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AIRDOS-EPA: A Computerized Methodology for Estimating Environmental Concentrations and Dose to Man from Airborne Releases of Radionuclides

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AIRDOS-EPA: A Computerized Methodology for Estimating Environmental Concentrations and Dose to Man from Airborne Releases of Radionuclides

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ABSTRACT

The AIRDOS-EPA computer code is a methodology, designed for use on IBM-360 computers, that estimates radionuclide concentrations in air; rates of deposition on ground surfaces; ground surface concentrations; intake rates via inhalation of air and ingestion of meat, milk, and fresh vegetables; and radiation doses to man from airborne releases of radionuclides. This report describes the atmospheric and terrestrial transport models used in the code, their computer implementation, and the applicability of the code to the assessment of radiological impacts. A listing of the code and a demonstration run of the code are presented in the appendices.

A modified Gaussian plume equation is used to estimate both horizontal and vertical dispersion of as many as 36 radionuclides released from one to six stacks or area sources. Radionuclide concentrations in meat, milk, and fresh produce consumed by man are estimated by coupling the output of the atmospheric transport models with the U.S. Nuclear Regulatory Commission, Regulatory Guide 1.109 terrestrial food chain models. Dose conversion factors are input to the code, and doses to man at each distance and direction specified are estimated for total body, red marrow, lungs, endosteal cells, stomach wall, lower large intestine wall, thyroid, liver, kidneys, testes, and ovaries through the following exposure modes: (1) immersion in air containing radionuclides, (2) exposure to ground surfaces contaminated by deposited radionuclides, (3) immersion in contaminated water, (4) inhalation of radionuclides in air, and (5) ingestion of food produced in the area.

The code may be run to estimate highest annual individual dose in the area or annual population dose. For either option, output tables summarize doses by nuclide, exposure mode, and organ. Also, for either a square or circular grid option, ground concentrations of radionuclides and intake rates by man are tabulated for each environmental location. Working level exposures are also calculated and tabulated for inhalation of ^{222}Rn short-lived progeny. Run time is less than 5 min on the IBM 360/91, and the core requirement is 650 K (kilocore).

1. INTRODUCTION

The AIRDOS-EPA computer code was developed at Oak Ridge National Laboratory (ORNL) to be used by the U.S. Environmental Protection Agency (EPA) as part of a methodology to evaluate health risks to man from atmospheric radionuclide releases. This report describes the final version of an interim methodology outlined under Task I of Interagency Agreement No. EPA-78-D-X0394 between ORNL and the EPA. The models and parameters described in AIRDOS-EPA will be reviewed and reevaluated under Task II of this interagency agreement.

The code is a modified version of AIRDOS-II (Moore, 1977), which has been used by the Environmental Sciences Division (ESD) and the Health and Safety Research Division (HASRD) of ORNL for several years to assess radiological impacts of routine operations of nuclear facilities. Both point sources and uniform area sources of atmospheric releases of radionuclides can be evaluated by AIRDOS-EPA, which estimates (1) concentrations in air, (2) rates of deposition on ground surfaces, (3) ground surface concentrations, (4) intake rates by man via food ingestion and air inhalation, and (5) radiation doses received by man.

As many as 36 radionuclides released from one to six stacks or area sources can be handled in a single computer run. Annual-average meteorological data for the area surrounding a nuclear facility may be supplied as input to the code, which then estimates air and ground concentrations and intake rates by man for each radionuclide at various distances and directions from the release point or the center of an area source. From these values, doses to man at each distance and direction specified are estimated for total body, red marrow, lungs, endosteal cells, stomach wall, lower large intestine wall, thyroid, liver, kidneys, testes, and ovaries through each of five exposure modes. These modes are (1) immersion in air containing radionuclides, (2) exposure to ground surfaces contaminated by deposited radionuclides, (3) immersion in contaminated water, (4) inhalation of radionuclides in air, and (5) ingestion of food produced in the area. The dose calculations are made with the use of dose conversion factors supplied as input data for each radionuclide, exposure mode, and reference organ or tissue.

At the option of the user, the area surrounding the source may be subdivided either with a circular or a square grid. For the circular option, as many as 20 distances may be specified for each of 16 compass directions. Each distance represents the midpoint of a sector. The square option employs a 20 by 20 grid with the source at the center. The grid size is specified by the user.

The code may be run to estimate either the highest annual individual dose in the area or the annual population dose. For either of these options, tables are provided as output which summarize doses in several ways — by nuclide, exposure mode, and organ. Also, for either option selected, ground concentrations of radionuclides and intake rates by man are tabulated for each specified environmental location. In addition, working level exposures are calculated and tabulated for inhalation of ^{222}Rn and its short-lived progeny.

Section 2 of this report discusses the atmospheric and terrestrial transport of released radionuclides and the methods used for calculating the resultant dose to man from these radionuclides. Section 3 details the atmospheric and terrestrial transport models used in the code. Section 4 describes the input data requirements for the various user options. Section 5 lists terrestrial transport input parameters used in a demonstration run of the code. The methods used to determine the values presented are briefly discussed, and special problems in the determination of parameter values are identified. A listing of the code and a demonstration run of the code are presented in Appendix A and B, respectively.

2. APPLICABILITY OF THE COMPUTER CODE FOR ATMOSPHERIC DISPERSION CALCULATIONS AND RADIOLOGICAL ASSESSMENTS

Release rates (in curies per year) to the atmosphere from each point or area source are known collectively as the source term. The plume containing radionuclides is dispersed both horizontally and vertically as it is blown downwind. The code estimates the annual-average concentration (picocuries per cubic centimeter) of each radionuclide in the source term in air at ground level as a function of direction and distance from the source; annual-average frequencies of wind direction, wind speed, and atmospheric stability category are employed as input data.

Radionuclides in the form of particulates or reactive gases deposit on ground or water surfaces through scavenging processes, which primarily consist of washout by rainfall, and through dry deposition processes. The code estimates the deposition rate for each radionuclide in units of picocuries per square centimeter per second for each location for which estimated air concentrations are calculated.

Both the air concentrations and the ground deposition rates are average values in the crosswind direction over each of sixteen 22.5° sectors emanating from the source. For the square grid option, the 22.5° sector-averaged values in a circular coordinate system are converted to values in rectangular coordinates. Sector-averaging is a realistic treatment for assessments using average meteorological data, but the code does provide an option to the user to compute plume centerline values if desired for a special application. Plume centerline values are several times higher than sector-averaged values.

The average concentration of a radionuclide in air at ground level at an environmental location is used to estimate the external dose from gamma radiation to an individual living at that location for an entire year as a result of his immersion in an assumed semi-infinite cloud of that concentration. A conversion factor for immersion gamma dose at the skin surface is supplied as input data for each radionuclide. These values are multiplied by correction factors, also supplied as input, to estimate the external gamma dose contributions for each radionuclide to other reference organs.

The air concentration at each location is also used to estimate internal dose via inhalation. Input dose conversion factors (rem per microcurie) for each radionuclide and organ include contributions from radioactive daughters growing in after human intake, and, when multiplied by the intake for one year (microcuries), result in values for a dose commitment resulting from that annual intake.

Rates of deposition on ground surfaces are employed to estimate external doses resulting from gamma radiation emanating from contaminated ground. A period of time, supplied as input, is allowed for surface buildup. Doses are estimated for a point 1 m above an infinite plane with the calculated concentration in units of picocuries per square centimeter. Dose conversion is handled in the same way as for air immersion doses.

The external dose from water immersion is calculated as resulting only from immersion in water subjected to deposition from the atmosphere. It is usually estimated very conservatively in assessments, but even so it makes almost no contribution to the total doses. The critical pathway of exposure from water immersion is by swimming in a home outdoor swimming pool because the shallow depth of water in home pools minimizes dilution of deposited radionuclides. Dose calculation is similar to that for air immersion except that a use factor, often chosen as 0.01 in assessments, is employed to account for the fraction of time spent by a typical person in his home pool.

Ingestion doses resulting from deposition of radionuclides on crop land and pasture are estimated separately for vegetable, meat, and milk consumption. A terrestrial model described later in this report was adopted to estimate steady-state concentrations in these three food types for continuous deposition on agricultural land. Intake by man is calculated from input values assumed for daily consumption of each of the three types of food. Dose conversion factors (rem per microcurie) supplied as input data for each radionuclide and reference organ are used to calculate dose commitments resulting from one year's intake. Dose contributions from radioactive daughters growing in after intake are included in the dose conversion factors for each radionuclide assumed to be ingested.

The number of meat producing animals, dairy cattle, and square meters of area on which vegetable crops are produced is specified for each environmental location in the assessment region. When population doses are to be estimated for a site-specific assessment, any additional quantity (supplemental to locally produced supply) of each of the three food types required to feed the population is assumed to come from outside the assessment area in an uncontaminated state. Options in the code allow the user to specify the fraction of each food type produced at each individual's specific location, the fraction produced within the entire assessment area, and the fraction which is consumed within the area but produced outside the area.

No attempt is made in AIRDOS-EPA to assess either health risks or genetic damage. However, concentrations in air and on ground surfaces and intake rates by man, from which it may be possible to evaluate these effects, are calculated and tabulated for each environmental location for which doses are estimated.

3. ATMOSPHERIC AND TERRESTRIAL TRANSPORT MODELS AND THEIR COMPUTER IMPLEMENTATION

The general organization of the models as implemented in the subroutines of the code are described in detail in this section.

3.1 Organization of the Code

AIRDOS-EPA, written in Fortran-IV computer language, is designed to be run on the IBM-360 computers. It is organized as follows:

MAIN Program

1. SUBROUTINE CONCEN

   1.1 SUBROUTINE QY

1.1.1 SUBROUTINE QY1

1.1.2 SUBROUTINE QY2

1.1.3 SUBROUTINE QY3

1.2 SUBROUTINE QX

1.3 SUBROUTINE CHIQ

2. SUBROUTINE DIRECT

3. SUBROUTINE DOSEN

3.1 FUNCTION CV

3.2 SUBROUTINE RVALUE

3.3 SUBROUTINE DOSMIC

MAIN is a short program in which options are selected by the user to apply to subroutine CONCEN or subroutine DIRECT. CONCEN calculates and prints out concentrations in air and rates of deposition of radionuclides on ground surfaces from the source term supplied as input. Subroutine DIRECT may be called by MAIN to bypass CONCEN and to supply the above values directly as input.

If CONCEN is called by MAIN, the program can then be terminated, or alternatively, DOSEN will be called. If DIRECT is called by MAIN, DOSEN is then called.

Subroutine QY (and subroutines QY1, QY2, and QY3 called by QY) estimates depletion of radionuclide plumes as a result of dry deposition on ground surfaces. Subroutine QX is used for the same purpose except that it is used for the special cases in which gravitational fall of radionuclide particulates is significant.

Subroutine CHIQ calculates and prints a table of χ/Q values (the ratio of actual concentration in air to the release rate) for each radionuclide in the source term.

Subroutine DOSEN, employing concentrations in air and rates of deposition on ground surfaces calculated in CONCEN or input directly using DIRECT, calculates environmental concentrations, intake rates by man through ingestion and inhalation, and radiation doses. Function CV and subroutine RVALUE are used in the ingestion model of DOSEN.

Subroutine DOSMIC, called by DOSEN, summarizes doses and prints output tables.

3.2 Atmospheric Dispersion and Deposition

Subroutine CONCEN includes models used for plume rise above the top of a stack or roof vent through which radionuclides are released, the atmospheric dispersion model for dilution of radionuclides in an air-borne plume while being blown downwind, and models describing deposition processes. Parameter requirements for characterizing the nuclear facility or the site releasing radionuclides, meteorological data requirements, and a detailed description of atmospheric dispersion and deposition models are given below.

3.2.1 Input parameters characterizing the nuclear facility or release site

Input data for CONCEN must include the number of radionuclides (36 maximum) released from the facility, the name of each radionuclide as a representation with a maximum of eight alphameric characters (such as RN-222 for ^{222}Rn) and the annual-average release rate for each radionuclide in units of curies per year. The physical height of the release and the effective diameter for an area source must also be entered. For plume rise calculations based on the momentum of stack gases, the inside diameter of the stack (meters) and the velocity of the stack gases (meters per second) must be entered as input. Plume rise calculations based on buoyancy of hot stack gases requires that the heat release of the stack in calories per second be entered as input.

3.2.2 Meteorological data

The quality of meteorological data for assessment areas varies from that of great detail covering many years of observations taken at meteorological towers located near a site to the other extreme of very sparse information. In some cases, data from sites located some distance away must be used with modifications based on regional mapping of weather conditions. In any case, the data must be summarized in the specific form described below.

First, the annual frequency of wind direction must be determined for each of 16 compass directions starting at direction 1 for wind blowing *toward* due north and proceeding *counterclockwise* through direction 16. Meteorological data are usually presented for the direction *from* which the wind is blowing. The sum of the wind direction frequencies must equal 1.

Next, the frequency of each Pasquill stability category for each of the 16 wind directions must be determined. The extent of vertical and horizontal dispersion of a windblown plume is a function of the stability of the air. Pasquill (1961) described six atmospheric stability categories ranging from A (very unstable) to F (very stable). A seventh category, G (extremely stable), is included in AIRDOS-EPA. The sum of the frequencies for categories A through G will be equal to 1 for *each* of the 16 wind directions. Meteorological data are often not summarized by Pasquill category but instead may be grouped into categories denoted as stable, unstable, and neutral, or may be reported in terms of solar input or vertical temperature gradients. In such cases, conversion to the Pasquill system can be accomplished by reference to established guidelines (Turner, 1969; Slade, 1968).

The average wind speed must be determined for each wind direction and Pasquill category. Meteorological summaries usually present frequencies for various ranges of wind speeds from which the average can be derived. The atmospheric dispersion equation in the code has wind speed in the denominator, however, so a wind speed derived from the average of the reciprocals of wind speeds for the various ranges is used in AIRDOS-EPA as discussed in Sect. 3.2.4. A second set of wind speeds (reciprocal-averaged) must be calculated for each direction and Pasquill category.

The average depth of the atmospheric mixing layer (or lid) for the area must be included. The lid value, which is usually within the range 500 to 2000 m (Holzworth, 1972), is the distance from the ground to the bottom of a more stable layer of air lying above less stable air. The lid restricts the vertical dispersion of an airborne plume after it has travelled some distance downwind of the source. If a specific lid value is not available from site data, it may be estimated from contour maps (Slade, 1968; Holzworth, 1972). The average temperature in the area (°K) is required input if plume rise resulting from buoyancy of hot plumes is calculated by the code.

3.2.3 Plume rise

Gases discharged from a stack or roof vent will rise above the stack as a result of the momentum of the gas or, if the gases are substantially above ambient temperature, because of thermal buoyancy. This plume rise, Δh, when added to the actual physical height of the stack, h, results in an important parameter for dispersion calculations, H, which is referred to as the effective stack height. As a plume is blown downwind from a stack, its centerline, which starts out at the actual physical height of the stack, soon reaches an elevation of H, where it remains unless gravitational settling of particulates produces a downward tilt to the plume or until meteorological conditions change.

Plume rise calculations are subject to much uncertainty. Many equations have been proposed for predicting plume rise, but none has been entirely satisfactory (Turner, 1969). The user can elect, through an option in the main program, to use either the equation given by Rupp et al. (1948) to estimate plume rise for momentum dominated plumes, or to use Briggs' equations (1969) for hot plumes that rise because of buoyancy, or to supply his own values for plume rise.

The equation given by Rupp et al. for momentum dominated plumes is

$$\Delta h = 1.5\ vd/\mu \quad , \qquad (1)$$

in which

Δh = plume rise (m),

v = effluent stack gas velocity (m/sec),

d = inside stack diameter (m),

μ = wind velocity (m/sec).

The code treats buoyant plume rise according to Briggs' recommendations in the following way:

For stability categories A, B, C, and D, the equation used is

$$\Delta h = \frac{1.6\ F^{1/3}\ x^{2/3}}{\mu} \quad , \tag{2}$$

where

Δh = plume rise (m),

$F = 3.7 \times 10^{-5}\ Q_H$,

x = distance downwind (m),

μ = wind speed (m/sec).

The quantity Q_H is the heat emission from the stack due to the efflux of stack gases in calories per second.

Equation (2) is valid to a point where x is approximately equal to 10h, where the plume levels off. The equation used for values greater than 10h is

$$\Delta h = \frac{1.6\ F^{1/3}\ (10h)^{2/3}}{\mu} \quad . \tag{3}$$

Equation (2) is also used for stable categories E, F, and G to a distance $x = 2.4\ \mu S^{-1/2}$, beyond which the plume is assumed to level off. For higher values of x, the equation used is

$$\Delta h = 2.9\left(\frac{F}{\mu S}\right)^{1/3} \quad , \tag{4}$$

where S is the stability parameter defined as

$$S = \frac{g}{T_a}\left(\frac{\partial T_a}{\partial z} + \Gamma\right) \quad , \tag{5}$$

in which

g = the gravitational acceleration (m/sec^2),

T_a = air temperature (°K),

z = vertical distance above stack (m),

Γ = adiabatic lapse rate of atmosphere (0.0098°K/m) .

The value of the vertical temperature gradient, $\partial T_a/\partial z$, is positive for stable categories.

Equations for both momentum and buoyancy plume rise contain wind speed in the denominator, which obviously produces an unrealistic infinite plume rise for an absolute calm. Very low wind speeds (i.e., a relative calm) could produce unrealistically high values of plume rise. Inclusion of relative calms in averaging plume rise over a series of wind-speed categories can underestimate downwind pollutant concentrations. This is especially true for real meteorological conditions in which wind speed fluctuates considerably during downwind plume travel. An added factor is that the average plume rise is particularly sensitive to wind shear, $d\mu/dz$, at the low wind speeds, which would substantially reduce it from a value calculated using the wind speed at the actual release height. The true average wind speed for each Pasquill stability category is used in the code to estimate plume rise because it is always greater than the reciprocal-averaged wind speed, and therefore produces the most conservative (smallest) plume rise values. This procedure does not risk underestimating the significant contribution of relatively calm periods to downwind pollutant concentrations which could ensue from direct use of a plume rise based on each wind-speed category to be applied to dispersion calculations for that category.

There is, however, no completely satisfactory answer to the plume rise question which covers all meteorological or assessment conditions. For this reason, the option is available to compute plume rise by any other equation or under any other assumptions and to include a value in the input data to be used for each Pasquill atmospheric stability category. The user may use the Rupp equation with true average wind speeds for population dose calculations, for instance, but might wish to use even more conservative values for estimating the highest individual doses in the area to account for local turbulence created by building wakes. In other instances, roof vent releases may be subjected to the influence of other structures in the area so that the user may not wish to account for plume rise at all. In such cases, input values of zero would be used for plume rise. Negative values for plume rise can even be used in some cases to account for downwash, but the effective stack height, of course, should always be maintained above zero. For estimating concentrations of pollutants from buoyant plumes during periods of relative stagnancy (wind speed <1 m/sec), one can use Briggs' (1969) recommended equation for calms ($\Delta h = 5\ F^{1/4}\ S^{-3/8}$) to estimate specific input values for plume rise.

3.2.4 Plume dispersion

The basic equation used to estimate dispersion in an airborne plume as it is blown downwind from a stack is the Gaussian plume equation of Pasquill (1961) as modified by Gifford (1961).

$$\chi = \frac{Q}{2\pi\sigma_y\sigma_z\mu} \exp\left[-\frac{1}{2}\left(\frac{y}{\sigma_y}\right)^2\right]\left\{\exp\left[-\frac{1}{2}\left(\frac{z-H}{\sigma_z}\right)^2\right] + \exp\left[-\frac{1}{2}\left(\frac{z+H}{\sigma_z}\right)^2\right]\right\} \quad , \quad (6)$$

where

χ = concentration in air at x meters downwind, y meters crosswind, and z meters above ground (Ci/m^3),

Q = uniform emission rate from the stack (Ci/sec),

μ = mean wind speed (m/sec),

σ_y = horizontal dispersion coefficient (m),

σ_z = vertical dispersion coefficient (m),

H = effective stack height (physical stack height, h, plus the plume rise, (Δh) (m),

y = crosswind distance (m),

z = vertical distance (m).

The downwind distance x comes into Eq. (6) through σ_y and σ_z, which are functions of x as well as the Pasquill atmospheric stability category applicable during emission from the stack. The code converts χ in Eq. (6) and other plume dispersion equations from units of curies per cubic meter to units of picocuries per cubic centimeter.

Annual-average meteorological data sets usually include frequencies for several wind-speed categories for each wind direction and Pasquill atmospheric stability category. AIRDOS-EPA uses reciprocal-averaged wind speeds in the atmospheric dispersion equations, which permit a single calculation to replace separate calculations for each wind-speed category. This procedure saves much computer running time. The reciprocal averaged wind speed μ_r for each direction and Pasquill category is defined by the equation

$$\frac{1}{\mu_r} = \sum_{1}^{n} \frac{f_n}{\mu_n} \quad , \tag{7}$$

in which

f_n = fraction of time for wind-speed category n,

μ_n = average wind speed within the wind-speed category n (m/sec).

Equation (6) is applied to ground-level concentrations in air at the centerline of a plume by setting $y = 0$ and $z = 0$, which results in

$$\chi = \frac{Q}{\pi \sigma_y \sigma_z \mu} \exp\left[-\frac{1}{2}\left(\frac{H}{\sigma_z}\right)^2 \right] . \tag{8}$$

The average ground-level concentration in air over a sector of 22.5°, χ_{ave}, can be approximated by the following expression

$$\chi_{ave} = f\chi \quad , \tag{9}$$

where f is the integral of the exponential expression $\exp\left[-\frac{1}{2}\left(\frac{y}{\sigma_y}\right)^2 \right]$ in Eq. (6) from a value of $y = 0$ to $y = \infty$ divided by y_s, the value of y at the edge of the 22.5° sector, which is the value of the downwind distance, x, multiplied by the tangent of half of the sector angle. The expression is

$$f = \frac{\int_0^\infty \exp\left[-\left(\frac{0.5}{\sigma_y^2}\right) y^2 \right] dy}{y_s} . \tag{10}$$

The definite integral in the numerator of Eq. (10) is evaluated as

$$\sigma_y \sqrt{\frac{\pi}{2}} . \tag{11}$$

Since $y_s = x \tan (11.25°)$,

$$f = \frac{6.300836 \, \sigma_y}{x} . \tag{12}$$

The equation for sector-averaged ground level concentration in air is therefore

$$\chi = \frac{Q}{0.15871\ \pi x \sigma_z \mu} \exp\left[-\frac{1}{2}\left(\frac{H}{\sigma_z}\right)^2\right] \quad . \tag{13}$$

This method of sector-averaging compresses the plume within the bounds of each of the sixteen 22.5° sectors for unstable Pasquill atmospheric stability categories in which horizontal dispersion is great enough to extend significantly beyond the sector edges. It is not a precise method, however, because the integration over the y-axis, which is perpendicular to the downwind direction, x, involves increasing values for x as y is increased from 0 to ∞.

An average lid for the assessment area is provided as part of the input data. The lid is assumed not to affect the plume until x becomes equal to $2x_L$, where x_L is the value of x for which σ_z = 0.47 times the height of the lid (Turner, 1969). For values of x greater than $2x_L$, vertical dispersion is restricted and radionuclide concentration in air is assumed to be uniform from ground to lid.

The average concentration between ground and lid, which is the ground-level concentration in air for values of x greater than $2x_L$, may be expressed by

$$\chi_{ave} = \frac{\int_0^\infty \chi \, dz}{L} \quad , \tag{14}$$

where χ is taken from Eq. (6) and L is the lid height. The value of H in Eq. (6) may be set at zero since χ_{ave} is not a function of the effective stack height. The resulting simplified expression

$$\chi_{ave} = \frac{\int_0^\infty \frac{Q}{\pi\sigma_y\sigma_z\mu} \exp\left(-\frac{z^2}{2\sigma_z^2}\right)\exp\left(-\frac{y^2}{2\sigma_y^2}\right)dz}{L} , \tag{15}$$

may be evaluated for constant x and y values (σ_y and σ_z held constant) by using a definite integral similar to that in Eq. (11). The result is

$$\chi_{ave} = \frac{Q}{2.5066\ \sigma_y L\mu} \exp\left(-\frac{y^2}{2\sigma_y^2}\right). \tag{16}$$

One obtains the sector-averaged concentration at ground level by replacing the exponential expression containing y by f in Eq. (12):

$$\chi_{ave} = \frac{Q}{0.397825\ xL\mu} . \tag{17}$$

It should be noted at this point that for values of the downwind distance greater than $2x_L$, dispersion, as expressed in Eq. (17), no longer can be said to be represented by the Pasquill equation. The model is simply a uniform distribution within a rectangle of dimensions L and 2x tan (11.25°).

Equations (13) and (17) describe the usual case where radionuclides are dispersed downwind as gases or as particulates too small in size to be significantly affected by gravity during plume travel out to 80 to 160 kilometers.

Gravitational settling can be handled in the code, however, by tilting the plume downward after it has leveled off at a value of H by subtracting $V_g x/\mu$ from H in the plume dispersion equations. Values for V_g, the gravitational fall (or settling) velocity in meters per second, are provided as input data for each radionuclide in the source term. The subtracted expression, $V_g x/\mu$, represents the fall of particulates at x meters downwind. For most cases, $V_g = 0$, and the plume centerline remains at an elevation of H. Subtraction of $V_g x/\mu$ from H in Eq. (13) results in the following equation used for sector-averaged ground-level concentration of a radionuclide in air where gravitational settling is involved:

$$\chi = \frac{Q}{0.15871\ \pi x \sigma_z \mu} \exp\left[-\frac{1}{2}\left(\frac{H - V_g x/\mu}{\sigma_z}\right)^2\right] . \tag{18}$$

A problem arises, of course, if the value of $V_g x/\mu$ becomes greater than H because the centerline of the plume would be below ground level. This problem is solved in the code by a statement which sets the effective stack height equal to zero for all cases where $H - V_g x/\mu$ has a negative value.

3.2.5 Deposition Processes

Particulates and reactive or soluble gases may deposit on ground or water surfaces through two distinctly different processes: (1) dry deposition, and (2) scavenging. These are discussed in the following sections.

3.2.5.1 Dry deposition. Dry deposition is the process by which particles deposit on grass, leaves, and other types of surfaces by impingement, electrostatic interactions, or chemical reactions, or by which gases react chemically with surface components or dissolve in surface moisture.

The rate of deposition on earth surfaces is proportional to the ground-level concentration of the radionuclide in air (Slade, 1968),

$$R_d = V_d \chi \quad , \tag{19}$$

where

R_d = surface deposition rate (pCi/cm^2-sec),

χ = ground-level concentration in air (pCi/cm^3),

V_d = deposition velocity (cm/sec).

It should be stressed here that V_d is merely a proportionality constant even though it has units of velocity. Values of V_d must be obtained from field studies and wind tunnel experiments in which the ratio R_d/χ can be reliably determined. Care should be taken in selecting values for V_d to be sure that the values represent the total deposited radionuclide per unit of ground area and not just the quantity deposited on vegetation, which is often reported in the literature (Hoffman, 1977; Miller et al., 1978). If a radionuclide plume is treated as being tilted downward by gravitational settling, the deposition velocity for the radionuclide should be at least as great as its gravitational fall (or settling) velocity.

3.2.5.2 Scavenging. Scavenging of radionuclides in a plume is the process through which rain or snow removes particles or dissolves gases and deposits them on ground or water. The fraction of particles or soluble gases removed by scavenging from a vertical column of air per unit time during rain or snow is Φ, the scavenging coefficient, which has units of $second^{-1}$. The rate of deposition from scavenging is

$$R_s = \Phi \chi_{ave} L \quad , \tag{20}$$

where

R_s = surface deposition rate (pCi/cm^2-sec),

Φ = scavenging coefficient (sec^{-1}),

χ_{ave} = average concentration in vertical column up to lid height (pCi/cm^3),

L = lid height (cm).

The scavenging coefficient used for each radionuclide is the sum of scavenging coefficients for washout, rainout, and snowout for particles or the coefficient for dissolving gases in rain drops. The average concentration in the vertical column, χ_{ave}, is computed through use of Eq. (17). The scavenging coefficient is averaged over an entire year, which includes all periods during which rain or snow does not fall. The treatment of scavenging can be described, therefore, as a continuous removal of a fraction of the plume per second over an entire year.

The value for the total ground deposition rate, R_t, computed in subroutine CONCEN for each environmental location, is the sum of R_d and R_s.

3.2.6 Depletion of airborne plumes

Deposition on ground surfaces by dry processes, scavenging, and radioactive decay deplete the airborne plume as it is blown downwind from the release point. Depletion is taken into account by substituting a reduced release rate Q' for the original release rate designated by Q in Eq. (13) and (18) for each downwind distance x (Slade, 1968). For scavenging, the depletion fraction Q'/Q for each x value is the simple exponential expression

$$\frac{Q'}{Q} = e^{-\Phi t} \quad . \tag{21}$$

The value of t is the time in seconds that is required for the plume to reach a point x meters downwind.

The depletion fraction takes a much more complex form for dry deposition. Derivation of this depletion fraction (Van der Hoven, 1968) starts with Eq. (6), where z is set equal to zero for ground-level concentrations and the quantity $V_g x/\mu$ is subtracted from H for a tilted plume:

$$\chi(x, y, 0) = \frac{Q'}{\pi\sigma_y\sigma_z\mu} \exp\left[-\frac{(H - V_g x/\mu)^2}{2\sigma_z^2}\right] \exp\left(-\frac{y^2}{2\sigma_y^2}\right) . \qquad (22)$$

The rate of deposition on the ground is

$$w(x, y) = V_d\chi(x, y, 0) \quad . \qquad (23)$$

Depletion per unit distance downwind is

$$\frac{\partial Q'}{\partial x} = -\int_{-\infty}^{\infty} w(x, y)\, dy \quad . \qquad (24)$$

If we let A represent the exponential expression containing H and recognize symmetry, we now have

$$\frac{\partial Q'}{\partial x} = -2\int_0^{\infty} \frac{Q'V_dA}{\pi\sigma_y\sigma_z\mu} \exp\left(-\frac{y^2}{2\sigma_y^2}\right) dy \quad . \qquad (25)$$

The definite integral of Eq. (25) can be evaluated as

$$\frac{\partial Q'}{\partial x} = -\left(\frac{2}{\pi}\right)^{1/2} \frac{Q'V_dA}{\sigma_z\mu} \quad . \qquad (26)$$

Then, by integrating

$$\ln\left(\frac{Q'}{Q}\right) = -\left(\frac{2}{\pi}\right)^{1/2} \int_0^x \frac{V_d A}{\sigma_z \mu}\, dx \quad . \tag{27}$$

After substituting for A, the depletion fraction can then be represented by

$$\frac{Q'}{Q} = \exp\left\{-\left(\frac{2}{\pi}\right)^{1/2} \frac{V_d}{\mu} \int_0^x \frac{\exp\left[-\frac{(H - V_g x/\mu)^2}{2\sigma_z^2}\right]}{\sigma_z} dx\right\}, \tag{28}$$

for any value of downwind distance x.

The integral expression must be evaluated numerically. Values for the vertical dispersion coefficient σ_z are expressed as functions of x in the form x^D/F where D and F are constants with different values for each Pasquill atmospheric stability category.

Values for the quotient Q'/Q (the depletion fraction) for cases in which $V_g = 0$ are obtained from Subroutine QY, which is called from CONCEN. Subroutine QY obtains depletion fractions for the conditions $V_d = 0.01$ m/sec and $\mu = 1$ m/sec for each Pasquill stability category from the data storage subroutines QY1, QY2, and QY3. These storage subroutines contain values for release heights of 1, 1.5, 2, 3, 4, 5, 6, 7, 8, 9, 10, 12.5, 15, 17.5, 20, 25, 30, 35, 40, 50, 60, 70, 80, 90, 100, 120, 140, 160, 180, 200, 240, 260, 300, and 400 m and for the following downwind distances in meters: 35, 65, 100, 150, 200, 300, 400, 500, 650, 800, 1,000, 1,500, 2,000, 4,000, 7,000, 10,000, 25,000, 60,000, 90,000, and 200,000.

The stored depletion fractions were initially calculated numerically by use of a Simpson's rule computer subroutine. Linear interpolations by QY produce a fraction for the required x value, release height, and Pasquill category for $V_d = 0.01$ m/sec and $\mu = 1$ m/sec. Then, QY converts value to the appropriate value for the actual V_d and μ by use of the equation,

$$\left(\frac{Q'}{Q}\right)_2 = \left(\frac{Q'}{Q}\right)_1^{100\ V_d/\mu} \quad , \tag{29}$$

in which subscript 2 refers to the desired value and subscript 1 refers to the value for $V_d = 0.01$ m/sec and $\mu = 1$ m/sec.

Calculation of depletion fractions by QY through use of stored depletion fractions is a very fast computer process as compared with numerical integration, which would be required otherwise. If V_g, the gravitational fall velocity, is not zero, however, QY cannot be used. In this case, a Simpson's rule subroutine using numerical integration (Subroutine QX) is called by CONCEN to evaluate the depletion fractions.

For downwind distances greater than $2x_L$ where Eq. (16) applies to the ground-level concentration in air, the depletion per unit distance downwind is

$$\frac{\partial Q'}{\partial x} = -\int_{-\infty}^{\infty} \frac{V_d Q'}{2.5066\ \sigma_y L \mu} \exp\left(-\frac{y^2}{2\ \sigma_y^2}\right) dy \quad . \tag{30}$$

Integration is accomplished by using the definite integral

$$\int_0^\infty \exp\,(-a^2y^2)\;dy = \frac{\sqrt{\pi}}{2a} \quad , \tag{31}$$

where $a = 1/(\sqrt{2}\ \sigma_y)$. The resulting equation

$$d\ \ln Q' = -\frac{V_d}{L\mu}\ dx \quad , \tag{32}$$

when integrated from $2x_L$ to x produces the relationship

$$\frac{Q'_x}{Q'_{2x_L}} = \exp\left[-\ \frac{V_d(x - 2x_L)}{L\mu}\right] \quad , \tag{33}$$

in which Q'_x and Q'_{2x_L} are the reduced release rates at distances x and $2x_L$, respectively, for x values greater than $2x_L$. The depletion fraction at $2x_L$, Q'_{2x_L}/Q, obtained from Eq. (28) is multiplied by Q'_x/Q'_{2x_L} in Eq. (33) to give the depletion fraction at x, Q'_x/Q.

Use of a reduced release rate to estimate depletion by dry processes, referred to as the source depletion model, is a descriptively unrealistic treatment because it removes material from the entire vertical column, while, in fact, removal occurs only at the bottom of a plume. Proposed surface depletion models (Markee, 1967; Horst, 1977) have not come into general use, however, because of their computational complexities and because concentrations in air calculated from these models do not differ greatly from those calculated using source depletion for elevated releases and moderate deposition strength (Horst, 1977; Miller et al., 1978). The source depletion model as implemented in AIRDOS-EPA meets the important requirements of maintaining material balance as a plume is blown downwind of a source.

The depletion fraction for radioactive decay is

$$\frac{Q'}{Q} = e^{-\lambda_r t} \tag{34}$$

in which λ_r is the radioactive decay constant and t is the time required for plume travel. The decay constant used in CONCEN is referred to as the "effective decay constant" since it is not the true radiological decay constant for a radionuclide λ_i in all cases. For example, if a radionuclide is a short-lived daughter in equilibrium with a longer-lived parent, the effective decay constant for the daughter would be the true radiological decay constant of its parent.

The overall depletion fraction used in the code is the product of the depletion fractions for dry deposition, scavenging, and radioactive decay.

The atmospheric dispersion equations use the reciprocal-averaged wind speed μ_r but neither μ_r nor the true average wind speed μ_a can adequately be used to calculate reduced release rates to account for radiological decay and scavenging losses because averaging of exponential terms is required. An approximate calculational method used in AIRDOS-EPA for this purpose involves establishing three wind speeds (1 m/sec, μ_a m/sec, and 6 m/sec) to simulate the actual wind-speed spectrum for each specific wind direction and Pasquill category. The wind speeds 1 and 6 m/sec were chosen because they approximate the upper and lower bounds in most meteorological data sets.

If f_1, f_2, and f_3 are designated as the time fractions for wind speeds 1, μ_a, and 6 m/sec, respectively, then

$$f_1 + \mu_a f_2 + 6f_3 = \mu_a \quad , \tag{35}$$

$$f_1 + \frac{f_2}{\mu_a} + \frac{f_3}{6} = \frac{1}{\mu_r} \quad , \tag{36}$$

and

$$f_1 + f_2 + f_3 = 1 \quad . \tag{37}$$

Solving the above three simultaneous equations results in

$$f_2 = \frac{\frac{7}{6} - \frac{\mu_a}{6} - \frac{1}{\mu_r}}{\frac{7}{6} - \frac{\mu_a}{6} - \frac{1}{\mu_a}} \quad , \tag{38}$$

$$f_3 = \frac{(\mu_a - 1)(1 - f_2)}{5} \quad , \tag{39}$$

and

$$f_1 = 1 - f_2 - f_3 \quad . \tag{40}$$

The depletion fraction to account for radioactive decay is then approximated by

$$f_1 \exp\,(-\lambda_r x) + f_2 \exp\left[-\lambda_r\left(\frac{x}{\mu_a}\right)\right] + f_3 \exp\left[-\lambda_r\left(\frac{x}{6}\right)\right] \tag{41}$$

in which x is the downwind distance in meters and λ_r is the decay constant in units of seconds^{-1}. Similarly, the depletion fraction accounting for scavenging losses is

$$f_1 \exp\,(-\Phi x) + f_2 \exp\left[-\Phi\left(\frac{x}{\mu_a}\right)\right] + f_3 \exp\left[-\Phi\left(\frac{x}{6}\right)\right] \quad . \tag{42}$$

The overall depletion fraction is

$$\frac{Q'}{Q} = \left(\frac{Q'}{Q}\right)_{dry} \left\{ f_1 \exp\,(-\lambda_r x) + f_2 \exp\left[-\lambda_r\left(\frac{x}{\mu_a}\right)\right] + f_3 \exp\left[-\lambda_r\left(\frac{x}{6}\right)\right]\right\}$$

$$\left\{ f_1 \exp\,(-\Phi x) + f_2 \exp\left[-\Phi\left(\frac{x}{\mu_a}\right)\right] + f_3 \exp\left[-\Phi\left(\frac{x}{6}\right)\right]\right\} \qquad (43)$$

in which $\left(\frac{Q'}{Q}\right)_{dry}$ is the depletion fraction for dry deposition.

3.2.7 Values of parameters used in dispersion equations

The values of the horizontal and vertical dispersion coefficients, σ_y and σ_z (Table 1), used for dispersion calculations in CONCEN and to calculate depletion fractions in QY and QX are those recommended by G. A. Briggs of the Atmospheric Turbulence and Diffusion Laboratory at Oak Ridge, Tennessee (Gifford, 1976). These values, which are different functions of the downwind distance x for each of the Pasquill stability categories A through F, are used in the code as the functions $\sigma_y = x^{A}/C$ and $\sigma_z = x^{D}/F$ to facilitate integrations over x. The parameters A, C, D, and F for each Pasquill atmospheric stability category and specific ranges of x are stored in a data statement. Pasquill category G (extremely stable) was added to the code. Values for σ_y and σ_z for category G were derived by subtracting half of the difference between values for categories E and F from the values for F for each downwind distance.

Reciprocal-averaged wind speeds for each wind direction and Pasquill category are used for μ values in the dispersion equations instead of the true average values because μ is in the denominator of the equations. The process of averaging over a series of ranges of wind speeds actually involves averaging a series of terms containing the factors $1/\mu_1$, $1/\mu_2$, $1/\mu_3$, etc.

Table 1. Formulas recommended by Briggs[a] for σ_y and σ_z for open-country conditions[b]

Pasquill type	σ_y (m)	σ_z (m)
A	$0.22\ x\ (1 + 0.0001\ x)^{-1/2}$	$0.20\ x$
B	$0.16\ x\ (1 + 0.0001\ x)^{-1/2}$	$0.12\ x$
C	$0.11\ x\ (1 + 0.0001\ x)^{-1/2}$	$0.08\ x\ (1 + 0.0002\ x)^{-1/2}$
D	$0.08\ x\ (1 + 0.0001\ x)^{-1/2}$	$0.06\ x\ (1 + 0.0015\ x)^{-1/2}$
E	$0.06\ x\ (1 + 0.0001\ x)^{-1/2}$	$0.03\ x\ (1 + 0.0003\ x)^{-1}$
F	$0.04\ x\ (1 + 0.0001\ x)^{-1/2}$	$0.016\ x\ (1 + 0.0003\ x)^{-1}$

[a]G. A. Briggs, Air Resources Atmospheric Turbulence and Diffusion Laboratory National Oceanic and Atmospheric Administration, Oak Ridge, Tennessee.

[b]Values of x are downwind distances in meters.

3.2.8 χ/Q tabulations

The value χ/Q is the actual concentration of the radionuclide in air at ground level divided by the release rate of the radionuclide. Subroutine CHIQ called from CONCEN calculates χ/Q values and prints a table for each radionuclide listing χ/Q values in seconds per cubic meter for each of the 16 compass directions for the specific downwind distances (from 1 to 20) supplied as input. The χ/Q values are not calculated if the assessment area is a square grid.

3.2.9 Area sources

At the option of the user, the source can be a finite area with the reference point for the grid system at its centroid. Radionuclides are assumed to be released uniformly throughout the area. The method used to estimate environmental concentrations resulting from area releases is a modification by Christopher B. Nelson (EPA) of the method described by Mills and Reeves (1973) and implemented by Culkowski and Patterson (1976).

The method consists basically of transforming the original area source into an annular segment with the same area. This transformation is dependent on the distance between the centroid of the area source and the receptor. At large distances the transformed area source approaches a point source at the origin while at distances very close to the centroid it becomes a circular source centered at the receptor.

The principle of reciprocity is used to calculate the effective χ/Q. That is, the problem is equivalent to interchanging source and receptor and calculating the mean χ/Q from a point source to one or more sector segments according to the angular width of the transformed source. The mean value of χ/Q for each sector segment is estimated by calculating χ/Q at the distance which would provide the exact value of the mean if the variation in χ/Q were proportional to $r^{-1.5}$ for distances from the point source to locations within the sector segment. The χ/Q for the entire transformed source is the sum of the χ/Q values for each sector weighted by the portion of the total annular source contained in that sector.

Point-source χ/Q values for a typical annual-average meteorology were found to be nearly identical to those for a circular area source with a diameter of 718 m at distances greater than 1600 m from its center. For this reason, the code includes a statement providing default to point-source treatment if the ratio of downwind distance to source diameter exceeds 2.5.

Any uncertainties in the area-source treatment stemming from the assumption that χ/Q is proportional to $x^{-1.5}$ or other assumptions in the model are applicable only to locations near the edge of an area source. Comparisons were made of calculated concentrations in air at ground level with values calculated by AREAS (Moore, 1978), an area-source code based on entirely different principles, which was developed to evaluate widely dispersed pollutant sources within a 20 by 20 square grid system. A 718-m diameter circular area was used. Agreement was within 10% at distances greater than 600 m from the edge of the area source. The AREAS values were 20% higher at 330 m and 90% higher at 100 m from the edge.

The differences found within a few hundred meters from the edge of the source may not be relevant, however, because, the AREAS values represent averages over a square grid. The average can differ substantially from the actual value for a receptor point located in a region of rapidly changing χ/Q. Nevertheless, caution should be exercised when applying the area-source treatment where the ratio of distance from the center to the diameter of a source is less than ∿1.3.

3.2.10 Limitations of the dispersion treatment

The AIRDOS-EPA treatment of dispersion uses the Gaussian plume equation. This equation is an empirical formula which is based on an analytical solution to the diffusion equation under the restrictive assumptions of constant wind speed, no wind shear, flat topography, Fickian diffusion, and no chemical or physical interactions of plume components during plume travel. The parameters σ_y and σ_z are not defined explicitly by the mathematical assumptions of the model. They must be determined empirically. The Gaussian plume equation has shown considerable success under ideal field test conditions. However, dispersion in plumes is increased by surface roughness caused by buildings, hills, and other environmental factors. Thermal sources present in urban areas also increase dispersion. The meteorological data employed in an assessment near a source for which these factors are significant should reflect this increased atmospheric instability.

There is a lower limit of applicability of the Pasquill equation with respect to wind speed. Dispersion is treated only in crosswind and vertical directions and is ignored in the downwind direction. Consequently, χ unrealistically approaches ∞ as wind speed approaches zero. The contribution of periods of relative calm, which significantly affect average pollutant concentrations, may therefore be overestimated. Wind speeds much less than 1 m/sec should probably not be used in dispersion estimates.

The ideal plume described by the Pasquill equation often does not exist under real atmospheric conditions. Instantaneous changes in wind direction, and updrafts and downdrafts produced by terrain features and other meteorological changes produce significant deviations from the ideal plume. Many of these deviations average out, however, when the equation is used to estimate average concentrations of pollutants released continuously from a source.

The dispersion treatment in AIRDOS-EPA assumes a continuous plume extending indefinitely outward from the source in a single direction with a single wind speed and atmospheric stability. Fractional contributions to downwind concentrations in each compass direction are based on frequencies of wind speed and stability category. Realistically, however, wind speed and direction often fluctuate almost continuously, and the atmospheric stability will ultimately change as a plume is blown downwind. Also, deviations from site-specific annual-average meteorology can be expected at locations beyond a few miles from the plant site.

These limiting factors as applied to dose assessments can be resolved into two components: (1) factors affecting estimation of the highest individual dose in the area, and (2) factors affecting population dose estimates. The highest individual doses are usually close to the release point — at the plant boundary at distances from the source of perhaps 800 to 1000 m or less for low-level releases or at distances of only a few thousand meters for elevated releases. The Gaussian model as applied to annual-average meteorology using sector averaging is generally regarded as applicable over these short distances. Uncertainties arise mainly because of possible air turbulence or downdrafts created by buildings and other structures in the immediate plant area. Correction for building effects can be accomplished in a conservative manner by reducing the effective stack height.

Population dose assessments depend largely on estimated concentrations at greater distances. Uncertainties arising specifically from the use of the Pasquill equation are eliminated at distances far enough downwind that vertical dispersion is restricted by the lid. At such distances sector-averaged dispersion is simply calculated as proportional to the area of a rectangle with dimensions of the lid height and the cross-section distance. The most serious question here concerns deviations from site-specific meteorology, particularly with respect to frequencies of wind direction. For a relatively uniform population distribution, population dose estimates should be fairly reliable to the extent that atmospheric dispersion is involved. On the other hand, if a heavily populated area lies far out from the source, but within the assessment area and contributes substantially to the calculated population dose, a correction may have to be made for changes in frequencies of wind direction.

Lid heights are not known precisely, and they vary greatly from season to season and even change greatly from daylight to dark and vice versa when solar input changes. Uncertainties in lid values can result in dose uncertainties for those downwind distances great enough that vertical dispersion is restricted by the lid. This would not usually affect areas close to the plant where the highest individual dose will be received but may affect population dose to some extent. The treatment in the code would seem to overestimate concentrations at all distances somewhat, however, by not considering lid penetration. This effect can occur at certain times, such as in early morning, when a low lid lying just above the top of a stack is penetrated by the stack gases. Pollutants can be blown out of the area under these conditions without dispersing downward at all. Conditions for lid penetration are infrequent at most sites. Ignoring the effect, therefore, probably does not greatly affect dose estimates, but it does impart a small degree of conservatism to the calculations.

3.2.11 Direct input of concentrations in air and rates of deposition on ground surfaces (subroutine DIRECT)

Environmental concentrations, intake rates by man, and radiation doses can be calculated in AIRDOS-EPA from concentrations in air and ground deposition rates provided directly as input to the code by specifying OPTION (1) = 2 in MAIN. Subroutine DIRECT is called by this option, which bypasses CONCEN, the atmospheric dispersion subroutine. Data required for DIRECT are (1) integers specifying the lower and upper bounds of the assessment area; (2) SQSD, as also required in CONCEN; (3) the specific downwind distances (IDIST values) for the circular option; (4) S_e (SEQWL), the assumed fraction of equilibrium for ^{222}Rn short-life progeny used for working level (WL) calculations; (5) number of radionuclides (NNUCS); and (6) a data set for each radionuclide consisting of the name of the radionuclide, its deposition velocity, and its scavenging coefficient, followed by 400 air concentrations in a 20 by 20 array and 400 ground deposition rates in the same format. Tables of the input data are printed listing air concentrations, and the dry, wet, and total deposition rates. These data are used in DOSEN to calculate doses, environmental concentrations, and rates of intake by man.

3.3 Calculations of Radiation Doses, Environmental Concentrations, and Intake Rates by Man

Subroutine DOSEN, called from the main program, estimates doses, concentrations, and intake rates at specified environmental locations through the use of ground-level concentrations in air and ground deposition rates computed in Subroutine CONCEN or provided directly as input. Doses are estimated for 11 organs including total body. Modes of exposure described below are (1) immersion in air, (2) exposure to ground surfaces contaminated by deposited radionuclides, (3) immersion in water such as by swimming in a backyard pool, (4) inhalation of air containing radionuclides, and (5) ingestion of food produced on contaminated land.

3.3.1 Air immersion doses

The equation used for estimating external doses from immersion in air containing gamma emitting radionuclides is

$$D_{imm} = (1.0 \times 10^{-6})(8760)\ \chi\ C_{imm} \quad , \qquad (44)$$

in which

D_{imm} = air immersion dose (rem/year),

χ = ground-level concentration of the radionuclide in air (pCi/cm^3),

C_{imm} = dose conversion factor for immersion in an infinite cloud ($rems\text{-}cm^3/\mu Ci\ hr$),

1.0×10^{-6} = $\mu Ci/pCi$,

8760 = hr/year.

The code receives a skin dose conversion factor as input data for each radionuclide for infinite cloud exposure. This skin dose conversion factor is multiplied in the code by an external dose correction factor (FROG) for total body and each reference organ, also supplied as input data for each radionuclide.

Equation (44) applies to environmental locations at which the airborne plume has essentially reached ground level. It can, however, overestimate doses near a low-level release because of the small vertical spread of the plume under these conditions. On the other hand, Eq. (44) can underestimate dose for overhead plumes at locations close to the stack where χ may be very low, but where the individual may be irradiated from above. A case in point would be a release of energetic gamma emitters from a tall stack of a plant with a close-in plant boundary. For such a case, a separate calculation should be made for dose from the overhead plume, and this dose should be added to the immersion dose calculated by Eq. (44).

3.3.2 Surface exposure doses

Dose due to gamma emissions from radionuclides deposited on ground surfaces is estimated by

$$D_{surf} = (1.0 \times 10^{-6})(8760)R_t \frac{1 - \exp(-\lambda_T t)}{\lambda_T} (86400)C_{surf} \quad , \qquad (45)$$

where

D_{surf} = dose from surface exposure (rems/year),

R_t = surface deposition rate (pCi/cm^2-sec),

λ_T = radioactive decay constant λ_r + environmental decay constant λ_w (day^{-1}),

t = time allotted for surface buildup (days),

C_{surf} = dose conversion factor for surface exposure to an infinite plane at a point 1 m above ground (rems-cm^2/ μCi hr),

1.0×10^{-6} = μCi/pCi,

8760 = hr/year,

86400 = sec/day,

Input data includes a skin surface dose conversion factor which is multiplied in the AIRDOS-EPA code by external dose correction factors (FROG) for total body and reference organs.

The expression in Eq. (45),

$$R_t \frac{1 - \exp(-\lambda_T t)}{\lambda_T} (86400) \quad , \tag{46}$$

represents the surface concentration in picocuries per square centimeter after a buildup time of t days. There is very little available information on environmental removal rates from ground surfaces, so a value of zero is usually used for the environmental decay constant. The value of λ_T then would be simply the radiological decay constant.

3.3.3 Water immersion doses

Doses resulting from immersion in water subjected to deposition of radionuclides from the atmosphere are estimated similarly to those resulting from air immersion. The ultimate concentration of a radionuclide in a body of water is inversely proportional to its depth, so swimming in a shallow body of water such as a backyard swimming pool is taken as representing the most significant exposure pathway for water immersion. Water immersion doses are included in DOSEN for completeness but normally do not contribute significantly to total dose even though assumed parameters for assessments are usually very conservative.

The equation is

$$D_{wimm} = (1.0 \times 10^{-6})(8760)\,\frac{R_t}{d}\,\frac{1 - \exp(-\lambda_T t)}{\lambda_T}\,(86400)\,C_{wimm}\ , \qquad (47)$$

in which

D_{wimm} = water immersion dose (rem/year),

R_t = surface deposition rate (pCi/cm^2-sec),

d = depth of water (cm),

λ_T = radioactive decay constant λ_r + environmental decay constant for water λ_w (day^{-1}),

t = time allotted for buildup in water (days),

C_{wimm} = dose conversion factor for immersion in a body of water of infinite dimensions (rems-cm^3/μCi-hr),

1.0×10^{-6} = μCi/pCi,

8760 = hr/year,

86400 = sec/day .

3.3.4 Inhalation doses

The following equation is used to estimate inhalation dose at each environmental location:

$$D_{inh} = (1.0 \times 10^{-6})(8760)\,\chi\,B_r C_{inh}\ , \qquad (48)$$

where

D_{inh} = inhalation dose (rem/year),

χ = ground-level concentration of the radionuclide in air (pCi/cm^3),

B_r = breathing rate (cm^3/hr),

C_{inh} = dose conversion factor for inhalation (rem/μCi),

1.0×10^{-6} = μCi/pCi,

8760 = hr/year.

The C_{inh} values are dose commitment resulting from the initial intake of 1 μCi for the radionuclide. These dose conversion factors should include contributions of radioactive daughters growing in after the intake of the parent nuclide.

3.3.5 Ingestion doses

Doses to the various organs from the ingestion of radionuclides other than ^3H (tritium) and ^{14}C are calculated from radionuclide concentrations in food and annual consumption rates for individuals or populations. Radionuclide concentrations in meat, milk, and vegetables are calculated through implementation of models described in U.S. Nuclear Regulatory Commission (NRC) Regulatory Guide 1.109 (1977). The models are described below by Pleasant (1979).

3.3.5.1 Concentrations in and on vegetation. Radioactive material concentrates in vegetation as a result of deposition onto the plant foliage and from uptake of activity initially deposited on the ground. The following equation is used for estimating the concentration $C_i^v(r, \theta)$ in picocuries per kilogram of nuclide i in and on vegetation at the location (r, θ):

$$C_i^v(r, \theta) = d_i(r, \theta) \left\{ \frac{R[1 - \exp(-\lambda_{Ei} t_e)]}{Y_v \lambda_{Ei}} + \frac{B_{iv}[1 - \exp(-\lambda_i t_b)]}{P \lambda_i} \right\} \exp(-\lambda_i t_h), \tag{49}$$

where

$d_i(r, \theta)$ = the deposition rate of radionuclide i onto ground at location (r, θ), in pCi/m^2-hr ($d_i(r, \theta) = 3.6 \times 10^7 R_t$);

R = the fraction of deposited activity retained on edible portions of crops, dimensionless;

λ_i = the radioactive decay constant of nuclide i, in hr^{-1};

λ_{Ei} = the effective removal rate constant for radionuclide i from crops, in hr^{-1}, where $\lambda_{Ei} = \lambda_i + \lambda_w$, and λ_w is the removal rate constant for physical loss by weathering;

t_e = the time period that crops are exposed to contamination during the growing season, in hr;

Y_v = the agricultural productivity (yield), of the edible portion of vegetation in kg/m^2;

B_{iv} = the concentration factor for uptake of radionuclide i from soil by edible parts of crops, in pCi/kg per pCi/kg dry soil;

t_b = the period of long-term buildup for activity in soil, in hr;

P = the effective density of the top 15 cm of soil, in kg(dry soil)/m^2;

t_h = a holdup time that represents the time interval between harvest and consumption of the vegetation, in hr.

In the AIRDOS-EPA code, when Eq. (49) is used to calculate C_i^V for pasture grasses, Y_{v1} and B_{iv1} values based on dry weight, are used for Y_v and B_{iv}. When the equation is used for fresh produce ingested by man, fresh weight values Y_{v2} and B_{iv2} are used. In addition a washing factor DD1 is multiplied by the first term of Eq. (49) to account for removal of surface-adhered radionuclides during processing of food consumed by man.

The above model has several conceptual limitations. The model may overestimate radionuclide concentrations in vegetation via root uptake because the model assumes that radiological decay is the only removal process from the soil. However, harvesting of vegetable crops, grazing of pasture grasses, erosion of soil, and leaching of radionuclides in percolating water may also remove radionuclides from the root zone soil. The model may also underestimate radionuclide concentrations in vegetation because radionuclides initially deposited on vegetation surfaces may be incorporated directly into the plant matrix and not be completely removed by environmental processes. Additionally, the model does not attempt to simulate daughter buildup in the vegetation. A method to account for daughter buildup in the AIRDOS-EPA code will be discussed elsewhere in this report.

3.3.5.2 Concentrations in milk. The concentration of radionuclide i in milk depends upon the amount and contamination level of the feed consumed by the animal. The concentration of radionuclide i in the animal's feed is calculated by use of the equation

$$C_i^V(r, \theta) = f_p f_s C_i^p(r, \theta) + (1 - f_p f_s) C_i^s(r, \theta), \tag{50}$$

where

$C_i^V(r, \theta)$ = the concentration of radionuclide i in the animal's feed, in pCi/kg;

$C_i^p(r, \theta)$ = the concentration of radionuclide i on pasture grass [calculated using Eq. (49) with $t_h = 0$], in pCi/kg;

$C_i^S(r, \theta)$ = the concentration of radionuclide i in stored feeds [calculated using Eq. (49) with t_h = 2160 hr (90 days)], in pCi/kg;

f_p = the fraction of the year that animals graze on pasture,

f_s = the fraction of daily feed that is pasture grass when the animals graze on pasture.

Using the value of $C_i^V(r, \theta)$ calculated by use of this equation, the concentration of radionuclide i in milk is estimated as

$$C_i^M(r, \theta) = F_m C_i^V(r, \theta) Q_F \exp(-\lambda_i t_f) \ , \tag{51}$$

where

$C_i^M(r, \theta)$ = the concentration in milk of nuclide i, in pCi/liter;

$C_i^V(r, \theta)$ = the concentration of radionuclide i in the animal's feed, in pCi/kg;

F_m = the average fraction of the animal's daily intake of radionuclide i which appears in each liter of milk, in days/liter;

Q_F = the amount of feed consumed by the animal per day, in kg/day;

t_f = the average transport time of the activity from the feed into the milk and to the receptor;

λ_i = the radiological decay constant of nuclide i, in days^{-1}.

3.3.5.3 Concentrations in meat. The radionuclide concentration in meat depends upon the amount and contamination level of the feed consumed by the animal, as in the milk pathway. Using the value of $C_i^V(r, \theta)$ as calculated in Eq. (50), the radionuclide concentration in meat is estimated as

$$C_i^F(r, \theta) = F_f C_i^V(r, \theta) Q_F \exp(-\lambda_i t_s) \ , \tag{52}$$

where

$C_i^F(r, \theta)$ = the concentration of nuclide i in animal flesh, in pCi/kg;

F_f = the fraction of the animal's daily intake of nuclide i which appears in each kilogram of flesh, in days/kg;

$C_i^V(r, \theta)$ = the concentration of radionuclide i in the animal's feed, in pCi/kg;

Q_F = the amount of feed consumed by the animal per day, in kg/day;

λ_i = the radiological decay constant of nuclide i, in days^{-1};

t_s = the average time (days) from slaughter to consumption.

For concentration in beef, it is assumed that beef cattle are on open pasture for the same grazing periods as given for milk cattle.

3.3.5.4 Calculation of annual organ doses. The following equation is used to calculate the annual dose committed to organ j of an individual resulting from ingestion of all radionuclides other than ^3H and ^{14}C in produce, milk, meat, and leafy vegetables.

$$D_j^D(r, \theta) = \sum_i DFI_{ij}[U^V f_g C_i^V(r, \theta) + U^M C_i^M(r, \theta) + U^F C_i^F(r, \theta) + U^L f_\ell C_i^L(r, \theta)] \; , \quad (53)$$

where

$D_j^D(r, \theta)$ = the annual dose committed to organ j of an individual from dietary intake of atmospherically released radionuclides

DFI_{ij} = the dose conversion factor for the ingestion of nuclide i for organ j in millirem/pCi;

U^V, U^M, U^F, U^L = the ingestion rates of produce (nonleafy vegetables, fruit, and grains), milk, meat, and leafy vegetables, respectively, for individuals;

f_g = the fraction of produce ingested grown in garden of interest;

f_ℓ = the fraction of leafy vegetables grown in garden of interest.

The terms in Eq. (53) containing $C_i^V(r, \theta)$, $C_i^M(r, \theta)$, $C_i^F(r, \theta)$, and $C_i^L(r, \theta)$ represent the dose to organ j from ingestion of produce, milk, meat, and leafy vegetables, respectively. Equations (51) and (52) are used to calculate $C_i^M(r, \theta)$ and $C_i^F(r, \theta)$, respectively. Equation (49) is used to calculate $C_i^V(r, \theta)$; the values used for the parameters t_e, Y_v, and t_h are those appropriate for produce consumed by man. Similarly Eq. (49) is used to calculate $C_i^L(r, \theta)$ with parameter values t_e, Y_v, and t_h chosen so as to be appropriate for leafy vegetables consumed by man.

Dose conversion factors for dose commitments resulting from an annual intake of a radionuclide are provided as input to the code in units of rem per microcurie and are converted to units of millirem per picocurie for use in Eq. (53). The dose conversion factors should include contributions by both the radionuclides and its daughters growing in after intake. Doses resulting from ingestion of produce and leafy vegetables are combined in DOSEN and designated simply as vegetable doses.

Input data required for calculation of ingestion doses include number of meat producing animals, number of dairy cattle, and area (square meters) of vegetable crop production for each environmental location. The area of land associated with an environmental location is the grid area if the 20 by 20 square grid option is used. For the circular option, the area is that of the portion of a 22.5° sector having the environmental location at its central point. Population data for each location are included for population dose calculations.

Various possible assumptions with regard to food sources can be handled within the code. For each of the three types of food, a number is included in the input data that specifies the ratio

$$A/(A + B) \tag{54}$$

in which

A = quantity ingested which is produced at the individual's environmental location, and

B = quantity ingested whose source represents an average produced over the assessment area.

Another number for each food type specifies the *minimum* fraction the individual ingests that comes from outside the assessment area altogether and that is assumed to contain no radionuclides. The fraction imported for each type of food may be calculated by the code and can be greater than this minimum value if needed to meet the nutritional requirements for the population. The user can exercise an option, however, to fix the minimum value so that it will not be exceeded under any conditions.

If it were desired not to consider ingestion at all, each of the three minimum fractions imported could be set at 1.0. For calculations of the maximum individual dose in the area, it is usually desirable to set and fix the minimum fraction to be imported at zero. If the ratios defined in Eq. (54) each have values of 1.0, complete availability of each of the three food types produced at the individual's specific location is assumed in the code regardless of input values used for numbers of meat producing animals and dairy cattle or area of vegetable crop production.

3.3.6 Calculations for special cases

If a radionuclide interacts with environmental components in a unique fashion, it must be treated as a special case. Tritium (^{3}H) and ^{14}C are given special treatment in Subroutine DOSEN because the stable forms of these elements constitute significant fractions of the elemental composition of the human body and man's food and drink. Transport processes within soil, plants, cattle, and man which apply to trace quantities of radionuclides do not necessarily apply to cases where the corresponding stable elements are present in such quantities that saturation effects are significant.

If tritium (T) is released to the atmosphere as HT or T_2, atoms of T may exchange with hydrogen atoms in water molecules in the air, and we may wish to treat the plume as though it contained HTO initially. The tritium may then be assumed to follow water almost precisely through the environment. For this reason doses from drinking water are included for tritium. Rather than attempting to relate the doses to the ground deposition rate, it is assumed that doses from ingestion of food and drinking water at an environmental location are proportional to tritium concentration in the air (Killough and McKay, 1976).

The total ingestion dose from tritium if the source of all of an individual's food and drinking water is assumed to be at his specific environmental location is

$$D_t = C_f \chi + C_w \chi \qquad (55)$$

where

D_t = total ingestion dose (rem/year),

C_f = dose conversion factor for food (rem-cm^3/pCi-year),

C_w = dose conversion factor for drinking water (rem-cm^3/pCi-year),

χ = ground-level concentration of tritium in air at an environmental location (pCi/cm^3).

For the purpose of summarizing in the code the food ingestion pathways for all radionuclides in a source term, the tritium ingestion dose from food is artificially broken down into ingestion doses from vegetables (D_v), meat (D_b), and milk (D_c). The total food ingestion dose from tritium (D_t) is equal to the sum of D_v, D_b, and D_c. The equations used in the code are

$$D_v = 0.505\ C_f(f_{v1}\chi + f_{v2}\chi_v) \quad , \tag{56}$$

$$D_b = 0.185\ C_f(f_{b1}\chi + f_{b2}\chi_b) \quad , \tag{57}$$

$$D_c = 0.310\ C_f(f_{c1}\chi + f_{c2}\chi_c) \quad , \tag{58}$$

where

D_v, D_b, and D_c = tritium food ingestion dose from vegetables, meat, and milk, respectively (rem/year),

χ_v = average ground-level concentration of tritium in air over the assessment area weighted by quantities of vegetables produced as a function of location,

χ_b = as above for χ_v except applied to meat,

χ_c = as above for χ_v except applied to milk,

f_{v1} = fraction of vegetable intake which is produced at individual's environmental location,

f_{v2} = fraction of vegetable intake whose source represents an average produced over the assessment area,

f_{b1} = as above for f_{v1} except applied to meat,

f_{b2} = as above for f_{v2} except applied to meat,

f_{c1} = as above for f_{v1} except applied to milk,

f_{c2} = as above for f_{v2} except applied to milk,

0.505 = the fraction of C_f for vegetable ingestion,

0.185 = the fraction of C_f for meat ingestion,

0.310 = the fraction of C_f for milk ingestion.

The total-body dose conversion factor for ingestion is 8.3×10^{-5} rem per microcurie (Killough et al., 1978). This number is used to derive the value of C_f, based on the specific activity of tritium in atmospheric moisture with an average specific humidity of 8 grams of H_2O per cubic meter of air (Killough and McKay, 1976). If tritium in food is in equilibrium with atmospheric tritium and man consumes 1638 g of water daily in his food, C_f is 6.18 rem-cm^3/pCi-year. The C_w value for an assumed daily drinking water intake of 1512 g is 5.70 rem-cm^3/pCi-year. This value should be used, however, only if the source of each individual's drinking water is assumed to be at his specific environmental location. For all other cases, C_w should be reduced to account for dilution by distant sources.

The code breaks down the food ingestion dose from tritium into percentage contributions of 50.5% from vegetables, 18.5% from meat, and 31.0% from milk. The percentages are based on approximate water contents of foods: 82.4% for vegetables, 62.3% for meat, 87.5% for milk (Moore, 1977), for daily intakes of 0.532 kg of vegetables, 0.258 kg of meat, and 0.307 kg of milk (Rupp, 1979).

Tritium is the only radionuclide in a source term in which the total dose estimated to derive from vegetables, meat, and milk may not equal the total ingestion dose. The difference is the dose from drinking water.

Tritium doses via inhalation of air and skin absorption are estimated by the code and added to the dose estimated to be received via ingestion. The dose conversion factor for inhalation of air containing tritium includes a contribution for skin absorption from air.

If ^{14}C is released in the form of CO_2, it will mix with atmospheric CO_2, and become available for plant photosynthesis. Cattle grazing on pasture will take in ^{14}C in grass, and then man will receive it in milk and beef. Factors in a data statement are used in the code to multiply by the concentration of ^{14}C in air to obtain an ingestion dose for each reference organ. These dose conversion factors, listed in Table 2, are based on specific activity calculations for ^{14}C in body tissues in equilibrium with atmospheric ^{14}C (Killough and Rohwer, 1978).

Nearly all of the ^{14}C doses come from ingestion. Breakdown by the three food pathways is accomplished by estimating carbon intakes for meat, milk, and vegetables. The weight of total carbon intake per day is approximated by the relations (Moore, 1977)

$$W_v = 79.96\ V \ , \tag{59}$$

$$W_b = 238.16\ T_b \ , \tag{60}$$

$$W_c = 68.9\ T_c, \text{ and} \tag{61}$$

$$W_t = W_v + W_b + W_c \ , \tag{62}$$

where

W_v, W_b, W_c, and W_t = weight of daily carbon intake via vegetables, meat, milk, and total intake, respectively

Table 2. Dose conversion factors for ^{14}C

Organ	Dose conversion factors[a] ($rem\text{-}cm^3/pCi\text{-}year$)
Whole body	1.16×10^3
Red marrow	2.03×10^3
Lungs	5.07×10^2
Endosteal cells	1.85×10^3
Stomach wall	7.43×10^2
Lower large intestine wall	8.92×10^2
Thyroid	5.27×10^2
Liver	7.30×10^2
Kidneys	6.49×10^2
Testes	4.46×10^2
Ovaries	4.46×10^2

[a]These factors are based on the assumption that the specific activity in human tissue is equal to the average steady state value in the atmosphere (Killough and Rohwer, 1978).

