8                   |
| PERCENT CO               | 0                       | 0                      | 0                     |
| PERCENT N2               | 83.7                    | 83.7                   | 83.7                  |
| STATIC PRES, IN H2O      | -0.1                    | -0.1                   | -0.1                  |
| PITOT COEF               | 0.79                    | 0.79                   | 0.79                  |
| SQRT DELTA P, IN H2O     | 0.251                   | 0.248                  | 0.245                 |
| STACK AREA, SQ FT        | 2.405                   | 2.405                  | 2.405                 |
| NOZZLE DIAM, IN          | 1.24                    | 0.387                  | 0.367                 |
| TEST TIME, MIN           | 260                     | 60                     | 30                    |
| MASS PARTICULATE, G      | 0                       | 0                      | 0                     |
| F-FACTOR, DSCF/MBTU      |                         |                        |                       |
| VOLUME, DSCF             | 881.833                 | 28.948                 | 13.403                |
| WATER VAPOR, SCF         | 51.678                  | 1.845                  | 0.739                 |
| PERCENT MOISTURE         | 0.055                   | 0.060                  | 0.052                 |
| MOLECULAR WT DRY, LB/LB  | 29.552                  | 29.552                 | 29.552                |
| MOLECULAR WT WET, LB/LB  | 28.91                   | 28.86                  | 28.95                 |
| STACK PRES, IN HG        | 28.59                   | 28.59                  | 28.59                 |
| STACK VELOCITY, FT/SEC   | 16.15                   | 16.38                  | 16.11                 |
| MASS FLOW, DSCFM         | 1,480                   | 1,421                  | 1,417                 |
| MASS FLOW, ACFM          | 2,331                   | 2,363                  | 2,325                 |
| PERCENT EXCESS AIR       |                         |                        |                       |
| PERCENT ISOKINETIC       | 65.762                  | 100.057                | 92.915                |
| GRAIN LOADING, GR/DSCF   | 0.00000                 | 0.00000                | 0.00000               |
| GRAIN LOADING, GR/ACF    | 0.00000                 | 0.00000                | 0.00000               |
| EMISSION RATE, LB/HR-STD | 0.00000                 | 0.00000                | 0.00000               |
| EMISSION RATE, LB/MBTU   |                         |                        |                       |

Plant ROCK OF AGESDate 1/1/83Sample Location SAW HOUSESample Type M-53Run Number 3Operator BARKERAmbient Temperature 70Barometric Pressure 28.60Static Pressure, (H<sub>2</sub>O) -10

Filter Number(s) \_\_\_\_\_

Leak Check: Initial at .10 " Hg, .024 CFM  
Final at .13 " Hg, .015 CFMPitot Leak Check: ✓

## Impinger Volumes

| Initial | Final | Net Gain |
|---------|-------|----------|
| 520.0   | 487.1 | -32.9    |
| 545.8   | 535.1 | -10.7    |
| 502.2   | 452.4 | -49.8    |
| 671.4   | 637.6 | -33.8    |
| —       | —     | —        |
| —       | —     | —        |
| —       | —     | —        |
| —       | —     | —        |

## Silica Gel

|   |   |      |
|---|---|------|
| — | — | 16.1 |
| — | — | —    |
| — | — | —    |
| — | — | —    |
| — | — | —    |

Probe Length and Type 5" PYREXNozzle Size & I.D. .1387 / 905Pitot Coefficient & I.D. .8321Assumed Moisture .275Molecular Weight, Dry, (M<sub>d</sub>) 28.8Meter Box Number 0554Meter Coefficient .7235 $\alpha$  Factor 1.012K = 834.939

$$K(N_d)^4 = 834.939 \cdot (1.387)^4 = 1884$$

$$\Delta H = K(N_d)^4 \left( \frac{T_m}{T_s} \right) (P)$$

## SASS Condensate

| Total Volume | 32.7 |
|--------------|------|
| —            | —    |

| Traverse Point Number | Sampling Time, min | Gas Meter Reading (V <sub>m</sub> ), ft <sup>3</sup> | Velocity Head (ΔP <sub>s</sub> ), in. H <sub>2</sub> O | Orifice Pressure Differential (ΔH), in. H <sub>2</sub> O |        | Temperature °F |       |          |                |      |           | Pump Vacuum in. Hg | Avg. $\sqrt{\Delta P}$ |  |  |
|-----------------------|--------------------|--|--|--|--------|----------------|-------|----------|----------------|------|-----------|--------------------|------------------------|--|--|
|                       |                    |  |  | Desired  | Actual | Stack          | Probe | Impinger | Organic Module | Oven | Gas Meter |                    |                        |  |  |
|                       |                    |  |  |  |        |                |       |          |                |      | In        | Out                |                        |  |  |
| A-1                   | 5                  | 727.64   | .07  | .94  | .94    | 310            |       | 61       |                | 345  | 81        | 68                 | 7.5                    |  |  |
| 2                     | 10                 | 730.409  | .07  | .94  | .94    | 320            |       | 62       |                | 345  | 91        | 37                 | 7.5                    |  |  |
| 3                     | 15                 | 733.49   | .07  | .96  | .96    | 293            |       | 65       |                | 344  | 88        | 84                 | 7.5                    |  |  |
| 4                     | 20                 | 736.43   | .07  | .97  | .97    | 283            |       | 78       |                | 337  | 88        | 88                 | 7.5                    |  |  |
| 5                     | 25                 | 739.37   | .07  | .98  | .98    | 250            |       | 68       |                | 265  | 88        | 85                 | 7.5                    |  |  |
| 6                     | 30                 | 742.252  | .065   | .91  | .91    | 278            |       | 69       |                | 258  | 88        | 88                 | 7.5                    |  |  |
| X                     | 1709               | 745.74   | .07  | 1.07   | 1.07   | 276            |       | 66       |                | 260  | 88        | 78                 | 7.5                    |  |  |
| B-1                   | 35                 | 1719   | .081   | 1.27   | 1.27   | 276            |       | 66       |                | 360  | 88        | 91                 | 7.5                    |  |  |
| 2                     | 40                 | 748.68   | .09  | 1.09   | 1.09   | 203            |       | 66       |                | 92   | 90        | 90                 | 7.0                    |  |  |

7602/5/81/Rev 1

Comments: \* changed

Run No. 3 M-58

Date 7/1/83

Sampling Location SAC 1st floor

**Comments:**

Plant ROCK OF Ages  
Date 1/7/83  
Sample Location SAR HOUSE  
Sample Type HIC L.  
Run Number 1  
Operator BARKER'S  
Ambient Temperature 75  
Barometric Pressure 30.03  
Static Pressure, ( $H_2O$ ) -10  
Filter Number(s) N/A

Leak Check: Initial at 13" Hg, .013 CFM  
Final at 25" Hg, .007 CFM

**Pitot Leak Check:**

#### **Pitot Leak Check:**

Probe Length and Type \_\_\_\_\_  
 Nozzel Size & I.D. \_\_\_\_\_, 387  
 Pitot Coefficient & I.D. \_\_\_\_\_ 0.4322  
 Assumed Moisture \_\_\_\_\_  
 Molecular Weight, Dry, ( $M_d$ ) \_\_\_\_\_  
 Meter Box Number \_\_\_\_\_ NIAFF-D554  
 Meter Coefficient \_\_\_\_\_ 7.2K  
 $\alpha$  Factor \_\_\_\_\_ 1.012  
 $K = \frac{641.373}{5}$   
 $K(N_d)^4 = \underline{\quad} \times (\underline{\quad})^4 = 16873$   
 $\Delta H = K(N_d)^4 \left( \frac{T_m}{T_s} \right) (P)$

SASS Condensate \_\_\_\_\_  
Total Volume 17.6

### Comments:

## ISOKINETIC CALCULATIONS - USEPA: M/5 BASIS

ROCK OF AGES - NO. 3

| RUN NUMBER               | 3-M5/8  | 3-HCL   |
|--------------------------|---------|---------|
| DATE OF TEST             | 7-7-83  | 7-7-83  |
| OPERATOR                 | VB      | VB      |
| METER VOLUME, CF         | 36.383  | 13.856  |
| METER COEF               | 1.012   | 1.012   |
| BAROMETRIC PRES, HG      | 28.6    | 28.6    |
| DELTA H, IN H2O          | 0.976   | 0.647   |
| METER TEMP, DEG F        | 88.4    | 91      |
| STACK TEMP, DEG F        | 276.7   | 326.8   |
| CONDENSATE, ML           | 32.7    | 17.2    |
| PERCENT CO2              | 7.5     | 7.5     |
| PERCENT O2               | 8.8     | 8.8     |
| PERCENT CO               | 0       | 0       |
| PERCENT N2               | 83.7    | 83.7    |
| STATIC PRES, IN H2O      | -0.1    | -0.1    |
| PITOT COEF               | 0.79    | 0.79    |
| SQRT DELTA P, IN H2O     | 0.263   | 0.257   |
| STACK AREA, SQ FT        | 2.405   | 2.405   |
| NOZZLE DIAM, IN          | 0.387   | 0.387   |
| TEST TIME, MIN           | 60      | 30      |
| MASS PARTICULATE, G      | 0       | 0       |
| F-FACTOR, DSCF/MBTU      | 0       | 0       |
| VOLUME, DSCF             | 33.176  | 12.564  |
| WATER VAPOR, SCF         | 1.539   | 0.810   |
| PERCENT MOISTURE         | 0.044   | 0.061   |
| MOLECULAR WT DRY, LB/LB  | 29.552  | 29.552  |
| MOLECULAR WT WET, LB/LB  | 29.04   | 28.85   |
| STACK PRES, IN HG        | 28.59   | 28.59   |
| STACK VELOCITY, FT/SEC   | 16.73   | 16.95   |
| MASS FLOW, DSCFM         | 1,580   | 1,474   |
| MASS FLOW, ACFM          | 2,414   | 2,446   |
| PERCENT EXCESS AIR       |         |         |
| PERCENT ISOKINETIC       | 103.100 | 83.741  |
| GRAIN LOADING, GR/DSCF   | 0.00000 | 0.00000 |
| GRAIN LOADING, GR/ACF    | 0.00000 | 0.00000 |
| EMISSION RATE, LB/HR-STD | 0.00000 | 0.00000 |
| EMISSION RATE, LB/MBTU   |         |         |

~~VOST~~ ACUREX CORPORATION  
~~AMBIENT AIR / PERSONNEL MONITORING LOG~~

COMPANY PARK OFFICE LOCATION WELLSVILLE PROJECT NO. 27-1001 RECORDED BY C. C. L.

SECTION 5  
ANALYTICAL RESULTS

- 5.1 FUEL AND ASH SAMPLE PROXIMATE AND ULTIMATE ANALYSES
- 5.2 PARTICULATE EMISSIONS FROM SASS SAMPLES
- 5.3 PARTICULATE AND SULFUR OXIDES EMISSIONS FROM EPA METHOD 5/8 SAMPLES
- 5.4 HC1 EMISSIONS FROM HC1 TRAIN SAMPLES
- 5.5 TRACE ELEMENT AND LEACHABLE ANION ANALYSES
- 5.6 TOTAL CHROMATOGRAPHABLE ORGANICS (TCO), GRAVIMETRIC ORGANICS (GRAV), GAS CHROMATOGRAPHY/MASS SPECTROMETRY (GC/MS), AND INFRARED SPECTRA (IR) OF TOTAL SAMPLE EXTRACTS
- 5.7 LIQUID CHROMATOGRAPHY (LC) SEPARATION AND IR SPECTRA OF LC FRACTIONS
- 5.8 GC/MS ANALYSES OF VOST TRAPS
- 5.9 N<sub>2</sub>O ANALYSES BY GC/ECD
- 5.10 BIOASSAY RESULTS

## 5.1 FUEL AND ASH SAMPLE PROXIMATE AND ULTIMATE ANALYSES

In the following, the sample denoted cyclone ash test 3 is a blind duplicate of the cyclone ash test 1 sample.

## LABORATORY CERTIFICATE

**CURTIS & TOMPKINS, LTD.**

ESTABLISHED 1878

Bulk Oil & Chemical Surveyors, Samplers & Weighers  
Analytical & Consulting Chemists

**SOUTHERN DIVISION**  
 401 Canal Street  
 WILMINGTON, CA 90748  
 213-549-6740  
 TWX 910-345-6820  
 ANALYST WILN

290 Division Street  
 San Francisco, CA 94103  
 415-861-1863  
 Telex: 171042  
 CABLE: ANALYST SFO

Laboratory No. 83n160  
 Preliminary No. 4625

**FOOD TECHNOLOGISTS****ENVIRONMENTAL ANALYSTS****MEMBERS, OFFICIAL CHEMISTS  
AND/OR SAMPLERS FOR GOVERNMENT  
AGENCIES AND TRADE ORGANIZATIONS**

Reported 12/14/83  
 Sampled -----  
 Received 11/22/83

For ACUREX CORPORATION

Report on 11 samples of Products

**Mark**

- 1) 819449, RA Coal, Test 1
- 2) 819485, RA Pet, Test 2
- 3) 819478, RA Coal, Pet, Test 2
- 4) 900209, DM Coal Water Slurry
- 5) 819498, RA Bottom Ash, Test 1
- 6) 819498, RA Bottom Ash, Test 2
- 7) 819476, RA Cyclone Ash, Test 1
- 8) 819504, RA Cyclone Ash, Test 2
- 9) 819457, RA Cyclone Ash, Test 3
- 10) 819475, RA Composite Particulate, Test 1
- 11) 819475, RA Composite Particulate, Test 2

P.O. RB59186A Rel 7

SEE ATTACHED FOR RESULTS

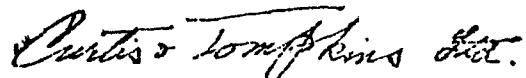
SAMPLES DISCARDED 30 DAYS AFTER RECEIPT UNLESS OTHERWISE REQUESTED

| <u>ULTIMATE ANALYSIS - Dry Basis, %</u> | <u>1</u>           | <u>2</u> | <u>3</u> | <u>4</u> | <u>5</u> | <u>6</u> | <u>7</u> | <u>8</u> | <u>9</u> | <u>10</u> | <u>11</u> |
|---|--------------------|----------|----------|----------|----------|----------|----------|----------|----------|-----------|-----------|
| Carbon -----                            | 71.50              | 73.80    | 73.10    | 83.50    | 16.70    | 21.20    | 30.90    | 33.60    | 30.90    | 14.50     | 21.10     |
| Hydrogen-----                           | 5.30               | 10.30    | 5.60     | 5.30     | 0.14     | 0.17     | 1.40     | 0.92     | 1.07     | 1.54      | 1.10      |
| Nitrogen (1st Test) -----               | 1.51               | 0.08     | 1.27     | 1.52     | 0.20     | 0.35     | 1.00     | 1.20     | 1.06     | 1.00      | 0.48      |
| Nitrogen (2nd Test) -----               | 1.53               | 0.16     | 1.48     | 1.62     |          |          |          |          |          |           |           |
| Nitrogen (3rd Test) -----               | 1.58               | 0.20     | 1.40     | 1.66     |          |          |          |          |          |           |           |
| Sulfur (1st Test) -----                 | 0.092 <sup>a</sup> | 0.07     | 0.63     | 0.84     | 0.24     | 0.18     | 4.50     | 2.90     | 4.60     |           |           |
| Sulfur (2nd Test) -----                 | 0.095 <sup>a</sup> | 0.10     | 0.65     | 0.90     |          |          |          |          |          |           |           |
| Sulfur (3rd Test) -----                 | 0.098 <sup>a</sup> | 0.08     | 0.68     | 0.95     |          |          |          |          |          |           |           |
| Ash -----                               | 8.78               | 1.66     | 7.02     | 4.41     | 81.59    | 0.54     | 51.06    | 51.04    | 48.39    | 61.40     | 42.71     |
| Oxygen (by Difference)-----             | 12.50              | 13.93    | 12.29    | 4.09     | 1.08     | 77.48    | 10.94    | 10.08    | 13.79    | 21.56     | 34.61     |
| Chloride -----                          | 0.20               | 0.07     | 0.23     | 0.20     | 0.05     | 0.08     | 0.20     | 0.26     | 0.19     |           |           |

PROXIMATE ANALYSIS - Dry Basis, %

|                           |        |        |        |        |       |       |       |       |       |       |       |
|---------------------------|--------|--------|--------|--------|-------|-------|-------|-------|-------|-------|-------|
| Gross Heating Value       |        |        |        |        |       |       |       |       |       |       |       |
| BTU per Lb. -----         | 13,825 | 12,870 | 13,670 | 15,020 | 600   | 1,600 | 4,940 | 5,340 | 4,700 |       |       |
| Volatile Matter -----     | 34.14  | 92.92  | 42.33  | 30.69  |       |       |       |       |       |       |       |
| Fixed Carbon -----        | 57.08  | 5.42   | 50.65  | 64.90  |       |       |       |       |       |       |       |
| Ash -----                 | 8.78   | 1.66   | 7.02   | 4.41   | 81.59 | 0.54  | 51.06 | 51.04 | 48.39 | 61.40 | 42.71 |
| Moisture (as Rec'd) ----- | 2.73   | 0.53   | 1.43   | 44.07  | 0.15  | 0.14  | 8.73  | 3.99  | 8.97  |       |       |

<sup>a</sup>J. Vale of Curtis and Thompkins reported by phone to H. Lips of Acurex on March 23, 1984, that the sulfur analyses for sample 1 were 0.92, 0.95, and 0.98 for the three tests, respectively (authors)



## 5.2 PARTICULATE EMISSIONS FROM SASS SAMPLES

**ACUREX**  
**ANALYTICAL REPORT**

Sample of: CMEA/Rock of Ages

Sample Date: 7-7-83

Requested By: L. Waterland

I.D. Number: 307735-62

Analytical Method: SASS -1 Particulate weights

Date of Analysis: 7/19 - 7/22-83

| Lab I.D. Number | Component          | Analytical Result                   | Unit |
|-----------------|--------------------|-------------------------------------|------|
| 819461          | SASS probe<br>wash | 1.5993<br>1.4276 tare<br>0.1717 net | g    |
| 819456          | 10 $\mu$ cyclone   | 0.0877                              |      |
| 819457          | 3 $\mu$ cyclone    | 0.2156                              |      |
| 819458          | 1 $\mu$ cyclone    | 0.0793                              |      |
| 819463          | Filter 354 (#1)    | 1.3160<br>1.0341 tare<br>0.2819 net |      |
| 819464          | Filter 360 (#2)    | 1.1973<br>1.1419 tare<br>0.0554 net |      |

Analysis By Neasten

5-9 Date 7-22-83

## ISOKINETIC PERFORMANCE WORKSHEET &amp; PARTICULATE CALCULATIONS

Plant Rock of AgesPerformed by DaRosaDate 2-6-83Sample Location Saw HouseTest No./Type 1 - SASS

|   |                               |         |
|---|-------------------------------|---------|
| Barometric Pressure (in. Hg)  | $P_b$                         | 28.24   |
| Meter volume (std),<br>$17.64 \left( \frac{V_m}{\alpha} \right) \left( \frac{P_b + \Delta H}{T_m + 460} \right)$ $17.64 \left( \frac{992.884}{(972)} \right) \left( \frac{(28.24) + (2.012)}{13.6 + 460} \right)$ | $V_m$ std                     | 967.246 |
| Volume of liquid collected (grams)  | $V_l_c$                       | 964.7   |
| Volume of liquid at standard condition (scf)<br>$V_l_c \times 0.04707$  | $V_w$ std                     | 45.408  |
| Stack gas proportion of water vapor<br>$\frac{V_w \text{ std}}{V_w \text{ std} + V_m \text{ std}}, \quad \frac{45.408}{(45.408) + (967.246)}$   | $B_{w0}$                      | 0.045   |
| Molecular weight, stack gas dry<br>(1b/lb-mole)<br>$(\% CO_2 \times 0.44) + (\% O_2 \times 0.32) + (\% N_2 + \% CO \times 0.28)$<br>$(7.1 \times 0.44) + (12.2 \times 0.32) + (80.7 + \text{blank} \times 0.28)$  | $M_d$<br><i>From MPR Avg.</i> | 29.624  |
| Molecular weight, stack gas wet<br>(1b/lb-mole)<br>$M_d(1-B_{w0}) + 18(B_{w0}), \quad (29.624)(1-0.045) + 18(0.045)$  | $M_s$                         | 29.10   |
| Absolute stack pressure (in. Hg)<br>$P_b + \frac{P_{stack} \text{ (in. H}_2\text{O)}}{13.6}, \quad (28.24) + \frac{(-0.1)}{13.6}$   | $P_s$                         | 28.23   |

|   |  |                        |
|---|--|------------------------|
| Temperature stack gas, average ( $^{\circ}$ F)  | $T_s$  | 274.3                  |
| Stack velocity (fps)<br>85.49 ( $C_p$ ) $(\sqrt{\Delta P_s \text{ avg}})$   | $\sqrt{\frac{T_s \text{ avg} + 460}{P_s \text{ avg} M_s}}$ | $V_s(\text{avg})$ 4.94 |
| 85.49 ( <u>.79</u> ) $(\sqrt{.234})^2$  | $\sqrt{\frac{(274.3) + 460}{(28.23)(29.10)}}$              |                        |
| Total sample time (minutes)   | $\theta$   | 260                    |
| Nozzle diameter, actual (inches)  | $N_d$  | 1.240                  |
| Percent isokinetic (%)<br>17.33 $(T_s + 460)(V_w \text{ std} + V_m \text{ std})$  | %I   | 76.421                 |
| $\frac{\theta \ V_s \ P_s \ N_d^2}{17.33 ((____ + 460)((____) + (____))}$<br>$\frac{(\____)(\____)(\____)(\____)^2}{}$  |  |                        |
| Area of stack ( $\text{ft}^2$ ) $\pi = 3.1416$<br>$\pi r^2 \div 144, \pi (\underline{10.5''})^2 \div 144$   | $A_s$  | 2.405                  |
| Stack gas volume at standard conditions (dscfm)<br>60 $(1 - B_{wo}) V_s \text{ avg } A_s \left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$ | ACFM<br>$Q_s$  | 2,156<br>1,397         |
| $60 (1 - \underline{\quad})(\underline{\quad})(\underline{\quad}) \left( \frac{528}{\underline{\quad} + 460} \right) \left( \frac{(\underline{\quad})}{(29.92)} \right)$    |  |                        |
| Particulate matter concentration, dry (gr/dscf)<br>15.432 $\frac{M_p \text{ (grams)}}{V_m \text{ std}}$ , 15.432 $\frac{(0.8156)}{(967.246)}$                               | $C_s \text{ (std)}$  | 0.01308                |
| Emission rate of particulate matter (lb/hr)<br>0.00857 $(Q_s) C_s \text{ (std)}$ , 0.00857 $(\underline{\quad})(\underline{\quad})$   | $E_p$  |                        |

**ACUREX**  
**ANALYTICAL REPORT**

Sample of: CMEA/ Rock of Ages

Sample Date: 7-7-83

Requested By: L. Waterhouse

I.D. Number: 307735-62

Analytical Method: SASS-2 Particulate Weights

Date of Analysis: 7/19 - 7/22/83

| Lab I.D. Number | Component    | Analytical Result                   | Unit |
|-----------------|--------------|-------------------------------------|------|
| 819482          | Protein wash | 1.5820<br>1.4321 tare<br>0.1499 net | g    |
| 819492          | 10µ cyclone  | 0.1181                              |      |
| 819493          | 3µ cyclone   | 0.3160                              |      |
| 819494          | 1µ cyclone   | broken                              |      |
| 819475          | Filter 346   | 1.3105<br>1.1292 tare<br>0.1813 net |      |
| 819495          | Filter 357   | 1.2937<br>1.1488 tare<br>0.1449 net |      |
| 819486          | Filter 380   | 1.2947<br>1.1560 tare<br>0.1387 net |      |

Analysis By Brewster

## ISOKINETIC PERFORMANCE WORKSHEET &amp; PARTICULATE CALCULATIONS

Plant Rock of AgesPerformed by D. R. S.Date 7-7-83Sample Location Saw HouseTest No./Type 2-SASS

|  |                       |         |
|--|-----------------------|---------|
| Barometric Pressure (in. Hg)   | $P_b$                 | 28.60   |
| Meter volume (std),<br>$17.64 \left( \frac{V_m}{\alpha} \right) \left( P_b + \frac{\Delta H}{13.6} \right)$ $17.64 \left( \frac{960.049}{(.973)} \right) \left( \frac{(28.60)}{(107.7)} + \frac{(1.988)}{13.6} \right)$                              | $V_m$ std             | 881.833 |
| Volume of liquid collected (grams)   | $V_l_c$               | 1097.9  |
| Volume of liquid at standard condition (scf)<br>$V_l_c \times 0.04707$   | $V_w$ std             | 51.678  |
| Stack gas proportion of water vapor<br>$\frac{V_w \text{ std}}{V_w \text{ std} + V_m \text{ std}}, \frac{(51.678)}{51.678 + (881.833)}$  | $B_{wo}$              | 0.055   |
| Molecular weight, stack gas dry<br>$(\text{lb/lb-mole})$<br>$(\% \text{CO}_2 \times 0.44) + (\% \text{O}_2 \times 0.32) + (\% \text{N}_2 + \% \text{CO} \times 0.28)$<br>$(7.5 \times 0.44) + (8.8 \times 0.32) + (83.7 + \text{_____} \times 0.28)$ | $M_d$<br>From MPR Avg | 29.552  |
| Molecular weight, stack gas wet<br>$(\text{lb/lb-mole})$<br>$M_d(1-B_{wo}) + 18(B_{wo}), (29.552)(1-0.055) + 18(0.055)$  | $M_s$                 | 28.91   |
| Absolute stack pressure (in. Hg)<br>$P_b + \frac{P_{stack} \text{ (in. H}_2\text{O)}}{13.6}, (28.60) + \frac{(-0.1)}{13.6}$  | $P_s$                 | 28.59   |

|   |                     |        |
|---|---------------------|--------|
| Temperature stack gas, average ( $^{\circ}$ F)  | $T_s$               | 290.5  |
| Stack velocity (fps)<br>$85.49 (C_p) (\sqrt{\Delta P_s \text{ avg}}) \sqrt{\frac{T_s \text{ avg} + 460}{P_s M_s}}$<br>$85.49 (.79)(.251) \sqrt{\frac{(290.5) + 460}{(28.59)(28.91)}}$ | $V_s(\text{avg})$   | 16.15  |
| Total sample time (minutes)   | $\theta$            | 260    |
| Nozzle diameter, actual (inches)  | $N_d$               | 1.240  |
| Percent isokinetic (%)<br>$17.33 (T_s + 460)(V_w \text{ std} + V_m \text{ std})$  | %I                  |        |
| $\frac{\theta V_s P_s N_d^2}{17.33 ( \text{___} + 460) ((\text{___}) + (\text{___})) (\text{___})(\text{___})(\text{___})(\text{___})^2}$   |                     | 65.762 |
| Area of stack ( $\text{ft}^2$ ) $\pi = 3.1416$<br>$\pi r^2 \div 144, \pi (\underline{10.5})^2 \div 144$   | $A_s$               | 2.405  |
| Stack gas volume at standard conditions (dscfm)<br>$60 (1 - B_{w0}) V_s \text{ avg } A_s \left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$           | $A_{\text{cfm}}$    | 2,331  |
| $60 (1 - \underline{\quad})(\underline{\quad})(\underline{\quad}) \left( \frac{528}{\underline{\quad} + 460} \right) \left( \frac{(\underline{\quad})}{(29.92)} \right)$              | $Q_s$               | 1,480  |
| Particulate matter concentration, dry (gr/dscf)<br>$15.432 \frac{M_p \text{ (grams)}}{V_m \text{ std}}, 15.432 \frac{(\underline{\quad})}{(\underline{\quad})}$                       | $C_s \text{ (std)}$ |        |
| Emission rate of particulate matter (lb/hr)<br>$0.00857 (Q_s) C_s \text{ (std)}, 0.00857 (\underline{\quad})(\underline{\quad})$  | $E_p$               |        |

\*  $\mu$  cycle lost

### 5.3 PARTICULATE AND SULFUR OXIDES EMISSIONS FROM EPA METHOD 5/8 SAMPLES

# ACUREX ANALYTICAL REPORT

Sample of: CMEA/Rock of Ages

Sample Date: 7/6 - 7/7/83

Requested By: L. Waterland

I.D. Number: 307735.6)

Analytical Method: M/5 Filter weights  
 Date of Analysis: 7-22-83

| Lab I.D. Number | Component             | Analytical Result                             | Unit |
|-----------------|-----------------------|---|------|
| 819571          | Filter Blank          | 0.47655<br>0.47385 tare<br><u>0.00270</u> net | g    |
| 819566          | M/5 Filter,<br>test 1 | 0.52386<br>0.47819 tare<br><u>0.04567</u> net |      |
| 819472          | M/5 Filter,<br>test 2 | 0.53376<br>0.47424 tare<br><u>0.05552</u> net |      |
| 819490          | M/5 Filter,<br>test 3 | 0.50041<br>0.47654 tare<br><u>0.02387</u> net |      |

Analysis By Murphy

5-17 Date 7-22-83

**ACUREX**  
**ANALYTICAL REPORT**

Sample of: CMEA/Rock of Ages

Sample Date: 7/16 - 7/18/83

Requested By: Waterland

I.D. Number: 307735-62

Analytical Method: Sulfate analyses of MetRock 8 impingers

Date of Analysis: 7-25-83

| Lab I.D. Number                                  | Component                                  | Analytical Result        | Unit                    |
|--|--|--------------------------|-------------------------|
| 819569   | 80% IMA<br>blank                           | 0.5                      | mg SO <sub>3</sub>      |
| 819567   | MSK-1<br>1st impinger                      | 5.7                      |                         |
| 819470   | MSK-2<br>1st impinger                      | 4.6                      |                         |
| 819491   | MSK-3<br>1st impinger                      | 2.5                      |                         |
| 819570   | 690 H <sub>2</sub> O <sub>2</sub><br>blank | 3.2                      | mg SO <sub>2</sub>      |
| 819568   | MSK-1<br>2T3 impinger                      | 963.4                    |                         |
| 819471   | MSK-2<br>2T3 impinger                      | 946.9                    |                         |
| 819487   | MSK-3<br>2T3 impinger                      | 450.8                    |                         |
| Lot 0282 audit<br>Samples : 4xxx<br>8xxx<br>9xxx |  | 355.4<br>2345.4<br>873.5 | mg SO <sub>2</sub> /dsu |

Analysis By Murray

Date 7-25-83

## ISOKINETIC PERFORMANCE WORKSHEET &amp; PARTICULATE CALCULATIONS

 Plant Rock of Ages

 Performed by D. K.

 Date 7-6-83

 Sample Location Saw House

 Test No./Type 1 - M5/8

|  |                        |        |
|--|------------------------|--------|
| Barometric Pressure (in. Hg)   | $P_b$                  | 28.24  |
| Meter volume (std),<br>$17.64 \left( \frac{V_m}{\alpha} \right) \left( P_b + \frac{\Delta H}{13.6} \right)$ $17.64 \left( \frac{(30.22)}{1.012} \right) \left( \frac{(28.24) + (.703)}{13.6} \right)$ $\frac{(2.546)}{(2.546) + (28.161)}$ | $V_m$ std              | 28.161 |
| Volume of liquid collected (grams)   | $V_{l_c}$              | 54.1   |
| Volume of liquid at standard condition (scf)<br>$V_{l_c} \times 0.04707$   | $V_w$ std              | 2.546  |
| Stack gas proportion of water vapor<br>$\frac{V_w \text{ std}}{V_w \text{ std} + V_m \text{ std}}, \frac{(2.546)}{(2.546) + (28.161)}$   | $B_{w0}$               | 0.083  |
| Molecular weight, stack gas dry<br>(lb/lb-mole)<br>$(\% CO_2 \times 0.44) + (\% O_2 \times 0.32) + (\% N_2 + \% CO \times 0.28)$<br>$(7.1 \times 0.44) + (12.2 \times 0.32) + (80.7 + \text{blank} \times 0.28)$                           | $M_d$<br>From MPR Avg. | 29.624 |
| Molecular weight, stack gas wet<br>(lb/lb-mole)<br>$M_d(1-B_{w0}) + 18(B_{w0}), (29.624)(1-.083) + 18(.083)$   | $M_s$                  | 28.66  |
| Absolute stack pressure (in. Hg)<br>$P_b + \frac{P_{stack} \text{ (in. H}_2\text{O)}}{13.6}, (28.24) + \frac{(-0.1)}{13.6}$  | $P_s$                  | 28.23  |

|  |  |                         |
|--|--|-------------------------|
| Temperature stack gas, average ( $^{\circ}$ F)   | $T_s$  | 295.3                   |
| Stack velocity (fps)<br>85.49 ( $C_p$ ) $(\sqrt{\Delta P_s \text{ avg}})$  | $\sqrt{\frac{T_s \text{ avg} + 460}{P_s \text{ avg} M_s}}$       | $V_s(\text{avg})$ 15.07 |
| 85.49 (.79) (.231)   | $\sqrt{\frac{(295.3 + 460)}{(28.23)(28.66)}}$                    |                         |
| Total sample time (minutes)  | $\theta$   | 60                      |
| Nozzle diameter, actual (inches)   | $N_d$  | 0.387                   |
| Percent isokinetic (%)<br>17.33 $(T_s + 460)(V_w \text{ std} + V_m \text{ std})$   | %I   | 105.109                 |
| $\theta$ $V_s$ $P_s$ $N_d^2$<br>$\frac{17.33 (\underline{\quad} + 460)((\underline{\quad}) + (\underline{\quad}))}{(\underline{\quad})(\underline{\quad})(\underline{\quad})(\underline{\quad}))^2}$ |  |                         |
| Area of stack ( $\text{ft}^2$ ) $\pi = 3.1416$<br>$\pi r^2 \div 144, \pi (\underline{0.5''})^2 \div 144$   | $A_s$  | 2.405                   |
| Stack gas volume at standard conditions (dscfm)<br>60 $(1 - B_{w0})V_s \text{ avg } A_s \left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$                           | ACFM   | 2,175                   |
| $60 (1 - \underline{\quad})(\underline{\quad})(\underline{\quad}) \left( \frac{528}{\underline{\quad} + 460} \right) \left( \frac{(\underline{\quad})}{(29.92)} \right)$                             | $Q_s$  | 1,316                   |
| Particulate matter concentration, dry (gr/dscf)<br>15.432 $\frac{M_p \text{ (grams)}}{V_m \text{ std}}, 15.432 \frac{(\underline{0.00857})}{(\underline{28.161})}$                                   | $C_s(\text{std})$  | 0.02355                 |
| Emission rate of particulate matter (lb/hr)<br><del>0.00857 (<math>Q_s</math>) <math>C_s(\text{std})</math>, 0.00857 (<math>\underline{\quad}</math>) (<math>\underline{\quad}</math>)</del>         | $\frac{SO_2}{E_p} = \frac{963.7}{28.161} = 34.2 \text{ mg dscf}$ |                         |

## ISOKINETIC PERFORMANCE WORKSHEET &amp; PARTICULATE CALCULATIONS

Plant Rock of AgesPerformed by DR RorDate 2-7-83Sample Location Saw HouseTest No./Type 2 - ms/8

|   |           |        |
|---|-----------|--------|
| Barometric Pressure (in. Hg)  | $P_b$     | 28.60  |
| Meter volume (std),<br>$17.64 \left( \frac{V_m}{\alpha} \right) \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right)$ $17.64 \left( \frac{31.853}{1.012} \right) \left( \frac{(28.60) + \frac{0.813}{13.6}}{(90.) + 460} \right)$ | $V_m$ std | 28.948 |
| Volume of liquid collected (grams)  | $V_l_c$   | 39.2   |
| Volume of liquid at standard condition (scf)<br>$V_l_c \times 0.04707$  | $V_w$ std | 1.845  |
| Stack gas proportion of water vapor<br>$\frac{V_w \text{ std}}{V_w \text{ std} + V_m \text{ std}}, \quad \frac{(1.845)}{(1.845) + (28.948)}$  | $B_{wo}$  | 0.060  |
| Molecular weight, stack gas dry<br>$(1b/1b\text{-mole})$<br>$(\% CO_2 \times 0.44) + (\% O_2 \times 0.32) + (\% N_2 + \% CO \times 0.28)$<br>$(7.5 \times 0.44) + (8.8 \times 0.32) + (83.7 + \underline{\hspace{2cm}} \times 0.28)$      | $M_d$     | 29.552 |
| Molecular weight, stack gas wet<br>$(1b/1b\text{-mole})$<br>$M_d(1-B_{wo}) + 18(B_{wo}), \quad (29.552)(1-0.060) + 18(0.060)$   | $M_s$     | 28.86  |
| Absolute stack pressure (in. Hg)<br>$P_b + \frac{P_{stack} \text{ (in. H}_2\text{O)}}{13.6}, \quad (28.60) + \frac{(-0.1)}{13.6}$   | $P_s$     | 28.59  |

|  |  |                |
|--|--|----------------|
| Temperature stack gas, average ( $^{\circ}$ F)   | $T_s$  | 329            |
| Stack velocity (fps)<br>$85.49 (C_p) \sqrt{\frac{T_s \text{ avg} + 460}{P_s \text{ avg} M_s}}$<br>$85.49 (.79)(.248) \sqrt{\frac{(329) + 460}{(28.59)(28.86)}}$  | $V_s(\text{avg})$                                    | 16.38          |
| Total sample time (minutes)  | $\theta$   | 60             |
| Nozzle diameter, actual (inches)   | $N_d$  | 0.387          |
| Percent isokinetic (%)<br>$17.33 (T_s + 460)(V_w \text{ std} + V_m \text{ std})$<br>$\frac{\theta \quad V_s \quad P_s \quad N_d^2}{17.33 ((\text{___} + 460)((\text{___}) + (\text{___})) \quad (\text{___})(\text{___})(\text{___})(\text{___})^2)}$  | %I   | 100.057        |
| Area of stack ( $\text{ft}^2$ ) $\pi = 3.1416$<br>$\pi r^2 \div 144, \quad \pi (\text{___})^2 \div 144$  | $A_s$  | 2.405          |
| Stack gas volume at standard conditions (dscfm)<br>$60 (1 - B_{wo}) V_s \text{ avg } A_s \left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$<br>$60 (1 - \text{___})(\text{___})(\text{___}) \left( \frac{528}{\text{___} + 460} \right) \left( \frac{(\text{___})}{(29.92)} \right)$ | ACFM<br>$Q_s$  | 2,363<br>1,421 |
| Particulate matter concentration, dry (gr/dscf)<br>$15.432 \frac{M_p \text{ (grams)}}{V_m \text{ std}}, \quad 15.432 \frac{(20.682)}{(28.948)}$  | $C_s \text{ (std)}$                                  | 0.03029        |
| Emission rate of particulate matter (lb/hr)<br><del><math>0.00857 (Q_s) C_s \text{ (std)}</math></del> , $0.00857 (\text{___})(\text{___})$  | $SO_2 = \frac{546.9}{28.948} = 32.7 \text{ mg/decf}$ |                |

## ISOKINETIC PERFORMANCE WORKSHEET &amp; PARTICULATE CALCULATIONS

 Plant Rock of Ages

 Performed by Dick Ros

 Date 2-2-83

 Sample Location Saw House

 Test No./Type 3 - m5/8

|  |                       |        |
|--|-----------------------|--------|
| Barometric Pressure (in. Hg)   | $P_b$                 | 28.60  |
| Meter volume (std),<br>$17.64 \left( \frac{V_m}{\alpha} \right) \left( P_b + \frac{\Delta H}{13.6} \right)$ $17.64 \left( \frac{(36.388)}{(1.012)} \right) \left( \frac{(28.60)}{(86.4)} + \frac{(.976)}{13.6} \right)$                              | $V_m$ std             | 33.176 |
| Volume of liquid collected (grams)   | $V_l_c$               | 32.7   |
| Volume of liquid at standard condition (scf)<br>$V_l_c \times 0.04707$   | $V_w$ std             | 1.539  |
| Stack gas proportion of water vapor<br>$\frac{V_w \text{ std}}{V_w \text{ std} + V_m \text{ std}}, \quad \frac{(.539)}{(.539) + (33.176)}$   | $B_{wo}$              | 0.044  |
| Molecular weight, stack gas dry<br>$(\text{lb/lb-mole})$<br>$(\% \text{CO}_2 \times 0.44) + (\% \text{O}_2 \times 0.32) + (\% \text{N}_2 + \% \text{CO} \times 0.28)$<br>$(7.5 \times 0.44) + (8.8 \times 0.32) + (83.7 + \text{_____} \times 0.28)$ | $M_d$<br>From MPR Aug | 27.552 |
| Molecular weight, stack gas wet<br>$(\text{lb/lb-mole})$<br>$M_d(1-B_{wo}) + 18(B_{wo}), \quad (27.552)(1-0.044) + 18(0.044)$  | $M_s$                 | 27.04  |
| Absolute stack pressure (in. Hg)<br>$P_b + \frac{P_{stack} \text{ (in. H}_2\text{O)}}{13.6}, \quad (28.60) + \frac{(-0.1)}{13.6}$  | $P_s$                 | 28.59  |

|  |  |  |
|--|--|--|
| Temperature stack gas, average ( $^{\circ}$ F)   | $T_s$  | 276.7  |
| Stack velocity (fps)<br>85.49 ( $C_p$ ) $(\sqrt{4P_s \text{ avg}})$  | $\sqrt{\frac{T_s \text{ avg} + 460}{P_s \text{ avg} M_s}}$ | $V_s(\text{avg})$<br>16.73                     |
| Total sample time (minutes)  | $\theta$   | 60   |
| Nozzle diameter, actual (inches)   | $N_d$  | 0.387  |
| Percent isokinetic (%)<br>17.33 $(T_s + 460)(V_w \text{ std} + V_m \text{ std})$   | %I   | 103.100  |
| $\frac{\theta \ V_s \ P_s \ N_d^2}{17.33 (\underline{\quad} + 460)((\underline{\quad}) + (\underline{\quad})) (\underline{\quad})(\underline{\quad})(\underline{\quad})(\underline{\quad})^2}$ |  |  |
| Area of stack ( $\text{ft}^2$ ) $\pi = 3.1416$<br>$\pi r^2 \div 144, \pi (\underline{10.5})^2 \div 144$  | $A_s$  | 2.405  |
| Stack gas volume at standard conditions (dscfm)<br>60 $(1 - B_{wo}) V_s \text{ avg } A_s \left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$                    | ACFM   | 2,414  |
| $60 (1 - \underline{\quad})(\underline{\quad})(\underline{\quad}) \left( \frac{528}{\underline{\quad} + 460} \right) \left( \frac{(\underline{\quad})}{(29.92)} \right)$                       | $Q_s$  | 1,580  |
| Particulate matter concentration, dry (gr/dscf)<br>15.432 $\frac{M_p \text{ (grams)}}{V_m \text{ std}}, 15.432 \frac{(0.02117)}{(33.126)}$   | $C_s \text{ (std)}$  | 0.00985  |
| Emission rate of particulate matter (lb/hr)<br><del>0.00857 (<math>Q_s</math>) <math>C_s</math>, 0.00857 (<math>\underline{\quad}</math>) (<math>\underline{\quad}</math>)</del>               | $\frac{SC_3}{F_p}$   | $\frac{450.8}{33.126} = 14.8 \text{ lbs/dscf}$ |

#### 5.4 HC1 EMISSIONS FROM HC1 TRAIN SAMPLES



Energy & Environmental Division

Acurex

October 6, 1983

Attention: Larry Waterland

Acurex ID#: 8309-035

Customer PO#: 307736.62

Subject: Vermont Chloride Determinations; received 7/7/83

The above samples were analyzed for chloride by argentometric titration.

| <u>Sample #</u>   | <u>Volume, mL</u> | <u>Total Chloride, mg/L</u> | <u>Total Chloride, mg</u> |
|-------------------|-------------------|-----------------------------|---------------------------|
| Test 3<br>819474  | 405               | 310                         | 130                       |
| Blank 2<br>819447 | 143               | 13                          | 2                         |

Prepared by: Stephen Guinnane Approved by: Greg Nicoll  
Stephen Guinnane  
Analyst  
Operations Manager