V = daily vegetable consumption (kg),

T_b = daily meat consumption (kg),

T_c = daily milk consumption (liters).

Normalization is accomplished by using weight fractions of ^{14}C for each food type in the dose equations:

$$D_v = CF_v\ (f_{v1}\chi + f_{v2}\chi_v) \quad , \tag{63}$$

$$D_b = CF_b\ (f_{b1}\chi + f_{b2}\chi_b) \quad \text{, and} \tag{64}$$

$$D_c = CF_c\ (f_{c1}\chi + f_{c2}\chi_c) \quad , \tag{65}$$

where D_v, D_b, and D_c = ingestion dose for ^{14}C from vegetables, meat, and milk (rem/year);

C = dose conversion factor for ^{14}C (rem-cm^3/pCi-year);

F_v = weight fraction of ^{14}C from vegetables (W_v/W_t);

F_b = weight fraction of ^{14}C from meat (W_b/W_t);

F_c = weight fraction of ^{14}C from milk (W_c/W_t);

f_{v1} = fraction of vegetable intake which is produced at individual's environmental location;

f_{v2} = fraction of vegetable intake whose source represents an average produced over the assessment area;

f_{b1} = as above for f_{v1} except applied to meat;

f_{b2} = as above for f_{v2} except applied to meat;

f_{c1} = as above for f_{v1} except applied to milk;

f_{c2} = as above for f_{v2} except applied to milk;

χ = ground-level concentration of ^{14}C in air at individual's environmental location (pCi/cm^3);

χ_v = average ground-level concentration of ^{14}C in air over the assessment area weighted by quantities of vegetables produced as a function of location;

χ_b = as above for χ_v except applied to meat;

χ_c = as above for χ_v except applied to milk.

The total dose from ^{14}C is the sum of D_v, D_b, and D_c.

3.3.7 Environmental concentrations and intake rates

Health risks to man as a result of radiation exposures are not directly related to dose commitments, but are more closely correlated with environmental concentrations and rates of intake of radionuclides by ingestion and inhalation. To facilitate health risk estimations, DOSEN calculates and prints tables of the following for each radionuclide and specified environmental location: (1) concentration in air (curies per m^3); (2) ground concentration (curies per m^2), (3) ingestion intake rate (picocuries per year), and (4) inhalation intake rate (picocuries per year). In addition, these values are written as unformatted output so that they may be used as input data for computer assessments of health risks.

3.3.8 Working level calculations for ^{222}Rn

Working level (WL) is calculated for ^{222}Rn and its short-life progeny at each specified environmental location. One WL is defined as any combination of short-life progeny (^{218}Po, ^{214}Pb, ^{214}Bi, and ^{214}Po) in one liter of air that will release 1.3×10^5 MeV of alpha particle kinetic energy during decay to ^{210}Pb. The equation used (Evans, 1969) is

$$WL = 0.01\ S_e C \qquad (66)$$

in which

C = concentration of ^{222}Rn in air (pCi/liter),

0.01 = conversion factor,

S_e = assumed fraction of equilibrium for short-life progeny.

The value of S_e is input in CONCEN as SEQWL. The default value is 0.7. Calculations of WL and printing of tables are done in subroutine DOSMIC.

3.3.9. Buildup of radioactive daughters on surfaces after deposition of a parent radionuclide

A radionuclide building up on ground surfaces or in water as a result of the deposition of its parent may contribute to doses from surface exposure, water immersion, and food ingestion. To calculate this effect, the daughter should be added to the source term with a zero release rate if it is not also released to the atmosphere at the source. Input parameters for the daughter are supplied as follows: I1, I2, I3, I4, and I5 (integer indices for one to as many as five parent radionuclides in the source term) and F1, F2, F3, F4, and F5 (buildup factors for each parent). The F factor is defined as the surface input rate of the daughter from parent decay per unit aerial deposition rate of the parent.

The total surface input rate from buildup of a daughter is the sum of the products of each F value multiplied by the aerial deposition rate of the parent. This sum added to the aerial deposition rate of the daughter, d_i, is d_{ieff}, the effective surface input rate.

The value of d_{ieff} is used to calculate surface and water concentrations after buildup time t_b. The use of d_{ieff} for ingestion intake is more complicated and requires the use of a modified version of Eq. (49) for calculating the concentration $C_i^V(r, \theta)$ of a nuclide in and on vegetation. The appropriate equation is

$$C_i^V(r, \theta) = d_i(r, \theta) \frac{R[1 - \exp(-\lambda_{Ei} t_e)]}{Y_v \lambda_{Ei}} +$$

$$d_{ieff}(r, \theta) \; B_{iv} \frac{[1 - \exp(-\lambda_i t_b)]}{P\lambda_i} \; \exp(\lambda_i t_h) \quad . \qquad (67)$$

4. USE OF THE CODE

Options available to the user and data requirements are described below.

4.1 Options Available to the User

4.1.1 Options in the main program (MAIN)

The options available in MAIN are applied to subroutines CONCEN and DIRECT. Option (1) specifies the flow of the code. If option (1) = 0, CONCEN is called to estimate concentrations of the radionuclides in air and rates of deposition on ground surfaces, and then subroutine DOSEN is called to calculate doses to man, environmental concentrations, and intake rates. If option (1) = 1, however, the program is terminated after completion of the calculations in CONCEN. If it is desired to calculate doses and intake rates directly from input values of radionuclide concentrations in air and ground deposition rates, option (1) is specified as 2. MAIN will then call subroutine DIRECT, which reads the required input data, and then it will call DOSEN.

Option (2) determines whether a square grid environmental configuration [option (2) = 0] or a circular configuration [option (2) = 1] are used in the assessment.

Option (3) determines whether the values calculated by CONCEN will represent averages over sectors of 22.5° [option (3) = 0] or will represent the centerline of a plume [option (3) = 1].

Option (4) determines how plume rise is calculated. If option (4) = 0, Briggs' equations for buoyant plumes are used. If option (4) = 1, Rupp's equation for momentum-type emissions is used. Specific values for plume rise for each Pasquill atmospheric stability category can be entered as input data if option (4) is specified as 2.

Option (5) allows the user to vary the deposition velocity of each radionuclide in the source term with the direction and distance from the plant. This option is invoked if option (5) = 1 and if the circular configuration [i.e., option (2) = 1] is used.

Option (6) is an integer value from 0 to a maximum of 36 which specifies the number of radionuclides in the source term for which concentrations in air and rates of deposition on ground surfaces are punched on cards. For example, if option (6) = 4 and there are 16 radionuclides in the source term, concentrations and deposition rates will be punched for the first four radionuclides in the list.

Option (7) is specified as 1 if the radionuclides in the source term are assumed to be released uniformly from a circular area such as from a tailings pile of a uranium mill. The reference point for environmental locations is the center of the circular area. If option (7) = 0, a point release is assumed.

The user can eliminate the printing of the main output table of CONCEN, which lists estimated concentrations in air and ground deposition rates in the environment, by setting option (8) = 1. If option (8) = 0, then the table is printed.

A table of χ/Q values for each radionuclide in the source term is normally printed by subroutine CHIQ called by CONCEN if the assessment area is circular, but the user can eliminate these tables from the output by setting option (9) = 1. If option (9) = 0, then the tables are printed.

Details of options selected in MAIN are given below.

4.1.1.1 The circular option. For this option, the area around the plant is divided into sixteen 22.5° sectors emanating from the release point. The midpoint of each sector is one of sixteen compass directions numbered 1 through 16 starting with direction 1 for due north and proceeding counterclockwise to NNE for direction 16. As many as 20 distances are entered as input data to represent midpoints of environmental locations for all sectors.

The parameter SQSD in Subroutine CONCEN sets the length of a side of each of the 400 grid squares for the square grid option discussed in Sect. 4.1.1.2. A value for this parameter must also be selected for the circular option because it is used in the code in a statement testing the importance of radiological decay during plume travel. The SQSD value should be approximately equal to 0.1 of the radius of the circular assessment area.

4.1.1.2 The square grid option. If the square grid option is selected in the main program, the code will estimate concentrations in air and ground deposition rates at the midpoints of each of 400 square grids in a 20 by 20 array with the release point located at the center. The array is aligned north-south and east-west with the abscissa numbers going from 1 to 20 from west to east and with the ordinate numbers going from 1 to 20 from south to north. An input parameter SQSD sets the length of the side of each of the 400 grid squares.

The code computes concentrations by starting at grid (1, 1) and proceeds through grid (1, 20), and then goes to (2, 1), proceeds to (2, 20), and continues this process through grid (20, 20). For each grid square, the center of the square is identified as within one of 16 sectors emanating from the release point by reference to a data statement within the computer code. The compass directions at the midpoints of each of these 22.5° sectors are numbered from 1 to 16 starting with 1 for due north and proceeding counterclockwise through direction 16. Downwind distance is calculated from the grid identifiers and the value of SQSD.

The very poor resolution for the area near the plant afforded by the preceding procedure is improved within the computer code by recomputing concentrations for the innermost 16 grid squares. This 16-grid area is converted into a 20 by 20 grid; the concentration in each of the 16 inner grid squares is then computed as the average value for 25 uniformly distributed smaller grid squares.

The square grid configuration has an advantage over the circular configuration in that the environmental areas are more compact and, hence, are more amenable to discrete characterization. A more important consideration, however, is that concentration values in a square grid arrangement can be more readily adapted to multiple point source or area source assessments.

4.1.1.3 Option for varying deposition velocity. An input value for dry deposition velocity is entered for each radionuclide in the source term. In a normal computer run, this value is used to estimate the rate of dry deposition of the radionuclide on ground or water surface and the resulting depletion of the plume for all directions and distances from the plant. This procedure is adequate for areas with relatively uniform environmental characteristics, but it may be inaccurate for areas consisting of a wide variety of surfaces such as tall grass, forests, or lakes. There may be as much as an order of magnitude difference in deposition velocity between bare soil and forest canopy (Sehmel et al., 1973), for example, and this may lead to considerable differences in air concentrations downwind of a forest versus a bare-soil region.

To assess non-uniform areas more realistically, the user of the code may elect through option (5) to use a different value for deposition velocity for each environmental location identified by direction and distance from the plant. This option is available only for the circular configuration [i.e., option (2) = 1] because integration of plume depletion equations must proceed outward from the plant for each direction and cover each environmental location in stepwise fashion. For this option, multiplier parameters for each environmental location specified by direction and distance and upper and lower bounds for distances must be added to the input data. The deposition velocity for each radionuclide within a specific environmental location is the product of the initial deposition velocity entered for the radionuclide and the multiplier for the location.

4.1.1.4 The area source option. For this option, the source is assumed to be an area such as a tailings pile with a uniformly distributed rate of release of radionuclides. The dispersion treatment is described in Sect. 3.2.9. The diameter in meters of a circle of the same area as the source must be entered as input in CONCEN to use this option. If this value is less than 10 m, however, the area source is treated as a point source.

4.1.2 Optional features of subroutine CONCEN

The first data input of CONCEN are specifications of lower and upper bounds for grid abscissa and ordinate as integer values for NOL, NOU, NRL, and NRU. Normally, for the square grid option, the abscissa limits are NOL = 1 and NOU = 20, going from west to east, and the ordinate limits are NRL = 1 and NRU = 20, going from south to north. The user can, however, specify higher values for NOL and NRL or lower values for NOU and NRU for special applications. Integers for NOL to NOU are column numbers, and integers for NRL to NRU are row numbers. The circular option requires that NOU must not exceed 16 as an upper bound for column numbers because only 16 compass directions are involved. The numbering starts at NOL = 1 for due north and proceeds counterclockwise to 16 for NNE. The row numbers for the circular option (NRL to NRU), which may range from 1 to 20, refer to distances in meters from the source, which are supplied by the user as integer values of the IDIST input parameter.

If the square grid option is selected in the main program, the grid size is specified in CONCEN as the value SQSD, the length of the side of the grid squares in meters. A value of 8000 m for SQSD produces a square assessment area superscribing a circle with a radius of 50 miles.

For the circular configuration, the number of distances from the plant in each compass direction (IDIST values) should be equal to the value of NRU.

The assessment area for which doses and intake rates are calculated in DOSEN is identical to that defined by the bounds set in CONCEN. The agricultural and population input data entered in DOSEN in 20 by 20 arrays should contain 0 values for all elements of these arrays lying outside the bounds of the assessment area.

4.1.3. Options and optional features of subroutine DOSEN

The first input data for DOSEN are six options. The first, LIPO, is a specification as to whether the calculations are to be made for the maximally exposed individual (LIPO = 0) or for the population in the area (LIPO = 1).

The second option (NNTB) determines the number of tables to be printed listing doses by grid location, exposure mode and organ by individual radionuclide. Each of these tables is lengthy, and it is usually desirable to minimize the printed output by specifying NNTB = 0.

Doses by radionuclide, organ, and pathway are punched on cards if option (3), NRTB, is specified as 1. If NRTB = 0, punching of these values is omitted.

If option (4), NSTB, is 1, concentrations in air, ground concentrations, ingestion intake rates, and inhalation intake rates by man for each environmental location for each radionuclide except ^{222}Rn are printed and written as unformatted output. If NSTB = 0, output of these values is omitted. Working levels for ^{222}Rn are outputted if NSTB = 1 and omitted if NSTB = 0.

The fifth and sixth options, NTTB and NUTB, control calculations and printing by DOSMIC. Dose summary tables are printed if NTTB = 1 and omitted if NTTB = 0. Working levels for ^{222}Rn are calculated and tabulated if NUTB = 1 but omitted if NUTB = 0.

In addition to the six specified options above, there are several options available to the user for treating ingestion. The parameters RVEG, RBEF, and RMLK for vegetables, meat, and milk specify the ratio of the quantity of each type of food ingested by a person that is produced at his environmental location to the sum of that produced at his location and the quantity that he ingests that is produced throughout the entire assessment area. The radionuclide content of each of the three food types produced throughout the entire assessment area is a weighted average over the grid system. The assessment area is bounded by the integers NOL, NRL, NOU, and NRU in a 20 by 20 grid system. Therefore, quantities of food produced (and human population) should be listed as 0 for all locations lying outside of these bounds.

The *minimum* fractions of each of the individual's intake of each food type that comes from outside of the assessment area altogether, and assumed to be uncontaminated, are specified as F3VEGM, F3BEFM, and F3MLKM. The code can compute a higher imported fraction for each food type if required to meet nutritional requirements as specified in the input data. The user can fix the minimum imported fractions to be *actual* fractions by setting IMPFIX = 1.

Fallout interception fractions for pasture grasses and fresh vegetables consumed by man are designated R1 and R2, respectively. These factors are applied to all radionuclides, but may be optionally changed for any specific radionuclide by setting IFLAG, normally 0, at 1 or 2. If IFLAG = 1, special parameters RD1 and RD2 are used instead of R1 and R2. If IFLAG = 2, RD1 and RD2 are used for dry deposition, and RW1 and RW2 are used for wet deposition.

4.2 Data Input and Example Run

The listing of the AIRDOS-EPA COMPUTER CODE IN Appendix A identifies the order and format of the input parameters in the READ statements and their corresponding FORMAT statements. Parameter names and their definitions and units are listed in Tables 3, 4, 5, and 6 for the main program and subroutines CONCEN, DIRECT, and DOSEN, respectively. Table 7 lists the parameters from these tables with their data card formats.

Appendix B is the output of an example run of the code.

Table 3. Input parameters for main program

Name	Number of values	Definition	
WORD	1	the word OPTIONS	
OPTION	9	<u>Option (1)</u>	0 to run the entire code
			1 if it is desired to run only subroutine CONCEN
			2 if subroutine DIRECT is to be called instead of CONCEN
		<u>Option (2)</u>	0 for the 20 by 20 square grid configuration
			1 for the circular configuration
		<u>Option (3)</u>	0 for sector-averaged computations
			1 for plume centerline computations
		<u>Option (4)</u>	0 to compute plume rise for buoyant plumes using Briggs' equations
			1 to compute plume rise for momentum-type emissions by Rupp's equation
			2 to use specific values for plume rise entered as input data for each Pasquill atmospheric stability category
		<u>Option (5)</u>	0 if deposition velocity is not varied with direction and distance for each radionuclide
			1 if deposition velocity varies with direction and distance [may only be used if option (2) = 1]
		<u>Option (6)</u>	An integer from 0 to 36 specifying the number of radionuclides in the source term for which air concentrations and ground deposition rates are punched on cards

Table 3. (continued)

Name	Number of values		Definition
		Option (7)	0 for point-source atmospheric dispersion calculations
			1 for calculations for a uniform circular area source
		Option (8)	0 to print the main output table of CONCEN
			1 to omit printing the above
		Option (9)	0 to print χ/Q tables
			1 to omit χ/Q tables

Table 4. Input parameters for subroutine CONCEN

Name	Number of Values	Definition	Units
NOL	1	Lower grid limit (abscissa)	
NOU	1	Upper grid limit (abscissa)	
NRL	1	Lower grid limit (ordinate)	
NRU	1	Upper grid limit (ordinate)	
PR	7	Specific plume rise for each Pasquill category	meters
WORD	1	The word AREA	
SQSD	1	The exact length of the side of each grid square when using the square grid configuration. A value for SQSD must also be used for the circular option which corresponds to the approximate length of each grid square in a 20 by 20 grid superscribed on the circular assessment area	meters
SEQWL (S_e)	1	Assumed fraction of equilibrium for the short-life progeny of ^{222}Rn (default value = 0.7)	
IDIST	20	Distances from plant to be used with circular option	meters
WORD	1	The word AIR	
LIDAI (L)	1	Height of lid	meters
RR	1	Rainfall rate in area	centimeters/year
TA	1	Average air temperature in area	°K
TG	3	Vertical temperature gradient for Pasquill categories E, F, and G	°K/meter
PERD	16	Wind direction frequency (16 directions)	

Table 4. (Cont'd)

Name	Number of values	Definition	Units
UDCAT (μ_r)	112	Reciprocal-averaged wind speeds (7 Pasquill categories, 16 directions)	meters/sec
UDAV (μ_a)	112	True-average wind speeds (7 Pasquill categories, 16 directions)	meters/sec
FRAW	112	Frequencies for Pasquill stability categories (each of 16 directions)	
WORD	1	The word STACKS	
NUMST	1	Number of stacks or release areas	
PH (h)	NUMST	Physical height of stack	meters
DIA (d)	NUMST	Diameter of stack	meters
VEL (v)	NUMST	Velocity of stack gases	meters/sec
QH (Q_h)	NUMST	Heat release from stack	cal/sec
DIM	NUMST	Diameter of area source	meters
WORD	1	The word NUCLIDES	
NNUCS	1	Number of nuclides in source term	
NAMNUC	NNUCS	Name of nuclide, such as I-131 or RU-103	
ANLAM	NNUCS	Effective radiological decay constant in the plume	day^{-1}
SC (Φ)	NNUCS	Scavenging coefficient	sec^{-1}
VD (V_d)	NNUCS	Dry deposition velocity	meters/sec
VG (V_g)	NNUCS	Gravitational (or settling) velocity	meters/sec
REL (Q)	NNUCS x NUMST	Release rate of radionuclide from stack	curies/year

Table 4. (Cont'd)

Name	Number of values	Definition	Units
BOUND	20	First value is upper bound of area represented by first IDIST value and lower bound of area represented by second IDIST value, and continuing for all 20 possible IDIST values [BOUND values and subsequent VDCOEF and LIST values are to be entered only if Option (5) = 1]	meters
VDCOEF	(NOU-NOL+1) X(NRU-NRL+1)	Factor to be multiplied by VD to give dry deposition velocity representative of the area for a specific compass direction and IDIST value	
LIST	20	0 to print concentrations for distance corresponding to IDIST 1 to suppress printing for IDIST distance	

Table 5. Input parameters for subroutine DIRECT

Name	Number of values	Definition	Units
NOL	1	Lower grid limit (abscissa)	
NOU	1	Upper grid limit (abscissa)	
NRL	1	Lower grid limit (ordinate)	
NRU	1	Upper grid limit (ordinate)	
SQSD	1	The length of the side of each grid square if input air concentrations and ground deposition rates are for a square grid configuration	meters
IDIST	20	Distances from point of release or center of circular area source for a circular configuration	meters
SEQWL (S_e)	1	Assumed fraction of equilibrium for the short-life progeny of ^{222}Rn (default value = 0.7)	
NNUCS	1	Number of nuclides in source term	
NAMNUC	NNUCS	Name of nuclide	
VD (V_d)	NNUCS	Dry deposition velocity	meters/sec
SC (Φ)	NNUCS	Scavenging coefficient	sec^{-1}
ACON (χ)	400	Concentration in air at ground level for each environmental location (input in a 20 by 20 array)	picocuries/cm^3
GCON (R_t)	400	Rate of deposition on ground surface for each environmental location (input in a 20 by 20 array)	picocuries/cm^2-sec

Table 6. Input parameters for subroutine DOSEN

Name	Number of values	Definition	Units
LIPO	1	Option — 0 for individual dose, 1 for population dose	
NNTB	1	Number of individual radionuclide dose tables by grid location and pathway to be printed. Used to suppress printing	
NRTB	1	Option — 1 for punching on cards doses by nuclide, organ and pathway, 0 for omitting the above	
NSTB	1	Option — 1 for printing and unformatted output of environmental concentrations and intake rates by man for each nuclide, 0 for omitting the above	
NTTB	1	Option — 1 for printing dose summary tables, 0 for omitting the above	
NUTB	1	Option — 1 for printing of working levels for ^{222}Rn if it is in the source term, 0 for omitting the above	
NOBCT	400	Number of meat producing animals for each environmental location (input in a 20 by 20 array)	
NOMCT	400	Number of dairy cattle for each environmental location (input in a 20 by 20 array)	
INTFC	400	Area of vegetable crop production for each environmental location (input in a 20 by 20 array)	m^2
INTPA	400	Population for each environmental location (input in a 20 by 20 array)	
INTWA	400	Identification as to whether an environmental location contains significant water areas (0 or 1) (input in a 20 by 20 array)	
IMPFIX	1	The integer 1 fixes the fraction of each food type imported into the assessment area at the minimum fraction specified as F3VEGM, F3BEFM, and F3MLKM defined below	

Table 6. (continued)

Name	Number of values	Definition	Units
RVEG	1	The fraction representing the quantity of ingested vegetables produced at the environmental location divided by the total quantity ingested which is produced throughout the assessment area including the quantity ingested which is produced at the environmental location	
F3VEGM	1	The minimum fraction of ingested vegetables which is imported into the assessment area. The code may compute a higher value to be used unless IMPFIX = 1	
RBEF	1	Same as RVEG except applied to meat	
F3BEFM	1	Same as F3VEGM except applied to meat	
RMLK	1	Same as RVEG except applied to milk	
F3MLKM	1	Same as F3VEGM except applied to milk	
BRTHRT (B_r)	1	Breathing rate of man	cm^3/hr
DILFAC (d)	1	Depth of water to be used for water immersion doses	centimeters
USEFAC	1	Fraction of time spent swimming	
T (t)	1	Buildup time allotted for surface deposition	days
DD1	1	Fraction of radioactivity retained on leafy vegetables and produce after washing	
TSUBH1 (t_{h1})	1	Time delay — ingestion of pasture grass by animals	hr
TSUBH2 (t_{h2})	1	Time delay — ingestion of stored feed by animals	hr
TSUBH3 (t_{h3})	1	Time delay — ingestion of leafy vegetables by man	hr
TSUBH4 (t_{h4})	1	Time delay — ingestion of produce by man	hr
LAMW (λ_w)	1	Removal rate constant for physical loss by weathering	hr^{-1}

Table 6. (continued)

Name	Number of values	Definition	Units
TSUBE1 (t_{e1})	1	Period of exposure during growing season — pasture grass	hr
TSUBE2 (t_{e2})	1	Period of exposure during growing season — crops or leafy vegetables	hr
YSUBV1 (Y_{v1})	1	Agricultural productivity by unit area (grass-cow-milk-pathway)	kg/m^2
YSUBV2 (Y_{v2})	1	Agricultural productivity by unit area (produce or leafy vegetables)	kg/m^2
FSUBP (f_p)	1	Fraction of year animals graze on pasture	
FSUBS (f_s)	1	Fraction of daily feed that is pasture grass when animals graze on pasture	
QSUBF (Q_F)	1	Consumption rate of contaminated feed or forage by an animal (dry weight)	kg/day
TSUBF (t_f)	1	Transport time from animal feed-milk-man	days
UV ($U_{ap}{}^V$)	1	Rate of ingestion of produce by man	kg/year
UM ($U_{ap}{}^M$)	1	Rate of ingestion of milk by man	liters/year
UF ($U_{ap}{}^F$)	1	Rate of ingestion of meat by man	kg/year
UL ($U_{ap}{}^L$)	1	Rate of ingestion of leafy vegetables by man	kg/year
TSUBS (t_s)	1	Average time from slaughter of meat animal to consumption	days
FSUBG (f_g)	1	Fraction of produce ingested grown in garden of interest	
FSUBL (f_ℓ)	1	Fraction of leafy vegetables grown in garden of interest	
TSUBB (t_b)	1	Period of long-term buildup for activity in soil	years
P	1	Effective surface density of soil (dry weight) (assumes 15-cm plow layer)	kg/m^2

Table 6. (continued)

Name	Number of values	Definition	Units
TAUBEF	1	Fraction of meat producing herd slaughtered per day	
MSUBB	1	Muscle mass of meat producing animal at slaughter	kilograms
VSUBM	1	Milk production of cow	liters/day
R1 (R_1)	1	Fallout interception fraction for pasture	
R2 (R_2)	1	Fallout interception fraction for vegetable crops	
NUMORG	NNUCS	Number of organs considered for the radionuclide	
LAMRR (λ_i)	NNUCS	Radioactive decay constant for the radionuclide	day^{-1}
CFSBA (C_{imm})	NNUCS	Skin dose conversion factor for submersion in air	rem-cm^3/μCi-hr
CFSBW (C_{wimm})	NNUCS	Skin dose conversion factor for submersion in water	rem-cm^3/μCi-hr
CFSUR (C_{surf})	NNUCS	Skin dose conversion factor for surface exposure	rem-cm^2/μCi-hr
KFLAG	NNUCS	Usually 0; a value of 1 is used for a radionuclide which is a daughter product assumed to have an effective decay constant in the plume (ANLAM) equal to the decay constant of its longer-lived parent, and it is desired to use the ANLAM value to calculate its decay on ground surfaces and in water instead of its true decay constant, LAMRR	
TDCF (C_f)	NNUCS	Dose conversion factor for food; always 0 except for tritium	rem-cm^3/pCi-year
TDCW (C_w)	NNUCS	Dose conversion factor for drinking water; always 0 except for tritium	rem-cm^3/pCi-year
FROG	NNUCS X 11	Dose correction factors for whole body and each reference organ to multiply by external doses for skin. The order of the organs is given under NAMORG in this table	

Table 6. (continued)

Name	Number of values	Definition	Units
FSUBMI (F_m)	NNUCS	Average fraction of animal's daily intake of nuclide which appears in each liter of milk	days/liter
FSUBFI (F_f)	NNUCS	Fraction of animal's daily intake of nuclide which appears in each kg of flesh	days/kg
BSUBV1 (B_{iv1})	NNUCS	Concentration factor for uptake of nuclide from soil for pasture and forage (pCi/kg dry weight per pCi/kg dry soil)	
BSUBV2 (B_{iv2})	NNUCS	Concentration factor for uptake of nuclide from soil by edible parts of crops (pCi/kg wet weight per pCi/kg dry soil)	
LAMSUR (λ_w)	NNUCS	Environmental decay constant for surface for the radio-nuclide	day^{-1}
LAMH20	NNUCS	Environmental decay constant for water areas for the radionuclides	day^{-1}
IFLAG	NNUCS	0 for a normal run; 1 if special values RD1 and RD2 are to be used instead of R1 and R2. 2 if special values RD1 and RD2 for dry deposition processes and special values RW1 and RW2 for wet deposition (scavenging) processes are to be used.	
RD1 (RD_1)	NNUCS	Special value for R1 as defined for IFLAG	
RD2 (RD_2)	NNUCS	Special value for R2 as defined for IFLAG	
RW1 (RW_1)	NNUCS	Special value for R1 as defined for IFLAG	
RW2 (RW_2)	NNUCS	Special value for R2 as defined for IFLAG	

Table 6. (continued)

Name	Number of values	Definition	Units
ISOL	NNUCS	Solubility class for nuclide D = days W = weeks Y = years	
AMAD	NNUCS	Particle size for nuclide	μ
F1INH	NNUCS	Gastrointestinal uptake fraction for inhalation	
I1	1	Index integer for a parent radionuclide contributing to surface buildup	
I2	1	As above for a second parent	
I3	1	As above for a third parent	
I4	1	As above for a fourth parent	
I5	1	As above for a fifth parent	
F1	1	Surface input rate for the nuclide resulting from decay of parent I1 per unit aerial deposition rate of I1	
F2	1	As above except for parent I2	
F3	1	As above except for parent I3	
F4	1	As above except for parent I4	
F5	1	As above except for parent I5	
NAMORG	NUMORG X NNUCS	Name of organ, to be written as follows: TOT.BODY (for whole body), R MAR, LUNGS, ENDOST, S WALL, LLI WALL, THYROID, LIVER, KIDNEYS, TESTES, OVARIES	
CFINHA	NUMORG X NNUCS	Dose conversion factor for the organ for inhalation	rem/μCi
F1ING	NUMORG X NNUCS	Gastrointestinal uptake fraction for ingestion	
CFINGA	NUMORG X NNUCS	Dose conversion factor for the organ for ingestion	rem/μCi

Table 7. Data deck preparation for AIRDOS-EPA

Parameters	Number of values	Number of cards	Data type	Format
		Main program		
WORD, OPTION	1 for WORD, 9 for OPTION	1	WORD=OPTIONS OPTIONS values-integer	A8,5I1,I2,3I1
		Subroutine CONCEN		
NOL,NOU,NRL,NRU	1 for each parameter	1	Integer	8I10
PR	7	1	Fixed point	8F10.0
WORD	1	1	WORD=AREA	A8
SQSD	1	1	Fixed point	8F10.0
SEQWL	1	1	Fixed point	F10.0
IDIST	20	3	Integer	8I10
WORD	1	1	WORD=AIR	A8
LIDA1	1	1	Integer	8I10
RR,TA,TG	1 for RR, 1 for TA, 3 for TG	1	Fixed point	8F10.0
PERD	16	1	Fixed point	16F5.0
UDCAT	112	7	Fixed point	16F5.0
UDAV	112	7	Fixed point	16F5.0
FRAW	112	16	Fixed point	7F10.0

Table 7. (Continued)

Parameters	Number of values	Number of cards	Data type	Format	
WORD	1	1	WORD=STACKS	A8	
NUMST	1	1	Integer	8I10	
PH,DIA,VEL,QH,DIM	(1 for each parameter) x value of NUMST	Value of NUMST	Fixed point	8F10.0	
WORD	1	1	WORD=NUCLIDES	A8	*a* (WORD through ANLAM,SC,VD,VG)
NNUCS	1	1	Integer	8I10	
NAMNUC	1	1	Alphameric	A8	
ANLAM,SC,VD,VG	1 for each parameter	1	Fixed point	8F10.0	
REL	Value of NUMST	1	Fixed Point	8F10.0	
BOUND	20	3	Fixed point	8F10.0	*b* (BOUND through LIST)
VDCOEF	(NOU-NOL + 1) x (NRL-NRU + 1)	Number required for a maximum of 10 values per card	Fixed point	10F8.4	
LIST	20	1	Integer	20I1	
		Subroutine DIRECT			
NOL,NOU,NRL,NRU	1 for each parameter	1	Integer	8I10	
SQSD	1	1	Fixed point	8F10.0	
IDIST	20	3	Integer	8I10	
SEQWL	1	1	Fixed point	F10.0	
NNUCS	1	1	Integer	8I10	
NAMNUC,VD,SC	1 for each parameter	1	Alphameric, fixed point, floating point	A8 F12.4 E10.3	*c* (NAMNUC,VD,SC through GCON)
ACON	400	50	Floating point	8E10.3	
GCON	400	50	Floating point	8E10.3	

Table 7. (Continued)

Parameters	Number of values	Number of cards	Data type	Format
		Subroutine DOSEN		
LIPO	1	1	Integer	5I10
NNTB,NRTB,NSTB,NTTB, NUTB	1 for each parameter	1	Integer	5I10
NOBCT	400	25	Integer	16I5
NOMCT	400	25	Integer	16I5
INTFC	400	50	Floating point	8E10.3
INTPA	400	50	Fixed point	8F10.1
INTWA	400	10	Integer	40I2
IMPFIX	1	1	Integer	I10
RVEG,F3VEGM,RBEF, F3BEFM,RMLK,F3MLKM	1 for each parameter	1	Fixed point	6F10.3
BRTHRT,DILFAC, USEFAC,T,DD1	1 for each parameter	1	Fixed point	6F10.3
TSUBH1,TSUBH2, TSUBH3,TSUBH4	1 for each parameter	1	Floating point	8E10.3
LAMW	1	1	Floating point	8E10.3
TSUBE1,TSUBE2	1 for each parameter	1	Floating point	8E10.3
YSUBV1,YSUBV2	1 for each parameter	1	Floating point	8E10.3
FSUBP	1	1	Floating point	8E10.3
FSUBS	1	1	Floating point	8E10.3
QSUBF	1	1	Floating point	8E10.3

Table 7. (Continued)

Parameters	Number of values	Number of cards	Data type	Format	
TSUBF	1	1	Floating point	8E10.3	
UV,UM,UF,UL	1 for each parameter	1	Floating point	8E10.3	
TSUBS	1	1	Floating point	8E10.3	
FSUBG,FSUBL	1 for each parameter	1	Floating point	8E10.3	
TSUBB	1	1	Floating point	8E10.3	
P	1	1	Floating point	8E10.3	
TAUBEF,MSUBB,VSUBM	1 for each parameter	1	Fixed point	10F8.4	
R1,R2	1 for each parameter	1	Fixed point	10F8.4	
NUMORG,LAMRR,CFSBA, CFSBW,CFSUR,KFLAG, TDCF,TDCW	1 for each parameter	1	Integer and floating point	I10,4E10.3, I10,2E10.3	
FROG	11	1	Fixed point	11F5.3	
FSUBMI,FSUBFI,BSUBV1, BSUBV2	1 for each parameter	1	Floating point	8E10.3	
LAMSUR,LAMH2O,IFLAG, RD1,RD2,RW1,RW2	1 for each parameter	1	Floating point, integer, and fixed point	2E10.3,I1, 6F8.4	
I1,I2,I3,I4,I5,F1,F2, F3,F4,F5	1 for each parameter	1	Integer and floating point	5I4,5E10.3	*d*
ISOL,AMAD,F1INH	1 for each parameter	1	Alphameric and floating point	T11,A1,T15, E10.3,T27, E10.3	
NAMORG,CFINHA	1 for each parameter x value of NUMORG	NUMORG	Alphameric and floating point	A8,T10,E10.3	
F1ING	1	1	Floating point	T11,E10.3	
CFINGA	Value of NUMORG	NUMORG	Floating point	T11,E10.3	

[a]A set of the three cards in this bracket is required for each radionuclide. The number of these sets of cards must be equal to the value of NNUCS.

[b]The cards in the bracket for BOUND, VDCOEF, and LIST should not be included in the data deck unless OPTION (5) = 1.

[c]A set of the cards in this bracket is required for each radionuclide. The total number of these sets is the value of NNUCS.

[d]One set of cards in this bracket is required for each radionuclide. Each set is referred to as the radionuclide data deck for the specific radionuclide. The number of radionuclide data decks must be equal to the value of NNUCS. The set of cards for NAMORG, CFINHA, FIING, and CFINGA for each radionuclide is referred to as the organ data deck for the specific radionuclide.

5. TERRESTRIAL TRANSPORT INPUT PARAMETERS

The parameter values listed in the following sections have been used in the demonstration computer run given in Appendix B. For the parameters B_{iv}, F_m, and F_f, a review of original references is currently being performed. The values listed for these parameters reflect the *current* status of this review. The listed values will undoubtedly change as new references are reviewed or become available. Many of the other parameter values listed are derived from the extensive and well-documented reviews by Ng et al. (1977) and Hoffman and Baes (1979). A statistical distribution has been described for many of the parameters reviewed by Hoffman and Baes (1979), and the values taken from this review and listed in this section are the mean values with respect to the distribution described for the parameter.

The values listed for the soil-plant bioaccumulation factor B_{iv}, the forage-to-milk transfer coefficient F_m, and the forage-to-meat transfer coefficient F_f were derived from a review of original experimental data according to the methodology described below. Individual observations or the average of replicate observations (whichever given by the author) specific for the parameter were taken from the reference. When necessary, reported B_{iv} data were transformed to adhere to the strict definitions of the parameter by using appropriate fresh weight-dry weight conversion factors (Morrison, 1956; Spector, 1956). Ingestion rates given by Liden and Gustafsson (1967) and Bell (1978) were used to derive some values of F_f from associated meat and forage data. All measurements applicable to the parameter in a reference were used to calculate an arithmetic mean value for that reference. Finally, the values for each reference were used to derive an unweighted arithmetic mean for all references combined. This final value, unless otherwise noted, is the value listed for the parameter.

The parameters used in the terrestrial transport models in Sect. 3 are designed to represent annually averaged values at equilibrium over a wide range of environmental conditions. Empirical data used in deriving values for these parameters may not always reflect annual average or equilibrium conditions. In addition, data from laboratory or otherwise-controlled experiments which do not adequately simulate field conditions may lead to erroneous evaluations for specific assessment sites. Furthermore, empirical data may not adequately reflect the true distribution of values associated with each parameter under various conditions. Thus, caution should be used in the interpretation of parameter values presented and results generated by the sample run.

5.1 Agricultural Productivity by Unit Area Y_v

In this report agricultural productivity, in kilograms per square meter, is given in dry weight for the above-ground portion of pasture grasses Y_{v1} and in fresh weight for the edible portions of leafy vegetables and produce ingested directly by man Y_{v2}. Since dry weight measurements of productivity for pasture grasses are most commonly found in the literature, direct comparison with productivity estimates for stored feeds and silage can be made. Fresh weight productivity estimates for leafy vegetables and produce consumed directly by man are appropriate because data on human food consumption is generally given in fresh weight. In addition, modern packaging and refrigeration techniques are designed to reduce desiccation and present a product as similar to harvest condition as possible. Table 8 presents mean values of Y_{v1} and Y_{v2} derived from the review and analysis of agricultural productivity by Baes and Orton (1979).

5.2 The Fraction of Atmospherically Depositing Radionuclides Intercepted by Above-Ground Portions of Plants R

The fraction of atmospherically depositing radionuclides intercepted and initially retained on above-ground portions of either forage crops or leafy vegetables and fresh produce ingested by man is symbolized by R_1 and R_2, respectively, where R_1, $R_2 \leq 1$. It is assumed in the model that unedible portions of vegetable crop plants are plowed into the soil at harvest.

5.2.1 Interception fraction R_1 for forage crops

Caution must be exercised when selecting a value of R_1 for assessment purposes because a correlation between R and Y_v has been demonstrated for forage crops (Chamberlain, 1970; Miller, 1979b). This correlation is likely because the fraction of an atmospherically depositing nuclide intercepted by a plant is highly dependent on the surface area available for interception. For forage crops, the available surface area or leaf area index is highly correlated to the above-ground standing crop biomass or productivity Y_{v1}.

Miller (1979a) analyzed associated measured values of R and Y_v and described a distribution for the ratio R/Y_v based on lognormal statistics. The resulting distribution of this ratio has been used in the present report to derive an arithmetic mean value of $R_1 = 0.57$. This R_1 value has been determined such that when combined with the mean Y_{v1} value of 0.28 (Table 8) the resultant ratio of R_1/Y_{v1} numerically equals the mean value (2.03) of the distribution of R/Y_v described by Miller (1979a).

5.2.2 Interception fraction R_2 for leafy vegetables and fresh produce

The correlation which Chamberlain (1970) demonstrated between R and Y_v is specific for pasture grasses. Such a relationship is not expected to exist for all leafy vegetables and fresh produce ingested by man for the following considerations:

1. On a weight basis, the edible portion of vegetable plants varies by species from nearly 100% for leafy vegetables to a very small fraction for food grains;
2. Surface area-to-weight ratios differ greatly among various types of vegetables; and
3. Edible portions of some vegetables are enclosed by tissue layers and fail to intercept atmospheric radionuclides (i.e., corn, peas, etc.).

Measurements of the interception fraction R_2 specific for edible portions of leafy vegetables and fresh produce ingested directly by man are unavailable. It is expected that the value of R_2 will be less than that of R_1 since most vegetable crops are usually cultivated in rows. On a unit area basis, this spacing of vegetable crops exposes more surface soil than the dense spacing of most forage crops. Booth et al. (1971) recognized this problem in their terrestrial model TERMOD and set the interception fraction value for fresh produce and vegetable crops lower than that for grasses. However, the magnitude of the actual difference between R_1 and R_2 is speculative. The R_2 value of 0.2 used by the NRC (U.S. Nuclear Regulatory Commission Regulatory Guide 1.109,

Table 8. Estimated values of above-ground agricultural productivity for forage grasses and edible portions of vegetable crops

Parameter	Mean Value[a] (kg/m^2)
Y_{v1} measured in dry weight (forage grasses)	0.28
Y_{v2} measured in fresh weight (leafy vegetables)[b]	1.9
Y_{v2} measured in fresh weight (non-leafy vegetables)[c]	0.57

[a]The mean estimates given above are the inverse of values derived by Baes and Orton (1979) for estimates of $1/Y_v$ based on experimental data.

[b]Y_{v2} for leafy vegetables is based on edible portions of cabbage, lettuce, and spinach.

[c]Y_{v2} for nonleafy vegetables is based on edible portions of broccoli, cauliflower, green peas, lima beans, and sweet corn.

1977) is less than the R_1 value of 0.57 presented in Sect. 5.2.1; and therefore, we chose the NRC value for use in the AIRDOS-EPA sample run (Appendix B).

5.3 Deposition Velocity V_d

The deposition velocity V_d (centimeters per second) is used in the code as a transfer factor relating an air concentration to a surface deposition rate (Hoffman, 1977; Miller et al., 1978). Field measurements of V_d are generally based on measured concentrations in vegetation cut at a specific height above the ground surface and fail to measure total deposition on a unit area basis. The fraction of radionuclide deposited on soil, leaf litter, and uncut vegetation is usually not measured. Thus, an estimate of V_d appropriate for the total deposit on a unit area basis is derived from a V_d specific for deposition onto vegetation by the following method:

$$V_d \text{ (total)} = V_d \text{ (specific for vegetation)}/R \quad , \tag{68}$$

where R is the fraction of atmospherically depositing nuclides intercepted by the above-ground edible portion of the vegetation. Values of V_d (total) are appropriate for use in the AIRDOS-EPA code because V_d is used to estimate plume depletion and total ground area deposition.

The following values of V_d appear to be relevant for forage grasses under dry conditions (Heinemann and Vogt, in press):

1. 2 cm/sec for reactive gases (molecular iodine),
2. 0.1 cm/sec for small particulates (<4 μm in diameter), and
3. 0.01 cm/sec for relatively unreactive gases (CH_3I).

Dividing the above specific V_d values by a mean forage grass interception fraction R_1 of 0.57 (Sect. 5.2.1) produces the following values of V_d (total):

1. 3.5 cm/sec for reactive gases,
2. 0.18 cm/sec for small particulates, and
3. 0.018 cm/sec for relatively unreactive gases.

These values are specific for deposition on grasslands. It is assumed in the code that the V_d (total) for grasslands is equal to the V_d (total) for vegetable crops. This assumption may be false since depositional conditions for grasslands and vegetable croplands are probably different (Hosker, 1974); however, measured values of V_d (total) have not been published for vegetable crops. We propose that the value of V_d (total) for particulates >4 μm in diameter be set equal to the gravitational fall velocity of the particle size considered (Sehmel et al., 1973).

There is a potential for error in calculating plume depletion in atmospheric transport models from a specific value of V_d (total) calculated for a grassland environment. When various environmental conditions such as buildings, trees, rough terrain, and other potential scavengers are present, the use of a different V_d (total) may be warranted.

5.4 The Plant/Soil Bioaccumulation Factor B_{iv}

The transfer of radionuclides from soil to the above-ground portions of pasture grasses is parameterized by B_{iv1}. Radionuclide transfer from soil to the edible portions of leafy vegetables and fresh produce ingested by man is parameterized by B_{iv2}. In the model, it is assumed that radionuclides incorporated into nonedible portions of vegetable crops are returned to the soil by the plowing under of the nonedible portion after harvesting of the edible portion.

A review of the available literature was made to determine values of B_{iv1} and B_{iv2} for various elements. Measurements of radionuclide concentrations in soil and vegetation reported in the literature are given in both fresh and dry weight for vegetation and may be specific for both edible and nonedible plant portions. Thus, only data which was applicable to (or could easily be converted to conform with) the following definitions of B_{iv1} and B_{iv2} were considered. The definitions of B_{iv1} and B_{iv2} are as follows:

$$B_{iv1} = \frac{\text{radionuclide concentration in entire above-ground portion of plant at maturity per unit dry wt}}{\text{radionuclide concentration in soil per unit dry wt}}$$

$$B_{iv2} = \frac{\text{radionuclide concentration in edible portion of plant at maturity per unit fresh wt}}{\text{radionuclide concentration in soil per unit dry wt}}$$

The effects of chemical and physical forms of the element will likely influence B_{iv} values to a greater extent than isotopic effects. Therefore, element-specific, rather than isotope-specific values of B_{iv} were chosen. This consideration allows consolidation of measured B_{iv} values and incorporation of a greater number of references into the determination of B_{iv}.

Determinations of B_{iv1} and B_{iv2} (Tables 9 and 10, respectively) were made from original literature references whenever available. However, the review document by Ng et al. (1968) was used to derive B_{iv} values when original sources were unavailable. References in which

Table 9. Values of B_{ivl} derived from a review of the literature

Element	B_{ivl}	References
Sr	1.2×10^{0}	Hardy et al., (1969) Arkhipov et al. (1974) Romney et al. (1957) Romney et al. (1966).
Tc	2.2×10^{2}	Wildung et al. (1977).
I	2.0×10^{-1}	Ng et al. (1978).
Cs	1.5×10^{-1}	Rediske et al. (1955); Haak and Eriksson (1973); Frederiksson et al. (1966); Frederiksson et al. (1969); Evans and Dekker (1968); Hardy et al. (1977); Romney et al. (1957); Barber (1964).
Pb	1.1×10^{-1}	Cox and Rains (1972); Zimdahl et al. (1978); Rabinowitz (1972); Dedolph et al. (1970).
Po	4.2×10^{-3}	Watters et al. (1969).
Ra	9.7×10^{-2}	Kirchmann et al. (1968); Taskayev et al. (1977); Debortoli and Gaglione (1972).
Ac	1.0×10^{-2}	Ng et al. (1968) (based on 25% dry matter).
Th	2.7×10^{-3}	Bondietti et al. (in press).
Pa	1.0×10^{-2}	Ng et al. (1968) (based on 25% dry matter).
U	8.5×10^{-3}	Bondietti et al. (in press). Adams et al. (1955).
Pu	2.2×10^{-3}	Romney et al. (1970); Price (1972); Rediske et al. (1955); Cummings and Bankert (1971); Adams et al. (1975); Hardy et al. (1977); Brown and McFarlane (1978); Bondietti et al. (in press).

Table 10. Values of B_{iv2} derived from a review of the literature

Element	B_{iv2}	References
Sr	2.9×10^{-1}	Romney et al. (1957); Essington et al. (1962); Arkhipov et al. (1974); Hardy et al. (1977).
Tc[a]	1.1×10^{0}	Wildung et al. (1977).
I	5.5×10^{-2}	Ng et al. (1978).
Cs	9.3×10^{-3}	Romney et al. (1957); Schulz (1965); Haak and Eriksson (1973) Fredriksson et al. (1966); Fredriksson et al. (1969); Evans and Dekker (1968); Hardy et al. (1977); Essington et al. (1962).
Pb	3.9×10^{-3}	Wilson and Cline (1966); Ter Haar (1979); John and Van Laerhoven (1972); Rabinowitz (1972); Dedolph et al (1970).
Po	2.6×10^{-4}	Watters et al. (1969).
Ra	6.2×10^{-2}	Vavilov et al. (1964); Mordberg et al. (1976); Kirchmann et al. (1968); DeBortoli and Gaglione (1972).
Ac	2.5×10^{-3}	Ng et al. (1968).
Th	3.5×10^{-4}	Bondietti et al. (in preparation).
Pa	2.5×10^{-3}	Ng et al. (1968).
U	2.9×10^{-4}	Bondietti et al. (in press); Adams et al. (1975).
Pu	2.0×10^{-4}	Cline (1968); Wilson and Cline, (1966); Cummings and Bankert (1971); Dahlman et al (1976); Bondietti and Sweeton (1976); Schulz et al. (1975); Adams et al. (1975); Hardy et al. (1977); Brown and McFarlane (1978).

[a]The derived value for technetium was 5.5×10^{1}. This value has been adjusted to account for removal of vegetable crops by harvesting over 100 years (see Sect. 5.4.1).

directly deposited or resuspended material may have significantly contributed to the reported plant radionuclide concentration were not considered in our analysis of B_{iv}.

The derived value of B_{iv2} for technetium is relatively high with respect to B_{iv2} values for the other elements (Table 10). The harvesting and removal of vegetable crops from the soil may remove significant quantities of technetium from the agricultural system over long periods of time. This removal after 100 years may be quite significant. The following procedure to adjust the technetium B_{iv2} is made to simulate the effect of harvesting and removal of vegetable crops on the soil concentration of technetium. Without an adjustment of the B_{iv2} value for technetium given in Table 10, the AIRDOS-EPA model would overpredict technetium concentrations in vegetables after 100 years with an average of one harvest per year, because the model assumes no radionuclide loss from the soil via uptake by crop plants and their subsequent harvesting. An estimate of this removal effect k is given by the following equation:

$$k = \frac{C_{sh}}{C_{sn}} \quad , \qquad (69)$$

where

k = adjustment factor to account for removal of technetium from soil via harvesting of crops,

C_{sh} = concentration of technetium in soil after 100 years with harvesting of vegetable crops,

C_{sn} = concentration of technetium in soil after 100 years with no harvesting of vegetable crops.

The concentration of technetium in soil with a deposition rate of 1 Ci/m^2-year would be C_{sn} = 100 Ci/m^2 after 100 years with no removal via harvesting or other removal processes. The concentration of technetium in soil with removal by harvesting of the crop after 100 years is given by:

$$C_{sh} = \sum_{n=1}^{100} d_s f^{n-1} = d_s \frac{1 - f^{100}}{1 - f} , \qquad (70)$$

where

f = the fraction of technetium remaining in the soil after one year,

n = time in years = 100 years,

d_s = deposition rate on soil (Ci/m^2-year).

The fraction of technetium remaining in the soil after one year is given by:

$$f = \frac{1 - (B_{iv2} \cdot Y_{v2})}{P} , \qquad (71)$$

where

B_{iv2} = the plant/soil bioaccumulation factor,

Y_{v2} = the standing crop biomass of the edible portion of the vegetable crop in kg/m^2,

P = the effective surface density of the soil in kg/m^2.

Using values of $n = 100$ year, $d_s = 1\ Ci/m^2$ year, $B_{iv2} = 5.5 \times 10^1$, $Y_{v2} = 2.0\ kg/m^2$, and $P = 215\ kg/m^2$ and substituting Eq. (71) into Eq. (70), a value of $C_{sh} = 2.0 \times 10^0$ results. Thus, the value of k in Eq. (69) is 2.0×10^{-2}. Multiplying k by the above value of B_{iv2} for technetium gives an effective B_{iv2} of 1.1×10^0. This adjusted value of B_{iv2} is given in Table 10. For our determination of B_{iv1}, it is assumed that technetium removed from the soil by forage plants is returned to the soil via excretion by grazing animals and decay of ungrazed grasses. Thus, the above calculation was not performed for B_{ivl}.

5.5 Milk-Transfer Coefficient F_m

The milk-transfer coefficient F_m represents the fraction of the total daily intake of a nuclide which is transferred to a liter of the cow's milk at equilibrium. Unfortunately, very few measurements of F_m involve equilibrium conditions. Usually, single oral doses are administered to the cow, and milk concentrations are monitored for several days. Values of F_m can be derived from such experiments according to the methodology described by Ng et al. (1977) in which the total fraction of the oral dose recovered in milk after six days or more is divided by the daily rate of milk production.

Determinations of F_m (Table 11) were made from original literature references whenever available. However, for many elements the well-documented review by Ng et al. (1977) was the primary literature source. References in which the chemical form of the nuclide administered orally to the cow was clearly atypical of forms found in the environment were excluded from the analysis of F_m. As for the analysis of B_{iv}, the values of F_m given in Table 11 are element- rather than nuclide-specific.

5.6 The Meat-Transfer Coefficient F_f

The meat-transfer coefficient F_f represents the fraction of the total daily intake of a nuclide which is transferred to a kilogram of muscle in the meat-producing animal at equilibrium. (For the demonstration

Table 11. Estimates of the milk-transfer coefficient F_m for dairy cows

Element	F_m (day/liter)	References
Sr	2.4×10^{-3}	Cragle and Dermott (1959); Garner et al (1960); Squire et al. (1958); Comar et al. (1961).
Tc	9.9×10^{-3}	Ng et al. (1977).
I	1.0×10^{-2}	Ng et al. (1977); Hoffman (1979).
Cs	5.6×10^{-3}	Hawthorne (1967); Ward et al. (1965); Johnson et al. (1968).
Pb	9.9×10^{-5}	Stanley et al. (1971); Kerin and Kerin (1971); Nelmes et al. (1974); Donovan et al. (1969); Bovay (1971); Lynch et al. (1974).
Po	1.2×10^{-4}	McInroy (1973).
Ra	5.9×10^{-4}	Kirchmann et al. (1972).
Ac	2.0×10^{-5}	Ng et al. (1977).
Th	5.0×10^{-6}	Ng et al. (1977).
Pa	5.0×10^{-6}	Ng et al. (1977).
U	1.2×10^{-4}	Chapman and Hammons (1963).
Pu	4.5×10^{-8}	Sansom (1964); Garten (1978)[a]

[a]Derived from range based on a review of Stanley et al. (1976) and reported by Garten (1978).

run, beef is the meat consumed at the specified environmental locations.) It is assumed that equilibrium conditions exist when slaughter occurs. Measured intake rates and associated meat and forage elemental concentrations may yield values of F_f which are suspect, because it has not been conclusively shown that equilibrium between intake rate and meat concentration are ever attained. Thus, the age and time of exposure from intake for each animal may significantly influence the measured value. However, a review of the available literature was made to give estimates of F_f for beef cattle (Table 12).

Values of F_f based on immature cattle (less than 6 months of age) were excluded from analysis when data for adult cattle were available. Data for other ruminant species were included when literature references for cattle F_f's were unavailable. Extrapolation from these species to beef cattle may result in invalid conclusions.

5.7 Other Environmental Terrestrial Transport Parameters

A list of environmental parameters used in the AIRDOS-EPA code demonstration run, and not previously discussed above, are given in Tables 13 and 14. Values of the radiological decay constant λ_i (day^{-1}) are taken from Kocher (1977). The values for the parameters f_p, f_s, Q_F, and P (defined in Table 6) are the means of their respective statistical distributions as described in Hoffman and Baes (1979). Other parameter values are taken from the U.S. NRC Regulatory Guide 1.109 (1977).

Table 12. Estimates of the meat-transfer coefficient F_f for beef cattle

Element	F_f (day/kg)	References
Sr	3.0×10^{-4}	Ng et al. (1978).
Tc	8.7×10^{-3}	Ng et al. (1968).
I	7.0×10^{-3}	Ng et al.,(1978).
Cs	1.4×10^{-2}	Ward and Johnson (1965).
Pb	9.1×10^{-4}	Nelmes et al. (1974).
Po	4.0×10^{-3}[a]	Beasley and Palmer (1966); Holtzman (1966,a) Hill (1965).
Ra	5.0×10^{-4}[b]	Hardy et al. (1969); Bell (1978); Holtzman (1955a,b).
Ac	1.6×10^{-6}[c]	
Th	1.6×10^{-6}[c]	
Pa	1.6×10^{-6}[c]	
U	1.6×10^{-6}[c]	
Pu	4.1×10^{-7}	Ng et al. (1978); Garten (1978)[d]

[a] F_f values are specific for caribou and reindeer using daily food intake rates estimated by Liden and Gustafsson (1966).

[b] F_f values are specific for sheep, caribou, and reindeer using daily food intake rates estimated by Liden and Gustafsson (1966) for caribou and reindeer and by Bell (1978) for sheep.

[c] F_f value estimated by using value for americium and curium given by Ng et al. (1978).

[d] Derived from range based on a review of Stanley et al. (1978) and reported by Garten (1978).

Table 13. Radiological decay constant λ_i for selected nuclides[a]

Nuclide	λ_i (day^{-1})
^{3}H	1.54×10^{-4}
^{14}C	3.32×10^{-7}
^{89}Sr	4.32×10^{-2}
^{90}Sr	6.54×10^{-5}
^{99}Tc	8.92×10^{-9}
^{131}I	8.62×10^{-2}
^{210}Pb	8.52×10^{-5}
^{210}Po	5.02×10^{-3}
^{222}Rn	1.81×10^{-1}
^{226}Ra	1.19×10^{-6}
^{228}Ra	3.15×10^{-4}
^{227}Ac	8.72×10^{-5}
^{228}Th	9.93×10^{-4}
^{230}Th	2.47×10^{-8}
^{232}Th	1.35×10^{-13}
^{231}Pa	5.82×10^{-8}
^{234}U	7.77×10^{-9}
^{235}U	2.68×10^{-12}
^{238}U	4.25×10^{-13}
^{238}Pu	2.17×10^{-5}
^{239}Pu	7.79×10^{-8}

[a]Derived from Kocher (1977).

Table 14. Environmental parameters used in AIRDOS-EPA to estimate radionuclide concentrations in meat, milk, and vegetables consumed by man[a]

Parameter	Value	Units	Reference
t_{e1}	720	hr	U.S. NRC Reg. Guide 1.109 (1977)
t_{e2}	1440	hr	U.S. NRC Reg. Guide 1.109 (1977)
f_p	0.4		Shor and Fields (1979b)
f_s	0.4		Shor and Fields (1979b)
Q_F	16	kg/day	Shor and Fields (1979a)
t_f	4	days	U.S. NRC Reg. Guide 1.109 (1977)
t_s	20	days	U.S. NRC Reg. Guide 1.109 (1977)
t_b	8.76×10^5	hr	
t_{h1}	0	hr	U.S. NRC Reg. Guide 1.109 (1977)
t_{h2}	2160	hr	U.S. NRC Reg. Guide 1.109 (1977)
t_{h3}	336	hr	U.S. NRC Reg. Guide 1.109 (1977)
t_{h4}	336	hr	U.S. NRC Reg. Guide 1.109 (1977)
λ_W	0.0021	hr^{-1}	U.S. NRC Reg. Guide 1.109 (1977)
P	215	kg/m^2 (dry wt)	Derived from Baes (1979)
RD_1[b]	0.63		
RD_2[b]	0.20		
RW_1[b]	0.63		
RW_2[b]	0.20		

[a]For a description of the parameter see Table 6.

[b]We have not been able to determine values of R_1 and R_2 specific for dry and wet deposition.

5.8 Ingestion and Inhalation Rates U_{ap} for the Average Adult

The available surveys on food ingestion and air inhalation rates have recently been reviewed by Rupp (1979). The values in Table 15 are the mean values of the ranges found by Rupp and are specific for the average adult. These values are used in the demonstration run of the code to estimate population doses.

Table 15. Ingestion and inhalation rates U_{ap} for the average adult[a]

Pathway	Rate
Leafy vegetables $U_{ap}{}^{L}$	18 kg/year
Other fresh produce $U_{ap}{}^{V}$	176 kg/year
Meat (excluding fish) $U_{ap}{}^{F}$	94 kg/year
Milk $U_{ap}{}^{M}$	112 liter/year
Inhalation $U_{ap}{}^{I}$	8030 m^3/year

[a]Values listed are given by Rupp (1979).

6. REFERENCES

Adams, W. H., J. R. Buckholz, C. W. Christenson, G. L. Johnson, and E. B. Fowler. 1975. *Studies of Plutonium, Americium, and Uranium in Environmental Matrices.* LA-5661, Los Alamos Scientific Laboratory, Los Alamos, New Mexico.

Arkhipov, N. P., Y. A. Fedorov, E. F. Bondar, R. M. Aleksakhin, G. N. Romanov, and L. T. Feuraleva. 1974. Predicting ^{90}Sr accumulation in the crop harvest as a result of its uptake from the soil. *Soviet Soil Sci.* 6(4): 412-419.

Baes, C. F., III. 1979. The soil loss constant λ_{s1}, due to leaching from soils. IN Hoffman, F. O. and C. F. Baes, III (eds.). *A Statistical Analysis of Selected Parameters for Predicting Food Chain Transport and Internal Dose of Radionuclides. Final Report.* ORNL/NUREG/TM-282.

Baes, C. F., III and T. H. Orton. 1979. Productivity of agricultural crops and forage Y_v. IN Hoffman, F. O. and C. F. Baes, III (eds.). *A Statistical Analysis of Selected Parameters for Predicting Food Chain Transport and Internal Dose of Radionuclides. Final Report.* ORNL/NUREG/TM-282.

Barber, D. A. 1964. Influence of soil organic matter on the entry of cesium-137 into plants. *Nature* 294: 1326-1327.

Beasley, T. M. and H. E. Palmer. 1966. Lead-210 and polonium-210 in biological samples from Alaska. *Science* 152: 1062-1064.

Bell, C. Professor, Animal Science Department, University of Tennessee, Knoxville, Tenn. 37916. 1978. Personal communication to A. P. Watson, August 17, 1978.

Bondietti, E. A. and F. H. Sweeton. 1976. Transuranic speciation in the environment. pp. 449-476. IN *Transuranics in Natural Environments.* NVO-178.

Bondietti, E. A., J. R. Trabalka, C. T. Garten, and G. G. Killough. In press. Biochemistry of actinides: A nuclear fuel cycle perspective. IN *Radioactive Waste in Geologic Storage.* American Chemical Society Symposium Service.

Bondietti, E. A., C. T. Garten, Jr., C. W. Francis, and Eyman, L. D. (in preparation). Uranium and thorium in the biosphere: A review emphasizing behavior applicable to the thorium fuel cycle. *Journal of Environmental Quality.*

Booth, R. S., S. V. Kaye, and P. S. Rohwer. 1971. Systems analysis methodology for predicting dose to man from a radioactively contaminated terrestrial environment. pp. 877-893. IN *Radionuclides in Ecosystems, Proceedings of the Third National Symposium on Radioecology.* CONF-710501.

Bovay, E. 1971. Accumulation of Pb on vegetation along expressways. Feeding tests on dairy cows with forage contaminated with Pb. pp. 101-117. IN Switzerland Federal Committee for Air Hygiene Investigations: The Problem of Leaded Gasoline. *Bull. der Eidg. Gesundheitsamtes* Suppl. B, No. 3.

Briggs, G. A. 1969. *Plume Rise, AEC Critical Review Series*. TID-25075.

Brown, K. W. and J. C. McFarlane. 1978. Plutonium uptake by plants grown in soil containing plutonium-238 dioxide particles. *Health Phys.* 35:481-485.

Chamberlain, A. C. 1970. Interception and retention of radioactive aerosols by vegetation. *Atm. Environ.* 4:57-78.

Chapman, T. S. and S. Hammons, Jr. 1963. Some observations concerning uranium content of ingesta and excreta of cattle. *Health Phys.* 9: 79-81.

Cline, J. F. 1968. Uptake of ^{241}Am and ^{239}Pu by plants. pp. 8.24-8.25. IN Thompson, R. C. and Paulette Teal (eds.). *Pacific Northwest Laboratory Annual Report for 1967 to the USAEC Division of Biology and Medicine, Volume I*. BNWL-714.

Comar, C. L., R. H. Wasserman, and A. R. Twardock. 1961. Secretion of calcium and strontium into milk. *Health Phys.* 7: 69-80.

Cox, W. J. and D. W. Rains. 1972. Effect of lime on Pb uptake by five plant species. *J. Environ. Qual.* 1(2): 167-71.

Cragle, R. G. and B. J. Demott. 1959. Strontium and calcium uptake and excretion in lactating dairy cows. *J. Dairy Sci.* 42(8): 1367-1372.

Culkowski, W. M. and M. R. Patterson. 1976. *A Comprehensive Atmospheric Transport and Diffusion Model*. ORNL/NSF/EATC-17.

Cummings, S. L. and L. Bankert. 1971. The uptake of cerium-144, promethium-147, and plutonium-238 by oat plants from soils. *Radiat. Data Rep.* 12(2): 83-85.

Dahlman, R. C., E. A. Bondietti, and L. D. Eyman. 1976. Biological pathways and chemical behavior of plutonium and other actinides in the environment. pp. 47-80 IN A. M. Friedman (ed.). *Actinides in the Environment, ACS Symposium Series 35*. American Chemical Society, Washington.

DeBortoli, M. and P. Gaglione. 1972. Radium-226 in environmental materials and foods. *Health Phys.* 22(1): 43-48.

Dedolph, R., G. Ter Haar, R. Holtzman, and H. Lucas, Jr. 1970. Sources of Pb in perenniel ryegrass and radishes. *Environ. Sci. Technol.* 4(3): 217-225.

Donovan, P. P., D. T. Feeley, and P. P. Canavan. 1969. Lead contamination in mining areas in Western Ireland II. Survey of animals, pastures, foods, and waters. *J. Sci. Fd. Agric.* 20: 43-45.

Essington, E., H. Nishita, and A. Wallace. 1962. Influence of chelates on availability of fission products to plants grown in a contaminated soil. *Soil Sci.* 94: 96-105.

Evans, E. J. and A. J. Dekker. 1968. Comparative Cs-137 content of agricultural crops grown in a contaminated soil. *Can. J. Plant Sci.* 48: 183-188.

Evans, R. D. 1969. Engineer's guide to the elementary behavior of radon daughters. *Health Phys.* 17: 229-252.

Fredriksson, L. Å. Eriksson, and H. Lönsjö. 1966. *Studies on Plant Accumulation of Fission Products under Swedish Conditions. VIII. Uptake of* ^{137}Cs *in Agricultural Crops as Influenced by Soil Characteristics, and Rate of Potassium Fertilization in a Three Year Micro Plot Experiment.* Research Institute of National Defense. Stockholm, Sweden, FOA 4 Rapport A 4486-4623.

Fredriksson, L., H. Lönsjö, and Å. Eriksson. 1969. *Studies on Plant Accumulation of Fission Products under Swedish Conditions. XII. Uptake of* ^{137}Cs *by Barley and Peas from 12 Different Top Soils Combined with 2 Subsoils in a Long Term Micro Plot Experiment.* Research Institute of National Defense. Stockholm, Sweden, FOA 4 Rapport C 4405-4428.

Garner, R. J., H. G. Jones, and B. F. Sansom. 1960. Fission products and the dairy cow: 2. Some aspects of the metabolism of the alkaline earth elements calcium, strontium, and barium. *Biochem. J.* 76: 572.

Garten, C. T. 1978. A review of parameter values used to assess the transport of plutonium, uranium, and thorium in terrestrial food chains. *Environmental Research* (in press).

Gifford, F. A., Jr. 1961. Use of routine meteorological observations for estimating atmospheric dispersion. *Nucl. Saf.* 2(4): 47-57.

Gifford, F. A., Jr. 1976. Turbulent diffusion-typing schemes: A review. *Nucl. Saf.* 17(1): 68-86.

Haak, E. and Å. Eriksson. 1973. *Studies on Plant Accumulation of Fission Products under Swedish Conditions. VIX. Uptake of* ^{137}Cs *by Wheat and Timothy from Six Different Soils as Influenced by Rate of K-Fertilization and by Type and Rate of N-Fertilization in Pot Experiments.* The Research Institute of National Defence, Stockholm, Sweden, FOA 4 Rapport C 4557-A3.

Hardy, E., J. Rivera, I. Fisenne, W. Pond, and D. Hogue. 1969. Comparative utilization of dietary radium-226 and other alkaline earths by pigs and sheep. pp. 183-190. IN Sikov, M. R. and D. D. Mahlum (eds.). *Proceedings of the Ninth Annual Hanford Biology Sumposium, Richland, Washington, May 5-8, 1969.* CONF-690501.