SG/GN/ats

## ISOKINETIC PERFORMANCE WORKSHEET &amp; PARTICULATE CALCULATIONS

Plant \_\_\_\_\_ Performed by \_\_\_\_\_

Date \_\_\_\_\_

Sample Location \_\_\_\_\_

Test No./Type \_\_\_\_\_

|   |                   |        |
|---|-------------------|--------|
| Barometric Pressure (in. Hg)  | $P_b$             |        |
| Meter volume (std),<br>$17.64 \left( \frac{V_m}{\alpha} \right) \left( \frac{P_b + \Delta H}{T_m + 460} \right)$ $17.64 \left( \frac{(\text{_____})}{(\text{_____})} \right) \left( \frac{(\text{_____}) + (\text{_____})}{(\text{_____}) + 460} \right)$             | $V_m \text{ std}$ | 17.100 |
| Volume of liquid collected (grams)  | $V_l_c$           |        |
| Volume of liquid at standard condition (scf)<br>$V_l_c \times 0.04707$  | $V_w \text{ std}$ | 0.2532 |
| Stack gas proportion of water vapor<br>$\frac{V_w \text{ std}}{V_w \text{ std} + V_m \text{ std}}, \quad \frac{(\text{_____})}{(\text{_____}) + (\text{_____})}$  | $B_{wo}$          | 0.500  |
| Molecular weight, stack gas dry<br>(lb/lb-mole)<br>$(\% \text{CO}_2 \times 0.44) + (\% \text{O}_2 \times 0.32) + (\% \text{N}_2 + \% \text{CO} \times 0.28)$<br>$(\text{_____} \times 0.44) + (\text{_____} \times 0.32) + (\text{_____} + \text{_____} \times 0.28)$ | $M_d$             | 27.62  |
| Molecular weight, stack gas wet<br>(lb/lb-mole)<br>$M_d(1-B_{wo}) + 18(B_{wo}), \quad (\text{_____})(1-\underline{\text{_____}}) + 18(\underline{\text{_____}})$  | $M_s$             | 27.23  |
| Absolute stack pressure (in. Hg)<br>$P_b + \frac{P_{stack} \text{ (in. H}_2\text{O)}}{13.6}, \quad (\text{_____}) + \frac{(\text{_____})}{13.6}$  | $P_s$             | 27.25  |

|  |                   |            |
|--|-------------------|------------|
| Temperature stack gas, average (°F)  | $T_s$             |            |
| Stack velocity (fps)<br>85.49 ( $C_p$ ) ( $\sqrt{\Delta P_s}$ avg) $\sqrt{\frac{T_s \text{ avg} + 460}{P_s M_s}}$  | $V_s(\text{avg})$ |            |
| 85.49 ( $\underline{\quad}$ ) ( $\sqrt{\underline{\quad}}$ ) $\sqrt{\frac{(\underline{\quad}) + 460}{(\underline{\quad})(\underline{\quad})}}$   |                   |            |
| Total sample time (minutes)  | $\theta$          |            |
| Nozzle diameter, actual (inches)   | $N_d$             |            |
| Percent isokinetic (%)<br>17.33 ( $T_s + 460$ ) ( $V_w$ std + $V_m$ std)   | %I                |            |
| $\frac{\theta V_s P_s N_d^2}{17.33 (\underline{\quad} + 460)((\underline{\quad}) + (\underline{\quad}))}$<br>$\frac{(\underline{\quad})(\underline{\quad})(\underline{\quad})(\underline{\quad})^2}{(\underline{\quad})(\underline{\quad})(\underline{\quad})(\underline{\quad})^2}$ |                   |            |
| Area of stack (ft <sup>2</sup> ) $\pi = 3.1416$<br>$\pi r^2 \div 144$ , $\pi (\underline{\quad})^2 \div 144$   | $A_s$             |            |
| Stack gas volume at standard conditions (dscfm)<br>60 (1 - $B_{w0}$ ) $V_s$ avg $A_s \left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$  | $Q_s$             |            |
| $60 (1 - \underline{\quad})(\underline{\quad})(\underline{\quad}) \left( \frac{528}{\underline{\quad} + 460} \right) \left( \frac{(\underline{\quad})}{(29.92)} \right)$   |                   |            |
| Particulate matter concentration, dry (gr/dscf)<br>15.432 $\frac{M_p \text{ (grams)}}{V_m \text{ std}}$ , 15.432 $\frac{(\underline{\quad})}{(\underline{\quad})}$   | $C_s(\text{std})$ | - $\times$ |
| Emission rate of particulate matter (lb/hr)<br>0.00857 ( $Q_s$ ) $C_s(\text{std})$ , 0.00857 $(\underline{\quad})(\underline{\quad})$  | $E_p$             |            |

\* Impinger solution destroyed  
in transit

7602/5/81/Rev 1

## ISOKINETIC PERFORMANCE WORKSHEET &amp; PARTICULATE CALCULATIONS

Plant \_\_\_\_\_

Performed by \_\_\_\_\_

Date \_\_\_\_\_

Sample Location \_\_\_\_\_

Test No./Type \_\_\_\_\_

|  |                   |        |
|--|-------------------|--------|
| Barometric Pressure (in. Hg)   | $P_b$             |        |
| Meter volume (std),<br>$17.64 \left( \frac{V_m}{\alpha} \right) \left( \frac{P_b + \frac{\Delta H}{13.6}}{T_m + 460} \right)$<br>$17.64 \left( \frac{(\underline{\quad})}{(\underline{\quad})} \right) \left( \frac{(\underline{\quad}) + (\underline{\quad})}{(\underline{\quad}) + 460} \right)$ | $V_m \text{ std}$ |        |
| Volume of liquid collected (grams)   | $V_{l_c}$         |        |
| Volume of liquid at standard condition (scf)<br>$V_{l_c} \times 0.04707$   | $V_w \text{ std}$ |        |
| Stack gas proportion of water vapor<br>$\frac{V_w \text{ std}}{V_w \text{ std} + V_m \text{ std}}, \frac{(\underline{\quad})}{(\underline{\quad}) + (\underline{\quad})}$  | $B_{wo}$          |        |
| Molecular weight, stack gas dry<br>(lb/lb-mole)<br>$(\% CO_2 \times 0.44) + (\% O_2 \times 0.32) + (\% N_2 + \% CO \times 0.28)$<br>$(\underline{\quad} \times 0.44) + (\underline{\quad} \times 0.32) + (\underline{\quad} + \underline{\quad} \times 0.28)$                                      | $M_d$             | 27.552 |
| Molecular weight, stack gas wet<br>(lb/lb-mole)<br>$M_d(1-B_{wo}) + 18(B_{wo}), \underline{27.552}(1-\underline{0.552}) + 18(\underline{0.552})$   | $M_s$             | 28.157 |
| Absolute stack pressure (in. Hg)<br>$P_b + \frac{P_{stack} \text{ (in. H}_2\text{O)}}{13.6}, (\underline{\quad}) + \frac{(\underline{\quad})}{13.6}$   | $P_s$             | 28.57  |

|   |                   |       |
|---|-------------------|-------|
| Temperature stack gas, average (°F)   | $T_s$             |       |
| Stack velocity (fps)<br>85.49 ( $C_p$ ) ( $\sqrt{\Delta P_s}$ avg)<br>$\sqrt{\frac{T_s \text{ avg} + 460}{P_s M_s}}$<br>85.49 (____) ( $\sqrt{\text{_____}}$ ) $\sqrt{\frac{(____) + 460}{(____)(____)}}$ | $v_s(\text{avg})$ |       |
| Total sample time (minutes)   | $\theta$          |       |
| Nozzle diameter, actual (inches)  | $N_d$             |       |
| Percent isokinetic (%)<br>17.33 ( $T_s$ + 460)( $V_w$ std + $V_m$ std)  | %I                | 72.75 |
| $\theta$ $v_s$ $P_s$ $N_d^2$<br>17.33 (____ + 460)((____) + (____))<br>(____)(____)(____)(____ $^2$ )   |                   |       |
| Area of stack (ft $^2$ ) $\pi = 3.1416$<br>$\pi r^2 \div 144$ , $\pi (\text{____})^2 \div 144$  | $A_s$             | 2.455 |
| Stack gas volume at standard conditions (dscfm)<br>60 (1 - $B_{wo}$ ) $V_s$ avg $A_s$ $\left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$                                 | $A_{std}$         | 2.325 |
| 60 (1 - ____)(____)(____) $\left( \frac{528}{____ + 460} \right) \left( \frac{(\text{____})}{(29.92)} \right)$  | $Q_s$             | 1.417 |
| Particulate matter concentration, dry (gr/dscf)<br>15.432 $\frac{M_p \text{ (grams)}}{V_m \text{ std}}$ , 15.432 $\frac{(\text{____})}{(\text{____})}$  | $C_s$ (std)       | -     |
| Emission rate of particulate matter (lb/hr)<br>0.00857 ( $Q_s$ ) $C_s$ (std), 0.00857 (____)(____)  | $E_p$             |       |

\* Impinger solution destroyed  
in transit

7602/5/81/Rev 1

## ISOKINETIC PERFORMANCE WORKSHEET &amp; PARTICULATE CALCULATIONS

Plant \_\_\_\_\_ Performed by \_\_\_\_\_

Date \_\_\_\_\_

Sample Location \_\_\_\_\_

Test No./Type \_\_\_\_\_

|   |                   |                    |
|---|-------------------|--------------------|
| Barometric Pressure (in. Hg)  | $P_b$             |                    |
| Meter volume (std),<br>$17.64 \left( \frac{V_m}{\alpha} \right) \left( P_b + \frac{\Delta H}{13.6} \right)$ $17.64 \left( \frac{(\text{_____})}{(\text{_____})} \right) \left( \frac{(\text{_____})}{(\text{_____})} + \frac{(\text{_____})}{13.6} \right)$           | $V_m \text{ std}$ | 12.5 $\text{ft}^3$ |
| Volume of liquid collected (grams)  | $V_l_c$           |                    |
| Volume of liquid at standard condition (scf)<br>$V_l_c \times 0.04707$  | $V_w \text{ std}$ | 1.0 $\text{ft}^3$  |
| Stack gas proportion of water vapor<br>$\frac{V_w \text{ std}}{V_w \text{ std} + V_m \text{ std}}, \quad \frac{(\text{_____})}{(\text{_____}) + (\text{_____})}$  | $B_{wo}$          | 0.50               |
| Molecular weight, stack gas dry<br>(lb/lb-mole)<br>$(\% \text{CO}_2 \times 0.44) + (\% \text{O}_2 \times 0.32) + (\% \text{N}_2 + \% \text{CO} \times 0.28)$<br>$(\text{_____} \times 0.44) + (\text{_____} \times 0.32) + (\text{_____} + \text{_____} \times 0.28)$ | $M_d$             | 28.02              |
| Molecular weight, stack gas wet<br>(lb/lb-mole)<br>$M_d(1-B_{wo}) + 18(B_{wo}), \quad (\text{_____})(1-\text{_____}) + 18(\text{_____})$  | $M_s$             | 28.45              |
| Absolute stack pressure (in. Hg)<br>$P_b + \frac{P_{stack} \text{ (in. H}_2\text{O)}}{13.6}, \quad (\text{_____}) + \frac{(\text{_____})}{13.6}$  | $P_s$             | 28.57              |

|   |                     |        |
|---|---------------------|--------|
| Temperature stack gas, average (°F)   | $T_s$               |        |
| Stack velocity (fps)<br>85.49 ( $C_p$ ) ( $\sqrt{\Delta P_s}$ avg)  | $v_s(\text{avg})$   | 15.75  |
| $85.49 \left( \frac{T_s \text{ avg} + 460}{P_s \text{ avg} M_s} \right)$  |                     |        |
| Total sample time (minutes)   | $\theta$            |        |
| Nozzle diameter, actual (inches)  | $N_d$               |        |
| Percent isokinetic (%)<br>17.33 $(T_s + 460)(V_w \text{ std} + V_m \text{ std})$  | %I                  | 10.14  |
| $\frac{\theta \ v_s \ p_s \ N_d^2}{17.33 \left( \frac{(T_s + 460)(V_w \text{ std} + V_m \text{ std})}{(A_s)(\theta)(N_d^2)} \right)}$   |                     |        |
| Area of stack (ft <sup>2</sup> ) $\pi = 3.1416$<br>$\pi r^2 \div 144, \pi (\frac{N_d}{12})^2 \div 144$  | $A_s$               | 2.1405 |
| Stack gas volume at standard conditions (dscfm)<br>60 $(1 - B_{w0})V_s \text{ avg} A_s \left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$         | $A_s \text{ dscfm}$ | 2.1405 |
| $60 (1 - B_{w0})V_s \text{ avg} A_s \left( \frac{528}{T_s \text{ avg} + 460} \right) \left( \frac{P_s}{29.92} \right)$  | $Q_s$               | 1.474  |
| <del>HCR</del><br>Particulate matter concentration, dry (mg/dscf)<br>15.432 $\frac{M_p \text{ (grams)}}{V_m \text{ std}}$ , <del>15.432</del> <del>(1.10)</del> <del>(1.10)</del> | $C_s \text{ (std)}$ | 9.55   |
| Emission rate of particulate matter (lb/hr)<br>0.00857 $(Q_s) C_s \text{ (std)}$ , 0.00857 $(Q_s) C_s \text{ (std)}$  | $E_p$               |        |

## 5.5 TRACE ELEMENT AND LEACHABLE ANION ANALYSES

In the following, the bottom ash test 3 sample is a blind duplicate of the bottom ash test 2 sample and the cyclone ash test 3 sample is a blind audit sample consisting of NBS 1633a flyash.

# **COMMERCIAL TESTING & ENGINEERING CO.**



Reply to

Instrument Analysis Division  
490 Orchard Street  
Golden, CO 80401

Phone: 303-278-9521

January 9, 1983

Mr. Christopher Mann  
Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountian View, CA 94042

RE: IAD #97-N182-116-28  
Subcontract #SW59159A  
Release #11

## Analytical Report

Twenty-eight samples were received for analysis on November 30, 1983. These samples were assigned our IAD identification #97-N182-116-28.

Trace element determinations using Spark Source Mass Spectrometry per EPA level 1 protocol will be reported in separate reports upon completion of analysis.

Arsenic and Antimony were determined on four of the samples using hydride generation atomic absorption spectrophotometry. Mercury was determined on all twenty-eight samples using flameless cold vapor atomic absorption spectrophotometry.

The results of these determinations are presented in Table No. I and No. II and are reported in parts per million (ppm) by weight on an "as received" basis.



Table No. I  
(ppm by Weight)

| <u>Sample ID</u>                        | <u>Arsenic (As)</u> | <u>Antimony (Sb)</u> |
|---|---------------------|----------------------|
| 819454 RA Imp 2 and 3, Test 1           | <u>&lt;0.001</u>    | 0.003                |
| 819455 RA Imp 2 and 3,<br>Blank, Test 1 | <u>&lt;0.001</u>    | <u>&lt;0.001</u>     |
| 819467 RA Imp 2 and 3, Test 2           | 0.001               | 0.002                |
| 819469 RA Imp 2 and 3,<br>Blank, Test 2 | <u>&lt;0.001</u>    | <u>&lt;0.001</u>     |

Table No. II  
(ppm by Weight)

| <u>Sample ID</u>                       | <u>Mercury (Hg)</u> |
|--|---------------------|
| 819463 RA Filter + 1 $\mu$ , Test 1    | 0.09                |
| 819475 RA Filter, Test 2               | 0.11                |
| 819458 RA Filter Blank                 | 0.03                |
| 819456 RA 10 $\mu$ + 3 $\mu$ , Test 1  | 5.0                 |
| 819492 RA 10 $\mu$ + 3 $\mu$ , Test 2  | 6.0                 |
| 819459 RA XAD-2, Test 1                | 0.23                |
| 819465 RA XAD-2, Test 2                | 0.24                |
| 819461 RA XAD-2, Blank                 | 0.03                |
| 819452 RA Imp 1, Test 1                | 0.002               |
| 819466 RA Imp 1, Test 2                | 0.010               |
| 819448 RA Imp 1, Blank                 | <u>&lt;0.001</u>    |
| 819449 RA Coal, Test 1                 | 0.09                |
| 819485 RA PET, Test 2                  | 0.35                |
| 819478 RA Coal/PET, Test 2             | 0.20                |
| 819488 RA Bottom Ash, Test 1           | <u>&lt;0.01</u>     |
| 819495 RA Bottom Ash Leachate, Test 1  | <u>0.002</u>        |
| 819498 RA Bottom Ash, Test 2           | <u>&lt;0.01</u>     |
| 819496 RA Bottom Ash Leachate, Test 2  | <u>&lt;0.001</u>    |
| 819493 RA Bottom Ash, Test 3           | 0.02                |
| 819476 RA Cyclone Ash, Test 1          | 0.78                |
| 819482 RA Cyclone Ash Leachate, Test 1 | <u>&lt;0.001</u>    |
| 819504 RA Cyclone Ash, Test 2          | 1.15                |
| 819486 RA Cyclone Ash Leachate, Test 2 | <u>&lt;0.001</u>    |
| 819464 RA Cyclone Ash, Test 3          | 0.11                |
| 819454 RA Imp 2 and 3, Test 1          | 0.008               |
| 819455 RA Imp 2 and 3 Blank, Test 1    | <u>&lt;0.001</u>    |
| 819467 RA Imp 2 and 3, Test 2          | 0.011               |
| 819469 RA Imp 2 and 3 Blank, Test 2    | <u>&lt;0.001</u>    |

Analytical Report  
#97-N182-116-28  
Page 3

If you have any questions concerning these results, please call.

---

Harold A. Connell  
Assistant Laboratory Manager

*Robert L. Taylor* 9 Jan '84

Robert L. Taylor, Ph.D., Manager  
Instrumental Analysis Division

HAC/gh

5-39

COMMERCIAL TESTING & ENGINEERING CO.



# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

Reply to

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Mr. Christopher Mann  
Acurex Corporation  
555 Clyde Avenue  
Mountain View, CA 94039

Date: January 4, 1984

P. O. No.: Subcontract #SW59159A  
Release #11

Analyst: G. Meagher

Sample No.: 819449 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28

RA coal, test 1 CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT        | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|----------------|-------|------------|-------|------------|-------|
| Uranium    | 2     | Terbium        | 0.2   | Ruthenium  |       | Vanadium   | 40    |
| Thorium    | 5     | Gadolinium     | 0.7   | Molybdenum | 27    | Titanium   | MC    |
| Bismuth    |       | Europium       | 0.3   | Niobium    | *12   | Scandium   | 35    |
| Lead       | 3     | Samarium       | 1     | Zirconium  | 31    | Calcium    | MC    |
| Thallium   |       | Neodymium      | 7     | Yttrium    | 10    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium   | 3     | Strontium  | 110   | Chlorine   | 270   |
| Gold       |       | Cerium         | 18    | Rubidium   | 5     | Sulfur     | 590   |
| Platinum   |       | Lanthanum      | 25    | Bromine    | 21    | Phosphorus | 100   |
| Iridium    |       | Barium         | 100   | Selenium   | *130  | Silicon    | MC    |
| Osmium     |       | Cesium         | 0.5   | Arsenic    | 11    | Aluminum   | MC    |
| Rhenium    |       | Iodine         | 1     | Germanium  | 1     | Magnesium  | MC    |
| Tungsten   |       | Tellurium      |       | Gallium    | 16    | Sodium     | MC    |
| Tantalum   |       | Antimony       | <1    | Zinc       | 53    | Fluorine   | ≈830  |
| Hafnium    |       | Tin            | 0.5   | Copper     | 14    | Oxygen     | NR    |
| Lutetium   |       | Indium         | STD   | Nickel     | 2     | Nitrogen   | NR    |
| Ytterbium  |       | Cadmium        | 1     | Cobalt     | 8     | Carbon     | NR    |
| Thulium    |       | Silver         |       | Iron       | MC    | Boron      | 30    |
| Erbium     |       | Palladium      |       | Manganese  | 8     | Beryllium  | 9     |
| Holmium    |       | Rhodium        |       | Chromium   | 120   | Lithium    | 74    |
| Dysprosium |       | *Heterogeneous |       |            |       | Hydrogen   |       |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.2 ppm

MC — Major Component >1000 ppm

INT — Interference

Approved:

5-40

*Robert L. Dayton*  
3 Feb-84

# COMMERCIAL TESTING & ENGINEERING CO.

Reply to

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Mr. Christopher Mann  
Aurex Corporation  
555 Clyde Avenue  
Mountain View, CA 94039

Date: January 4, 1984

Subcontract #SW59159A

Analyst: G. Meagher

P. O. No.: Release #11

Sample No.: 819488  
RA bottom ash,  
test 1

IAD No.: 97-N182-116-28

## CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 9     | Terbium      | 0.8   | Ruthenium  |       | Vanadium   | 44    |
| Thorium    | 14    | Gadolinium   | 3     | Molybdenum | 6     | Titanium   | MC    |
| Bismuth    |       | Europium     | 2     | Niobium    | 9     | Scandium   | 30    |
| Lead       | 9     | Samarium     | 7     | Zirconium  | 34    | Calcium    | MC    |
| Thallium   | 1     | Neodymium    | 14    | Yttrium    | 11    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 7     | Strontium  | 210   | Chlorine   | 98    |
| Gold       |       | Cerium       | 22    | Rubidium   | 8     | Sulfur     | 320   |
| Platinum   |       | Lanthanum    | 30    | Bromine    | 4     | Phosphorus | 740   |
| Iridium    |       | Barium       | 350   | Selenium   | 13    | Silicon    | MC    |
| Osmium     |       | Cesium       | 2     | Arsenic    | 4     | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 2     | Germanium  | 1     | Magnesium  | MC    |
| Tungsten   | 1     | Tellurium    | <0.2  | Gallium    | 10    | Sodium     | MC    |
| Tantalum   | 0.9   | Antimony     | 4     | Zinc       | 11    | Fluorine   | MC    |
| Hafnium    | 3     | Tin          | 0.8   | Copper     | 18    | Oxygen     | NR    |
| Lutetium   | 0.3   | Indium       | STD   | Nickel     | 160   | Nitrogen   | NR    |
| Ytterbium  | 1     | Cadmium      | 0.4   | Cobalt     | 22    | Carbon     | NR    |
| Thulium    | 0.2   | Silver       | 0.5   | Iron       | MC    | Boron      | 31    |
| Erbium     | 2     | Palladium    |       | Manganese  | 13    | Beryllium  | 22    |
| Holmium    | 2     | Rhodium      |       | Chromium   | 50    | Lithium    | 120   |
| Dysprosium | 3     |              |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.1 ppm

MC — Major Component >1000 ppm

INT — Interference

5- 41 Approved:

*Robert L. Daykin*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Mr. Christopher Mann  
Acurex Corporation  
555 Clyde Avenue  
Mountain View, CA 94039

Date: January 4, 1984

Subcontract #SW59159A  
P. O. No.: Release #11

Analyst: G. Meagher

Sample No.: 819495      SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS      IAD No.: 97-N182-116-28  
RA bottom ash  
Leachate, test 1      CONCENTRATION IN  $\mu\text{g/mL}$

| ELEMENT    | CONC.        | ELEMENT      | CONC.        | ELEMENT    | CONC.        | ELEMENT    | CONC.        |
|------------|--------------|--------------|--------------|------------|--------------|------------|--------------|
| Uranium    |              | Terbium      |              | Ruthenium  |              | Vanadium   | 0.02         |
| Thorium    |              | Gadolinium   |              | Molybdenum | 0.1          | Titanium   | 0.3          |
| Bismuth    |              | Europium     |              | Niobium    | $\leq 0.001$ | Scandium   | $\leq 0.001$ |
| Lead       | $\leq 0.004$ | Samarium     |              | Zirconium  | 0.003        | Calcium    | MC           |
| Thallium   |              | Neodymium    |              | Yttrium    | 0.001        | Potassium  | MC           |
| Mercury    | NR           | Praseodymium |              | Strontium  | 0.6          | Chlorine   | 0.5          |
| Gold       |              | Cerium       | 0.001        | Rubidium   | 0.008        | Sulfur     | MC           |
| Platinum   |              | Lanthanum    |              | Bromine    | 0.03         | Phosphorus | 0.1          |
| Iridium    |              | Barium       | 0.06         | Selenium   | 0.1          | Silicon    | 4            |
| Osmium     |              | Cesium       |              | Arsenic    | 0.03         | Aluminum   | 0.5          |
| Rhenium    |              | Iodine       | 0.002        | Germanium  | 0.002        | Magnesium  | 4            |
| Tungsten   |              | Tellurium    |              | Gallium    | 0.01         | Sodium     | MC           |
| Tantalum   |              | Antimony     | $\leq 0.004$ | Zinc       | 0.03         | Fluorine   | $\approx 4$  |
| Hafnium    |              | Tin          |              | Copper     | 0.01         | Oxygen     | NR           |
| Lutetium   |              | Indium       | STD          | Nickel     | 0.01         | Nitrogen   | NR           |
| Ytterbium  |              | Cadmium      |              | Cobalt     | $\leq 0.001$ | Carbon     | NR           |
| Thulium    |              | Silver       | $\leq 0.002$ | Iron       | 0.06         | Boron      | 0.2          |
| Erbium     |              | Palladium    |              | Manganese  | 0.002        | Beryllium  |              |
| Holmium    |              | Rhodium      |              | Chromium   | 0.02         | Lithium    | 3            |
| Dysprosium |              |              |              |            |              | Hydrogen   | NR           |

STD — Internal Standard

NR — Not Reported

All elements not detected  $< 0.001 \mu\text{g/mL}$

MC — Major Component  $> 10 \mu\text{g/mL}$

INT — Interference

Approved:  
5-42

*Robert L. Taylor  
3 Feb 84*

# COMMERCIAL TESTING & ENGINEERING CO.

Reply to

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7535  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW 59159A Release Number 11 Project 7601

Sample No.: 819476 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA cyclone ash,  
test 1 CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 2     | Terbium      | 0.2   | Ruthenium  |       | Vanadium   | 85    |
| Thorium    | 2     | Gadolinium   | 0.9   | Molybdenum | 8     | Titanium   | MC    |
| Bismuth    | 0.4   | Europium     | 0.4   | Niobium    | 4     | Scandium   | 26    |
| Lead       | 14    | Samarium     | 3     | Zirconium  | 8     | Calcium    | MC    |
| Thallium   | 2     | Neodymium    | 3     | Yttrium    | 5     | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 1     | Strontium  | 90    | Chlorine   | 250   |
| Gold       |       | Cerium       | 4     | Rubidium   | 2     | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 6     | Bromine    | 49    | Phosphorus | MC    |
| Iridium    |       | Barium       | 130   | Selenium   | 170   | Silicon    | MC    |
| Osmium     |       | Cesium       | 0.4   | Arsenic    | 52    | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 3     | Germanium  | 4     | Magnesium  | MC    |
| Tungsten   | 0.5   | Tellurium    | 0.4   | Gallium    | 19    | Sodium     | MC    |
| Tantalum   | 0.4   | Antimony     | 6     | Zinc       | 37    | Fluorine   | =260  |
| Hafnium    | 0.3   | Tin          | 1     | Copper     | 34    | Oxygen     | NR    |
| Lutetium   | <0.1  | Indium       | STD   | Nickel     | 79    | Nitrogen   | NR    |
| Ytterbium  | 0.5   | Cadmium      | 0.4   | Cobalt     | 6     | Carbon     | NR    |
| Thulium    | 0.2   | Silver       | 0.5   | Iron       | MC    | Boron      | 110   |
| Erbium     | 0.5   | Palladium    |       | Manganese  | 11    | Beryllium  | 7     |
| Holmium    | 0.7   | Rhodium      |       | Chromium   | 51    | Lithium    | 79    |
| Dysprosium | 1     |              |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.1 ppm

MC — Major Component > 1000 ppm

INT — Interference

Approved:  
5-43

3 Feb 84

*Robert L. Taylor*

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

Reply to

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

P. O. No.: Subcontract #SW59159A  
Release #11 Project #7601

Analyst: G. Meagher

Sample No.: 819482 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA cyclone ash, leachate CONCENTRATION IN  $\mu\text{g}/\text{ml}$

Test 1

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 0.69  | Terbium      | 0.06  | Ruthenium  |       | Vanadium   | 7.4   |
| Thorium    | 0.31  | Gadolinium   | 0.23  | Molybdenum | 0.22  | Titanium   | MC    |
| Bismuth    | 0.005 | Europium     | 0.09  | Niobium    | 0.19  | Scandium   | 0.85  |
| Lead       | 0.27  | Samarium     | 0.76  | Zirconium  | 0.95  | Calcium    | MC    |
| Thallium   | 0.21  | Neodymium    | 0.72  | Yttrium    | 1.2   | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 0.34  | Strontium  | MC    | Chlorine   | 6.6   |
| Gold       |       | Cerium       | 0.85  | Rubidium   | 0.63  | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 1.2   | Bromine    | 0.51  | Phosphorus | MC    |
| Iridium    |       | Barium       | 2.1   | Selenium   | 0.80  | Silicon    | MC    |
| Osmium     |       | Cesium       | 0.05  | Arsenic    | 4.1   | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 0.008 | Germanium  | 0.22  | Magnesium  | MC    |
| Tungsten   | 0.03  | Tellurium    | 0.01  | Gallium    | 6.5   | Sodium     | MC    |
| Tantalum   | 0.03  | Antimony     | 0.15  | Zinc       | MC    | Fluorine   | MC    |
| Hafnium    | 0.03  | Tin          | 0.02  | Copper     | MC    | Oxygen     | NR    |
| Lutetium   | 0.03  | Indium       | STD   | Nickel     | 4.0   | Nitrogen   | NR    |
| Ytterbium  | 0.27  | Cadmium      | 0.17  | Cobalt     | 7.4   | Carbon     | NR    |
| Thulium    | 0.04  | Silver       | 0.008 | Iron       | MC    | Boron      | 1.8   |
| Erbium     | 0.30  | Palladium    |       | Manganese  | MC    | Beryllium  | 0.32  |
| Holmium    | 0.40  | Rhodium      |       | Chromium   | 3.7   | Lithium    | >4.1  |
| Dysprosium | 0.63  |              |       |            |       | Hydrogen   | NR    |

STD - Internal Standard

NR - Not Reported

All elements not detected < 0.001  $\mu\text{g}/\text{ml}$

MC - Major Component >10  $\mu\text{g}/\text{ml}$

INT - Interference

Approved:  
5-44

*Robert L. Daykin*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Mr. Christopher Mann  
Acurex Corporation  
555 Clyde Avenue  
Mountain View, CA 94039

Date: January 4, 1984

Analyst: G. Meagher

P. O. No.: Subcontract #SW59159A

Release #11

Sample No.: 819456 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28

RA 10 $\mu$  + 3 $\mu$ , test 1 CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 9     | Terbium      | 2     | Ruthenium  |       | Vanadium   | 940   |
| Thorium    | 20    | Gadolinium   | 6     | Molybdenum | 84    | Titanium   | MC    |
| Bismuth    | 6     | Europium     | 3     | Niobium    | 48    | Scandium   | 73    |
| Lead       | 460   | Samarium     | 17    | Zirconium  | 240   | Calcium    | MC    |
| Thallium   | 40    | Neodymium    | 28    | Yttrium    | 82    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 24    | Strontium  | MC    | Chlorine   | 850   |
| Gold       |       | Cerium       | 150   | Rubidium   | 72    | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 87    | Bromine    | 220   | Phosphorus | MC    |
| Iridium    |       | Barium       | MC    | Selenium   | MC    | Silicon    | MC    |
| Osmium     |       | Cesium       | 11    | Arsenic    | MC    | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 29    | Germanium  | 56    | Magnesium  | MC    |
| Tungsten   | 8     | Tellurium    | 3     | Gallium    | 830   | Sodium     | MC    |
| Tantalum   | 2     | Antimony     | 150   | Zinc       | MC    | Fluorine   | =880  |
| Hafnium    | 2     | Tin          | 43    | Copper     | 722   | Oxygen     | NR    |
| Lutetium   | 0.4   | Indium       | STD   | Nickel     | 830   | Nitrogen   | NR    |
| Ytterbium  | 3     | Cadmium      | 14    | Cobalt     | 64    | Carbon     | NR    |
| Thulium    | 0.8   | Silver       | 35    | Iron       | MC    | Boron      | MC    |
| Erbium     | 4     | Palladium    |       | Manganese  | MC    | Beryllium  | 31    |
| Holmium    | 6     | Rhodium      |       | Chromium   | MC    | Lithium    | >530  |
| Dysprosium | 9     |              |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.2 ppm

MC — Major Component >1000 ppm

INT — Interference

Approved:  
5-45

*Robert T. Taylor*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW59159A Release 11 Project 7601

Sample No.: 819463 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA filter + 1 $\mu$ , test 1 CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 62    | Terbium      | 1     | Ruthenium  |       | Vanadium   | 66    |
| Thorium    | 25    | Gadolinium   | 4     | Molybdenum | 65    | Titanium   | MC    |
| Bismuth    | 20    | Europium     | 3     | Niobium    | 14    | Scandium   | 10    |
| Lead       | 600   | Samarium     | 12    | Zirconium  | 68    | Calcium    | MC    |
| Thallium   | 31    | Neodymium    | 32    | Yttrium    | 58    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 14    | Strontium  | 420   | Chlorine   | 470   |
| Gold       |       | Cerium       | 61    | Rubidium   | 15    | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 61    | Bromine    | 250   | Phosphorus | MC    |
| Iridium    |       | Barium       | 940   | Selenium   | 400   | Silicon    | MC    |
| Osmium     |       | Cesium       | 4     | Arsenic    | 550   | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 6     | Germanium  | 39    | Magnesium  | MC    |
| Tungsten   | 12    | Tellurium    | 2     | Gallium    | 350   | Sodium     | MC    |
| Tantalum   | 2     | Antimony     | 51    | Zinc       | 860   | Fluorine   | MC    |
| Hafnium    | 1     | Tin          | 30    | Copper     | 440   | Oxygen     | NR    |
| Lutetium   | 0.3   | Indium       | STD   | Nickel     | 210   | Nitrogen   | NR    |
| Ytterbium  | 2     | Cadmium      | 77    | Cobalt     | 100   | Carbon     | NR    |
| Thulium    | 0.4   | Silver       | 12    | Iron       | MC    | Boron      | MC    |
| Erbium     | 1     | Palladium    |       | Manganese  | 67    | Beryllium  | 29    |
| Holmium    | 2     | Rhodium      |       | Chromium   | 150   | Lithium    | >370  |
| Dysprosium | 3     |              |       |            |       | Hydrogen   | NR    |

STD - Internal Standard

NR - Not Reported

All elements not detected < 0.1 ppm

MC - Major Component >1000 ppm

INT - Interference

Approved:  
5-46

*Robert E. Taylor  
3 Feb 84*

# COMMERCIAL TESTING & ENGINEERING CO.

Reply to

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW 59159A Release Number 11 Project 7601

Sample No.: 819459  
RA XAD-2,  
test 1

SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS

IAD No.: 97-N182-116-28

CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT                                  | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--|-------|------------|-------|------------|-------|
| Uranium    |       | Terbium                                  |       | Ruthenium  |       | Vanadium   | 0.1   |
| Thorium    |       | Gadolinium                               |       | Molybdenum | 0.4   | Titanium   | 5     |
| Bismuth    |       | Europium                                 |       | Niobium    |       | Scandium   | <0.04 |
| Lead       | 0.3   | Samarium                                 |       | Zirconium  | 0.05  | Calcium    | 10    |
| Thallium   |       | Neodymium                                |       | Yttrium    |       | Potassium  | 8     |
| Mercury    | NR    | Praseodymium                             |       | Strontium  | 0.1   | Chlorine   | 13    |
| Gold       |       | Cerium                                   |       | Rubidium   | 0.1   | Sulfur     | 20    |
| Platinum   | *0.1  | Lanthanum                                |       | Bromine    | 0.3   | Phosphorus | 2     |
| Iridium    |       | Barium                                   | 0.8   | Selenium   | 0.5   | Silicon    | 10    |
| Osmium     |       | Cesium                                   | 0.2   | Arsenic    | 0.07  | Aluminum   | 3     |
| Rhenium    |       | Iodine                                   | 0.07  | Germanium  | <0.07 | Magnesium  | 27    |
| Tungsten   |       | Tellurium                                | 0.05  | Gallium    | 0.1   | Sodium     | 40    |
| Tantalum   |       | Antimony                                 |       | Zinc       | 2     | Fluorine   | =22   |
| Hafnium    |       | Tin                                      | 0.07  | Copper     | 0.6   | Oxygen     | NR    |
| Lutetium   |       | Indium                                   | STD   | Nickel     | 2     | Nitrogen   | NR    |
| Ytterbium  |       | Cadmium                                  |       | Cobalt     | 0.1   | Carbon     | NR    |
| Thulium    |       | Silver                                   |       | Iron       | 12    | Boron      | 0.07  |
| Erbium     |       | Palladium                                |       | Manganese  | 0.4   | Beryllium  |       |
| Holmium    |       | Rhodium                                  |       | Chromium   | 1     | Lithium    | 1     |
| Dysprosium |       | *Probable Contamination from sample prep |       |            |       | Hydrogen   | NR    |

STD - Internal Standard

NR - Not Reported

All elements not detected < 0.001 µg/mL

MC - Major Component > 100 µg/mL

INT - Interference

Approved:

5-47

*Robert E. Daugler*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

Reply to

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW 59159A Release Number 11 Project 7601

Sample No.: 819461 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA XAD-2, blank

### CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT  | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--|-------|------------|-------|------------|-------|
| Uranium    |       | Terbium  |       | Ruthenium  |       | Vanadium   | 0.02  |
| Thorium    |       | Gadolinium                                       |       | Molybdenum | 0.1   | Titanium   | 0.3   |
| Bismuth    |       | Europium   |       | Niobium    |       | Scandium   | <0.01 |
| Lead       | 0.3   | Samarium   |       | Zirconium  | 0.02  | Calcium    | 42    |
| Thallium   |       | Neodymium  |       | Yttrium    |       | Potassium  | 3     |
| Mercury    | NR    | Praseodymium                                     |       | Strontium  | 0.1   | Chlorine   | 6     |
| Gold       |       | Cerium   |       | Rubidium   |       | Sulfur     | 4     |
| Platinum   | *0.1  | Lanthanum  |       | Bromine    | 0.1   | Phosphorus | 0.6   |
| Iridium    |       | Barium   | 0.3   | Selenium   | 0.04  | Silicon    | 14    |
| Osmium     |       | Cesium   |       | Arsenic    | <0.01 | Aluminum   | 0.5   |
| Rhenium    |       | Iodine   | 0.05  | Germanium  | <0.01 | Magnesium  | 11    |
| Tungsten   |       | Tellurium  |       | Gallium    | 0.1   | Sodium     | 28    |
| Tantalum   |       | Antimony   |       | Zinc       | 0.8   | Fluorine   | ~13   |
| Hafnium    |       | Tin  |       | Copper     | 0.3   | Oxygen     | NR    |
| Lutetium   |       | Indium   | STD   | Nickel     | 1     | Nitrogen   | NR    |
| Ytterbium  |       | Cadmium  | <0.02 | Cobalt     | <0.02 | Carbon     | NR    |
| Thulium    |       | Silver   |       | Iron       | 1     | Boron      | 0.04  |
| Erbium     |       | Palladium  |       | Manganese  | 0.1   | Beryllium  |       |
| Holmium    |       | Rhodium  |       | Chromium   | 0.3   | Lithium    | 0.3   |
| Dysprosium |       | *Probable contamination from sample preparation. |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.01 ppm

MC — Major Component > 100 ppm

INT — Interference

Approved:

5-48

Robert E. Dayton  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Mr. Christopher Mann  
Acurex Corporation  
555 Clyde Avenue  
Mountain View, CA 94039

Date: January 4, 1984

Subcontract #SW59159A  
P. O. No.: Release #11

Analyst: G. Meagher

Sample No.: 819452 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA Imp 1, test 1 CONCENTRATION IN  $\mu\text{g/mL}$

| ELEMENT    | CONC. | ELEMENT        | CONC. | ELEMENT    | CONC.  | ELEMENT    | CONC.         |
|------------|-------|----------------|-------|------------|--------|------------|---------------|
| Uranium    |       | Terbium        |       | Ruthenium  |        | Vanadium   | 0.006         |
| Thorium    |       | Gadolinium     |       | Molybdenum | *0.02  | Titanium   | 0.2           |
| Bismuth    |       | Europium       |       | Niobium    |        | Scandium   | 0.004         |
| Lead       | 0.6   | Samarium       |       | Zirconium  | 0.01   | Calcium    | 1             |
| Thallium   | 0.07  | Neodymium      |       | Yttrium    |        | Potassium  | *1            |
| Mercury    | NR    | Praseodymium   |       | Strontium  | 0.04   | Chlorine   | 0.1           |
| Gold       |       | Cerium         |       | Rubidium   |        | Sulfur     | 4             |
| Platinum   |       | Lanthanum      |       | Bromine    | 0.02   | Phosphorus | 0.3           |
| Iridium    |       | Barium         | 0.3   | Selenium   | 0.1    | Silicon    | 6             |
| Osmium     |       | Cesium         |       | Arsenic    | <0.004 | Aluminum   | 0.2           |
| Rhenium    |       | Iodine         |       | Germanium  |        | Magnesium  | 4             |
| Tungsten   |       | Tellurium      |       | Gallium    | 0.06   | Sodium     | 1             |
| Tantalum   |       | Antimony       |       | Zinc       | 2      | Fluorine   | $\approx 0.3$ |
| Hafnium    |       | Tin            | 0.3   | Copper     | 0.5    | Oxygen     | NR            |
| Lutetium   |       | Indium         | STD   | Nickel     | 0.2    | Nitrogen   | NR            |
| Ytterbium  |       | Cadmium        | 0.05  | Cobalt     | 0.01   | Carbon     | NR            |
| Thulium    |       | Silver         | 0.08  | Iron       | 1      | Boron      | 0.005         |
| Erbium     |       | Palladium      |       | Manganese  | 0.04   | Beryllium  |               |
| Holmium    |       | Rhodium        |       | Chromium   | 0.2    | Lithium    | 0.05          |
| Dysprosium |       | *Heterogeneous |       |            |        | Hydrogen   | NR            |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.006  $\mu\text{g/mL}$

MC — Major Component > 10  $\mu\text{g/mL}$

INT — Interference

Approved:

5-49

*Robert E. Daugler*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

Reply to

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Mr. Christopher Mann  
Acurex Corporation  
555 Clyde Avenue  
Mountain View, CA 94039

Date: January 4, 1984

Subcontract #SW59159A  
P. O. No.: Release #11

Analyst: G. Meagher

Sample No.: 819448 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28

RA Imp 1 blank

CONCENTRATION IN  $\mu\text{g/mL}$

| ELEMENT    | CONC. | ELEMENT      | CONC.       | ELEMENT    | CONC. | ELEMENT    | CONC.         |
|------------|-------|--------------|-------------|------------|-------|------------|---------------|
| Uranium    |       | Terbium      |             | Ruthenium  |       | Vanadium   | <0.001        |
| Thorium    |       | Gadolinium   |             | Molybdenum | 0.1   | Titanium   | 0.03          |
| Bismuth    |       | Europium     |             | Niobium    |       | Scandium   | 0.001         |
| Lead       |       | Samarium     |             | Zirconium  | 0.02  | Calcium    | 0.2           |
| Thallium   |       | Neodymium    |             | Yttrium    |       | Potassium  | 0.1           |
| Mercury    | NR    | Praseodymium |             | Strontium  | 0.006 | Chlorine   | 0.1           |
| Gold       |       | Cerium       |             | Rubidium   |       | Sulfur     | 0.2           |
| Platinum   |       | Lanthanum    |             | Bromine    | 0.03  | Phosphorus | 0.2           |
| Iridium    |       | Barium       | 0.03        | Selenium   | 0.006 | Silicon    | 0.4           |
| Osmium     |       | Cesium       |             | Arsenic    | 0.002 | Aluminum   | 0.1           |
| Rhenium    |       | Iodine       | 0.005       | Germanium  |       | Magnesium  | 0.3           |
| Tungsten   |       | Tellurium    |             | Gallium    | 0.007 | Sodium     | 0.8           |
| Tantalum   |       | Antimony     | $\leq 0.01$ | Zinc       | 0.05  | Fluorine   | $\approx 0.2$ |
| Hafnium    |       | Tin          | 0.2         | Copper     | 0.004 | Oxygen     | NR            |
| Lutetium   |       | Indium       | STD         | Nickel     | 0.01  | Nitrogen   | NR            |
| Ytterbium  |       | Cadmium      |             | Cobalt     | 0.07  | Carbon     | NR            |
| Thulium    |       | Silver       |             | Iron       | 0.7   | Boron      |               |
| Erbium     |       | Palladium    |             | Manganese  | 0.01  | Beryllium  |               |
| Holmium    |       | Rhodium      |             | Chromium   | 0.03  | Lithium    | 0.004         |
| Dysprosium |       |              |             |            |       | Hydrogen   |               |

STD - Internal Standard

NR - Not Reported

All elements not detected  $< 0.002 \mu\text{g/mL}$

MC - Major Component  $> 10 \mu\text{g/mL}$

INT - Interference

Approved:

5-50

*Robert E. Dayton*  
3 Feb '84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
 INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Acurex Corporation  
 555 Clyde Avenue  
 P.O. Box 7555  
 Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW59159A Release 11 Project 7601

Sample No.: 819478  
 RA coal/PET, test 2

SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS

IAD No.: 97-N182-116-28

CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 2     | Terbium      |       | Ruthenium  |       | Vanadium   | 11    |
| Thorium    | 4     | Gadolinium   |       | Molybdenum | 17    | Titanium   | MC    |
| Bismuth    | 2     | Europium     |       | Niobium    | 2     | Scandium   | 9     |
| Lead       | 28    | Samarium     | 1     | Zirconium  | 8     | Calcium    | MC    |
| Thallium   |       | Neodymium    | 4     | Yttrium    | 4     | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 2     | Strontium  | 24    | Chlorine   | 110   |
| Gold       |       | Cerium       | 4     | Rubidium   | 2     | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 6     | Bromine    | 10    | Phosphorus | 170   |
| Iridium    |       | Barium       | 41    | Selenium   | 4     | Silicon    | MC    |
| Osmium     |       | Cesium       | 0.9   | Arsenic    | 3     | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 0.9   | Germanium  | <0.1  | Magnesium  | MC    |
| Tungsten   |       | Tellurium    |       | Gallium    | 5     | Sodium     | MC    |
| Tantalum   | 3     | Antimony     | 24    | Zinc       | 10    | Fluorine   | ~71   |
| Hafnium    |       | Tin          | 0.9   | Copper     | 27    | Oxygen     | NR    |
| Lutetium   |       | Indium       | STD   | Nickel     | 340   | Nitrogen   | NR    |
| Ytterbium  |       | Cadmium      | 2     | Cobalt     | 9     | Carbon     | NR    |
| Thulium    |       | Silver       |       | Iron       | MC    | Boron      | 14    |
| Erbium     |       | Palladium    |       | Manganese  | 17    | Beryllium  | 0.8   |
| Holmium    |       | Rhodium      |       | Chromium   | 43    | Lithium    | 5     |
| Dysprosium |       |              |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.1 ppm