Hardy, E. P., B. G. Bennett, and L. T. Alexander. 1977. *Radionuclide Uptake by Cultivated Crops.* HASL-321, Health and Safety Laboratory, New York.

Hawthorne, H. A. 1967. Field studies of the transfers of ^{137}Cs from fallout to milk. pp. 77-85. IN B. Aberg and F. P. Hungate (eds.). *Radiological Concentration Processes, Proceedings of an International Symposium in Stockholm, Sweden, April 1966.*

Heinemann, K. and Vogt, K. J. In press. Messungen zur ablagerung und biologischen halbwertszeit von jod auf vegetation. *Proceedings of the 12th Annual Symposium of the Fachverband fur Strahlenschutz, October 2-6, 1978, Norderney, Federal Republic of Germany.*

Hill, C. R. 1965. Polonium-210 in man. *Nature* 208(5009): 423-428.

Hoffman, F. O. 1977. A reassessment of the deposition velocity in the prediction of the environmental transport of radioiodine from air to milk. *Health Phys.* 32(5): 437-441.

Hoffman, F. O. 1979. The coefficient for the transfer of radionuclides from animal intake to milk F_m. IN Hoffman, F. O. and C. F. Baes, III (eds.). *A Statistical Analysis of Selected Parameters for Predicting Food Chain Transport and Internal Dose of Radionuclides. Final Report.* ORNL/NUREG/TM-282.

Hoffman, F. O. and C. F. Baes, III (eds.). 1979. *A Statistical Analysis of Selected Parameters for Predicting Food Chain Transport and Internal Dose of Radionuclides. Final Report.* ORNL/NUREG/TM-282.

Holtzman, R. B. 1966a. Natural levels of lead-210, polonium-210 and radium-226 in humans and biota of the arctic. *Nature* 210: 1094-1097.

Holtzman, R. B. 1966b. ^{226}Ra and the natural airborne nuclides ^{210}Pb and ^{210}Po in arctic biota. pp. 1087-1096. IN Snyder, W. S. (ed.). *Proceedings of the First International Congress of Radiation Protection.* IRPA. Rome, 5-10 September 1966.

Holzworth, G. C. 1972. *Mixing Heights, Wind Speeds and Potential for Urban Air Pollution throughout the Contiguous United States.* Publication No. AP-101. U.S. Environmental Protection Agency, Office of Air Programs, Research Triangle Park, N.C. 27711.

Horst, T. W. 1977. A surface depletion model for deposition from a Gaussian plume. *Atmos. Environ.* 11: 41-46.

Hosker, R. P., Jr. 1974. Estimates of dry deposition and plume depletion over forests and grassland. pp. 29-309. IN *Physical Behavior of Radioactive Contaminants in the Atmosphere*. Proc. of a Symposium jointly organized by the IAEA and the World Meteorological Organization. Vienna, 12-16 November 1973.

John, M. K. and C. J. Van Laerhoven. 1972. Lead distribution in plants grown on a contaminated soil. *Environ. Lett.* 3(2): 111-116.

Johnson, J. E., G. M. Ward, E. Firestone, and K. L. Knox. 1968. Metabolism of radioactive cesium (^{134}Cs and ^{137}Cs) and potassium by dairy cattle as influenced by high and low forage diets. *J. Nutr.* 94: 282-288.

Kerin, D. and Z. Kerin. 1971. Lead contamination of milk and honey caused by industrial lead aerosols. *Prot. Vitae* 2: 61-62. IN *Kettering Abstracts* 9(240): 206-207.

Killough, G. G. and L. R. McKay. 1976. *A Methodology for Calculating Radiation Doses from Radioactivity Released to the Environment.* ORNL-4992.

Killough, G. G. and P. S. Rohwer. 1978. A new look at the dosimetry of ^{14}C released to the atmosphere as carbon dioxide. *Health Phys.* 34: 141-159.

Killough, G. G., D. E. Dunning, Jr., S. R. Bernard, and J. C. Pleasant. 1978. *Estimates of Internal Dose Equivalent to 22 Target Organs for Radionuclides Occurring in Routine Releases from Nuclear Fuel-Cycle Facilities. Vol. 1.* ORNL/NUREG/TM-190.

Kirchmann, R., A. Lafontaine, J. van der Hoek, and G. Koch. 1972. Comparison of the rate of transfer to cow milk of ^{226}Ra from drinking water and ^{226}Ra incorporated in hay. *C. R. Soc. Biol.* 166(11): 1557-1562.

Kirchmann, R., R. Boulenger, and A. LaFontaine. 1968. Absorption of ^{226}Ra in cultivated plants. pp. 1045-1051. IN W. S. Snyder *et al.* (eds.). *Proceedings of the IRPA Congress on Radiation Protection.* Rome, 1966, Vol. II, Pergamon Press.

Kocher, D. C. (ed.). 1977. *Nuclear Decay Data for Radionuclides Occurring in Routine Releases from Nuclear Fuel Cycle Facilities.* ORNL/NUREG/TM-102.

Kocher, D. C. 1979. *Dose-Rate Conversion Factors for External Exposure to Photon and Electron Radiation from Radionuclides Occurring in Routine Releases from Nuclear Fuel Cycle Facilities.* ORNL/NUREG/TM-283.

Lidén, K., and M. Gustafsson. 1967. Relationships and seasonal variation of ^{137}Cs in lichen, reindeer and man in Northern Sweden 1961 to 1965. p. 193. IN *Proceedings of International Symposium, Stockholm, 1966.* Pergamon Press, Oxford, 1967.

Lynch, G. P., D. G. Cornell, and D. F. Smith. 1974. Excretion of cadmium and lead into milk. pp. 470-474. IN Hoekstra, W. G., J. W. Suttie, H. E. Ganther, and W. Mertz (eds.). *Trace Element Metabolism in Animals - 2.* University Park Press, Baltimore, Md.

McInroy, J. F. 1973. *Polonium-210 Metabolism in Ruminants.* Ph.D. Dissertation. Colorado State University. Fort Collins, Colo.

Markee, E. H., Jr. 1967. A parametric study of gaseous plume depletion by ground surface adsorption. pp. 602-614. IN Mawson, C. A. (ed.). *USAEC Meteorological Information Meeting, September 11-14, 1967.* AECL-2787.

Mills, M. T. and M. Reeves. 1973. *A Multi-Source Atmospheric Transport Model for Deposition of Trace Contaminant.* ORNL/NSF/EATC/2.

Miller, C. W. 1979a. The interception Fraction. IN Hoffman, F. O. and C. F. Baes, III (eds.). *A Statistical Analysis of Selected Parameters for Predicting Food Chain Transport and Internal Dose of Radionuclides. Final Report.* ORNL/NUREG/TM-282.

Miller, C. W. 1979b. Validation of a model to predict aerosol interception by vegetation. IN *International Symposium on Biological Implications of Radionuclides Released from Nuclear Industries.* IAEA-SM-237/53. Vienna, 26-30 March 1979.

Miller, C. W., F. O. Hoffman, and D. L. Shaeffer. 1978. The importance of variations in the deposition velocity assumed for the assessment of airborne radionuclide releases. *Health Phys.* 34: 730-734.

Moore, R. E. 1978. *AREAS: A Computer Code for Estimating Air Pollutant Concentrations from Dispersed Sources.* ORNL/TM-6364.

Moore, R. E. 1977. *The AIRDOS-II Computer Code for Estimating Radiation Dose to Man from Airborne Radionuclides in Areas Surrounding Nuclear Facilities.* ORNL-5245.

Mordberg, E. L., V. M. Aliksandruk, G. F. Kovygin, I. I. Shevckenko, V. M. Blyumshtein, and G. F. Yushkevich. 1976. Translocation of isotopes of the uranium-radium series into the grain of some agricultural crops. *Gig. Sanit.* 2: 58-61 (Abstract only, *Chem. Abstr.* 84: 134563).

Morrison, Frank B. 1956. *Feeds and Feeding. A Handbook for the Student and Stockman.* 22nd ed. The Morrison Publishing Co., Ithaca, New York.

Nelmes, A. J., R. St. J. Buxton, F. A. Fairweather, and A. E. Martin. 1974. The implication of the transfer of trace metals from sewage sludge to man. pp. 145-153 IN *Proceedings of the University of Missouri 8th Annual Conference on Trace Substances in Environmental Health.*

Ng, Y. C., C. A. Burton, S. E. Thompson, R. K. Tandy, H. K. Kretner, and M. W. Pratt. 1968. Prediction of the maximum dosage to man from the fallout of nuclear devices. IN *Handbook for Estimating the Maximum Internal Dose from Radionuclides Released to the Biosphere.* UCRL-50163, pt. IV. Lawrence Radiation Laboratory.

Ng, Y. C., C. S. Colsher, D. J. Quinn, and S. E. Thompson. 1977. *Transfer Coefficients for the Prediction of the Dose to Man via the Forage-Cow-Milk Pathway from Radionuclides Released to the Biosphere.* UCRL-51939, Lawrence Livermore Laboratory.

Ng, Y. C., W. A. Phillips, Y. E. Ricker, R. K. Tandy, and S. E. Thompson. 1978. *Methodology for Assessing Dose Commitment to Individuals and to the Population from Ingestion of Terrestrial Foods Contaminated by Emissions from a Nuclear Fuel Reprocessing Plant at the Savannah River Plant - Draft Report.* UCID-17743.

Pasquill, F. 1961. The estimation of the dispersion of windborne material. *Meteorol. Mag.* 90: 33.

Pleasant, J. C. 1979. *INGDOS - A Conventional Computer Code to Implement U.S. Nuclear Regulatory Guide 1.109 Models for Estimation of Annual Doses from Ingestion of Atmospherically Released Radionuclides in Food.* ORNL/TM-6100.

Price, K. R. 1972. *Uptake of ^{237}Np, ^{239}Pu, ^{241}Am, and ^{244}Cm from Soil by Tumbleweed and Cheatgrass.* AEC Research and Development Report. BNWL-1688.

Rabinowitz, M. 1972. Plant uptake of soil and atmospheric lead in Southern California. *Chemosphere* 1(4): 175-180.

Rediske, J. H., J. F. Cline, and A. A. Selders. 1955. *The Absorption of Fission Products by Plants.* HW-36734.

Romney, E. M., A. J. Steen, R. A. Wood, and W. A. Rhoads. 1966. Concentration of radionuclides by plants grown on ejecta from the sedan thermonuclear cratering detonation. pp. 391-398. IN *Radioecological Concentration Processes.* Proceedings of International Symposium, Stockholm, Sweden.

Romney, E. M., H. M. Mork, and K. H. Larson. 1970. Persistence of plutonium in soil, plants, and small mammals. *Health Phys.* 19: 487-491.

Romney, E. M., J. W. Neel, H. Nishita, J. H. Olafson, and K. H. Larson. 1957. Plant uptake of ^{90}Sr, ^{91}Y, ^{106}Ru, ^{137}Cs, and ^{144}Ce from soils. *Soil Sci.* 83: 369-376.

Rupp, A. F., S. E. Beall, L. P. Bornwasser, and D. H. Johnson. 1948. *Dilution of Stock Gasses in Cross Winds.* USAEC Report AECD-1811 (CE-1620). Clinton Laboratories.

Rupp, E. M. 1979. Dietary intake and inhalation rates U_{ap}. IN Hoffman, F. O. and C. F. Baes, III (eds.). *A Statistical Analysis of Selected Parameters for Predicting Food Chain Transport and Internal Dose of Radionuclides. Final Report.* ORNL/NUREG/TM-282.

Sansom, B. F. 1964. The transfer of plutonium-239 from the diet of a cow to its milk. *Br. Vet. J.* 120: 158-161.

Schulz, R. K. 1965. Soil chemistry of radionuclides. *Health Phys.* 11: 1317-1324.

Schulz, P. K., G. A. Tompkins, and K. J. Babock. 1975. Uptake of plutonium and americium by plants from soil: uptake by wheat from various soils and effect of oxidation of plutonium added to soil. IN *Proceedings of International Symposium on Transuranium Nuclides in the Environment.* San Francisco, 17-21 November 1975, Vienna, IAEA (1976) as quoted by Bulman, R. A. 1976. *Concentration of Actinides in the Food Chain.* NRPB-R44, Harwell, Didcot, OXon. OX11 ORQ. June 1976.

Sehmel, G. A., S. L. Sutter, and M. T. Dana. 1973. Dry deposition processes. pp. 43-49. IN *Pacific Northwest Laboratory Annual Report for 1972 to the USAEC Division of Biomedical and Environmental Research. Volume II Physical Sciences, Part 1 Atmospheric Sciences.* BNWL-1751 PT1.

Shor, R. W. and D. E. Fields. 1979a. Animal feed consumption rate Q_F. IN Hoffman, F. O. and C. F. Baes, III (eds.). *A Statistical Analysis of Selected Parameters for Predicting Food Chain Transport and Internal Dose of Radionuclides. Final Report.* ORNL/NUREG/TM-282.

Shor, R. W. and D. E. Fields. 1979b. The fraction of total feed composed of fresh forage F_s and the fraction of the year fresh forage is utilized F_p. IN Hoffman, F. O. and C. F. Baes, III (eds.). *A Statistical Analysis of Selected Parameters for Predicting Food Chain Transport and Internal Dose of Radionuclides. Final Report.* ORNL/NUREG/TM-282.

Slade, D. H. (ed.). 1968. *Meteorology and Atomic Energy - 1968.* U.S. Atomic Energy Commission/Division of Technical Information.

Spector, William S. 1956. *Handbook of Biological Data.* W. B. Saunders Co., Philadelphia. p. 187.

Squire, H. M., L. J. Middleton, B. F. Sansom, and C. R. Coid. 1958. Experiments on the metabolism of certain fission products in dairy cows. pp. 207-219. Extermann, R. C. (ed.). IN *Radioisotopes in Scientific Research*, Vol. IV, Pergamon Press.

Stanley, R. E., A. A. Mullen, and E. W. Bretthauer. 1971. Transfer to milk of ingested radiolead. *Health Phys.* 21: 211-215.

Taskayev, A. K., V. Ya. Ovchenkov, R. M. Aleksakhin, and I. I. Shirktomova. 1977. Uptake of ^{226}Ra by plants and change in its state in the soil-plant tops-litterfall system. *Pochvovedeniye* 2: 42-48.

Ter Haar, G. 1979. Air as a source of lead in edible crops. *Environ. Sci. Technol.* 4(3): 226-230.

Turner, D. B. 1969. *Workbook of Atmospheric Dispersion Estimates*. Air Pollution Control Administration. Cincinnati, Ohio.

U.S. Nuclear Regulatory Commission. 1977. Regulatory Guide 1.109, *Calculation of Annual Doses to Man from Routine Releases of Reactor Effluents for the Purpose of Evaluating Compliance with 10 CFR Part 50* Appendix I (Revision 1). Office of Standards Development.

Van der Hoven. I. 1968. Deposition of particles and gasses. pp. 202-208. IN Slade, D. (ed.). *Meteorology and Atomic Energy - 1968*. U.S. Atomic Energy Commission. USAEC TID-24190.

Vavilov, P. P., O. N. Papova, and R. P. Kodaneva. 1964. The behavior of radium in plants. *Dokl. Akad. Nauk.-S.S.S.R.* 517: 992-994 [translated abstract *Nucl. Sci. Abstr.* 19(2): 2016].

Ward, G. M. and J. E. Johnson. 1965. The cesium-137 content of beef from dairy and feed-lot cattle. *Health Phys.* 11: 95-100.

Ward, G. M., J. E. Johnson, and H. F. Stewart. 1965. ^{137}Cs passage from precipitation to milk. pp. 703-710. IN A. W. Klement, Jr. (ed.). *Radioactive Fallout from Nuclear Weapons Tests*. USAEC Symposium Series #5.

Watters, R. L., J. E. Johnson, and W. R. Hansen. 1969. *A Study of Unsupported Polonium-210 for Ion Exchange in Soil and Uptake in Vegetation*. COO-1733-3, Colorado State University, Fort Collins, Colo.

Wildung, R. E., T. R. Garland, and D. A. Cataldo. 1977. Accumulation of technetium by plants. *Health Phys.* 32: 314-317.

Wilson, D. O. and J. F. Cline. 1966. Removal of plutonium-239, tungsten-185, and lead-210 from soils. *Nature* 209: 941-942.

Zimdahl, R. L., D. T. McCreary, and S. M. Gwynn. 1978. Lead uptake by plants - the influence of lead source. *Bull. Environ. Contam. Toxicol.* 19(4): 431-435.

Appendix A

LISTING OF THE AIRDOS-EPA CODE

```
C
C                    AIRDOS-EPA CODE
C
C       R. E. MOORE  HEALTH AND SAFETY RESEARCH DIV.  ORNL
C
C
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD, ACON(36,20,
     >  20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11), ORMODI(36,12,8)
     > , VD(36),VDCOEF(20,20),NOL,NOU,NRL,NRU
      REAL*8 NAMNUC
      INTEGER OPTION(9)
      REAL*8 WORD,OPT
      DATA OPT/'OPTIONS '/
      READ(50,9004)WORD,OPTION
      IF (WORD.NE.OPT) GO TO 20
      WRITE(51,9005)
      WRITE(51,9006)
      WRITE(51,9007)
      IF (OPTION(1).EQ.1) WRITE(51,9008)
      IF (OPTION(1).EQ.2) WRITE(51,9017)
      IF (OPTION(2).EQ.1) WRITE(51,9009)
      IF (OPTION(2).EQ.0) WRITE(51,9019)
      IF (OPTION(1).NE.2) GO TO 10
      CALL DIRECT(OPTION(2))
      CALL DOSEN
      STOP
   10 IF (OPTION(3).EQ.0) WRITE(51,9011)
      IF (OPTION(3).EQ.1) WRITE(51,9010)
      IF (OPTION(4).EQ.0) WRITE(51,9012)
      IF (OPTION(4).EQ.1) WRITE(51,9013)
      IF (OPTION(5).EQ.1.AND.OPTION(2).EQ.1) WRITE(51,9015)
      IF (OPTION(5).EQ.1.AND.OPTION(2).NE.1) WRITE(51,9016)
      IF (OPTION(5).EQ.1.AND.OPTION(2).NE.1) STOP
      IF (OPTION(6).NE.0) WRITE(51,9018)OPTION(6)
      IF (OPTION(7).EQ.1) WRITE(51,9000)
      IF (OPTION(8).EQ.1) WRITE(51,9001)
      IF (OPTION(9).EQ.1) WRITE(51,9002)
      IF (OPTION(4).EQ.2) WRITE(51,9014)
      CALL CONCEN(OPTION(2),OPTION(3),OPTION(4),OPTION(5),OPTION(6),
     > OPTION(7),OPTION(8),OPTION(9),&20)
      IF (OPTION(1).EQ.0) CALL DOSEN
      STOP
   20 WRITE(51,9003)WORD
      STOP 10
 9000 FORMAT(' ',T30,'THE CALCULATIONS ARE MADE FOR A UNIFORM CIRCULAR A
     >REA SOURCE')
 9001 FORMAT(' ',T30,'THE MAIN OUTPUT TABLE IN SUBROUTINE CONCEN IS NOT
     >PRINTED')
 9002 FORMAT(' ',T30,'THE CHI/Q TABLES ARE NOT PRINTED')
 9003 FORMAT('0ERROR IN DATA DECK.  PROGRAM TERMINATED.  WORD=',A8)
 9004 FORMAT(A8,5I1,I2,3I1)
 9005 FORMAT('1',T50,'OUTPUT OF AIRDOS-EPA COMPUTER CODE')
 9006 FORMAT('0')
 9007 FORMAT(' ',T20,'OPTIONS SELECTED--')
 9008 FORMAT('0',T30,'PROGRAM TERMINATED AFTER PRINTING RADIONUCLIDE CON
     >CENTRATIONS')
 9009 FORMAT(' ',T30,'RADIONUCLIDE CONCENTRATIONS ARE LISTED FOR DIRECTI
     >ON AND DISTANCE FROM FACILITY')
 9010 FORMAT(' ',T30,'RADIONUCLIDE CONCENTRATIONS LISTED ARE PLUME CENTE
     >RLINE VALUES')
 9011 FORMAT('0',T30,'RADIONUCLIDE CONCENTRATIONS LISTED ARE SECTOR-AVER
     >AGED VALUES')
 9012 FORMAT(' ',T30,'PLUME RISE IS COMPUTED FOR BUOYANT PLUMES BY BRIGG
     >S EQUATIONS')
 9013 FORMAT(' ',T30,
     > 'PLUME RISE IS COMPUTED FOR MOMENTUM-TYPE EMISSIONS')
```

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 9014 FORMAT(' ',T30,'SPECIFIC PLUME RISE USED FOR EACH AIR STABILITY CL
     >ASS (METERS)-')
 9015 FORMAT('0',T30,'DEPOSITION VELOCITY IS VARIED WITH DIRECTION AND D
     >ISTANCE')
 9016 FORMAT('0',T30,'ERROR--ILLEGAL USE OF VARIABLE DEPOSITION VELOCITY
     > WITH SQUARE GRID')
 9017 FORMAT('0',T30,'DOSES ARE CALCULATED FROM INPUT AIR CONCENTRATIONS
     > AND GROUND DEPOSITION RATES')
 9018 FORMAT(' ',T30,'AIR CONCENTRATIONS AND GROUND DEPOSITION RATES ARE
     > PUNCHED ON CARDS FOR THE FIRST ',I2,' RADIONUCLIDES')
 9019 FORMAT(' ',T30,'THE ASSESSMENT AREA IS A 20 BY 20 SQUARE GRID')
      END
      SUBROUTINE CONCEN(LORT,LOST,LRISE,LDEP,LPUN,LARE,LTAB,LCHI,*)
C
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD, ACON(36,20,
     >  20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11), ORMODI(36,12,8)
     > , VD(36),VDCOEF(20,20),NCL,NOU,NFL,NRU
      COMMON /PCOM/ REL(6,36),IDIST(20),NUMST
      COMMON /FCOM/ FEQWL,INTPA(20,20)
      REAL*8 NAMNUC,WORD
C
      REAL*8 W1,W2,W3,W4
      DIMENSION AA(7,4,4),DIA(6),FRAW(7,16),PERD(16),AVON(20,20), PH(6),
     >  PR(7),QH(6), SC(36),TAI(36),TG(3),TGD(36), UDAV(7,16), UDCAT(7,
     > 16),VEL(6),VG(36), NOMA(36),NSPTMO(20,20), NSPTM1(20,10),
     > FDSTOR(36,6,7),BOUND(21),LIST(20)
      DIMENSION DIM(6)
      DATA NOMA/36*0/,ALPH/'     '/
      DATA W1/'AREA    '/,W2/'AIR     '/,W3/'STACKS  '/,W4/'NUCLIDES'/
      EQUIVALENCE (NSPTMO(1,11),NSPTM1(1,1))
      DATA NSPTMO/ 07,07,07,07,08,08,08,08,09,09,09,09,10,10,10,10,11,
     > 11,11,11, 07,07,07,07,08,08,08,08,09,09,09,09,10,10,10,10,11,11,
     > 11,11, 07,07,07,07,07,08,08,08,08,09,09,10,10,10,10,11,11,11,11,
     > 11, 07,07,07,07,07,07,08,08,08,09,09,10,10,10,11,11,11,11,11,11,
     > 06,06,07,07,07,07,08,08,08,09,09,10,10,10,11,11,11,11,12,12, 06,
     > 06,06,07,07,07,07,08,08,09,09,10,10,11,11,11,11,12,12,12, 06,06,
     > 06,06,06,07,07,07,08,09,09,10,11,11,11,12,12,12,12,12, 06,06,06,
     > 06,06,06,07,07,08,09,09,10,11,11,12,12,12,12,12,12, 05,05,06,06,
     > 06,06,06,06,07,08,10,11,12,12,12,12,12,12,13,13, 05,05,05,05,05,
     > 05,05,05,06,07,11,12,13,13,13,13,13,13,13,13/
      DATA NSPTM1/ 05,05,05,05,05,05,05,05,04,03,15,14,13,13,13,13,13,
     > 13,13,13, 05,05,04,04,04,04,04,04,03,02,16,15,14,14,14,14,14,14,
     > 13,13, 04,04,04,04,04,04,03,03,02,01,01,16,15,15,14,14,14,14,14,
     > 14, 04,04,04,04,04,03,03,03,02,01,01,16,15,15,15,14,14,14,14,14,
     > 04,04,04,03,03,03,03,02,02,01,01,16,16,15,15,15,15,14,14,14, 04,
     > 04,03,03,03,03,02,02,02,01,01,16,16,16,15,15,15,15,14,14, 03,03,
     > 03,03,03,03,02,02,02,01,01,16,16,16,15,15,15,15,15,15, 03,03,03,
     > 03,03,02,02,02,02,01,01,16,16,16,16,15,15,15,15,15,15, 03,03,03,03,
     > 02,02,02,02,01,01,01,01,16,16,16,16,15,15,15,15, 03,03,03,03,02,
     > 02,02,02,01,01,01,01,16,16,16,16,15,15,15,15/
C
C-----THIS ARRAY HOLDS THE VALUES FOR CONSTANTS ASSOCIATED WITH EACH
C-----OF THE 7 PASQUILL AIR STABILITY CATAGORIES (A,C,D,F).
C
      DATA AA/.9757,.9986,.9767,.9600,.9615,.9733,.9986, .8660,.8493,
     > .8540,.8670,.8670,.8540,.8360, .8660,.8493,.8540,.8670,.8670,
     > .8540,.8360, .6294,.6303,.6254,.6342,.6260,.6342,.8360, 3.928,
     > 6.205,7.623,10.00,14.13,21.28,31.03, 1.841,2.213,3.266,5.261,
     > 7.357,9.333,10.093, 1.841,2.213,3.266,5.261,7.357,9.333,10.093,
     > .2083,.2946,.3977,.6166,.8042,1.233,10.093, 1.000,1.000,.9540,
     > .8061,.8600,.8823,.8257, 1.000,1.000,.8330,.6715,.6290,.6321,
     > .6547, 1.000,1.000,.8330,.5099,.4054,.3710,.3818, 1.000,1.000,
     > .5524,.5251,.1110,.1106,.1106, 5.020,8.350,10.015,7.48,15.50,
     > 34.70,61.25, 5.020,8.350,4.400,2.950,3.150,6.132,18.80, 5.020,
     > 8.350,4.400,.8100,.5240,.7640,2.115, 5.020,8.350,.3320,.9300,
     > .0349,.0694,.1739/
C
C---END OF DECLARATIONS
```

```
C
      DO 20 NO=1,20
         DO 10 NR=1,20
   10       VDCOEF(NO,NR)=1.
   20    CONTINUE
      READ(50,9008) NOL,NOU,NRL,NRU
      READ(50,9009) PR
      READ(50,9011) WORD
      IF (WORD.NE.W1) RETURN 1
      READ(50,9009) SQSD
      READ(50,9000) SEQWL
      READ(50,9008) IDIST
      READ(50,9011) WORD
      IF (WORD.NE.W2) RETURN 1
      READ(50,9008) LIDA1
      READ(50,9009) RR,TA,TG
      READ(50,9010) PERD
      READ(50,9010) ((UDCAT(I,J),J=1,16),I=1,7)
      READ(50,9010) (( UDAV(I,J),J=1,16),I=1,7)
      READ(50,9012) FRAW
      READ(50,9011) WORD
      IF (WORD.NE.W3) RETURN 1
      READ(50,9008) NUMST
      DO 30 J=1,NUMST
   30    READ(50,9009) PH(J),DIA(J),VEL(J),QH(J),DIM(J)
      READ(50,9011) WORD
      IF (WORD.NE.W4) RETURN 1
      READ(50,9008) NNUCS
      DO 40 I=1,NNUCS
         READ(50,9011)  NAMNUC(I)
         READ(50,9009) ANLAM(I),SC(I),VD(I),VG(I)
   40    READ(50,9009) (REL(J,I),J=1,NUMST)
      IF (LDEP.NE.1) GO TO 50
      READ(50,9009)  (BOUND(I),I=2,21)
      READ(50,9059)  ((VDCOEF(I,J),J=NRL,NRU),I=NOL,NOU)
      READ(50,9060)  LIST
      BOUND(1)=0.0
   50 LID1=LIDA1
      FEQWL=SEQWL
      LA1=LIDA1
      IF (LIDA1.EQ.10000) LA1=ALPH
      IF (LRISE.EQ.2) WRITE(51,9014) PR
      WRITE(51,9013)
      WRITE(51,9015)
      WRITE(51,9013)
      WRITE(51,9013)
      WRITE(51,9016) TA
      WRITE(51,9017)
      WRITE(51,9018) TG(1)
      WRITE(51,9019) TG(2)
      WRITE(51,9020) TG(3)
      WRITE(51,9022) RR
      WRITE(51,9021) LA1
      WRITE(51,9023) NUMST
      WRITE(51,9013)
      WRITE(51,9013)
      WRITE(51,9024)
      WRITE(51,9013)
```

```
      WRITE(51,9025)
      WRITE(51,9026)
      WRITE(51,9027) (PH(I),I=1,NUMST)
      WRITE(51,9028) (DIA(I),I=1,NUMST)
      WRITE(51,9029) (VEL(I),I=1,NUMST)
      WRITE(51,9030) (QH(I),I=1,NUMST)
      IF (LARE.EQ.1) WRITE(51,9066) (DIM(I),I=1,NUMST)
      WRITE(51,9035)
      WRITE(51,9036)
      WRITE(51,9037)
      WRITE(51,9013)
      DO 70 J=1,NUMST
         DO 60 I=1,NNUCS
            WRITE(51,9038) J,NAMNUC(I),REL(J,I)
   60       CONTINUE
   70    CONTINUE
      WRITE(51,9039)
      WRITE(51,9040)
      WRITE(51,9041)
      WRITE(51,9042)
      WRITE(51,9013)
      DO 80 I=1,NNUCS
         WRITE(51,9043) NAMNUC(I),VG(I),VD(I),SC(I),ANLAM(I)
   80    CONTINUE
C
      WRITE(51,9031)
      WRITE(51,9013)
      WRITE(51,9032)
      WRITE(51,9033)
      WRITE(51,9013)
      DO 90 MO=1,16
         WRITE(51,9034) MO,(FRAW(I,MO),I=1,7)
   90    CONTINUE
      WRITE(51,9044)
      WRITE(51,9013)
      WRITE(51,9045)
      WRITE(51,9046)
      WRITE(51,9047)
      WRITE(51,9013)
      DO 100 I=1,16
         WRITE(51,9048) I,PERD(I),UDCAT(1,I),UDCAT(2,I),UDCAT(3,I),
     >    UDCAT(4,I),UDCAT(5,I),UDCAT(6,I),UDCAT(7,I)
  100    CONTINUE
      WRITE(51,9049)
      WRITE(51,9050)
      WRITE(51,9013)
      WRITE(51,9045)
      WRITE(51,9046)
      WRITE(51,9047)
      WRITE(51,9013)
      DO 110 I=1,16
         WRITE(51,9051) I,PERD(I),UDAV(1,I),UDAV(2,I),UDAV(3,I),UDAV(4,I)
     >     , UDAV(5,I),UDAV(6,I),UDAV(7,I)
  110    CONTINUE
      WRITE(51,9049)
      IF (LDEP.NE.1) GO TO 130
      WRITE(51,9061)
      WRITE(51,9062)
```

```
      WRITE(51,9063)
      WRITE(51,9013)
      DO 120 I=NOL,NOU
         DO 120 J=NRL,NRU
            WRITE(51,9064)I,IDIST(J),VDCOEF(I,J)
  120       CONTINUE
      IF (LTAB.EQ.1) GO TO 150
  130 WRITE(51,9052)
      WRITE(51,9053)
      WRITE(51,9054)
      IF (LORT.EQ.0) GO TO 140
      WRITE(51,9055)
      WRITE(51,9056)
      WRITE(51,9013)
      GO TO 150
  140 WRITE(51,9057)
      WRITE(51,9013)
  150 CONTINUE
      DO 170 J=1,NUMST
         DO 160 I=1,NNUCS
  160       REL(J,I)=REL(J,I)*3.17098E4
  170    CONTINUE
C---END OF INPUT ROUTINE
C
C---THIS SUBROUTINE CALCULATES AIR CONCENTRATION(ACON)
C---AND GROUND DEPOSITION RATE(GCON)
      DO 180 K=1,20
         DO 180 J=1,20
            DO 180 I=1,36
               AVON(J,K)=0.
               ACON(I,J,K)=0.
  180          GCON(I,J,K)=0.
C-----IF(EXP(-(ANLAM(I)*SQRT(2*10*SQSD**2)/(2*8.64E4)).LT.0.99))
C-----REDUCES TO
C-----IF(ANLAM(I).GT.(122.188054/SQSD))
      DISTG=122.188054/SQSD
C
C-----THIS BLOCK EXAMINES CERTAIN INPUT VALUES FOR EQUALITY.  IF THEY
C-----ARE EQUAL, THEN MUCH OF THE FOLLOWING CALCULATION NEED NOT BE
C-----PERFORMED FOR THAT NUCLIDE.  NOMA IS THE ARRAY OF FLAGS THAT
C-----EQUALITY HAS BEEN FOUND & WITH WHICH NUCLIDE.
C
      DO 190 I=2,NNUCS
         IEN=I-1
         DO 190 M=1,IEN
            IF (REL(1,M).EQ.0) GO TO 190
            IF (VD(I).NE.VD(M)) GO TO 190
            IF (VG(I).NE.VG(M)) GO TO 190
            IF (SC(I).NE.SC(M)) GO TO 190
            IF (ANLAM(I).GT.DISTG) GO TO 190
            IF (ANLAM(M).GT.DISTG) GO TO 190
            NOMA(I)=M
            M=IEN
  190       CONTINUE
      IF (LORT.EQ.1.AND.NOU.GT.16) STOP10
C
C-----THIS BLOCK LOOPS THRU THE GRID COVERING THE AREA AROUND THE PLANT.
C
```

```
      DO 680 NO=NOL,NOU
         DO 200 I=1,NNUCS
            IF (LDEP.NE.1) GO TO 210
            DO 200 J=1,NUMST
               DO 200 K=1,7
                  FDSTOR(I,J,K)=1
  200             CONTINUE
  210    DO 670 NR=NRL,NRU
            JFLAG=0
            DO 220 I=1,NNUCS
               TAI(I)=0.
  220          TGD(I)=0.
            IF (LORT.EQ.1) GO TO 240
C-----ROUTINE TO REFINE THE 4 BY 4 BLOCK OF SQUARES AT THE CENTER OF THE
C-----SQUARE GRID BY DIVIDING EACH SQUARE INTO 25 SMALLER SQUARES
            IF (NO.LT.9.OR.NO.GT.12) GO TO 230
            IF (NR.LT.9.OR.NR.GT.12) GO TO 230
            JFLAG=1
            DO 610 NOP=1,5
               DO 610 NRP=1,5
C-----COMPUTE DISTANCE FROM CENTER OF SUBSQUARE TO CENTER OF GRID
                  X=SQRT((11.-NO-(NOP*2.-1.)/10.)**2+(11.-NR-(NRP*2.-1.)
     >              /10.)**2) *SQSD
C-----EACH SUBSQUARE IS EVALUATED IN DIRECTION THAT IT WOULD BE IN IF IT
C-----WERE IN THE SAME POSITION AS A FULL-SIZE SQUARE
                  MO=NSPTMO(5*(NO-9)+NOP,5*(NR-9)+NRP)
                  GO TO 250
  230             X=SQRT( (10.5-NO)*(10.5-NO)+(10.5-NR)*(10.5-NR) ) *
     >             SQSD
                  MO=NSPTMO(NO,NR)
                  GO TO 250
  240             X=IDIST(NR)
                  MO=NO
  250             X0=X
                  THETA=1.0
                  M=0
C
C-----THIS BLOCK LOOPS THRU THE STACKS (EMISSION POINTS).
C
                  DO 600 J=1,NUMST
                     IF (LARE.EQ.0) GO TO 290
C
C-----AREA SOURCE BLOCK (BY CHRISTOPHER B. NELSON,EPA).
C
C... CONSIDER SOURCES TO BE POINT SOURCES IF LESS THAN 10 METERS
C... DIAM. OR IF RATIO OF DISTANCE X TO THE DIAM. IS GREATER THAN 2.5.
C
                     TESTAR=X/(DIM(J)+.00001)
                     IF (DIM(J).LT.10..OR.TESTAR.GT.2.5) GO TO 290
C
C... R0 IS THE RADIUS OF THE SOURCE.
C... R1 IS THE INNER RADIUS OF THE TRANSFORMED SOURCE.
C... R2 IS THE OUTER RADIUS OF THE TRANSFORMED SOURCE.
C... X IS THE EFFECTIVE DISTANCE FOR CALCULATING CHI/Q.
C... THETA IS THE ANGULAR WIDTH IN SECTORS OF THE TRANSFORMED SOURCE.
C... (MULTIPLY THETA BY PI/8.0 TO CONVERT THETA TO RADIANS.)
C... 0.88622693=SQRT(PI/4.)
C... 2.5198421=4.0**(2/3)
```

```
C... 4.5135167=8./SQRT(PI)
C
                    R0=DIM(J)/2.0
                    IF (X0.GT.0.88622693*R0) GO TO 270
                    IF (X0.GT.0.5*R0) GO TO 260
C
C... 0.LE.X0.LE.R0/2.
                    R1=0.
                    R2=R0
                    X=R2/2.5198421
                    THETA=16.
                    GO TO 280
C
C... R0/2.LT.X0.LE.R0*SQRT(PI/4.)
  260               R1=0.
                    R2=2.*X0
                    X=R2/2.5198421
                    THETA=4.0*(R0/X0)**2
                    GO TO 280
C
C... R0*SQRT(PI/4).LT.X0
  270               R1=X0-0.88622693*R0
                    R2=X0+0.88622693*R0
                    X=(X0*(SQRT(R2)+SQRT(R1))/2.0)**0.66666667
                    THETA=4.5135167*R0/X0
C
C... M IS THE NUMBER OF SECTORS ON EACH SIDE OF MO WHICH
C... INCLUDE THE TRANSFORMED SOURCE.
  280               M=INT(THETA/2.0+0.5)
C... DTHETA IS THE ANGULAR WIDTH OF THE TRANSFORMED SOURCE IN THE FIRST
C... AND LAST SECTORS.
                    DTHETA=AMOD((THETA/2.0+0.5),1.0)
                    IF (DTHETA.GT.0.) GO TO 290
                    M=M-1
                    DTHETA=1.0
  290               IF (M.EQ.0) DTHETA=THETA
C... LL IS THE TOTAL NUMBER OF SECTORS WHICH CONTRIBUTE TO CHI/Q.
                    LL=2*M+1
C... L1 IS THE INITIAL SECTOR.
                    L1=MOD(MO-M+15,16)+1
                    DO 580 L=1,LL
                       MO=MOD(L1+L+14,16)+1
                       IF (L.EQ.1.OR.L.EQ.LL) GO TO 300
                       PERW=PERD(MO)/THETA
                       GO TO 310
  300                  PERW=PERD(MO)*DTHETA/THETA
C
C-----END OF AREA SOURCE BLOCK.
C
C-----THIS BLOCK LOOPS THRU THE 7 PASQUILL AIR STABILITY CATEGORIES.
C
  310                  DO 580 JH=1,7
                          IF (FRAW(JH,MO).EQ.0) GO TO 580
                          U = UDAV(JH,MO)
                          UD=UDCAT(JH,MO)
                          IF (U.GT.6.OR.U.LT.1.) GO TO 320
                          FF2=(1.167-U/6.-1./UD) / (1.167-U/6.-1./U)
                          FF3=((U-1.)*(1.-FF2))/5.
```

```
                    FF1=1.-FF2-FF3                             CONC1730
                    GO TO 330                                  CONC1735
  320               FF1=0.                                     CONC1740
                    FF2=1.                                     CONC1745
                    FF3=0.                                     CONC1750
C-----THIS BLOCK CALCULATES PLUME RISE                         CONC1755
C-----RISE=0..BRIGGS' EQUATIONS FOR BUOYANT PLUMES             CONC1760
C-----RISE=1..RUPP'S EQUATIONS FOR MOMENTUM-TYPE EMISSIONS     CONC1765
C-----RISE=2..READ PLUME RISE FROM CARDS                       CONC1770
  330               IF (LRISE.EQ.1) GO TO 360                  CONC1775
                    IF (LRISE.EQ.2) GO TO 370                  CONC1780
                    IF (LRISE.NE.0) STOP11                     CONC1785
                    IF (JH.GT.4) GO TO 340                     CONC1790
                    IF (X.LE.10.*PH(J)) GO TO 350              CONC1795
                    H =PH(J)+(1.6/U*( (.0037000*QH(J)*PH(J)*PH(J) CONC1800
     >               )** .33333333))                           CONC1805
                    GO TO 380                                  CONC1810
  340               S=9.80665/TA*(TG(JH-4)+.0098)              CONC1815
                    IF (X.LE.2.4*U/SQRT(S)) GO TO 350          CONC1820
                    H =PH(J)+(2.9*( (.000037*QH(J)/U/S)**      CONC1825
     >               .33333333 ) )                             CONC1830
                    GO TO 380                                  CONC1835
  350               H =PH(J)+(1.6/U*( (.000037*QH(J)*X*X)**    CONC1840
     >               .33333333 ))                              CONC1845
                    GO TO 380                                  CONC1850
  360               H =PH(J)+1.5*VEL(J)*DIA(J)/U               CONC1855
                    GO TO 380                                  CONC1860
  370               H =PH(J)+PR(JH)                            CONC1865
C     END OF PLUME RISE CALCULATIONS                           CONC1870
  380               NX=1                                       CONC1875
                    IF (X.GT.1000) NX=2                        CONC1880
                    IF (X.GT.3000) NX=3                        CONC1885
                    IF (X.GT.10000) NX=4                       CONC1890
                    A=AA(JH,NX,1)                              CONC1895
                    C=AA(JH,NX,2)                              CONC1900
                    D=AA(JH,NX,3)                              CONC1905
                    F=AA(JH,NX,4)                              CONC1910
C                                                              CONC1915
C-----THIS BLOCK LOOPS THRU THE DIFFERENT NUCLIDES RELEASED IN THE PLUMECONC1920
C                                                              CONC1925
                    DO 570 I=1,NNUCS                           CONC1930
                      IF (NOMA(I).GT.0.AND.J.EQ.1) GO TO 570   CONC1935
C-----DETERMINE XLIDO (VALUE OF X WHERE LID AFFECTS VERTICAL DISPERSION) CONC1940
                      Y1=0.                                    CONC1945
                      Y2=10000.                                CONC1950
                      DO 410 IX1=1,3                           CONC1955
                        DO 390 IX2=1,10                        CONC1960
                          Y=Y1+Y2*IX2                          CONC1965
                          IF (Y**D.GT.(.47*F*(LID1+Y*VG(I)/UD) CONC1970
     >                     )) GO TO 400                        CONC1975
  390                     CONTINUE                             CONC1980
  400                   Y1=Y1+Y2*(IX2-1)                       CONC1985
  410                   Y2=Y2/10.                              CONC1990
                      XLIDO=2.*Y                               CONC1995
C-----THIS BLOCK FINDS DEPLETION FRACTION                      CONC2000
                      VD1=VD(I)                                CONC2005
C-----SECTION TO FIND DEPLETION IF BY VARIABLE DEPOSITION      CONC2010
C-----LDEP=1 IS OPTION FOR VARIABLE DEPOSITION VELOCITY        CONC2015
```

```
C-----BOUND(NR) IS THE LOWER BOUND ON THE INTERVAL OF INTEGRATION
C-----BOUND(NR+1) IS THE UPPER BOUND
                                 IF (LDEP.NE.1) GO TO 480
                                 VD1=VD1*VDCOEF(NO,NR)
                                 IF (X.GT.XLIDO) GO TO 420
                                 CALL QX(BOUND(NR),X,U,UD,H,VD1,VG(I),JH,
     >                            FDD)
                                 GO TO 440
  420                            IF (BOUND(NR).GE.XLIDO) GO TO 430
                                 CALL QX(BOUND(NR),XLIDO,U,UD,H,VD1,VG(I),
     >                            JH, FDD)
                                 FDD=FDD*EXP(-((X-XLIDO)*VD1/(LID1*UD)))
                                 GO TO 440
  430                            FDD=FDD*EXP(-((X-BOUND(NR))*VD1/(LID1*UD))
     >                            )
  440                            FDD=FDD*FDSTOR(I,J,JH)
                                 IF (X.EQ.BOUND(NR+1)) FDSTOR(I,J,JH)=FDD
                                 IF (X.EQ.BOUND(NR+1)) GO TO 530
                                 IF (BOUND(NR+1).GT.XLIDO) GO TO 450
                                 CALL QX(X,BOUND(NR+1),U,UD,H,VD1,VG(I),JH,
     >                             FD1)
                                 GO TO 470
  450                            IF (X.GT.XLIDO) GO TO 460
                                 CALL QX(X,XLIDO,U,UD,H,VD1,VG(I),JH,FD1)
                                 FD1=FD1*EXP(-((BOUND(NR+1)-XLIDO)*VD1/
     >                            (LID1* UD)))
                                 GO TO 470
  460                            FD1=EXP(-((BOUND(NR+1)-XLIDO)*VD1/(LID1*
     >                            UD)))
  470                            FDSTOR(I,J,JH)=FDD*FD1
                                 GO TO 530
C-----END VARIABLE DEPOSITION SECTION
C-----SECTION FOR DEPLETION IF BY CONSTANT DEPOSITION
  480                            IF (X.GT.XLIDO) GO TO 500
                                 IF (VG(I).NE.0) GO TO 490
                                 CALL QY(0,X,U,UD,H,VD1,VG(I),JH,FDD)
                                 GO TO 530
  490                            CONTINUE
                                 CALL QX(0,X,U,UD,H,VD1,VG(I),JH,FDD)
                                 GO TO 530
  500                            CONTINUE
                                 IF (VG(I).NE.0) GO TO 510
                                 CALL QY(0,XLIDO,U,UD,H,VD1,VG(I),JH,FDD)
                                 GO TO 520
  510                            CONTINUE
                                 CALL QX(0,XLIDO,U,UD,H,VD1,VG(I),JH,FDD)
  520                            CONTINUE
                                 FDD=FDD*EXP(-((X-XLIDO)*VD1/(LID1*UD)))
C-----END CONSTANT DEPOSITION SECTION
  530                            CONTINUE
C-----END DEPLETION FRACTION BLOCK
                                 QRED=-ANLAM(I)*X/86400.
                                 QRED=REL(J,I)*FDD*(FF1*EXP(-SC(I)*X)+FF2*
     >                            EXP(-SC(I)*X/U)+FF3*EXP (-SC(I)*X/6.))*
     >                            (FF1* EXP(QRED)+FF2*EXP(QRED/U)+FF3*
     >                            EXP(QRED/6.))
                                 CHAD=QRED/(6.2832*((X**A)/C)*((X**D)/F)*
     >                            UD)
```

```
                         IF ((VG(I)*X)/UD.GE.H) H=(VG(I)*X)/UD
                         IF ((.5*(((((VG(I)*X)/UD)+H)/((X**D)/F))**
     >                    2)).GT.50) BX=0
                         IF ((.5*(((((VG(I)*X)/UD)+H)/((X**D)/F))**
     >                    2)).GT.50) GO TO 540
                         BX=CHAD*(EXP(-.5*(((((VG(I)*X)/UD)-H)/((X*
     >                    *D) /F))**2))+ EXP(-.5*(((((-VG(I)*X)/UD)
     >                    +H)/ ((X**D)/F))**2)))
  540                    BT=BX
                         BU=0
                         VERT=QRED/(2.5066*((X**A)/C)*LID1*UD)
                         IF (X.LE.XLIDO) GO TO 550
                         BT=VERT
                         BU=BT
                         VERT=0
  550                    FRAC=(6.300835*((X**A)/C))/X
                         IF (LOST.EQ.1) FRAC=1.
  560                    FRAC=FRAC*PERW
                         VERT=FRAC*VERT
                         BU =FRAC*BU
                         BT =FRAC*BT
                         IF (I.EQ.1) AVON(NO,NR)=(FRAW(JH,MO)*
     >                    (VERT+BU))/1000000.+AVON(NO,NR)
                         TGD(I)=TGD(I)+FRAW(JH,MO)*(VD1*BT+SC(I)*
     >                    LID1* (VERT+BU))
                         TAI(I)=TAI(I)+FRAW(JH,MO)*BT
  570                    CONTINUE
C-----END OF NUCLIDE LOOP-----------------------------------------------
  580                  CONTINUE
C-----END OF PASQUILL CATAGORY LOOP-------------------------------------
                   DO 590 I=1,NNUCS
                     M=NOMA(I)
                     IF (M.LE.0.OR.J.GT.1) GO TO 590
                     TGD(I)=TGD(M)*REL(J,I)/REL(J,M)
                     TAI(I)=TAI(M)*REL(J,I)/REL(J,M)
  590                CONTINUE
  600              CONTINUE
C-----END OF STACK LOOP-------------------------------------------------
                 IF (JFLAG.NE.1) GO TO 630
  610            CONTINUE
C-----FIND AVERAGE OF CONCENTRATIONS OF SUBSQUARES
           DO 620 I=1,NNUCS
             TGD(I)=TGD(I)/25.
             TAI(I)=TAI(I)/25.
  620        CONTINUE
           AVON(NO,NR)=AVON(NO,NR)/25.
  630      IF (LDEP.EQ.1.AND.LIST(NR).EQ.1) GO TO 670
           IF (LORT.EQ.1) GO TO 650
           DO 640 I=1,NNUCS
             ACON(I,NO,NR)=TAI(I)/1000000.
             GCON(I,NO,NR)=TGD(I)/10000.
             VD1=VD(I)
             DRYCON=ACON(I,NO,NR)*VD1*100
             WETCON=(GCON(I,NO,NR)-DRYCON)*(SC(I)/(SC(I)+1.E-30))
      IF (LTAB.EQ.1) GO TO 670
  640        WRITE(51,9058) NO,NR,NAMNUC(I),ACON(I,NO,NR),DRYCON,
     >        WETCON, GCON(I,NO,NR)
           GO TO 670
```

```
 650        DO 660 I=1,NNUCS                                             CONC2600
               ACON(I,NO,NR)=TAI(I)/1000000.                             CONC2605
               GCON(I,NO,NR)=TGD(I)/10000.                               CONC2610
               VD1=VD(I)                                                 CONC2615
               IF (LDEP.EQ.1) VD1=VD1*VDCOEF(NO,NR)                      CONC2620
               DRYCON=ACON(I,NO,NR)*VD1*100                              CONC2625
               WETCON=(GCON(I,NO,NR)-DRYCON)*(SC(I)/(SC(I)+1.E-30))      CONC2630
      IF (LTAB.EQ.1) GO TO 670                                           CONC2634
 660           WRITE(51,9058) NO,IDIST(NR),NAMNUC(I),ACON(I,NO,NR),      CONC2635
     >          DRYCON,WETCON, GCON(I,NO,NR)                             CONC2640
 670        CONTINUE                                                     CONC2645
 680     CONTINUE                                                        CONC2650
      IF (LCHI.EQ.1) GO TO 690                                           CONC2655
      IF (LORT.EQ.1) CALL CHIQ                                           CONC2660
 690  IF (LPUN.EQ.0) GO TO 710                                           CONC2665
      DO 700 I=1,LPUN                                                    CONC2670
         PUNCH 9065,((ACON(I,NO,NR),NR=1,20),NO=1,20)                    CONC2675
         PUNCH 9065,((GCON(I,NO,NR),NR=1,20),NO=1,20)                    CONC2680
 700     CONTINUE                                                        CONC2685
 710  CONTINUE                                                           CONC2690
      IF (LORT.EQ.1) GO TO 720                                           CONC2695
      ASQSD=((SQSD**2)*400.)/1.E6                                        CONC2700
      WRITE(51,9001)                                                     CONC2705
      WRITE(51,9002)ASQSD                                                CONC2710
      WRITE(51,9003)                                                     CONC2715
      WRITE(51,9004)SQSD                                                 CONC2720
      WRITE(51,9005)                                                     CONC2725
      WRITE(51,9006)                                                     CONC2730
      WRITE(51,9007)                                                     CONC2735
C-----END OF GRID LOOP---------------------------------------------------CONC2740
 720  RETURN                                                             CONC2745
9000  FORMAT(F10.0)                                                      CONC2755
9001  FORMAT('1',T30,'NOTE-THE AREA SURROUNDING THE PLANT IS A SQUARE    CONC2760
     >WITH AN AREA')                                                     CONC2765
9002  FORMAT(' ',T35,'OF',F10.1,1X,                                      CONC2770
     > 'SQUARE KILOMETERS WITH THE PLANT AT THE CENTER.')                CONC2775
9003  FORMAT(' ',T35,'THE SQUARE AREA IS ALIGNED DUE NORTH-SOUTH AND EASCONC2780
     >T-WEST. THE')                                                      CONC2785
9004  FORMAT(' ',T35,'400 SMALLER SQUARES, WHICH ARE EACH ',F7.1,1X,     CONC2790
     > 'METERS ON A SIDE,')                                              CONC2795
9005  FORMAT(' ',T35,'ARE IDENTIFIED BY COLUMN AND ROW. COLUMNS ARE NUMBCONC2800
     >ERED FROM')                                                        CONC2805
9006  FORMAT(' ',T35,'1 TO 20 FROM WEST TO EAST. ROWS ARE NUMBERED FROM CONC2810
     >1 TO 20 FROM')                                                     CONC2815
9007  FORMAT(' ',T35,'SOUTH TO NORTH.')                                  CONC2820
9008  FORMAT(8I10)                                                       CONC2825
9009  FORMAT(8F10.0)                                                     CONC2830
9010  FORMAT(16F5.0)                                                     CONC2835
9011  FORMAT(A8)                                                         CONC2840
9012  FORMAT(7F10.0)                                                     CONC2845
9013  FORMAT('0')                                                        CONC2850
9014  FORMAT(' ',T30,'A',F10.1,'     B',F10.1,'     C',F10.1,'     D',F10.1,  CONC2855
     > '     E',F10.1,'     F',F10.1,'     G',F10.1)                     CONC2860
9015  FORMAT('1',T20,'METEOROLOGICAL AND PLANT INFORMATION SUPPLIED TO PCONC2865
     >ROGRAM----')                                                       CONC2870
9016  FORMAT('0',T30,'AVERAGE AIR TEMPERATURE (DEG K)',T100,F10.1)       CONC2875
9017  FORMAT('0',T30,'AVERAGE VERTICAL TEMPERATURE GRADIENT OF THE AIR (CONC2880
     >DEG K/METER)')                                                     CONC2885
```

```
9018 FORMAT('0',T40,'IN STABILITY CLASS E',T100,F10.4)                  CONC2890
9019 FORMAT('0',T40,'IN STABILITY CLASS F',T100,F10.4)                  CONC2895
9020 FORMAT('0',T40,'IN STABILITY CLASS G',T100,F10.4)                  CONC2900
9021 FORMAT('0',T30,'HEIGHT OF LID (METERS)',T100,I10)                  CONC2905
9022 FORMAT('0',T30,'RAINFALL RATE (CM/YEAR)',T100,F10.2)               CONC2910
9023 FORMAT('0',T30,'NUMBER OF STACKS IN THE PLANT',T100,I10)           CONC2915
9024 FORMAT('0',T30,'STACK INFORMATION--')                              CONC2920
9025 FORMAT('0',T89,'STACK NUMBER')                                     CONC2925
9026 FORMAT('0',T70,'1',T80,'2',T90,'3',T100,'4',T110,'5',T120,'6')     CONC2930
9027 FORMAT('0',T20,'HEIGHT (METERS)',T62,6F10.4)                       CONC2935
9028 FORMAT('0',T20,'DIAMETER (METERS)',T62,6F10.4)                     CONC2940
9029 FORMAT('0',T20,'EFFLUENT VELOCITY (METERS/SEC)',T62,6F10.4)        CONC2945
9030 FORMAT('0',T20,'RATE OF HEAT EMISSION (CAL/SECOND)',T62,6E10.2)    CONC2950
9031 FORMAT('1',T26,'FREQUENCY OF ATMOSPHERIC STABILITY CLASSES FOR EACCONC2955
    >H DIRECTION')                                                      CONC2960
9032 FORMAT('0',T7,'SECTOR',T40,                                        CONC2965
    > 'FRACTION OF TIME IN EACH STABILITY CLASS')                       CONC2970
9033 FORMAT('0',T25,'A',T37,'B',T49,'C',T61,'D',T73,'E',T85,'F',T97,    CONC2975
    > 'G')                                                              CONC2980
9034 FORMAT(' ',T7,I4,T23,F6.4,T35,F6.4,T47,F6.4,T59,F6.4,T71,F6.4,     CONC2985
    > T83,F6.4,T95,F6.4)                                                CONC2990
9035 FORMAT('1',T50,'RELEASE RATES FOR RADIONUCLIDES')                  CONC2995
9036 FORMAT('0',T45,'STACK',T61,'NUCLIDE',T80,'RELEASE RATE')           CONC3000
9037 FORMAT(' ',T80,'(CURIES/YEAR)')                                    CONC3005
9038 FORMAT(' ',T45,I2,T63,A8,T80,E10.3)                                CONC3010
9039 FORMAT('1',T46,'PLUME DEPLETION AND DEPOSITION PARAMETERS')        CONC3015
9040 FORMAT('0',T20,'NUCLIDE',T40,'GRAVITATIONAL',T60,                  CONC3020
    > 'DEPOSITION VELOCITY',T85,'SCAVENGING',T100,                      CONC3025
    > 'EFFECTIVE DECAY CONSTANT')                                       CONC3030
9041 FORMAT(' ',T40,'FALL VELOCITY',T85,'COEFFICIENT',T108,'IN PLUME')  CONC3035
9042 FORMAT(' ',T41,'(METERS/SEC)',T63,'(METERS/SEC)',T87,'(1/SEC)',    CONC3040
    > T108,'(PER DAY)')                                                 CONC3045
9043 FORMAT(' ',T21,A8,T37,F10.3,T61,F10.5,T85,E10.3,T107,E10.3)        CONC3050
9044 FORMAT('1',T36,'FREQUENCIES OF WIND DIRECTIONS AND RECIPROCAL-AVERCONC3055
    >AGED WIND SPEEDS')                                                 CONC3060
9045 FORMAT('0',T20,'WIND TOWARD',T50,'FREQUENCY',T82,                  CONC3065
    > 'WIND SPEEDS FOR EACH STABILITY CLASS')                           CONC3070
9046 FORMAT(' ',T94,'(METERS/SEC)')                                     CONC3075
9047 FORMAT('0',T73,'A',T81,'B',T90,'C',T99,'D',T108,'E',T116,'F',T124,CONC3080
    >  'G')                                                             CONC3085
9048 FORMAT(' ',T25,I2,T52,F5.3,T71,F5.2,T79,F5.2,T88,F5.2,T97,F5.2,    CONC3090
    > T106,F5.2,T114,F5.2,T122,F5.2)                                    CONC3095
9049 FORMAT('0',T20,'WIND DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARCONC3100
    >TING AT 1 FOR DUE NORTH')                                          CONC3105
9050 FORMAT('1',T38,'FREQUENCIES OF WIND DIRECTIONS AND TRUE-AVERAGE WICONC3110
    >ND SPEEDS')                                                        CONC3115
9051 FORMAT(' ',T25,I2,T52,F5.3,T71,F5.2,T79,F5.2,T88,F5.2,T97,F5.2,    CONC3120
    > T106,F5.2,T114,F5.2,T122,F5.2)                                    CONC3125
9052 FORMAT('1',T46,'ESTIMATED RADIONUCLIDE CONCENTRATIONS')            CONC3130
9053 FORMAT('0',T10,'AREA',T30,'NUCLIDE',T42,'AIR CONCENTRATION',T64,   CONC3135
    > 'DRY DEPOSITION RATE',T88,'WET DEPOSITION RATE',T112,             CONC3140
    > 'GROUND DEPOSITION RATE')                                         CONC3145
9054 FORMAT(T47,'(PCI/CC)',T64,'(PCI/SQUARE CM-SEC)',T88,               CONC3150
    > '(PCI/SQUARE CM-SEC)',T113,'(PCI/SQUARE CM-SEC)')                 CONC3155
9055 FORMAT(' WIND TOWARD',T17,'DISTANCE')                              CONC3160
9056 FORMAT(' ',T17,'(METERS)')                                         CONC3165
9057 FORMAT(' ',T4,'COLUMN',T21,'ROW')                                  CONC3170
9058 FORMAT(' ',T6,I2,T18,I6,T31,A8,T45,E10.3,T68,E10.3,T92,E10.3,T118,CONC3175
```

```
    >  E10.3)
9059 FORMAT(10F8.4)
9060 FORMAT(20I1)
9061 FORMAT('1',T50,'DEPOSITION VELOCITY COEFFICIENTS')
9062 FORMAT('0',T37,'DIRECTION',T55,'DISTANCE',T72,
    > 'DEPOSITION COEFFICIENT')
9063 FORMAT(' ',T55,'(METERS)',T78,'(NO UNITS)')
9064 FORMAT(' ',T40,I2,T57,I6,T78,F8.4)
9065 FORMAT(8E10.4)
9066 FORMAT('0',T20,'DIAMETER OF AREA SOURCE (METERS)',T62,6F10.4)
     END
```

```
      SUBROUTINE QY(BND,X,U,UD,HS,VD,VG,INDEX1,QXR)
C
C       R. E. MOORE   HEALTH AND SAFETY RESEARCH DIV.,   ORNL  3-1-78
C
C       A TABLE CALLOUT SUBROUTINE FOR DETERMINING DEPLETION FRACTIONS F
C       DEPOSITION FOR CONSTANT DEPOSITION VELOCITY AND FOR ZERO GRAVITA
C       EFFECT.
C
C       TABULATED VALUES IN DATA STATEMENT WERE DERIVED THROUGH THE USE
C       SUBROUTINE QX, A SIMPSON'S RULE SUBROUTINE WRITTEN ORIGINALLY BY
C       D. E. DUNNING, MODIFIED BY J. F. HULL, AND LATER CHANGED BY
C       D. P. STEWART.
C
      COMMON /QCOM/ REFA(34,7,20)
      DIMENSION XIDI(20),KP(34)
      REAL KP
      INTEGER IDOM
      DATA XIDI/35.,65.,100.,150.,200.,300.,400.,500.,650.,800.,1000.,
     > 1500.,2000.,4000.,7000.,10000.,25000.,60000.,90000.,200000./
      DATA KP/1.,1.5,2.,3.,4.,5.,6.,7.,8.,9.,10.,12.5,15.,17.5,20.,25.,
     > 30.,35.,40.,50.,60.,70.,80.,90.,100.,120.,140.,160.,180.,200.,
     > 240.,260.,300.,400./
      IF (IDOM.EQ.121) GO TO 20
   10 CALL QY1
      CALL QY2
      CALL QY3
      IDOM=121
   20 JH=INDEX1
      H1=HS
      DO 30 ID=1,20
         IF (X.LT.XIDI(ID)) GO TO 50
   30    CONTINUE
   40 ID2=35
      GO TO 60
   50 ID1=ID
      ID2=ID-1
   60 DO 70 KR=1,34
         IF (H1.LT.KP(KR)) GO TO 90
   70    CONTINUE
   80 KP2=21
      GO TO 100
   90 KP1=KR
      KP2=KR-1
  100 IF (KP2.EQ.0.AND.ID2.EQ.0) GO TO 140
      IF (KP2.EQ.0) GO TO 150
      IF (ID2.EQ.0) GO TO 170
      IF (X.GE.200000.) GO TO 110
      IF (H1.GE.400.) GO TO 130
      CUX1=REFA(KP1,JH,ID2)-((REFA(KP1,JH,ID2)-REFA(KP1,JH,ID1))* ((X-
     > XIDI(ID2))/(XIDI(ID1)-XIDI(ID2))))
      CUX2=REFA(KP2,JH,ID2)-((REFA(KP2,JH,ID2)-REFA(KP2,JH,ID1))* ((X-
     > XIDI(ID2))/(XIDI(ID1)-XIDI(ID2))))
     CUXA=CUX1-(((CUX1-CUX2)*(KP(KP1)-H1))/(KP(KP1)-KP(KP2)))
     GO TO 190
  110 IF (H1.GT.400.) GO TO 120
     CUX1=X*((REFA(KP1,JH,20)-REFA(KP1,JH,19))/110000.)+ (REFA(KP1,JH,
```

```
    > 19)-.8181818*(REFA(KP1,JH,20)-REFA(KP1,JH,19)))
      CUX2=X*((REFA(KP2,JH,20)-REFA(KP2,JH,19))/110000.)+ (REFA(KP2,JH,
    > 19)-.8181818*(REFA(KP2,JH,20)-REFA(KP2,JH,19)))
      CUXA=CUX1-(((CUX1-CUX2)*(KP(KP1)-H1))/(KP(KP1)-KP(KP2)))
      GO TO 190
  120 CUM1=H1*((REFA(34,JH,20)-REFA(33,JH,20))/100.)+4.*REFA(33,JH,20)-
    > 3.*REFA(34,JH,20)
      CUM2=H1*((REFA(34,JH,19)-REFA(33,JH,19))/100.)+4.*REFA(33,JH,19)-
    > 3.*REFA(34,JH,19)
      CUXA=((CUM1-CUM2)/110000.)*X+CUM1-1.8181818*(CUM1-CUM2)
      GO TO 190
  130 CUX1=H1*((REFA(34,JH,ID1)-REFA(33,JH,ID1))/100.)+4.*REFA(33,JH,
    > ID1)-3.*REFA(34,JH,ID1)
      CUX2=H1*((REFA(34,JH,ID2)-REFA(33,JH,ID2))/100.)+4.*REFA(33,JH,
    > ID2)-3.*REFA(34,JH,ID2)
      CUXA=((CUX2-CUX1)/(XIDI(ID2)-XIDI(ID1)))*(X-XIDI(ID1))+CUX1
      GO TO 190
  140 CUXA=1.-(1.-REFA(1,JH,1)*(X/XIDI(1)))
      GO TO 190
  150 IF (X.GE.200000.) GO TO 160
      CUXA=REFA(1,JH,ID2)-((REFA(1,JH,ID2)-REFA(1,JH,ID1))* ((X-
    > XIDI(ID2))/(XIDI(ID1)-XIDI(ID2))))
      GO TO 190
  160 CUXA=((REFA(1,JH,20)-REFA(1,JH,19))/110000.)*X+REFA(1,JH,20)-
    > 1.8181818*(REFA(1,JH,20)-REFA(1,JH,19))
      GO TO 190
  170 IF (H1.GT.400.) GO TO 180
      CUX1=1.-(1.-REFA(KP1,JH,1)*(X/XIDI(1)))
      CUX2=1.-(1.-REFA(KP2,JH,1)*(X/XIDI(1)))
      CUXA=CUX1-(((CUX1-CUX2)*(KP(KP1)-H1))/(KP(KP1)-KP(KP2)))
      GO TO 190
  180 CUX1=1.-((1.-REFA(33,JH,1))*(X/XIDI(1)))
      CUX2=1.-((1.-REFA(34,JH,1))*(X/XIDI(1)))
      CUXA=((CUX2-CUX1)/100.)*H1+CUX1-3.*(CUX2-CUX1)
  190 QXR=CUXA**((100.*VD)/UD)
      RETURN
      END
```