MC — Major Component > 1000 ppm

INT — Interference

Approved:

5-51

*Robert L. Daykin*  
 3 Feb-84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract No. SW59159A Release 11 Project 7601

Sample No.: 819485 RA PET, test #2 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28

CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    |       | Terbium      |       | Ruthenium  |       | Vanadium   | 0.4   |
| Thorium    |       | Gadolinium   |       | Molybdenum | 8     | Titanium   | 84    |
| Bismuth    | 0.5   | Europium     |       | Niobium    |       | Scandium   | <0.1  |
| Lead       | 32    | Samarium     |       | Zirconium  | 0.2   | Calcium    | 53    |
| Thallium   | 0.3   | Neodymium    |       | Yttrium    | <0.1  | Potassium  | 11    |
| Mercury    | NR    | Praseodymium |       | Strontium  | <0.1  | Chlorine   | 99    |
| Gold       |       | Cerium       | <0.1  | Rubidium   | <0.1  | Sulfur     | 15    |
| Platinum   |       | Lanthanum    |       | Bromine    |       | Phosphorus | 53    |
| Iridium    |       | Barium       | 17    | Selenium   |       | Silicon    | 530   |
| Osmium     |       | Cesium       |       | Arsenic    | <0.1  | Aluminum   | MC    |
| Rhenium    |       | Iodine       | <0.1  | Germanium  | <0.1  | Magnesium  | 40    |
| Tungsten   | 0.8   | Tellurium    |       | Gallium    | 3     | Sodium     | 180   |
| Tantalum   |       | Antimony     | 22    | Zinc       | 6     | Fluorine   | ≈200  |
| Hafnium    |       | Tin          |       | Copper     | 38    | Oxygen     | NR    |
| Lutetium   |       | Indium       | STD   | Nickel     | 290   | Nitrogen   | NR    |
| Ytterbium  |       | Cadmium      | 2     | Cobalt     | 13    | Carbon     | NR    |
| Thulium    |       | Silver       |       | Iron       | 22    | Boron      | 0.7   |
| Erbium     |       | Palladium    |       | Manganese  | 4     | Beryllium  |       |
| Holmium    |       | Rhodium      |       | Chromium   | 11    | Lithium    | 22    |
| Dysprosium |       |              |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.1 ppm

MC — Major Component

INT — Interference

Approved:

*Robert L. Taylor*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
 INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Mr. Christopher Mann  
 Acurex Corporation  
 555 Clyde Avenue  
 Mountain View, CA 94039

Date: January 4, 1984

Subcontract #SW59159A  
 P. O. No.: Release #11

Sample No.: 819498 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
 RA bottom ash,  
 test 2 CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 22    | Terbium      | 3     | Ruthenium  |       | Vanadium   | 24    |
| Thorium    | 31    | Gadolinium   | 8     | Molybdenum | 16    | Titanium   | MC    |
| Bismuth    |       | Europium     | 4     | Niobium    | 15    | Scandium   | 41    |
| Lead       | 52    | Samarium     | 15    | Zirconium  | 92    | Calcium    | MC    |
| Thallium   | 4     | Neodymium    | 32    | Yttrium    | 62    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 10    | Strontium  | 510   | Chlorine   | 36    |
| Gold       |       | Cerium       | 42    | Rubidium   | 25    | Sulfur     | 270   |
| Platinum   |       | Lanthanum    | 66    | Bromine    | 5     | Phosphorus | MC    |
| Iridium    |       | Barium       | MC    | Selenium   | 17    | Silicon    | MC    |
| Osmium     |       | Cesium       | 5     | Arsenic    | 7     | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 0.7   | Germanium  | 4     | Magnesium  | MC    |
| Tungsten   | 4     | Tellurium    | 0.3   | Gallium    | 63    | Sodium     | MC    |
| Tantalum   | 5     | Antimony     | 15    | Zinc       | 23    | Fluorine   | ≈250  |
| Hafnium    | 5     | Tin          | 2     | Copper     | 48    | Oxygen     | NR    |
| Lutetium   | 0.9   | Indium       | STD   | Nickel     | 150   | Nitrogen   | NR    |
| Ytterbium  | 7     | Cadmium      | 4     | Cobalt     | 110   | Carbon     | NR    |
| Thulium    | 1     | Silver       | 0.6   | Iron       | MC    | Boron      | 130   |
| Erbium     | 4     | Palladium    |       | Manganese  | 72    | Beryllium  | 24    |
| Holmium    | 5     | Rhodium      |       | Chromium   | 220   | Lithium    | >400  |
| Dysprosium | 8     |              |       |            |       | Hydrogen   | NR    |

STD - Internal Standard

NR - Not Reported

All elements not detected < 0.1 ppm

MC - Major Component >1000 ppm

INT - Interference

Approved:

5-53

Robert L. Jaylin  
 3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

Reply to

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Mr. Christopher Mann  
Acurex Corporation  
555 Clyde Avenue  
Mountain View, CA 94039

Date: January 4, 1984

Subcontract #SW59159A  
P. O. No.: Release #11

Analyst: G. Meagher

Sample No.: 819496 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA bottom ash  
leachate, test 2 CONCENTRATION IN  $\mu\text{g/mL}$

| ELEMENT    | CONC. | ELEMENT      | CONC.  | ELEMENT    | CONC.  | ELEMENT    | CONC.  |
|------------|-------|--------------|--------|------------|--------|------------|--------|
| Uranium    |       | Terbium      |        | Ruthenium  |        | Vanadium   | 0.05   |
| Thorium    |       | Gadolinium   |        | Molybdenum | 0.5    | Titanium   | 0.2    |
| Bismuth    |       | Europium     |        | Niobium    | 0.003  | Scandium   | <0.002 |
| Lead       | 0.009 | Samarium     |        | Zirconium  | 0.01   | Calcium    | MC     |
| Thallium   |       | Neodymium    |        | Yttrium    | 0.009  | Potassium  | MC     |
| Mercury    | NR    | Praseodymium |        | Strontium  | 3      | Chlorine   | 3      |
| Gold       |       | Cerium       |        | Rubidium   | 0.02   | Sulfur     | MC     |
| Platinum   |       | Lanthanum    |        | Bromine    | 0.08   | Phosphorus | 0.3    |
| Iridium    |       | Barium       | 0.3    | Selenium   | 0.1    | Silicon    | 5      |
| Osmium     |       | Cesium       |        | Arsenic    | 0.01   | Aluminum   | MC     |
| Rhenium    |       | Iodine       | 0.01   | Germanium  | 0.01   | Magnesium  | 0.9    |
| Tungsten   | 0.02  | Tellurium    |        | Gallium    | 0.09   | Sodium     | MC     |
| Tantalum   |       | Antimony     | 0.2    | Zinc       | 0.06   | Fluorine   | ~7     |
| Hafnium    |       | Tin          |        | Copper     | 0.03   | Oxygen     | NR     |
| Lutetium   |       | Indium       | STD    | Nickel     | 0.02   | Nitrogen   | NR     |
| Ytterbium  |       | Cadmium      | 0.004  | Cobalt     | <0.003 | Carbon     | NR     |
| Thulium    |       | Silver       | <0.004 | Iron       | 0.6    | Boron      | 0.4    |
| Erbium     |       | Palladium    |        | Manganese  | 0.005  | Beryllium  |        |
| Holmium    |       | Rhodium      |        | Chromium   | 0.06   | Lithium    | 0.07   |
| Dysprosium |       |              |        |            |        | Hydrogen   | NR     |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.002  $\mu\text{g/mL}$

MC — Major Component > 10  $\mu\text{g/mL}$

INT — Interference

Approved:  
5-54

*Robert L. Daykin  
3 Feb 84*

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

Reply to

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW 59159A Release Number 11 Project 7601

Sample No.: 819504 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA cyclone ash,  
test 2 CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 12    | Terbium      | 0.6   | Ruthenium  |       | Vanadium   | 45    |
| Thorium    | 11    | Gadolinium   | 2     | Molybdenum | 20    | Titanium   | MC    |
| Bismuth    | 1     | Europium     | 0.8   | Niobium    | 9     | Scandium   | 8     |
| Lead       | 70    | Samarium     | 4     | Zirconium  | 19    | Calcium    | MC    |
| Thallium   | 14    | Neodymium    | 15    | Yttrium    | 11    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 7     | Strontium  | 170   | Chlorine   | 250   |
| Gold       |       | Cerium       | 22    | Rubidium   | 5     | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 35    | Bromine    | 77    | Phosphorus | MC    |
| Iridium    |       | Barium       | 360   | Selenium   | 130   | Silicon    | MC    |
| Osmium     |       | Cesium       | 2     | Arsenic    | 70    | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 8     | Germanium  | 8     | Magnesium  | MC    |
| Tungsten   | 2     | Tellurium    | 0.4   | Gallium    | 22    | Sodium     | MC    |
| Tantalum   | 1     | Antimony     | 26    | Zinc       | 88    | Fluorine   | ≈380  |
| Hafnium    | <0.7  | Tin          | 5     | Copper     | 45    | Oxygen     | NR    |
| Lutetium   | 0.2   | Indium       | STD   | Nickel     | 39    | Nitrogen   | NR    |
| Ytterbium  | 1     | Cadmium      | 8     | Cobalt     | 10    | Carbon     | NR    |
| Thulium    | 0.4   | Silver       | 1     | Iron       | MC    | Boron      | 840   |
| Erbium     | 2     | Palladium    |       | Manganese  | 27    | Beryllium  | 10    |
| Holmium    | 3     | Rhodium      |       | Chromium   | 68    | Lithium    | 380   |
| Dysprosium | 5     |              |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.1 ppm

MC — Major Component > 1000 ppm

INT — Interference

Approved:  
5-55

*Robert L. Daykin*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

Reply to

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW 59159A Release Number 11 Project 7601

Sample No.: 819486 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA cyclone ash leachate, test 2 CONCENTRATION IN  $\mu\text{g/mL}$

| ELEMENT    | CONC.        | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|--------------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 0.05         | Terbium      | 0.007 | Ruthenium  |       | Vanadium   | 0.3   |
| Thorium    | 0.01         | Gadolinium   | 0.03  | Molybdenum | 0.02  | Titanium   | MC    |
| Bismuth    |              | Europium     | 0.01  | Niobium    | 0.005 | Scandium   | 0.1   |
| Lead       | 0.1          | Samarium     | 0.06  | Zirconium  | 0.01  | Calcium    | MC    |
| Thallium   | 0.09         | Neodymium    | 0.2   | Yttrium    | 0.5   | Potassium  | MC    |
| Mercury    | NR           | Praseodymium | 0.08  | Strontium  | 4     | Chlorine   | 0.7   |
| Gold       |              | Cerium       | 0.2   | Rubidium   | 0.1   | Sulfur     | MC    |
| Platinum   |              | Lanthanum    | 0.3   | Bromine    | 0.08  | Phosphorus | MC    |
| Iridium    |              | Barium       | 0.05  | Selenium   | 0.2   | Silicon    | MC    |
| Osmium     |              | Cesium       | 0.02  | Arsenic    | 0.2   | Aluminum   | MC    |
| Rhenium    |              | Iodine       | 0.001 | Germanium  | 0.07  | Magnesium  | MC    |
| Tungsten   | $\leq 0.003$ | Tellurium    | 0.001 | Gallium    | 5     | Sodium     | MC    |
| Tantalum   | 0.005        | Antimony     | 0.05  | Zinc       | 12    | Fluorine   | MC    |
| Hafnium    | 0.004        | Tin          | 0.003 | Copper     | 6     | Oxygen     | NR    |
| Lutetium   | 0.002        | Indium       | STD   | Nickel     | 0.8   | Nitrogen   | NR    |
| Ytterbium  | 0.03         | Cadmium      | 0.1   | Cobalt     | 1     | Carbon     | NR    |
| Thulium    | 0.002        | Silver       |       | Iron       | MC    | Boron      | 0.2   |
| Erbium     | 0.008        | Palladium    |       | Manganese  | MC    | Beryllium  | 0.07  |
| Holmium    | 0.01         | Rhodium      |       | Chromium   | 1     | Lithium    | >2    |
| Dysprosium | 0.02         |              |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected  $< 0.001 \mu\text{g/mL}$

MC — Major Component

INT — Interference

5-56

Approved:

*Robert L. Taylor*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

Reply to

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Mr. Christopher Mann  
Acurex Corporation  
555 Clyde Avenue  
Mountain View, CA 94039

Date: January 4, 1984

P. O. No.: Subcontract #SW59159A  
Release #11

Sample No.: 819492 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA 10 $\mu$  + 3 $\mu$ , test 2 CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 9     | Terbium      | 2     | Ruthenium  |       | Vanadium   | 320   |
| Thorium    | 8     | Gadolinium   | 8     | Molybdenum | 140   | Titanium   | MC    |
| Bismuth    | 20    | Europium     | 3     | Niobium    | 29    | Scandium   | 50    |
| Lead       | 890   | Samarium     | 20    | Zirconium  | 56    | Calcium    | MC    |
| Thallium   | 42    | Neodymium    | 48    | Yttrium    | 64    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 22    | Strontium  | 690   | Chlorine   | MC    |
| Gold       |       | Cerium       | 75    | Rubidium   | 22    | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 90    | Bromine    | 220   | Phosphorus | MC    |
| Iridium    |       | Barium       | 830   | Selenium   | 680   | Silicon    | MC    |
| Osmium     |       | Cesium       | 4     | Arsenic    | 810   | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 12    | Germanium  | 44    | Magnesium  | MC    |
| Tungsten   | 19    | Tellurium    | 6     | Gallium    | 290   | Sodium     | MC    |
| Tantalum   | 4     | Antimony     | 680   | Zinc       | MC    | Fluorine   | ≈340  |
| Hafnium    | 3     | Tin          | 35    | Copper     | 650   | Oxygen     | NR    |
| Lutetium   | 1     | Indium       | STD   | Nickel     | MC    | Nitrogen   | NR    |
| Ytterbium  | 10    | Cadmium      | 67    | Cobalt     | 74    | Carbon     | NR    |
| Thulium    | 0.8   | Silver       | 36    | Iron       | MC    | Boron      | MC    |
| Erbium     | 4     | Palladium    |       | Manganese  | 200   | Beryllium  | 43    |
| Holmium    | 6     | Rhodium      |       | Chromium   | MC    | Lithium    | >540  |
| Dysprosium | 9     |              |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.2 ppm

MC — Major Component > 1000 ppm

INT — Interference

Approved:

5-57

*Robert E. Day Jr.*  
3 Feb - 84

# COMMERCIAL TESTING & ENGINEERING CO.

Reply to

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW 59159A Release Number 11 Project 7601

Sample No.: 819475  
RA Filter,  
test 2

SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS

IAD No.: 97-N182-116-28

CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 78    | Terbium      | 0.2   | Ruthenium  | .     | Vanadium   | 170   |
| Thorium    | 2     | Gadolinium   | 1     | Molybdenum | 170   | Titanium   | 110   |
| Bismuth    | 86    | Europium     | 0.3   | Niobium    | 2     | Scandium   | 13    |
| Lead       | MC    | Samarium     | 2     | Zirconium  | 6     | Calcium    | MC    |
| Thallium   | 96    | Neodymium    | 4     | Yttrium    | 7     | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 1     | Strontium  | 71    | Chlorine   | MC    |
| Gold       |       | Cerium       | 3     | Rubidium   | 96    | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 3     | Bromine    | 240   | Phosphorus | MC    |
| Iridium    |       | Barium       | 53    | Selenium   | 300   | Silicon    | MC    |
| Osmium     |       | Cesium       | 16    | Arsenic    | MC    | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 7     | Germanium  | 330   | Magnesium  | MC    |
| Tungsten   | 33    | Tellurium    | 8     | Gallium    | MC    | Sodium     | MC    |
| Tantalum   | 4     | Antimony     | MC    | Zinc       | MC    | Fluorine   | ~310  |
| Hafnium    |       | Tin          | 250   | Copper     | MC    | Oxygen     | NR    |
| Lutetium   |       | Indium       | STD   | Nickel     | MC    | Nitrogen   | NR    |
| Ytterbium  |       | Cadmium      | 700   | Cobalt     | 240   | Carbon     | NR    |
| Thulium    |       | Silver       | 19    | Iron       | MC    | Boron      | MC    |
| Erbium     | <0.2  | Palladium    |       | Manganese  | MC    | Beryllium  | 25    |
| Holmium    | <0.3  | Rhodium      |       | Chromium   | MC    | Lithium    | >312  |
| Dysprosium | <0.5  |              |       |            |       | Hydrogen   | NR    |

STD - Internal Standard

NR - Not Reported

All elements not detected < 0.1 ppm

MC - Major Component > 500 ppm

INT - Interference

Approved:

*Robert L. Dayton*  
3 Feb-84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

Reply to

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW 59159A Release Number 11 Project 7601

Sample No.: 819465 RA XAD-2, test 2 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28

CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT  | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--|-------|------------|-------|------------|-------|
| Uranium    |       | Terbium  |       | Ruthenium  |       | Vanadium   | 0.03  |
| Thorium    |       | Gadolinium                                       |       | Molybdenum | 2     | Titanium   | 1     |
| Bismuth    |       | Europium   |       | Niobium    |       | Scandium   | <0.01 |
| Lead       | 0.2   | Samarium   |       | Zirconium  | <0.04 | Calcium    | 2     |
| Thallium   |       | Neodymium  |       | Yttrium    |       | Potassium  | 2     |
| Mercury    | NR    | Praseodymium                                     |       | Strontium  | 0.08  | Chlorine   | 49    |
| Gold       |       | Cerium   |       | Rubidium   | <0.01 | Sulfur     | 21    |
| Platinum   | *0.2  | Lanthanum  |       | Bromine    | 0.4   | Phosphorus | 7     |
| Iridium    |       | Barium   | 0.4   | Selenium   | 0.5   | Silicon    | 33    |
| Osmium     |       | Cesium   | 0.2   | Arsenic    | 0.03  | Aluminum   | 2     |
| Rhenium    |       | Iodine   | 0.09  | Germanium  | 0.02  | Magnesium  | 4     |
| Tungsten   |       | Tellurium  |       | Gallium    | 0.06  | Sodium     | 6     |
| Tantalum   |       | Antimony   |       | Zinc       | 0.8   | Fluorine   | =91   |
| Hafnium    |       | Tin  |       | Copper     | 0.2   | Oxygen     | NR    |
| Lutetium   |       | Indium   | STD   | Nickel     | 0.3   | Nitrogen   | NR    |
| Ytterbium  |       | Cadmium  |       | Cobalt     | 0.1   | Carbon     | NR    |
| Thulium    |       | Silver   |       | Iron       | 6     | Boron      | 0.1   |
| Erbium     |       | Palladium  |       | Manganese  | 0.1   | Beryllium  |       |
| Holmium    |       | Rhodium  |       | Chromium   | 1     | Lithium    | 0.1   |
| Dysprosium |       | *Probable contamination from sample preparation. |       |            |       | Hydrogen   | NR    |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.02 ppm

MC — Major Component > 100 ppm

INT — Interference

Approved:

5-59

*Robert L. Daykin*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW59159A Release 11 Project 7601

Sample No.: 819466  
RA Imp 1, test 2

SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS

IAD No.: 97-N182-116-28

CONCENTRATION IN  $\mu\text{g/mL}$

| ELEMENT    | CONC. | ELEMENT        | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC.  |
|------------|-------|----------------|-------|------------|-------|------------|--------|
| Uranium    |       | Terbium        |       | Ruthenium  |       | Vanadium   | 0.02   |
| Thorium    |       | Gadolinium     |       | Molybdenum | 0.3   | Titanium   | 0.4    |
| Bismuth    |       | Europium       |       | Niobium    | 0.002 | Scandium   | <0.002 |
| Lead       |       | Samarium       |       | Zirconium  | 0.003 | Calcium    | MC     |
| Thallium   |       | Neodymium      |       | Yttrium    |       | Potassium  | 0.5    |
| Mercury    | NR    | Praseodymium   |       | Strontium  | 0.02  | Chlorine   | MC     |
| Gold       |       | Cerium         |       | Rubidium   | 0.006 | Sulfur     | MC     |
| Platinum   |       | Lanthanum      |       | Bromine    | 0.1   | Phosphorus | 0.4    |
| Iridium    |       | Barium         | 0.03  | Selenium   | 0.3   | Silicon    | MC     |
| Osmium     |       | Cesium         | 0.007 | Arsenic    | 0.009 | Aluminum   | 0.6    |
| Rhenium    |       | Iodine         | *0.2  | Germanium  | 0.001 | Magnesium  | 2      |
| Tungsten   |       | Tellurium      | 0.003 | Gallium    | 0.03  | Sodium     | MC     |
| Tantalum   |       | Antimony       | 0.007 | Zinc       | 0.3   | Fluorine   | MC     |
| Hafnium    |       | Tin            | 0.01  | Copper     | 0.3   | Oxygen     | NR     |
| Lutetium   |       | Indium         | STD   | Nickel     | MC    | Nitrogen   | NR     |
| Ytterbium  |       | Cadmium        |       | Cobalt     | 0.7   | Carbon     | NR     |
| Thulium    |       | Silver         | 0.02  | Iron       | MC    | Boron      | 0.006  |
| Erbium     |       | Palladium      |       | Manganese  | 2     | Beryllium  |        |
| Holmium    | <0.1  | Rhodium        |       | Chromium   | MC    | Lithium    | 0.04   |
| Dysprosium |       | *Heterogeneous |       |            |       | Hydrogen   |        |

STD — Internal Standard

NR — Not Reported

All elements not detected < 0.002  $\mu\text{g/mL}$

MC — Major Component > 10  $\mu\text{g/mL}$

INT — Interference

Approved:

5-60

*Robert L. Daykin*  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300  
 INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to



To: Acurex Corporation  
 555 Clyde Avenue  
 P.O. Box 7555  
 Mountain View, CA 94039

Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract No. SW59159A Release 11 Project 7601

Sample No.: 819493 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
 RA Bottom Ash test #3 CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 16    | Terbium      | 2     | Ruthenium  |       | Vanadium   | 140   |
| Thorium    | 32    | Gadolinium   | 5     | Molybdenum | 9     | Titanium   | MC    |
| Bismuth    |       | Europium     | 2     | Niobium    | 39    | Scandium   | 73    |
| Lead       | 17    | Samarium     | 11    | Zirconium  | 270   | Calcium    | MC    |
| Thallium   | <0.4  | Neodymium    | 42    | Yttrium    | 41    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 22    | Strontium  | 400   | Chlorine   | 230   |
| Gold       |       | Cerium       | 49    | Rubidium   | 22    | Sulfur     | MC    |
| Platinum   |       | Lanthanum    | 56    | Bromine    | 6     | Phosphorus | MC    |
| Iridium    |       | Barium       | 890   | Selenium   | 18    | Silicon    | MC    |
| Osmium     |       | Cesium       |       | Arsenic    | 8     | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 3     | Germanium  | 3     | Magnesium  | MC    |
| Tungsten   | 2     | Tellurium    |       | Gallium    | 28    | Sodium     | MC    |
| Tantalum   | 2     | Antimony     | 29    | Zinc       | 55    | Fluorine   | MC    |
| Hafnium    | 3     | Tin          | 2     | Copper     | 110   | Oxygen     | NR    |
| Lutetium   | 0.4   | Indium       | STD   | Nickel     | 220   | Nitrogen   | NR    |
| Ytterbium  | 4     | Cadmium      | 0.6   | Cobalt     | 64    | Carbon     | NR    |
| Thulium    | 1     | Silver       | 0.3   | Iron       | MC    | Boron      | 78    |
| Erbium     | 3     | Palladium    |       | Manganese  | 42    | Beryllium  | 10    |
| Holmium    | 5     | Rhodium      |       | Chromium   | 430   | Lithium    | >530  |
| Dysprosium | 7     |              |       |            |       | Hydrogen   | NR    |

STD - Internal Standard

NR - Not Reported

All elements not detected  $\leq 0.2$  ppm

MC - Major Component  $\geq 1000$  ppm

INT - Interference

Approved:

5-61

Robert L. Dayton  
 3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 AREA CODE 312 953-9300

INSTRUMENTAL ANALYSIS DIVISION, 490 ORCHARD STREET, GOLDEN, COLORADO 80401, PHONE: 303 278-9521

Reply to

To: Acurex Corporation  
555 Clyde Avenue  
P.O. Box 7555  
Mountain View, CA 94039



Date: February 3, 1984

Analyst: G. Meagher

P. O. No.: Subcontract SW 59159A Release Number 11 Project: 7601

Sample No.: 319464 SPARK SOURCE MASS SPECTROGRAPHIC ANALYSIS IAD No.: 97-N182-116-28  
RA cyclone ash, test 3

## CONCENTRATION IN PPM WEIGHT

| ELEMENT    | CONC. | ELEMENT      | CONC. | ELEMENT    | CONC. | ELEMENT    | CONC. |
|------------|-------|--------------|-------|------------|-------|------------|-------|
| Uranium    | 9     | Terbium      | 0.6   | Ruthenium  |       | Vanadium   | 44    |
| Thorium    | 14    | Gadolinium   | 2     | Molybdenum | 6     | Titanium   | MC    |
| Bismuth    |       | Europium     | 1     | Niobium    | 13    | Scandium   | 15    |
| Lead       | 32    | Samarium     | 5     | Zirconium  | 28    | Calcium    | MC    |
| Thallium   | 3     | Neodymium    | 10    | Yttrium    | 12    | Potassium  | MC    |
| Mercury    | NR    | Praseodymium | 9     | Strontium  | 210   | Chlorine   | 13    |
| Gold       |       | Cerium       | 30    | Rubidium   | 28    | Sulfur     | 220   |
| Platinum   |       | Lanthanum    | 34    | Bromine    | 5     | Phosphorus | MC    |
| Iridium    |       | Barium       | 310   | Selenium   | 13    | Silicon    | MC    |
| Osmium     |       | Cesium       | 4     | Arsenic    | 18    | Aluminum   | MC    |
| Rhenium    |       | Iodine       | 0.2   | Germanium  | 7     | Magnesium  | MC    |
| Tungsten   | 1     | Tellurium    | 0.2   | Gallium    | 19    | Sodium     | MC    |
| Tantalum   | 1     | Antimony     | 5     | Zinc       | 24    | Fluorine   | ~610  |
| Hafnium    | 1     | Tin          | 2     | Copper     | 14    | Oxygen     | NR    |
| Lutetium   | 0.2   | Indium       | STD   | Nickel     | 31    | Nitrogen   | NR    |
| Ytterbium  | 1     | Cadmium      | 0.8   | Cobalt     | 10    | Carbon     | NR    |
| Thulium    | 0.4   | Silver       | 0.2   | Iron       | MC    | Boron      | 27    |
| Erbium     | 0.8   | Palladium    |       | Manganese  | 9     | Beryllium  | 5     |
| Holmium    | 1     | Rhodium      |       | Chromium   | 42    | Lithium    | >370  |
| Dysprosium | 2     |              |       |            |       | Hydrogen   | NR    |

STD - Internal Standard

NR - Not Reported

All elements not detected < 0.1 ppm

MC - Major Component > 1000 ppm

INT - Interference

Approved:

5-62

Robert L. Daykin  
3 Feb 84

# COMMERCIAL TESTING & ENGINEERING CO.

GENERAL OFFICES: 1919 SOUTH HIGHLAND AVE., SUITE 210-B, LOMBARD, ILLINOIS 60148 • (312) 953-9300

ROBERT L. TAYLOR, Ph.D.

MANAGER

INSTRUMENTAL ANALYSIS DIVISION



PLEASE ADDRESS ALL CORRESPONDENCE TO:  
490 ORCHARD ST., GOLDEN, CO 80401  
OFFICE TEL. (303) 278-9521

June 8, 1984

Mr. Christopher Mann  
Acurex Corporation  
P.O. Box 7555  
Mountain View, CA 94039

RE: IAD #97-N815-116-18  
Subcontract #SW 59159A  
Release #13

## Analytical Report

Eighteen samples, previously analyzed for trace elements by spark source mass spectrometry under our IAD identification #97-N182-116-28, were logged in under our IAD identification #97-N815-116-18 on February 22, 1984.

Chlorine and Fluorine were determined using specific ion electrode methodology. Boron and Phosphorus were determined colorimetrically.

Depending on sample type and the amount of sample available, Sulfur was determined turbidimetrically or by X-ray fluorescence spectrometry while the remaining elemental analysis was performed using either atomic absorption/emission spectrophotometry or X-ray fluorescence spectrometry.

The results of these determinations are presented in the following tables. Samples #1, 2, 3, 4, 6, 7, 8, 10, 12, 13, 15, 17 and 18 are reported in weight per cent (Wt.%) on an "as received" basis. Samples #5, 9, 11, 14 and 16 are reported in micrograms per millilitres ( $\mu\text{g/mL}$ ) on an "as received" basis.

If you have any questions concerning these results, please call.

Harold A. Connell  
Assistant Lab Manager

Robert L. Taylor, Jr.  
Robert L. Taylor, Ph.D., Mngr.  
Instrumental Analysis Div.

as



Charter Member

Table No. I  
(Wt.%-As Received)

| <u>Parameter</u> | <u>819463</u><br><u>RA Filter + 1μ, Test 1</u> |
|------------------|--|
| Aluminum (Al)    | 5.39   |
| Boron (B)        | *  |
| Calcium (Ca)     | 11.05  |
| Fluorine (F)     | *  |
| Iron (Fe)        | 8.21   |
| Potassium (K)    | 4.39   |
| Lithium (Li)     | *  |
| Magnesium (Mg)   | 1.54   |
| Sodium (Na)      | 3.37   |
| Phosphorus (P)   | 12.20  |
| Sulfur (S)       | 3.31   |
| Silicon (Si)     | **   |
| Titanium (Ti)    | 0.51   |

\* Insufficient sample for analysis.

\*\* Unable to analyze due to contamination  
from the fiberglass filter.



Table No. II  
(Wt.%-As Received)

| <u>Parameter</u> | <u>819475</u><br><u>RA Filter, Test 2</u> |
|------------------|---|
| Aluminum (Al)    | 1.30                                      |
| Arsenic (As)     | 0.13                                      |
| Boron (B)        | *   |
| Calcium (Ca)     | 0.25                                      |
| Chlorine (Cl)    | 0.03 (300 µg/g)                           |
| Chromium (Cr)    | 0.02 (200 µg/g)                           |
| Copper (Cu)      | 0.02 (180 µg/g)                           |
| Iron (Fe)        | 3.94                                      |
| Potassium (K)    | 2.86                                      |
| Lithium (Li)     | *   |
| Magnesium (Mg)   | <u>&lt;0.1</u>                            |
| Manganese (Mn)   | 0.04 (400 µg/g)                           |
| Sodium (Na)      | 0.57                                      |
| Nickel (Ni)      | 0.03 (250 µg/g)                           |
| Phosphorus (P)   | 3.93                                      |
| Lead (Pb)        | 4.69                                      |
| Sulfur (S)       | 2.58                                      |
| Antimony (Sb)    | <u>&lt;0.01</u> ( <u>&lt;100</u> µg/g)    |
| Silicon (Si)     | 3.89                                      |
| Zinc (Zn)        | 0.10                                      |

\* Insufficient sample for analysis.



Table No. III  
(Wt.%-As Received)

| <u>Parameter</u> | <u>319456</u><br>RA $10\mu + 3\mu$ , Test 1 |
|------------------|---|
| Aluminum (Al)    | 7.58  |
| Arsenic (As)     | 0.05 (490 $\mu\text{g/g}$ )                 |
| Boron (B)        | 0.02 (230 $\mu\text{g/g}$ )                 |
| Barium (Ba)      | 0.19  |
| Calcium (Ca)     | 1.32  |
| Chromium (Cr)    | 0.004 (40 $\mu\text{g/g}$ )                 |
| Iron (Fe)        | 10.79                                       |
| Potassium (K)    | 1.17  |
| Lithium (Li)     | 0.10 (950 $\mu\text{g/g}$ )                 |
| Magnesium (Mg)   | 0.43  |
| Manganese (Mn)   | 0.09 (900 $\mu\text{g/g}$ )                 |
| Sodium (Na)      | 0.45  |
| Phosphorus (P)   | 1.67  |
| Sulfur (S)       | 1.59  |
| Selenium (Se)    | $\leq 0.001$ ( $\leq 10 \mu\text{g/g}$ )    |
| Silicon (Si)     | 12.81                                       |
| Strontium (Sr)   | 0.12  |
| Titanium (Ti)    | 0.68  |
| Zinc (Zn)        | 0.06 (610 $\mu\text{g/g}$ )                 |

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Table No. IV  
(Wt.%-As Received)

| <u>Parameter</u> | <u>819492</u><br><u>RA 10<math>\mu</math>+3<math>\mu</math>, Test 2</u> |
|------------------|---|
| Aluminum (Al)    | 9.03  |
| Boron (B)        | $\leq$ 0.008 ( $\leq$ 80 $\mu$ g/g)                                     |
| Calcium (Ca)     | 1.37  |
| Chlorine (Cl)    | 0.42  |
| Chromium (Cr)    | 0.14  |
| Iron (Fe)        | 11.22   |
| Potassium (K)    | 1.22  |
| Lithium (Li)     | 0.02 (200 $\mu$ g/g)  |
| Magnesium (Mg)   | 0.40  |
| Sodium (Na)      | 0.52  |
| Nickel (Ni)      | 0.03 (250 $\mu$ g/g)  |
| Phosphorus (P)   | 1.71  |
| Sulfur (S)       | 3.06  |
| Silicon (Si)     | 14.97   |
| Titanium (Ti)    | 0.83  |
| Zinc (Zn)        | 0.07 (680 $\mu$ g/g)  |

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Table No. V  
( $\mu\text{g/mL}$ -As Received)

| <u>Parameter</u> | <u>819466</u> | <u>RA Imp 1, Test 2</u> |
|------------------|---------------|-------------------------|
| Calcium (Ca)     |               | 2.2                     |
| Chlorine (Cl)    | 4,500         | (0.45%)                 |
| Chromium (Cr)    | 96            |                         |
| Fluorine (F)     | 42            |                         |
| Iron (Fe)        | 450           |                         |
| Sodium (Na)      | 2,000         | (0.20%)                 |
| Nickel (Ni)      | 71            |                         |
| Sulfur (S)       | 7,700         | (0.77%)                 |
| Silicon (Si)     | 12            |                         |



Table No. VI  
(Wt.%-As Received)

| <u>Parameter</u> | <u>819449</u><br><u>RA Coal, Test 1</u> |
|------------------|---|
| Aluminum (Al)    | 1.19                                    |
| Calcium (Ca)     | 0.19                                    |
| Iron (Fe)        | 0.34                                    |
| Potassium (K)    | 0.12                                    |
| Magnesium (Mg)   | 0.05 (480 µg/g)                         |
| Sodium (Na)      | 0.05 (520 µg/g)                         |
| Silicon (Si)     | 1.87                                    |
| Titanium (Ti)    | 0.05 (540 µg/g)                         |

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Table No. VII  
(Wt.% As Received)

| <u>Parameter</u> | <u>819485</u>         |
|------------------|-----------------------|
|                  | <u>RA PET, Test 2</u> |
| Silicon (Si)     | 0.07                  |

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Table No. VIII  
(Wt.%-As Received)

| <u>Parameter</u> | <u>819488</u>                |
|------------------|------------------------------|
|                  | <u>RA Bottom Ash, Test 1</u> |
| Aluminum (Al)    | 12.89                        |
| Calcium(Ca)      | 1.19                         |
| Fluorine (F)     | <u>&lt;0.01</u>              |
| Iron (Fe)        | 4.75                         |
| Potassium (K)    | 1.24                         |
| Magnesium (Mg)   | 0.46                         |
| Sodium (Na)      | 0.56                         |
| Silicon (Si)     | 21.16                        |
| Titanium (Ti)    | 0.68                         |



Table No. IX  
( $\mu\text{g}/\text{mL}$ -As Received)

| <u>Parameter</u> | <u>819495</u><br><u>RA Bottom Ash Leachate, Test 1</u> |
|------------------|--|
| Calcium (Ca)     | 110  |
| Potassium (K)    | 7.3  |
| Magnesium (Mg)   | 4.7  |
| Sulfur (S)       | 110  |

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Table No. X  
(Wt.%-As Received)

| <u>Parameter</u> | <u>819498</u><br><u>RA Bottom Ash, Test 2</u> |
|------------------|---|
| Aluminum (Al)    | 16.43   |
| Barium (Ba)      | 0.10 (985 µg/g)                               |
| Calcium (Ca)     | 2.59  |
| Fluorine (F)     | <0.01   |
| Iron (Fe)        | 3.86  |
| Potassium (K)    | 1.14  |
| Lithium (Li)     | 0.005(54 µg/g)                                |
| Magnesium (Mg)   | 0.47  |
| Sodium (Na)      | 0.52  |
| Phosphorus (P)   | 0.10  |
| Sulfur (S)       | 0.54  |
| Silicon (Si)     | 21.27   |
| Titanium (Ti)    | 0.74  |

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Table No. XI  
( $\mu\text{g/mL}$ -As Received)

| <u>Parameter</u> | <u>RA Bottom Ash Leachate, Test 2</u> |
|------------------|---------------------------------------|
| Aluminum (Al)    | 319496                                |
| Calcium (Ca)     | 14                                    |
| Potassium (K)    | 53                                    |
| Sodium (Na)      | 5.1                                   |
| Sulfur (S)       | 7.1                                   |
|                  | 90                                    |

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Table No. XII  
(Wt.% - As Received)

| <u>Parameter</u> | <u>819493</u>                |
|------------------|------------------------------|
|                  | <u>RA Bottom Ash, Test 3</u> |
| Aluminum (Al)    | 16.84                        |
| Barium (Ba)      | 0.10                         |
| Calcium (Ca)     | 1.14                         |
| Fluorine (F)     | <u>≤0.01</u>                 |
| Iron (Fe)        | 3.94                         |
| Potassium (K)    | 1.20                         |
| Lithium (Li)     | 0.008 (75 µg/g)              |
| Magnesium (Mg)   | 0.34                         |
| Sodium (Na)      | 0.42                         |
| Phosphorus (P)   | 0.09                         |
| Silicon (Si)     | 20.88                        |
| Sulfur (S)       | 0.11                         |
| Titanium (Ti)    | 0.74                         |

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Table No. XIII  
(Wt % As Received)

| <u>Parameter</u> | <u>819476</u>                 |
|------------------|-------------------------------|
|                  | <u>RA Cyclone Ash, Test 1</u> |
| Aluminum (Al)    | 5.62                          |
| Calcium (Ca)     | 0.67                          |
| Iron (Fe)        | 9.52                          |
| Potassium (K)    | 0.51                          |
| Magnesium (Mg)   | 0.15                          |
| Sodium (Na)      | 0.26                          |
| Phosphorus (P)   | 0.27                          |
| Sulfur (S)       | 4.05                          |
| Silicon (Si)     | 8.20                          |
| Titanium (Ti)    | 0.35                          |



Table No. XIV  
( $\mu\text{g/mL}$ -As Received)

| <u>Parameter</u> | <u>819482</u> | <u>RA Cyclone Ash Leachate, Test 1</u> |
|------------------|---------------|--|
| Aluminum (Al)    |               | 1,500 (0.15%)                          |
| Calcium (Ca)     |               | 1.8                                    |
| Copper (Cu)      |               | 18                                     |
| Fluorine (F)     |               | 42                                     |
| Iron (Fe)        |               | 1,100 (0.11%)                          |
| Potassium (K)    |               | 140                                    |
| Lithium (Li)     |               | 4.7                                    |
| Magnesium (Mg)   |               | 110                                    |
| Manganese (Mn)   |               | 24                                     |
| Sodium (Na)      |               | 170                                    |
| Phosphorus (P)   |               | 0.02                                   |
| Sulfur (S)       |               | 15,300 (1.53%)                         |
| Silicon (Si)     |               | 89                                     |
| Strontium (Sr)   |               | 24                                     |
| Titanium (Ti)    |               | 4.4                                    |
| Zinc (Zn)        |               | 44                                     |



Table No. XV  
(Wt.%-As Received)

| <u>Parameter</u> | <u>819504</u>                 |
|------------------|-------------------------------|
|                  | <u>RA Cyclone Ash, Test 2</u> |
| Aluminum (Al)    | 6.66                          |
| Calcium (Ca)     | 2.27                          |
| Iron (Fe)        | 11.27                         |
| Potassium (K)    | 0.64                          |
| Magnesium (Mg)   | 0.43                          |
| Sodium (Na)      | 0.27                          |
| Phosphorus (P)   | 0.33                          |
| Sulfur (S)       | 2.81                          |
| Silicon (Si)     | 9.84                          |
| Titanium (Ti)    | 0.45                          |



Table No. XIV  
( $\mu\text{g/mL}$ -As Received)

| <u>Parameter</u> | <u>819486</u><br><u>RA Cyclone Ash Leachate, Test 2</u> |
|------------------|---|
| Aluminum (Al)    | 1,100 (0.11%)   |
| Calcium (Ca)     | 1.9   |
| Fluorine (F)     | 38  |
| Iron (Fe)        | 540   |
| Potassium (K)    | 56  |
| Lithium (Li)     | 4.4   |
| Magnesium (Mg)   | 96  |
| Manganese (Mn)   | 18  |
| Sodium (Na)      | 170   |
| Phosphorus (P)   | <0.01   |
| Sulfur (S)       | 3,900 (0.39%)   |
| Silicon (Si)     | 210   |
| Titanium (Ti)    | 0.5   |



Table No. XVII  
(Wt.%-As Received)

| <u>Parameter</u> | <u>819464</u><br><u>RA Cyclone Ash, Test 3</u> |
|------------------|--|
| Aluminum (Al)    | 13.57  |
| Calcium (Ca)     | 1.28   |
| Iron (Fe)        | 9.35   |
| Potassium (K)    | 1.75   |
| Lithium (Li)     | 0.01 (110 µg/g)                                |
| Magnesium (Mg)   | 0.47   |
| Sodium (Na)      | 0.24   |
| Phosphorus (P)   | 0.16   |
| Silicon (Si)     | 21.43  |
| Titanium (Ti)    | 0.76   |



Table No. XVIII  
(Wt.% - As Received)

| <u>Parameter</u> | <u>819478</u><br><u>RA Coat/PET, Test 2</u> |
|------------------|---|
| Aluminum (Al)    | 1.56  |
| Calcium (Ca)     | 0.09 (930 µg/g)                             |
| Iron (Fe)        | 0.38  |
| Potassium (K)    | 0.09 (910 µg/g)                             |
| Magnesium (Mg)   | 0.04 (370 µg/g)                             |
| Sodium (Na)      | 0.04 (370 µg/g)                             |
| Silicon (Si)     | 1.37  |
| Titanium (Ti)    | 0.05 (480 µg/g)                             |

5-81

COMMERCIAL TESTING & ENGINEERING CO.





 ACUREX  
Corporation

## **ANALYSIS LABORATORIES**

## **DATA REPORTING FORM**

CUSTOMER CMEA DATE January 13, 1984

DATE January 13, 1984

CUSTOMER CONTRACT NO. 307736.62 ACUREX CONTRACT NO. 8311-030

ACUREX CONTRACT NO. 8311-030

RESULTS REPORT TO L. Waterland TELEPHONE \_\_\_\_\_

## **TELEPHONE**

**ADDRESS** \_\_\_\_\_

## **Vermont**

ANALYST C. McMillen

REVIEWER *Frank S. Coley*

**5.6 TOTAL CHROMATOGRAPHABLE ORGANICS (TCO), GRAVIMETRIC ORGANICS (GRAV), GAS CHROMATOGRAPHY/MASS SPECTROMETRY (GC/MS), AND INFRARED SPECTRA (IR) OF TOTAL SAMPLE EXTRACTS**

Acurex/ES

January 16, 1984  
Acurex ID#: 8310-003  
8311-030  
Client PO#: 307736.62

Attention: Larry Waterland

Sample: Vermont, Rock of Ages, 2 SASS Trains;  
Received 7/12/83

The above samples were analyzed by Level 1 protocol. The XAD and OMC extracts were combined per your instruction. Organic extracts were also analyzed for the semivolatile priority pollutants by gas chromatography/mass spectrometry employing a J&W SE-54 30 meter capillary column. The column was held at 30°C for 2 minutes, then ramped at 10°C per minute to 270°C. In addition to the priority pollutants, other organics including benzo(c)phenanthrene, dibenzo(c,g)carbazole, 7,12-dimethylbenzo(a)anthracene, 3-methylcholanthrene, and perylene were sought employing the computerized library search and manual interpretation. The assignment and quantitation of these organics is tentative since analytical standards of these compounds were not available for analysis. Benzo(c)phenanthrene, dibenzo(c,g)carbazole, 7,12-dimethylbenzo(a)anthracene, 3-methylcholanthrene and perylene were not detected in any of the samples at levels above 400 µg per 10 mL of extract.