```
      SUBROUTINE QY1                                                    QY1
      COMMON /QCOM/ REFA(34,7,20)                                       QY1
      DIMENSION SEFA(34,7,20)                                           QY1
      DIMENSION AA(114),AB(114),AC(114),AD(114),AE(114),AF(114),AG(114),QY1
     > AH(114),AI(114),AJ(114),AK(114),AL(114),AM(114),AN(114),AO(70)   QY1
      EQUIVALENCE (SEFA( 1,1, 1),AA(1)),(SEFA(13,4, 1),AB(1)),(SEFA(25, QY1
     > 7, 1),AC(1)),(SEFA( 3,4, 2),AD(1)),(SEFA(15,7, 2),AE(1)),        QY1
     > (SEFA(27,3, 3),AF(1)),(SEFA( 5,7, 3),AG(1)),(SEFA(17,3, 4),AH(1))QY1
     > ,(SEFA(29,6, 4),AI(1)),(SEFA( 7,3, 5),AJ(1)),(SEFA(19,6, 5),AK(1)QY1
     > ),(SEFA(31,2, 6),AL(1)),(SEFA( 9,6, 6),AM(1)),(SEFA(21,2, 7),    QY1
     > AN(1)),(SEFA(33,5, 7),AO(1))                                     QY1
      DATA AA/ .9229E 00,.9370E 00,.9483E 00,.9639E 00,.9728E 00,.9798E QY1
     > 00, .9851E 00,.9882E 00,.9919E 00,.9941E 00,.9957E 00,.9982E 00, QY1
     > .9991E 00,.9993E 00,.9997E 00,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.9051E 00,.9283E 00,     QY1
     > .9448E 00,.9665E 00,.9790E 00,.9878E 00,.9929E 00,.9959E 00,     QY1
     > .9978E 00,.9988E 00,.9991E 00,.9997E 00,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.8943E 00,.9259E 00,.9476E 00,.9738E 00,     QY1
     > .9874E 00,.9943E 00,.9976E 00,.9990E 00,.9990E 00,.9996E 00,     QY1
     > .9999E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .8839E 00,.9234E 00,.9494E 00,.9791E 00,.9922E 00,.9974E 00,     QY1
     > .9992E 00,.9994E 00,.9999E 00,.1000E 01,.1000E 01,.1000E 01/     QY1
      DATA AB/ .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E QY1
     > 01, .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01, QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.8958E 00,.9496E 00,     QY1
     > .9775E 00,.9966E 00,.9988E 00,.9999E 00,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.9598E 00,.9944E 00,.9994E 00,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .9994E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01/     QY1
      DATA AC/ .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E QY1
     > 01, .1000E 01,.1000E 01,.1000E 01,.1000E 01,.9004E 00,.9151E 00, QY1
     > .9256E 00,.9408E 00,.9510E 00,.9590E 00,.9655E 00,.9708E 00,     QY1
     > .9752E 00,.9789E 00,.9820E 00,.9875E 00,.9921E 00,.9948E 00,     QY1
     > .9967E 00,.9987E 00,.9989E 00,.9996E 00,.9999E 00,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
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> .1000E 01,.1000E 01,.8687E 00,.8921E 00,.9090E 00,.9326E 00,     QY1
> .9491E 00,.9611E 00,.9701E 00,.9772E 00,.9826E 00,.9868E 00,     QY1
> .9900E 00,.9953E 00,.9979E 00,.9991E 00,.9990E 00,.9998E 00,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .8445E 00,.8766E 00,.8997E 00,.9319E 00,.9535E 00,.9683E 00,     QY1
> .9786E 00,.9858E 00,.9907E 00,.9940E 00,.9963E 00,.9989E 00,     QY1
> .9992E 00,.9998E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.8222E 00,.8620E 00/     QY1
  DATA AD/ .8919E 00,.9340E 00,.9603E 00,.9772E 00,.9875E 00,.9934E QY1
> 00, .9965E 00,.9983E 00,.9992E 00,.9997E 00,.1000E 01,.1000E 01, QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.8008E 00,.8664E 00,.9116E 00,.9637E 00,     QY1
> .9867E 00,.9957E 00,.9987E 00,.9990E 00,.9997E 00,.9999E 00,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .8356E 00,.9325E 00,.9758E 00,.9980E 00,.9996E 00,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.9672E 00,.9983E 00,     QY1
> .9998E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01/     QY1
  DATA AE/ .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E QY1
> 01, .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01, QY1
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
> .1000E 01,.1000E 01,.8850E 00,.8995E 00,.9098E 00,.9246E 00,     QY1
> .9352E 00,.9436E 00,.9501E 00,.9556E 00,.9617E 00,.9647E 00,     QY1
> .9683E 00,.9757E 00,.9813E 00,.9856E 00,.9882E 00,.9936E 00,     QY1
> .9964E 00,.9980E 00,.9990E 00,.9993E 00,.9998E 00,.1000E 01,     QY1
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> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY1
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     > .1000E 01,.1000E 01,.1000E 01,.1000E 01/
      DO 30 I=1,34
         DO 20 K=1,7
            DO 10 L=1,7
10             REFA(I,K,L)=SEFA(I,K,L)
20          CONTINUE
30       CONTINUE
      RETURN
      END
```

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      SUBROUTINE QY2                                                    QY2
      COMMON /QCOM/ REFA(34,7,20)                                       QY2
      DIMENSION SEFA(34,7,20)                                           QY2
      DIMENSION BQ(98),BC(114),BD(114),BE(114),BF(114),BG(114),BH(114), QY2
     > BI(114),BJ(114),BK(114),BL(114),BM(114),BN(114),BO(114),BP(86)   QY2
      EQUIVALENCE (SEFA( 1,1,14),BQ(1)),(SEFA(31,3,14),BC(1)),(SEFA( 9, QY2
     > 7,14),BD(1)),(SEFA(21,3,15),BE(1)),(SEFA(33,6,15),BF(1)),        QY2
     > (SEFA(11,3,16),BG(1)),(SEFA(23,6,16),BH(1)),(SEFA( 1,3,17),BI(1))QY2
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     > ),(SEFA(15,2,19),BM(1)),(SEFA(27,5,19),BN(1)),(SEFA( 5,2,20),    QY2
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> .6017E 00,.6078E 00,.6132E 00,.6224E 00,.6300E 00,.6365E 00,
> .6422E 00,.6472E 00,.6518E 00,.6598E 00,.6666E 00,.6725E 00,
> .6778E 00,.6826E 00,.6909E 00,.6946E 00,.7013E 00,.7148E 00,
> .1665E 00,.1730E 00,.1778E 00,.1850E 00,.1890E 00,.1947E 00,
> .1983E 00,.2015E 00,.2030E 00,.2068E 00,.2092E 00,.2140E 00,
> .2182E 00,.2219E 00,.2251E 00,.2300E 00,.2355E 00,.2397E 00,
> .2434E 00,.2500E 00,.2556E 00,.2607E 00,.2653E 00,.2696E 00,
> .2784E 00,.2811E 00,.2879E 00,.2942E 00,.3003E 00,.3058E 00,
> .3168E 00,.3216E 00,.3315E 00,.3541E 00,.4445E-02,.4679E-02,
> .4866E-02,.5170E-02,.5418E-02,.5633E-02,.5824E-02,.5999E-02,
> .6162E-02,.6314E-02,.6458E-02,.6792E-02,.7078E-02,.7388E-02,
> .7663E-02,.8189E-02,.8693E-02,.9191E-02,.9700E-02,.1077E-01,
> .1186E-01,.1301E-01,.1427E-01,.1562E-01,.1708E-01,.2036E-01,
> .2409E-01,.2837E-01,.3324E-01,.3873E-01,.5173E-01,.5932E-01,
> .7684E-01,.1353E 00,.3120E-07,.3430E-07,.3686E-07,.4112E-07,
> .4477E-07,.4811E-07,.5126E-07,.5433E-07,.5752E-07,.6046E-07,
> .6362E-07,.7194E-07,.8128E-07,.9203E-07,.1046E-06,.1374E-06/
  DATA BP/ .1849E-06,.2553E-06,.3616E-06,.7781E-06,.1815E-05,.4514E-
> 05, .1165E-04,.3083E-04,.8184E-04,.5435E-03,.3051E-02,.1348E-01,
> .4544E-01,.1173E 00,.3945E 00,.5580E 00,.8127E 00,.9910E 00,
> .1555E-14,.1933E-14,.2286E-14,.2977E-14,.3706E-14,.4522E-14,
> .5473E-14,.6609E-14,.7995E-14,.9711E-14,.1186E-13,.2018E-13,
> .3607E-13,.6798E-13,.1349E-12,.6143E-12,.3299E-11,.2013E-10,
> .1339E-09,.6559E-08,.2887E-06,.9102E-05,.1779E-03,.2027E-02,
> .1354E-01,.1542E 00,.4907E 00,.7884E 00,.9324E 00,.9820E 00,
> .9988E 00,.9998E 00,.1000E 01,.1000E 01,.2217E-33,.2222E-33,
> .2231E-33,.2266E-33,.2369E-33,.2738E-33,.4361E-33,.1266E-32,
> .6106E-32,.3799E-31,.2696E-30,.5640E-28,.1856E-25,.7880E-23,
> .3573E-20,.4526E-15,.1309E-10,.4985E-07,.2293E-04,.2535E-01,
> .3578E 00,.7910E 00,.9570E 00,.9932E 00,.9988E 00,.1000E 01,
```

```
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
     > .1000E 01,.1000E 01/
      DO 30 I=1,34
         DO 20 K=1,7
            DO 10 L=14,20
10             REFA(I,K,L)=SEFA(I,K,L)
20          CONTINUE
30       CONTINUE
      RETURN
      END
```

```
      SUBROUTINE QY3                                                     QY3
      COMMON /QCOM/ REFA(34,7,20)                                        QY3
      DIMENSION SEFA(34,7,20)                                            QY3
      DIMENSION CA(44),AP(114),AQ(114),AR(114),AS(114),AT(114),AU(114),  QY3
     > AV(114),AW(114),AX(114),AY(114),AZ(114),BA(114),BB(16)            QY3
      EQUIVALENCE (SEFA( 1,1, 8),CA(1)), (SEFA(11,2, 8),AP(1)),(SEFA(23,QY3
     > 5, 8),AQ(1)),(SEFA( 1,2, 9),AR(1)),(SEFA(13,5, 9),AS(1)),         QY3
     > (SEFA(25,1,10),AT(1)),(SEFA( 3,5,10),AU(1)),(SEFA(15,1,11),AV(1))QY3
     > ,(SEFA(27,4,11),AW(1)),(SEFA( 5,1,12),AX(1)),(SEFA(17,4,12),AY(1)QY3
     > ),(SEFA(29,7,12),AZ(1)),(SEFA( 7,4,13),BA(1)),(SEFA(19,7,13),     QY3
     > BB(1))                                                            QY3
      DATA CA/ .8298E 00,.8434E 00, .8531E 00,.8672E 00,.8771E 00,       QY3
     > .8850E 00,.8916E 00,.8970E 00, .9018E 00,.9060E 00,.9098E 00,     QY3
     > .9180E 00,.9246E 00,.9303E 00, .9352E 00,.9436E 00,.9501E 00,     QY3
     > .9556E 00,.9617E 00,.9683E 00, .9744E 00,.9792E 00,.9831E 00,     QY3
     > .9863E 00,.9882E 00,.9928E 00, .9954E 00,.9972E 00,.9983E 00,     QY3
     > .9990E 00,.9991E 00,.9994E 00, .9998E 00,.1000E 01,.7585E 00,     QY3
     > .7792E 00,.7943E 00,.8160E 00, .8318E 00,.8442E 00,.8545E 00,     QY3
     > .8632E 00,.8709E 00,.8777E 00/                                    QY3
      DATA AP/ .8838E 00,.8952E 00,.9075E 00,.9166E 00,.9243E 00,.9391E QY3
     > 00, .9477E 00,.9561E 00,.9631E 00,.9739E 00,.9816E 00,.9871E 00, QY3
     > .9911E 00,.9940E 00,.9959E 00,.9982E 00,.9993E 00,.9992E 00,      QY3
     > .9997E 00,.9999E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .6871E 00,.7139E 00,.7338E 00,.7634E 00,.7853E 00,.8030E 00,      QY3
     > .8178E 00,.8306E 00,.8418E 00,.8518E 00,.8616E 00,.8804E 00,      QY3
     > .8963E 00,.9120E 00,.9213E 00,.9401E 00,.9542E 00,.9652E 00,      QY3
     > .9737E 00,.9853E 00,.9922E 00,.9959E 00,.9979E 00,.9990E 00,      QY3
     > .9987E 00,.9997E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.5895E 00,.6204E 00,      QY3
     > .6450E 00,.6846E 00,.7163E 00,.7432E 00,.7667E 00,.7875E 00,      QY3
     > .8063E 00,.8232E 00,.8386E 00,.8717E 00,.8986E 00,.9202E 00,      QY3
     > .9373E 00,.9631E 00,.9790E 00,.9886E 00,.9940E 00,.9985E 00,      QY3
     > .9991E 00,.9998E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.4799E 00,.5268E 00,.5647E 00,.6257E 00,      QY3
     > .6746E 00,.7160E 00,.7515E 00,.7825E 00,.8098E 00,.8339E 00,      QY3
     > .8553E 00,.8987E 00,.9304E 00,.9532E 00,.9692E 00,.9876E 00,      QY3
     > .9955E 00,.9983E 00,.9992E 00,.9999E 00,.1000E 01,.1000E 01/      QY3
      DATA AQ/ .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E QY3
     > 01, .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01, QY3
     > .3226E 00,.3959E 00,.4595E 00,.5680E 00,.6573E 00,.7318E 00,      QY3
     > .7931E 00,.8424E 00,.8820E 00,.9129E 00,.9370E 00,.9737E 00,      QY3
     > .9899E 00,.9965E 00,.9987E 00,.9996E 00,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1865E 00,.3136E 00,      QY3
     > .4461E 00,.6825E 00,.8441E 00,.9331E 00,.9746E 00,.9914E 00,      QY3
     > .9973E 00,.9991E 00,.9991E 00,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,      QY3
     > .1000E 01,.1000E 01,.8211E 00,.8317E 00,.8443E 00,.8551E 00,      QY3
     > .8680E 00,.8758E 00,.8792E 00,.8876E 00,.8924E 00,.8966E 00,      QY3
     > .9004E 00,.9060E 00,.9151E 00,.9207E 00,.9256E 00,.9337E 00,      QY3
     > .9408E 00,.9461E 00,.9510E 00,.9590E 00,.9655E 00,.9708E 00,      QY3
     > .9752E 00,.9789E 00,.9820E 00,.9868E 00,.9906E 00,.9933E 00,      QY3
```

```
      SUBROUTINE CHIQ
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD, ACON(36,20,
     > 20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11), ORMODI(36,12,8)
     > , VD(36),VDCOEF(20,20),NOL,NOU,NRL,NRU
      REAL*8 NAMNUC,WORD
      COMMON /PCOM/ REL(6,36),IDIST(20),NUMST
      COMMON /TCOM/ KIQ(36,20,20)
      DIMENSION REGL(35)
      REAL KIQ
      DO 30 I=1,NNUCS
         DO 20 NO=1,16
            DO 10 NR=1,20
   10          KIQ(I,NO,NR)=0
   20       CONTINUE
   30    CONTINUE
      DO 50 I=1,NNUCS
         REGL(I)=0
         DO 40 J=1,NUMST
   40       REGL(I)=REGL(I)+REL(J,I)
   50    CONTINUE
      DO 90 I=1,NNUCS
         DO 80 NO=NOL,NOU
            DO 60 NR=NRL,NRU
               IF (REGL(I).EQ.0) GO TO 70
   60          KIQ(I,NO,NR)=(ACON(I,NO,NR)/REGL(I))*1.E6
            GO TO 80
   70       KIQ(I,NO,NR)=0.
   80       CONTINUE
   90    CONTINUE
      DO 130 I=1,NNUCS
         WRITE(51,9000)NAMNUC(I)
         WRITE(51,9001)
         WRITE(51,9002)
         WRITE(51,9003)
         WRITE(51,9001)
         WRITE(51,9004)
         WRITE(51,9005)
         NO=1
         DO 100 NR=NRL,NRU
  100       WRITE(51,9007)IDIST(NR),KIQ(I,NO,NR),KIQ(I,NO+1,NR),KIQ(I,
     >       NO+2,NR),KIQ(I,NO+3,NR),KIQ(I,NO+4,NR),KIQ(I,NO+5,NR),
     >       KIQ(I,NO+6,NR), KIQ(I,NO+7,NR)
         ISP= (22-2*(NRU/2))/2
         DO 110 IG=1,ISP
  110       WRITE(51,9001)
         WRITE(51,9006)
         WRITE(51,9005)
         NO=9
         DO 120 NR=NRL,NRU
  120       WRITE(51,9007)IDIST(NR),KIQ(I,NO,NR),KIQ(I,NO+1,NR),KIQ(I,
     >       NO+2,NR),KIQ(I,NO+3,NR),KIQ(I,NO+4,NR),KIQ(I,NO+5,NR),
     >       KIQ(I,NO+6,NR), KIQ(I,NO+7,NR)
  130    CONTINUE
      RETURN
 9000 FORMAT('1',T25,'GROUND-LEVEL CHI/Q VALUES FOR ',A8,
     > 'AT VARIOUS DISTANCES IN EACH COMPASS DIRECTION')
```

```
 DATA AU/ .4898E 00,.5434E 00,.5870E 00,.6243E 00,.6570E 00,.6864E QY3
> 00, .7092E 00,.7373E 00,.7594E 00,.8073E 00,.8465E 00,.8788E 00, QY3
> .9048E 00,.9431E 00,.9673E 00,.9820E 00,.9905E 00,.9977E 00,     QY3
> .9992E 00,.9997E 00,.9999E 00,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.2448E 00,.3011E 00,.3507E 00,.4374E 00,     QY3
> .5127E 00,.5794E 00,.6387E 00,.6915E 00,.7383E 00,.7795E 00,     QY3
> .8147E 00,.8848E 00,.9315E 00,.9610E 00,.9788E 00,.9944E 00,     QY3
> .9985E 00,.9990E 00,.9998E 00,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .9490E-01,.1655E 00,.2472E 00,.4257E 00,.5953E 00,.7377E 00,     QY3
> .8409E 00,.9094E 00,.9514E 00,.9753E 00,.9881E 00,.9984E 00,     QY3
> .9993E 00,.9999E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.8071E 00,.8204E 00,     QY3
> .8298E 00,.8435E 00,.8531E 00,.8607E 00,.8672E 00,.8725E 00,     QY3
> .8771E 00,.8781E 00,.8850E 00,.8930E 00,.8995E 00,.9050E 00/     QY3
 DATA AV/ .9098E 00,.9180E 00,.9246E 00,.9303E 00,.9352E 00,.9436E QY3
> 00, .9501E 00,.9556E 00,.9617E 00,.9647E 00,.9683E 00,.9744E 00, QY3
> .9792E 00,.9831E 00,.9863E 00,.9882E 00,.9928E 00,.9943E 00,     QY3
> .9964E 00,.9990E 00,.7242E 00,.7441E 00,.7584E 00,.7792E 00,     QY3
> .7943E 00,.8062E 00,.8160E 00,.8244E 00,.8318E 00,.8383E 00,     QY3
> .8442E 00,.8568E 00,.8673E 00,.8761E 00,.8838E 00,.8952E 00,     QY3
> .9075E 00,.9166E 00,.9243E 00,.9391E 00,.9477E 00,.9561E 00,     QY3
> .9631E 00,.9689E 00,.9739E 00,.9816E 00,.9871E 00,.9911E 00,     QY3
> .9940E 00,.9959E 00,.9982E 00,.9989E 00,.9988E 00,.9999E 00,     QY3
> .6376E 00,.6624E 00,.6809E 00,.7084E 00,.7236E 00,.7453E 00,     QY3
> .7592E 00,.7712E 00,.7770E 00,.7913E 00,.8003E 00,.8186E 00,     QY3
> .8343E 00,.8477E 00,.8597E 00,.8770E 00,.8960E 00,.9098E 00,     QY3
> .9216E 00,.9408E 00,.9552E 00,.9662E 00,.9748E 00,.9813E 00,     QY3
> .9862E 00,.9930E 00,.9964E 00,.9982E 00,.9992E 00,.9990E 00,     QY3
> .9998E 00,.9999E 00,.1000E 01,.1000E 01,.5086E 00,.5353E 00,     QY3
> .5567E 00,.5911E 00,.6190E 00,.6429E 00,.6639E 00,.6829E 00,     QY3
> .7002E 00,.7162E 00,.7310E 00,.7641E 00,.7904E 00,.8178E 00,     QY3
> .8398E 00,.8768E 00,.9062E 00,.9288E 00,.9471E 00,.9718E 00,     QY3
> .9858E 00,.9932E 00,.9970E 00,.9986E 00,.9991E 00,.9997E 00/     QY3
 DATA AW/ .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E QY3
> 01, .1000E 01,.1000E 01,.3873E 00,.4252E 00,.4561E 00,.5062E 00, QY3
> .5471E 00,.5823E 00,.6133E 00,.6412E 00,.6683E 00,.6901E 00,     QY3
> .7120E 00,.7596E 00,.7997E 00,.8338E 00,.8630E 00,.9079E 00,     QY3
> .9398E 00,.9618E 00,.9764E 00,.9918E 00,.9975E 00,.9992E 00,     QY3
> .9993E 00,.9998E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .2134E 00,.2627E 00,.3062E 00,.3830E 00,.4505E 00,.5112E 00,     QY3
> .5664E 00,.6167E 00,.6625E 00,.7040E 00,.7417E 00,.8196E 00,     QY3
> .8777E 00,.9196E 00,.9487E 00,.9810E 00,.9936E 00,.9981E 00,     QY3
> .9994E 00,.9999E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.6700E-01,.1182E 00,     QY3
> .1791E 00,.3204E 00,.4701E 00,.6098E 00,.7277E 00,.8190E 00,     QY3
> .8851E 00,.9300E 00,.9590E 00,.9908E 00,.9983E 00,.9989E 00,     QY3
> .9998E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,     QY3
> .1000E 01,.1000E 01,.7941E 00,.8071E 00,.8164E 00,.8298E 00/     QY3
 DATA AX/ .8394E 00,.8469E 00,.8531E 00,.8556E 00,.8630E 00,.8672E QY3
```

```
> 00, .8707E 00,.8786E 00,.8850E 00,.8906E 00,.8952E 00,.9032E 00,
> .9098E 00,.9157E 00,.9203E 00,.9285E 00,.9352E 00,.9412E 00,
> .9458E 00,.9501E 00,.9529E 00,.9617E 00,.9659E 00,.9705E 00,
> .9744E 00,.9777E 00,.9831E 00,.9854E 00,.9882E 00,.9947E 00,
> .7050E 00,.7242E 00,.7382E 00,.7584E 00,.7731E 00,.7847E 00,
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> .9911E 00,.9931E 00,.9959E 00,.9990E 00,.6087E 00,.6323E 00,
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> .7419E 00,.7556E 00,.7642E 00,.7819E 00,.7970E 00,.8101E 00,
> .8217E 00,.8389E 00,.8578E 00,.8719E 00,.8846E 00,.9053E 00,
> .9217E 00,.9350E 00,.9463E 00,.9556E 00,.9635E 00,.9757E 00,
> .9839E 00,.9897E 00,.9935E 00,.9954E 00,.9985E 00,.9992E 00,
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> .6643E 00,.6956E 00,.7209E 00,.7476E 00,.7698E 00,.8086E 00/
  DATA AY/ .8417E 00,.8686E 00,.8920E 00,.9283E 00,.9536E 00,.9709E
> 00, .9823E 00,.9894E 00,.9937E 00,.9981E 00,.9995E 00,.9999E 00,
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
> .3359E 00,.3688E 00,.3957E 00,.4394E 00,.4751E 00,.5061E 00,
> .5336E 00,.5586E 00,.5829E 00,.6029E 00,.6229E 00,.6678E 00,
> .7071E 00,.7418E 00,.7731E 00,.8259E 00,.8678E 00,.9011E 00,
> .9272E 00,.9633E 00,.9828E 00,.9919E 00,.9962E 00,.9986E 00,
> .9995E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1628E 00,.2005E 00,
> .2340E 00,.2936E 00,.3469E 00,.3958E 00,.4414E 00,.4842E 00,
> .5245E 00,.5625E 00,.5984E 00,.6790E 00,.7479E 00,.8050E 00,
> .8525E 00,.9203E 00,.9601E 00,.9816E 00,.9921E 00,.9985E 00,
> .9998E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
> .1000E 01,.1000E 01,.3335E-01,.5966E-01,.9211E-01,.1735E 00,
> .2716E 00,.3792E 00,.4885E 00,.5918E 00,.6846E 00,.7639E 00,
> .8284E 00,.9314E 00,.9764E 00,.9921E 00,.9975E 00,.9999E 00,
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
> .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01/
  DATA AZ/ .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E
> 01, .7850E 00,.7979E 00,.8071E 00,.8204E 00,.8298E 00,.8372E 00,
> .8435E 00,.8486E 00,.8531E 00,.8540E 00,.8607E 00,.8685E 00,
> .8749E 00,.8803E 00,.8850E 00,.8930E 00,.8995E 00,.9050E 00,
> .9098E 00,.9180E 00,.9246E 00,.9303E 00,.9352E 00,.9399E 00,
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> .7242E 00,.7440E 00,.7584E 00,.7698E 00,.7792E 00,.7872E 00,
> .7943E 00,.8005E 00,.8062E 00,.8182E 00,.8283E 00,.8367E 00,
> .8442E 00,.8568E 00,.8673E 00,.8761E 00,.8838E 00,.8952E 00,
> .9075E 00,.9166E 00,.9243E 00,.9312E 00,.9391E 00,.9477E 00,
> .9561E 00,.9631E 00,.9689E 00,.9739E 00,.9816E 00,.9846E 00,
> .9893E 00,.9959E 00,.5876E 00,.6105E 00,.6276E 00,.6529E 00,
> .6669E 00,.6870E 00,.6998E 00,.7109E 00,.7163E 00,.7295E 00,
> .7379E 00,.7550E 00,.7697E 00,.7824E 00,.7937E 00,.8106E 00,
> .8292E 00,.8431E 00,.8554E 00,.8764E 00,.8936E 00,.9081E 00,
> .9207E 00,.9322E 00,.9414E 00,.9567E 00,.9679E 00,.9766E 00,
> .9839E 00,.9883E 00,.9947E 00,.9965E 00,.9981E 00,.9998E 00,
> .4262E 00,.4485E 00,.4665E 00,.4955E 00,.5190E 00,.5392E 00/
  DATA BA/ .5572E 00,.5734E 00,.5884E 00,.6022E 00,.6152E 00,.6447E
> 00, .6689E 00,.6945E 00,.7160E 00,.7543E 00,.7876E 00,.8162E 00,
```

```
     > .8421E 00,.8851E 00,.9171E 00,.9425E 00,.9609E 00,.9739E 00,
     > .9829E 00,.9933E 00,.9976E 00,.9989E 00,.9997E 00,.9999E 00,
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.2994E 00,.3288E 00,
     > .3527E 00,.3918E 00,.4238E 00,.4516E 00,.4764E 00,.4990E 00,
     > .5211E 00,.5394E 00,.5578E 00,.5996E 00,.6368E 00,.6706E 00,
     > .7015E 00,.7556E 00,.8020E 00,.8416E 00,.8746E 00,.9251E 00,
     > .9579E 00,.9776E 00,.9884E 00,.9947E 00,.9975E 00,.9994E 00,
     > .9999E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
     > .1000E 01,.1000E 01,.1309E 00,.1612E 00,.1883E 00,.2366E 00,
     > .2801E 00,.3206E 00,.3588E 00,.3952E 00,.4300E 00,.4635E 00,
     > .4958E 00,.5713E 00,.6400E 00,.7018E 00,.7565E 00,.8450E 00,
     > .9075E 00,.9481E 00,.9725E 00,.9934E 00,.9981E 00,.9996E 00,
     > .9999E 00,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
     > .1903E-01,.3428E-01,.5345E-01,.1034E 00,.1678E 00,.2443E 00,
     > .3296E 00,.4194E 00,.5092E 00,.5953E 00,.6741E 00,.8284E 00,
     > .9204E 00,.9661E 00,.9875E 00,.9984E 00,.9998E 00,.1000E 01/
      DATA BB/ .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E
     > 01, .1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,.1000E 01,
     > .1000E 01,.1000E 01,.1000E 01,.1000E 01/
      DO 30 I=1,34
         DO 20 K=1,7
            DO 10 L=8,13
10             REFA(I,K,L)=SEFA(I,K,L)
20          CONTINUE
30       CONTINUE
      RETURN
      END
```

```
      SUBROUTINE QX(BND,X,U,UD,HS,VD,VG,INDEX1,QXR)
C
C-----NUMERICAL INTEGRATION BY SIMPSON'S RULE
C-----ROUTINE CHANGED BY D.P.STEWART 7/76
C
      FUNC(D,F,HH,X)=F*EXP(-(HH**2*F**2)/(2.*X**(2*D)))/X**D
      REAL AB(7,4,2)
      INTEGER AC(5,4)
C               1          2          3        4          5          6          7
      DATA AB/ 1.0000, 1.0000, .9540, .8061, .8600, .8823, .8257,
     > 99.9999,99.9999, .8330, .6715, .6290, .6321, .6547, 99.9999,
     > 99.9999, .5524, .5099, .4054, .3710, .3818, 99.9999,99.9999,
     > 99.9999, .5251, .1110, .1106, .1106, 5.0200, 8.3500,10.0150,
     > 7.4800,15.5000,34.7000,61.2500, 99.9999,99.9999, 4.4000, 2.9500,
     > 3.1500, 6.1320,18.8000, 99.9999,99.9999, .3320, .8100, .5240,
     > .7640, 2.1150, 99.9999,99.9999,99.9999, .9300, .0349, .0694,
     > .1739/
C                  1       2       3       4       5
      DATA AC/ 0, 0,99999, 1000, 1000, 1000, 1000, 0,10000, 3000, 10000,
     >  3000, 0,99999,10000, 0,10000, 0, 0,99999/
      IF (INDEX1-3) 10,20,30
C-----SET UP BOUNDS OF INTEGRATION
C-----INDEX3 GIVES COLUMN OF AC CONTAINING LOWER BOUNDS
C-----INDEX4 GIVES COLUMN WITH UPPER BOUND
C-----LIM1 AND LIM2 DETERMINE  THE ROWS OF AC USED
C-----THEY ALSO DETERMINE WHICH VALUES OF D AND F SHOULD BE USED
   10 INDEX3=1
      INDEX4=3
      LIM2=1
      LIM1=1
      GO TO 40
   20 INDEX3=1
      INDEX4=4
      LIM2=3
      LIM1=1
      IF (BND.GE.1000.) LIM1=2
      IF (BND.GE.10000) LIM1=3
      GO TO 40
   30 INDEX3=2
      INDEX4=5
      LIM2=4
      LIM1=1
      IF (BND.GE.1000) LIM1=2
      IF (BND.GE.3000) LIM1=3
      IF (BND.GE.10000) LIM1=4
   40 QXR=0
      STOR1=AC(INDEX3,LIM1)
      AC(INDEX3,LIM1)=BND
      AC(INDEX4,LIM2)=X
      EPS=.1
C-----THIS LOOP SPLITS THE INTEGRATION ACCORDING TO CHANGES IN D AND F
      DO 90 INDEX2=LIM1,LIM2
         D=AB(INDEX1,INDEX2,1)
         F=AB(INDEX1,INDEX2,2)
         B=AC(INDEX4,INDEX2)
         IF (X.LT.B) B=X
```

```
      A=AC(INDEX3,INDEX2)
      WIDTH=(B-A)/2.
      JLIM=1
C-----FOFA AND FOFB ARE THE FUNCTION VALUES AT ENDPOINTS OF INTERVAL
      FOFA=0.0
      IF (A.EQ.0.0) GO TO 50
      HA=HS-VG*A/UD
      IF (HA.LT.1.0) HA=1.0
      FOFA=FUNC(D,F,HA,A)
   50 HB=HS-VG*B/UD
      IF (HB.LT.1.0) HB=1.0
      FOFB=FUNC(D,F,HB,B)
      X1=A+WIDTH
      H1=HS-VG*X1/UD
      IF (H1.LT.1.0) H1=1.0
C-----COMPUTE FIRST APPROXIMATION OF SIMP
      SIMP=(FOFA+4*FUNC(D,F,H1,X1)+FOFB)*WIDTH/3.
C-----THIS SECTION IS REPEATED UNTIL THE CHANGE IN SIMP IS LESS THAN EPS
   60 FUNC1=0.0
      FUNC2=0.0
      WIDTH=WIDTH/2
      JLIM=JLIM*2
      OLDS=SIMP
      JLESS=JLIM-1
      DO 70 J=1,JLESS
         X1=A+(2*J-1.)*WIDTH
         H1=HS-VG*X1/UD
         IF (H1.LT.1.0) H1=1.0
         FUNC1=FUNC1+FUNC(D,F,H1,X1)
         X2=A+2*J*WIDTH
         H2=HS-VG*X2/UD
         IF (H2.LT.1.0) H2=1.0
         FUNC2=FUNC2+FUNC(D,F,H2,X2)
   70    CONTINUE
      X1=A+2*JLIM*WIDTH
      H1=HS-VG*X1/UD
      IF (H1.LT.1.0) H1=1.0
      FUNC1=FUNC1+FUNC(D,F,H1,X1)
      SIMP=(FOFA+4*FUNC1+2*FUNC2+FOFB)*WIDTH/3
      IF (ABS(SIMP-OLDS).GT.EPS) GO TO 60
C-----END SIMP APPROXIMATION LOOP
   80 QXR=QXR+SIMP
      IF (X.LT.AC(INDEX4,INDEX2)) GO TO 100
   90 CONTINUE
  100 QXR=EXP(-.79788*QXR*VD/UD)
      AC(INDEX3,LIM1)=STOR1
      RETURN
      END
```

```
      SUBROUTINE CHIQ
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD, ACON(36,20,
     > 20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11), ORMODI(36,12,8)
     > , VD(36),VDCOEF(20,20),NOL,NOU,NRL,NRU
      REAL*8 NAMNUC,WORD
      COMMON /PCOM/ REL(6,36),IDIST(20),NUMST
      COMMON /TCOM/ KIQ(36,20,20)
      DIMENSION REGL(35)
      REAL KIQ
      DO 30 I=1,NNUCS
         DO 20 NO=1,16
            DO 10 NR=1,20
   10          KIQ(I,NO,NR)=0
   20       CONTINUE
   30    CONTINUE
      DO 50 I=1,NNUCS
         REGL(I)=0
         DO 40 J=1,NUMST
   40       REGL(I)=REGL(I)+REL(J,I)
   50    CONTINUE
      DO 90 I=1,NNUCS
         DO 80 NO=NOL,NOU
            DO 60 NR=NRL,NRU
               IF (REGL(I).EQ.0) GO TO 70
   60          KIQ(I,NO,NR)=(ACON(I,NO,NR)/REGL(I))*1.E6
            GO TO 80
   70       KIQ(I,NO,NR)=0.
   80       CONTINUE
   90    CONTINUE
      DO 130 I=1,NNUCS
         WRITE(51,9000) NAMNUC(I)
         WRITE(51,9001)
         WRITE(51,9002)
         WRITE(51,9003)
         WRITE(51,9001)
         WRITE(51,9004)
         WRITE(51,9005)
         NO=1
         DO 100 NR=NRL,NRU
  100       WRITE(51,9007)IDIST(NR),KIQ(I,NO,NR),KIQ(I,NO+1,NR),KIQ(I,
     >       NO+2,NR),KIQ(I,NO+3,NR),KIQ(I,NO+4,NR),KIQ(I,NO+5,NR),
     >       KIQ(I,NO+6,NR), KIQ(I,NO+7,NR)
         ISP=(22-2*(NRU/2))/2
         DO 110 IG=1,ISP
  110       WRITE(51,9001)
         WRITE(51,9006)
         WRITE(51,9005)
         NO=9
         DO 120 NR=NRL,NRU
  120       WRITE(51,9007)IDIST(NR),KIQ(I,NO,NR),KIQ(I,NO+1,NR),KIQ(I,
     >       NO+2,NR),KIQ(I,NO+3,NR),KIQ(I,NO+4,NR),KIQ(I,NO+5,NR),
     >       KIQ(I,NO+5,NR), KIQ(I,NO+7,NR)
  130    CONTINUE
      RETURN
 9000 FORMAT('1',T25,'GROUND-LEVEL CHI/Q VALUES FOR ',A8,
     > 'AT VARIOUS DISTANCES IN EACH COMPASS DIRECTION')
```

```
9001 FORMAT('0')                                                      CHIQ 280
9002 FORMAT(' ',T20,'DISTANCE',T52,'CHI/Q TOWARD INDICATED DIRECTION') CHIQ 285
9003 FORMAT(' ',T20,'(METERS)',T60,'(SEC/CUBIC METER)')               CHIQ 290
9004 FORMAT(' ',T32,'N',T43,'NNW',T54,'NW',T65,'WNW',T76,'W',T87,'WSW',CHIQ 295
    > T98,'SW',T109,'SSW')                                            CHIQ 300
9005 FORMAT(' ')                                                      CHIQ 305
9006 FORMAT(' ',T32,'S',T43,'SSE',T54,'SE',T65,'ESE',T76,'E',T87,'ENE',CHIQ 310
    > T98,'NE',T109,'NNE')                                            CHIQ 315
9007 FORMAT(' ',T19,I7,T30,E9.3,T41,E9.3,T52,E9.3,T63,E9.3,T74,E9.3,   CHIQ 320
    > T85,E9.3,T96,E9.3,T107,E9.3)                                    CHIQ 325
     END                                                              CHIQ 330
```

```
      SUBROUTINE DIRECT(LORT)
C        READS AIR CONCENTRATIONS AND GROUND DEPOSITION RATES FOR
C        RADIONUCLIDES DIRECTLY FOR TRANSMISSION TO THE DOSEN
C        SUBROUTINE.
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD, ACON(36,20,
     > 20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11), ORMODI(36,12,8)
     > , VD(36),VDCOEF(20,20),NOL,NOU,NRL,NRU
      COMMON /PCOM/ REL(6,36),IDIST(20),NUMST
      COMMON /FCOM/ FEQWL,INTPA(20,20)
      DIMENSION SC(36)
      REAL*8 NAMNUC,WORD
      READ(50,9000)NOL,NOU,NRL,NRU
      READ(50,9001)SQSD
      READ(50,9000)IDIST
      READ(50,9002)SEQWL
      READ(50,9000)NNUCS
      DO 10 I=1,NNUCS
         READ(50,9003)NAMNUC(I),VD(I),SC(I)
         READ(50,9004)((ACON(I,NO,NR),NR=1,20),NO=1,20)
         READ(50,9004)((GCON(I,NO,NR),NR=1,20),NO=1,20)
   10    CONTINUE
      FEQWL=SEQWL
      WRITE(51,9005)
      WRITE(51,9006)
      WRITE(51,9007)
      IF (LORT.EQ.0) GO TO 20
      WRITE(51,9008)
      WRITE(51,9009)
      WRITE(51,9019)
      GO TO 30
   20 WRITE(51,9010)
      WRITE(51,9019)
   30 CONTINUE
      IF (LORT.EQ.1) GO TO 70
      DO 60 NO=NOL,NOU
         DO 50 NR=NRL,NRU
            DO 40 I=1,NNUCS
               VD1=VD(I)
               DRYCON=ACON(I,NO,NR)*VD1*100
               WETCON=(GCON(I,NO,NR)-DRYCON)*(SC(I)/(SC(I)+1.E-30))
   40          WRITE(51,9018) NO,NR,NAMNUC(I),ACON(I,NO,NR),DRYCON,
     >          WETCON, GCON(I,NO,NR)
   50       CONTINUE
   60    CONTINUE
      GO TO 110
   70 CONTINUE
      DO 100 NO=NOL,NOU
         DO 90 NR=NRL,NRU
            DO 80 I=1,NNUCS
               VD1=VD(I)
               DRYCON=ACON(I,NO,NR)*VD1*100
               WETCON=(GCON(I,NO,NR)-DRYCON)*(SC(I)/(SC(I)+1.E-30))
   80          WRITE(51,9018) NO,IDIST(NR),NAMNUC(I),ACON(I,NO,NR),
     >          DRYCON,WETCON, GCON(I,NO,NR)
   90       CONTINUE
  100    CONTINUE
```

```
  110 CONTINUE
  120 CONTINUE
      IF (LORT.EQ.1) GO TO 130
      ASQSD=((SQSD**2)*400.)/1.E6
      WRITE(51,9011)
      WRITE(51,9012)ASQSD
      WRITE(51,9013)
      WRITE(51,9014)SQSD
      WRITE(51,9015)
      WRITE(51,9016)
      WRITE(51,9017)
C-----END OF GRID LOOP------------------------------------------
  130 RETURN
 9000 FORMAT(8I10)
 9001 FORMAT(8F10.0)
 9002 FORMAT(F10.0)
 9003 FORMAT(A8,F12.4,E10.3)
 9004 FORMAT(8E10.3)
 9005 FORMAT('1',T48,'INPUT RADIONUCLIDE CONCENTRATIONS')
 9006 FORMAT('0',T10,'AREA',T30,'NUCLIDE',T42,'AIR CONCENTRATION',T64,
     > 'DRY DEPOSITION RATE',T88,'WET DEPOSITION RATE',T112,
     > 'GROUND DEPOSITION RATE')
 9007 FORMAT(T47,'(PCI/CC)',T64,'(PCI/SQUARE CM-SEC)',T88,
     > '(PCI/SQUARE CM-SEC)',T113,'(PCI/SQUARE CM-SEC)')
 9008 FORMAT(' WIND TOWARD',T17,'DISTANCE')
 9009 FORMAT(' ',T17,'(METERS)')
 9010 FORMAT(' ',T4,'COLUMN',T21,'ROW')
 9011 FORMAT('1',T30,'NOTE-THE AREA SURROUNDING THE PLANT IS A SQUARE
     >WITH AN AREA')
 9012 FORMAT(' ',T35,'OF',F10.1,1X,
     > 'SQUARE KILOMETERS WITH THE PLANT AT THE CENTER.')
 9013 FORMAT(' ',T35,'THE SQUARE AREA IS ALIGNED DUE NORTH-SOUTH AND EAS
     >T-WEST. THE')
 9014 FORMAT(' ',T35,'400 SMALLER SQUARES, WHICH ARE EACH ',F7.1,1X,
     > 'METERS ON A SIDE,')
 9015 FORMAT(' ',T35,'ARE IDENTIFIED BY COLUMN AND ROW. COLUMNS ARE NUMB
     >ERED FROM')
 9016 FORMAT(' ',T35,'1 TO 20 FROM WEST TO EAST. ROWS ARE NUMBERED FROM
     >1 TO 20 FROM')
 9017 FORMAT(' ',T35,'SOUTH TO NORTH.')
 9018 FORMAT(' ',T6,I2,T18,I6,T31,A8,T45,E10.3,T68,E10.3,T92,E10.3,T118,
     >  E10.3)
 9019 FORMAT('0')
      END
```

```
      SUBROUTINE DOSEN
C
C       USNRC REG. GUIDE 1.109 MODELS FOR INGESTION DOSE CALCULATIONS
C       WERE IMPLEMENTED AND INCORPORATED WITHIN DOSEN BY J. C. PLEASANT
C       OF THE MATHEMATICS DEPARTMENT, EAST TENNESSEE STATE UNIVERSITY.
C
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD, ACON(36,20,
     > 20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11), ORMODI(36,12,8)
     > , VD(36),VDCOEF(20,20),NOL,NOU,NRL,NRU
      COMMON /INGDOS/LAMW,TSUBB,P,BSUBV,DR,RATUA
      COMMON NOML(11),NRML(11)
      COMMON /RVAL/ S1,S3,SD1,SD3,ACN,GCN,SW1,SW3
      COMMON /TCOM/ KIQ(36,20,20)
      COMMON /PCOM/ REL(6,36),IDIST(20),NUMST
      COMMON /FCOM/ FEQWL,INTPA(20,20)
C
      DIMENSION VAGAC(36),VAGCON(36),BAGAC(36),BAGCON(36)
      DIMENSION FING(36,20,20),GBUP(36,20,20)
      DIMENSION GI(36,4),PARSIZ(36),CLASS(36)
      DIMENSION GFIN(36,20,20)
      REAL KIQ
      REAL*8 NADRN
      REAL*8 NAMNUC,WORD,NADEC1,NADEC3, NAMES(11),NAMORG(11)
      REAL CFINGA(11),CFINHA(11),DOSING(11),FROG(11),INTPA,
     > LAMH2O,LAMSUR,MSUBB,LAMRR,INTFC(20,20), DCC14(11),DOSIN(11,36),
     > VEGDOS(11),BEFDOS(11),MLKDOS(11), LAMI,LAMW,LEFDOS,MAGAC(36),
     > MAGCON(36)
      INTEGER INTWA(20,20),NOBCT(20,20),NOMCT(20,20),TNOBCT,TNOMCT
      INTEGER CLASS
      DATA NAMES/'TOT.BODY','R MAR   ','LUNGS   ','ENDOST  ','S WALL  ',
     > 'LLI WALL','THYROID ','LIVER   ','KIDNEYS ','TESTES  ',
     > 'OVARIES '/
      DATA NADRN/'RN-222  '/
      DATA NADEC1/'H-3     '/,NADEC3/'C-14    '/
      DATA DCC14/1.16E3,2.03E3,5.07E2,1.85E3,7.43E2,8.92E2,5.27E2,
     > 7.30E2,6.49E2,4.46E2,4.46E2/
C---END OF DECLARATIONS
      DO 10 K=1,36
         DO 10 J=1,11
            DOSIN(J,K)=0.
            DO 10 I=1,8
   10          ORMODI(K,J,I)=0
      DO 40 I=1,36
         DO 30 NO=1,20
            DO 20 NR=1,20
               GBUP(I,NO,NR)=0.
               FING(I,NO,NR)=0.
   20          CONTINUE
   30       CONTINUE
   40    CONTINUE
      READ(50,9061) LIPO
      READ(50,9061) NNTB,NRTB,NSTB,NTTB,NUTB
      READ(50,9062) ((NOBCT(I,J),J=1,20),I=1,20)
      READ(50,9063) ((NOMCT(I,J),J=1,20),I=1,20)
      READ(50,9064) ((INTFC(I,J),J=1,20),I=1,20)
      READ(50,9065) ((INTPA(I,J),J=1,20),I=1,20)
```

```
      READ(50,9066)((INTWA(I,J),J=1,20),I=1,20)
      READ(50,9067)IMPFIX
      READ(50,9068)RVEG,F3VEGM,RBEF,F3BEFM,RMLK,F3MLKM
      READ(50,9069)BRTHRT,DILFAC,USEFAC,T,DD1
C READ PARAMETERS FOR NRC MODEL
      READ(50,9000)TSUBH1,TSUBH2,TSUBH3,TSUBH4
      READ(50,9000)LAMW
      READ(50,9000)TSUBE1,TSUBE2
      READ(50,9000)YSUBV1,YSUBV2
      READ(50,9000)FSUBP
      READ(50,9000)FSUBS
      READ(50,9000)QSUBF
      READ(50,9000)TSUBF
      READ(50,9000)UV,UM,UF,UL
      READ(50,9000)TSUBS
      READ(50,9000)FSUBG,FSUBL
      READ(50,9000)TSUBB
      READ(50,9000)P
      READ(50,9070)TAUBEF,MSUBB,VSUBM
      TAUCM=UM/365.
      TAUBM=UF/365.
      V=(UL+UV)/365.
      A=(UV+UL)/YSUBV2
      READ(50,9070)R1,R2
      S10=R2
      S30=R1
      S1=R2
      S3=R1
      WRITE(51,9001)
      IF (LIPO.EQ.1) GO TO 50
      WRITE(51,9002)
      GO TO 60
   50 WRITE(51,9003)
   60 CONTINUE
      IF (NNTB.GT.0) GO TO 70
      WRITE(51,9004)
      GO TO 80
   70 WRITE(51,9005)NNTB
   80 CONTINUE
      IF (NRTB.NE.0) WRITE(51,9006)
      IF (NSTB.NE.0) WRITE(51,9007)
      IF (NTTB.NE.0) WRITE(51,9008)
      IF (NUTB.NE.0) WRITE(51,9009)
      WRITE(51,9071)
      WRITE(51,9072)
      WRITE(51,9072)
      WRITE(51,9073)
      WRITE(51,9074)
      WRITE(51,9075)
      WRITE(51,9076)
      WRITE(51,9072)
      DO 100 NO=1,20
         DO 90 NR=1,20
            WRITE(51,9077)NO,NR,NOBCT(NO,NR),NOMCT(NO,NR),INTFC(NO,NR),
     >       INTWA(NO,NR),INTPA(NO,NR)
C
   90       CONTINUE
  100    CONTINUE
```

```
      WRITE(51,9078)
      WRITE(51,9079)
      WRITE(51,9080)NNUCS
      WRITE(51,9012)TSUBH1
      WRITE(51,9013)TSUBH2
      WRITE(51,9014)TSUBH3
      WRITE(51,9015)TSUBH4
      WRITE(51,9016)LAMW
      WRITE(51,9017)TSUBE1
      WRITE(51,9018)TSUBE2
      WRITE(51,9019)YSUBV1
      WRITE(51,9020)YSUBV2
      WRITE(51,9021)FSUBP
      WRITE(51,9022)FSUBS
      WRITE(51,9023)QSUBF
      WRITE(51,9024)TSUBF
      WRITE(51,9025)UV
      WRITE(51,9026)UM
      WRITE(51,9027)UF
      WRITE(51,9028)UL
      WRITE(51,9029)TSUBS
      WRITE(51,9030)FSUBG
      WRITE(51,9031)FSUBL
      WRITE(51,9011)TSUBB
      WRITE(51,9010)P
      WRITE(51,9081)RVEG
      WRITE(51,9082)RBEF
      WRITE(51,9083)RMLK
      WRITE(51,9072)
      IF (IMPFIX.EQ.0) GO TO 110
      WRITE(51,9084)
      GO TO 120
  110 WRITE(51,9085)
  120 WRITE(51,9086)F3VEGM
      WRITE(51,9087)F3BEFM
      WRITE(51,9088)F3MLKM
      WRITE(51,9089)BRTHRT
      WRITE(51,9090)T
      WRITE(51,9091)DILFAC
      WRITE(51,9092)USEFAC
      WRITE(51,9093)MSUBB
      WRITE(51,9096)TAUBEF
      WRITE(51,9097)VSUBM
      WRITE(51,9094)S1
      WRITE(51,9095)S3
      WRITE(51,9098)DD1
      TPOP=0
      TNOBCT=0
      TNOMCT=0
      TARFC=0
      DO 140 NO=NOL,NOU
         DO 130 NR=NRL,NRU
            TPOP=INTPA(NO,NR)+TPOP
            TNOBCT=NOBCT(NO,NR)+TNOBCT
            TNOMCT=NOMCT(NO,NR)+TNOMCT
  130       TARFC=INTFC(NO,NR)+TARFC
  140    CONTINUE
      ANUMM=TARFC/A
```

```
      TKGBCA=TAUBM*365.*TPOP
      ANOBCT=TNOBCT
      TKGBPA=ANOBCT*TAUBEP*365.*MSUBB
      CONMK=TAUCM*TPOP
      ANOMCT=TNOMCT
      PRNMK=VSUBM*ANOMCT
      YCONMK=CONMK*365.
      YPRNMK=PRNMK*365.
      PFCY=YSUBV2*TARFC
      CFCY=TPOP*V*365.
      AF=ANUMM/TPOP
      IF (ANUMM.GE.TPOP) AF=1.
      F3V=F3VEGM
      IF ((1.-AF).GE.F3V) F3V=1.-AF
      IF (IMPFIX.EQ.1) F3V=F3VEGM
      F1V=RVEG*(1.-F3V)
      F2V=1.-F3V-F1V
      BF=TKGBPA/TKGBCA
      IF (TKGBPA.GE.TKGBCA) BF=1.
      F3B=F3BEFM
      IF ((1.-BF).GE.F3B) F3B=1.-BF
      IF (IMPFIX.EQ.1) F3B=F3BEFM
      F1B=RBEF*(1.-F3B)
      F2B=1.-F3B-F1B
      CF=PRNMK/CONMK
      IF (PRNMK.GE.CONMK) CF=1.
      F3M=F3MLKM
      IF ((1.-CF).GE.F3M) F3M=1.-CF
      IF (IMPFIX.EQ.1) F3M=F3MLKM
      F1M=RMLK*(1.-F3M)
      F2M=1.-F3M-F1M
      WRITE(51,9099)
      WRITE(51,9100)TPOP
      WRITE(51,9101)TNOBCT
      WRITE(51,9102)TNOMCT
      WRITE(51,9103)TARFC
      WRITE(51,9104)TKGBCA
      WRITE(51,9105)TKGBPA
      WRITE(51,9106)YCONMK
      WRITE(51,9107)YPRNMK
      WRITE(51,9108)CFCY
      WRITE(51,9109)PFCY
      DO 680 I = 1, NNUCS
         READ(50,9110)NUMORG,LAMBR,CFSBA,CFSBW,CFSUR,KFLAG,TDCF,TDCW
         READ(50,9111) (PROG(IM),IM=1,11)
         READ(50,9000)FSUBMI,FSUBFI,BSUBV1,BSUBV2
         READ(50,9112)LAMSUR,LAMH2O,IFLAG,RD1,RD2,RW1,RW2
         READ(50,9032)I1,I2,I3,I4,I5,F1,F2,F3,F4,F5
         LAMI = LAMBR/24.
C  IFLAG=1 IF SPECIAL VALUES USED FOR R1 AND R2
C  IFLAG=2 IF R1 AND R2 ARE GIVEN FOR DRY AND WET DEPOSITION
         SD3=RD1
         SD1=RD2
         SW3=RW1
         SW1=RW2
C READ INHALATION DOSE CONVERSION FACTORS
C HEADER CARD GIVES  SOLUBILITY, PARTICLE SIZE, AND G.I. UPTAKE FRACTION
         READ(50,9033)ISOL,AMAD,F1INH
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      DO 150 J=1,NUMORG
         READ(50,9034) NAMORG(J),CFINHA(J)
  150    CONTINUE
C READ INGESTION DOSE CONVERSION FACTORS
C HEADER CARD GIVES G.I. UPTAKE FRACTION
      READ(50,9035) F1ING
      DO 160 J=1,NUMORG
         READ(50,9035) CFINGA(J)
  160    CONTINUE
      CLASS(I)=ISOL
      PARSIZ(I)=AMAD
      GI(I,1)=F1INH
      GI(I,2)=F1ING
      IF (I1.EQ.0) GO TO 170
      IF (I2.EQ.0) I2=1
      IF (I3.EQ.0) I3=1
      IF (I4.EQ.0) I4=1
      IF (I5.EQ.0) I5=1
  170 CONTINUE
      IF (I.GT.NNTB) GO TO 180
      WRITE(51,9113) NAMNUC(I)
      WRITE(51,9072)
      WRITE(51,9114)
      WRITE(51,9115)
      WRITE(51,9072)
      WRITE(51,9116)
      WRITE(51,9117)
      WRITE(51,9072)
  180 VAGCON(I)=0.
      BAGCON(I)=0.
      MAGCON(I)=0.
      VAGAC(I)=0.
      BAGAC(I)=0.
      MAGAC(I)=0.
      IF (I1.NE.0) GO TO 210
      DO 200 NO=NOL,NOU
         DO 190 NR=NRL,NRU
            VAGCON(I)=INTFC(NO,NR)*GCON(I,NO,NR)+VAGCON(I)
            BAGCON(I)=NOBCT(NO,NR)*GCON(I,NO,NR)+BAGCON(I)
            MAGCON(I)=NOMCT(NO,NR)*GCON(I,NO,NR)+MAGCON(I)
            VAGAC(I)=INTFC(NO,NR)*ACON(I,NO,NR)+VAGAC(I)
            BAGAC(I)=NOBCT(NO,NR)*ACON(I,NO,NR)+BAGAC(I)
            MAGAC(I)=NOMCT(NO,NR)*ACON(I,NO,NR)+MAGAC(I)
  190       CONTINUE
  200    CONTINUE
      VAGCON(I)=VAGCON(I)/TARFC
      BAGCON(I)=BAGCON(I)/ANOBCT
      MAGCON(I)=MAGCON(I)/ANOMCT
      VAGAC(I)=VAGAC(I)/TARFC
      BAGAC(I)=BAGAC(I)/ANOBCT
      MAGAC(I)=MAGAC(I)/ANOMCT
      GO TO 290
  210 IF (REL(1,I).NE.0.) GO TO 240
      DO 230 NO=NOL,NOU
         DO 220 NR=NRL,NRU
            GCI=F1*GCON(I1,NO,NR)+F2*GCON(I2,NO,NR)+F3*GCON(I3,NO,NR)
     >       + F4*GCON(I4,NO,NR)+F5*GCON(I5,NO,NR)
            VAGCON(I)=INTFC(NO,NR)*GCI+VAGCON(I)
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            BAGCON(I)=NOBCT(NO,NR)*GCI+BAGCON(I)                        DOSE1440
            MAGCON(I)=NOMCT(NO,NR)*GCI+MAGCON(I)                        DOSE1445
220         CONTINUE                                                    DOSE1450
230      CONTINUE                                                       DOSE1455
      VAGCON(I)=VAGCON(I)/TARFC                                         DOSE1460
      BAGCON(I)=BAGCON(I)/ANOBCT                                        DOSE1465
      MAGCON(I)=MAGCON(I)/ANOMCT                                        DOSE1470
      GO TO 290                                                         DOSE1475
240   MODE=1                                                            DOSE1480
      BSUBV=BSUBV2                                                      DOSE1485
      TSUBE=TSUBE2                                                      DOSE1490
      YSUBV=YSUBV2                                                      DOSE1495
      TSUBH=TSUBH4                                                      DOSE1500
      DR=DD1                                                            DOSE1505
      DO 260 NO=NOL,NOU                                                 DOSE1510
         DO 250 NR=NRL,NRU                                              DOSE1515
            GCN=GCON(I,NO,NR)                                           DOSE1520
            ACN=ACON(I,NO,NR)                                           DOSE1525
            CALL RVALUE(IFLAG,MODE,I,NO,NR,R)                           DOSE1530
            A=CV(I,LAMI,1.,1.,TSUBE,YSUBV,TSUBH,R)                      DOSE1535
            GCI=F1*GCON(I1,NO,NR)+F2*GCON(I2,NO,NR)+F3*GCON(I3,NO,NR)   DOSE1540
     >       + F4*GCON(I4,NO,NR)+F5*GCON(I5,NO,NR)                      DOSE1545
            GFA=GCON(I,NO,NR)+RATUA*GCI                                 DOSE1550
            VAGCON(I)=INTFC(NO,NR)*GFA+VAGCON(I)                        DOSE1555
250         CONTINUE                                                    DOSE1560
260      CONTINUE                                                       DOSE1565
      VAGCON(I)=VAGCON(I)/TARFC                                         DOSE1570
      MODE=2                                                            DOSE1575
      DR=1.                                                             DOSE1580
      TSUBE=TSUBE1                                                      DOSE1585
      YSUBV=YSUBV1                                                      DOSE1590
      BSUBV=BSUBV1                                                      DOSE1595
      TSUBH=TSUBH1                                                      DOSE1600
      DO 280 NO=NOL,NOU                                                 DOSE1605
         DO 270 NR=NRL,NRU                                              DOSE1610
            GCN=GCON(I,NO,NR)                                           DOSE1615
            ACN=ACON(I,NO,NR)                                           DOSE1620
            CALL RVALUE(IFLAG,MODE,I,NO,NR,R)                           DOSE1625
            A=CV(I,LAMI,1.,1.,TSUBE,YSUBV,TSUBH,R)                      DOSE1630
            GCI=F1*GCON(I1,NO,NR)+F2*GCON(I2,NO,NR)+F3*GCON(I3,NO,NR)   DOSE1635
     >       + F4*GCON(I4,NO,NR)+F5*GCON(I5,NO,NR)                      DOSE1640
            GFA=GCON(I,NO,NR)+RATUA*GCI                                 DOSE1645
            BAGCON(I)=NOBCT(NO,NR)*GFA+BAGCON(I)                        DOSE1650
            MAGCON(I)=NOMCT(NO,NR)*GFA+MAGCON(I)                        DOSE1655
270         CONTINUE                                                    DOSE1660
280      CONTINUE                                                       DOSE1665
      BAGCON(I)=BAGCON(I)/ANOBCT                                        DOSE1670
      MAGCON(I)=MAGCON(I)/ANOMCT                                        DOSE1675
290   CONTINUE                                                          DOSE1680
      IF (NAMNUC(I)-NADEC1) 300,310,300                                 DOSE1685
300   NTRIT = 0                                                         DOSE1690
      GO TO 320                                                         DOSE1695
310   NTRIT = 1                                                         DOSE1700
320   CONTINUE                                                          DOSE1705
      DO 560 NO=NOL,NOU                                                 DOSE1710
         DO 550 NR=NRL,NRU                                              DOSE1715
            GCI=0                                                       DOSE1720
            IF (I1.EQ.0) GO TO 330                                      DOSE1725
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          GCI=F1*GCON(I1,NO,NR)+F2*GCON(I2,NO,NR)+F3*GCON(I3,NO,NR)
     >     + F4*GCON(I4,NO,NR)+F5*GCON(I5,NO,NR)
  330     GCN=GCON(I,NO,NR)+GCI
  340     ACN=ACON(I,NO,NR)
          IF (I1.NE.0) GO TO 350
          D1=1.
          D2=1.
          D3=1.
          D4=1.
          IF (GCON(I,NO,NR).EQ.0.) GO TO 350
          D4=F1M+F2M*(MAGCON(I)/GCON(I,NO,NR))
          D3=F1B+F2B*(BAGCON(I)/GCON(I,NO,NR))
          D2=F1V+F2V*(VAGCON(I)/GCON(I,NO,NR))
          D1=D2
          GO TO 360
  350     IF (REL(1,I).NE.0.) GO TO 360
          D4=F1M+F2M*(MAGCON(I)/GCI)
          D3=F1B+F2B*(BAGCON(I)/GCI)
          D2=F1V+F2V*(VAGCON(I)/GCI)
          D1=D2
  360     CONTINUE
  370     DO 540 J=1,11
             X=LAMRR+LAMSUR
             IF (KFLAG.EQ.1) X=ANLAM(I)+LAMSUR
             DO 380 N=1,NUMORG
                IF (NAMES(J)-NAMORG(N)) 380,390,380
  380           CONTINUE
             L=1
             GO TO 400
  390        L=N
C  INHALATION DOSE CALCULATIONS
  400        CFINH=CFINHA(L)
             CFING=CFINGA(L)
             IF (ACN.EQ.0) DOS1=0
             IF (ACN.EQ.0) DOS2=0
             IF (ACN.EQ.0.) GO TO 410
             DOS1=ACN*1.E-6*BRTHRT*8760.*CFINH
C  AIR SUBMERSION DOSE CALCULATIONS
             DOS2=ACN*1.E-6*8760.*CFSBA*FROG(J)
C  SURFACE EXPOSURE DOSE CALCULATIONS
  410        ALT=X*T
             IF (ALT.GT.0.03) GO TO 420
             DOS3=GCN*1.E-6*8760.*CFSUR*FROG(J)*((0.1666667*ALT-
     >         0.5)*ALT+T) *3600.*24.
             GBUP(I,NO,NR)=GCN*1.E-8*24.*3600.* ((0.1666667*ALT-
     >         0.5)*ALT+T)
             GO TO 430
  420        DOS3=GCN*1.E-6*8760.*CFSUR*FROG(J)*(1-EXP(-X*T))/X*
     >         3600.*24.
             GBUP(I,NO,NR)=GCN*1.E-8*24.*3600.*(1.-EXP(-X*T))/X
C  INGESTION DOSE CALCULATIONS
  430        IF (NTRIT.NE.1.AND.NAMNUC(I).NE.NADEC3) GO TO 450
             IF (NTRIT.NE.1) GO TO 440
C  INGESTION DOSE CALCULATIONS FOR H-3
             VEGDOS(J)=(F1V*ACN+F2V*VAGAC(I))*TDCP*.505
             BEFDOS(J)=(F1B*ACN+F2B*BAGAC(I))*TDCP*.185
             MLKDOS(J)=(F1M*ACN+F2M*MAGAC(I))*TDCP*.310
             DOSING(J)=VEGDOS(J)+BEFDOS(J)+MLKDOS(J)+ACN*TDCW
```

```
                  KIQ(I,NO,NR)=(((F1V*ACN+F2V*VAGAC(I))*1.E6)/8.)*1560.*DOSE2020
     >             .505*365.+(((ACN*1.E6)/8.)*1440.*365.)*(TDCW/5.70)   DOSE2021
                  GFIN(I,NO,NR)=(((F1B*ACN+F2B*BAGAC(I))*1.E6)/8.)*1560.DOSE2025
     >             *.185*365.                                           DOSE2026
                  FING(I,NO,NR)=(((F1M*ACN+F2M*MAGAC(I))*1.E6)/8.)*1560.DOSE2030
     >             *.310*365.                                           DOSE2031
                  TDCWB=TDCW                                            DOSE2034
                  GO TO 480                                             DOSE2035
  440             CONTINUE                                              DOSE2040
C  INGESTION DOSE CALCULATIONS FOR C-14                                 DOSE2045
                  WTCV=79.96*V                                          DOSE2050
                  WTCB=238.16*TAUBM                                     DOSE2055
                  WTCM=68.9*TAUCM                                       DOSE2060
                  WTF=WTCV+WTCB+WTCM                                    DOSE2065
                  DOSING(J)=(DCC14(J)/WTF)*(WTCV*(F1V*ACN+F2V*VAGAC(I))+DOSE2070
     >             WTCB*(F1B*ACN+F2B*BAGAC(I))+WTCM*(F1M*ACN+F2M*       DOSE2075
     >             MAGAC(I)))                                           DOSE2080
                  VEGDOS(J)=(DCC14(J)/WTF)*(WTCV*(F1V*ACN+F2V*VAGAC(I)))DOSE2085
                  BEFDOS(J)=(DCC14(J)/WTF)*(WTCV*(F1B*ACN+F2B*BAGAC(I)))DOSE2090
                  MLKDOS(J)=(DCC14(J)/WTF)*(WTCV*(F1M*ACN+F2M*MAGAC(I)))DOSE2095
                  KIQ(I,NO,NR)=((F1V*ACN+F2V*VAGAC(I))/1.8E-7)*WTCV*365.DOSE2100
                  GFIN(I,NO,NR)=((F1B*ACN+F2B*BAGAC(I))/1.8E-7)*WTCB*365DOSE2105
     >                                                                  DOSE2106
                  FING(I,NO,NR)=((F1M*ACN+F2M*MAGAC(I))/1.8E-7)*WTCM*365DOSE2110
     >                                                                  DOSE2111
                  GO TO 480                                             DOSE2115
C  INGESTION DOSES DEFINED AS ZERO IF GROUND CONCENTRATION IS ZERO      DOSE2120
  450             IF (GCN.NE.0) GO TO 460                               DOSE2125
                  DOSING(J)=0.                                          DOSE2130
                  VEGDOS(J)=0.                                          DOSE2135
                  BEFDOS(J)=0.                                          DOSE2140
                  MLKDOS(J)=0.                                          DOSE2145
                  KIQ(I,NO,NR)=0.                                       DOSE2150
                  GFIN(I,NO,NR)=0.                                      DOSE2155
                  FING(I,NO,NR)=0.                                      DOSE2160
                  GO TO 480                                             DOSE2165
C INGESTION DOSE CALCULATIONS USING NRC MODEL                           DOSE2170
C CALCULATE CIV=CONCENTRATION OF RADIONUCLIDE IN THE ANIMAL'S FEED USINGDOSE2175
C SLIGHTLY SIMPLIFIED FORM OF EQ C-11, REG GUIDE 1.109.27.              DOSE2180
C CIV= FSUBP*FSUBS*(CONC. OF NUCLIDE ON PASTURE GRASS)                  DOSE2185
C       + (1.0-FSUBP*FSUBS)*(CONC. OF NUCLIDE IN STORED FEEDS)          DOSE2190
C USE PARAMETERS FOR GRASS-COW-MILK-MAN-PATHWAY                         DOSE2195
C FIRST TERM..  USE TSUBH VALUE FOR INGESTION BY ANIMALS OF PASTURE GRASDOSE2200
C THE DEPOSITION RATE GCN IS IN UNITS OF PCI/SQUARE CM-SEC.             DOSE2205
C TO CONVERT TO PCI/SQUARE METER-HR,MULTIPLY BY 3.6E7.                  DOSE2210
  460             DEPRAT= GCN*3.6E7                                     DOSE2215
                  GCRU=GCON(I,NO,NR)*3.6E7                              DOSE2220
                  GCN=GCRU/3.6E7                                        DOSE2225
                  TSUBH=TSUBH1                                          DOSE2230
                  TSUBE=TSUBE1                                          DOSE2235
                  YSUBV=YSUBV1                                          DOSE2240
                  BSUBV=BSUBV1                                          DOSE2245
C LAMI IS THE RADIOACTIVE DECAY CONSTANT OF NUCLIDE I, IN HR**-1.       DOSE2250
                  LAMI = LAMRR/24.                                      DOSE2255
                  MODE=2                                                DOSE2260
                  CALL RVALUE(IFLAG,MODE,I,NO,NR,R)                     DOSE2265
                  DR=1.                                                 DOSE2270
                  TERM1=FSUBP*FSUBS *CV(I,LAMI,DEPRAT,GCRU,TSUBE,YSUBV, DOSE2275
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```
     >              TSUBH,R)
C SECOND TERM..  USE TSUBH VALUE FOR INGESTION BY ANIMALS OF STORED FEED
                    TSUBH=TSUBH2
                    TERM2=(1.0-FSUBP*FSUBS)*CV(I,LAMI,DEPRAT,GCRU,TSUBE,
     >               YSUBV,TSUBH,R)
                    CIV=TERM1 + TERM2
C
C CALCULATE CIM=NUCLIDE CONCENTRATION IN MILK USING EQ C-10, REG GUIDE
C 1.109-27
                    CIM=FSUBMI*CIV*QSUBF*EXP(-LAMRR*TSUBF)
C DFIJ IS THE DOSE CONVERSION FACTOR FOR THE INGESTION OF NUCLIDE I, ORG
C IN MREM/PCI.
                    DFIJ = 0.001*CFING
C CALCULATE MLKDOS(J)=ANNUAL DOSE TO ORGAN J FROM INGESTION OF RADIONUCL
C IN MILK USING EQ C-13,  REG GUIDE 1.109-28.
                    IF (I1.NE.0.AND.REL(1,I).NE.0.) D4=F1M+F2M*(MAGCON(I)/
     >                (GCON(I,NO,NR)+RATUA*GCI))
                    IF (I1.NE.0.AND.REL(1,I).NE.0.) D3=F1B+F2B*(BAGCON(I)/
     >                (GCON(I,NO,NR)+RATUA*GCI))
                    MLKDOS(J)=DFIJ*UM*CIM*D4
C THE NRC MODEL GIVES DOSES IN MREM/YR.  TO CONVERT TO REM/YR,
C MULTIPLY BY 0.001
                    MLKDOS(J) = MLKDOS(J)*.001
C CALCULATE CIF=NUCLIDE CONCENTRATION IN MEAT USING EQ C-12, REG GUIDE 1
                    CIF=FSUBFI*CIV*QSUBF*EXP(-LAMRR *TSUBS)
C CALCULATE BEFDOS(J)=ANNUAL DOSE TO ORGAN J FROM INGESTION OF
C RADIONUCLIDE I IN MEAT.  (REG GUIDE 1.109-28, EQ C-13)
                    BEFDOS(J)=DFIJ*UF*CIF*D3
                    BEFDOS(J) = BEFDOS(J) *.001
C CALCULATE CIVP=CONCENTRATION OF RADIONUCLIDE IN PRODUCE CONSUMED BY MA
C USE PARAMETERS FOR CROP/VEGETATION-MAN PATHWAY., TSUBH VALUE FOR PRODU
                    TSUBE= TSUBE2
                    YSUBV= YSUBV2
                    TSUBH= TSUBH4
                    BSUBV=BSUBV2
                    DR=DD1
                    MODE=1
                    CALL RVALUE(IFLAG,MODE,I,NO,NR,R)
                    CIVP=CV(I,LAMI,DEPRAT,GCRU,TSUBE,YSUBV,TSUBH,R)
C CALCULATE PRODOS=ANNUAL DOSE TO ORGAN J FROM INGESTION BY MAN OF RADIO
C IN PRODUCE.   (REG GUIDE 1.109-28, EQ C-13)
                    IF (I1.NE.0.AND.REL(1,I).NE.0.) D2=F1V+F2V*(VAGCON(I)/
     >                (GCON(I,NO,NR)+RATUA*GCI))
                    D1=D2
                    PRODOS=DFIJ*UV*FSUBG*CIVP*D2
C CALCULATE CIVL=CONCENTRATION OF RADIONUCLIDE IN LEAFY VEGETABLES.
C USE PARAMETERS FOR CROP/VEGETATION-MAN PATHWAY.
C THE TSUBH VALUE IS FOR LEAFY VEGETABLES.
                    TSUBE=TSUBE2
                    YSUBV=YSUBV2
                    TSUBH=TSUBH3
                    BSUBV=BSUBV2
                    DR=DD1
                    CIVL=CV(I,LAMI,DEPRAT,GCRU,TSUBE,YSUBV,TSUBH,R)
C CALCULATE LEFDOS=ANNUAL DOSE TO ORGAN J FROM INGESTION OF RADIONUCLIDE
C IN LEAFY VEGETABLES.   (REG GUIDE 1.109-28, EQ C-13)
                    LEFDOS=DFIJ*UL*FSUBL*CIVL*D1
C VEGDOS(J) IS THE ANNUAL DOSE TO ORGAN J FROM INGESTION OF RADIONUCLIDE
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C IN PRODUCE AND LEAFY VEGETABLES.
                  VEGDOS(J)=PRODOS + LEFDOS
                  VEGDOS(J) = VEGDOS(J)*.001
                  DOSING(J)=BEFDOS(J) + MLKDOS(J) + VEGDOS(J)
                  IF (J.NE.11) GO TO 470
                  KIQ(I,NO,NR)=UL*FSUBL*CIVL*D1+UV*FSUBG*CIVP*D2
                  GFIN(I,NO,NR)=UF*CIF*D3
                  FING(I,NO,NR)=UM*CIM*D4
  470             GCN=DEPRAT/3.6E7
C  WATER SUBMERSION DOSE CALCULATIONS
  480             X=LAMRR+LAMH2O
                  IF (KFLAG.EQ.1) X=ANLAM(I)+LAMH2O
  490             IF (GCN.EQ.0) DOS5=0
                  IF (GCN.EQ.0) GO TO 510
                  ALT=X*T
                  IF (ALT.GT.0.03) GO TO 500
                  DOS5=GCN*1.E-6*8760.*CFSBW*FROG(J)*USEFAC/DILFAC*
     >             ((0.1666667* ALT-0.5)*ALT+T)*3600.*24.
                  GO TO 510
  500             DOS5=GCN*1.E-6*8760.*CFSBW*FROG(J)*USEFAC/DILFAC*(1-
     >             EXP(-X*T))/X *3600.*24.
  510             TDOS=DOS1+DOS2+DOS3+DOSING(J)+DOS5
                  IF (I.GT.NNTB) GO TO 520
                  WRITE(51,9118)NO,NR,NAMES(J),DOS1,DOS2,DOS3,DOSING(J),
     >              DOS5,TDOS
  520             CONTINUE
                  IF (LIPO.EQ.0) GO TO 530
C POPULATION DOSE CALCULATIONS
                  ORMODI(I,J,1)=DOS1*INTPA(NO,NR)+ORMODI(I,J,1)
                  ORMODI(I,J,2)=DOS2*INTPA(NO,NR)+ORMODI(I,J,2)
                  ORMODI(I,J,3)=DOS3*INTPA(NO,NR)+ORMODI(I,J,3)
                  ORMODI(I,J,4)=DOSING(J)*INTPA(NO,NR)+ORMODI(I,J,4)
                  ORMODI(I,J,5)=DOS5*INTPA(NO,NR)+ORMODI(I,J,5)
                  ORMODI(I,J,6)=VEGDOS(J)*INTPA(NO,NR)+ORMODI(I,J,6)
                  ORMODI(I,J,7)=BEFDOS(J)*INTPA(NO,NR)+ORMODI(I,J,7)
                  ORMODI(I,J,8)=MLKDOS(J)*INTPA(NO,NR)+ORMODI(I,J,8)
                  GO TO 540
C  CALCULATIONS OF THE HIGHEST INDIVIDUAL DOSE FOR EACH RADIONUCLIDE
C  AND ORGAN AND GRID LOCATION WHERE RECEIVED
  530             IF (TDOS.LE.DOSIN(J,I)) GO TO 540
                  NOMM(I,J)=NO
                  NRMM(I,J)=NR
                  ORMODI(I,J,1)=DOS1
                  ORMODI(I,J,2)=DOS2
                  ORMODI(I,J,3)=DOS3
                  ORMODI(I,J,4)=DOSING(J)
                  ORMODI(I,J,5)=DOS5
                  ORMODI(I,J,6)=VEGDOS(J)
                  ORMODI(I,J,7)=BEFDOS(J)
                  ORMODI(I,J,8)=MLKDOS(J)
                  DOSIN(J,I)=TDOS
  540             CONTINUE
  550          CONTINUE
  560       CONTINUE
  570    CONTINUE
  580    WRITE(51,9119)NAMNUC(I)
         IF (IFLAG.GT.2.OR.IFLAG.LT.0) PRINT 9120
  590    IF (IFLAG.NE.1) GO TO 600
```

```
      WRITE(51,9121) SD1
      WRITE(51,9122) SD3
600   IF (IFLAG.NE.2) GO TO 610
      WRITE(51,9123) SD1
      WRITE(51,9124) SW1
      WRITE(51,9125) SD3
      WRITE(51,9126) SW3
610   WRITE(51,9127) LAMRR
      IF (KFLAG.NE.1) GO TO 620
      WRITE(51,9128)
      WRITE(51,9129)
620   WRITE(51,9130) LAMSUR
      WRITE(51,9131) LAMH2O
      IF (NTRIT.NE.1) GO TO 630
      WRITE(51,9132) TDCF
      WRITE(51,9133) TDCW
630   IF (NTRIT.EQ.1) GO TO 650
      WRITE(51,9036)  FSUBMI
      WRITE(51,9037)  FSUBFI
      WRITE(51,9038)  BSUBV1
      WRITE(51,9039)
      WRITE(51,9040)  BSUBV2
      WRITE(51,9041)
      WRITE(51,9042) F1INH
      WRITE(51,9043) F1ING
      WRITE(51,9044) AMAD
      WRITE(51,9045) ISOL
      IF (I1.EQ.0) GO TO 640
      WRITE(51,9046)
      WRITE(51,9047)
      WRITE(51,9048)
      WRITE(51,9049) NAMNUC(I1),F1
      IF (F2.EQ.0.) GO TO 640
      WRITE(51,9050) NAMNUC(I2),F2
      IF (F3.EQ.0.) GO TO 640
      WRITE(51,9050) NAMNUC(I3),F3
      IF (F4.EQ.0.) GO TO 640
      WRITE(51,9050) NAMNUC(I4),F4
      IF (F5.EQ.0.) GO TO 640
      WRITE(51,9050) NAMNUC(I5),F5
640   CONTINUE
650   CONTINUE
      WRITE(51,9134)
      WRITE(51,9135)
      WRITE(51,9136)
      WRITE(51,9137)
      WRITE(51,9072)
      DO 670 J=1,NUMORG
         DO 660 K=1,11
            IF (NAMORG(J).NE.NAMES(K)) GO TO 660
            CASBA=CFSBA*FROG(K)
            CASUR=CFSUR*FROG(K)
            CASBW=CFSBW*FROG(K)
            WRITE(51,9138) NAMORG(J),CFINHA(J),CFINGA(J),CASBA,CASUR,
     >      CASBW
            CONTINUE
660      CONTINUE
670   CONTINUE
680   CONTINUE
```

```
C START OF MAXIMIZING CALCULATIONS FOR THE INDIVIDUAL DOSE OPTION       DOSE3150
      IF (LIPO.EQ.1) GO TO 850                                          DOSE3155
      DO 840 J=1,11                                                     DOSE3160
         ADSE=0                                                         DOSE3165
         DO 750 NO=NOL,NOU                                              DOSE3170
            DO 740 NR=NRL,NRU                                           DOSE3175
               DSE=0                                                    DOSE3180
               AKR=0                                                    DOSE3185
               BKR=0                                                    DOSE3190
               DKR=0                                                    DOSE3195
               EKR=0                                                    DOSE3200
               VEG=0                                                    DOSE3205
               BEF=0                                                    DOSE3210
               AME=0                                                    DOSE3215
               DO 730 I=1,NNUCS                                         DOSE3220
                  AC=ACON(I,NOMM(I,J),NRMM(I,J))                        DOSE3225
                  IF (AC.EQ.0.) GO TO 690                               DOSE3230
                  AKR=ORMODI(I,J,1)/AC*ACON(I,NO,NR)+AKR                DOSE3235
                  BKR=ORMODI(I,J,2)/AC*ACON(I,NO,NR)+BKR                DOSE3240
  690             BC=GBUP(I,NOMM(I,J),NRMM(I,J))                        DOSE3245
                  IF (BC.EQ.0) GO TO 700                                DOSE3250
                  DKR=ORMODI(I,J,3)/BC*GBUP(I,NO,NR)+DKR                DOSE3255
                  EKR=ORMODI(I,J,5)/BC*GBUP(I,NO,NR)+EKR                DOSE3260
  700             IF (NAMNUC(I).EQ.NADEC1.OR.NAMNUC(I).EQ.NADEC3) GO TO DOSE3265
     >             710                                                  DOSE3270
                  IF (BC.EQ.0) GO TO 720                                DOSE3275
                  VEG=ORMODI(I,J,6)*(KIQ(I,NO,NR)/(KIQ(I,NOMM(I,J),     DOSE3280
     >             NRMM(I,J))+1.E-60))+VEG                              DOSE3285
                  BEF=ORMODI(I,J,7)*(GFIN(I,NO,NR)/(GFIN(I,NOMM(I,J),   DOSE3290
     >             NRMM(I,J))+1.E-60))+BEF                              DOSE3295
                  AME=ORMODI(I,J,8)*(FING(I,NO,NR)/(FING(I,NOMM(I,J),   DOSE3300
     >             NRMM(I,J))+1.E-60))+AME                              DOSE3305
                  GO TO 720                                             DOSE3310
  710             ACO=ACON(I,NO,NR)                                     DOSE3315
                  VEG=((F1V*ACO+F2V*VAGAC(I))/(F1V*AC+F2V*VAGAC(I)+1.E- DOSE3320
     >             60))* ORMODI(I,J,6)+VEG                              DOSE3325
                  BEF=((F1B*ACO+F2B*BAGAC(I))/(F1B*AC+F2B*BAGAC(I)+1.E- DOSE3330
     >             60))* ORMODI(I,J,7)+BEF                              DOSE3335
                  AME=((F1M*ACO+F2M*MAGAC(I))/(F1M*AC+F2M*MAGAC(I)+1.E- DOSE3340
     >             60))* ORMODI(I,J,8)+AME                              DOSE3345
                  IF (NAMNUC(I).EQ.NADEC1) AME=AME+ACO*TDCWB            DOSE3349
  720             CONTINUE                                              DOSE3350
                  TING=VEG+BEF+AME                                      DOSE3355
  730             DSE=AKR+BKR+DKR+EKR+TING                              DOSE3365
               IF (DSE.LT.ADSE) GO TO 740                               DOSE3370
               ADSE=DSE                                                 DOSE3375
               NOML(J)=NO                                               DOSE3380
               NRML(J)=NR                                               DOSE3385
  740          CONTINUE                                                 DOSE3390
  750       CONTINUE                                                    DOSE3395
         NO=NOML(J)                                                     DOSE3400
         NR=NRML(J)                                                     DOSE3405
         DO 830 I=1,NNUCS                                               DOSE3410
            AC=ACON(I,NOMM(I,J),NRMM(I,J))                              DOSE3415
      IF (AC.EQ.0.) GO TO 760                                           DOSE3419
            ACI=ACON(I,NO,NR)                                           DOSE3420
            IF (ACI.EQ.0.) GO TO 760                                    DOSE3425
            ORMODI(I,J,1)=ORMODI(I,J,1)/AC*ACI                          DOSE3430
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```
            ORMODI(I,J,2)=ORMODI(I,J,2)/AC*ACI
            GO TO 770
  760       ORMODI(I,J,1)=0.
            ORMODI(I,J,2)=0.
  770       BC=GBUP(I,NOMM(I,J),NRMM(I,J))
      IF (BC.EQ.0.) GO TO 780
            BCI=GBUP(I,NO,NR)
            IF (BCI.EQ.0) GO TO 780
            ORMODI(I,J,3)=ORMODI(I,J,3)/BC*BCI
            ORMODI(I,J,5)=ORMODI(I,J,5)/BC*BCI
            GO TO 790
  780       ORMODI(I,J,3)=0
            ORMODI(I,J,5)=0
  790       IF (NAMNUC(I).EQ.NADEC1.OR.NAMNUC(I).EQ.NADEC3) GO TO 810
            IF (BCI.EQ.0) GO TO 800
            ORMODI(I,J,6)=ORMODI(I,J,6)*(KIQ(I,NO,NR)/(KIQ(I,NOMM(I,J),
     >       NRMM(I,J))+1.E-60))
            ORMODI(I,J,7)=ORMODI(I,J,7)*(GPIN(I,NO,NR)/(GPIN(I,NOMM(I,J)
     >       ,NRMM(I,J))+1.E-60))
            ORMODI(I,J,8)=ORMODI(I,J,8)*(PING(I,NO,NR)/(PING(I,NOMM(I,J)
     >       ,NRMM(I,J))+1.E-60))
            GO TO 820
  800       ORMODI(I,J,6)=0
            ORMODI(I,J,7)=0
            ORMODI(I,J,8)=0
            GO TO 820
  810       CONTINUE
            ORMODI(I,J,6)=((F1V*ACI+F2V*VAGAC(I))/(F1V*AC+F2V*VAGAC(I)+
     >       1.E-60) )* ORMODI(I,J,6)
            ORMODI(I,J,7)=((F1B*ACI+F2B*BAGAC(I))/(F1B*AC+F2B*BAGAC(I)+
     >       1.E-60) )* ORMODI(I,J,7)
            ORMODI(I,J,8)=((F1M*ACI+F2M*MAGAC(I))/(F1M*AC+F2M*MAGAC(I)+
     >       1.E-60) )* ORMODI(I,J,8)
  820       ORMODI(I,J,4)=ORMODI(I,J,6)+ORMODI(I,J,7)+ORMODI(I,J,8)
            IF (NAMNUC(I).EQ.NADEC1) ORMODI(I,J,4)=ORMODI(I,J,4)+ACI*
     >       TDCWB
  830       CONTINUE
  840    CONTINUE
C END OF MAXIMIZING CALCULATIONS FOR THE INDIVIDUAL DOSE OPTION
  850 IF (NRTB.EQ.0) GO TO 880
      DO 870 I=1,NNUCS
         PUNCH 9139,NAMNUC(I)
         DO 860 MD=1,8
            PUNCH 9140,(ORMODI(I,J,MD),J=1,11)
  860       CONTINUE
  870    CONTINUE
  880 CONTINUE
C  OUTPUT FOR HEALTH RISK CALCULATIONS
      IF (NSTB.EQ.0) GO TO 980
      IF (FEQWL.EQ.0.) FEQWL=0.7
      DO 970 I=1,NNUCS
         TIME=0
         WRITE(25)NAMNUC(I),PARSIZ(I),CLASS(I),(GI(I,J),J=1,4),TIME,LIPO
         WRITE(25)NOL,NOU,NRL,NRU,(IDIST(IG),IG=NRL,NRU)
         IF (LIPO.EQ.1) GO TO 890
         WRITE(51,9051)NAMNUC(I)
         GO TO 900
  890    WRITE(51,9052)NAMNUC(I)
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900     CONTINUE                                                        DOSE3720
        WRITE(51,9053)                                                  DOSE3725
        IF (LIPO.EQ.1) GO TO 910                                        DOSE3730
        WRITE(51,9054)                                                  DOSE3735
        GO TO 920                                                       DOSE3740
910     WRITE(51,9055)                                                  DOSE3745
920     WRITE(51,9056)                                                  DOSE3750
        WRITE(51,9057)                                                  DOSE3755
        WRITE(51,9058)                                                  DOSE3760
        ALIP=LIPO                                                       DOSE3765
        DO 960 NO=NOL,NOU                                               DOSE3770
           DO 950 NR=NRL,NRU                                            DOSE3775
              ACUP=ACON(I,NO,NR)*1.E-6*(ALIP*(INTPA(NO,NR)-1.)+1.)      DOSE3780
              GBIP=GBUP(I,NO,NR)*(ALIP*(INTPA(NO,NR)-1.)+1.)            DOSE3785
              FIOP=(KIQ(I,NO,NR)+GFIN(I,NO,NR)+FING(I,NO,NR))* (ALIP*   DOSE3790
     >         (INTPA(NO,NR)-1.)+1.)                                    DOSE3795
              FINH=ACON(I,NO,NR)*BRTHRT*8760.*(ALIP*(INTPA(NO,NR)-1.)+  DOSE3800
     >         1.)                                                      DOSE3805
              WRITE(51,9059)NO,IDIST(NR),ACUP,GBIP,FIOP,FINH            DOSE3810
              IF (NAMNUC(I).EQ.NADRN) GO TO 930                         DOSE3815
              WRITE(25) ACUP,GBIP,FIOP,FINH                             DOSE3820
              GO TO 940                                                 DOSE3825
930        WAL=FEQWL*10.*ACON(I,NO,NR)*(ALIP*(INTPA(NO,NR)-1.)+1.)      DOSE3830
              WRITE(25) FEQWL,WAL                                       DOSE3835
940           CONTINUE                                                  DOSE3840
950           CONTINUE                                                  DOSE3845
960        CONTINUE                                                     DOSE3850
        WRITE(51,9060)                                                  DOSE3855
        IF(LIPO.EQ.1)WRITE(25)INTPA                                     DOSE3856
970     CONTINUE                                                        DOSE3860
980   CONTINUE                                                          DOSE3865
      CALL DOSMIC(NTTB,NUTB)                                            DOSE3870
990   RETURN                                                            DOSE3875
9000  FORMAT(8E10.3)                                                    DOSE3885
9001  FORMAT('1',T42,                                                   DOSE3890
     > 'OPTIONS SELECTED FOR DOSE AND INTAKE CALCULATIONS')             DOSE3895
9002  FORMAT('0',T20,'CALCULATIONS ARE MADE FOR THE MAXIMALLY-EXPOSED INDOSE3900
     >DIVIDUAL.')                                                       DOSE3905
9003  FORMAT('0',T20,'CALCULATIONS ARE MADE FOR THE POPULATION.')       DOSE3910
9004  FORMAT(' ',T20,'TABLES FOR EACH NUCLIDE LISTING DOSES BY ORGAN ANDDOSE3915
     > PATHWAY AT EACH ENVIRONMENTAL LOCATION ARE OMITTED.')            DOSE3920
9005  FORMAT(' ',T20,'TABLES LISTING DOSES BY ORGAN AND PATHWAY AT EACH DOSE3925
     >ENVIRONMENTAL LOCATION ARE PRINTED FOR ',I2,' NUCLIDES')          DOSE3930
9006  FORMAT(' ',T20,'DOSES BY NUCLIDE,ORGAN, AND PATHWAY ARE PUNCHED ONDOSE3935
     > CARDS')                                                          DOSE3940
9007  FORMAT(' ',T20,'ENVIRONMENTAL CONCENTRATIONS AND INTAKE RATES BY MDOSE3945
     >AN FOR EACH NUCLIDE ARE PRINTED AND WRITTEN UNFORMATTED.')        DOSE3950
9008  FORMAT(' ',T20,'DOSE SUMMARY TABLES ARE PRINTED')                 DOSE3955
9009  FORMAT(' ',T20,'WORKING LEVELS ARE CALCULATED FOR RN-222 IF IT IS DOSE3960
     >IN THE SOURCE TERM')                                              DOSE3965
9010  FORMAT('0',T13,'EFFECTIVE SURFACE DENSITY OF SOIL (KG/SQ. M, DRY',DOSE3970
     > ' WEIGHT) (ASSUMES 15 CM PLOW LAYER)',T110,E12.4)                DOSE3975
9011  FORMAT('0',T13,'PERIOD OF LONG-TERM BUILDUP FOR ',                DOSE3980
     > 'ACTIVITY IN SOIL (YEARS)',T110,E12.4)                           DOSE3985
9012  FORMAT('0',T13,'TIME DELAY--INGESTION OF PASTURE GRASS BY ',      DOSE3990
     > 'ANIMALS (HR)',T110,E12.4)                                       DOSE3995
9013  FORMAT('0',T13,'TIME DELAY--INGESTION OF STORED FEED BY ',        DOSE4000
     > 'ANIMALS (HR)',T110,E12.4)                                       DOSE4005
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9014 FORMAT('0',T13,'TIME DELAY--INGESTION OF LEAFY VEGETABLES ',
    > 'BY MAN (HR)' ,T110,E12.4)
9015 FORMAT('0',T13,'TIME DELAY--INGESTION OF PRODUCE BY ', 'MAN (HR)',
    > T110,E12.4)
9016 FORMAT('0',T13,'REMOVAL RATE CONSTANT FOR PHYSICAL LOSS BY ',
    > 'WEATHERING (PER HOUR)',T110,E12.4)
9017 FORMAT('0',T13,'PERIOD OF EXPOSURE DURING GROWING SEASON--',
    > 'PASTURE GRASS (HR)',T110,E12.4)
9018 FORMAT('0',T13,'PERIOD OF EXPOSURE DURING GROWING SEASON--',
    > 'CROPS OR LEAFY VEGETABLES (HR)',T110,E12.4)
9019 FORMAT('0',T13,'AGRICULTURAL PRODUCTIVITY BY UNIT AREA ',
    > '(GRASS-COW-MILK-MAN PATHWAY (KG/SQ. METER))',T110,E12.4)
9020 FORMAT('0',T13,'AGRICULTURAL PRODUCTIVITY BY UNIT AREA ',
    > '(PRODUCE OR LEAFY VEG INGESTED BY MAN (KG/SQ. METER))',T110,
    > E12.4)
9021 FORMAT('0',T13,'FRACTION OF YEAR ANIMALS GRAZE ON PASTURE ', T110,
    > E12.4)
9022 FORMAT('0',T13,'FRACTION OF DAILY FEED THAT IS PASTURE GRASS ',
    > 'WHEN ANIMAL GRAZES ON PASTURE',T110,E12.4)
9023 FORMAT('0',T13,'CONSUMPTION RATE OF CONTAMINATED FEED OR FORAGE ',
    >  'BY AN ANIMAL IN KG/DAY (DRY WEIGHT)',T110,E12.4)
9024 FORMAT('0',T13,'TRANSPORT TIME FROM ANIMAL FEED-MILK-MAN (DAY)',
    > T110,E12.4)
9025 FORMAT('0',T13,'RATE OF INGESTION OF PRODUCE BY MAN (KG/YR)',
    > T110,E12.4)
9026 FORMAT('0',T13,'RATE OF INGESTION OF MILK BY MAN (LITERS/YR)',
    > T110,E12.4)
9027 FORMAT('0',T13,'RATE OF INGESTION OF MEAT BY MAN (KG/YR)', T110,
    > E12.4)
9028 FORMAT('0',T13,'RATE OF INGESTION OF LEAFY VEGETABLES BY MAN ',
    > '(KG/YR)',T110,E12.4)
9029 FORMAT('0',T13,'AVERAGE TIME FROM SLAUGHTER OF MEAT ANIMAL TO ',
    > 'CONSUMPTION (DAY)',T110,E12.4)
9030 FORMAT('0',T13,'FRACTION OF PRODUCE INGESTED GROWN IN GARDEN ',
    > 'OF INTEREST',T110,E12.4)
9031 FORMAT('0',T13,'FRACTION OF LEAFY VEGETABLES GROWN IN GARDEN ',
    > 'OF INTEREST',T110,E12.4)
9032 FORMAT(5I4,5E10.3)
9033 FORMAT(T11,A1,T15,E10.3,T27,E10.3)
9034 FORMAT(A8,T10,E10.3)
9035 FORMAT(T11,E10.3)
9036 FORMAT('0',T13,'AVERAGE FRACTION OF ANIMAL''S DAILY INTAKE ',
    > 'OF NUCLIDE WHICH APPEARS IN EACH L OF MILK (DAYS/L)', T110,
    > E12.4)
9037 FORMAT('0',T13,'FRACTION OF ANIMAL''S DAILY INTAKE OF NUCLIDE ',
    > 'WHICH APPEARS IN EACH KG OF FLESH (DAYS/KG)',T110,E12.4)
9038 FORMAT('0',T13,'CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SO
    >IL FOR PASTURE AND FORAGE',T110,E12.4)
9039 FORMAT(' ',T20,'(IN PCI/KG DRY WEIGHT PER PCI/KG DRY SOIL)')
9040 FORMAT('0',T13,'CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SO
    >IL BY EDIBLE PARTS OF CROPS',T110,E12.4)
9041 FORMAT(' ',T20,'(IN PCI/KG WET WEIGHT PER PCI/KG DRY SOIL)')
9042 FORMAT('0',T13,'GI UPTAKE FRACTION (INHALATION)',T110,E12.4)
9043 FORMAT('0',T13,'GI UPTAKE FRACTION (INGESTION)' ,T110,E12.4)
9044 FORMAT('0',T13,'PARTICLE SIZE (MICRONS)',T110,E12.4)
9045 FORMAT('0',T13,'SOLUBILITY CLASS',T110,A1)
9046 FORMAT('0',T20,'CONCENTRATIONS ON GROUND AND WATER INCLUDE CONTRIB
    >UTIONS RESULTING FROM ')
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9047 FORMAT(' ',T20,'DECAY OF THE FOLLOWING PARENT NUCLIDES AFTER DEPOSDOSE4300
    >ITION--')                                                         DOSE4305
9048 FORMAT('0',T40,'NUCLIDE',T67,'BUILDUP FACTOR')                    DOSE4310
9049 FORMAT('0',T41,A8,T69,E10.3)                                      DOSE4315
9050 FORMAT(' ',T41,A8,T69,E10.3)                                      DOSE4320
9051 FORMAT('1',T45,'CONCENTRATIONS AND INTAKE RATES FOR ',A8)         DOSE4325
9052 FORMAT('1',T30,'POPULATION-WEIGHTED CONCENTRATIONS AND POPULATION DOSE4330
    >INTAKES FOR ',A8)                                                 DOSE4335
9053 FORMAT('0',T10,'AREA',T42,'AIR CONCENTRATION',T63,                DOSE4340
    > 'GROUND CONCENTRATION',T89,'INGESTION INTAKE',T114,              DOSE4345
    > 'INHALATION INTAKE')                                             DOSE4350
9054 FORMAT(' ',T41,'(CURIES/CUBIC METER)',T63,'(CURIES/SQUARE METER)',DOSE4355
    > T92,'(PCI/YEAR)',T117,'(PCI/YEAR)')                              DOSE4360
9055 FORMAT(' ',T38,'(MAN-CURIES/CUBIC METER)',T62,                    DOSE4365
    > '(MAN-CURIES/SQUARE METER)',T90,'(MAN-PCI/YEAR)',T115,           DOSE4370
    > '(MAN-PCI/YEAR)')                                                DOSE4375
9056 FORMAT(' ',T3,'DIRECTION',T19,'DISTANCE')                         DOSE4380
9057 FORMAT(' ',T19,'(METERS)')                                        DOSE4385
9058 FORMAT('0')                                                       DOSE4390
9059 FORMAT(' ',T6,I2,T18,I7,T45,E10.3,T68,E10.3,T92,E10.3,T118,E10.3) DOSE4395
9060 FORMAT('0',T10,'DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARTING DOSE4400
    >AT 1 FOR DUE NORTH')                                              DOSE4405
9061 FORMAT(5I10)                                                      DOSE4410
9062 FORMAT(16I5)                                                      DOSE4415
9063 FORMAT(16I5)                                                      DOSE4420
9064 FORMAT(8E10.3)                                                    DOSE4425
9065 FORMAT(8F10.1)                                                    DOSE4430
9066 FORMAT(40I2)                                                      DOSE4435
9067 FORMAT(I10)                                                       DOSE4440
9068 FORMAT(6F10.3)                                                    DOSE4445
9069 FORMAT(6F10.3)                                                    DOSE4450
9070 FORMAT (10F8.4)                                                   DOSE4455
9071 FORMAT('1')                                                       DOSE4460
9072 FORMAT('0')                                                       DOSE4465
9073 FORMAT('0',T48,'SUMMARY OF AREA SURROUNDING PLANT')               DOSE4470
9074 FORMAT('0',T20,'AREA',T40,'NO. MEAT ANIMALS',T60,                 DOSE4475
    > 'NO. MILK CATTLE' ,T80,'FOOD CROPS',T95,'WATER AREA',T113,       DOSE4480
    > 'POPULATION')                                                    DOSE4485
9075 FORMAT(' ',T78,'(SQUARE METERS)')                                 DOSE4490
9076 FORMAT('0',T16,'COLUMN',T26,'ROW')                                DOSE4495
9077 FORMAT(' ',T18,I2,T27,I2,T45,I5,T64,I5,T78,E10.3,T100,I2,T110,    DOSE4500
    > F10.1)                                                           DOSE4505
9078 FORMAT(' ',T20,'FOR WATER AREAS--0= NONE OR MINIMAL AND 1= MAJOR WDOSE4510
    >ATER AREA PRESENT')                                               DOSE4515
9079 FORMAT('1',T36,'LIST OF INPUT VALUES FOR RADIONUCLIDE-INDEPENDENT DOSE4520
    >VARIABLES')                                                       DOSE4525
9080 FORMAT('0',T13,'NUMBER OF NUCLIDES CONSIDERED',T110,I12)          DOSE4530
9081 FORMAT('0',T13,'VEGETABLE INGESTION RATIO-IMMEDIATE SURROUNDING ARDOSE4535
    >EA/TOTAL WITHIN AREA',T110,E12.4)                                 DOSE4540
9082 FORMAT('0',T13,'MEAT INGESTION RATIO-IMMEDIATE SURROUNDING AREA/TODOSE4545
    >TAL WITHIN AREA',T110,E12.4)                                      DOSE4550
9083 FORMAT('0',T13,'MILK INGESTION RATIO-IMMEDIATE SURROUNDING AREA/TODOSE4555
    >TAL WITHIN AREA',T110,E12.4)                                      DOSE4560
9084 FORMAT(' ',T25,'MINIMUM FRACTIONS OF FOOD TYPES FROM OUTSIDE AREA DOSE4565
    >LISTED BELOW ARE ACTUAL FIXED VALUES')                            DOSE4570
9085 FORMAT(' ',T25,'ACTUAL FRACTIONS OF FOOD TYPES FROM OUTSIDE AREA CDOSE4575
    >AN BE GREATER THAN THE MINIMUM FRACTIONS LISTED BELOW')           DOSE4580
9086 FORMAT('0',T13,                                                   DOSE4585
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     > 'MINIMUM FRACTION VEGETABLES INGESTED FROM OUTSIDE AREA',T110,    DOSE4590
     > E12.4)                                                            DOSE4595
9087 FORMAT('0',T13,'MINIMUM FRACTION MEAT INGESTED FROM OUTSIDE AREA',DOSE4600
     >  T110,E12.4)                                                      DOSE4605
9088 FORMAT('0',T13,'MINIMUM FRACTION MILK INGESTED FROM OUTSIDE AREA',DOSE4610
     >  T110,E12.4)                                                      DOSE4615
9089 FORMAT('0',T13,'INHALATION RATE OF MAN (CUBIC CENTIMETERS/HR)',     DOSE4620
     > T110,E12.4)                                                       DOSE4625
9090 FORMAT('0',T13,'BUILDUP TIME FOR RADIONUCLIDES DEPOSITED ON GROUNDDOSE4630
     > AND WATER (DAYS)',T110,E12.4)                                     DOSE4635
9091 FORMAT('0',T13,'DILUTION FACTOR FOR WATER FOR SWIMMING (CM)',T110,DOSE4640
     >  E12.4)                                                           DOSE4645
9092 FORMAT('0',T13,'FRACTION OF TIME SPENT SWIMMING',T110,E12.4)        DOSE4650
9093 FORMAT('0',T13,'MUSCLE MASS OF ANIMAL AT SLAUGHTER (KG)',T110,      DOSE4655
     > E12.4)                                                            DOSE4660
9094 FORMAT('0',T13,'FALLOUT INTERCEPTION FRACTION-VEGETABLES', T110,    DOSE4665
     > E12.4)                                                            DOSE4670
9095 FORMAT('0',T13,'FALLOUT INTERCEPTION FRACTION-PASTURE',T110,E12.4) DOSE4675
9096 FORMAT('0',T13,'FRACTION OF ANIMAL HERD SLAUGHTERED PER DAY',T110,DOSE4680
     >  E12.4)                                                           DOSE4685
9097 FORMAT('0',T13,'MILK PRODUCTION OF COW (LITERS/DAY)',T110,E12.4)   DOSE4690
9098 FORMAT('0',T13,'FRACTION OF RADIOACTIVITY RETAINED ON LEAFY VEGETADOSE4695
     >BLES AND PRODUCE AFTER WASHING',T110,E12.4)                        DOSE4700
9099 FORMAT('1',T51,'COMPUTED VALUES FOR THE AREA')                      DOSE4705
9100 FORMAT('0',T13,'TOTAL POPULATION',T110,F12.1)                       DOSE4710
9101 FORMAT('0',T13,'TOTAL NUMBER OF MEAT ANIMALS',T110,I12)             DOSE4715
9102 FORMAT('0',T13,'TOTAL NUMBER OF MILK CATTLE',T110,I12)              DOSE4720
9103 FORMAT('0',T13,                                                     DOSE4725
     > 'TOTAL AREA OF VEGETABLE FOOD CROPS (SQUARE METERS)',T110,E12.4) DOSE4730
9104 FORMAT('0',T13,'TOTAL MEAT CONSUMPTION (KG PER YEAR)',T110,E12.4)  DOSE4735
9105 FORMAT('0',T13,'TOTAL MEAT PRODUCTION (KG PER YEAR)',T110,E12.4)   DOSE4740
9106 FORMAT('0',T13,'TOTAL MILK CONSUMPTION (LITERS/YEAR)',T110,E12.4)  DOSE4745
9107 FORMAT('0',T13,'TOTAL MILK PRODUCTION (LITERS/YEAR)',T110,E12.4)   DOSE4750
9108 FORMAT('0',T13,'TOTAL VEGETABLE FOOD CONSUMPTION (KG PER YEAR)',    DOSE4755
     > T110,E12.4)                                                       DOSE4760
9109 FORMAT('0',T13,'TOTAL VEGETABLE FOOD PRODUCED (KG PER YEAR)',T110,DOSE4765
     >  E12.4)                                                           DOSE4770
9110 FORMAT(I10,4E10.3,I10,2E10.3)                                       DOSE4775
9111 FORMAT(11F5.3)                                                      DOSE4780
9112 FORMAT (2E10.3,I1,6F8.4)                                            DOSE4785
9113 FORMAT('1',T42,'RESULTS OF DOSE COMPUTATIONS FOR NUCLIDE ',A8)      DOSE4790
9114 FORMAT('0',T15,'AREA',T26,'ORGAN',T60,                              DOSE4795
     > 'DOSE THROUGH EACH PATHWAY (REMS/YEAR)')                          DOSE4800
9115 FORMAT('0',T11,'COLUMN',T20,'ROW')                                  DOSE4805
9116 FORMAT('0',T40,'INHALATION',T55,'SUBMERSION',T70,'SURFACE',T85,     DOSE4810
     > 'INGESTION',T100,'SUBMERSION',T117,'TOTAL')                       DOSE4815
9117 FORMAT(' ',T57,'IN AIR',T69,'EXPOSURE',T102,'IN WATER')             DOSE4820
9118 FORMAT(' ',T13,I2,T20,I2,T25,A8,T40,E10.3,T55,E10.3,T70,E10.3,T85,DOSE4825
     >  E10.3,T100,E10.3,T115,E10.3)                                     DOSE4830
9119 FORMAT('1',T47,'LIST OF INPUT DATA FOR NUCLIDE ',A8)                DOSE4835
9120 FORMAT('0',T13,'FLAG ERROR')                                        DOSE4840
9121 FORMAT('0',T13,'FALLOUT INTERCEPTION FRACTION-VEGETABLES', T110,    DOSE4845
     > E12.4)                                                            DOSE4850
9122 FORMAT('0',T13,'FALLOUT INTERCEPTION FRACTION-PASTURE',T110,E12.4) DOSE4855
9123 FORMAT ('0',T13, 'FALLOUT INTERCEPTION FRACTION(DRY)-VEGETABLES',   DOSE4860
     > T110, E12.4)                                                      DOSE4865
9124 FORMAT ('0',T13, 'FALLOUT INTERCEPTION FRACTION(WET)-VEGETABLES',   DOSE4870
     > T110, E12.4)                                                      DOSE4875
```

```
9125 FORMAT('0',T13,'FALLOUT INTERCEPTION FRACTION(DRY)-PASTURE', T110,
    > E12.4)
9126 FORMAT('0',T13,'FALLOUT INTERCEPTION FRACTION(WET)-PASTURE', T110,
    > E12.4)
9127 FORMAT('0',T13,'RADIOACTIVE DECAY CONSTANT (PER DAY)',T110,E12.4)
9128 FORMAT('0',T25,'RADIOACTIVE DECAY FOR SURFACE EXPOSURE AND FOR WAT
    >ER IMMERSION PROCEEDS IN ACCORDANCE WITH THE')
9129 FORMAT(' ',T25,'EFFECTIVE DECAY CONSTANT IN THE PLUME INSTEAD OF T
    >HE ABOVE VALUE')
9130 FORMAT('0',T13,'ENVIRONMENTAL DECAY CONSTANT--SURFACE (PER DAY)',
    > T110,E12.4)
9131 FORMAT('0',T13,'ENVIRONMENTAL DECAY CONSTANT--WATER (PER DAY)',
    > T110,E12.4)
9132 FORMAT('0',T13,'DOSE CONVERSION FACTOR FOR FOOD INGESTION (REM-CC/
    >PCI-YEAR)',T110,E12.4)
9133 FORMAT('0',T13,'DOSE CONVERSION FACTOR FOR WATER INGESTION (REM-CC
    >/PCI-YEAR)',T110,E12.4)
9134 FORMAT('0',T55,'DOSE CONVERSION FACTORS')
9135 FORMAT('0',T5,'ORGAN',T20,'INHALATION',T38,'INGESTION',T58,
    > 'SUBMERSION IN AIR',T83,'SURFACE EXPOSURE',T107,
    > 'SUBMERSION IN WATER')
9136 FORMAT(' ',T17,'(REMS/MICROCURIE)',T34,'(REMS/MICROCURIE)',T59,
    > '(REMS-CUBIC CM/',T83,'(REMS-SQUARE CM/',T109,'(REMS-CUBIC CM/')
9137 FORMAT(' ',T60,'MICROCURIE-HR)',T84,'MICROCURIE-HR)',T110,
    > 'MICROCURIE-HR)')
9138 FORMAT(' ',T4,A8,T21,E10.3,T38,E10.3,T61,E10.3,T86,E10.3,T111,
    > E10.3)
9139 FORMAT(A8)
9140 FORMAT(6E10.4)
     END
```

```
      FUNCTION CV(I,LAMI,DEPRAT,GCRU,TSUBE,YSUBV,TSUBH,R)               CV
C CALCULATES THE CONCENTRATION OF NUCLIDE I IN AND ON VEGETATION USING  CV
C EQ C-5, REG GUIDE 1.109-25. THE INPUT PARAMETERS ARE DEFINED AS FOLLOWCV
C                                                                       CV
C     I         INDEXES NUCLIDE                                         CV
C     LAMI      RADIOACTIVE DECAY CONSTANT FOR THE NUCLIDE  (HR**-1)    CV
C     DEPRAT    DEPOSITION RATE OF RADIONUCLIDE I ONTO GROUND           CV
C               AT THE GIVEN LOCATION ( PCI /M**2-HR)                   CV
C     TSUBE     PERIOD OF CROP, LEAFY VEGETABLE, OR PASTURE GRASS EXPOSUCV
C               DURING GROWING SEASON (HR)                              CV
C     YSUBV     AGRICULTURAL PRODUCTIVITY BY UNIT AREA (MEASURED IN WET CV
C               WEIGHT)  (KG/M**2)                                      CV
C     TSUBH     TIME DELAY BETWEEN HARVEST OF VEGETATION OR CROPS AND   CV
C               INGESTION (HR)                                          CV
C     R         FRACTION OF DEPOSITED ACTIVITY RETAINED                 CV
C               ON CROPS, DIMENSIONLESS                                 CV
C                                                                       CV
      REAL LAMEI,LAMI,LAMRR,LAMW                                        CV
      COMMON /INGDOS/LAMW,TSUBB,P,BSUBV,DR,RATUA                        CV
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD,ACON(36,20, CV
     > 20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11),ORMODI(36,12,8), CV
     > VD(36),VDCOEF(20,20),NOL,NOU,NRL,NRU                             CV
      REAL*8 NAMNUC,WORD                                                CV
C THE EFFECTIVE REMOVAL RATE CONSTANT FOR THE RADIONUCLIDE FROM CROPS   CV
C IN HR**-1 IS  (REG GUIDE 1.109-4)                                     CV
      LAMEI = LAMI + LAMW                                               CV
C WHERE LAMW IS THE REMOVAL RATE CONSTANT FOR WEATHERING.               CV
C                                                                       CV
C THE FOLLOWING CODE CALCULATES CV= CONCENTRATION OF NUCLIDE I USING EQ CV
      STUBB=TSUBB*8760.                                                 CV
      ALT=LAMEI*TSUBE                                                   CV
      IF (ALT.GT.0.03) GO TO 10                                         CV
      XNUD1=(R*DR/YSUBV)*((0.1666667*ALT-0.5)*ALT+TSUBE)                CV
      GO TO 20                                                          CV
   10 XNUD1=(R*DR/YSUBV)*((1.0-EXP(-LAMEI*TSUBE))/LAMEI)                CV
   20 CONTINUE                                                          CV
      ALT=LAMI*STUBB                                                    CV
      IF (ALT.GT.0.03) GO TO 30                                         CV
      XNUD2=(BSUBV/P)*((0.1666667*ALT-0.5)*ALT+STUBB)                   CV
      GO TO 40                                                          CV
   30 XNUD2=(BSUBV/P)*((1.0-EXP(-LAMI*STUBB))/LAMI)                     CV
   40 CONTINUE                                                          CV
      SUM=XNUD1+XNUD2                                                   CV
      PROD=SUM*EXP(-LAMI*TSUBH)                                         CV
      SUM2=XNUD2                                                        CV
      PROD2=SUM2*EXP(-LAMI*TSUBH)                                       CV
      RATUA=SUM2/SUM                                                    CV
      CV = GCRU * PROD + (DEPRAT-GCRU)*PROD2                            CV
      RETURN                                                            CV
      END                                                               CV
```

```
      SUBROUTINE RVALUE (IFLAG,MODE,I,NO,NR,R)
      COMMON /RVAL/ S1,S3,SD1,SD3,ACN,GCN,SW1,SW3
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD,ACON(36,20,
     > 20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11),ORMODI(36,12,8),
     > VD(36),VDCOEF(20,20),NOL,NOU,NRL,NRU
      REAL*8 NAMNUC,WORD
C THIS SUBROUTINE ASSIGNS A VALUE TO THE PARAMETER
C     R = THE FRACTION OF DEPOSITED ACTIVITY RETAINED ON CROPS (DIMENSION
C AS FOLLOWS..
C (1)  IF THE VALUES USED FOR S1 AND S3 ARE NOT NUCLIDE-SPECIFIC (NORMAL
C      IFLAG=0), THEN
C             R = S1 FOR VEGETABLES (MODE=1)
C             R = S3 FOR PASTURE    (MODE=2)
C (2)  IF VALUES FOR S1 AND S3 ARE NUCLIDE-SPECIFIC, AND DEPOSITION RATES
C      ARE NOT SPECIFIED SEPARATELY FOR WET AND DRY DEPOSITION (SPECIAL R
C      IFLAG=1), THEN
C             R = SD1 FOR VEGETABLES (MODE=1)
C             R = SD3 FOR PASTURE    (MODE=2)
C (3)  IF VALUES FOR S1 AND S3 ARE NUCLIDE-SPECIFIC, AND DEPOSITION RATES
C      ARE SPECIFIED SEPARATELY FOR WET AND DRY DEPOSITION (IFLAG=2), THE
C      R IS CALCULATED BY AVERAGING DRY AND WET DEPOSITION RATES AS FOLLO
C
C      R =(SD1*DRY DEP RATE  +  SW1*WET DEP RATE) /(DRY DEP RATE+WET DEP
C    FOR VEGETABLES (MODE = 1).
C
C R=(SD3*DRY DEP RATE + SW3*WET DEP RATE)/ (DRY DEP RATE + WET DEP RATE)
C    FOR PASTURE (MODE = 2)
      IF (IFLAG.EQ.0.AND.MODE.EQ.1) R=S1
      IF (IFLAG.EQ.0.AND.MODE.EQ.2) R=S3
      IF (IFLAG.EQ.1.AND.MODE.EQ.1) R=SD1
      IF (IFLAG.EQ.1.AND.MODE.EQ.2) R=SD3
C CALCULATE DRY AND WET DEPOSITION RATES.
      DRYDEP = ACN*VD(I)*VDCOEF(NO,NR)
      WETDEP = GCN - DRYDEP
C THE SUM OF THESE DEPOSITION RATES IS GIVEN BY GCN.
      IF (IFLAG.EQ.2.AND.MODE.EQ.1) R=  (SD1*DRYDEP+SW1*WETDEP)/ GCN
      IF (IFLAG.EQ.2.AND.MODE.EQ.2) R=  (SD3*DRYDEP+SW3*WETDEP)/ GCN
C PRINT ERROR MESSAGE IF NONE OF THESE CONDITIONS IS MET.
      IF (MODE.NE.1.AND.MODE.NE.2) WRITE(51,9000)
      IF (IFLAG.NE.0.AND.IFLAG.NE.1.AND.IFLAG.NE.2) WRITE(51,9001)
      RETURN
 9000 FORMAT('0ERROR.. MODE SHOULD BE 1 OR 2 IN SUBROUTINE RVALUE')
 9001 FORMAT('0ERROR.. IFLAG SHOULD BE 0,1,OR 2 IN SUBROUTINE RVALUE')
      END
```

```
      SUBROUTINE DOSMIC(NNTB,NUTB)
C
      COMMON /OCOM/ NAMNUC(36),WORD,NNUCS,ANLAM(36),RR,SQSD, ACON(36,20,
     >  20),GCON(36,20,20),LIPO,NOMM(36,11),NRMM(36,11), ORMODI(36,12,8)
     > , VD(36),VDCOEF(20,20),NOL,NOU,NRL,NRU
      COMMON NOML(11),NRML(11)
      COMMON /PCOM/ REL(6,36),IDIST(20),NUMST
      COMMON /FCOM/ FEQWL,INTPA(20,20)
      REAL INTPA
      DIMENSION DOSE(12),PTIJ(36,11),TOTJM(11,8),PTOJM(11,8),TOTJ(11),
     > TIJ(36,11),PCT(8),WL(20,20)
      REAL*8 NAMNUC,MODE(8),NAMES(11),WORD,FLAG(8)
      REAL*8 NADRN
      DATA NADRN/'RN-222  '/
      DATA FLAG/' ',' ',' ',' ',' ','*','*','*'/
      DATA NAMES/'TOT.BODY','R MAR   ','LUNGS   ','ENDOST  ','S WALL  ',
     > 'LLI WALL','THYROID ','LIVER   ','KIDNEYS ','TESTES  ',
     > 'OVARIES '/
      DATA MODE/'SUBM AIR','SURFACE ','SWIMMING','INHAL.  ','INGEST. ',
     > '  VEGET.','  MEAT  ','  MILK  '/
C           INITIALIZE
      IF (NTTB.EQ.0) GO TO 470
      DO 20 J=1,11
         DO 10 MD=1,8
   10       TOTJM(J,MD)=0
   20    CONTINUE
      DO 30 J=1,11
   30    TOTJ(J)=0
      DO 50 I=1,36
         DO 40 J=1,11
   40       TIJ(I,J)=0
   50    CONTINUE
      DO 70 I=1,NNUCS
         DO 60 J=1,11
            ORM=ORMODI(I,J,1)
            ORMODI(I,J,1)=ORMODI(I,J,2)
            ORMODI(I,J,2)=ORMODI(I,J,3)
            ORMODI(I,J,3)=ORMODI(I,J,5)
            ORMODI(I,J,5)=ORMODI(I,J,4)
            ORMODI(I,J,4)=ORM
   60       CONTINUE
   70    CONTINUE
      DO 100 I=1,NNUCS
         IF (NAMNUC(I).NE.NADRN.OR.NUTB.EQ.0) GO TO 100
         DO 90 MD=1,5
            DO 80 J=1,12
               ORMODI(I,J,MD)=0
   80          CONTINUE
   90       CONTINUE
         GO TO 110
  100    CONTINUE
  110 CONTINUE
  120 DO 150 J=1,11
         DO 140 MD=1,8
            DO 130 I=1,NNUCS
  130          TOTJM(J,MD)=ORMODI(I,J,MD)+TOTJM(J,MD)
```

```
140          CONTINUE
150       CONTINUE
       DO 170 J=1,11
          DO 160 MD=1,8
160          IF (TOTJM(J,MD).LT.1.E-40) TOTJM(J,MD)=1.E-40
170       CONTINUE
       DO 190 J=1,11
          DO 180 MD=1,5
180          TOTJ(J)=TOTJM(J,MD)+TOTJ(J)
190       CONTINUE
       DO 220 J=1,11
          DO 200 MD=1,5
200          PTOJM(J,MD)=TOTJM(J,MD)/TOTJ(J)*100.
          DO 210 MD=6,8
210          PTOJM(J,MD)=TCTJM(J,5)/TOTJ(J)*100.0*TOTJM(J,MD)/TOTJM(J,5)
220       CONTINUE
       DO 300 J=1,11
          WRITE(51,9000)NAMES(J)
          IF (LIPO.EQ.1) GO TO 230
          WRITE(51,9001)
          GO TO 240
230       WRITE(51,9002)
240       WRITE(51,9003)
          DO 290 I=1,NNUCS
             SUMA=0
             DO 250 MD=1,5
250             SUMA=ORMODI(I,J,MD)+SUMA
             IF (SUMA.LT.1.E-40) SUMA=1.E-40
             DO 260 MD=1,5
260             PCT(MD)=(ORMODI(I,J,MD)/SUMA)*100.
             MD=1
             PTOT=ORMODI(I,J,MD)/TOTJM(J,MD)*100.
             WRITE(51,9C05)NAMNUC(I),MODE(MD),ORMODI(I,J,MD),PCT(MD),PTOT
             DO 270 MD=2,5
                PTOT=ORMODI(I,J,MD)/TOTJM(J,MD)*100.
270             WRITE(51,9004)MODE(MD),ORMODI(I,J,MD),PCT(MD),PTOT
             DC 280 MD=6,8
                IF (ORMODI(I,J,5).EQ.0.) PCT(MD)=0.
                IF (ORMODI(I,J,5).EQ.0.) PTOT=0.
                IF (ORMODI(I,J,5).EQ.0.) GO TO 280
                PCT(MD)=ORMODI(I,J,MD)/ORMODI(I,J,5)*PCT(5)
                PTOT=ORMODI(I,J,MD)/TOTJM(J,5)*100.
280             WRITE(51,9006) MODE(MD),ORMODI(I,J,MD),FLAG(MD),PCT(MD),
    >            FLAG(MD),PTOT
290          CONTINUE
300       CONTINUE
       DO 340 J=1,11
          WRITE(51,9007)NAMES(J)
          IF (LIPO.EQ.1) GO TO 310
          WRITE(51,9008)
          GO TO 320
310       WRITE(51,9009)
320       DO 330 MD=1,8
             IF (TOTJM(J,MD).LE.1.E-40) TOTJM(J,MD)=0.
             WRITE(51,9010)MODE(MD),FLAG(MD),TOTJM(J,MD),FLAG(MD),
    >         PTOJM(J,MD)
330          CONTINUE
340       CONTINUE
```

```
      WRITE(51,9011)
      IF (LIPO.EQ.1) GO TO 350
      WRITE(51,9012)
      GO TO 360
  350 WRITE(51,9013)
  360 DO 370 J=1,11
  370    WRITE(51,9014) NAMES(J),TOTJ(J)
      DO 400 I=1,NNUCS
         DO 390 J=1,11
            DO 380 MD=1,5
               TIJ(I,J)=ORMODI(I,J,MD)+TIJ(I,J)
  380          PTIJ(I,J)=TIJ(I,J)/TOTJ(J)*100.
  390       CONTINUE
  400    CONTINUE
      WRITE(51,9015)
      WRITE(51,9016)
      WRITE(51,9017) (NAMES(J),J=1,11)
      WRITE(51,9019)
      DO 410 I=1,NNUCS
         WRITE(51,9018) NAMNUC(I),(PTIJ(I,J),J=1,11)
  410    CONTINUE
      IF (LIPO.EQ.1) GO TO 440
      WRITE(51,9020)
      WRITE(51,9021)
      WRITE(51,9022)
      DO 430 I=1,NNUCS
         DO 420 J=1,11
            WRITE(51,9023) NAMNUC(I),NAMES(J),TIJ(I,J),NOML(J),NRML(J)
  420       CONTINUE
  430    CONTINUE
      GO TO 470
  440 WRITE(51,9024)
      WRITE(51,9025)
      DO 460 I=1,NNUCS
         DO 450 J=1,11
            WRITE(51,9026) NAMNUC(I),NAMES(J),TIJ(I,J)
  450       CONTINUE
  460    CONTINUE
  470 CONTINUE
      IF (NUTB.EQ.0) GO TO 570
      DO 480 I=1,NNUCS
         IF (NAMNUC(I).EQ.NADRN) GO TO 490
  480    CONTINUE
      GO TO 570
  490 CONTINUE
      ALI=LIPO
      CWL=0
      DO 510 NO=NOL,NOU
         DO 500 NR=NRL,NRU
            IF (FEQWL.EQ.0.) FEQWL=0.7
            WL(NO,NR)=FEQWL*10.*ACON(I,NO,NR)*(ALI*(INTPA(NC,NR)-1.)+1.)
            CWL=CWL+WL(NO,NR)
  500       CONTINUE
  510    CONTINUE
      WRITE(51,9027)
      WRITE(51,9038) FEQWL
      WRITE(51,9003)
      WRITE(51,9028)
```

```
      IF(LIPO.EQ.1) WRITE(51,9040)                                      DOSM 826
      WRITE(51,9019)                                                    DOSM 830
      IF (LORT.EQ.0) GO TO 520                                          DOSM 835
      WRITE(51,9029)                                                    DOSM 840
      WRITE(51,9030)                                                    DOSM 845
      WRITE(51,9003)                                                    DOSM 850
      GC TO 530                                                         DOSM 855
  520 WRITE(51,9031)                                                    DOSM 860
      WRITE(51,9003)                                                    DOSM 865
  530 CONTINUE                                                          DOSM 870
      IF (LORT.EQ.0) GO TO 540                                          DOSM 875
      WRITE(51,9032)(((NO,IDIST(NR),WL(NO,NR)),NR=NRL,NRU),NO=NOL,NOU)  DOSM 880
      GC TO 550                                                         DOSM 885
  540 WRITE(51,9033)(((NO,NR,WL(NC,NR)),NR=NRL,NRU),NO=NOL,NOU)         DOSM 890
  550 CCNTINUE                                                          DOSM 895
  560 CONTINUE                                                          DOSM 900
      IF (LIPO.EQ.1) GO TO 569                                          DOSM 905
      WRITE(51,9034)                                                    DOSM 910
      WRITE(51,9035)                                                    DOSM 915
      WRITE(51,9036)                                                    DOSM 920
      WRITE(51,9019)                                                    DOSM 925
      WRITE(51,9037)((NAMES(J),NOML(J),NRML(J),WL(NCML(J),NRML(J))), J= DOSM 930
     > 1,11)                                                            DOSM 935
 569  IF(LIPO.EQ.1) WRITE(51,9039)CWL                                   DOSM 939
  570 CCNTINUE                                                          DOSM 940
      RETURN                                                            DOSM 945
 9000 FORMAT('1',T36,'PERCENT OF ',A8,' DOSE BY EACH PATHWAY')          DOSM 950
 9001 FORMAT('0',T20,'NUCLIDE',T35,'PATHWAY',T52,'DOSE(REMS)', T70,     DOSM 955
     > 'PERCENT OF TOTAL',T90,'PERCENT OF DOSE FROM ALL NUCLIDES')      DOSM 960
 9002 FORMAT('0',T20,'NUCLIDE',T35,'PATHWAY',T50,'DOSE(MAN-REMS)', T70, DOSM 965
     > 'PERCENT OF TOTAL',T90,'PERCENT CF DOSE FROM ALL NUCLIDES')      DOSM 970
 9003 FCRMAT('0')                                                       DOSM 975
 9004 FORMAT(' ',T35,A8,T52,E10.4,T75,F6.2,T103,F6.2)                   DOSM 980
 9005 FORMAT(' ',T20,A8,T35,A8,T52,E10.4,T75,F6.2,T103,F6.2)            DOSM 985
 9006 FORMAT(' ',T35,A8,T52,E10.4,T74,A1,F6.2,T102,A1,F6.2)             DOSM 990
 9007 FORMAT('0',T41,'CONTRIBUTION OF EXPOSURE MODES TO ',A8,' DOSES')  DOSM 995
 9008 FCRMAT('0',T10,'EXPOSURE MODE',T57,'ANNUAL DOSE(REMS)',T99,       DOSM1000
     > 'PERCENT OF TOTAL COSE')                                         DOSM1005
 9009 FORMAT('0',T10,'EXPOSURE MODE',T55,'ANNUAL DCSE(MAN-REMS)',T99,   DOSM1010
     > 'PERCENT OF TOTAL DOSE')                                         DOSM1015
 9010 FORMAT('0',T12,A8,T58,A1,E10.4,T103,A1,F10.4)                     DOSM1020
 9011 FCRMAT('1',T43,'TOTAL DOSE TO EACH ORGAN THROUGH ALL PATHWAYS')   DOSM1025
 9012 FCRMAT('0',T38,'ORGAN',T83,'DOSE(REMS)')                          DOSM1030
 9013 FORMAT('0',T38,'ORGAN',T81,'DOSE(MAN-REMS)')                      DOSM1035
 9014 FORMAT('0',T37,A8,T83,E10.4)                                      DOSM1040
 9015 FORMAT('1',T52,'CONTRIBUTORS TO ORGAN DOSES')                     DOSM1045
 9016 FCRMAT('0',T80,'PERCENT')                                         DOSM1050
 9017 FORMAT('0',T2,'NUCLIDE',1X,11A11)                                 DOSM1055
 9018 FORMAT(' ',T2,A8,11F11.4)                                         DOSM1060
 9019 FORMAT(' ')                                                       DOSM1065
 9020 FORMAT('1',T56,'ANNUAL DOSES(REMS)')                              DOSM1070
 9021 FORMAT('0',T20,'NUCLIDE',T40,'ORGAN',T60,'DOSE',T100,             DOSM1075
     > 'MAXIMUM LOCATION')                                              DOSM1080
 9022 FORMAT('0',T101,'COIUMN',T112,'ROW')                              DOSM1085
 9023 FORMAT('0',T21,A8,T39,A8,T58,E10.4,T103,I2,T113,I2)               DOSM1090
 9024 FORMAT('1',T48,'ANNUAL POPULATION DOSES(MAN-REMS)')               DOSM1095
 9025 FCRMAT('0',T38,'NUCLIDE',T62,'ORGAN',T85,'DOSE')                  DOSM1100
 9026 FORMAT('0',T39,A8,T61,A8,T83,E10.4)                               DOSM1105
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9027 FORMAT('1',T21,'WORKING LEVELS FOR RN-222 AND ITS SHORT-LIFE PROGEDOSM1110
    >NY AT VARIOUS LOCATIONS IN THE ENVIRONMENT')                      DOSM1115
9028 FORMAT(' ',T40,'AREA',T86,'WORKING LEVEL')                        DOSM1120
9029 FORMAT(' ',T32,'WIND TOWARD',T47,'DISTANCE')                      DOSM1125
9030 FORMAT(' ',T47,'(METERS)')                                        DOSM1130
9031 FORMAT(' ',T33,'COLUMN',T47,'ROW')                                DOSM1135
9032 FORMAT(' ',T36,I2,T47,I7,T87,E10.3)                               DOSM1140
9033 FORMAT(' ',T35,I2,T47,I2,T87,E10.3)                               DOSM1145
9034 FORMAT('1',T32,'WORKING LEVEL FOR RN-222 AND SHORT-LIFE PROGENY ATDOSM1150
    > LOCATION OF MAXIMUM')                                            DOSM1155
9035 FORMAT(' ',T43,'INDIVIDUAL DOSE FROM ALL PATHWAYS FOR EACH ORGAN')DOSM1160
9036 FORMAT('0',T35,'ORGAN',T56,'LOCATION OF MAXIMUM DOSE',T91,        DOSM1165
    > 'WORKING LEVEL')                                                 DOSM1170
9037 FORMAT(' ',T34,A8,T63,I2,T71,I2,T93,E10.3)                        DOSM1175
9038 FORMAT(' ',T32,'(FRACTION OF EQUILIBRIUM ASSUMED FOR WORKING LEVELDOSM1180
    > CALCULATIONS=',F5.3,')')                                         DOSM1185
9039 FORMAT('0',T32,'COLLECTIVE WORKING LEVEL= ',E10.3)                DOSM1190
9040 FORMAT(' ',T86,'(POPULATION)')                                    DOSM1195
     END                                                               DOSM1200
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Appendix B

OUTPUT OF AN EXAMPLE CASE RUN OF THE AIRDOS—EPA CODE

The example case is for a hypothetical atmospheric release of four radionuclides (^{226}Ra, ^{210}Po, ^{222}Rn, and ^{3}H) near ground level (1 m elevation) from a circular area source 1000 m in diameter. The meteorology and population distribution are representative of a western site in the U.S.

A period of 100 years was assumed for the buildup of radionuclides on ground surfaces resulting from aerial deposition. The buildup of two of the daughters of ^{226}Ra (^{210}Pb and ^{210}Po) on ground surface is calculated for this period.

The example run computes annual population doses (man-rem) within a radius of 88514 m (55 miles). Population-weighted concentrations in air and on ground surfaces, and population intake rates by ingestion and inhalation within this radius are also computed for each radionuclide at 11 distances away from the source in each of 16 compass directions. Working levels for ^{222}Rn are computed for each of these environmental locations.

Dose conversion factors for the external exposure modes used in the example run are from D. C. Kocher (1979). The internal dose conversion factors (inhalation and ingestion) are for 50-year dose commitments (Killough et al., 1978).

OUTPUT OF AIRDOS-EPA COMPUTER CODE

OPTIONS SELECTED--

RADIONUCLIDE CONCENTRATIONS ARE LISTED FOR DIRECTION AND DISTANCE FROM FACILITY

RADIONUCLIDE CONCENTRATIONS LISTED ARE SECTOR-AVERAGED VALUES
THE CALCULATIONS ARE MADE FOR A UNIFORM CIRCULAR AREA SOURCE
SPECIFIC PLUME RISE USED FOR EACH AIR STABILITY CLASS (METERS)-