Submitted by: Greg Nicoll  
Greg Nicoll  
Operations Manager

Viorica Lopez-Avila  
Viorica Lopez-Avila, Ph.D.  
Technical Director

GN/VLA/ats



 ACUREX  
Corporation

## **ANALYSIS LABORATORIES**

## **DATA REPORTING FORM**

CUSTOMER CMEA

DATE January 16, 1984

CUSTOMER CONTRACT NO. 307736.62

ACUBEX CONTRACT NO. 8310-003

**RESULTS REPORT TO** L. Waterland

## **TELEPHONE**

**ADDRESS** \_\_\_\_\_

## **Vermont**

\* mg/Kg

\*\* Duplicate injection

\*\*\* Normally found in laboratory blanks  
at this level

ANALYST U. Spannaquel, C. Beeman, S. Kraska

REVIEWER Doug Lefever

IR REPORT

SAMPLE: 8310-03-6 Front Half Rinse

IR REPORT

**SAMPLE:**

8310-03-8

XAD Test I

IR REPORT

**SAMPLE:** 8310-03-14 XAD B1k

IR REPORT

**SAMPLE:**

8310-03-28

Bottom Ash I

IR REPORT

**SAMPLE:**

8310-03-29

## Cyclone Ash I

IR REPORT

**SAMPLE:**

8310-03-20

### Front Half Rinse Test II



IR REPORT

**SAMPLE:** 8310-03-32      Bottom Ash II

IR REPORT

**SAMPLE:** 8310-03-33

Cyclone Ash II

GC/MS Detection Limits

| <u>ACID COMPOUND</u>                         | <u>ng</u> | <u>BASE/NEUTRAL COMPOUNDS</u>   | <u>ng</u> |
|--|-----------|---------------------------------|-----------|
| 21A 2,4,6-trichlorophenol                    | 5         | 41B 4-bromophenyl phenyl ether  | 1         |
| 22A p-chloro-m-cresol                        | 5         | 42B bis(2-chloroisopropyl)ether | 1         |
| 24A 2-chlorophenol                           | 5         | 43B bis(2-chloroethoxy)methane  | 1         |
| 31A 2,4-dichlorophenol                       | 5         | 52B hexachlorobutadiene         | 1         |
| 34A 2,4-dimethylphenol                       | 5         | 53B hexachlorocyclopentadiene   | 1         |
| 57A 2-nitrophenol                            | 5         | 54B isophorone                  | 1         |
| 58A 4-nitrophenol                            | 20        | 55B naphthalene                 | 1         |
| 59A 2,4-dinitrophenol                        | 20        | 56B nitrobenzene                | 1         |
| 60A 4,6-dinitro-o-cresol                     | 20        | 61B N-nitrosodimethylamine      | NA        |
| 64A pentachlorophenol                        | 5         | 62B N-nitrosodiphenylamine      | 1         |
| 65A phenol                                   | 1         | 63B N-nitrosodi-n-propylamine   | 5         |
| <u>BASE/NEUTRAL COMPOUNDS</u>                |           |                                 |           |
| 1B acenaphthene                              | 1         | 65B bis(2-ethylhexyl)phthalate  | 1         |
| 58 benzidine                                 | 20        | 67B butylbenzyl phthalate       | 1         |
| 88 1,2,4-trichlorobenzene                    | 1         | 68B di-n-butyl phthalate        | 1         |
| 98 hexachlorobenzene                         | 1         | 69B di-n-octyl phthalate        | 1         |
| 12B hexachloroethane                         | 1         | 70B diethyl phthalate           | 1         |
| 18B bis(2-chloroethyl)ether                  | 1         | 71B dimethyl phthalate          | 1         |
| 20B 2-chloronaphthalene                      | 1         | 72B benzo(a)anthracene          | 1         |
| 25B 1,2-dichlorobenzene                      | 1         | 73B benzo(a)pyrene              | 1         |
| 26B 1,3-dichlorobenzene                      | 1         | 74B 3,4-benzofluoranthene       | 1         |
| 27B 1,4-dichlorobenzene                      | 1         | 75B benzo(k)fluoranthene        | 1         |
| 29B 3,3'-dichlorobenzidine                   | 5         | 76B chrysene                    | 1         |
| 35B 2,4-dinitrotoluene                       | 1         | 77B acenaphthylene              | 1         |
| 36B 2,6-dinitrotoluene                       | 1         | 78B anthracene                  | 1         |
| 37B 1,2-diphenylhydrazine<br>(as azobenzene) | 1         | 79B benzo(ghi)perylene          | 5         |
| 39B fluoranthene                             | 1         | 80B fluorene                    | 1         |
| 40B 4-chlorophenyl phenyl ether              | 1         | 81B phenanthrene                | 1         |
|  |           | 82B dibenzo(a,h)anthracene      | 5         |
|  |           | 83B indeno(1,2,3-cd)pyrene      | 5         |
|  |           | 84B pyrene                      | 1         |

## 5.7 LIQUID CHROMATOGRAPHY (LC) SEPARATION AND IR SPECTRA OF LC FRACTIONS

Acurex/ES (CMEA)  
MS 2-2260

March 12, 1984  
Acurex ID#: 8402-020  
Client PO#: 307736.62

Attention: Larry Waterland

Sample: Cyclone Ash, Rock of Ages; Received 2/10/84

The above samples were subjected to liquid chromatography followed by gravimetric measurement and infrared spectrophotometry according to Level 1 protocol.

Results are enclosed.

Submitted by: John S. Labash  
John S. Labash  
Chemist

Approved by: Greg Nicoll  
Greg Nicoll  
Manager, Inorganic Chemistry

JSL/GN/ats

Enclosures

SAMPLE: Rock of Ages Cyclone Ash Test 1 #819476 8402-020-1

|                           | TCO<br>mg | GRAV<br>mg | TCO + GRAV<br>Total mg | Concentration<br>mg/ Kg |
|---------------------------|-----------|------------|------------------------|-------------------------|
| Total Sample <sup>1</sup> |           | 55         |                        | 1100                    |
| Taken for LC <sup>2</sup> |           | 22         |                        | 440                     |
| Recovered <sup>3</sup>    |           | 28         |                        | 560                     |

| Fraction | TCO in mg            |       |                |                    | GRAV in mg           |       |                |                    | TCO +<br>GRAV<br>Total mg | Concentration<br>mg/Kg |
|----------|----------------------|-------|----------------|--------------------|----------------------|-------|----------------|--------------------|---------------------------|------------------------|
|          | Found in<br>Fraction | Blank | Cor-<br>rected | Total <sup>4</sup> | Found in<br>Fraction | Blank | Cor-<br>rected | Total <sup>4</sup> |                           |                        |
| 1        |                      |       |                |                    | 5.0                  | <0.5  | 5.0            | 12                 |                           | 240                    |
| 2        |                      |       |                |                    | 0.8                  | <0.4  | 0.8            | 2                  |                           | 40                     |
| 3        |                      |       |                |                    | 2.2                  | <0.4  | 2.2            | 6                  |                           | 120                    |
| 4        |                      |       |                |                    | 1.8                  | <0.4  | 1.8            | 4                  |                           | 80                     |
| 5        |                      |       |                |                    | 2.2                  | <0.4  | 2.2            | 6                  |                           | 120                    |
| 6        |                      |       |                |                    | 11.6                 | <0.4  | 11.6           | 29                 |                           | 580                    |
| 7        |                      |       |                |                    | 4.6                  | 0.6   | 4.0            | 10                 |                           | 200                    |
| Sum      |                      |       |                |                    | 28.2                 | 0.6   | 27.6           | 69                 |                           | 1400                   |

1. Quantity in entire sample, determined before LC

2. Portion of whole sample used for LC, actual mg

3. Quantity recovered from LC column, actual mg

4. Total mg computed back to total sample

IR REPORT

**SAMPLE:** 2-20-1 LCF 1 Cyclone Ash Test 1

IR REPORT

**SAMPLE:** 2-20-1 LCF 2

IR REPORT

**SAMPLE:** 2-20-1 LCF 3

IR REPORT

SAMPLE: 2-20-1 LCF 4

IR REPORT

**SAMPLE** 2-20-1 LCF 5

IR REPORT

**SAMPLE:**

2-20-1 LCF 6

IR REPORT

**SAMPLE:** 2-20-1 LCF 7

SAMPLE: Rock of Ages Cyclone Ash Test 2 #819504 8402-020-2

|                           | TCO<br>mg | GRAV<br>mg | TCO + GRAV<br>Total mg | Concentration<br>mg/Kg |
|---------------------------|-----------|------------|------------------------|------------------------|
| Total Sample <sup>1</sup> |           | 25         |                        | 500                    |
| Taken for LC <sup>2</sup> |           | 22         |                        | 440                    |
| Recovered <sup>3</sup>    |           | 27         |                        | 540                    |

| Fraction | TCO in mg            |       |                |                    | GRAV in mg           |       |                |                    | TCO +<br>GRAV<br>Total mg | Concentration<br>mg/Kg |
|----------|----------------------|-------|----------------|--------------------|----------------------|-------|----------------|--------------------|---------------------------|------------------------|
|          | Found in<br>Fraction | Blank | Cor-<br>rected | Total <sup>4</sup> | Found in<br>Fraction | Blank | Cor-<br>rected | Total <sup>4</sup> |                           |                        |
| 1        |                      |       |                |                    | 5.0                  | <0.5  | 5.0            | 5.6                |                           | 110                    |
| 2        |                      |       |                |                    | 1.8                  | <0.4  | 1.8            | 2.0                |                           | 40                     |
| 3        |                      |       |                |                    | 3.4                  | <0.4  | 3.4            | 3.8                |                           | 76                     |
| 4        |                      |       |                |                    | 2.4                  | <0.4  | 2.4            | 2.7                |                           | 54                     |
| 5        |                      |       |                |                    | 2.6                  | <0.4  | 2.6            | 2.9                |                           | 58                     |
| 6        |                      |       |                |                    | 8.4                  | <0.4  | 8.4            | 9.3                |                           | 190                    |
| 7        |                      |       |                |                    | 3.6                  | 0.6   | 3.0            | 3.3                |                           | 66                     |
| Sum      |                      |       |                |                    | 27.2                 | 0.6   | 26.6           | 29.6               |                           | 590                    |

1. Quantity in entire sample, determined before LC

2. Portion of whole sample used for LC, actual mg

3. Quantity recovered from LC column, actual mg

4. Total mg computed back to total sample

IR REPORT

**SAMPLE:** 2-20-2 LCF 1 Cyclone Ash Test 2

IR REPORT

**SAMPLE:** 2-20-2 LCF 2

IR REPORT

**SAMPLE:**

2-20-2 LCF 3

IA REPORT

**SAMPLE:**

2-20-2 LCF 4

IA REPORT

**SAMPLE:**                  2-20-2

LCE 5

IA REPORT

**SAMPLE:** 2-20-2 LCF 6

**SAMPLE:** 2-20-2 LCF 7



ACUREX  
Corporation

Energy & Environmental Division

Acurex/ES (CMEA)  
MS 2-2260

March 13, 1984  
Acurex ID#: 8401-029  
Client PO#: 307736.62

Attention: Larry Waterland

Sample: Honor Rancho Inlet XAD, Rock of Ages XADs;  
Received 1/20/84

The above samples were subjected to liquid chromatography followed by TCO,  
gravimetric measurement, and infrared spectrophotometry according to Level 1  
protocol.

Results are enclosed.

Prepared by: John S. Labash  
John S. Labash  
Chemist

Approved by: Greg Nicoll  
Greg Nicoll  
Manager, Inorganic Chemistry

JSL/GN/ats

5-116

SAMPLE: 819459 Rock of Ages Test 1 XAD-2

|                           | TCO<br>mg | GRAV<br>mg | TCO + GRAV<br>Total mg | Concentration<br>mg/dscm |
|---------------------------|-----------|------------|------------------------|--------------------------|
| Total Sample <sup>1</sup> | 2.0       | 24         | 26                     |                          |
| Taken for LC <sup>2</sup> | 1.1       | 14         | 15                     |                          |
| Recovered <sup>3</sup>    | 0.6       | 7.9        | 8.5                    |                          |

| Fraction | TCO in mg            |       |                |                    | GRAV in mg           |       |                |                    | TCO +<br>GRAV<br>Total mg | Concentration<br>mg/dscm |
|----------|----------------------|-------|----------------|--------------------|----------------------|-------|----------------|--------------------|---------------------------|--------------------------|
|          | Found in<br>Fraction | Blank | Cor-<br>rected | Total <sup>4</sup> | Found in<br>Fraction | Blank | Cor-<br>rected | Total <sup>4</sup> |                           |                          |
| 1        | 0.6                  | <0.2  | 0.6            | 1.1                | 1.5                  | <0.5  | 1.5            | 2.6                | 3.7                       |                          |
| 2        | <0.1                 | <0.1  | <0.1           | <0.2               | <0.4                 | <0.4  | <0.4           | <0.7               | <0.9                      |                          |
| 3        | <0.1                 | <0.1  | <0.1           | <0.2               | <0.4                 | <0.4  | <0.4           | <0.7               | <0.9                      |                          |
| 4        | <0.1                 | 0.2   | <0.1           | <0.2               | <0.4                 | <0.4  | <0.4           | <0.7               | <0.9                      |                          |
| 5        | <0.1                 | <0.1  | <0.1           | <0.2               | 0.8                  | <0.4  | 0.8            | 1.4                | 1.4                       |                          |
| 6        | <0.1                 | <0.1  | <0.1           | <0.2               | 2.6                  | <0.4  | 2.6            | 4.6                | 4.6                       |                          |
| 7        | <0.1                 | <0.1  | <0.1           | <0.2               | 3.6                  | 0.6   | 3.0            | 5.3                | 5.3                       |                          |
| Sum      | 0.6                  | <0.9  | 0.6            | 1.1                | 8.5                  | 0.6   | 7.9            | 13.9               | 15                        |                          |

1. Quantity in entire sample, determined before LC

2. Portion of whole sample used for LC, actual mg

3. Quantity recovered from LC column, actual mg

4. Total mg computed back to total sample

IR REPORT

SAMPLE: 1-29-2 LCF 1

IR REPORT

**SAMPLE:** 1-29-2 LCF 2

IR REPORT

1-29-2 LCF 3

**SAMPLE:**

IR REPORT

**SAMPLE:** 1-29-2 LCF 4

IR REPORT

SAMF-E: 1-29-2 LCF 5

**SAMPLE:** 1-29-2 LCF 6

IR REPORT

**SAMPLE:** 1-29-2 LCF 7

SAMPLE: 819465 Rock of Ages Test 2 XAD-2

|                           | TCO<br>mg | GRAV<br>mg | TCO + GRAV<br>Total mg | Concentration<br>mg/dscm |
|---------------------------|-----------|------------|------------------------|--------------------------|
| Total Sample <sup>1</sup> | 3.2       | 27         | 30                     |                          |
| Taken for LC <sup>2</sup> | 1.6       | 13         | 15                     |                          |
| Recovered <sup>3</sup>    | <0.8      | 13.6       | 14                     |                          |

| Fraction | TCO in mg            |       |                |                    | GRAV in mg           |       |                |                    | TCO +<br>GRAV<br>Total mg | Concentration<br>mg/dscm |
|----------|----------------------|-------|----------------|--------------------|----------------------|-------|----------------|--------------------|---------------------------|--------------------------|
|          | Found in<br>Fraction | Blank | Cor-<br>rected | Total <sup>4</sup> | Found in<br>Fraction | Blank | Cor-<br>rected | Total <sup>4</sup> |                           |                          |
| 1        | <0.2                 | <0.2  | <0.2           | <0.4               | 3.2                  | <0.5  | 3.2            | 6.5                | 6.5                       |                          |
| 2        | <0.1                 | <0.1  | <0.1           | <0.2               | <0.4                 | <0.4  | <0.4           | <0.8               | <1                        |                          |
| 3        | <0.1*                | <0.1  | <0.1           | <0.2               | 1.2                  | <0.4  | 1.2            | 2.4                | 2.4                       |                          |
| 4        | <0.1                 | 0.2   | <0.1           | <0.2               | 1.0                  | <0.4  | 1.0            | 2.0                | 2.0                       |                          |
| 5        | <0.1                 | <0.1  | <0.1           | <0.2               | 0.6                  | <0.4  | 0.6            | 1.2                | 1.2                       |                          |
| 6        | <0.1                 | <0.1  | <0.1           | <0.2               | 3.8                  | <0.4  | 3.8            | 7.8                | 7.8                       |                          |
| 7        | <0.1                 | <0.1  | <0.1           | <0.2               | 4.4                  | 0.6   | 3.8            | 7.8                | 7.8                       |                          |
| Sum      | <0.8                 | <0.9  | <0.8           | <2                 | 14.2                 | 0.6   | 13.6           | 27.7               | 27.7                      |                          |

1. Quantity in entire sample, determined before LC

2. Portion of whole sample used for LC, actual mg

3. Quantity recovered from LC column, actual mg

4. Total mg computed back to total sample

\*Duplicate injection gave <0.1

IR REPORT

**SAMPLE:**

1-29-3 LCF 1

IR REPORT

**SAMPLE:**

1-29-3 LCF 2

IR REPORT

**SAMPLE:** 1-29-3 LCF 3

IR REPORT

**SAMPLE:** 1-29-3 LCF 4

IR REPORT

**SAMPLE:**

1-29-3 LCF 5

IR REPORT

**SAMPLE:** 1-29-3 LCF 6

IR REPORT

**SAMPLE:** 1-29-3 LCF 7

IR REPORT

**SAMPLE:** \_\_\_\_\_

1-29-BLK LCF-1

IR REPORT

SAMPLE: 1-29-BLK LCF 2

IR REPORT

**SAMPLE:** 1-29-BLK LCF 3

IR REPORT

**SAMPLE:** 1-29-BLK LCF 4

IR REPORT

**SAMPLE:** 1-29-BLK LCF 5

IR REPORT

SAMPLE: 1-29-BLK LCF 6

IR REPORT

**SAMPLE:** 1-29-BLK LCF 7

## 5.8 GC/MS ANALYSES OF VOST TRAPS

Acurex/E.S.

Attention: Larry Waterland

November 1, 1983

Acurex ID#: 8307-010

Customer PO#: 307736.62

Page 1 of 2

Subject: Analysis of Two VOST Sample Sets  
by GC/MS.

The above referenced samples were analyzed according to the latest revisions of the EPA VOST Protocol for Volatile Priority Pollutants and Xylenes. An attempt was also made to identify ethylene oxide, propylene oxide, 2-nitropropane and allyl chloride, but due to the lack of analytical standards for these compounds, it proved impossible.

Results are listed in Table 1.

Please call if you have any questions.

Prepared by:

*William G. Hellier*  
William G. Hellier  
Staff Chemist

Approved by:

*Viorica Lopez-Avila*  
Viorica Lopez-Avila, Ph.D.  
Technical Director

WGH/VLA/ats

Table 1. Volatile Organics Results

| Trap ID<br>Lab ID                 | Concentration (ng/trap)        |  |                               |                         |   |
|-----------------------------------|--------------------------------|--|-------------------------------|-------------------------|---|
|                                   | Tenax/C<br>819501<br>Sample -1 | Tenax<br>819501<br>Surrogate -2 <sup>a</sup> | Tenax/C<br>819502<br>Blank -3 | Tenax<br>819502<br>F -4 | Tenax/C<br>819503,<br>Air -5 <sup>a</sup> |
| <u>Compound</u>                   |                                |  |                               |                         |   |
| Chloromethane                     | 12                             | 10   | ND                            | ND                      | ND  |
| Bromomethane                      | ND                             | ND   | ND                            | ND                      | ND  |
| Vinyl chloride                    | ND                             | ND   | ND                            | ND                      | ND  |
| Chloroethane                      | ND                             | ND   | ND                            | ND                      | ND  |
| Dichloromethane                   | 65                             | >1,100                                       | 1,600                         | 115                     | 102                                       |
| 1,1-Dichloroethylene              | 98                             | ND   | 90                            | 80                      | ND  |
| 1,1-Dichloroethane                | ND                             | ND   | ND                            | ND                      | ND  |
| Trans-1,2-dichloroethylene        | ND                             | ND   | ND                            | ND                      | ND  |
| Chloroform                        | 22                             | 67   | ND                            | ND                      | 8   |
| 1,2-Dichloroethane                | ND                             | ND   | 37                            | ND                      | ND  |
| 1,1,1-Trichloroethane             | ND                             | ND   | ND                            | ND                      | ND  |
| - Carbon tetrachloride            | ND                             | ND   | ND                            | ND                      | ND  |
| Dichlorobromomethane              | ND                             | ND   | ND                            | ND                      | ND  |
| 1,2-Dichloropropane               | ND                             | ND   | ND                            | ND                      | ND  |
| 1,3-Dichloropropene(trans)        | ND                             | ND   | ND                            | ND                      | ND  |
| Trichloroethylene                 | 3                              | 483  | 5                             | ND                      | 17  |
| Chlorodibromomethane              | ND                             | ND   | ND                            | ND                      | ND  |
| 1,1,2-Trichloroethane             | ND                             | ND   | 72                            | ND                      | 21  |
| 1,3-Dichloropropene(cis)          | ND                             | ND   | ND                            | ND                      | ND  |
| Benzene                           | 7                              | ND   | 69                            | ND                      | 26  |
| 2-Chloroethyl vinyl ether         | ND                             | ND   | ND                            | ND                      | ND  |
| Bromoform                         | ND                             | ND   | 213                           | ND                      | ND  |
| Tetrachloroethylene               | ND                             | 51   | ND                            | ND                      | ND  |
| 1,1,2,2-Tetrachloroethane         | ND                             | ND   | 173                           | ND                      | ND  |
| Toluene                           | 140                            | 146  | 5                             | ND                      | 36  |
| Chlorobenzene                     | ND                             | 152  | 15                            | ND                      | 7   |
| Ethylbenzene                      | ND                             | 14   | 10                            | ND                      | 7   |
| Xylenes                           | ND                             | ND   | ND                            | ND                      | ND  |
| Dichlorodifluoromethane           | ND                             | ND   | ND                            | ND                      | ND  |
| Trichlorofluoromethane            | 28                             | ND   | ND                            | 335                     | ND  |
| <u>Percent Surrogate Recovery</u> |                                |  |                               |                         |   |
| Toluene-d <sub>8</sub>            | 95                             | 57   | 88                            | 50                      | 88  |

## 5.9 N<sub>2</sub>O ANALYSES BY GC/ECD



Energy & Environmental Division

Acurex/E.S.