```
A        0.0   B        0.0   C        0.0   D        0.0   E        0.0   F        0.0   G        0.0
```

METEOROLOGICAL AND PLANT INFORMATION SUPPLIED TO PROGRAM----

AVERAGE AIR TEMPERATURE (DEG K)	294.0
AVERAGE VERTICAL TEMPERATURE GRADIENT OF THE AIR (DEG K/METER)	
IN STABILITY CLASS E	0.0728
IN STABILITY CLASS F	0.1090
IN STABILITY CLASS G	0.1455
RAINFALL RATE (CM/YEAR)	20.32
HEIGHT OF LID (METERS)	2000
NUMBER OF STACKS IN THE PLANT	1

STACK INFORMATION--

	STACK NUMBER					
	1	2	3	4	5	6
HEIGHT (METERS)	1.0000					
DIAMETER (METERS)	0.0					
EFFLUENT VELOCITY (METERS/SEC)	0.0					
RATE OF HEAT EMISSION (CAL/SECOND)	0.0					
DIAMETER OF AREA SOURCE (METERS)	1000.0000					

RELEASE RATES FOR RADIONUCLIDES

STACK	NUCLIDE	RELEASE RATE (CURIES/YEAR)
1	RA-226	0.100E-01
1	PB-210	0.0
1	PO-210	0.200E-01
1	RN-222	0.100E 01
1	H-3	0.100E 01

PLUME DEPLETION AND DEPOSITION PARAMETERS

NUCLIDE	GRAVITATIONAL FALL VELOCITY (METERS/SEC)	DEPOSITION VELOCITY (METERS/SEC)	SCAVENGING COEFFICIENT (1/SEC)	EFFECTIVE DECAY CONSTANT IN PLUME (PER DAY)
RA-226	0.0	0.01000	0.460E-05	0.119E-05
PB-210	0.0	0.01000	0.460E-05	0.852E-04
PO-210	0.0	0.01000	0.460E-05	0.502E-02
RN-222	0.0	0.0	0.0	0.181E 00
H-3	0.0	0.0	0.0	0.154E-03

FREQUENCY OF ATMOSPHERIC STABILITY CLASSES FOR EACH DIRECTION

SECTOR	FRACTION OF TIME IN EACH STABILITY CLASS						
	A	B	C	D	E	F	G
1	0.0266	0.1531	0.1764	0.2935	0.1167	0.2337	0.0
2	0.0173	0.1026	0.1137	0.1939	0.1629	0.4096	0.0
3	0.0150	0.0710	0.0721	0.1817	0.1754	0.4848	0.0
4	0.0120	0.0420	0.0442	0.4096	0.1356	0.3566	0.0
5	0.0092	0.0460	0.0369	0.5786	0.0867	0.2426	0.0
6	0.0218	0.1033	0.0614	0.2902	0.1291	0.3942	0.0
7	0.0256	0.1180	0.0764	0.1654	0.1370	0.4776	0.0
8	0.0089	0.1101	0.1003	0.1727	0.2399	0.3682	0.0
9	0.0159	0.0889	0.1203	0.2928	0.2153	0.2667	0.0
10	0.0155	0.1335	0.1613	0.2935	0.1447	0.2514	0.0
11	0.0326	0.1855	0.1526	0.3277	0.1003	0.2013	0.0
12	0.0427	0.2116	0.1474	0.3271	0.0900	0.1812	0.0
13	0.0527	0.2398	0.1703	0.3032	0.0823	0.1517	0.0
14	0.0444	0.2267	0.1727	0.3226	0.0891	0.1444	0.0
15	0.0409	0.2368	0.2057	0.2873	0.0897	0.1397	0.0
16	0.0308	0.1856	0.2092	0.3364	0.1073	0.1308	0.0

FREQUENCIES OF WIND DIRECTIONS AND RECIPROCAL-AVERAGED WIND SPEEDS

WIND TOWARD	FREQUENCY	WIND SPEEDS FOR EACH STABILITY CLASS (METERS/SEC)						
		A	B	C	D	E	F	G
1	0.091	1.30	1.37	2.45	4.00	3.27	1.13	0.0
2	0.054	1.26	1.24	2.14	3.30	3.14	1.26	0.0
3	0.083	1.00	1.11	1.80	3.40	3.08	1.27	0.0
4	0.081	1.10	1.02	1.91	5.53	3.23	1.23	0.0
5	0.053	1.00	1.03	2.18	6.11	3.37	1.11	0.0
6	0.027	0.98	1.08	1.61	3.98	3.27	1.08	0.0
7	0.040	0.97	1.05	1.92	2.84	3.31	1.16	0.0
8	0.048	1.31	1.19	2.11	3.16	3.64	1.27	0.0
9	0.129	1.19	1.14	2.43	4.01	3.81	1.33	0.0
10	0.064	1.28	1.23	2.49	4.15	3.55	1.31	0.0
11	0.056	1.29	1.23	2.29	4.27	3.50	1.18	0.0
12	0.053	1.28	1.34	2.52	4.56	3.30	1.11	0.0
13	0.048	1.19	1.40	2.48	4.72	3.21	1.10	0.0
14	0.053	1.27	1.58	2.89	4.51	3.26	1.14	0.0
15	0.064	1.32	1.48	2.80	3.96	3.28	1.08	0.0
16	0.055	1.22	1.64	2.94	4.99	3.33	1.14	0.0

WIND DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARTING AT 1 FOR DUE NORTH

FREQUENCIES OF WIND DIRECTIONS AND TRUE-AVERAGE WIND SPEEDS

WIND TOWARD	FREQUENCY	WIND SPEEDS FOR EACH STABILITY CLASS (METERS/SEC)						
		A	B	C	D	E	F	G
1	0.091	1.82	2.22	3.59	5.70	3.51	1.58	0.0
2	0.054	1.78	1.96	3.19	4.64	3.37	1.77	0.0
3	0.083	1.36	1.72	2.79	5.17	3.30	1.78	0.0
4	0.081	1.53	1.52	3.24	7.11	3.47	1.73	0.0
5	0.053	1.36	1.48	3.62	7.66	3.61	1.55	0.0
6	0.027	1.32	1.64	2.74	5.96	3.50	1.50	0.0
7	0.040	1.29	1.56	2.84	4.12	3.55	1.64	0.0
8	0.048	1.83	1.83	2.90	4.46	3.86	1.78	0.0
9	0.129	1.67	1.78	3.28	5.36	4.00	1.86	0.0
10	0.064	1.80	1.84	3.30	5.61	3.78	1.83	0.0
11	0.056	1.81	1.93	3.33	6.33	3.73	1.66	0.0
12	0.053	1.79	2.10	3.63	6.52	3.54	1.57	0.0
13	0.048	1.68	2.20	3.71	6.32	3.44	1.54	0.0
14	0.053	1.78	2.46	3.95	6.02	3.50	1.60	0.0
15	0.064	1.84	2.37	3.92	5.69	3.52	1.51	0.0
16	0.055	1.72	2.52	4.03	6.12	3.57	1.61	0.0

WIND DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARTING AT 1 FOR DUE NORTH

ESTIMATED RADIONUCLIDE CONCENTRATIONS

AREA WIND TOWARD	DISTANCE (METERS)	NUCLIDE	AIR CONCENTRATION (PCI/CC)	DRY DEPOSITION RATE (PCI/SQUARE CM-SEC)	WET DEPOSITION RATE (PCI/SQUARE CM-SEC)	GROUND DEPOSITION RATE (PCI/SQUARE CM-SEC)
1	1207	RA-226	0.292E-09	0.292E-09	0.671E-11	0.299E-09
1	1207	PB-210	0.0	0.0	0.0	0.0
1	1207	PO-210	0.584E-09	0.584E-09	0.134E-10	0.598E-09
1	1207	RN-222	0.767E-07	0.0	0.0	0.0
1	1207	H-3	0.769E-07	0.0	0.0	0.0
1	2414	RA-226	0.862E-10	0.862E-10	0.377E-11	0.900E-10
1	2414	PB-210	0.0	0.0	0.0	0.0
1	2414	PO-210	0.172E-09	0.172E-09	0.753E-11	0.180E-09
1	2414	RN-222	0.291E-07	0.0	0.0	0.0
1	2414	H-3	0.292E-07	0.0	0.0	0.0
1	4023	RA-226	0.310E-10	0.310E-10	0.207E-11	0.330E-10
1	4023	PB-210	0.0	0.0	0.0	0.0
1	4023	PO-210	0.619E-10	0.619E-10	0.415E-11	0.661E-10
1	4023	RN-222	0.134E-07	0.0	0.0	0.0
1	4023	H-3	0.134E-07	0.0	0.0	0.0
1	5632	RA-226	0.165E-10	0.165E-10	0.142E-11	0.180E-10
1	5632	PB-210	0.0	0.0	0.0	0.0
1	5632	PO-210	0.331E-10	0.331E-10	0.283E-11	0.359E-10
1	5632	RN-222	0.827E-08	0.0	0.0	0.0
1	5632	H-3	0.835E-08	0.0	0.0	0.0
1	7241	RA-226	0.990E-11	0.990E-11	0.105E-11	0.110E-10
1	7241	PB-210	0.0	0.0	0.0	0.0
1	7241	PO-210	0.198E-10	0.198E-10	0.210E-11	0.219E-10
1	7241	RN-222	0.579E-08	0.0	0.0	0.0
1	7241	H-3	0.586E-08	0.0	0.0	0.0
1	12068	RA-226	0.387E-11	0.387E-11	0.587E-12	0.446E-11
1	12068	PB-210	0.0	0.0	0.0	0.0
1	12068	PO-210	0.775E-11	0.775E-11	0.117E-11	0.892E-11
1	12068	RN-222	0.293E-08	0.0	0.0	0.0
1	12068	H-3	0.299E-08	0.0	0.0	0.0
1	20113	RA-226	0.161E-11	0.161E-11	0.323E-12	0.194E-11
1	20113	PB-210	0.0	0.0	0.0	0.0
1	20113	PO-210	0.323E-11	0.323E-11	0.647E-12	0.387E-11
1	20113	RN-222	0.161E-08	0.0	0.0	0.0
1	20113	H-3	0.166E-08	0.0	0.0	0.0
1	32180	RA-226	0.680E-12	0.680E-12	0.181E-12	0.861E-12
1	32180	PB-210	0.0	0.0	0.0	0.0
1	32180	PO-210	0.136E-11	0.136E-11	0.362E-12	0.172E-11
1	32180	RN-222	0.920E-09	0.0	0.0	0.0
1	32180	H-3	0.971E-09	0.0	0.0	0.0
1	48270	RA-226	0.337E-12	0.337E-12	0.108E-12	0.445E-12
1	48270	PB-210	0.0	0.0	0.0	0.0
1	48270	PO-210	0.674E-12	0.674E-12	0.215E-12	0.889E-12
1	48270	RN-222	0.565E-09	0.0	0.0	0.0
1	48270	H-3	0.613E-09	0.0	0.0	0.0
1	64360	RA-226	0.174E-12	0.174E-12	0.707E-13	0.245E-12
1	64360	PB-210	0.0	0.0	0.0	0.0
1	64360	PO-210	0.349E-12	0.349E-12	0.141E-12	0.490E-12
1	64360	RN-222	0.397E-09	0.0	0.0	0.0
1	64360	H-3	0.442E-09	0.0	0.0	0.0
1	80450	RA-226	0.113E-12	0.113E-12	0.513E-13	0.165E-12
1	80450	PB-210	0.0	0.0	0.0	0.0
1	80450	PO-210	0.226E-12	0.226E-12	0.103E-12	0.329E-12
1	80450	RN-222	0.300E-09	0.0	0.0	0.0
1	80450	H-3	0.344E-09	0.0	0.0	0.0

2	1207	RA-226	0.340E-09	0.340E-09	0.618E-11	0.347E-09
2	1207	PB-210	0.0	0.0	0.0	0.0
2	1207	PO-210	0.681E-09	0.681E-09	0.124E-10	0.693E-09
2	1207	RN-222	0.954E-07	0.0	0.0	0.0
2	1207	H-3	0.956E-07	0.0	0.0	0.0
2	2414	RA-226	0.666E-10	0.666E-10	0.206E-11	0.687E-10
2	2414	PB-210	0.0	0.0	0.0	0.0
2	2414	PO-210	0.133E-09	0.133E-09	0.413E-11	0.137E-09
2	2414	RN-222	0.246E-07	0.0	0.0	0.0
2	2414	H-3	0.247E-07	0.0	0.0	0.0
2	4023	RA-226	0.231E-10	0.231E-10	0.108E-11	0.242E-10
2	4023	PB-210	0.0	0.0	0.0	0.0
2	4023	PO-210	0.463E-10	0.463E-10	0.217E-11	0.484E-10
2	4023	RN-222	0.114E-07	0.0	0.0	0.0
2	4023	H-3	0.115E-07	0.0	0.0	0.0
2	5632	RA-226	0.121E-10	0.121E-10	0.722E-12	0.129E-10
2	5632	PB-210	0.0	0.0	0.0	0.0
2	5632	PO-210	0.243E-10	0.243E-10	0.144E-11	0.257E-10
2	5632	RN-222	0.713E-08	0.0	0.0	0.0
2	5632	H-3	0.719E-08	0.0	0.0	0.0
2	7241	RA-226	0.699E-11	0.699E-11	0.521E-12	0.751E-11
2	7241	PB-210	0.0	0.0	0.0	0.0
2	7241	PO-210	0.140E-10	0.140E-10	0.104E-11	0.150E-10
2	7241	RN-222	0.501E-08	0.0	0.0	0.0
2	7241	H-3	0.507E-08	0.0	0.0	0.0
2	12068	RA-226	0.260E-11	0.260E-11	0.280E-12	0.288E-11
2	12068	PB-210	0.0	0.0	0.0	0.0
2	12068	PO-210	0.520E-11	0.520E-11	0.559E-12	0.576E-11
2	12068	RN-222	0.256E-08	0.0	0.0	0.0
2	12068	H-3	0.261E-08	0.0	0.0	0.0
2	20113	RA-226	0.103E-11	0.103E-11	0.148E-12	0.117E-11
2	20113	PB-210	0.0	0.0	0.0	0.0
2	20113	PO-210	0.205E-11	0.205E-11	0.297E-12	0.235E-11
2	20113	RN-222	0.142E-08	0.0	0.0	0.0
2	20113	H-3	0.146E-08	0.0	0.0	0.0
2	32180	RA-226	0.384E-12	0.384E-12	0.795E-13	0.463E-12
2	32180	PB-210	0.0	0.0	0.0	0.0
2	32180	PO-210	0.767E-12	0.767E-12	0.159E-12	0.926E-12
2	32180	RN-222	0.820E-09	0.0	0.0	0.0
2	32180	H-3	0.862E-09	0.0	0.0	0.0
2	48270	RA-226	0.184E-12	0.184E-12	0.461E-13	0.230E-12
2	48270	PB-210	0.0	0.0	0.0	0.0
2	48270	PO-210	0.367E-12	0.367E-12	0.923E-13	0.460E-12
2	48270	RN-222	0.507E-09	0.0	0.0	0.0
2	48270	H-3	0.547E-09	0.0	0.0	0.0
2	64360	RA-226	0.840E-13	0.840E-13	0.291E-13	0.113E-12
2	64360	PB-210	0.0	0.0	0.0	0.0
2	64360	PO-210	0.168E-12	0.168E-12	0.582E-13	0.226E-12
2	64360	RN-222	0.358E-09	0.0	0.0	0.0
2	64360	H-3	0.396E-09	0.0	0.0	0.0
2	80450	RA-226	0.529E-13	0.529E-13	0.208E-13	0.737E-13
2	80450	PB-210	0.0	0.0	0.0	0.0
2	80450	PO-210	0.106E-12	0.106E-12	0.415E-13	0.147E-12
2	80450	RN-222	0.272E-09	0.0	0.0	0.0
2	80450	H-3	0.308E-09	0.0	0.0	0.0
3	1207	RA-226	0.401E-09	0.401E-09	0.625E-11	0.408E-09
3	1207	PB-210	0.0	0.0	0.0	0.0
3	1207	PO-210	0.803E-09	0.803E-09	0.125E-10	0.815E-09
3	1207	RN-222	0.116E-06	0.0	0.0	0.0
3	1207	H-3	0.116E-06	0.0	0.0	0.0
3	2414	RA-226	0.111E-09	0.111E-09	0.297E-11	0.114E-09
3	2414	PB-210	0.0	0.0	0.0	0.0
3	2414	PO-210	0.222E-09	0.222E-09	0.594E-11	0.228E-09
3	2414	RN-222	0.431E-07	0.0	0.0	0.0
3	2414	H-3	0.433E-07	0.0	0.0	0.0
3	4023	RA-226	0.380E-10	0.380E-10	0.152E-11	0.396E-10

3	4023	PB-210	0.0	0.0	0.0	0.0
3	4023	PO-210	0.761E-10	0.761E-10	0.304E-11	0.791E-10
3	4023	RN-222	0.201E-07	0.0	0.0	0.0
3	4023	H-3	0.202E-07	0.0	0.0	0.0
3	5632	RA-226	0.198E-10	0.198E-10	0.998E-12	0.208E-10
3	5632	PB-210	0.0	0.0	0.0	0.0
3	5632	PO-210	0.397E-10	0.397E-10	0.200E-11	0.417E-10
3	5632	RN-222	0.125E-07	0.0	0.0	0.0
3	5632	H-3	0.127E-07	0.0	0.0	0.0
3	7241	RA-226	0.113E-10	0.113E-10	0.708E-12	0.120E-10
3	7241	PB-210	0.0	0.0	0.0	0.0
3	7241	PO-210	0.226E-10	0.226E-10	0.142E-11	0.240E-10
3	7241	RN-222	0.883E-08	0.0	0.0	0.0
3	7241	H-3	0.893E-08	0.0	0.0	0.0
3	12068	RA-226	0.414E-11	0.414E-11	0.371E-12	0.451E-11
3	12068	PB-210	0.0	0.0	0.0	0.0
3	12068	PO-210	0.828E-11	0.828E-11	0.742E-12	0.902E-11
3	12068	RN-222	0.453E-08	0.0	0.0	0.0
3	12068	H-3	0.462E-08	0.0	0.0	0.0
3	20113	RA-226	0.160E-11	0.160E-11	0.192E-12	0.179E-11
3	20113	PB-210	0.0	0.0	0.0	0.0
3	20113	PO-210	0.320E-11	0.320E-11	0.384E-12	0.358E-11
3	20113	RN-222	0.252E-08	0.0	0.0	0.0
3	20113	H-3	0.260E-08	0.0	0.0	0.0
3	32180	RA-226	0.573E-12	0.573E-12	0.997E-13	0.672E-12
3	32180	PB-210	0.0	0.0	0.0	0.0
3	32180	PO-210	0.115E-11	0.115E-11	0.199E-12	0.134E-11
3	32180	RN-222	0.146E-08	0.0	0.0	0.0
3	32180	H-3	0.153E-08	0.0	0.0	0.0
3	48270	RA-226	0.270E-12	0.270E-12	0.568E-13	0.327E-12
3	48270	PB-210	0.0	0.0	0.0	0.0
3	48270	PO-210	0.540E-12	0.540E-12	0.114E-12	0.654E-12
3	48270	RN-222	0.902E-09	0.0	0.0	0.0
3	48270	H-3	0.972E-09	0.0	0.0	0.0
3	64360	RA-226	0.117E-12	0.117E-12	0.347E-13	0.152E-12
3	64360	PB-210	0.0	0.0	0.0	0.0
3	64360	PO-210	0.235E-12	0.235E-12	0.693E-13	0.304E-12
3	64360	RN-222	0.638E-09	0.0	0.0	0.0
3	64360	H-3	0.705E-09	0.0	0.0	0.0
3	80450	RA-226	0.730E-13	0.730E-13	0.244E-13	0.974E-13
3	80450	PB-210	0.0	0.0	0.0	0.0
3	80450	PO-210	0.146E-12	0.146E-12	0.487E-13	0.195E-12
3	80450	RN-222	0.485E-09	0.0	0.0	0.0
3	80450	H-3	0.549E-09	0.0	0.0	0.0
4	1207	RA-226	0.350E-09	0.350E-09	0.548E-11	0.355E-09
4	1207	PB-210	0.0	0.0	0.0	0.0
4	1207	PO-210	0.700E-09	0.700E-09	0.110E-10	0.711E-09
4	1207	RN-222	0.100E-06	0.0	0.0	0.0
4	1207	H-3	0.100E-06	0.0	0.0	0.0
4	2414	RA-226	0.888E-10	0.888E-10	0.242E-11	0.913E-10
4	2414	PB-210	0.0	0.0	0.0	0.0
4	2414	PO-210	0.178E-09	0.178E-09	0.483E-11	0.183E-09
4	2414	RN-222	0.329E-07	0.0	0.0	0.0
4	2414	H-3	0.330E-07	0.0	0.0	0.0
4	4023	RA-226	0.314E-10	0.314E-10	0.126E-11	0.327E-10
4	4023	PB-210	0.0	0.0	0.0	0.0
4	4023	PO-210	0.628E-10	0.628E-10	0.252E-11	0.654E-10
4	4023	RN-222	0.153E-07	0.0	0.0	0.0
4	4023	H-3	0.154E-07	0.0	0.0	0.0
4	5632	RA-226	0.167E-10	0.167E-10	0.837E-12	0.176E-10
4	5632	PB-210	0.0	0.0	0.0	0.0
4	5632	PO-210	0.335E-10	0.335E-10	0.167E-11	0.351E-10
4	5632	RN-222	0.955E-08	0.0	0.0	0.0
4	5632	H-3	0.963E-08	0.0	0.0	0.0
4	7241	RA-226	0.982E-11	0.982E-11	0.602E-12	0.104E-10
4	7241	PB-210	0.0	0.0	0.0	0.0

4	7241	PO-210	0.196E-10	0.196E-10	0.120E-11	0.208E-10
4	7241	RN-222	0.672E-08	0.0	0.0	0.0
4	7241	H-3	0.679E-08	0.0	0.0	0.0
4	12068	RA-226	0.378E-11	0.378E-11	0.323E-12	0.410E-11
4	12068	PB-210	0.0	0.0	0.0	0.0
4	12068	PO-210	0.755E-11	0.755E-11	0.645E-12	0.820E-11
4	12068	RN-222	0.344E-08	0.0	0.0	0.0
4	12068	H-3	0.350E-08	0.0	0.0	0.0
4	20113	RA-226	0.152E-11	0.152E-11	0.171E-12	0.169E-11
4	20113	PB-210	0.0	0.0	0.0	0.0
4	20113	PO-210	0.303E-11	0.303E-11	0.343E-12	0.338E-11
4	20113	RN-222	0.190E-08	0.0	0.0	0.0
4	20113	H-3	0.196E-08	0.0	0.0	0.0
4	32180	RA-226	0.594E-12	0.594E-12	0.922E-13	0.686E-12
4	32180	PB-210	0.0	0.0	0.0	0.0
4	32180	PO-210	0.119E-11	0.119E-11	0.184E-12	0.137E-11
4	32180	RN-222	0.110E-08	0.0	0.0	0.0
4	32180	H-3	0.115E-08	0.0	0.0	0.0
4	48270	RA-226	0.289E-12	0.289E-12	0.541E-13	0.343E-12
4	48270	PB-210	0.0	0.0	0.0	0.0
4	48270	PO-210	0.579E-12	0.579E-12	0.108E-12	0.687E-12
4	48270	RN-222	0.676E-09	0.0	0.0	0.0
4	48270	H-3	0.730E-09	0.0	0.0	0.0
4	64360	RA-226	0.142E-12	0.142E-12	0.344E-13	0.176E-12
4	64360	PB-210	0.0	0.0	0.0	0.0
4	64360	PO-210	0.284E-12	0.284E-12	0.688E-13	0.353E-12
4	64360	RN-222	0.477E-09	0.0	0.0	0.0
4	64360	H-3	0.528E-09	0.0	0.0	0.0
4	80450	RA-226	0.918E-13	0.918E-13	0.249E-13	0.117E-12
4	80450	PB-210	0.0	0.0	0.0	0.0
4	80450	PO-210	0.184E-12	0.184E-12	0.497E-13	0.233E-12
4	80450	RN-222	0.362E-09	0.0	0.0	0.0
4	80450	H-3	0.411E-09	0.0	0.0	0.0
5	1207	RA-226	0.217E-09	0.217E-09	0.367E-11	0.221E-09
5	1207	PB-210	0.0	0.0	0.0	0.0
5	1207	PO-210	0.434E-09	0.434E-09	0.734E-11	0.441E-09
5	1207	RN-222	0.630E-07	0.0	0.0	0.0
5	1207	H-3	0.631E-07	0.0	0.0	0.0
5	2414	RA-226	0.466E-10	0.466E-10	0.147E-11	0.480E-10
5	2414	PB-210	0.0	0.0	0.0	0.0
5	2414	PO-210	0.931E-10	0.931E-10	0.293E-11	0.961E-10
5	2414	RN-222	0.169E-07	0.0	0.0	0.0
5	2414	H-3	0.170E-07	0.0	0.0	0.0
5	4023	RA-226	0.169E-10	0.169E-10	0.789E-12	0.177E-10
5	4023	PB-210	0.0	0.0	0.0	0.0
5	4023	PO-210	0.339E-10	0.339E-10	0.158E-11	0.355E-10
5	4023	RN-222	0.785E-08	0.0	0.0	0.0
5	4023	H-3	0.790E-08	0.0	0.0	0.0
5	5632	RA-226	0.918E-11	0.918E-11	0.533E-12	0.972E-11
5	5632	PB-210	0.0	0.0	0.0	0.0
5	5632	PO-210	0.184E-10	0.184E-10	0.107E-11	0.194E-10
5	5632	RN-222	0.489E-08	0.0	0.0	0.0
5	5632	H-3	0.494E-08	0.0	0.0	0.0
5	7241	RA-226	0.557E-11	0.557E-11	0.391E-12	0.596E-11
5	7241	PB-210	0.0	0.0	0.0	0.0
5	7241	PO-210	0.111E-10	0.111E-10	0.783E-12	0.119E-10
5	7241	RN-222	0.344E-08	0.0	0.0	0.0
5	7241	H-3	0.348E-08	0.0	0.0	0.0
5	12068	RA-226	0.223E-11	0.223E-11	0.216E-12	0.244E-11
5	12068	PB-210	0.0	0.0	0.0	0.0
5	12068	PO-210	0.446E-11	0.446E-11	0.432E-12	0.489E-11
5	12068	RN-222	0.175E-08	0.0	0.0	0.0
5	12068	H-3	0.178E-08	0.0	0.0	0.0
5	20113	RA-226	0.926E-12	0.926E-12	0.118E-12	0.104E-11
5	20113	PB-210	0.0	0.0	0.0	0.0
5	20113	PO-210	0.185E-11	0.185E-11	0.236E-12	0.209E-11

5	20113	RN-222	0.957E-09	0.0	0.0	0.0
5	20113	H-3	0.990E-09	0.0	0.0	0.0
5	32180	RA-226	0.392E-12	0.392E-12	0.657E-13	0.458E-12
5	32180	PB-210	0.0	0.0	0.0	0.0
5	32180	PO-210	0.784E-12	0.784E-12	0.131E-12	0.915E-12
5	32180	RN-222	0.548E-09	0.0	0.0	0.0
5	32180	H-3	0.579E-09	0.0	0.0	0.0
5	48270	RA-226	0.195E-12	0.195E-12	0.393E-13	0.234E-12
5	48270	PB-210	0.0	0.0	0.0	0.0
5	48270	PO-210	0.390E-12	0.390E-12	0.787E-13	0.468E-12
5	48270	RN-222	0.336E-09	0.0	0.0	0.0
5	48270	H-3	0.365E-09	0.0	0.0	0.0
5	64360	RA-226	0.104E-12	0.104E-12	0.258E-13	0.130E-12
5	64360	PB-210	0.0	0.0	0.0	0.0
5	64360	PO-210	0.209E-12	0.209E-12	0.515E-13	0.261E-12
5	64360	RN-222	0.236E-09	0.0	0.0	0.0
5	64360	H-3	0.263E-09	0.0	0.0	0.0
5	80450	RA-226	0.688E-13	0.688E-13	0.189E-13	0.877E-13
5	80450	PB-210	0.0	0.0	0.0	0.0
5	80450	PO-210	0.138E-12	0.138E-12	0.377E-13	0.175E-12
5	80450	RN-222	0.178E-09	0.0	0.0	0.0
5	80450	H-3	0.205E-09	0.0	0.0	0.0
6	1207	RA-226	0.164E-09	0.164E-09	0.293E-11	0.167E-09
6	1207	PB-210	0.0	0.0	0.0	0.0
6	1207	PO-210	0.329E-09	0.329E-09	0.586E-11	0.334E-09
6	1207	RN-222	0.518E-07	0.0	0.0	0.0
6	1207	H-3	0.519E-07	0.0	0.0	0.0
6	2414	RA-226	0.302E-10	0.302E-10	0.101E-11	0.312E-10
6	2414	PB-210	0.0	0.0	0.0	0.0
6	2414	PO-210	0.603E-10	0.603E-10	0.202E-11	0.623E-10
6	2414	RN-222	0.135E-07	0.0	0.0	0.0
6	2414	H-3	0.136E-07	0.0	0.0	0.0
6	4023	RA-226	0.103E-10	0.103E-10	0.531E-12	0.108E-10
6	4023	PB-210	0.0	0.0	0.0	0.0
6	4023	PO-210	0.206E-10	0.206E-10	0.106E-11	0.216E-10
6	4023	RN-222	0.627E-08	0.0	0.0	0.0
6	4023	H-3	0.631E-08	0.0	0.0	0.0
6	5632	RA-226	0.536E-11	0.536E-11	0.355E-12	0.572E-11
6	5632	PB-210	0.0	0.0	0.0	0.0
6	5632	PO-210	0.107E-10	0.107E-10	0.710E-12	0.114E-10
6	5632	RN-222	0.391E-08	0.0	0.0	0.0
6	5632	H-3	0.395E-08	0.0	0.0	0.0
6	7241	RA-226	0.310E-11	0.310E-11	0.257E-12	0.335E-11
6	7241	PB-210	0.0	0.0	0.0	0.0
6	7241	PO-210	0.619E-11	0.619E-11	0.515E-12	0.671E-11
6	7241	RN-222	0.275E-08	0.0	0.0	0.0
6	7241	H-3	0.278E-08	0.0	0.0	0.0
6	12068	RA-226	0.117E-11	0.117E-11	0.140E-12	0.130E-11
6	12068	PB-210	0.0	0.0	0.0	0.0
6	12068	PO-210	0.233E-11	0.233E-11	0.279E-12	0.251E-11
6	12068	RN-222	0.140E-08	0.0	0.0	0.0
6	12068	H-3	0.143E-08	0.0	0.0	0.0
6	20113	RA-226	0.468E-12	0.468E-12	0.747E-13	0.542E-12
6	20113	PB-210	0.0	0.0	0.0	0.0
6	20113	PO-210	0.935E-12	0.935E-12	0.149E-12	0.108E-11
6	20113	RN-222	0.776E-09	0.0	0.0	0.0
6	20113	H-3	0.804E-09	0.0	0.0	0.0
6	32180	RA-226	0.188E-12	0.188E-12	0.404E-13	0.228E-12
6	32180	PB-210	0.0	0.0	0.0	0.0
6	32180	PO-210	0.375E-12	0.375E-12	0.807E-13	0.456E-12
6	32180	RN-222	0.447E-09	0.0	0.0	0.0
6	32180	H-3	0.474E-09	0.0	0.0	0.0
6	48270	RA-226	0.915E-13	0.915E-13	0.233E-13	0.115E-12
6	48270	PB-210	0.0	0.0	0.0	0.0
6	48270	PO-210	0.183E-12	0.183E-12	0.466E-13	0.230E-12
6	48270	RN-222	0.275E-09	0.0	0.0	0.0

6	48270	H-3	0.300E-09	0.0	0.0	0.0
6	64360	RA-226	0.451E-13	0.451E-13	0.147E-13	0.598E-13
6	64360	PB-210	0.0	0.0	0.0	0.0
6	64360	PO-210	0.902E-13	0.902E-13	0.293E-13	0.120E-12
6	64360	RN-222	0.193E-09	0.0	0.0	0.0
6	64360	H-3	0.217E-09	0.0	0.0	0.0
6	80450	RA-226	0.288E-13	0.288E-13	0.103E-13	0.392E-13
6	80450	PB-210	0.0	0.0	0.0	0.0
6	80450	PO-210	0.577E-13	0.577E-13	0.207E-13	0.783E-13
6	80450	RN-222	0.146E-09	0.0	0.0	0.0
6	80450	H-3	0.169E-09	0.0	0.0	0.0
7	1207	RA-226	0.203E-09	0.203E-09	0.356E-11	0.206E-09
7	1207	PB-210	0.0	0.0	0.0	0.0
7	1207	PO-210	0.406E-09	0.406E-09	0.713E-11	0.413E-09
7	1207	RN-222	0.625E-07	0.0	0.0	0.0
7	1207	H-3	0.626E-07	0.0	0.0	0.0
7	2414	RA-226	0.500E-10	0.500E-10	0.160E-11	0.516E-10
7	2414	PB-210	0.0	0.0	0.0	0.0
7	2414	PO-210	0.100E-09	0.100E-09	0.320E-11	0.103E-09
7	2414	RN-222	0.221E-07	0.0	0.0	0.0
7	2414	H-3	0.222E-07	0.0	0.0	0.0
7	4023	RA-226	0.167E-10	0.167E-10	0.831E-12	0.175E-10
7	4023	PB-210	0.0	0.0	0.0	0.0
7	4023	PO-210	0.334E-10	0.334E-10	0.166E-11	0.351E-10
7	4023	RN-222	0.103E-07	0.0	0.0	0.0
7	4023	H-3	0.103E-07	0.0	0.0	0.0
7	5632	RA-226	0.858E-11	0.858E-11	0.550E-12	0.913E-11
7	5632	PB-210	0.0	0.0	0.0	0.0
7	5632	PO-210	0.172E-10	0.172E-10	0.110E-11	0.183E-10
7	5632	RN-222	0.641E-08	0.0	0.0	0.0
7	5632	H-3	0.647E-08	0.0	0.0	0.0
7	7241	RA-226	0.482E-11	0.482E-11	0.395E-12	0.521E-11
7	7241	PB-210	0.0	0.0	0.0	0.0
7	7241	PO-210	0.964E-11	0.964E-11	0.791E-12	0.104E-10
7	7241	RN-222	0.450E-08	0.0	0.0	0.0
7	7241	H-3	0.456E-08	0.0	0.0	0.0
7	12068	RA-226	0.174E-11	0.174E-11	0.211E-12	0.195E-11
7	12068	PB-210	0.0	0.0	0.0	0.0
7	12068	PO-210	0.348E-11	0.348E-11	0.423E-12	0.390E-11
7	12068	RN-222	0.231E-08	0.0	0.0	0.0
7	12068	H-3	0.235E-08	0.0	0.0	0.0
7	20113	RA-226	0.672E-12	0.672E-12	0.112E-12	0.784E-12
7	20113	PB-210	0.0	0.0	0.0	0.0
7	20113	PO-210	0.134E-11	0.134E-11	0.223E-12	0.157E-11
7	20113	RN-222	0.128E-08	0.0	0.0	0.0
7	20113	H-3	0.132E-08	0.0	0.0	0.0
7	32180	RA-226	0.251E-12	0.251E-12	0.594E-13	0.310E-12
7	32180	PB-210	0.0	0.0	0.0	0.0
7	32180	PO-210	0.502E-12	0.502E-12	0.119E-12	0.621E-12
7	32180	RN-222	0.739E-09	0.0	0.0	0.0
7	32180	H-3	0.781E-09	0.0	0.0	0.0
7	48270	RA-226	0.121E-12	0.121E-12	0.339E-13	0.155E-12
7	48270	PB-210	0.0	0.0	0.0	0.0
7	48270	PO-210	0.241E-12	0.241E-12	0.677E-13	0.309E-12
7	48270	RN-222	0.457E-09	0.0	0.0	0.0
7	48270	H-3	0.496E-09	0.0	0.0	0.0
7	64360	RA-226	0.563E-13	0.563E-13	0.211E-13	0.774E-13
7	64360	PB-210	0.0	0.0	0.0	0.0
7	64360	PO-210	0.113E-12	0.113E-12	0.421E-13	0.155E-12
7	64360	RN-222	0.322E-09	0.0	0.0	0.0
7	64360	H-3	0.359E-09	0.0	0.0	0.0
7	80450	RA-226	0.354E-13	0.354E-13	0.147E-13	0.501E-13
7	80450	PB-210	0.0	0.0	0.0	0.0
7	80450	PO-210	0.709E-13	0.709E-13	0.294E-13	0.100E-12
7	80450	RN-222	0.244E-09	0.0	0.0	0.0
7	80450	H-3	0.280E-09	0.0	0.0	0.0

8	1207	RA-226	0.309E-09	0.309E-09	0.565E-11	0.315E-09
8	1207	PB-210	0.0	0.0	0.0	0.0
8	1207	PO-210	0.619E-09	0.619E-09	0.113E-10	0.630E-09
8	1207	RN-222	0.812E-07	0.0	0.0	0.0
8	1207	H-3	0.813E-07	0.0	0.0	0.0
8	2414	RA-226	0.585E-10	0.585E-10	0.183E-11	0.604E-10
8	2414	PB-210	0.0	0.0	0.0	0.0
8	2414	PO-210	0.117E-09	0.117E-09	0.365E-11	0.121E-09
8	2414	RN-222	0.202E-07	0.0	0.0	0.0
8	2414	H-3	0.203E-07	0.0	0.0	0.0
8	4023	RA-226	0.208E-10	0.208E-10	0.966E-12	0.217E-10
8	4023	PB-210	0.0	0.0	0.0	0.0
8	4023	PO-210	0.415E-10	0.415E-10	0.193E-11	0.435E-10
8	4023	RN-222	0.937E-08	0.0	0.0	0.0
8	4023	H-3	0.943E-08	0.0	0.0	0.0
8	5632	RA-226	0.110E-10	0.110E-10	0.645E-12	0.117E-10
8	5632	PB-210	0.0	0.0	0.0	0.0
8	5632	PO-210	0.221E-10	0.221E-10	0.129E-11	0.234E-10
8	5632	RN-222	0.584E-08	0.0	0.0	0.0
8	5632	H-3	0.589E-08	0.0	0.0	0.0
8	7241	RA-226	0.648E-11	0.648E-11	0.467E-12	0.695E-11
8	7241	PB-210	0.0	0.0	0.0	0.0
8	7241	PO-210	0.130E-10	0.130E-10	0.934E-12	0.139E-10
8	7241	RN-222	0.411E-08	0.0	0.0	0.0
8	7241	H-3	0.415E-08	0.0	0.0	0.0
8	12068	RA-226	0.249E-11	0.249E-11	0.251E-12	0.274E-11
8	12068	PB-210	0.0	0.0	0.0	0.0
8	12068	PO-210	0.498E-11	0.498E-11	0.503E-12	0.549E-11
8	12068	RN-222	0.210E-08	0.0	0.0	0.0
8	12068	H-3	0.214E-08	0.0	0.0	0.0
8	20113	RA-226	0.102E-11	0.102E-11	0.133E-12	0.115E-11
8	20113	PB-210	0.0	0.0	0.0	0.0
8	20113	PO-210	0.204E-11	0.204E-11	0.267E-12	0.231E-11
8	20113	RN-222	0.116E-08	0.0	0.0	0.0
8	20113	H-3	0.120E-08	0.0	0.0	0.0
8	32180	RA-226	0.403E-12	0.403E-12	0.711E-13	0.474E-12
8	32180	PB-210	0.0	0.0	0.0	0.0
8	32180	PO-210	0.806E-12	0.806E-12	0.142E-12	0.948E-12
8	32180	RN-222	0.673E-09	0.0	0.0	0.0
8	32180	H-3	0.706E-09	0.0	0.0	0.0
8	48270	RA-226	0.198E-12	0.198E-12	0.410E-13	0.239E-12
8	48270	PB-210	0.0	0.0	0.0	0.0
8	48270	PO-210	0.395E-12	0.395E-12	0.821E-13	0.477E-12
8	48270	RN-222	0.416E-09	0.0	0.0	0.0
8	48270	H-3	0.448E-09	0.0	0.0	0.0
8	64360	RA-226	0.896E-13	0.896E-13	0.254E-13	0.115E-12
8	64360	PB-210	0.0	0.0	0.0	0.0
8	64360	PO-210	0.179E-12	0.179E-12	0.507E-13	0.230E-12
8	64360	RN-222	0.294E-09	0.0	0.0	0.0
8	64360	H-3	0.324E-09	0.0	0.0	0.0
8	80450	RA-226	0.566E-13	0.566E-13	0.180E-13	0.745E-13
8	80450	PB-210	0.0	0.0	0.0	0.0
8	80450	PO-210	0.113E-12	0.113E-12	0.359E-13	0.149E-12
8	80450	RN-222	0.224E-09	0.0	0.0	0.0
8	80450	H-3	0.252E-09	0.0	0.0	0.0
9	1207	RA-226	0.416E-09	0.416E-09	0.809E-11	0.424E-09
9	1207	PB-210	0.0	0.0	0.0	0.0
9	1207	PO-210	0.831E-09	0.831E-09	0.162E-10	0.847E-09
9	1207	RN-222	0.993E-07	0.0	0.0	0.0
9	1207	H-3	0.995E-07	0.0	0.0	0.0
9	2414	RA-226	0.141E-09	0.141E-09	0.480E-11	0.146E-09
9	2414	PB-210	0.0	0.0	0.0	0.0
9	2414	PO-210	0.282E-09	0.282E-09	0.959E-11	0.291E-09
9	2414	RN-222	0.410E-07	0.0	0.0	0.0
9	2414	H-3	0.411E-07	0.0	0.0	0.0
9	4023	RA-226	0.519E-10	0.519E-10	0.260E-11	0.545E-10

9	4023	PB-210	0.0	0.0	0.0	0.0
9	4023	PO-210	0.104E-09	0.104E-09	0.520E-11	0.109E-09
9	4023	RN-222	0.189E-07	0.0	0.0	0.0
9	4023	H-3	0.190E-07	0.0	0.0	0.0
9	5632	RA-226	0.282E-10	0.282E-10	0.176E-11	0.299E-10
9	5632	PB-210	0.0	0.0	0.0	0.0
9	5632	PO-210	0.564E-10	0.564E-10	0.351E-11	0.599E-10
9	5632	RN-222	0.117E-07	0.0	0.0	0.0
9	5632	H-3	0.118E-07	0.0	0.0	0.0
9	7241	RA-226	0.170E-10	0.170E-10	0.129E-11	0.183E-10
9	7241	PB-210	0.0	0.0	0.0	0.0
9	7241	PO-210	0.340E-10	0.340E-10	0.258E-11	0.366E-10
9	7241	RN-222	0.823E-08	0.0	0.0	0.0
9	7241	H-3	0.831E-08	0.0	0.0	0.0
9	12068	RA-226	0.678E-11	0.678E-11	0.706E-12	0.748E-11
9	12068	PB-210	0.0	0.0	0.0	0.0
9	12068	PO-210	0.136E-10	0.136E-10	0.141E-11	0.150E-10
9	12068	RN-222	0.418E-08	0.0	0.0	0.0
9	12068	H-3	0.425E-08	0.0	0.0	0.0
9	20113	RA-226	0.284E-11	0.284E-11	0.380E-12	0.322E-11
9	20113	PB-210	0.0	0.0	0.0	0.0
9	20113	PO-210	0.568E-11	0.568E-11	0.760E-12	0.644E-11
9	20113	RN-222	0.230E-08	0.0	0.0	0.0
9	20113	H-3	0.237E-08	0.0	0.0	0.0
9	32180	RA-226	0.116E-11	0.116E-11	0.206E-12	0.137E-11
9	32180	PB-210	0.0	0.0	0.0	0.0
9	32180	PO-210	0.233E-11	0.233E-11	0.413E-12	0.274E-11
9	32180	RN-222	0.133E-08	0.0	0.0	0.0
9	32180	H-3	0.139E-08	0.0	0.0	0.0
9	48270	RA-226	0.576E-12	0.576E-12	0.121E-12	0.697E-12
9	48270	PB-210	0.0	0.0	0.0	0.0
9	48270	PO-210	0.115E-11	0.115E-11	0.241E-12	0.139E-11
9	48270	RN-222	0.819E-09	0.0	0.0	0.0
9	48270	H-3	0.876E-09	0.0	0.0	0.0
9	64360	RA-226	0.276E-12	0.276E-12	0.760E-13	0.352E-12
9	64360	PB-210	0.0	0.0	0.0	0.0
9	64360	PO-210	0.553E-12	0.553E-12	0.152E-12	0.705E-12
9	64360	RN-222	0.578E-09	0.0	0.0	0.0
9	64360	H-3	0.632E-09	0.0	0.0	0.0
9	80450	RA-226	0.177E-12	0.177E-12	0.545E-13	0.231E-12
9	80450	PB-210	0.0	0.0	0.0	0.0
9	80450	PO-210	0.354E-12	0.354E-12	0.109E-12	0.463E-12
9	80450	RN-222	0.439E-09	0.0	0.0	0.0
9	80450	H-3	0.492E-09	0.0	0.0	0.0
10	1207	RA-226	0.318E-09	0.318E-09	0.685E-11	0.325E-09
10	1207	PB-210	0.0	0.0	0.0	0.0
10	1207	PO-210	0.636E-09	0.636E-09	0.137E-10	0.650E-09
10	1207	RN-222	0.752E-07	0.0	0.0	0.0
10	1207	H-3	0.754E-07	0.0	0.0	0.0
10	2414	RA-226	0.655E-10	0.655E-10	0.257E-11	0.681E-10
10	2414	PB-210	0.0	0.0	0.0	0.0
10	2414	PO-210	0.131E-09	0.131E-09	0.513E-11	0.136E-09
10	2414	RN-222	0.193E-07	0.0	0.0	0.0
10	2414	H-3	0.194E-07	0.0	0.0	0.0
10	4023	RA-226	0.239E-10	0.239E-10	0.141E-11	0.253E-10
10	4023	PB-210	0.0	0.0	0.0	0.0
10	4023	PO-210	0.478E-10	0.478E-10	0.281E-11	0.506E-10
10	4023	RN-222	0.889E-08	0.0	0.0	0.0
10	4023	H-3	0.894E-08	0.0	0.0	0.0
10	5632	RA-226	0.128E-10	0.128E-10	0.956E-12	0.138E-10
10	5632	PB-210	0.0	0.0	0.0	0.0
10	5632	PO-210	0.257E-10	0.257E-10	0.191E-11	0.276E-10
10	5632	RN-222	0.551E-08	0.0	0.0	0.0
10	5632	H-3	0.555E-08	0.0	0.0	0.0
10	7241	RA-226	0.770E-11	0.770E-11	0.706E-12	0.840E-11
10	7241	PB-210	0.0	0.0	0.0	0.0

10	7241	PO-210	0.154E-10	0.154E-10	0.141E-11	0.168E-10
10	7241	RN-222	0.385E-08	0.0	0.0	0.0
10	7241	H-3	0.389E-08	0.0	0.0	0.0
10	12068	RA-226	0.301E-11	0.301E-11	0.391E-12	0.340E-11
10	12068	PB-210	0.0	0.0	0.0	0.0
10	12068	PO-210	0.603E-11	0.603E-11	0.782E-12	0.681E-11
10	12068	RN-222	0.195E-08	0.0	0.0	0.0
10	12068	H-3	0.198E-08	0.0	0.0	0.0
10	20113	RA-226	0.125E-11	0.125E-11	0.213E-12	0.146E-11
10	20113	PB-210	0.0	0.0	0.0	0.0
10	20113	PO-210	0.250E-11	0.250E-11	0.427E-12	0.292E-11
10	20113	RN-222	0.107E-08	0.0	0.0	0.0
10	20113	H-3	0.110E-08	0.0	0.0	0.0
10	32180	RA-226	0.510E-12	0.510E-12	0.118E-12	0.628E-12
10	32180	PB-210	0.0	0.0	0.0	0.0
10	32180	PO-210	0.102E-11	0.102E-11	0.236E-12	0.126E-11
10	32180	RN-222	0.616E-09	0.0	0.0	0.0
10	32180	H-3	0.645E-09	0.0	0.0	0.0
10	48270	RA-226	0.252E-12	0.252E-12	0.697E-13	0.322E-12
10	48270	PB-210	0.0	0.0	0.0	0.0
10	48270	PO-210	0.504E-12	0.504E-12	0.139E-12	0.643E-12
10	48270	RN-222	0.380E-09	0.0	0.0	0.0
10	48270	H-3	0.407E-09	0.0	0.0	0.0
10	64360	RA-226	0.126E-12	0.126E-12	0.452E-13	0.171E-12
10	64360	PB-210	0.0	0.0	0.0	0.0
10	64360	PO-210	0.252E-12	0.252E-12	0.904E-13	0.342E-12
10	64360	RN-222	0.268E-09	0.0	0.0	0.0
10	64360	H-3	0.294E-09	0.0	0.0	0.0
10	80450	RA-226	0.814E-13	0.814E-13	0.326E-13	0.114E-12
10	80450	PB-210	0.0	0.0	0.0	0.0
10	80450	PO-210	0.163E-12	0.163E-12	0.653E-13	0.228E-12
10	80450	RN-222	0.203E-09	0.0	0.0	0.0
10	80450	H-3	0.228E-09	0.0	0.0	0.0
11	1207	RA-226	0.214E-09	0.214E-09	0.547E-11	0.219E-09
11	1207	PB-210	0.0	0.0	0.0	0.0
11	1207	PO-210	0.427E-09	0.427E-09	0.109E-10	0.438E-09
11	1207	RN-222	0.518E-07	0.0	0.0	0.0
11	1207	H-3	0.519E-07	0.0	0.0	0.0
11	2414	RA-226	0.512E-10	0.512E-10	0.249E-11	0.537E-10
11	2414	PB-210	0.0	0.0	0.0	0.0
11	2414	PO-210	0.102E-09	0.102E-09	0.499E-11	0.107E-09
11	2414	RN-222	0.155E-07	0.0	0.0	0.0
11	2414	H-3	0.156E-07	0.0	0.0	0.0
11	4023	RA-226	0.186E-10	0.186E-10	0.139E-11	0.200E-10
11	4023	PB-210	0.0	0.0	0.0	0.0
11	4023	PO-210	0.372E-10	0.372E-10	0.277E-11	0.400E-10
11	4023	RN-222	0.708E-08	0.0	0.0	0.0
11	4023	H-3	0.713E-08	0.0	0.0	0.0
11	5632	RA-226	0.999E-11	0.999E-11	0.951E-12	0.109E-10
11	5632	PB-210	0.0	0.0	0.0	0.0
11	5632	PO-210	0.200E-10	0.200E-10	0.190E-11	0.219E-10
11	5632	RN-222	0.437E-08	0.0	0.0	0.0
11	5632	H-3	0.441E-08	0.0	0.0	0.0
11	7241	RA-226	0.603E-11	0.603E-11	0.709E-12	0.674E-11
11	7241	PB-210	0.0	0.0	0.0	0.0
11	7241	PO-210	0.121E-10	0.121E-10	0.142E-11	0.135E-10
11	7241	RN-222	0.305E-08	0.0	0.0	0.0
11	7241	H-3	0.308E-08	0.0	0.0	0.0
11	12068	RA-226	0.238E-11	0.238E-11	0.398E-12	0.277E-11
11	12068	PB-210	0.0	0.0	0.0	0.0
11	12068	PO-210	0.475E-11	0.475E-11	0.796E-12	0.555E-11
11	12068	RN-222	0.153E-08	0.0	0.0	0.0
11	12068	H-3	0.156E-08	0.0	0.0	0.0
11	20113	RA-226	0.100E-11	0.100E-11	0.220E-12	0.122E-11
11	20113	PB-210	0.0	0.0	0.0	0.0
11	20113	PO-210	0.200E-11	0.200E-11	0.440E-12	0.244E-11

11	20113	RN-222	0.838E-09	0.0	0.0	0.0
11	20113	H-3	0.865E-09	0.0	0.0	0.0
11	32180	RA-226	0.429E-12	0.429E-12	0.123E-12	0.552E-12
11	32180	PB-210	0.0	0.0	0.0	0.0
11	32180	PO-210	0.858E-12	0.858E-12	0.247E-12	0.110E-11
11	32180	RN-222	0.480E-09	0.0	0.0	0.0
11	32180	H-3	0.505E-09	0.0	0.0	0.0
11	48270	RA-226	0.215E-12	0.215E-12	0.731E-13	0.288E-12
11	48270	PB-210	0.0	0.0	0.0	0.0
11	48270	PO-210	0.431E-12	0.431E-12	0.146E-12	0.577E-12
11	48270	RN-222	0.294E-09	0.0	0.0	0.0
11	48270	H-3	0.318E-09	0.0	0.0	0.0
11	64360	RA-226	0.115E-12	0.115E-12	0.480E-13	0.163E-12
11	64360	PB-210	0.0	0.0	0.0	0.0
11	64360	PO-210	0.230E-12	0.230E-12	0.960E-13	0.326E-12
11	64360	RN-222	0.207E-09	0.0	0.0	0.0
11	64360	H-3	0.229E-09	0.0	0.0	0.0
11	80450	RA-226	0.754E-13	0.754E-13	0.346E-13	0.110E-12
11	80450	PB-210	0.0	0.0	0.0	0.0
11	80450	PO-210	0.151E-12	0.151E-12	0.693E-13	0.220E-12
11	80450	RN-222	0.157E-09	0.0	0.0	0.0
11	80450	H-3	0.178E-09	0.0	0.0	0.0
12	1207	RA-226	0.181E-09	0.181E-09	0.518E-11	0.186E-09
12	1207	PB-210	0.0	0.0	0.0	0.0
12	1207	PO-210	0.362E-09	0.362E-09	0.104E-10	0.372E-09
12	1207	RN-222	0.445E-07	0.0	0.0	0.0
12	1207	H-3	0.446E-07	0.0	0.0	0.0
12	2414	RA-226	0.448E-10	0.448E-10	0.237E-11	0.472E-10
12	2414	PB-210	0.0	0.0	0.0	0.0
12	2414	PO-210	0.896E-10	0.896E-10	0.473E-11	0.944E-10
12	2414	RN-222	0.141E-07	0.0	0.0	0.0
12	2414	H-3	0.141E-07	0.0	0.0	0.0
12	4023	RA-226	0.163E-10	0.163E-10	0.132E-11	0.176E-10
12	4023	PB-210	0.0	0.0	0.0	0.0
12	4023	PO-210	0.326E-10	0.326E-10	0.265E-11	0.352E-10
12	4023	RN-222	0.641E-08	0.0	0.0	0.0
12	4023	H-3	0.645E-08	0.0	0.0	0.0
12	5632	RA-226	0.873E-11	0.873E-11	0.911E-12	0.964E-11
12	5632	PB-210	0.0	0.0	0.0	0.0
12	5632	PO-210	0.175E-10	0.175E-10	0.182E-11	0.193E-10
12	5632	RN-222	0.395E-08	0.0	0.0	0.0
12	5632	H-3	0.399E-08	0.0	0.0	0.0
12	7241	RA-226	0.528E-11	0.528E-11	0.682E-12	0.597E-11
12	7241	PB-210	0.0	0.0	0.0	0.0
12	7241	PO-210	0.106E-10	0.106E-10	0.136E-11	0.119E-10
12	7241	RN-222	0.275E-08	0.0	0.0	0.0
12	7241	H-3	0.279E-08	0.0	0.0	0.0
12	12068	RA-226	0.209E-11	0.209E-11	0.385E-12	0.248E-11
12	12068	PB-210	0.0	0.0	0.0	0.0
12	12068	PO-210	0.419E-11	0.419E-11	0.771E-12	0.496E-11
12	12068	RN-222	0.139E-08	0.0	0.0	0.0
12	12068	H-3	0.141E-08	0.0	0.0	0.0
12	20113	RA-226	0.891E-12	0.891E-12	0.215E-12	0.111E-11
12	20113	PB-210	0.0	0.0	0.0	0.0
12	20113	PO-210	0.178E-11	0.178E-11	0.429E-12	0.221E-11
12	20113	RN-222	0.757E-09	0.0	0.0	0.0
12	20113	H-3	0.783E-09	0.0	0.0	0.0
12	32180	RA-226	0.391E-12	0.391E-12	0.121E-12	0.512E-12
12	32180	PB-210	0.0	0.0	0.0	0.0
12	32180	PO-210	0.781E-12	0.781E-12	0.243E-12	0.102E-11
12	32180	RN-222	0.433E-09	0.0	0.0	0.0
12	32180	H-3	0.457E-09	0.0	0.0	0.0
12	48270	RA-226	0.198E-12	0.198E-12	0.724E-13	0.270E-12
12	48270	PB-210	0.0	0.0	0.0	0.0
12	48270	PO-210	0.396E-12	0.396E-12	0.145E-12	0.541E-12
12	48270	RN-222	0.266E-09	0.0	0.0	0.0

12	48270	H-3	0.288E-09	0.0	0.0	0.0
12	64360	RA-226	0.108E-12	0.108E-12	0.480E-13	0.156E-12
12	64360	PB-210	0.0	0.0	0.0	0.0
12	64360	PO-210	0.215E-12	0.215E-12	0.960E-13	0.311E-12
12	64360	RN-222	0.187E-09	0.0	0.0	0.0
12	64360	H-3	0.208E-09	0.0	0.0	0.0
12	80450	RA-226	0.713E-13	0.713E-13	0.348E-13	0.106E-12
12	80450	PB-210	0.0	0.0	0.0	0.0
12	80450	PO-210	0.143E-12	0.143E-12	0.696E-13	0.212E-12
12	80450	RN-222	0.141E-09	0.0	0.0	0.0
12	80450	H-3	0.161E-09	0.0	0.0	0.0
13	1207	RA-226	0.163E-09	0.163E-09	0.499E-11	0.168E-09
13	1207	PB-210	0.0	0.0	0.0	0.0
13	1207	PO-210	0.326E-09	0.326E-09	0.998E-11	0.336E-09
13	1207	RN-222	0.390E-07	0.0	0.0	0.0
13	1207	H-3	0.391E-07	0.0	0.0	0.0
13	2414	RA-226	0.382E-10	0.382E-10	0.227E-11	0.404E-10
13	2414	PB-210	0.0	0.0	0.0	0.0
13	2414	PO-210	0.764E-10	0.764E-10	0.453E-11	0.809E-10
13	2414	RN-222	0.113E-07	0.0	0.0	0.0
13	2414	H-3	0.113E-07	0.0	0.0	0.0
13	4023	RA-226	0.139E-10	0.139E-10	0.128E-11	0.152E-10
13	4023	PB-210	0.0	0.0	0.0	0.0
13	4023	PO-210	0.279E-10	0.279E-10	0.255E-11	0.304E-10
13	4023	RN-222	0.511E-08	0.0	0.0	0.0
13	4023	H-3	0.514E-08	0.0	0.0	0.0
13	5632	RA-226	0.747E-11	0.747E-11	0.882E-12	0.836E-11
13	5632	PB-210	0.0	0.0	0.0	0.0
13	5632	PO-210	0.149E-10	0.149E-10	0.176E-11	0.167E-10
13	5632	RN-222	0.314E-08	0.0	0.0	0.0
13	5632	H-3	0.316E-08	0.0	0.0	0.0
13	7241	RA-226	0.454E-11	0.454E-11	0.664E-12	0.521E-11
13	7241	PB-210	0.0	0.0	0.0	0.0
13	7241	PO-210	0.908E-11	0.908E-11	0.133E-11	0.104E-10
13	7241	RN-222	0.218E-08	0.0	0.0	0.0
13	7241	H-3	0.221E-08	0.0	0.0	0.0
13	12068	RA-226	0.181E-11	0.181E-11	0.377E-12	0.218E-11
13	12068	PB-210	0.0	0.0	0.0	0.0
13	12068	PO-210	0.361E-11	0.361E-11	0.753E-12	0.437E-11
13	12068	RN-222	0.109E-08	0.0	0.0	0.0
13	12068	H-3	0.111E-08	0.0	0.0	0.0
13	20113	RA-226	0.778E-12	0.778E-12	0.211E-12	0.989E-12
13	20113	PB-210	0.0	0.0	0.0	0.0
13	20113	PO-210	0.156E-11	0.156E-11	0.421E-12	0.198E-11
13	20113	RN-222	0.595E-09	0.0	0.0	0.0
13	20113	H-3	0.615E-09	0.0	0.0	0.0
13	32180	RA-226	0.347E-12	0.347E-12	0.120E-12	0.466E-12
13	32180	PB-210	0.0	0.0	0.0	0.0
13	32180	PO-210	0.693E-12	0.693E-12	0.239E-12	0.932E-12
13	32180	RN-222	0.340E-09	0.0	0.0	0.0
13	32180	H-3	0.359E-09	0.0	0.0	0.0
13	48270	RA-226	0.177E-12	0.177E-12	0.716E-13	0.249E-12
13	48270	PB-210	0.0	0.0	0.0	0.0
13	48270	PO-210	0.354E-12	0.354E-12	0.143E-12	0.497E-12
13	48270	RN-222	0.209E-09	0.0	0.0	0.0
13	48270	H-3	0.226E-09	0.0	0.0	0.0
13	64360	RA-226	0.979E-13	0.979E-13	0.476E-13	0.145E-12
13	64360	PB-210	0.0	0.0	0.0	0.0
13	64360	PO-210	0.196E-12	0.196E-12	0.953E-13	0.291E-12
13	64360	RN-222	0.146E-09	0.0	0.0	0.0
13	64360	H-3	0.163E-09	0.0	0.0	0.0
13	80450	RA-226	0.651E-13	0.651E-13	0.346E-13	0.997E-13
13	80450	PB-210	0.0	0.0	0.0	0.0
13	80450	PO-210	0.130E-12	0.130E-12	0.692E-13	0.199E-12
13	80450	RN-222	0.111E-09	0.0	0.0	0.0
13	80450	H-3	0.127E-09	0.0	0.0	0.0

14	1207	RA-226	0.172E-09	0.172E-09	0.530E-11	0.178E-09
14	1207	PB-210	0.0	0.0	0.0	0.0
14	1207	PO-210	0.345E-09	0.345E-09	0.106E-10	0.355E-09
14	1207	RN-222	0.399E-07	0.0	0.0	0.0
14	1207	H-3	0.400E-07	0.0	0.0	0.0
14	2414	RA-226	0.420E-10	0.420E-10	0.231E-11	0.443E-10
14	2414	PB-210	0.0	0.0	0.0	0.0
14	2414	PO-210	0.840E-10	0.840E-10	0.462E-11	0.886E-10
14	2414	RN-222	0.117E-07	0.0	0.0	0.0
14	2414	H-3	0.118E-07	0.0	0.0	0.0
14	4023	RA-226	0.155E-10	0.155E-10	0.130E-11	0.168E-10
14	4023	PB-210	0.0	0.0	0.0	0.0
14	4023	PO-210	0.310E-10	0.310E-10	0.260E-11	0.337E-10
14	4023	RN-222	0.532E-08	0.0	0.0	0.0
14	4023	H-3	0.535E-08	0.0	0.0	0.0
14	5632	RA-226	0.839E-11	0.839E-11	0.900E-12	0.929E-11
14	5632	PB-210	0.0	0.0	0.0	0.0
14	5632	PO-210	0.168E-10	0.168E-10	0.180E-11	0.186E-10
14	5632	RN-222	0.327E-08	0.0	0.0	0.0
14	5632	H-3	0.330E-08	0.0	0.0	0.0
14	7241	RA-226	0.513E-11	0.513E-11	0.677E-12	0.581E-11
14	7241	PB-210	0.0	0.0	0.0	0.0
14	7241	PO-210	0.103E-10	0.103E-10	0.135E-11	0.116E-10
14	7241	RN-222	0.228E-08	0.0	0.0	0.0
14	7241	H-3	0.230E-08	0.0	0.0	0.0
14	12068	RA-226	0.206E-11	0.206E-11	0.384E-12	0.244E-11
14	12068	PB-210	0.0	0.0	0.0	0.0
14	12068	PO-210	0.412E-11	0.412E-11	0.769E-12	0.489E-11
14	12068	RN-222	0.114E-08	0.0	0.0	0.0
14	12068	H-3	0.116E-08	0.0	0.0	0.0
14	20113	RA-226	0.884E-12	0.884E-12	0.215E-12	0.110E-11
14	20113	PB-210	0.0	0.0	0.0	0.0
14	20113	PO-210	0.177E-11	0.177E-11	0.430E-12	0.220E-11
14	20113	RN-222	0.620E-09	0.0	0.0	0.0
14	20113	H-3	0.639E-09	0.0	0.0	0.0
14	32180	RA-226	0.390E-12	0.390E-12	0.123E-12	0.513E-12
14	32180	PB-210	0.0	0.0	0.0	0.0
14	32180	PO-210	0.781E-12	0.781E-12	0.245E-12	0.103E-11
14	32180	RN-222	0.354E-09	0.0	0.0	0.0
14	32180	H-3	0.372E-09	0.0	0.0	0.0
14	48270	RA-226	0.199E-12	0.199E-12	0.740E-13	0.272E-12
14	48270	PB-210	0.0	0.0	0.0	0.0
14	48270	PO-210	0.397E-12	0.397E-12	0.148E-12	0.545E-12
14	48270	RN-222	0.217E-09	0.0	0.0	0.0
14	48270	H-3	0.234E-09	0.0	0.0	0.0
14	64360	RA-226	0.109E-12	0.109E-12	0.495E-13	0.158E-12
14	64360	PB-210	0.0	0.0	0.0	0.0
14	64360	PO-210	0.217E-12	0.217E-12	0.990E-13	0.316E-12
14	64360	RN-222	0.152E-09	0.0	0.0	0.0
14	64360	H-3	0.168E-09	0.0	0.0	0.0
14	80450	RA-226	0.722E-13	0.722E-13	0.363E-13	0.109E-12
14	80450	PB-210	0.0	0.0	0.0	0.0
14	80450	PO-210	0.144E-12	0.144E-12	0.725E-13	0.217E-12
14	80450	RN-222	0.115E-09	0.0	0.0	0.0
14	80450	H-3	0.131E-09	0.0	0.0	0.0
15	1207	RA-226	0.187E-09	0.187E-09	0.569E-11	0.192E-09
15	1207	PB-210	0.0	0.0	0.0	0.0
15	1207	PO-210	0.373E-09	0.373E-09	0.114E-10	0.385E-09
15	1207	RN-222	0.429E-07	0.0	0.0	0.0
15	1207	H-3	0.429E-07	0.0	0.0	0.0
15	2414	RA-226	0.511E-10	0.511E-10	0.295E-11	0.541E-10
15	2414	PB-210	0.0	0.0	0.0	0.0
15	2414	PO-210	0.102E-09	0.102E-09	0.590E-11	0.108E-09
15	2414	RN-222	0.146E-07	0.0	0.0	0.0
15	2414	H-3	0.147E-07	0.0	0.0	0.0
15	4023	RA-226	0.188E-10	0.188E-10	0.166E-11	0.205E-10

15	4023	PB-210	0.0	0.0	0.0	0.0
15	4023	PO-210	0.377E-10	0.377E-10	0.333E-11	0.410E-10
15	4023	RN-222	0.662E-08	0.0	0.0	0.0
15	4023	H-3	0.666E-08	0.0	0.0	0.0
15	5632	RA-226	0.101E-10	0.101E-10	0.115E-11	0.113E-10
15	5632	PB-210	0.0	0.0	0.0	0.0
15	5632	PO-210	0.203E-10	0.203E-10	0.230E-11	0.226E-10
15	5632	RN-222	0.406E-08	0.0	0.0	0.0
15	5632	H-3	0.410E-08	0.0	0.0	0.0
15	7241	RA-226	0.620E-11	0.620E-11	0.865E-12	0.707E-11
15	7241	PB-210	0.0	0.0	0.0	0.0
15	7241	PO-210	0.124E-10	0.124E-10	0.173E-11	0.141E-10
15	7241	RN-222	0.282E-08	0.0	0.0	0.0
15	7241	H-3	0.286E-08	0.0	0.0	0.0
15	12068	RA-226	0.248E-11	0.248E-11	0.491E-12	0.297E-11
15	12068	PB-210	0.0	0.0	0.0	0.0
15	12068	PO-210	0.496E-11	0.496E-11	0.982E-12	0.594E-11
15	12068	RN-222	0.141E-08	0.0	0.0	0.0
15	12068	H-3	0.144E-08	0.0	0.0	0.0
15	20113	RA-226	0.106E-11	0.106E-11	0.275E-12	0.134E-11
15	20113	PB-210	0.0	0.0	0.0	0.0
15	20113	PO-210	0.213E-11	0.213E-11	0.549E-12	0.268E-11
15	20113	RN-222	0.766E-09	0.0	0.0	0.0
15	20113	H-3	0.791E-09	0.0	0.0	0.0
15	32180	RA-226	0.472E-12	0.472E-12	0.156E-12	0.628E-12
15	32180	PB-210	0.0	0.0	0.0	0.0
15	32180	PO-210	0.945E-12	0.945E-12	0.312E-12	0.126E-11
15	32180	RN-222	0.436E-09	0.0	0.0	0.0
15	32180	H-3	0.460E-09	0.0	0.0	0.0
15	48270	RA-226	0.239E-12	0.239E-12	0.937E-13	0.333E-12
15	48270	PB-210	0.0	0.0	0.0	0.0
15	48270	PO-210	0.478E-12	0.478E-12	0.187E-12	0.666E-12
15	48270	RN-222	0.267E-09	0.0	0.0	0.0
15	48270	H-3	0.289E-09	0.0	0.0	0.0
15	64360	RA-226	0.130E-12	0.130E-12	0.625E-13	0.193E-12
15	64360	PB-210	0.0	0.0	0.0	0.0
15	64360	PO-210	0.261E-12	0.261E-12	0.125E-12	0.386E-12
15	64360	RN-222	0.187E-09	0.0	0.0	0.0
15	64360	H-3	0.208E-09	0.0	0.0	0.0
15	80450	RA-226	0.861E-13	0.861E-13	0.456E-13	0.132E-12
15	80450	PB-210	0.0	0.0	0.0	0.0
15	80450	PO-210	0.172E-12	0.172E-12	0.912E-13	0.263E-12
15	80450	RN-222	0.141E-09	0.0	0.0	0.0
15	80450	H-3	0.161E-09	0.0	0.0	0.0
16	1207	RA-226	0.219E-09	0.219E-09	0.599E-11	0.225E-09
16	1207	PB-210	0.0	0.0	0.0	0.0
16	1207	PO-210	0.437E-09	0.437E-09	0.120E-10	0.449E-09
16	1207	RN-222	0.525E-07	0.0	0.0	0.0
16	1207	H-3	0.526E-07	0.0	0.0	0.0
16	2414	RA-226	0.426E-10	0.426E-10	0.221E-11	0.448E-10
16	2414	PB-210	0.0	0.0	0.0	0.0
16	2414	PO-210	0.852E-10	0.852E-10	0.443E-11	0.896E-10
16	2414	RN-222	0.114E-07	0.0	0.0	0.0
16	2414	H-3	0.114E-07	0.0	0.0	0.0
16	4023	RA-226	0.159E-10	0.159E-10	0.125E-11	0.172E-10
16	4023	PB-210	0.0	0.0	0.0	0.0
16	4023	PO-210	0.319E-10	0.319E-10	0.250E-11	0.344E-10
16	4023	RN-222	0.517E-08	0.0	0.0	0.0
16	4023	H-3	0.520E-08	0.0	0.0	0.0
16	5632	RA-226	0.869E-11	0.869E-11	0.863E-12	0.955E-11
16	5632	PB-210	0.0	0.0	0.0	0.0
16	5632	PO-210	0.174E-10	0.174E-10	0.173E-11	0.191E-10
16	5632	RN-222	0.318E-08	0.0	0.0	0.0
16	5632	H-3	0.320E-08	0.0	0.0	0.0
16	7241	RA-226	0.536E-11	0.536E-11	0.649E-12	0.601E-11
16	7241	PB-210	0.0	0.0	0.0	0.0

16	7241	PO-210	0.107E-10	0.107E-10	0.130E-11	0.120E-10
16	7241	RN-222	0.221E-08	0.0	0.0	0.0
16	7241	H-3	0.224E-08	0.0	0.0	0.0
16	12068	RA-226	0.218E-11	0.218E-11	0.368E-12	0.254E-11
16	12068	PB-210	0.0	0.0	0.0	0.0
16	12068	PO-210	0.435E-11	0.435E-11	0.737E-12	0.509E-11
16	12068	RN-222	0.111E-08	0.0	0.0	0.0
16	12068	H-3	0.113E-08	0.0	0.0	0.0
16	20113	RA-226	0.940E-12	0.940E-12	0.206E-12	0.115E-11
16	20113	PB-210	0.0	0.0	0.0	0.0
16	20113	PO-210	0.188E-11	0.188E-11	0.413E-12	0.229E-11
16	20113	RN-222	0.601E-09	0.0	0.0	0.0
16	20113	H-3	0.620E-09	0.0	0.0	0.0
16	32180	RA-226	0.416E-12	0.416E-12	0.118E-12	0.533E-12
16	32180	PB-210	0.0	0.0	0.0	0.0
16	32180	PO-210	0.831E-12	0.831E-12	0.236E-12	0.137E-11
16	32180	RN-222	0.343E-09	0.0	0.0	0.0
16	32180	H-3	0.360E-09	0.0	0.0	0.0
16	48270	RA-226	0.211E-12	0.211E-12	0.713E-13	0.282E-12
16	48270	PB-210	0.0	0.0	0.0	0.0
16	48270	PO-210	0.421E-12	0.421E-12	0.143E-12	0.564E-12
16	48270	RN-222	0.210E-09	0.0	0.0	0.0
16	48270	H-3	0.226E-09	0.0	0.0	0.0
16	64360	RA-226	0.113E-12	0.113E-12	0.478E-13	0.161E-12
16	64360	PB-210	0.0	0.0	0.0	0.0
16	64360	PO-210	0.227E-12	0.227E-12	0.956E-13	0.323E-12
16	64360	RN-222	0.147E-09	0.0	0.0	0.0
16	64360	H-3	0.163E-09	0.0	0.0	0.0
16	80450	RA-226	0.751E-13	0.751E-13	0.352E-13	0.110E-12
16	80450	PB-210	0.0	0.0	0.0	0.0
16	80450	PO-210	0.150E-12	0.150E-12	0.704E-13	0.221E-12
16	80450	RN-222	0.111E-09	0.0	0.0	0.0
16	80450	H-3	0.126E-09	0.0	0.0	0.0

GROUND-LEVEL CHI/Q VALUES FOR RA-226 AT VARIOUS DISTANCES IN EACH COMPASS DIRECTION

DISTANCE (METERS)	CHI/Q TOWARD INDICATED DIRECTION (SEC/CUBIC METER)							
	N	NNW	NW	WNW	W	WSW	SW	SSW
1207	0.921E-06	0.107E-05	0.127E-05	0.110E-05	0.684E-06	0.518E-06	0.640E-06	0.976E-06
2414	0.272E-06	0.210E-06	0.349E-06	0.280E-06	0.147E-06	0.951E-07	0.158E-06	0.185E-06
4023	0.977E-07	0.730E-07	0.120E-06	0.991E-07	0.534E-07	0.324E-07	0.527E-07	0.655E-07
5632	0.522E-07	0.383E-07	0.625E-07	0.527E-07	0.290E-07	0.169E-07	0.271E-07	0.348E-07
7241	0.312E-07	0.220E-07	0.356E-07	0.310E-07	0.176E-07	0.976E-08	0.152E-07	0.204E-07
12068	0.122E-07	0.821E-08	0.131E-07	0.119E-07	0.703E-08	0.367E-08	0.548E-08	0.786E-08
20113	0.509E-08	0.323E-08	0.504E-08	0.478E-08	0.292E-08	0.147E-08	0.212E-08	0.322E-08
32180	0.214E-08	0.121E-08	0.181E-08	0.187E-08	0.124E-08	0.592E-09	0.792E-09	0.127E-08
48270	0.106E-08	0.579E-09	0.852E-09	0.912E-09	0.615E-09	0.289E-09	0.381E-09	0.623E-09
64360	0.550E-09	0.265E-09	0.370E-09	0.448E-09	0.330E-09	0.142E-09	0.178E-09	0.283E-09
80450	0.357E-09	0.167E-09	0.230E-09	0.289E-09	0.217E-09	0.909E-10	0.112E-09	0.178E-09
	S	SSE	SE	ESE	E	ENE	NE	NNE
1207	0.131E-05	0.100E-05	0.674E-06	0.570E-06	0.515E-06	0.544E-06	0.544E-06	0.689E-06
2414	0.444E-06	0.207E-06	0.161E-06	0.141E-06	0.120E-06	0.132E-06	0.132E-06	0.134E-06
4023	0.164E-06	0.753E-07	0.587E-07	0.513E-07	0.439E-07	0.490E-07	0.490E-07	0.503E-07
5632	0.889E-07	0.405E-07	0.315E-07	0.275E-07	0.236E-07	0.265E-07	0.265E-07	0.274E-07
7241	0.536E-07	0.243E-07	0.190E-07	0.167E-07	0.143E-07	0.162E-07	0.162E-07	0.169E-07
12068	0.214E-07	0.950E-08	0.749E-08	0.660E-08	0.570E-08	0.649E-08	0.649E-08	0.686E-08
20113	0.896E-08	0.394E-08	0.315E-08	0.281E-08	0.245E-08	0.279E-08	0.279E-08	0.296E-08
32180	0.367E-08	0.161E-08	0.135E-08	0.123E-08	0.109E-08	0.123E-08	0.123E-08	0.131E-08
48270	0.182E-08	0.794E-09	0.679E-09	0.624E-09	0.558E-09	0.626E-09	0.626E-09	0.664E-09
64360	0.872E-09	0.398E-09	0.362E-09	0.340E-09	0.309E-09	0.343E-09	0.343E-09	0.358E-09
80450	0.558E-09	0.257E-09	0.238E-09	0.225E-09	0.205E-09	0.228E-09	0.228E-09	0.237E-09

GROUND-LEVEL CHI/Q VALUES FOR PB-210 AT VARIOUS DISTANCES IN EACH COMPASS DIRECTION

DISTANCE (METERS)	CHI/Q TOWARD INDICATED DIRECTION (SEC/CUBIC METER)							
	N	NNW	NW	WNW	W	WSW	SW	SSW
1207	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2414	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4023	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5632	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7241	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12068	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20113	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
32180	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
48270	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
64360	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80450	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

	S	SSE	SE	ESE	E	ENE	NE	NNE
1207	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2414	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
4023	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
5632	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
7241	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
12068	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
20113	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
32180	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
48270	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
64360	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
80450	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

GROUND-LEVEL CHI/Q VALUES FOR PO-210 AT VARIOUS DISTANCES IN EACH COMPASS DIRECTION

DISTANCE (METERS) — CHI/Q TOWARD INDICATED DIRECTION (SEC/CUBIC METER)

DISTANCE (METERS)	N	NNW	NW	WNW	W	WSW	SW	SSW
1207	0.921E-06	0.107E-05	0.127E-05	0.110E-05	0.684E-06	0.518E-06	0.640E-06	0.976E-06
2414	0.272E-06	0.210E-06	0.349E-06	0.280E-06	0.147E-06	0.951E-07	0.158E-06	0.185E-06
4023	0.977E-07	0.730E-07	0.120E-06	0.991E-07	0.534E-07	0.324E-07	0.527E-07	0.655E-07
5632	0.522E-07	0.383E-07	0.625E-07	0.527E-07	0.290E-07	0.169E-07	0.271E-07	0.348E-07
7241	0.312E-07	0.220E-07	0.356E-07	0.310E-07	0.176E-07	0.976E-08	0.152E-07	0.204E-07
12068	0.122E-07	0.821E-08	0.131E-07	0.119E-07	0.703E-08	0.367E-08	0.548E-08	0.786E-08
20113	0.509E-08	0.323E-08	0.504E-08	0.478E-08	0.292E-08	0.147E-08	0.212E-08	0.322E-08
32180	0.214E-08	0.121E-08	0.181E-08	0.187E-08	0.124E-08	0.592E-09	0.792E-09	0.127E-08
48270	0.106E-08	0.579E-09	0.852E-09	0.912E-09	0.615E-09	0.289E-09	0.381E-09	0.623E-09
64360	0.550E-09	0.265E-09	0.370E-09	0.448E-09	0.330E-09	0.142E-09	0.178E-09	0.283E-09
80450	0.357E-09	0.167E-09	0.230E-09	0.289E-09	0.217E-09	0.909E-10	0.112E-09	0.178E-09

DISTANCE (METERS)	S	SSE	SE	ESE	E	ENE	NE	NNE
1207	0.131E-05	0.100E-05	0.674E-06	0.570E-06	0.515E-06	0.544E-06	0.544E-06	0.689E-06
2414	0.444E-06	0.207E-06	0.161E-06	0.141E-06	0.120E-06	0.132E-06	0.132E-06	0.134E-06
4023	0.164E-06	0.753E-07	0.587E-07	0.513E-07	0.439E-07	0.490E-07	0.490E-07	0.503E-07
5632	0.889E-07	0.405E-07	0.315E-07	0.275E-07	0.236E-07	0.265E-07	0.265E-07	0.274E-07
7241	0.536E-07	0.243E-07	0.190E-07	0.167E-07	0.143E-07	0.162E-07	0.162E-07	0.169E-07
12068	0.214E-07	0.950E-08	0.749E-08	0.660E-08	0.570E-08	0.649E-08	0.649E-08	0.686E-08
20113	0.896E-08	0.394E-08	0.315E-08	0.281E-08	0.245E-08	0.279E-08	0.279E-08	0.296E-08
32180	0.367E-08	0.161E-08	0.135E-08	0.123E-08	0.109E-08	0.123E-08	0.123E-08	0.131E-08
48270	0.182E-08	0.794E-09	0.679E-09	0.624E-09	0.558E-09	0.626E-09	0.626E-09	0.664E-09
64360	0.872E-09	0.398E-09	0.362E-09	0.340E-09	0.309E-09	0.343E-09	0.343E-09	0.358E-09
80450	0.558E-09	0.257E-09	0.238E-09	0.225E-09	0.205E-09	0.228E-09	0.228E-09	0.237E-09

GROUND-LEVEL CHI/Q VALUES FOR RN-222 AT VARIOUS DISTANCES IN EACH COMPASS DIRECTION

CHI/Q TOWARD INDICATED DIRECTION (SEC/CUBIC METER)

DISTANCE (METERS)	N	NNW	NW	WNW	W	WSW	SW	SSW
1207	0.242E-05	0.301E-05	0.364E-05	0.315E-05	0.199E-05	0.163E-05	0.197E-05	0.256E-05
2414	0.917E-06	0.777E-06	0.136E-05	0.104E-05	0.534E-06	0.426E-06	0.697E-06	0.638E-06
4023	0.421E-06	0.360E-06	0.633E-06	0.482E-06	0.248E-06	0.198E-06	0.324E-06	0.296E-06
5632	0.261E-06	0.225E-06	0.396E-06	0.301E-06	0.154E-06	0.123E-06	0.202E-06	0.184E-06
7241	0.183E-06	0.158E-06	0.279E-06	0.212E-06	0.108E-06	0.866E-07	0.142E-06	0.129E-06
12068	0.923E-07	0.808E-07	0.143E-06	0.108E-06	0.551E-07	0.443E-07	0.727E-07	0.662E-07
20113	0.506E-07	0.448E-07	0.794E-07	0.599E-07	0.302E-07	0.245E-07	0.403E-07	0.367E-07
32180	0.290E-07	0.259E-07	0.460E-07	0.346E-07	0.173E-07	0.141E-07	0.233E-07	0.212E-07
48270	0.178E-07	0.160E-07	0.285E-07	0.213E-07	0.106E-07	0.867E-08	0.144E-07	0.131E-07
64360	0.125E-07	0.113E-07	0.201E-07	0.150E-07	0.743E-08	0.610E-08	0.102E-07	0.928E-08
80450	0.947E-08	0.858E-08	0.153E-07	0.114E-07	0.562E-08	0.461E-08	0.769E-08	0.705E-08

DISTANCE (METERS)	S	SSE	SE	ESE	E	ENE	NE	NNE
1207	0.313E-05	0.237E-05	0.163E-05	0.140E-05	0.123E-05	0.126E-05	0.126E-05	0.166E-05
2414	0.129E-05	0.610E-06	0.489E-06	0.443E-06	0.355E-06	0.370E-06	0.370E-06	0.359E-06
4023	0.596E-06	0.280E-06	0.223E-06	0.202E-06	0.161E-06	0.168E-06	0.168E-06	0.163E-06
5632	0.370E-06	0.174E-06	0.138E-06	0.125E-06	0.989E-07	0.103E-06	0.103E-06	0.100E-06
7241	0.260E-06	0.122E-06	0.961E-07	0.869E-07	0.688E-07	0.718E-07	0.718E-07	0.697E-07
12068	0.132E-06	0.615E-07	0.484E-07	0.437E-07	0.344E-07	0.359E-07	0.359E-07	0.349E-07
20113	0.726E-07	0.338E-07	0.264E-07	0.239E-07	0.188E-07	0.195E-07	0.195E-07	0.190E-07
32180	0.418E-07	0.194E-07	0.151E-07	0.137E-07	0.107E-07	0.112E-07	0.112E-07	0.108E-07
48270	0.258E-07	0.120E-07	0.929E-08	0.838E-08	0.658E-08	0.683E-08	0.683E-08	0.662E-08
64360	0.182E-07	0.845E-08	0.653E-08	0.588E-08	0.461E-08	0.479E-08	0.479E-08	0.464E-08
80450	0.139E-07	0.641E-08	0.494E-08	0.444E-08	0.349E-08	0.362E-08	0.362E-08	0.351E-08

GROUND-LEVEL CHI/Q VALUES FOR H-3 AT VARIOUS DISTANCES IN EACH COMPASS DIRECTION

DISTANCE (METERS) — CHI/Q TOWARD INDICATED DIRECTION (SEC/CUBIC METER)

DISTANCE (METERS)	N	NNW	NW	WNW	W	WSW	SW	SSW
1207	0.242E-05	0.301E-05	0.365E-05	0.316E-05	0.199E-05	0.164E-05	0.197E-05	0.256E-05
2414	0.921E-06	0.780E-06	0.137E-05	0.104E-05	0.536E-06	0.428E-06	0.699E-06	0.640E-06
4023	0.424E-06	0.363E-06	0.637E-06	0.485E-06	0.249E-06	0.199E-06	0.326E-06	0.297E-06
5632	0.263E-06	0.227E-06	0.399E-06	0.304E-06	0.156E-06	0.125E-06	0.204E-06	0.186E-06
7241	0.185E-06	0.160E-06	0.282E-06	0.214E-06	0.110E-06	0.878E-07	0.144E-06	0.131E-06
12068	0.942E-07	0.823E-07	0.146E-06	0.110E-06	0.562E-07	0.452E-07	0.742E-07	0.674E-07
20113	0.523E-07	0.462E-07	0.819E-07	0.618E-07	0.312E-07	0.254E-07	0.418E-07	0.378E-07
32180	0.306E-07	0.272E-07	0.483E-07	0.363E-07	0.183E-07	0.149E-07	0.246E-07	0.223E-07
48270	0.193E-07	0.172E-07	0.307E-07	0.230E-07	0.115E-07	0.947E-08	0.156E-07	0.141E-07
64360	0.140E-07	0.125E-07	0.222E-07	0.166E-07	0.830E-08	0.686E-08	0.113E-07	0.102E-07
80450	0.108E-07	0.972E-08	0.173E-07	0.130E-07	0.645E-08	0.534E-08	0.883E-08	0.796E-08

DISTANCE (METERS)	S	SSE	SE	ESE	E	ENE	NE	NNE
1207	0.314E-05	0.238E-05	0.164E-05	0.141E-05	0.123E-05	0.126E-05	0.126E-05	0.166E-05
2414	0.130E-05	0.612E-06	0.491E-06	0.445E-06	0.357E-06	0.371E-06	0.371E-06	0.361E-06
4023	0.599E-06	0.282E-06	0.225E-06	0.203E-06	0.162E-06	0.169E-06	0.169E-06	0.164E-06
5632	0.373E-06	0.175E-06	0.139E-06	0.126E-06	0.998E-07	0.104E-06	0.104E-06	0.101E-06
7241	0.262E-06	0.123E-06	0.972E-07	0.879E-07	0.696E-07	0.725E-07	0.725E-07	0.705E-07
12068	0.134E-06	0.626E-07	0.493E-07	0.446E-07	0.351E-07	0.366E-07	0.366E-07	0.355E-07
20113	0.747E-07	0.348E-07	0.273E-07	0.247E-07	0.194E-07	0.202E-07	0.202E-07	0.196E-07
32180	0.437E-07	0.204E-07	0.159E-07	0.144E-07	0.113E-07	0.117E-07	0.117E-07	0.114E-07
48270	0.276E-07	0.128E-07	0.100E-07	0.908E-08	0.713E-08	0.737E-08	0.737E-08	0.713E-08
64360	0.199E-07	0.927E-08	0.723E-08	0.655E-08	0.514E-08	0.531E-08	0.531E-08	0.513E-08
80450	0.155E-07	0.720E-08	0.561E-08	0.509E-08	0.399E-08	0.412E-08	0.412E-08	0.398E-08

OPTIONS SELECTED FOR DOSE AND INTAKE CALCULATIONS

CALCULATIONS ARE MADE FOR THE POPULATION.
TABLES FOR EACH NUCLIDE LISTING DOSES BY ORGAN AND PATHWAY AT EACH ENVIRONMENTAL LOCATION ARE OMITTED.
ENVIRONMENTAL CONCENTRATIONS AND INTAKE RATES BY MAN FOR EACH NUCLIDE ARE PRINTED AND WRITTEN UNFORMATTED.
DOSE SUMMARY TABLES ARE PRINTED
WORKING LEVELS ARE CALCULATED FOR RN-222 IF IT IS IN THE SOURCE TERM

SUMMARY OF AREA SURROUNDING PLANT

AREA COLUMN	ROW	NO. MEAT ANIMALS	NO. MILK CATTLE	FOOD CROPS (SQUARE METERS)	WATER AREA	POPULATION
1	1	10000	10000	0.100E 21	0	0.0
1	2	10000	10000	0.100E 21	0	0.0
1	3	10000	10000	0.100E 21	0	0.0
1	4	10000	10000	0.100E 21	0	0.0
1	5	10000	10000	0.100E 21	0	0.0
1	6	10000	10000	0.100E 21	0	38.0
1	7	10000	10000	0.100E 21	0	0.0
1	8	10000	10000	0.100E 21	0	0.0
1	9	10000	10000	0.100E 21	0	5.0
1	10	10000	10000	0.100E 21	0	306.0
1	11	10000	10000	0.100E 21	0	2330.0
1	12	10000	10000	0.100E 21	0	0.0
1	13	10000	10000	0.100E 21	0	0.0
1	14	10000	10000	0.100E 21	0	0.0
1	15	10000	10000	0.100E 21	0	0.0
1	16	10000	10000	0.100E 21	0	0.0
1	17	10000	10000	0.100E 21	0	0.0
1	18	10000	10000	0.100E 21	0	0.0
1	19	10000	10000	0.100E 21	0	0.0
1	20	10000	10000	0.100E 21	0	0.0
2	1	10000	10000	0.100E 21	0	0.0
2	2	10000	10000	0.100E 21	0	0.0
2	3	10000	10000	0.100E 21	0	0.0
2	4	10000	10000	0.100E 21	0	0.0
2	5	10000	10000	0.100E 21	0	0.0
2	6	10000	10000	0.100E 21	0	0.0
2	7	10000	10000	0.100E 21	0	197.0
2	8	10000	10000	0.100E 21	0	91.0
2	9	10000	10000	0.100E 21	0	410.0
2	10	10000	10000	0.100E 21	0	197.0
2	11	10000	10000	0.100E 21	0	181.0
2	12	10000	10000	0.100E 21	0	0.0
2	13	10000	10000	0.100E 21	0	0.0
2	14	10000	10000	0.100E 21	0	0.0
2	15	10000	10000	0.100E 21	0	0.0
2	16	10000	10000	0.100E 21	0	0.0
2	17	10000	10000	0.100E 21	0	0.0
2	18	10000	10000	0.100E 21	0	0.0
2	19	10000	10000	0.100E 21	0	0.0
2	20	10000	10000	0.100E 21	0	0.0
3	1	10000	10000	0.100E 21	0	0.0
3	2	10000	10000	0.100E 21	0	0.0
3	3	10000	10000	0.100E 21	0	0.0
3	4	10000	10000	0.100E 21	0	0.0
3	5	10000	10000	0.100E 21	0	0.0
3	6	10000	10000	0.100E 21	0	0.0
3	7	10000	10000	0.100E 21	0	0.0
3	8	10000	10000	0.100E 21	0	0.0
3	9	10000	10000	0.100E 21	0	643.0

3	10	10000	10000	0.100E 21	0	858.0
3	11	10000	10000	0.100E 21	0	365.0
3	12	10000	10000	0.100E 21	0	0.0
3	13	10000	10000	0.100E 21	0	0.0
3	14	10000	10000	0.100E 21	0	0.0
3	15	10000	10000	0.100E 21	0	0.0
3	16	10000	10000	0.100E 21	0	0.0
3	17	10000	10000	0.100E 21	0	0.0
3	18	10000	10000	0.100E 21	0	0.0
3	19	10000	10000	0.100E 21	0	0.0
3	20	10000	10000	0.100E 21	0	0.0
4	1	10000	10000	0.100E 21	0	0.0
4	2	10000	10000	0.100E 21	0	0.0
4	3	10000	10000	0.100E 21	0	0.0
4	4	10000	10000	0.100E 21	0	0.0
4	5	10000	10000	0.100E 21	0	0.0
4	6	10000	10000	0.100E 21	0	0.0
4	7	10000	10000	0.100E 21	0	102.0
4	8	10000	10000	0.100E 21	0	135.0
4	9	10000	10000	0.100E 21	0	338.0
4	10	10000	10000	0.100E 21	0	2954.0
4	11	10000	10000	0.100E 21	0	4881.0
4	12	10000	10000	0.100E 21	0	0.0
4	13	10000	10000	0.100E 21	0	0.0
4	14	10000	10000	0.100E 21	0	0.0
4	15	10000	10000	0.100E 21	0	0.0
4	16	10000	10000	0.100E 21	0	0.0
4	17	10000	10000	0.100E 21	0	0.0
4	18	10000	10000	0.100E 21	0	0.0
4	19	10000	10000	0.100E 21	0	0.0
4	20	10000	10000	0.100E 21	0	0.0
5	1	10000	10000	0.100E 21	0	0.0
5	2	10000	10000	0.100E 21	0	0.0
5	3	10000	10000	0.100E 21	0	0.0
5	4	10000	10000	0.100E 21	0	0.0
5	5	10000	10000	0.100E 21	0	0.0
5	6	10000	10000	0.100E 21	0	97.0
5	7	10000	10000	0.100E 21	0	197.0
5	8	10000	10000	0.100E 21	0	0.0
5	9	10000	10000	0.100E 21	0	79.0
5	10	10000	10000	0.100E 21	0	69.0
5	11	10000	10000	0.100E 21	0	4185.0
5	12	10000	10000	0.100E 21	0	0.0
5	13	10000	10000	0.100E 21	0	0.0
5	14	10000	10000	0.100E 21	0	0.0
5	15	10000	10000	0.100E 21	0	0.0
5	16	10000	10000	0.100E 21	0	0.0
5	17	10000	10000	0.100E 21	0	0.0
5	18	10000	10000	0.100E 21	0	0.0
5	19	10000	10000	0.100E 21	0	0.0
5	20	10000	10000	0.100E 21	0	0.0
6	1	10000	10000	0.100E 21	0	0.0
6	2	10000	10000	0.100E 21	0	191.0
6	3	10000	10000	0.100E 21	0	0.0
6	4	10000	10000	0.100E 21	0	0.0
6	5	10000	10000	0.100E 21	0	0.0
6	6	10000	10000	0.100E 21	0	0.0
6	7	10000	10000	0.100E 21	0	0.0
6	8	10000	10000	0.100E 21	0	168.0
6	9	10000	10000	0.100E 21	0	181.0
6	10	10000	10000	0.100E 21	0	5578.0
6	11	10000	10000	0.100E 21	0	5226.0
6	12	10000	10000	0.100E 21	0	0.0
6	13	10000	10000	0.100E 21	0	0.0
6	14	10000	10000	0.100E 21	0	0.0
6	15	10000	10000	0.100E 21	0	0.0

6	16	10000	10000	0.100E 21	0	0.0
6	17	10000	10000	0.100E 21	0	0.0
6	18	10000	10000	0.100E 21	0	0.0
6	19	10000	10000	0.100E 21	0	0.0
6	20	10000	10000	0.100E 21	0	0.0
7	1	10000	10000	0.100E 21	0	0.0
7	2	10000	10000	0.100E 21	0	0.0
7	3	10000	10000	0.100E 21	0	0.0
7	4	10000	10000	0.100E 21	0	0.0
7	5	10000	10000	0.100E 21	0	0.0
7	6	10000	10000	0.100E 21	0	0.0
7	7	10000	10000	0.100E 21	0	0.0
7	8	10000	10000	0.100E 21	0	303.0
7	9	10000	10000	0.100E 21	0	179.0
7	10	10000	10000	0.100E 21	0	466.0
7	11	10000	10000	0.100E 21	0	92.0
7	12	10000	10000	0.100E 21	0	0.0
7	13	10000	10000	0.100E 21	0	0.0
7	14	10000	10000	0.100E 21	0	0.0
7	15	10000	10000	0.100E 21	0	0.0
7	16	10000	10000	0.100E 21	0	0.0
7	17	10000	10000	0.100E 21	0	0.0
7	18	10000	10000	0.100E 21	0	0.0
7	19	10000	10000	0.100E 21	0	0.0
7	20	10000	10000	0.100E 21	0	0.0
8	1	10000	10000	0.100E 21	0	0.0
8	2	10000	10000	0.100E 21	0	0.0
8	3	10000	10000	0.100E 21	0	0.0
8	4	10000	10000	0.100E 21	0	0.0
8	5	10000	10000	0.100E 21	0	0.0
8	6	10000	10000	0.100E 21	0	0.0
8	7	10000	10000	0.100E 21	0	327.0
8	8	10000	10000	0.100E 21	0	580.0
8	9	10000	10000	0.100E 21	0	280.0
8	10	10000	10000	0.100E 21	0	206.0
8	11	10000	10000	0.100E 21	0	0.0
8	12	10000	10000	0.100E 21	0	0.0
8	13	10000	10000	0.100E 21	0	0.0
8	14	10000	10000	0.100E 21	0	0.0
8	15	10000	10000	0.100E 21	0	0.0
8	16	10000	10000	0.100E 21	0	0.0
8	17	10000	10000	0.100E 21	0	0.0
8	18	10000	10000	0.100E 21	0	0.0
8	19	10000	10000	0.100E 21	0	0.0
8	20	10000	10000	0.100E 21	0	0.0
9	1	10000	10000	0.100E 21	0	0.0
9	2	10000	10000	0.100E 21	0	0.0
9	3	10000	10000	0.100E 21	0	0.0
9	4	10000	10000	0.100E 21	0	0.0
9	5	10000	10000	0.100E 21	0	0.0
9	6	10000	10000	0.100E 21	0	0.0
9	7	10000	10000	0.100E 21	0	0.0
9	8	10000	10000	0.100E 21	0	1931.0
9	9	10000	10000	0.100E 21	0	0.0
9	10	10000	10000	0.100E 21	0	225.0
9	11	10000	10000	0.100E 21	0	0.0
9	12	10000	10000	0.100E 21	0	0.0
9	13	10000	10000	0.100E 21	0	0.0
9	14	10000	10000	0.100E 21	0	0.0
9	15	10000	10000	0.100E 21	0	0.0
9	16	10000	10000	0.100E 21	0	0.0
9	17	10000	10000	0.100E 21	0	0.0
9	18	10000	10000	0.100E 21	0	0.0
9	19	10000	10000	0.100E 21	0	0.0
9	20	10000	10000	0.100E 21	0	0.0
10	1	10000	10000	0.100E 21	0	0.0

10	2	10000	10000	0.100E 21	0	0.0
10	3	10000	10000	0.100E 21	0	0.0
10	4	10000	10000	0.100E 21	0	0.0
10	5	10000	10000	0.100E 21	0	0.0
10	6	10000	10000	0.100E 21	0	1196.0
10	7	10000	10000	0.100E 21	0	0.0
10	8	10000	10000	0.100E 21	0	772.0
10	9	10000	10000	0.100E 21	0	365.0
10	10	10000	10000	0.100E 21	0	268.0
10	11	10000	10000	0.100E 21	0	353.0
10	12	10000	10000	0.100E 21	0	0.0
10	13	10000	10000	0.100E 21	0	0.0
10	14	10000	10000	0.100E 21	0	0.0
10	15	10000	10000	0.100E 21	0	0.0
10	16	10000	10000	0.100E 21	0	0.0
10	17	10000	10000	0.100E 21	0	0.0
10	18	10000	10000	0.100E 21	0	0.0
10	19	10000	10000	0.100E 21	0	0.0
10	20	10000	10000	0.100E 21	0	0.0
11	1	10000	10000	0.100E 21	0	0.0
11	2	10000	10000	0.100E 21	0	0.0
11	3	10000	10000	0.100E 21	0	0.0
11	4	10000	10000	0.100E 21	0	0.0
11	5	10000	10000	0.100E 21	0	0.0
11	6	10000	10000	0.100E 21	0	995.0
11	7	10000	10000	0.100E 21	0	164.0
11	8	10000	10000	0.100E 21	0	0.0
11	9	10000	10000	0.100E 21	0	411.0
11	10	10000	10000	0.100E 21	0	295.0
11	11	10000	10000	0.100E 21	0	7.0
11	12	10000	10000	0.100E 21	0	0.0
11	13	10000	10000	0.100E 21	0	0.0
11	14	10000	10000	0.100E 21	0	0.0
11	15	10000	10000	0.100E 21	0	0.0
11	16	10000	10000	0.100E 21	0	0.0
11	17	10000	10000	0.100E 21	0	0.0
11	18	10000	10000	0.100E 21	0	0.0
11	19	10000	10000	0.100E 21	0	0.0
11	20	10000	10000	0.100E 21	0	0.0
12	1	10000	10000	0.100E 21	0	0.0
12	2	10000	10000	0.100E 21	0	0.0
12	3	10000	10000	0.100E 21	0	0.0
12	4	10000	10000	0.100E 21	0	0.0
12	5	10000	10000	0.100E 21	0	0.0
12	6	10000	10000	0.100E 21	0	0.0
12	7	10000	10000	0.100E 21	0	426.0
12	8	10000	10000	0.100E 21	0	0.0
12	9	10000	10000	0.100E 21	0	483.0
12	10	10000	10000	0.100E 21	0	193.0
12	11	10000	10000	0.100E 21	0	328.0
12	12	10000	10000	0.100E 21	0	0.0
12	13	10000	10000	0.100E 21	0	0.0
12	14	10000	10000	0.100E 21	0	0.0
12	15	10000	10000	0.100E 21	0	0.0
12	16	10000	10000	0.100E 21	0	0.0
12	17	10000	10000	0.100E 21	0	0.0
12	18	10000	10000	0.100E 21	0	0.0
12	19	10000	10000	0.100E 21	0	0.0
12	20	10000	10000	0.100E 21	0	0.0
13	1	10000	10000	0.100E 21	0	0.0
13	2	10000	10000	0.100E 21	0	0.0
13	3	10000	10000	0.100E 21	0	0.0
13	4	10000	10000	0.100E 21	0	0.0
13	5	10000	10000	0.100E 21	0	0.0
13	6	10000	10000	0.100E 21	0	0.0
13	7	10000	10000	0.100E 21	0	71.0

13	8	10000	10000	0.100E 21	0	0.0
13	9	10000	10000	0.100E 21	0	58.0
13	10	10000	10000	0.100E 21	0	39.0
13	11	10000	10000	0.100E 21	0	755.0
13	12	10000	10000	0.100E 21	0	0.0
13	13	10000	10000	0.100E 21	0	0.0
13	14	10000	10000	0.100E 21	0	0.0
13	15	10000	10000	0.100E 21	0	0.0
13	16	10000	10000	0.100E 21	0	0.0
13	17	10000	10000	0.100E 21	0	0.0
13	18	10000	10000	0.100E 21	0	0.0
13	19	10000	10000	0.100E 21	0	0.0
13	20	10000	10000	0.100E 21	0	0.0
14	1	10000	10000	0.100E 21	0	0.0
14	2	10000	10000	0.100E 21	0	0.0
14	3	10000	10000	0.100E 21	0	0.0
14	4	10000	10000	0.100E 21	0	0.0
14	5	10000	10000	0.100E 21	0	0.0
14	6	10000	10000	0.100E 21	0	0.0
14	7	10000	10000	0.100E 21	0	0.0
14	8	10000	10000	0.100E 21	0	105.0
14	9	10000	10000	0.100E 21	0	91.0
14	10	10000	10000	0.100E 21	0	909.0
14	11	10000	10000	0.100E 21	0	2232.0
14	12	10000	10000	0.100E 21	0	0.0
14	13	10000	10000	0.100E 21	0	0.0
14	14	10000	10000	0.100E 21	0	0.0
14	15	10000	10000	0.100E 21	0	0.0
14	16	10000	10000	0.100E 21	0	0.0
14	17	10000	10000	0.100E 21	0	0.0
14	18	10000	10000	0.100E 21	0	0.0
14	19	10000	10000	0.100E 21	0	0.0
14	20	10000	10000	0.100E 21	0	0.0
15	1	10000	10000	0.100E 21	0	0.0
15	2	10000	10000	0.100E 21	0	0.0
15	3	10000	10000	0.100E 21	0	0.0
15	4	10000	10000	0.100E 21	0	0.0
15	5	10000	10000	0.100E 21	0	0.0
15	6	10000	10000	0.100E 21	0	0.0
15	7	10000	10000	0.100E 21	0	0.0
15	8	10000	10000	0.100E 21	0	0.0
15	9	10000	10000	0.100E 21	0	80.0
15	10	10000	10000	0.100E 21	0	194.0
15	11	10000	10000	0.100E 21	0	1197.0
15	12	10000	10000	0.100E 21	0	0.0
15	13	10000	10000	0.100E 21	0	0.0
15	14	10000	10000	0.100E 21	0	0.0
15	15	10000	10000	0.100E 21	0	0.0
15	16	10000	10000	0.100E 21	0	0.0
15	17	10000	10000	0.100E 21	0	0.0
15	18	10000	10000	0.100E 21	0	0.0
15	19	10000	10000	0.100E 21	0	0.0
15	20	10000	10000	0.100E 21	0	0.0
16	1	10000	10000	0.100E 21	0	0.0
16	2	10000	10000	0.100E 21	0	0.0
16	3	10000	10000	0.100E 21	0	0.0
16	4	10000	10000	0.100E 21	0	146.0
16	5	10000	10000	0.100E 21	0	0.0
16	6	10000	10000	0.100E 21	0	0.0
16	7	10000	10000	0.100E 21	0	0.0
16	8	10000	10000	0.100E 21	0	0.0
16	9	10000	10000	0.100E 21	0	67.0
16	10	10000	10000	0.100E 21	0	259.0
16	11	10000	10000	0.100E 21	0	6053.0
16	12	10000	10000	0.100E 21	0	0.0
16	13	10000	10000	0.100E 21	0	0.0

16	14	10000	10000	0.100E 21	0	0.0
16	15	10000	10000	0.100E 21	0	0.0
16	16	10000	10000	0.100E 21	0	0.0
16	17	10000	10000	0.100E 21	0	0.0
16	18	10000	10000	0.100E 21	0	0.0
16	19	10000	10000	0.100E 21	0	0.0
16	20	10000	10000	0.100E 21	0	0.0
17	1	10000	10000	0.100E 21	0	0.0
17	2	10000	10000	0.100E 21	0	0.0
17	3	10000	10000	0.100E 21	0	0.0
17	4	10000	10000	0.100E 21	0	0.0
17	5	10000	10000	0.100E 21	0	0.0
17	6	10000	10000	0.100E 21	0	0.0
17	7	10000	10000	0.100E 21	0	0.0
17	8	10000	10000	0.100E 21	0	0.0
17	9	10000	10000	0.100E 21	0	0.0
17	10	10000	10000	0.100E 21	0	0.0
17	11	10000	10000	0.100E 21	0	0.0
17	12	10000	10000	0.100E 21	0	0.0
17	13	10000	10000	0.100E 21	0	0.0
17	14	10000	10000	0.100E 21	0	0.0
17	15	10000	10000	0.100E 21	0	0.0
17	16	10000	10000	0.100E 21	0	0.0
17	17	10000	10000	0.100E 21	0	0.0
17	18	10000	10000	0.100E 21	0	0.0
17	19	10000	10000	0.100E 21	0	0.0
17	20	10000	10000	0.100E 21	0	0.0
18	1	10000	10000	0.100E 21	0	0.0
18	2	10000	10000	0.100E 21	0	0.0
18	3	10000	10000	0.100E 21	0	0.0
18	4	10000	10000	0.100E 21	0	0.0
18	5	10000	10000	0.100E 21	0	0.0
18	6	10000	10000	0.100E 21	0	0.0
18	7	10000	10000	0.100E 21	0	0.0
18	8	10000	10000	0.100E 21	0	0.0
18	9	10000	10000	0.100E 21	0	0.0
18	10	10000	10000	0.100E 21	0	0.0
18	11	10000	10000	0.100E 21	0	0.0
18	12	10000	10000	0.100E 21	0	0.0
18	13	10000	10000	0.100E 21	0	0.0
18	14	10000	10000	0.100E 21	0	0.0
18	15	10000	10000	0.100E 21	0	0.0
18	16	10000	10000	0.100E 21	0	0.0
18	17	10000	10000	0.100E 21	0	0.0
18	18	10000	10000	0.100E 21	0	0.0
18	19	10000	10000	0.100E 21	0	0.0
18	20	10000	10000	0.100E 21	0	0.0
19	1	10000	10000	0.100E 21	0	0.0
19	2	10000	10000	0.100E 21	0	0.0
19	3	10000	10000	0.100E 21	0	0.0
19	4	10000	10000	0.100E 21	0	0.0
19	5	10000	10000	0.100E 21	0	0.0
19	6	10000	10000	0.100E 21	0	0.0
19	7	10000	10000	0.100E 21	0	0.0
19	8	10000	10000	0.100E 21	0	0.0
19	9	10000	10000	0.100E 21	0	0.0
19	10	10000	10000	0.100E 21	0	0.0
19	11	10000	10000	0.100E 21	0	0.0
19	12	10000	10000	0.100E 21	0	0.0
19	13	10000	10000	0.100E 21	0	0.0
19	14	10000	10000	0.100E 21	0	0.0
19	15	10000	10000	0.100E 21	0	0.0
19	16	10000	10000	0.100E 21	0	0.0
19	17	10000	10000	0.100E 21	0	0.0
19	18	10000	10000	0.100E 21	0	0.0
19	19	10000	10000	0.100E 21	0	0.0

19	20	10000	10000	0.100E 21	0	0.0
20	1	10000	10000	0.100E 21	0	0.0
20	2	10000	10000	0.100E 21	0	0.0
20	3	10000	10000	0.100E 21	0	0.0
20	4	10000	10000	0.100E 21	0	0.0
20	5	10000	10000	0.100E 21	0	0.0
20	6	10000	10000	0.100E 21	0	0.0
20	7	10000	10000	0.100E 21	0	0.0
20	8	10000	10000	0.100E 21	0	0.0
20	9	10000	10000	0.100E 21	0	0.0
20	10	10000	10000	0.100E 21	0	0.0
20	11	10000	10000	0.100E 21	0	0.0
20	12	10000	10000	0.100E 21	0	0.0
20	13	10000	10000	0.100E 21	0	0.0
20	14	10000	10000	0.100E 21	0	0.0
20	15	10000	10000	0.100E 21	0	0.0
20	16	10000	10000	0.100E 21	0	0.0
20	17	10000	10000	0.100E 21	0	0.0
20	18	10000	10000	0.100E 21	0	0.0
20	19	10000	10000	0.100E 21	0	0.0
20	20	10000	10000	0.100E 21	0	0.0

FOR WATER AREAS--0= NONE OR MINIMAL AND 1= MAJOR WATER AREA PRESENT

LIST OF INPUT VALUES FOR RADIONUCLIDE-INDEPENDENT VARIABLES

NUMBER OF NUCLIDES CONSIDERED	5
TIME DELAY--INGESTION OF PASTURE GRASS BY ANIMALS (HR)	0.0
TIME DELAY--INGESTION OF STORED FEED BY ANIMALS (HR)	0.2160E 04
TIME DELAY--INGESTION OF LEAFY VEGETABLES BY MAN (HR)	0.3360E 03
TIME DELAY--INGESTION OF PRODUCE BY MAN (HR)	0.3360E 03
REMOVAL RATE CONSTANT FOR PHYSICAL LOSS BY WEATHERING (PER HOUR)	0.2100E-02
PERIOD OF EXPOSURE DURING GROWING SEASON--PASTURE GRASS (HR)	0.7200E 03
PERIOD OF EXPOSURE DURING GROWING SEASON--CROPS OR LEAFY VEGETABLES (HR)	0.1440E 04
AGRICULTURAL PRODUCTIVITY BY UNIT AREA (GRASS-COW-MILK-MAN PATHWAY (KG/SQ. METER))	0.2800E 00
AGRICULTURAL PRODUCTIVITY BY UNIT AREA (PRODUCE OR LEAFY VEG INGESTED BY MAN (KG/SQ. METER))	0.7160E 00
FRACTION OF YEAR ANIMALS GRAZE ON PASTURE	0.4000E 00
FRACTION OF DAILY FEED THAT IS PASTURE GRASS WHEN ANIMAL GRAZES ON PASTURE	0.4300E 00
CONSUMPTION RATE OF CONTAMINATED FEED OR FORAGE BY AN ANIMAL IN KG/DAY (DRY WEIGHT)	0.1560E 02
TRANSPORT TIME FROM ANIMAL FEED-MILK-MAN (DAY)	0.2000E 01
RATE OF INGESTION OF PRODUCE BY MAN (KG/YR)	0.1760E 03
RATE OF INGESTION OF MILK BY MAN (LITERS/YR)	0.1120E 03
RATE OF INGESTION OF MEAT BY MAN (KG/YR)	0.9400E 02
RATE OF INGESTION OF LEAFY VEGETABLES BY MAN (KG/YR)	0.1800E 02
AVERAGE TIME FROM SLAUGHTER OF MEAT ANIMAL TO CONSUMPTION (DAY)	0.2000E 02
FRACTION OF PRODUCE INGESTED GROWN IN GARDEN OF INTEREST	0.1000E 01
FRACTION OF LEAFY VEGETABLES GROWN IN GARDEN OF INTEREST	0.1000E 01
PERIOD OF LONG-TERM BUILDUP FOR ACTIVITY IN SOIL (YEARS)	0.1000E 03
EFFECTIVE SURFACE DENSITY OF SOIL (KG/SQ. M, DRY WEIGHT) (ASSUMES 15 CM PLOW LAYER)	0.2150E 03
VEGETABLE INGESTION RATIO-IMMEDIATE SURROUNDING AREA/TOTAL WITHIN AREA	0.5000E 00
MEAT INGESTION RATIO-IMMEDIATE SURROUNDING AREA/TOTAL WITHIN AREA	0.5000E 00
MILK INGESTION RATIO-IMMEDIATE SURROUNDING AREA/TOTAL WITHIN AREA	0.5000E 00

MINIMUM FRACTIONS OF FOOD TYPES FROM OUTSIDE AREA LISTED BELOW ARE ACTUAL FIXED VALUES

MINIMUM FRACTION VEGETABLES INGESTED FROM OUTSIDE AREA	0.2000E 00
MINIMUM FRACTION MEAT INGESTED FROM OUTSIDE AREA	0.2000E 00
MINIMUM FRACTION MILK INGESTED FROM OUTSIDE AREA	0.2000E 00

INHALATION RATE OF MAN (CUBIC CENTIMETERS/HR)	0.9167E 06
BUILDUP TIME FOR RADIONUCLIDES DEPOSITED ON GROUND AND WATER (DAYS)	0.3650E 05
DILUTION FACTOR FOR WATER FOR SWIMMING (CM)	0.1524E 03
FRACTION OF TIME SPENT SWIMMING	0.1000E-01
MUSCLE MASS OF ANIMAL AT SLAUGHTER (KG)	0.2000E 03
FRACTION OF ANIMAL HERD SLAUGHTERED PER DAY	0.3810E-02
MILK PRODUCTION OF COW (LITERS/DAY)	0.1100E 02
FALLOUT INTERCEPTION FRACTION-VEGETABLES	0.2000E 00
FALLOUT INTERCEPTION FRACTION-PASTURE	0.5700E 00
FRACTION OF RADIOACTIVITY RETAINED ON LEAFY VEGETABLES AND PRODUCE AFTER WASHING	0.1000E 01

COMPUTED VALUES FOR THE AREA

TOTAL POPULATION	53103.0
TOTAL NUMBER OF MEAT ANIMALS	1760000
TOTAL NUMBER OF MILK CATTLE	1760000
TOTAL AREA OF VEGETABLE FOOD CROPS (SQUARE METERS)	0.1760E 23
TOTAL MEAT CONSUMPTION (KG PER YEAR)	0.4992E 07
TOTAL MEAT PRODUCTION (KG PER YEAR)	0.4895E 09
TOTAL MILK CONSUMPTION (LITERS/YEAR)	0.5948E 07
TOTAL MILK PRODUCTION (LITERS/YEAR)	0.7066E 10
TOTAL VEGETABLE FOOD CONSUMPTION (KG PER YEAR)	0.1030E 08
TOTAL VEGETABLE FOOD PRODUCED (KG PER YEAR)	0.1260E 23

LIST OF INPUT DATA FOR NUCLIDE RA-226

RADIOACTIVE DECAY CONSTANT (PER DAY)	0.1190E-05
ENVIRONMENTAL DECAY CONSTANT--SURFACE (PER DAY)	0.0
ENVIRONMENTAL DECAY CONSTANT--WATER (PER DAY)	0.0
AVERAGE FRACTION OF ANIMAL'S DAILY INTAKE OF NUCLIDE WHICH APPEARS IN EACH L OF MILK (DAYS/L)	0.5900E-03
FRACTION OF ANIMAL'S DAILY INTAKE OF NUCLIDE WHICH APPEARS IN EACH KG OF FLESH (DAYS/KG)	0.3000E-02
CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SOIL FOR PASTURE AND FORAGE (IN PCI/KG DRY WEIGHT PER PCI/KG DRY SOIL)	0.9700E-01
CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SOIL BY EDIBLE PARTS OF CROPS (IN PCI/KG WET WEIGHT PER PCI/KG DRY SOIL)	0.6200E-01
GI UPTAKE FRACTION (INHALATION)	0.2000E 00
GI UPTAKE FRACTION (INGESTION)	0.2000E 00
PARTICLE SIZE (MICRONS)	0.1000E 01
SOLUBILITY CLASS	W

DOSE CONVERSION FACTORS

ORGAN	INHALATION (REMS/MICROCURIE)	INGESTION (REMS/MICROCURIE)	SUBMERSION IN AIR (REMS-CUBIC CM/ MICROCURIE-HR)	SURFACE EXPOSURE (REMS-SQUARE CM/ MICROCURIE-HR)	SUBMERSION IN WATER (REMS-CUBIC CM/ MICROCURIE-HR)
TOT. BODY	0.901E 01	0.726E 01	0.436E 01	0.100E-02	0.936E-02
S WALL	0.270E-02	0.437E-02	0.284E 01	0.654E-03	0.610E-02
LLI WALL	0.179E 00	0.333E 00	0.239E 01	0.548E-03	0.512E-02
LUNGS	0.557E 02	0.515E-04	0.385E 01	0.884E-03	0.825E-02
KIDNEYS	0.662E 00	0.590E 00	0.315E 01	0.725E-03	0.676E-02
LIVER	0.662E 00	0.590E 00	0.333E 01	0.764E-03	0.713E-02
OVARIES	0.664E 00	0.592E 00	0.229E 01	0.526E-03	0.491E-02
R MAR	0.192E 01	0.171E 01	0.626E 01	0.144E-02	0.134E-01
ENDOST	0.990E 01	0.882E 01	0.726E 01	0.167E-02	0.156E-01
TESTES	0.664E 00	0.591E 00	0.532E 01	0.122E-02	0.114E-01
THYROID	0.664E 00	0.591E 00	0.435E 01	0.100E-02	0.934E-02

LIST OF INPUT DATA FOR NUCLIDE PB-210

RADIOACTIVE DECAY CONSTANT (PER DAY)	0.8520E-04
ENVIRONMENTAL DECAY CONSTANT--SURFACE (PER DAY)	0.0
ENVIRONMENTAL DECAY CONSTANT--WATER (PER DAY)	0.0
AVERAGE FRACTION OF ANIMAL'S DAILY INTAKE OF NUCLIDE WHICH APPEARS IN EACH L OF MILK (DAYS/L)	0.9900E-04
FRACTION OF ANIMAL'S DAILY INTAKE OF NUCLIDE WHICH APPEARS IN EACH KG OF FLESH (DAYS/KG)	0.9100E-03
CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SOIL FOR PASTURE AND FORAGE (IN PCI/KG DRY WEIGHT PER PCI/KG DRY SOIL)	0.1100E 00
CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SOIL BY EDIBLE PARTS OF CROPS (IN PCI/KG WET WEIGHT PER PCI/KG DRY SOIL)	0.3900E-02
GI UPTAKE FRACTION (INHALATION)	0.8000E-01
GI UPTAKE FRACTION (INGESTION)	0.8000E-01
PARTICLE SIZE (MICRONS)	0.1000E 01
SOLUBILITY CLASS	W

CONCENTRATIONS ON GROUND AND WATER INCLUDE CONTRIBUTIONS RESULTING FROM DECAY OF THE FOLLOWING PARENT NUCLIDES AFTER DEPOSITION--

NUCLIDE	BUILDUP FACTOR
RA-226	0.221E 01

DOSE CONVERSION FACTORS

ORGAN	INHALATION (REMS/MICROCURIE)	INGESTION (REMS/MICROCURIE)	SUBMERSION IN AIR (REMS-CUBIC CM/ MICROCURIE-HR)	SURFACE EXPOSURE (REMS-SQUARE CM/ MICROCURIE-HR)	SUBMERSION IN WATER (REMS-CUBIC CM/ MICROCURIE-HR)
TOT. BODY	0.150E 02	0.733E 01	0.863E 00	0.874E-03	0.200E-02
S WALL	0.118E-02	0.189E-03	0.478E 00	0.484E-03	0.111E-02
LLI WALL	0.469E-01	0.203E-01	0.272E 00	0.275E-03	0.630E-03
LUNGS	0.618E 01	0.574E-04	0.563E 00	0.570E-03	0.131E-02
KIDNEYS	0.754E 01	0.303E 01	0.497E 00	0.504E-03	0.115E-02
LIVER	0.309E 01	0.144E 01	0.449E 00	0.455E-03	0.104E-02
OVARIES	0.120E 00	0.303E-01	0.454E 00	0.460E-03	0.105E-02
R MAR	0.294E 01	0.142E 01	0.136E 01	0.138E-02	0.315E-02
ENDOST	0.195E 02	0.964E 01	0.180E 01	0.183E-02	0.418E-02
TESTES	0.120E 00	0.303E-01	0.768E 00	0.778E-03	0.178E-02
THYROID	0.120E 00	0.303E-01	0.839E 00	0.849E-03	0.194E-02

LIST OF INPUT DATA FOR NUCLIDE PO-210

RADIOACTIVE DECAY CONSTANT (PER DAY)	0.5020E-02
ENVIRONMENTAL DECAY CONSTANT--SURFACE (PER DAY)	0.0
ENVIRONMENTAL DECAY CONSTANT--WATER (PER DAY)	0.0
AVERAGE FRACTION OF ANIMAL'S DAILY INTAKE OF NUCLIDE WHICH APPEARS IN EACH L OF MILK (DAYS/L)	0.1200E-03
FRACTION OF ANIMAL'S DAILY INTAKE OF NUCLIDE WHICH APPEARS IN EACH KG OF FLESH (DAYS/KG)	0.4000E-02
CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SOIL FOR PASTURE AND FORAGE (IN PCI/KG DRY WEIGHT PER PCI/KG DRY SOIL)	0.4200E-02
CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SOIL BY EDIBLE PARTS OF CROPS (IN PCI/KG WET WEIGHT PER PCI/KG DRY SOIL)	0.2600E-03
GI UPTAKE FRACTION (INHALATION)	0.1000E 00
GI UPTAKE FRACTION (INGESTION)	0.1000E 00
PARTICLE SIZE (MICRONS)	0.1000E 01
SOLUBILITY CLASS	W

CONCENTRATIONS ON GROUND AND WATER INCLUDE CONTRIBUTIONS RESULTING FROM DECAY OF THE FOLLOWING PARENT NUCLIDES AFTER DEPOSITION--

NUCLIDE	BUILDUP FACTOR
RA-226	0.124E 03

DOSE CONVERSION FACTORS

ORGAN	INHALATION (REMS/MICROCURIE)	INGESTION (REMS/MICROCURIE)	SUBMERSION IN AIR (REMS-CUBIC CM/ MICROCURIE-HR)	SURFACE EXPOSURE (REMS-SQUARE CM/ MICROCURIE-HR)	SUBMERSION IN WATER (REMS-CUBIC CM/ MICROCURIE-HR)
TOT.BODY	0.156E 01	0.562E 00	0.525E-02	0.102E-05	0.113E-04
S WALL	0.222E-02	0.454E-02	0.470E-02	0.914E-06	0.101E-04
LLI WALL	0.879E-01	0.179E 00	0.351E-02	0.684E-06	0.757E-05
LUNGS	0.458E 02	0.113E-07	0.494E-02	0.962E-06	0.107E-04
KIDNEYS	0.144E 02	0.932E 01	0.485E-02	0.944E-06	0.105E-04
LIVER	0.248E 01	0.161E 01	0.449E-02	0.874E-06	0.968E-05
OVARIES	0.803E 00	0.521E 00	0.272E-02	0.529E-06	0.586E-05
R MAR	0.855E 00	0.554E 00	0.556E-02	0.108E-05	0.120E-04
ENDOST	0.374E 00	0.242E 00	0.634E-02	0.123E-05	0.137E-04
TESTES	0.803E 00	0.521E 00	0.513E-02	0.998E-06	0.111E-04
THYROID	0.803E 00	0.521E 00	0.402E-02	0.783E-06	0.867E-05

LIST OF INPUT DATA FOR NUCLIDE RN-222

RADIOACTIVE DECAY CONSTANT (PER DAY)	0.1810E 00
ENVIRONMENTAL DECAY CONSTANT--SURFACE (PER DAY)	0.0
ENVIRONMENTAL DECAY CONSTANT--WATER (PER DAY)	0.0
AVERAGE FRACTION OF ANIMAL'S DAILY INTAKE OF NUCLIDE WHICH APPEARS IN EACH L OF MILK (DAYS/L)	0.0
FRACTION OF ANIMAL'S DAILY INTAKE OF NUCLIDE WHICH APPEARS IN EACH KG OF FLESH (DAYS/KG)	0.0
CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SOIL FOR PASTURE AND FORAGE (IN PCI/KG DRY WEIGHT PER PCI/KG DRY SOIL)	0.0
CONCENTRATION FACTOR FOR UPTAKE OF NUCLIDE FROM SOIL BY EDIBLE PARTS OF CROPS (IN PCI/KG WET WEIGHT PER PCI/KG DRY SOIL)	0.0
GI UPTAKE FRACTION (INHALATION)	0.0
GI UPTAKE FRACTION (INGESTION)	0.0
PARTICLE SIZE (MICRONS)	0.1000E 01
SOLUBILITY CLASS	*

DOSE CONVERSION FACTORS

ORGAN	INHALATION (REMS/MICROCURIE)	INGESTION (REMS/MICROCURIE)	SUBMERSION IN AIR (REMS-CUBIC CM/ MICROCURIE-HR)	SURFACE EXPOSURE (REMS-SQUARE CM/ MICROCURIE-HR)	SUBMERSION IN WATER (REMS-CUBIC CM/ MICROCURIE-HR)
TOT. BODY	0.229E-04	0.459E-02	0.244E 00	0.502E-04	0.521E-03
S WALL	0.488E-06	0.148E-01	0.242E 00	0.497E-04	0.516E-03
LLI WALL	0.141E-07	0.686E 00	0.178E 00	0.366E-04	0.380E-03
LUNGS	0.140E-02	0.115E-03	0.228E 00	0.469E-04	0.487E-03
KIDNEYS	0.503E-04	0.144E-01	0.212E 00	0.437E-04	0.453E-03
LIVER	0.413E-05	0.190E-02	0.211E 00	0.434E-04	0.451E-03
OVARIES	0.825E-06	0.540E-02	0.908E-01	0.187E-04	0.194E-03
R MAR	0.991E-05	0.473E-02	0.283E 00	0.582E-04	0.604E-03
ENDOST	0.334E-04	0.131E-01	0.311E 00	0.639E-04	0.664E-03
TESTES	0.818E-06	0.677E-03	0.274E 00	0.563E-04	0.585E-03
THYROID	0.837E-06	0.214E-03	0.202E 00	0.415E-04	0.431E-03

LIST OF INPUT DATA FOR NUCLIDE H-3

RADIOACTIVE DECAY CONSTANT (PER DAY)	0.1540E-03
ENVIRONMENTAL DECAY CONSTANT--SURFACE (PER DAY)	0.0
ENVIRONMENTAL DECAY CONSTANT--WATER (PER DAY)	0.0
DOSE CONVERSION FACTOR FOR FOOD INGESTION (REM-CC/PCI-YEAR)	0.6180E 01
DOSE CONVERSION FACTOR FOR WATER INGESTION (REM-CC/PCI-YEAR)	0.5700E-01

DOSE CONVERSION FACTORS

ORGAN	INHALATION (REMS/MICROCURIE)	INGESTION (REMS/MICROCURIE)	SUBMERSION IN AIR (REMS-CUBIC CM/ MICROCURIE-HR)	SURFACE EXPOSURE (REMS-SQUARE CM/ MICROCURIE-HR)	SUBMERSION IN WATER (REMS-CUBIC CM/ MICROCURIE-HR)
TOT. BODY	0.125E-03	0.830E-04	0.0	0.0	0.0
S WALL	0.125E-03	0.108E-03	0.0	0.0	0.0
LLI WALL	0.133E-03	0.143E-03	0.0	0.0	0.0
LUNGS	0.125E-03	0.836E-04	0.0	0.0	0.0
KIDNEYS	0.129E-03	0.856E-04	0.0	0.0	0.0
LIVER	0.124E-03	0.828E-04	0.0	0.0	0.0
OVARIES	0.124E-03	0.829E-04	0.0	0.0	0.0
R MAR	0.124E-03	0.826E-04	0.0	0.0	0.0
ENDOST	0.985E-04	0.656E-04	0.0	0.0	0.0
TESTES	0.125E-03	0.830E-04	0.0	0.0	0.0
THYROID	0.124E-03	0.828E-04	0.0	0.0	0.0

POPULATION-WEIGHTED CONCENTRATIONS AND POPULATION INTAKES FOR RA-226

AREA DIRECTION	DISTANCE (METERS)	AIR CONCENTRATION (MAN-CURIES/CUBIC METER)	GROUND CONCENTRATION (MAN-CURIES/SQUARE METER)	INGESTION INTAKE (MAN-PCI/YEAR)	INHALATION INTAKE (MAN-PCI/YEAR)
1	1207	0.0	0.0	0.0	0.0
1	2414	0.0	0.0	0.0	0.0
1	4023	0.0	0.0	0.0	0.0
1	5632	0.0	0.0	0.0	0.0
1	7241	0.0	0.0	0.0	0.0
1	12068	0.147E-15	0.523E-08	0.168E 04	0.118E 01
1	20113	0.0	0.0	0.0	0.0
1	32180	0.0	0.0	0.0	0.0
1	48270	0.169E-17	0.686E-10	0.199E 03	0.135E-01
1	64360	0.533E-16	0.231E-08	0.121E 05	0.428E 00
1	80450	0.264E-15	0.118E-07	0.919E 05	0.212E 01
2	1207	0.0	0.0	0.0	0.0
2	2414	0.0	0.0	0.0	0.0
2	4023	0.0	0.0	0.0	0.0
2	5632	0.0	0.0	0.0	0.0
2	7241	0.0	0.0	0.0	0.0
2	12068	0.0	0.0	0.0	0.0
2	20113	0.202E-15	0.713E-08	0.800E 04	0.162E 01
2	32180	0.349E-16	0.130E-08	0.362E 04	0.280E 00
2	48270	0.753E-16	0.291E-08	0.162E 05	0.605E 00
2	64360	0.165E-16	0.687E-09	0.776E 04	0.133E 00
2	80450	0.958E-17	0.412E-09	0.712E 04	0.769E-01
3	1207	0.0	0.0	0.0	0.0
3	2414	0.0	0.0	0.0	0.0
3	4023	0.0	0.0	0.0	0.0
3	5632	0.0	0.0	0.0	0.0
3	7241	0.0	0.0	0.0	0.0
3	12068	0.0	0.0	0.0	0.0
3	20113	0.0	0.0	0.0	0.0
3	32180	0.0	0.0	0.0	0.0
3	48270	0.174E-15	0.649E-08	0.255E 05	0.140E 01
3	64360	0.101E-15	0.403E-08	0.338E 05	0.809E 00
3	80450	0.267E-16	0.110E-08	0.144E 05	0.214E 00
4	1207	0.0	0.0	0.0	0.0
4	2414	0.0	0.0	0.0	0.0
4	4023	0.0	0.0	0.0	0.0
4	5632	0.0	0.0	0.0	0.0
4	7241	0.0	0.0	0.0	0.0
4	12068	0.0	0.0	0.0	0.0
4	20113	0.155E-15	0.531E-08	0.420E 04	0.124E 01
4	32180	0.801E-16	0.286E-08	0.541E 04	0.643E 00
4	48270	0.978E-16	0.358E-08	0.134E 05	0.785E 00
4	64360	0.420E-15	0.161E-07	0.117E 06	0.337E 01
4	80450	0.448E-15	0.176E-07	0.192E 06	0.360E 01
5	1207	0.0	0.0	0.0	0.0
5	2414	0.0	0.0	0.0	0.0
5	4023	0.0	0.0	0.0	0.0
5	5632	0.0	0.0	0.0	0.0
5	7241	0.0	0.0	0.0	0.0
5	12068	0.216E-15	0.732E-08	0.408E 04	0.174E 01
5	20113	0.182E-15	0.635E-08	0.797E 04	0.147E 01
5	32180	0.0	0.0	0.0	0.0
5	48270	0.154E-16	0.571E-09	0.312E 04	0.124E 00
5	64360	0.721E-17	0.277E-09	0.272E 04	0.579E-01
5	80450	0.288E-15	0.113E-07	0.165E 06	0.231E 01

6	1207	0.0	0.0	0.0	0.0
6	2414	0.576E-14	0.184E-06	0.142E 05	0.463E 02
6	4023	0.0	0.0	0.0	0.0
6	5632	0.0	0.0	0.0	0.0
6	7241	0.0	0.0	0.0	0.0
6	12068	0.0	0.0	0.0	0.0
6	20113	0.0	0.0	0.0	0.0
6	32180	0.315E-16	0.118E-08	0.664E 04	0.253E 00
6	48270	0.166E-16	0.641E-09	0.713E 04	0.133E 00
6	64360	0.252E-15	0.103E-07	0.219E 06	0.202E 01
6	80450	0.151E-15	0.632E-08	0.205E 06	0.121E 01
7	1207	0.0	0.0	0.0	0.0
7	2414	0.0	0.0	0.0	0.0
7	4023	0.0	0.0	0.0	0.0
7	5632	0.0	0.0	0.0	0.0
7	7241	0.0	0.0	0.0	0.0
7	12068	0.0	0.0	0.0	0.0
7	20113	0.0	0.0	0.0	0.0
7	32180	0.761E-16	0.290E-08	0.120E 05	0.611E 00
7	48270	0.216E-16	0.854E-09	0.706E 04	0.174E 00
7	64360	0.262E-16	0.111E-08	0.183E 05	0.211E 00
7	80450	0.326E-17	0.142E-09	0.362E 04	0.262E-01
8	1207	0.0	0.0	0.0	0.0
8	2414	0.0	0.0	0.0	0.0
8	4023	0.0	0.0	0.0	0.0
8	5632	0.0	0.0	0.0	0.0
8	7241	0.0	0.0	0.0	0.0
8	12068	0.0	0.0	0.0	0.0
8	20113	0.334E-15	0.117E-07	0.133E 05	0.268E 01
8	32180	0.234E-15	0.848E-08	0.231E 05	0.188E 01
8	48270	0.553E-16	0.206E-08	0.111E 05	0.444E 00
8	64360	0.185E-16	0.731E-09	0.811E 04	0.148E 00
8	80450	0.0	0.0	0.0	0.0
9	1207	0.0	0.0	0.0	0.0
9	2414	0.0	0.0	0.0	0.0
9	4023	0.0	0.0	0.0	0.0
9	5632	0.0	0.0	0.0	0.0
9	7241	0.0	0.0	0.0	0.0
9	12068	0.0	0.0	0.0	0.0
9	20113	0.0	0.0	0.0	0.0
9	32180	0.225E-14	0.817E-07	0.788E 05	0.161E 02
9	48270	0.0	0.0	0.0	0.0
9	64360	0.622E-16	0.245E-08	0.892E 04	0.500E 00
9	80450	0.0	0.0	0.0	0.0
10	1207	0.0	0.0	0.0	0.0
10	2414	0.0	0.0	0.0	0.0
10	4023	0.0	0.0	0.0	0.0
10	5632	0.0	0.0	0.0	0.0
10	7241	0.0	0.0	0.0	0.0
10	12068	0.360E-14	0.126E-06	0.516E 05	0.289E 02
10	20113	0.0	0.0	0.0	0.0
10	32180	0.394E-15	0.150E-07	0.309E 05	0.316E 01
10	48270	0.919E-16	0.362E-08	0.145E 05	0.738E 00
10	64360	0.338E-16	0.142E-08	0.106E 05	0.271E 00