September 2, 1983  
Acurex ID#: 8308-012  
Client PO#: 307736.62  
Page 1 of 1

Attention: Larry Waterland

Subject: Analysis of 2 Gas Bombs for Nitrous Oxide by GC/ECD

The above referenced samples were analyzed by GC/ECD according to previously reported method.

Results are listed in the table below:

| Sample ID | N <sub>2</sub> O (ppm) |
|-----------|------------------------|
| 812714    | 27                     |
| 812715    | 58                     |

If you have any questions, please call.

Submitted by: William G. Hellier  
William G. Hellier  
Staff Chemist

Approved by: Viorica Lopez-Avila  
Viorica Lopez-Avila, Ph.D.  
Technical Director

WGH/VLA/ats

5-147

## 5.10 BIOASSAY RESULTS

In the following, samples with the prefix "RA" are for these tests; samples with prefixes "HR", or "DM" are for other tests performed.



BIONETICS

5516 Nicholson Lane, Kensington, Maryland 20895 301 881-5600 • Telex 89-8369

April 18, 1984

Dr. Larry Waterland  
Acurex Corporation  
485 Clyde Avenue  
Mountain View, California 94042

RE: Acurex Subcontract No. RB59178A  
Release No. 6

Dear Larry:

Enclosed are three bound, and one unbound, copies of the final reports for the five XAD resin extract samples and six ash samples submitted for testing and evaluation in IERL-EPA Level 1 Ames/Salmonella mutagenesis and CHO cytotoxicity bioassays. All studies were conducted and evaluated under IERL-EPA Level 1 guidelines.

Bioassay of the samples took slightly longer than normal because a phased testing approach was used with the XAD-2 resin extract samples. This phased approach involved initial CHO cytotoxicity testing, then preliminary range-finding Ames tests with only one strain, followed by one or more definitive Ames assays. By using this approach, we were able to adequately test and evaluate all samples.

The summary of the bioassay data, the criteria used to evaluate the results, the critical data upon which the evaluations were based, and a graphic display of the relative ranking of the samples are presented in the attached tables and figures.

If you have any questions or comments concerning these reports or future testing, please fell free to contact me at (301) 881-5600, extension 536.

Sincerely,

LITTON BIONETICS, INC.

Robert R. Young  
Environmental Assessment Section  
Department of Molecular Toxicology

RRY/mg

Enclosures: Ames and CHO 7330-7346 Reports.

cc: Contracts, LBI No. 20993, 20988

TABLE 1  
BIOASSAY SUMMARY TABLE

Technical Directive or Project No. LBI Project No. 20988 and 20993.

Contract No. EPA No. 68-02-3188; ACUREX Subcontract No. RB 59178A Release No. 6.

| Sample Identification                                   | Health Effects Tests |                  |                  |                 |      | Ecological Effects Tests |  |        |              |                       |                 |                 |
|---|----------------------|------------------|------------------|-----------------|------|--------------------------|--|--------|--------------|-----------------------|-----------------|-----------------|
|   | AMES Salmonella      | RAM Cytotoxicity | CHO Cytotoxicity | Rodent Toxicity | Fish | Fresh Water              |  | Marine |              | Plant Stress Ethylene | Root Elongation | Insect Toxicity |
| HR XAD-2 EXTRACT,<br>INLET (819369)                     | H                    | M/H              |                  |                 |      | Invertebrate             |  | Fish   | Invertebrate | Algal                 |                 |                 |
| HR XAD-2 EXTRACT,<br>OUTLET (819370)                    | M                    | M                |                  |                 |      |                          |  |        |              |                       |                 |                 |
| RA XAD-2 EXTRACT,<br>TEST 1 (819459)                    | H                    | M                |                  |                 |      |                          |  |        |              |                       |                 |                 |
| RA XAD-2 EXTRACT,<br>TEST 2 (819465)                    | M                    | H/M              |                  |                 |      |                          |  |        |              |                       |                 |                 |
| DM XAD-2 EXTRACT<br>(900206)                            | M                    | M                |                  |                 |      |                          |  |        |              |                       |                 |                 |
| RA BOTTOM ASH,<br>TEST 1 (819488)                       | ND                   | ND               |                  |                 |      |                          |  |        |              |                       |                 |                 |
| RA BOTTOM ASH,<br>TEST 2 (819498)                       | ND                   | ND               |                  |                 |      |                          |  |        |              |                       |                 |                 |
| RA CYCLONE ASH,<br>TEST 1 (819476)                      | M/H                  | ND               |                  |                 |      |                          |  |        |              |                       |                 |                 |
| RA CYCLONE ASH,<br>TEST 2 (819504)                      | L/M                  | ND               |                  |                 |      |                          |  |        |              |                       |                 |                 |
| DM FILTER + 1 $\mu\text{m}$ PART.<br>(900204)           | ND                   | L                |                  |                 |      |                          |  |        |              |                       |                 |                 |
| DM 10 $\mu\text{m}$ + 3 $\mu\text{m}$ PART.<br>(900218) | ND                   | L                |                  |                 |      |                          |  |        |              |                       |                 |                 |

ND = No Detectable Toxicity

L = Low Toxicity

M = Moderate Toxicity

H = High Toxicity

TABLE 2

## DEFINITION OF TOXICITY CATEGORIES FOR HEALTH EFFECTS ASSAYS

| Assay <sup>a</sup> | Activity Measured <sup>b</sup>                  | Sample Type <sup>c</sup> | MAD <sup>d</sup> | Units    | Range of Concentration or Dosage |          |          |                     |
|--------------------|---|--------------------------|------------------|----------|----------------------------------|----------|----------|---------------------|
|                    |   |                          |                  |          | High                             | Moderate | Low      | Not Detectable (ND) |
| Ames               | MEC<br>(mutagenesis)                            | S                        | 5                | mg/plate | <0.05                            | 0.05-0.5 | 0.5-5    | ND at >5            |
|                    |   | AL, NAL                  | 200              | µl/plate | <2                               | 2-20     | 20-200   | ND at >200          |
|                    |   | E                        | 5000             | L/plate  | <50                              | 50-500   | 500-5000 | ND at >5000         |
| RAM                | EC <sub>50</sub><br>(lethality)                 | S                        | 1                | mg/ml    | <0.01                            | 0.01-0.1 | 0.1-1    | ND at >1            |
|                    |   | AL                       | 600              | µl/ml    | <6                               | 6-60     | 60-600   | ND at >600          |
|                    |   | NAL                      | 20               | µl/ml    | <0.2                             | 0.2-2    | 2-20     | ND at >20           |
|                    |   | E                        | 1000             | L/ml     | <10                              | 10-100   | 100-1000 | ND at >1000         |
| CHO                | EC <sub>50</sub><br>(lethality)                 | S                        | 1                | mg/ml    | <0.01                            | 0.01-0.1 | 0.1-1    | ND at >1            |
|                    |   | AL                       | 600              | µl/ml    | <6                               | 6-60     | 60-600   | ND at >600          |
|                    |   | NAL                      | 20               | µl/ml    | <0.2                             | 0.2-2    | 2-20     | ND at >20           |
|                    |   | E                        | 1000             | L/ml     | <10                              | 10-100   | 100-1000 | ND at >1000         |
| WAT                | LD <sub>50</sub><br>(lethality and toxic signs) | S                        | 5                | gm/kg    | <0.05                            | 0.05-0.5 | 0.5-5    | ND at >5            |
|                    |   | AL, NAL                  | 5                | ml/kg    | <0.05                            | 0.05-0.5 | 0.5-5    | ND at >5            |

<sup>a</sup>Standard test abbreviations are as follows:Ames: Ames Salmonella/microsome mutagenesis assay

RAM: Rabbit alveolar macrophage cytotoxicity assay

CHO: Rodent cell clonal toxicity assay

WAT: Acute in vivo test in rodents (whole animal test)<sup>b</sup>Standard abbreviations for measured endpoints are as follows:

MEC: Minimum effective concentration

EC<sub>50</sub>: Calculated concentration expected to produce effect in 50 percent of populationLD<sub>50</sub>: Calculated dose expected to kill 50 percent of population<sup>c</sup>S = Solid, AL = Aqueous liquid, NAL = Nonaqueous liquid, E = Extract and/or concentrate of unknown organic content (use equivalent volume of SASS train gas)<sup>d</sup>MAD = Maximum applicable dose

TABLE 3

HEALTH EFFECTS CRITICAL DATA SUMMARY FORM<sup>a</sup>

Contract No. EPA No. 68-02-3188 Technical Directive or Project No. LBI No. 20988 and 20993 Site Sampled HR, RA and DM  
 Acurex Subcontract No. RB 59178A  
 Release No. 6

| Sample Identification           | Ames Mutagenicity<br>[MEC] <sup>b</sup> | CHO Clonal Toxicity<br>[EC50] <sup>c</sup> | RAM Cytotoxicity [EC50] <sup>c</sup> |                 |     | Rodent Toxicity               |                   |                          |
|---------------------------------|---|--|--------------------------------------|-----------------|-----|-------------------------------|-------------------|--------------------------|
|                                 |   |  | Viability                            | Viability Index | ATP | ATP/Per 10 <sup>6</sup> Cells | LD50 <sup>d</sup> | Toxic Signs <sup>e</sup> |
| HR XAD-2 EXTRACT, INLET 819369  | 25 <sup>f</sup>                         | 11.5 <sup>f</sup>                          |                                      |                 |     |                               |                   |                          |
| HR XAD-2 EXTRACT, OUTLET 819370 | 100                                     | 18.4                                       |                                      |                 |     |                               |                   |                          |
| RA XAD-2 EXTRACT, TEST 1 819459 | 20                                      | 35.2                                       |                                      |                 |     |                               |                   |                          |
| RA XAD-2 EXTRACT, TEST 2 819465 | 137.5                                   | 9.35                                       |                                      |                 |     |                               |                   |                          |
| DM XAD-2 EXTRACT 900206         | 200                                     | 16.0                                       |                                      |                 |     |                               |                   |                          |
| RA BOTTOM ASH, TEST 1 819488    | >10000                                  | >1000 (4000)                               |                                      |                 |     |                               |                   |                          |
| RA BOTTOM ASH, TEST 2 819498    | >10000                                  | 1400                                       |                                      |                 |     |                               |                   |                          |
| RA CYCLONE ASH, TEST 1 819476   | 50                                      | >1000 (5000)                               |                                      |                 |     |                               |                   |                          |
| RA CYCLONE ASH, TEST 2 819504   | 500                                     | >1000 (1200)                               |                                      |                 |     |                               |                   |                          |
| DM FILTER + 1 μm PART. 900204   | >10000                                  | 140  |                                      |                 |     |                               |                   |                          |
| DM 10 μm + 3 μm PART. 900218    | >10000                                  | 450  |                                      |                 |     |                               |                   |                          |
|                                 |   |  |                                      |                 |     |                               |                   |                          |

<sup>a</sup>The assays, observed parameters and evaluation criteria are presented in IERL-RTP Procedures Manual; Level 1 Environmental Assessment Biological Tests, [EPA Contract No. 68-02-2681, Litton Bionetics, Inc., Kensington, Md.]

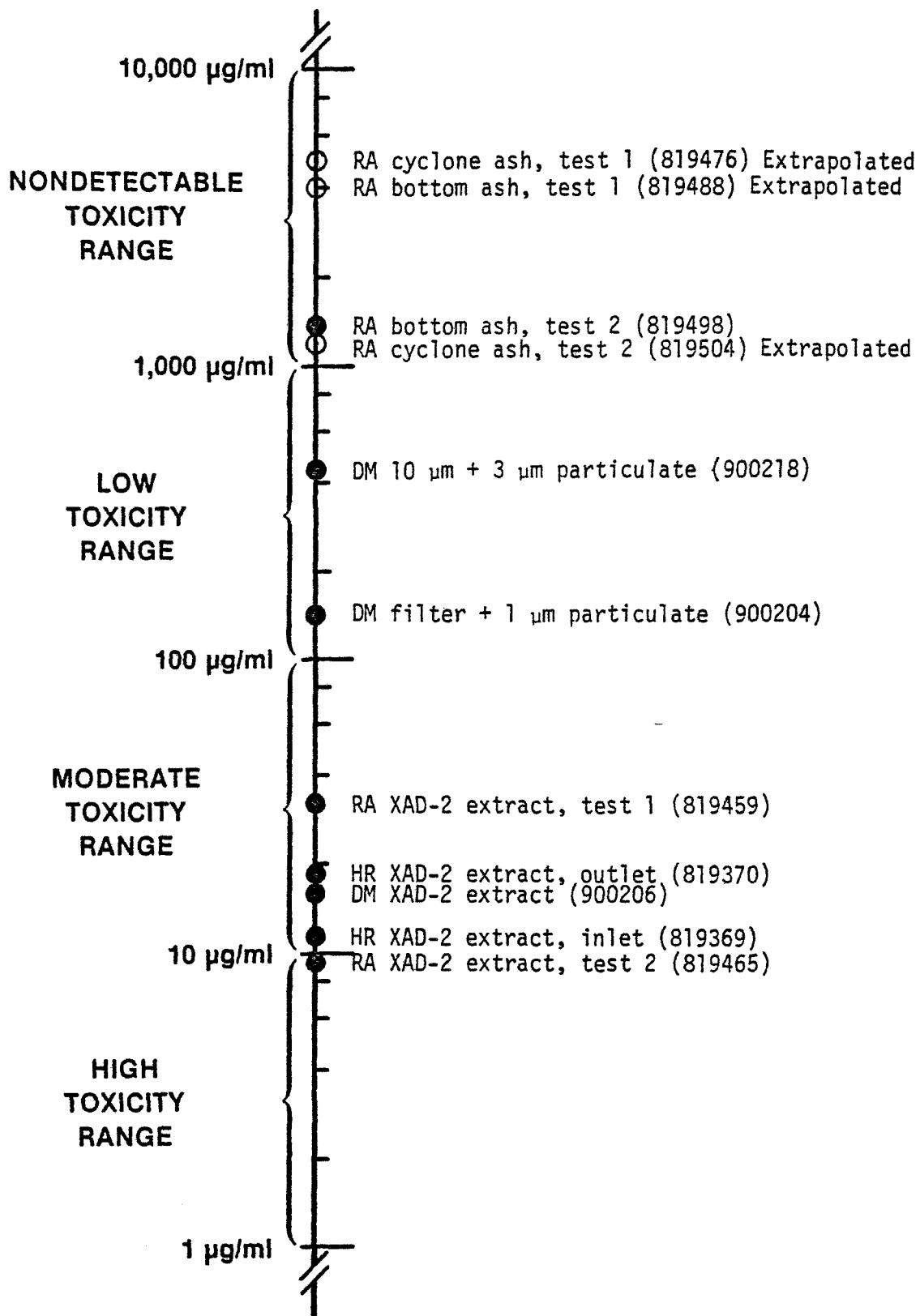
<sup>b</sup>MEC: Minimum Effective Concentration - Lowest concentration for any tester strain giving a mutagenic response.

<sup>c</sup>EC<sub>50</sub>: Effective concentration that reduces the observed parameter to 50 percent of the appropriate negative control.

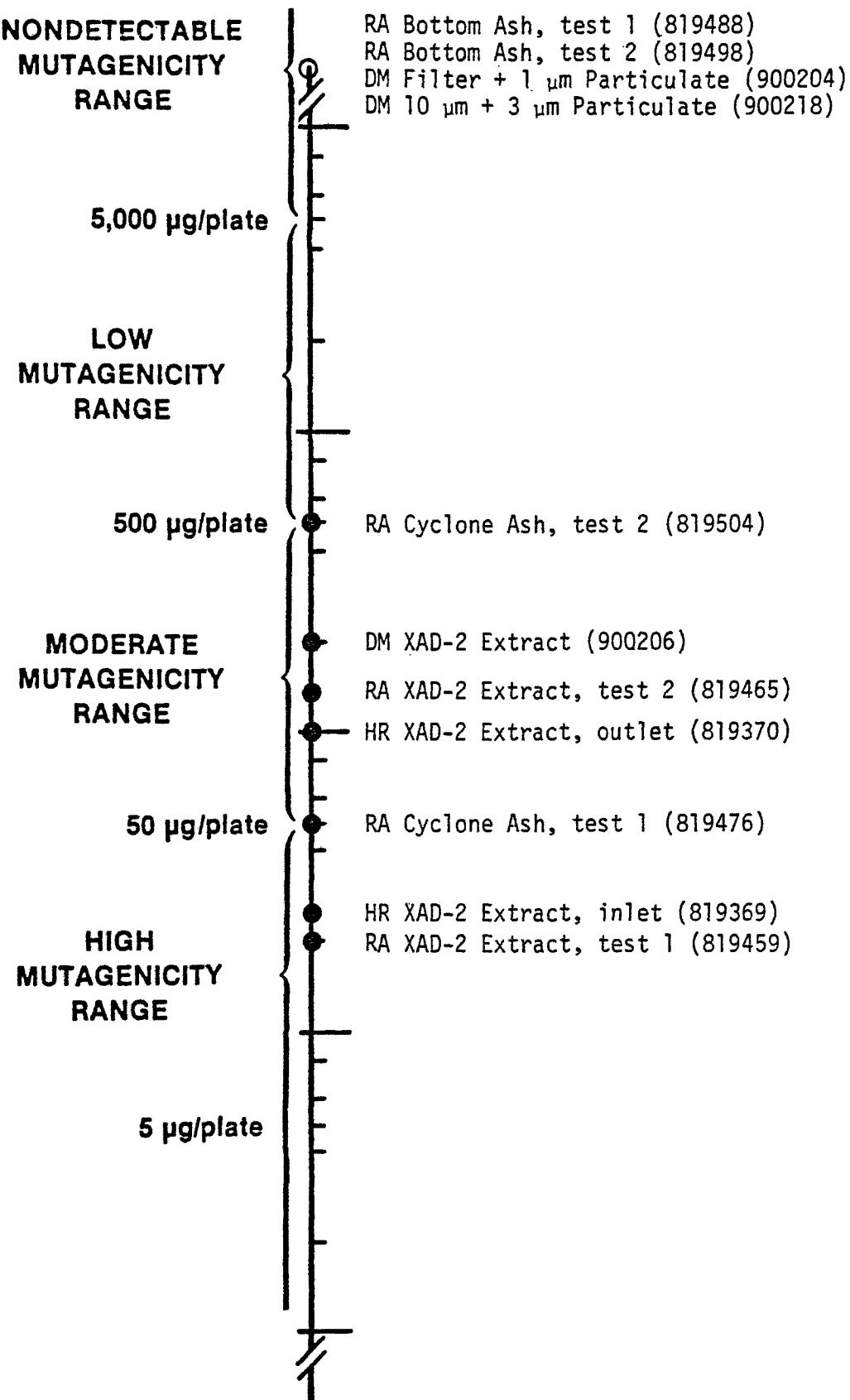
<sup>d</sup>LD<sub>50</sub>: The dose lethal to 50 percent of treated animals.

<sup>e</sup>Toxic signs are identified in a numbered list in the Level 1 manual. Only the number is reported here.

<sup>f</sup>Concentrations are μg organics per plate for Ames assay and per ml of culture medium for the CHO assay. Values in parenthesis are extrapolated values.



**Figure 1. Ranking of test material toxicity using EC<sub>50</sub> in EPA level 1 CHO clonal toxicity assay.**



**Figure 2. Ranking of test material mutagenicity using minimum effective concentration in EPA level 1 Ames mutagenesis assay.**

**TECHNICAL REPORT DATA**  
*(Please read instructions on the reverse before completing)*

|  |  |   |
|--|--|---|
| 1. REPORT NO.<br>EPA-600/7-86-011b   | 2.   | 3. RECIPIENT'S ACCESSION NO.                                |
| 4. TITLE AND SUBTITLE<br><b>Environmental Assessment of a Commercial Boiler Fired with a Coal/Waste Plastic Mixture; Volume II. Data Supplement</b>  |  | 5. REPORT DATE<br>April 1986                                |
| 7. AUTHOR(S)<br>R. DeRosier, H.I. Lips, and L.R. Waterland   |  | 6. PERFORMING ORGANIZATION CODE                             |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS<br>Acurex Corporation<br>Energy and Environmental Division<br>P.O. Box 7044<br>Mountain View, California 94039   |  | 10. PROGRAM ELEMENT NO.                                     |
|  |  | 11. CONTRACT/GANT NO.<br>68-02-3188                         |
| 12. SPONSORING AGENCY NAME AND ADDRESS<br>EPA, Office of Research and Development<br>Air and Energy Engineering Research Laboratory<br>Research Triangle Park, NC 27711  |  | 13. TYPE OF REPORT AND PERIOD COVERED<br>Final; 7/83 - 7/84 |
|  |  | 14. SPONSORING AGENCY CODE<br>EPA/600/13                    |
| 15. SUPPLEMENTARY NOTES AEERL project officer is Joseph A. McSorley, Mail Drop 65, 919/541-2920. Volume I contains the technical results.  |  |   |
| 16. ABSTRACT The report gives results of comprehensive emissions testing and laboratory analyses of a stoker-fired commercial boiler firing a coal/waste plastic mixture. In one test, the unit fired its typical coal fuel; in the other, shredded waste polyethylene terephthalate (PET) beverage bottles were added to the coal to about 16% by weight in the mixed fuel. NO <sub>x</sub> , total unburned hydrocarbon, and solid particulate were relatively unchanged for the two tests, as was the emitted particle size distribution. SO <sub>x</sub> emissions decreased with the coal/PET fuel in keeping with its lowered sulfur content; average CO emissions were also decreased. Flue gas emissions of most trace elements were comparable for both tests, as were the trace element compositions of corresponding ash streams. However, lead emissions were significantly increased for the coal/PET fuel, reflecting an increased lead content of the mixed fuel. The cyclone hopper ash for the coal/PET test had consistently lower leachable trace element and anion content than for the coal fuel test. Total flue gas organic emissions were comparable for both tests, in the 1 mg/dscm range; although levels of several semivolatile priority pollutants were higher for the mixed fuel. |  |   |
| 17. KEY WORDS AND DOCUMENT ANALYSIS  |  |   |
| a. DESCRIPTORS   | b. IDENTIFIERS/OPEN ENDED TERMS  | c. COSATI Field/Group                                       |
| Pollution<br>Assessments<br>Combustion<br>Coal<br>Plastics<br>Polyethylene Terephthalate   | Pollution Control<br>Stationary Sources<br>Environmental Assessment<br>Coal/Waste Fuel | 13B<br>14B<br>21B<br>21D<br>11I                             |
| 18. DISTRIBUTION STATEMENT<br>Release to Public  | 19. SECURITY CLASS (This Report)<br>Unclassified                                       | 20. SECURITY CLASS (This page)<br>Unclassified              |
|  | 21. NO. OF PAGES<br>203  | 22. PRICE   |