10	80450	0.288E-16	0.124E-08	0.139E 05	0.231E 00
11	1207	0.0	0.0	0.0	0.0
11	2414	0.0	0.0	0.0	0.0
11	4023	0.0	0.0	0.0	0.0
11	5632	0.0	0.0	0.0	0.0
11	7241	0.0	0.0	0.0	0.0
11	12068	0.236E-14	0.852E-07	0.422E 05	0.190E 02
11	20113	0.164E-15	0.617E-08	0.667E 04	0.132E 01
11	32180	0.0	0.0	0.0	0.0
11	48270	0.885E-16	0.366E-08	0.163E 05	0.711E 00
11	64360	0.339E-16	0.148E-08	0.116E 05	0.272E 00
11	80450	0.528E-18	0.238E-10	0.276E 03	0.424E-02

12					
12	1207	0.0	0.0	0.0	0.0
12	2414	0.0	0.0	0.0	0.0
12	4023	0.0	0.0	0.0	0.0
12	5632	0.0	0.0	0.0	0.0
12	7241	0.0	0.0	0.0	0.0
12	12068	0.0	0.0	0.0	0.0
12	20113	0.380E-15	0.145E-07	0.173E 05	0.305E 01
12	32180	0.0	0.0	0.0	0.0
12	48270	0.956E-16	0.403E-08	0.191E 05	0.768E 00
12	64360	0.208E-16	0.928E-09	0.761E 04	0.167E 00
13	80450	0.234E-16	0.107E-08	0.129E 05	0.188E 00
13	1207	0.0	0.0	0.0	0.0
13	2414	0.0	0.0	0.0	0.0
13	4023	0.0	0.0	0.0	0.0
13	5632	0.0	0.0	0.0	0.0
13	7241	0.0	0.0	0.0	0.0
13	12068	0.0	0.0	0.0	0.0
13	20113	0.552E-16	0.217E-08	0.287E 04	0.444E 00
13	32180	0.0	0.0	0.0	0.0
13	48270	0.103E-16	0.445E-09	0.229E 04	0.825E-01
13	64360	0.382E-17	0.175E-09	0.154E 04	0.306E-01
14	80450	0.491E-16	0.232E-08	0.297E 05	0.395E 00
14	1207	0.0	0.0	0.0	0.0
14	2414	0.0	0.0	0.0	0.0
14	4023	0.0	0.0	0.0	0.0
14	5632	0.0	0.0	0.0	0.0
14	7241	0.0	0.0	0.0	0.0
14	12068	0.0	0.0	0.0	0.0
14	20113	0.0	0.0	0.0	0.0
14	32180	0.410E-16	0.166E-08	0.418E 04	0.329E 00
14	48270	0.181E-16	0.765E-09	0.360E 04	0.145E 00
14	64360	0.988E-16	0.444E-08	0.359E 05	0.793E 00
15	80450	0.161E-15	0.747E-08	0.879E 05	0.129E 01
15	1207	0.0	0.0	0.0	0.0
15	2414	0.0	0.0	0.0	0.0
15	4023	0.0	0.0	0.0	0.0
15	5632	0.0	0.0	0.0	0.0
15	7241	0.0	0.0	0.0	0.0
15	12068	0.0	0.0	0.0	0.0
15	20113	0.0	0.0	0.0	0.0
15	32180	0.0	0.0	0.0	0.0
15	48270	0.191E-16	0.822E-09	0.317E 04	0.154E 00
15	64360	0.253E-16	0.115E-08	0.766E 04	0.203E 00
16	80450	0.103E-15	0.486E-08	0.472E 05	0.827E 00
16	1207	0.0	0.0	0.0	0.0
16	2414	0.0	0.0	0.0	0.0
16	4023	0.0	0.0	0.0	0.0
16	5632	0.127E-14	0.430E-07	0.731E 04	0.102E 02
16	7241	0.0	0.0	0.0	0.0
16	12068	0.0	0.0	0.0	0.0
16	20113	0.0	0.0	0.0	0.0
16	32180	0.0	0.0	0.0	0.0
16	48270	0.141E-16	0.583E-09	0.265E 04	0.113E 00
16	64360	0.294E-16	0.129E-08	0.102E 05	0.236E 00
	80450	0.454E-15	0.206E-07	0.238E 06	0.365E 01

DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARTING AT 1 FOR DUE NORTH

POPULATION-WEIGHTED CONCENTRATIONS AND POPULATION INTAKES FOR PB-210

AREA DIRECTION	DISTANCE (METERS)	AIR CONCENTRATION (NAN-CURIES/CUBIC METER)	GROUND CONCENTRATION (NAN-CURIES/SQUARE METER)	INGESTION INTAKE (NAN-PCI/YEAR)	INHALATION INTAKE (NAN-PCI/YEAR)
1	1207	0.0	0.0	0.0	0.0
1	2414	0.0	0.0	0.0	0.0
1	4023	0.0	0.0	0.0	0.0
1	5632	0.0	0.0	0.0	0.0
1	7241	0.0	0.0	0.0	0.0
1	12068	0.0	0.363E-08	0.545E 02	0.0
1	20113	0.0	0.0	0.0	0.0
1	32180	0.0	0.0	0.0	0.0
1	48270	0.0	0.476E-10	0.643E 01	0.0
1	64360	0.0	0.161E-08	0.391E 03	0.0
1	80450	0.0	0.821E-08	0.297E 04	0.0
2	1207	0.0	0.0	0.0	0.0
2	2414	0.0	0.0	0.0	0.0
2	4023	0.0	0.0	0.0	0.0
2	5632	0.0	0.0	0.0	0.0
2	7241	0.0	0.0	0.0	0.0
2	12068	0.0	0.0	0.0	0.0
2	20113	0.0	0.495E-08	0.259E 03	0.0
2	32180	0.0	0.902E-09	0.117E 03	0.0
2	48270	0.0	0.202E-08	0.524E 03	0.0
2	64360	0.0	0.477E-09	0.251E 03	0.0
2	80450	0.0	0.286E-09	0.230E 03	0.0
3	1207	0.0	0.0	0.0	0.0
3	2414	0.0	0.0	0.0	0.0
3	4023	0.0	0.0	0.0	0.0
3	5632	0.0	0.0	0.0	0.0
3	7241	0.0	0.0	0.0	0.0
3	12068	0.0	0.0	0.0	0.0
3	20113	0.0	0.0	0.0	0.0
3	32180	0.0	0.0	0.0	0.0
3	48270	0.0	0.450E-08	0.824E 03	0.0
3	64360	0.0	0.279E-08	0.109E 04	0.0
3	80450	0.0	0.761E-09	0.465E 03	0.0
4	1207	0.0	0.0	0.0	0.0
4	2414	0.0	0.0	0.0	0.0
4	4023	0.0	0.0	0.0	0.0
4	5632	0.0	0.0	0.0	0.0
4	7241	0.0	0.0	0.0	0.0
4	12068	0.0	0.0	0.0	0.0
4	20113	0.0	0.369E-08	0.136E 03	0.0
4	32180	0.0	0.198E-08	0.175E 03	0.0
4	48270	0.0	0.249E-08	0.433E 03	0.0
4	64360	0.0	0.112E-07	0.377E 04	0.0
4	80450	0.0	0.122E-07	0.622E 04	0.0
5	1207	0.0	0.0	0.0	0.0
5	2414	0.0	0.0	0.0	0.0
5	4023	0.0	0.0	0.0	0.0
5	5632	0.0	0.0	0.0	0.0
5	7241	0.0	0.0	0.0	0.0
5	12068	0.0	0.508E-08	0.132E 03	0.0
5	20113	0.0	0.440E-08	0.258E 03	0.0
5	32180	0.0	0.0	0.0	0.0
5	48270	0.0	0.396E-09	0.101E 03	0.0
5	64360	0.0	0.192E-09	0.879E 02	0.0
5	80450	0.0	0.786E-08	0.533E 04	0.0

6	1207	0.0	0.0	0.0	0.0
6	2414	0.0	0.127E-06	0.461E 03	0.0
6	4023	0.0	0.0	0.0	0.0
6	5632	0.0	0.0	0.0	0.0
6	7241	0.0	0.0	0.0	0.0
6	12068	0.0	0.0	0.0	0.0
6	20113	0.0	0.0	0.0	0.0
6	32180	0.0	0.820E-09	0.215E 03	0.0
6	48270	0.0	0.445E-09	0.231E 03	0.0
6	64360	0.0	0.714E-08	0.710E 04	0.0
6	80450	0.0	0.438E-08	0.664E 04	0.0
7	1207	0.0	0.0	0.0	0.0
7	2414	0.0	0.0	0.0	0.0
7	4023	0.0	0.0	0.0	0.0
7	5632	0.0	0.0	0.0	0.0
7	7241	0.0	0.0	0.0	0.0
7	12068	0.0	0.0	0.0	0.0
7	20113	0.0	0.0	0.0	0.0
7	32180	0.0	0.201E-08	0.388E 03	0.0
7	48270	0.0	0.593E-09	0.228E 03	0.0
7	64360	0.0	0.772E-09	0.593E 03	0.0
7	80450	0.0	0.988E-10	0.117E 03	0.0
8	1207	0.0	0.0	0.0	0.0
8	2414	0.0	0.0	0.0	0.0
8	4023	0.0	0.0	0.0	0.0
8	5632	0.0	0.0	0.0	0.0
8	7241	0.0	0.0	0.0	0.0
8	12068	0.0	0.0	0.0	0.0
8	20113	0.0	0.808E-08	0.429E 03	0.0
8	32180	0.0	0.589E-08	0.747E 03	0.0
8	48270	0.0	0.143E-08	0.358E 03	0.0
8	64360	0.0	0.507E-09	0.262E 03	0.0
8	80450	0.0	0.0	0.0	0.0
9	1207	0.0	0.0	0.0	0.0
9	2414	0.0	0.0	0.0	0.0
9	4023	0.0	0.0	0.0	0.0
9	5632	0.0	0.0	0.0	0.0
9	7241	0.0	0.0	0.0	0.0
9	12068	0.0	0.0	0.0	0.0
9	20113	0.0	0.0	0.0	0.0
9	32180	0.0	0.567E-07	0.255E 04	0.0
9	48270	0.0	0.0	0.0	0.0
9	64360	0.0	0.170E-08	0.289E 03	0.0
9	80450	0.0	0.0	0.0	0.0
10	1207	0.0	0.0	0.0	0.0
10	2414	0.0	0.0	0.0	0.0
10	4023	0.0	0.0	0.0	0.0
10	5632	0.0	0.0	0.0	0.0
10	7241	0.0	0.0	0.0	0.0
10	12068	0.0	0.872E-07	0.167E 04	0.0
10	20113	0.0	0.0	0.0	0.0
10	32180	0.0	0.104E-07	0.998E 03	0.0
10	48270	0.0	0.251E-08	0.468E 03	0.0
10	64360	0.0	0.983E-09	0.342E 03	0.0
10	80450	0.0	0.862E-09	0.450E 03	0.0
11	1207	0.0	0.0	0.0	0.0
11	2414	0.0	0.0	0.0	0.0
11	4023	0.0	0.0	0.0	0.0
11	5632	0.0	0.0	0.0	0.0
11	7241	0.0	0.0	0.0	0.0
11	12068	0.0	0.591E-07	0.136E 04	0.0
11	20113	0.0	0.428E-08	0.216E 03	0.0
11	32180	0.0	0.0	0.0	0.0
11	48270	0.0	0.254E-08	0.526E 03	0.0
11	64360	0.0	0.103E-08	0.376E 03	0.0
11	80450	0.0	0.165E-10	0.892E 01	0.0

12	1207	0.0	0.0	0.0	0.0
12	2414	0.0	0.0	0.0	0.0
12	4023	0.0	0.0	0.0	0.0
12	5632	0.0	0.0	0.0	0.0
12	7241	0.0	0.0	0.0	0.0
12	12068	0.0	0.0	0.0	0.0
12	20113	0.0	0.101E-07	0.558E 03	0.0
12	32180	0.0	0.0	0.0	0.0
12	48270	0.0	0.280E-08	0.618E 03	0.0
12	64360	0.0	0.644E-09	0.246E 03	0.0
12	80450	0.0	0.745E-09	0.418E 03	0.0
13	1207	0.0	0.0	0.0	0.0
13	2414	0.0	0.0	0.0	0.0
13	4023	0.0	0.0	0.0	0.0
13	5632	0.0	0.0	0.0	0.0
13	7241	0.0	0.0	0.0	0.0
13	12068	0.0	0.0	0.0	0.0
13	20113	0.0	0.150E-08	0.927E 02	0.0
13	32180	0.0	0.0	0.0	0.0
13	48270	0.0	0.309E-09	0.742E 02	0.0
13	64360	0.0	0.121E-09	0.497E 02	0.0
13	80450	0.0	0.161E-08	0.961E 03	0.0
14	1207	0.0	0.0	0.0	0.0
14	2414	0.0	0.0	0.0	0.0
14	4023	0.0	0.0	0.0	0.0
14	5632	0.0	0.0	0.0	0.0
14	7241	0.0	0.0	0.0	0.0
14	12068	0.0	0.0	0.0	0.0
14	20113	0.0	0.0	0.0	0.0
14	32180	0.0	0.115E-08	0.135E 03	0.0
14	48270	0.0	0.531E-09	0.116E 03	0.0
14	64360	0.0	0.308E-08	0.116E 04	0.0
14	80450	0.0	0.519E-08	0.284E 04	0.0
15	1207	0.0	0.0	0.0	0.0
15	2414	0.0	0.0	0.0	0.0
15	4023	0.0	0.0	0.0	0.0
15	5632	0.0	0.0	0.0	0.0
15	7241	0.0	0.0	0.0	0.0
15	12068	0.0	0.0	0.0	0.0
15	20113	0.0	0.0	0.0	0.0
15	32180	0.0	0.0	0.0	0.0
15	48270	0.0	0.570E-09	0.103E 03	0.0
15	64360	0.0	0.801E-09	0.248E 03	0.0
15	80450	0.0	0.338E-08	0.153E 04	0.0
16	1207	0.0	0.0	0.0	0.0
16	2414	0.0	0.0	0.0	0.0
16	4023	0.0	0.0	0.0	0.0
16	5632	0.0	0.299E-07	0.237E 03	0.0
16	7241	0.0	0.0	0.0	0.0
16	12068	0.0	0.0	0.0	0.0
16	20113	0.0	0.0	0.0	0.0
16	32180	0.0	0.0	0.0	0.0
16	48270	0.0	0.405E-09	0.858E 02	0.0
16	64360	0.0	0.894E-09	0.330E 03	0.0
16	80450	0.0	0.143E-07	0.771E 04	0.0

DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARTING AT 1 FOR DUE NORTH

POPULATION-WEIGHTED CONCENTRATIONS AND POPULATION INTAKES FOR PO-210

AREA DIRECTION	DISTANCE (METERS)	AIR CONCENTRATION (MAN-CURIES/CUBIC METER)	GROUND CONCENTRATION (MAN-CURIES/SQUARE METER)	INGESTION INTAKE (MAN-PCI/YEAR)	INHALATION INTAKE (MAN-PCI/YEAR)
1	1207	0.0	0.0	0.0	0.0
1	2414	0.0	0.0	0.0	0.0
1	4023	0.0	0.0	0.0	0.0
1	5632	0.0	0.0	0.0	0.0
1	7241	0.0	0.0	0.0	0.0
1	12068	0.294E-15	0.368E-08	0.119E 04	0.236E 01
1	20113	0.0	0.0	0.0	0.0
1	32180	0.0	0.0	0.0	0.0
1	48270	0.337E-17	0.482E-10	0.143E 03	0.271E-01
1	64360	0.107E-15	0.163E-08	0.872E 04	0.857E 00
1	80450	0.527E-15	0.831E-08	0.662E 05	0.424E 01
2	1207	0.0	0.0	0.0	0.0
2	2414	0.0	0.0	0.0	0.0
2	4023	0.0	0.0	0.0	0.0
2	5632	0.0	0.0	0.0	0.0
2	7241	0.0	0.0	0.0	0.0
2	12068	0.0	0.0	0.0	0.0
2	20113	0.404E-15	0.501E-08	0.574E 04	0.324E 01
2	32180	0.698E-16	0.914E-09	0.261E 04	0.561E 00
2	48270	0.151E-15	0.204E-08	0.117E 05	0.121E 01
2	64360	0.331E-16	0.483E-09	0.559E 04	0.266E 00
2	80450	0.192E-16	0.289E-09	0.513E 04	0.154E 00
3	1207	0.0	0.0	0.0	0.0
3	2414	0.0	0.0	0.0	0.0
3	4023	0.0	0.0	0.0	0.0
3	5632	0.0	0.0	0.0	0.0
3	7241	0.0	0.0	0.0	0.0
3	12068	0.0	0.0	0.0	0.0
3	20113	0.0	0.0	0.0	0.0
3	32180	0.0	0.0	0.0	0.0
3	48270	0.348E-15	0.456E-08	0.184E 05	0.279E 01
3	64360	0.201E-15	0.283E-08	0.244E 05	0.162E 01
3	80450	0.533E-16	0.771E-09	0.104E 05	0.428E 00
4	1207	0.0	0.0	0.0	0.0
4	2414	0.0	0.0	0.0	0.0
4	4023	0.0	0.0	0.0	0.0
4	5632	0.0	0.0	0.0	0.0
4	7241	0.0	0.0	0.0	0.0
4	12068	0.0	0.0	0.0	0.0
4	20113	0.309E-15	0.373E-08	0.301E 04	0.249E 01
4	32180	0.160E-15	0.201E-08	0.389E 04	0.129E 01
4	48270	0.196E-15	0.252E-08	0.965E 04	0.157E 01
4	64360	0.839E-15	0.113E-07	0.840E 05	0.674E 01
4	80450	0.896E-15	0.123E-07	0.139E 06	0.719E 01
5	1207	0.0	0.0	0.0	0.0
5	2414	0.0	0.0	0.0	0.0
5	4023	0.0	0.0	0.0	0.0
5	5632	0.0	0.0	0.0	0.0
5	7241	0.0	0.0	0.0	0.0
5	12068	0.432E-15	0.514E-08	0.291E 04	0.347E 01
5	20113	0.365E-15	0.446E-08	0.572E 04	0.293E 01
5	32180	0.0	0.0	0.0	0.0
5	48270	0.308E-16	0.401E-09	0.225E 04	0.247E 00
5	64360	0.144E-16	0.195E-09	0.196E 04	0.116E 00
5	80450	0.576E-15	0.796E-08	0.119E 06	0.463E 01

6	1207	0.0	0.0	0.0	0.0
6	2414	0.115E-13	0.129E-06	0.951E 04	0.925E 02
6	4023	0.0	0.0	0.0	0.0
6	5632	0.0	0.0	0.0	0.0
6	7241	0.0	0.0	0.0	0.0
6	12068	0.0	0.0	0.0	0.0
6	20113	0.0	0.0	0.0	0.0
6	32180	0.630E-16	0.831E-09	0.478E 04	0.506E 00
6	48270	0.331E-16	0.451E-09	0.514E 04	0.266E 00
6	64360	0.503E-15	0.723E-08	0.158E 06	0.404E 01
6	80450	0.301E-15	0.444E-08	0.148E 06	0.242E 01
7	1207	0.0	0.0	0.0	0.0
7	2414	0.0	0.0	0.0	0.0
7	4023	0.0	0.0	0.0	0.0
7	5632	0.0	0.0	0.0	0.0
7	7241	0.0	0.0	0.0	0.0
7	12068	0.0	0.0	0.0	0.0
7	20113	0.0	0.0	0.0	0.0
7	32180	0.152E-15	0.204E-08	0.864E 04	0.122E 01
7	48270	0.432E-16	0.600E-09	0.509E 04	0.347E 00
7	64360	0.525E-16	0.782E-09	0.132E 05	0.421E 00
7	80450	0.652E-17	0.100E-09	0.261E 04	0.524E-01
8	1207	0.0	0.0	0.0	0.0
8	2414	0.0	0.0	0.0	0.0
8	4023	0.0	0.0	0.0	0.0
8	5632	0.0	0.0	0.0	0.0
8	7241	0.0	0.0	0.0	0.0
8	12068	0.0	0.0	0.0	0.0
8	20113	0.668E-15	0.819E-08	0.952E 04	0.536E 01
8	32180	0.467E-15	0.596E-08	0.166E 05	0.375E 01
8	48270	0.111E-15	0.145E-08	0.797E 04	0.888E 00
8	64360	0.369E-16	0.514E-09	0.585E 04	0.297E 00
8	80450	0.0	0.0	0.0	0.0
9	1207	0.0	0.0	0.0	0.0
9	2414	0.0	0.0	0.0	0.0
9	4023	0.0	0.0	0.0	0.0
9	5632	0.0	0.0	0.0	0.0
9	7241	0.0	0.0	0.0	0.0
9	12068	0.0	0.0	0.0	0.0
9	20113	0.0	0.0	0.0	0.0
9	32180	0.450E-14	0.574E-07	0.565E 05	0.361E 02
9	48270	0.0	0.0	0.0	0.0
9	64360	0.124E-15	0.172E-08	0.643E 04	0.999E 00
9	80450	0.0	0.0	0.0	0.0
10	1207	0.0	0.0	0.0	0.0
10	2414	0.0	0.0	0.0	0.0
10	4023	0.0	0.0	0.0	0.0
10	5632	0.0	0.0	0.0	0.0
10	7241	0.0	0.0	0.0	0.0
10	12068	0.721E-14	0.883E-07	0.367E 05	0.579E 02
10	20113	0.0	0.0	0.0	0.0
10	32180	0.787E-15	0.105E-07	0.222E 05	0.632E 01
10	48270	0.184E-15	0.254E-08	0.104E 05	0.148E 01
10	64360	0.676E-16	0.995E-09	0.762E 04	0.543E 00
10	80450	0.575E-16	0.873E-09	0.100E 05	0.462E 00
11	1207	0.0	0.0	0.0	0.0
11	2414	0.0	0.0	0.0	0.0
11	4023	0.0	0.0	0.0	0.0
11	5632	0.0	0.0	0.0	0.0
11	7241	0.0	0.0	0.0	0.0
11	12068	0.473E-14	0.598E-07	0.301E 05	0.380E 02
11	20113	0.328E-15	0.434E-08	0.478E 04	0.263E 01
11	32180	0.0	0.0	0.0	0.0
11	48270	0.177E-15	0.257E-08	0.117E 05	0.142E 01
11	64360	0.678E-16	0.104E-08	0.839E 04	0.544E 00
11	80450	0.106E-17	0.167E-10	0.199E 03	0.848E-02

12	1207	0.0	0.0	0.0	0.0
12	2414	0.0	0.0	0.0	0.0
12	4023	0.0	0.0	0.0	0.0
12	5632	0.0	0.0	0.0	0.0
12	7241	0.0	0.0	0.0	0.0
12	12068	0.0	0.0	0.0	0.0
12	20113	0.759E-15	0.102E-07	0.124E 05	0.610E 01
12	32180	0.0	0.0	0.0	0.0
12	48270	0.191E-15	0.283E-08	0.138E 05	0.154E 01
12	64360	0.416E-16	0.652E-09	0.549E 04	0.334E 00
12	80450	0.468E-16	0.755E-09	0.931E 04	0.376E 00
13	1207	0.0	0.0	0.0	0.0
13	2414	0.0	0.0	0.0	0.0
13	4023	0.0	0.0	0.0	0.0
13	5632	0.0	0.0	0.0	0.0
13	7241	0.0	0.0	0.0	0.0
13	12068	0.0	0.0	0.0	0.0
13	20113	0.110E-15	0.152E-08	0.206E 04	0.887E 00
13	32180	0.0	0.0	0.0	0.0
13	48270	0.205E-16	0.313E-09	0.165E 04	0.165E 00
13	64360	0.763E-17	0.123E-09	0.111E 04	0.613E-01
13	80450	0.983E-16	0.163E-08	0.214E 05	0.789E 00
14	1207	0.0	0.0	0.0	0.0
14	2414	0.0	0.0	0.0	0.0
14	4023	0.0	0.0	0.0	0.0
14	5632	0.0	0.0	0.0	0.0
14	7241	0.0	0.0	0.0	0.0
14	12068	0.0	0.0	0.0	0.0
14	20113	0.0	0.0	0.0	0.0
14	32180	0.820E-16	0.117E-08	0.301E 04	0.658E 00
14	48270	0.361E-16	0.538E-09	0.259E 04	0.290E 00
14	64360	0.198E-15	0.312E-08	0.258E 05	0.159E 01
14	80450	0.322E-15	0.525E-08	0.634E 05	0.259E 01
15	1207	0.0	0.0	0.0	0.0
15	2414	0.0	0.0	0.0	0.0
15	4023	0.0	0.0	0.0	0.0
15	5632	0.0	0.0	0.0	0.0
15	7241	0.0	0.0	0.0	0.0
15	12068	0.0	0.0	0.0	0.0
15	20113	0.0	0.0	0.0	0.0
15	32180	0.0	0.0	0.0	0.0
15	48270	0.383E-16	0.577E-09	0.228E 04	0.307E 00
15	64360	0.506E-16	0.811E-09	0.552E 04	0.406E 00
15	80450	0.206E-15	0.342E-08	0.340E 05	0.165E 01
16	1207	0.0	0.0	0.0	0.0
16	2414	0.0	0.0	0.0	0.0
16	4023	0.0	0.0	0.0	0.0
16	5632	0.254E-14	0.302E-07	0.509E 04	0.204E 02
16	7241	0.0	0.0	0.0	0.0
16	12068	0.0	0.0	0.0	0.0
16	20113	0.0	0.0	0.0	0.0
16	32180	0.0	0.0	0.0	0.0
16	48270	0.282E-16	0.410E-09	0.191E 04	0.227E 00
16	64360	0.588E-16	0.906E-09	0.736E 04	0.472E 00
16	80450	0.909E-15	0.145E-07	0.172E 06	0.730E 01

DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARTING AT 1 FOR DUE NORTH

POPULATION-WEIGHTED CONCENTRATIONS AND POPULATION INTAKES FOR RN-222

AREA DIRECTION	DISTANCE (METERS)	AIR CONCENTRATION (MAN-CURIES/CUBIC METER)	GROUND CONCENTRATION (MAN-CURIES/SQUARE METER)	INGESTION INTAKE (MAN-PCI/YEAR)	INHALATION INTAKE (MAN-PCI/YEAR)
1	1207	0.0	0.0	0.0	0.0
1	2414	0.0	0.0	0.0	0.0
1	4023	0.0	0.0	0.0	0.0
1	5632	0.0	0.0	0.0	0.0
1	7241	0.0	0.0	0.0	0.0
1	12068	0.111E-12	0.0	0.0	0.893E 03
1	20113	0.0	0.0	0.0	0.0
1	32180	0.0	0.0	0.0	0.0
1	48270	0.283E-14	0.0	0.0	0.227E 02
1	64360	0.122E-12	0.0	0.0	0.976E 03
1	80450	0.700E-12	0.0	0.0	0.562E 04
2	1207	0.0	0.0	0.0	0.0
2	2414	0.0	0.0	0.0	0.0
2	4023	0.0	0.0	0.0	0.0
2	5632	0.0	0.0	0.0	0.0
2	7241	0.0	0.0	0.0	0.0
2	12068	0.0	0.0	0.0	0.0
2	20113	0.280E-12	0.0	0.0	0.225E 04
2	32180	0.747E-13	0.0	0.0	0.600E 03
2	48270	0.208E-12	0.0	0.0	0.167E 04
2	64360	0.706E-13	0.0	0.0	0.567E 03
2	80450	0.493E-13	0.0	0.0	0.396E 03
3	1207	0.0	0.0	0.0	0.0
3	2414	0.0	0.0	0.0	0.0
3	4023	0.0	0.0	0.0	0.0
3	5632	0.0	0.0	0.0	0.0
3	7241	0.0	0.0	0.0	0.0
3	12068	0.0	0.0	0.0	0.0
3	20113	0.0	0.0	0.0	0.0
3	32180	0.0	0.0	0.0	0.0
3	48270	0.580E-12	0.0	0.0	0.466E 04
3	64360	0.547E-12	0.0	0.0	0.439E 04
3	80450	0.177E-12	0.0	0.0	0.142E 04
4	1207	0.0	0.0	0.0	0.0
4	2414	0.0	0.0	0.0	0.0
4	4023	0.0	0.0	0.0	0.0
4	5632	0.0	0.0	0.0	0.0
4	7241	0.0	0.0	0.0	0.0
4	12068	0.0	0.0	0.0	0.0
4	20113	0.194E-12	0.0	0.0	0.156E 04
4	32180	0.148E-12	0.0	0.0	0.119E 04
4	48270	0.229E-12	0.0	0.0	0.184E 04
4	64360	0.141E-11	0.0	0.0	0.113E 05
4	80450	0.177E-11	0.0	0.0	0.142E 05
5	1207	0.0	0.0	0.0	0.0
5	2414	0.0	0.0	0.0	0.0
5	4023	0.0	0.0	0.0	0.0
5	5632	0.0	0.0	0.0	0.0
5	7241	0.0	0.0	0.0	0.0
5	12068	0.169E-12	0.0	0.0	0.136E 04
5	20113	0.189E-12	0.0	0.0	0.151E 04
5	32180	0.0	0.0	0.0	0.0
5	48270	0.265E-13	0.0	0.0	0.213E 03
5	64360	0.163E-13	0.0	0.0	0.131E 03
5	80450	0.745E-12	0.0	0.0	0.598E 04

6	1207	0.0	0.0	0.0	0.0
6	2414	0.258E-11	0.0	0.0	0.207E 05
6	4023	0.0	0.0	0.0	0.0
6	5632	0.0	0.0	0.0	0.0
6	7241	0.0	0.0	0.0	0.0
6	12068	0.0	0.0	0.0	0.0
6	20113	0.0	0.0	0.0	0.0
6	32180	0.751E-13	0.0	0.0	0.603E 03
6	48270	0.498E-13	0.0	0.0	0.400E 03
6	64360	0.108E-11	0.0	0.0	0.866E 04
6	80450	0.764E-12	0.0	0.0	0.614E 04
7	1207	0.0	0.0	0.0	0.0
7	2414	0.0	0.0	0.0	0.0
7	4023	0.0	0.0	0.0	0.0
7	5632	0.0	0.0	0.0	0.0
7	7241	0.0	0.0	0.0	0.0
7	12068	0.0	0.0	0.0	0.0
7	20113	0.0	0.0	0.0	0.0
7	32180	0.224E-12	0.0	0.0	0.180E 04
7	48270	0.817E-13	0.0	0.0	0.656E 03
7	64360	0.150E-12	0.0	0.0	0.120E 04
7	80450	0.224E-13	0.0	0.0	0.180E 03
8	1207	0.0	0.0	0.0	0.0
8	2414	0.0	0.0	0.0	0.0
8	4023	0.0	0.0	0.0	0.0
8	5632	0.0	0.0	0.0	0.0
8	7241	0.0	0.0	0.0	0.0
8	12068	0.0	0.0	0.0	0.0
8	20113	0.380E-12	0.0	0.0	0.305E 04
8	32180	0.390E-12	0.0	0.0	0.313E 04
8	48270	0.117E-12	0.0	0.0	0.936E 03
8	64360	0.606E-13	0.0	0.0	0.487E 03
8	80450	0.0	0.0	0.0	0.0
9	1207	0.0	0.0	0.0	0.0
9	2414	0.0	0.0	0.0	0.0
9	4023	0.0	0.0	0.0	0.0
9	5632	0.0	0.0	0.0	0.0
9	7241	0.0	0.0	0.0	0.0
9	12068	0.0	0.0	0.0	0.0
9	20113	0.0	0.0	0.0	0.0
9	32180	0.256E-11	0.0	0.0	0.206E 05
9	48270	0.0	0.0	0.0	0.0
9	64360	0.130E-12	0.0	0.0	0.104E 04
9	80450	0.0	0.0	0.0	0.0
10	1207	0.0	0.0	0.0	0.0
10	2414	0.0	0.0	0.0	0.0
10	4023	0.0	0.0	0.0	0.0
10	5632	0.0	0.0	0.0	0.0
10	7241	0.0	0.0	0.0	0.0
10	12068	0.233E-11	0.0	0.0	0.187E 05
10	20113	0.0	0.0	0.0	0.0
10	32180	0.476E-12	0.0	0.0	0.382E 04
10	48270	0.139E-12	0.0	0.0	0.111E 04
10	64360	0.718E-13	0.0	0.0	0.577E 03
10	80450	0.718E-13	0.0	0.0	0.577E 03
11	1207	0.0	0.0	0.0	0.0
11	2414	0.0	0.0	0.0	0.0
11	4023	0.0	0.0	0.0	0.0
11	5632	0.0	0.0	0.0	0.0
11	7241	0.0	0.0	0.0	0.0
11	12068	0.153E-11	0.0	0.0	0.123E 05
11	20113	0.137E-12	0.0	0.0	0.110E 04
11	32180	0.0	0.0	0.0	0.0
11	48270	0.121E-12	0.0	0.0	0.972E 03
11	64360	0.611E-13	0.0	0.0	0.490E 03
11	80450	0.110E-14	0.0	0.0	0.880E 01

12	1207	0.0	0.0	0.0	0.0
12	2414	0.0	0.0	0.0	0.0
12	4023	0.0	0.0	0.0	0.0
12	5632	0.0	0.0	0.0	0.0
12	7241	0.0	0.0	0.0	0.0
12	12068	0.0	0.0	0.0	0.0
12	20113	0.323E-12	0.0	0.0	0.259E 04
12	32180	0.0	0.0	0.0	0.0
12	48270	0.128E-12	0.0	0.0	0.103E 04
12	64360	0.360E-13	0.0	0.0	0.289E 03
12	80450	0.462E-13	0.0	0.0	0.371E 03
13	1207	0.0	0.0	0.0	0.0
13	2414	0.0	0.0	0.0	0.0
13	4023	0.0	0.0	0.0	0.0
13	5632	0.0	0.0	0.0	0.0
13	7241	0.0	0.0	0.0	0.0
13	12068	0.0	0.0	0.0	0.0
13	20113	0.423E-13	0.0	0.0	0.340E 03
13	32180	0.0	0.0	0.0	0.0
13	48270	0.121E-13	0.0	0.0	0.971E 02
13	64360	0.571E-14	0.0	0.0	0.458E 02
13	80450	0.834E-13	0.0	0.0	0.670E 03
14	1207	0.0	0.0	0.0	0.0
14	2414	0.0	0.0	0.0	0.0
14	4023	0.0	0.0	0.0	0.0
14	5632	0.0	0.0	0.0	0.0
14	7241	0.0	0.0	0.0	0.0
14	12068	0.0	0.0	0.0	0.0
14	20113	0.0	0.0	0.0	0.0
14	32180	0.371E-13	0.0	0.0	0.298E 03
14	48270	0.197E-13	0.0	0.0	0.158E 03
14	64360	0.138E-12	0.0	0.0	0.111E 04
14	80450	0.256E-12	0.0	0.0	0.206E 04
15	1207	0.0	0.0	0.0	0.0
15	2414	0.0	0.0	0.0	0.0
15	4023	0.0	0.0	0.0	0.0
15	5632	0.0	0.0	0.0	0.0
15	7241	0.0	0.0	0.0	0.0
15	12068	0.0	0.0	0.0	0.0
15	20113	0.0	0.0	0.0	0.0
15	32180	0.0	0.0	0.0	0.0
15	48270	0.213E-13	0.0	0.0	0.171E 03
15	64360	0.362E-13	0.0	0.0	0.291E 03
15	80450	0.169E-12	0.0	0.0	0.135E 04
16	1207	0.0	0.0	0.0	0.0
16	2414	0.0	0.0	0.0	0.0
16	4023	0.0	0.0	0.0	0.0
16	5632	0.464E-12	0.0	0.0	0.373E 04
16	7241	0.0	0.0	0.0	0.0
16	12068	0.0	0.0	0.0	0.0
16	20113	0.0	0.0	0.0	0.0
16	32180	0.0	0.0	0.0	0.0
16	48270	0.141E-13	0.0	0.0	0.113E 03
16	64360	0.381E-13	0.0	0.0	0.306E 03
16	80450	0.673E-12	0.0	0.0	0.541E 04

DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARTING AT 1 FOR DUE NORTH

POPULATION-WEIGHTED CONCENTRATIONS AND POPULATION INTAKES FOR H-3

AREA DIRECTION	DISTANCE (METERS)	AIR CONCENTRATION (MAN-CURIES/CUBIC METER)	GROUND CONCENTRATION (MAN-CURIES/SQUARE METER)	INGESTION INTAKE (MAN-PCI/YEAR)	INHALATION INTAKE (MAN-PCI/YEAR)
1	1207	0.0	0.0	0.0	0.0
1	2414	0.0	0.0	0.0	0.0
1	4023	0.0	0.0	0.0	0.0
1	5632	0.0	0.0	0.0	0.0
1	7241	0.0	0.0	0.0	0.0
1	12068	0.113E-12	0.0	0.147E 05	0.911E 03
1	20113	0.0	0.0	0.0	0.0
1	32180	0.0	0.0	0.0	0.0
1	48270	0.306E-14	0.0	0.158E 04	0.246E 02
1	64360	0.135E-12	0.0	0.953E 05	0.109E 04
1	80450	0.801E-12	0.0	0.719E 06	0.643E 04
2	1207	0.0	0.0	0.0	0.0
2	2414	0.0	0.0	0.0	0.0
2	4023	0.0	0.0	0.0	0.0
2	5632	0.0	0.0	0.0	0.0
2	7241	0.0	0.0	0.0	0.0
2	12068	0.0	0.0	0.0	0.0
2	20113	0.288E-12	0.0	0.672E 05	0.232E 04
2	32180	0.785E-13	0.0	0.295E 05	0.630E 03
2	48270	0.224E-12	0.0	0.129E 06	0.180E 04
2	64360	0.780E-13	0.0	0.611E 05	0.626E 03
2	80450	0.558E-13	0.0	0.557E 05	0.448E 03
3	1207	0.0	0.0	0.0	0.0
3	2414	0.0	0.0	0.0	0.0
3	4023	0.0	0.0	0.0	0.0
3	5632	0.0	0.0	0.0	0.0
3	7241	0.0	0.0	0.0	0.0
3	12068	0.0	0.0	0.0	0.0
3	20113	0.0	0.0	0.0	0.0
3	32180	0.0	0.0	0.0	0.0
3	48270	0.625E-12	0.0	0.210E 06	0.502E 04
3	64360	0.605E-12	0.0	0.274E 06	0.486E 04
3	80450	0.200E-12	0.0	0.115E 06	0.161E 04
4	1207	0.0	0.0	0.0	0.0
4	2414	0.0	0.0	0.0	0.0
4	4023	0.0	0.0	0.0	0.0
4	5632	0.0	0.0	0.0	0.0
4	7241	0.0	0.0	0.0	0.0
4	12068	0.0	0.0	0.0	0.0
4	20113	0.200E-12	0.0	0.363E 05	0.161E 04
4	32180	0.156E-12	0.0	0.448E 05	0.125E 04
4	48270	0.247E-12	0.0	0.108E 06	0.198E 04
4	64360	0.156E-11	0.0	0.927E 06	0.125E 05
4	80450	0.201E-11	0.0	0.152E 07	0.161E 05
5	1207	0.0	0.0	0.0	0.0
5	2414	0.0	0.0	0.0	0.0
5	4023	0.0	0.0	0.0	0.0
5	5632	0.0	0.0	0.0	0.0
5	7241	0.0	0.0	0.0	0.0
5	12068	0.173E-12	0.0	0.340E 05	0.139E 04
5	20113	0.195E-12	0.0	0.645E 05	0.157E 04
5	32180	0.0	0.0	0.0	0.0
5	48270	0.288E-13	0.0	0.244E 05	0.231E 03
5	64360	0.182E-13	0.0	0.211E 05	0.146E 03
5	80450	0.856E-12	0.0	0.127E 07	0.687E 04

6	1207	0.0	0.0	0.0	0.0
6	2414	0.259E-11	0.0	0.132E 06	0.208E 05
6	4023	0.0	0.0	0.0	0.0
6	5632	0.0	0.0	0.0	0.0
6	7241	0.0	0.0	0.0	0.0
6	12068	0.0	0.0	0.0	0.0
6	20113	0.0	0.0	0.0	0.0
6	32180	0.796E-13	0.0	0.525E 05	0.639E 03
6	48270	0.543E-13	0.0	0.556E 05	0.436E 03
6	64360	0.121E-11	0.0	0.170E 07	0.974E 04
6	80450	0.885E-12	0.0	0.159E 07	0.710E 04
7	1207	0.0	0.0	0.0	0.0
7	2414	0.0	0.0	0.0	0.0
7	4023	0.0	0.0	0.0	0.0
7	5632	0.0	0.0	0.0	0.0
7	7241	0.0	0.0	0.0	0.0
7	12068	0.0	0.0	0.0	0.0
7	20113	0.0	0.0	0.0	0.0
7	32180	0.237E-12	0.0	0.974E 05	0.190E 04
7	48270	0.888E-13	0.0	0.560E 05	0.713E 03
7	64360	0.168E-12	0.0	0.144E 06	0.135E 04
7	80450	0.258E-13	0.0	0.282E 05	0.207E 03
8	1207	0.0	0.0	0.0	0.0
8	2414	0.0	0.0	0.0	0.0
8	4023	0.0	0.0	0.0	0.0
8	5632	0.0	0.0	0.0	0.0
8	7241	0.0	0.0	0.0	0.0
8	12068	0.0	0.0	0.0	0.0
8	20113	0.392E-12	0.0	0.109E 06	0.315E 04
8	32180	0.409E-12	0.0	0.185E 06	0.329E 04
8	48270	0.125E-12	0.0	0.873E 05	0.101E 04
8	64360	0.668E-13	0.0	0.635E 05	0.536E 03
8	80450	0.0	0.0	0.0	0.0
9	1207	0.0	0.0	0.0	0.0
9	2414	0.0	0.0	0.0	0.0
9	4023	0.0	0.0	0.0	0.0
9	5632	0.0	0.0	0.0	0.0
9	7241	0.0	0.0	0.0	0.0
9	12068	0.0	0.0	0.0	0.0
9	20113	0.0	0.0	0.0	0.0
9	32180	0.268E-11	0.0	0.655E 06	0.215E 05
9	48270	0.0	0.0	0.0	0.0
9	64360	0.142E-12	0.0	0.713E 05	0.114E 04
9	80450	0.0	0.0	0.0	0.0
10	1207	0.0	0.0	0.0	0.0
10	2414	0.0	0.0	0.0	0.0
10	4023	0.0	0.0	0.0	0.0
10	5632	0.0	0.0	0.0	0.0
10	7241	0.0	0.0	0.0	0.0
10	12068	0.237E-11	0.0	0.426E 06	0.191E 05
10	20113	0.0	0.0	0.0	0.0
10	32180	0.498E-12	0.0	0.245E 06	0.400E 04
10	48270	0.149E-12	0.0	0.113E 06	0.119E 04
10	64360	0.788E-13	0.0	0.823E 05	0.633E 03
10	80450	0.806E-13	0.0	0.108E 06	0.647E 03
11	1207	0.0	0.0	0.0	0.0
11	2414	0.0	0.0	0.0	0.0
11	4023	0.0	0.0	0.0	0.0
11	5632	0.0	0.0	0.0	0.0
11	7241	0.0	0.0	0.0	0.0
11	12068	0.155E-11	0.0	0.342E 06	0.125E 05
11	20113	0.142E-12	0.0	0.531E 05	0.114E 04
11	32180	0.0	0.0	0.0	0.0
11	48270	0.131E-12	0.0	0.127E 06	0.105E 04
11	64360	0.676E-13	0.0	0.901E 05	0.543E 03
11	80450	0.125E-14	0.0	0.213E 04	0.100E 02

12	1207	0.0	0.0	0.0	0.0
12	2414	0.0	0.0	0.0	0.0
12	4023	0.0	0.0	0.0	0.0
12	5632	0.0	0.0	0.0	0.0
12	7241	0.0	0.0	0.0	0.0
12	12068	0.0	0.0	0.0	0.0
12	20113	0.333E-12	0.0	0.137E 06	0.268E 04
12	32180	0.0	0.0	0.0	0.0
12	48270	0.139E-12	0.0	0.148E 06	0.112E 04
12	64360	0.401E-13	0.0	0.588E 05	0.322E 03
12	80450	0.529E-13	0.0	0.995E 05	0.425E 03
13	1207	0.0	0.0	0.0	0.0
13	2414	0.0	0.0	0.0	0.0
13	4023	0.0	0.0	0.0	0.0
13	5632	0.0	0.0	0.0	0.0
13	7241	0.0	0.0	0.0	0.0
13	12068	0.0	0.0	0.0	0.0
13	20113	0.437E-13	0.0	0.225E 05	0.351E 03
13	32180	0.0	0.0	0.0	0.0
13	48270	0.131E-13	0.0	0.177E 05	0.105E 03
13	64360	0.636E-14	0.0	0.118E 05	0.511E 02
13	80450	0.956E-13	0.0	0.228E 06	0.767E 03
14	1207	0.0	0.0	0.0	0.0
14	2414	0.0	0.0	0.0	0.0
14	4023	0.0	0.0	0.0	0.0
14	5632	0.0	0.0	0.0	0.0
14	7241	0.0	0.0	0.0	0.0
14	12068	0.0	0.0	0.0	0.0
14	20113	0.0	0.0	0.0	0.0
14	32180	0.391E-13	0.0	0.325E 05	0.314E 03
14	48270	0.213E-13	0.0	0.278E 05	0.171E 03
14	64360	0.153E-12	0.0	0.276E 06	0.123E 04
14	80450	0.292E-12	0.0	0.675E 06	0.234E 04
15	1207	0.0	0.0	0.0	0.0
15	2414	0.0	0.0	0.0	0.0
15	4023	0.0	0.0	0.0	0.0
15	5632	0.0	0.0	0.0	0.0
15	7241	0.0	0.0	0.0	0.0
15	12068	0.0	0.0	0.0	0.0
15	20113	0.0	0.0	0.0	0.0
15	32180	0.0	0.0	0.0	0.0
15	48270	0.231E-13	0.0	0.246E 05	0.186E 03
15	64360	0.404E-13	0.0	0.591E 05	0.324E 03
15	80450	0.193E-12	0.0	0.363E 06	0.155E 04
16	1207	0.0	0.0	0.0	0.0
16	2414	0.0	0.0	0.0	0.0
16	4023	0.0	0.0	0.0	0.0
16	5632	0.468E-12	0.0	0.572E 05	0.376E 04
16	7241	0.0	0.0	0.0	0.0
16	12068	0.0	0.0	0.0	0.0
16	20113	0.0	0.0	0.0	0.0
16	32180	0.0	0.0	0.0	0.0
16	48270	0.151E-13	0.0	0.204E 05	0.122E 03
16	64360	0.421E-13	0.0	0.786E 05	0.338E 03
16	80450	0.763E-12	0.0	0.183E 07	0.613E 04

DIRECTIONS ARE NUMBERED COUNTERCLOCKWISE STARTING AT 1 FOR DUE NORTH

PERCENT OF TOT.BODY DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.8401E-09	0.00	99.76
	SURFACE	0.6896E-03	0.00	62.31
	SWIMMING	0.4223E-06	0.00	87.03
	INHAL.	0.1590E-02	0.01	73.40
	INGEST.	0.1535E 02	99.99	91.87
	VEGET.	0.1414E 02	* 92.11	* 84.63
	MEAT	0.9797E 00	* 6.38	* 5.87
	MILK	0.2296E 00	* 1.50	* 1.37
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.4167E-03	0.08	37.65
	SWIMMING	0.6256E-07	0.00	12.89
	INHAL.	0.0	0.0	0.0
	INGEST.	0.5011E 00	99.92	3.00
	VEGET.	0.4115E 00	* 82.05	* 2.46
	MEAT	0.7929E-01	* 15.81	* 0.47
	MILK	0.1029E-01	* 2.05	* 0.06
PO-210	SUBM AIR	0.2022E-11	0.00	0.24
	SURFACE	0.4935E-06	0.00	0.04
	SWIMMING	0.3587E-09	0.00	0.07
	INHAL.	0.5506E-03	0.06	25.42
	INGEST.	0.8549E 00	99.94	5.12
	VEGET.	0.7366E 00	* 86.11	* 4.41
	MEAT	0.1138E 00	* 13.30	* 0.68
	MILK	0.4453E-02	* 0.52	* 0.03
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2575E-04	1.75	1.19
	INGEST.	0.1442E-02	98.25	0.01
	VEGET.	0.7273E-03	* 49.56	* 0.00
	MEAT	0.2664E-03	* 18.16	* 0.00
	MILK	0.4464E-03	* 30.42	* 0.00

PERCENT OF R MAN DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.1206E-08	0.00	99.82
	SURFACE	0.9898E-03	0.03	60.12
	SWIMMING	0.6062E-06	0.00	85.97
	INHAL.	0.3388E-03	0.01	50.86
	INGEST.	0.3615E 01	99.96	79.34
	VEGET.	0.3330E 01	* 92.09	* 73.09
	MEAT	0.2308E 00	* 6.38	* 5.07
	MILK	0.5408E-01	* 1.50	* 1.19
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.6561E-03	0.67	39.85
	SWIMMING	0.9851E-07	0.00	13.97
	INHAL.	0.0	0.0	0.0
	INGEST.	0.9707E-01	99.33	2.13
	VEGET.	0.7972E-01	* 81.57	* 1.75
	MEAT	0.1536E-01	* 15.72	* 0.34
	MILK	0.1994E-02	* 2.04	* 0.04
PO-210	SUBM AIR	0.2140E-11	0.00	0.18
	SURFACE	0.5224E-06	0.00	0.03
	SWIMMING	0.3797E-09	0.00	0.05
	INHAL.	0.3018E-03	0.04	45.30
	INGEST.	0.8427E 00	99.96	18.50
	VEGET.	0.7261E 00	* 86.13	* 15.94
	MEAT	0.1122E 00	* 13.31	* 2.46
	MILK	0.4390E-02	* 0.52	* 0.10
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2554E-04	1.74	3.83
	INGEST.	0.1442E-02	98.26	0.03
	VEGET.	0.7273E-03	* 49.57	* 0.02
	MEAT	0.2664E-03	* 18.16	* 0.01
	MILK	0.4464E-03	* 30.43	* 0.01

PERCENT OF LUNGS DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.7406E-09	0.00	99.74
	SURFACE	0.6079E-03	5.76	69.05
	SWIMMING	0.3723E-06	0.00	90.04
	INHAL.	0.9830E-02	93.20	37.78
	INGEST.	0.1089E-03	1.03	7.00
	VEGET.	0.1003E-03	* 0.95	* 6.45
	MEAT	0.6950E-05	* 0.07	* 0.45
	MILK	0.1629E-05	* 0.02	* 0.10
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.2721E-03	98.56	30.90
	SWIMMING	0.4085E-07	0.01	9.88
	INHAL.	0.0	0.0	0.0
	INGEST.	0.3924E-05	1.42	0.25
	VEGET.	0.3223E-05	* 1.17	* 0.21
	MEAT	0.6209E-06	* 0.22	* 0.04
	MILK	0.8061E-07	* 0.03	* 0.01
PO-210	SUBM AIR	0.1903E-11	0.00	0.26
	SURFACE	0.4647E-06	0.00	0.05
	SWIMMING	0.3377E-09	0.00	0.08
	INHAL.	0.1617E-01	100.00	62.12
	INGEST.	0.1719E-07	0.00	0.00
	VEGET.	0.1481E-07	* 0.00	* 0.00
	MEAT	0.2288E-08	* 0.00	* 0.00
	MILK	0.8953E-10	* 0.00	* 0.00
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2575E-04	1.75	0.10
	INGEST.	0.1442E-02	98.25	92.74
	VEGET.	0.7273E-03	* 49.56	* 46.79
	MEAT	0.2664E-03	* 18.16	* 17.14
	MILK	0.4464E-03	* 30.42	* 28.72

PERCENT OF ENDOST DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.1397E-08	0.00	99.83
	SURFACE	0.1147E-02	0.01	56.82
	SWIMMING	0.7022E-06	0.00	84.26
	INHAL.	0.1747E-02	0.01	91.98
	INGEST.	0.1864E 02	99.98	94.77
	VEGET.	0.1717E 02	* 92.11	* 87.30
	MEAT	0.1190E 01	* 6.38	* 6.05
	MILK	0.2789E 00	* 1.50	* 1.42
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.8706E-03	0.13	43.15
	SWIMMING	0.1307E-06	0.00	15.69
	INHAL.	0.0	0.0	0.0
	INGEST.	0.6590E 00	99.87	3.35
	VEGET.	0.5412E 00	* 82.01	* 2.75
	MEAT	0.1043E 00	* 15.80	* 0.53
	MILK	0.1354E-01	* 2.05	* 0.07
PO-210	SUBM AIR	0.2441E-11	0.00	0.17
	SURFACE	0.5959E-06	0.00	0.03
	SWIMMING	0.4331E-09	0.00	0.05
	INHAL.	0.1320E-03	0.04	6.95
	INGEST.	0.3681E 00	99.96	1.87
	VEGET.	0.3172E 00	* 86.13	* 1.61
	MEAT	0.4901E-01	* 13.31	* 0.25
	MILK	0.1917E-02	* 0.52	* 0.01
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2029E-04	1.39	1.07
	INGEST.	0.1442E-02	98.61	0.01
	VEGET.	0.7273E-03	* 49.75	* 0.00
	MEAT	0.2664E-03	* 18.22	* 0.00
	MILK	0.4464E-03	* 30.54	* 0.00

PERCENT OF S WALL DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.5477E-09	0.00	99.67
	SURFACE	0.4495E-03	4.64	66.03
	SWIMMING	0.2753E-06	0.00	88.72
	INHAL.	0.4765E-06	0.00	1.76
	INGEST.	0.9237E-02	95.35	52.49
	VEGET.	0.8509E-02	* 87.84	* 48.35
	MEAT	0.5897E-03	* 6.09	* 3.35
	MILK	0.1382E-03	* 1.43	* 0.79
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.2309E-03	94.69	33.91
	SWIMMING	0.3467E-07	0.01	11.17
	INHAL.	0.0	0.0	0.0
	INGEST.	0.1292E-04	5.30	0.07
	VEGET.	0.1061E-04	* 4.35	* 0.06
	MEAT	0.2044E-05	* 0.84	* 0.01
	MILK	0.2654E-06	* 0.11	* 0.00
PO-210	SUBM AIR	0.1808E-11	0.00	0.33
	SURFACE	0.4414E-06	0.01	0.06
	SWIMMING	0.3208E-09	0.00	0.10
	INHAL.	0.7836E-06	0.01	2.90
	INGEST.	0.6906E-02	99.98	39.24
	VEGET.	0.5950E-02	* 86.15	* 33.81
	MEAT	0.9194E-03	* 13.31	* 5.22
	MILK	0.3597E-04	* 0.52	* 0.20
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2575E-04	1.75	95.33
	INGEST.	0.1442E-02	98.25	8.19
	VEGET.	0.7273E-03	* 49.56	* 4.13
	MEAT	0.2664E-03	* 18.16	* 1.51
	MILK	0.4464E-03	* 30.42	* 2.54

PERCENT OF LLI WALL DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.4593E-09	0.00	99.71
	SURFACE	0.3770E-03	0.05	74.11
	SWIMMING	0.2309E-06	0.00	92.04
	INHAL.	0.3159E-04	0.00	35.10
	INGEST.	0.7039E 00	99.94	71.90
	VEGET.	0.6484E 00	* 92.07	* 66.23
	MEAT	0.4494E-01	* 6.38	* 4.59
	MILK	0.1053E-01	* 1.50	* 1.08
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.1314E-03	8.65	25.83
	SWIMMING	0.1973E-07	0.00	7.86
	INHAL.	0.0	0.0	0.0
	INGEST.	0.1388E-02	91.35	0.14
	VEGET.	0.1140E-02	* 75.02	* 0.12
	MEAT	0.2196E-03	* 14.45	* 0.02
	MILK	0.2851E-04	* 1.88	* 0.00
PO-210	SUBM AIR	0.1353E-11	0.00	0.29
	SURFACE	0.3303E-06	0.00	0.06
	SWIMMING	0.2401E-09	0.00	0.10
	INHAL.	0.3102E-04	0.01	34.47
	INGEST.	0.2723E 00	99.99	27.81
	VEGET.	0.2346E 00	* 86.16	* 23.96
	MEAT	0.3625E-01	* 13.31	* 3.70
	MILK	0.1418E-02	* 0.52	* 0.14
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2739E-04	1.86	30.44
	INGEST.	0.1442E-02	98.14	0.15
	VEGET.	0.7273E-03	* 49.51	* 0.07
	MEAT	0.2664E-03	* 18.14	* 0.03
	MILK	0.4464E-03	* 30.39	* 0.05

PERCENT OF THYROID DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.8381E-09	0.00	99.82
	SURFACE	0.6879E-03	0.06	62.92
	SWIMMING	0.4213E-06	0.00	87.34
	INHAL.	0.1172E-03	0.01	27.50
	INGEST.	0.1249E 01	99.94	61.08
	VEGET.	0.1151E 01	* 92.06	* 56.27
	MEAT	0.7976E-01	* 6.38	* 3.90
	MILK	0.1869E-01	* 1.50	* 0.91
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.4050E-03	16.35	37.04
	SWIMMING	0.6081E-07	0.00	12.61
	INHAL.	0.0	0.0	0.0
	INGEST.	0.2071E-02	83.64	0.10
	VEGET.	0.1701E-02	* 68.69	* 0.08
	MEAT	0.3278E-03	* 13.24	* 0.02
	MILK	0.4255E-04	* 1.72	* 0.00
PO-210	SUBM AIR	0.1548E-11	0.00	0.18
	SURFACE	0.3780E-06	0.00	0.03
	SWIMMING	0.2747E-09	0.00	0.06
	INHAL.	0.2834E-03	0.04	66.51
	INGEST.	0.7925E 00	99.96	38.75
	VEGET.	0.6829E 00	* 86.13	* 33.39
	MEAT	0.1055E 00	* 13.31	* 5.16
	MILK	0.4128E-02	* 0.52	* 0.20
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2554E-04	1.74	5.99
	INGEST.	0.1442E-02	98.26	0.07
	VEGET.	0.7273E-03	* 49.57	* 0.04
	MEAT	0.2664E-03	* 18.16	* 0.01
	MILK	0.4464E-03	* 30.43	* 0.02

PERCENT OF LIVER DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.6401E-09	0.00	99.73
	SURFACE	0.5254E-03	0.04	70.74
	SWIMMING	0.3218E-06	0.00	90.73
	INHAL.	0.1168E-03	0.01	11.48
	INGEST.	0.1247E 01	99.95	32.85
	VEGET.	0.1149E 01	* 92.07	* 30.26
	MEAT	0.7962E-01	* 6.38	* 2.10
	MILK	0.1866E-01	* 1.50	* 0.49
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.2169E-03	0.22	29.20
	SWIMMING	0.3257E-07	0.00	9.18
	INHAL.	0.0	0.0	0.0
	INGEST.	0.9844E-01	99.78	2.59
	VEGET.	0.8084E-01	* 81.94	* 2.13
	MEAT	0.1558E-01	* 15.79	* 0.41
	MILK	0.2022E-02	* 2.05	* 0.05
PO-210	SUBM AIR	0.1728E-11	0.00	0.27
	SURFACE	0.4220E-06	0.00	0.06
	SWIMMING	0.3067E-09	0.00	0.09
	INHAL.	0.8753E-03	0.04	86.01
	INGEST.	0.2449E 01	99.96	64.52
	VEGET.	0.2110E 01	* 86.13	* 55.59
	MEAT	0.3261E 00	* 13.31	* 8.59
	MILK	0.1276E-01	* 0.52	* 0.34
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2554E-04	1.74	2.51
	INGEST.	0.1442E-02	98.26	0.04
	VEGET.	0.7273E-03	* 49.57	* 0.02
	MEAT	0.2664E-03	* 18.16	* 0.01
	MILK	0.4464E-03	* 30.43	* 0.01

PERCENT OF KIDNEYS DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.6070E-09	0.00	99.69
	SURFACE	0.4982E-03	0.04	67.43
	SWIMMING	0.3051E-06	0.00	89.34
	INHAL.	0.1168E-03	0.01	2.24
	INGEST.	0.1247E 01	99.95	7.98
	VEGET.	0.1149E 01	* 92.07	* 7.35
	MEAT	0.7962E-01	* 6.38	* 0.51
	MILK	0.1866E-01	* 1.50	* 0.12
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.2402E-03	0.12	32.51
	SWIMMING	0.3607E-07	0.00	10.56
	INHAL.	0.0	0.0	0.0
	INGEST.	0.2071E 00	99.88	1.33
	VEGET.	0.1701E 00	* 82.03	* 1.09
	MEAT	0.3278E-01	* 15.81	* 0.21
	MILK	0.4255E-02	* 2.05	* 0.03
PO-210	SUBM AIR	0.1867E-11	0.00	0.31
	SURFACE	0.4559E-06	0.00	0.06
	SWIMMING	0.3313E-09	0.00	0.10
	INHAL.	0.5083E-02	0.04	97.26
	INGEST.	0.1418E 02	99.96	90.69
	VEGET.	0.1222E 02	* 86.13	* 78.14
	MEAT	0.1887E 01	* 13.31	* 12.07
	MILK	0.7385E-01	* 0.52	* 0.47
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2657E-04	1.81	0.51
	INGEST.	0.1442E-02	98.19	0.01
	VEGET.	0.7273E-03	* 49.54	* 0.00
	MEAT	0.2664E-03	* 18.15	* 0.00
	MILK	0.4464E-03	* 30.41	* 0.00

PERCENT OF TESTES DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.1025E-08	0.00	99.81
	SURFACE	0.8413E-03	0.07	69.38
	SWIMMING	0.5153E-06	0.00	90.19
	INHAL.	0.1172E-03	0.01	27.48
	INGEST.	0.1249E 01	99.92	61.08
	VEGET.	0.1151E 01	* 92.05	* 56.27
	MEAT	0.7976E-01	* 6.38	* 3.90
	MILK	0.1869E-01	* 1.49	* 0.91
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.3708E-03	15.18	30.58
	SWIMMING	0.5568E-07	0.00	9.75
	INHAL.	0.0	0.0	0.0
	INGEST.	0.2071E-02	84.82	0.10
	VEGET.	0.1701E-02	* 69.65	* 0.08
	MEAT	0.3278E-03	* 13.42	* 0.02
	MILK	0.4255E-04	* 1.74	* 0.00
PO-210	SUBM AIR	0.1975E-11	0.00	0.19
	SURFACE	0.4822E-06	0.00	0.04
	SWIMMING	0.3505E-09	0.00	0.06
	INHAL.	0.2834E-03	0.04	66.48
	INGEST.	0.7925E 00	99.96	38.75
	VEGET.	0.6829E 00	* 86.13	* 33.39
	MEAT	0.1055E 00	* 13.31	* 5.16
	MILK	0.4128E-02	* 0.52	* 0.20
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2575E-04	1.75	6.04
	INGEST.	0.1442E-02	98.25	0.07
	VEGET.	0.7273E-03	* 49.56	* 0.04
	MEAT	0.2664E-03	* 18.16	* 0.01
	MILK	0.4464E-03	* 30.42	* 0.02

PERCENT OF OVARIES DOSE BY EACH PATHWAY

NUCLIDE	PATHWAY	DOSE(MAN-REMS)	PERCENT OF TOTAL	PERCENT OF DOSE FROM ALL NUCLIDES
RA-226	SUBM AIR	0.4402E-09	0.00	99.76
	SURFACE	0.3613E-03	0.03	62.21
	SWIMMING	0.2213E-06	0.00	86.99
	INHAL.	0.1172E-03	0.01	27.50
	INGEST.	0.1251E 01	99.96	61.12
	VEGET.	0.1153E 01	* 92.08	* 56.30
	MEAT	0.7989E-01	* 6.38	* 3.90
	MILK	0.1872E-01	* 1.50	* 0.91
PB-210	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.2192E-03	9.57	37.75
	SWIMMING	0.3292E-07	0.00	12.94
	INHAL.	0.0	0.0	0.0
	INGEST.	0.2071E-02	90.43	0.10
	VEGET.	0.1701E-02	* 74.26	* 0.08
	MEAT	0.3278E-03	* 14.31	* 0.02
	MILK	0.4255E-04	* 1.86	* 0.00
PO-210	SUBM AIR	0.1047E-11	0.00	0.24
	SURFACE	0.2556E-06	0.00	0.04
	SWIMMING	0.1858E-09	0.00	0.07
	INHAL.	0.2834E-03	0.04	66.51
	INGEST.	0.7925E 00	99.96	38.71
	VEGET.	0.6829E 00	* 86.13	* 33.35
	MEAT	0.1055E 00	* 13.31	* 5.15
	MILK	0.4128E-02	* 0.52	* 0.20
RN-222	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.0	0.0	0.0
	INGEST.	0.0	0.0	0.0
	VEGET.	0.0	* 0.0	* 0.0
	MEAT	0.0	* 0.0	* 0.0
	MILK	0.0	* 0.0	* 0.0
H-3	SUBM AIR	0.0	0.0	0.0
	SURFACE	0.0	0.0	0.0
	SWIMMING	0.0	0.0	0.0
	INHAL.	0.2554E-04	1.74	5.99
	INGEST.	0.1442E-02	98.26	0.07
	VEGET.	0.7273E-03	* 49.57	* 0.04
	MEAT	0.2664E-03	* 18.16	* 0.01
	MILK	0.4464E-03	* 30.43	* 0.02

CONTRIBUTION OF EXPOSURE MODES TO TOT.BODY DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.8421E-09	0.0000
SURFACE	0.1107E-02	0.0066
SWIMMING	0.4852E-06	0.0000
INHAL.	0.2166E-02	0.0130
INGEST.	0.1670E 02	99.9804
VEGET.	*0.1529E 02	* 91.4937
MEAT	*0.1173E 01	* 7.0218
MILK	*0.2448E 00	* 1.4651

CONTRIBUTION OF EXPOSURE MODES TO R MAR DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.1208E-08	0.0000
SURFACE	0.1646E-02	0.0361
SWIMMING	0.7051E-06	0.0000
INHAL.	0.6662E-03	0.0146
INGEST.	0.4556E 01	99.9492
VEGET.	*0.4136E 01	* 90.7460
MEAT	*0.3586E 00	* 7.8670
MILK	*0.6091E-01	* 1.3362

CONTRIBUTION OF EXPOSURE MODES TO LUNGS DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.7425E-09	0.0000
SURFACE	0.8804E-03	3.0940
SWIMMING	0.4135E-06	0.0015
INHAL.	0.2602E-01	91.4422
INGEST.	0.1554E-02	5.4624
VEGET.	*0.8308E-03	* 2.9195
MEAT	*0.2740E-03	* 0.9629
MILK	*0.4481E-03	* 1.5748

CONTRIBUTION OF EXPOSURE MODES TO ENDOST DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.1399E-08	0.0000
SURFACE	0.2018E-02	0.0103
SWIMMING	0.8333E-06	0.0000
INHAL.	0.1899E-02	0.0097
INGEST.	0.1967E 02	99.9801
VEGET.	*0.1803E 02	* 91.6523
MEAT	*0.1344E 01	* 6.8297
MILK	*0.2948E 00	* 1.4983

CONTRIBUTION OF EXPOSURE MODES TO S WALL DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.5495E-09	0.0000
SURFACE	0.6809E-03	3.7193
SWIMMING	0.3103E-06	0.0017
INHAL.	0.2701E-04	0.1475
INGEST.	0.1760E-01	96.1314
VEGET.	*0.1520E-01	* 83.0211
MEAT	*0.1778E-02	* 9.7107
MILK	*0.6209E-03	* 3.3916

CONTRIBUTION OF EXPOSURE MODES TO LLI WALL DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.4606E-09	0.0000
SURFACE	0.5087E-03	0.0519
SWIMMING	0.2508E-06	0.0000
INHAL.	0.9001E-04	0.0092
INGEST.	0.9790E 00	99.9388
VEGET.	*0.8849E 00	* 90.3329
MEAT	*0.8167E-01	* 8.3376
MILK	*0.1242E-01	* 1.2682

CONTRIBUTION OF EXPOSURE MODES TO THYROID DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.8397E-09	0.0000
SURFACE	0.1093E-02	0.0534
SWIMMING	0.4824E-06	0.0000
INHAL.	0.4261E-03	0.0208
INGEST.	0.2045E 01	99.9258
VEGET.	*0.1836E 01	* 89.7065
MEAT	*0.1859E 00	* 9.0806
MILK	*0.2331E-01	* 1.1387

CONTRIBUTION OF EXPOSURE MODES TO LIVER DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.6419E-09	0.0000
SURFACE	0.7427E-03	0.0196
SWIMMING	0.3547E-06	0.0000
INHAL.	0.1018E-02	0.0268
INGEST.	0.3796E 01	99.9536
VEGET.	*0.3341E 01	* 87.9624
MEAT	*0.4215E 00	* 11.0990
MILK	*0.3388E-01	* 0.8922

CONTRIBUTION OF EXPOSURE MODES TO KIDNEYS DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.6088E-09	0.0000
SURFACE	0.7389E-03	0.0047
SWIMMING	0.3415E-06	0.0000
INHAL.	0.5226E-02	0.0334
INGEST.	0.1563E 02	99.9619
VEGET.	*0.1354E 02	* 86.5506
MEAT	*0.2000E 01	* 12.7895
MILK	*0.9721E-01	* 0.6216

CONTRIBUTION OF EXPOSURE MODES TO TESTES DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.1027E-08	0.0000
SURFACE	0.1213E-02	0.0592
SWIMMING	0.5713E-06	0.0000
INHAL.	0.4264E-03	0.0208
INGEST.	0.2045E 01	99.9199
VEGET.	*0.1836E 01	* 89.7012
MEAT	*0.1859E 00	* 9.0800
MILK	*0.2331E-01	* 1.1386

CONTRIBUTION OF EXPOSURE MODES TO OVARIES DOSES

EXPOSURE MODE	ANNUAL DOSE(MAN-REMS)	PERCENT OF TOTAL DOSE
SUBM AIR	0.4412E-09	0.0000
SURFACE	0.5807E-03	0.0284
SWIMMING	0.2544E-06	0.0000
INHAL.	0.4261E-03	0.0208
INGEST.	0.2047E 01	99.9508
VEGET.	*0.1838E 01	* 89.7314
MEAT	*0.1860E 00	* 9.0801
MILK	*0.2334E-01	* 1.1393

TOTAL DOSE TO EACH ORGAN THROUGH ALL PATHWAYS

ORGAN	DOSE(MAN-REMS)
TOT.BODY	0.1671E 02
R MAR	0.4558E 01
LUNGS	0.2846E-01
ENDOST	0.1968E 02
S WALL	0.1831E-01
LLI WALL	0.9796E 00
THYROID	0.2047E 01
LIVER	0.3798E 01
KIDNEYS	0.1564E 02
TESTES	0.2047E 01
OVARIES	0.2048E 01

CONTRIBUTORS TO ORGAN DOSES

PERCENT

NUCLIDE	TOT. BODY	R MAR	LUNGS	ENDOST	S WALL	LLI WALL	THYROID	LIVER	KIDNEYS	TESTES	OVARIES
RA-226	91.8693	79.3290	37.0638	94.7674	52.9205	71.8967	61.0738	32.8553	7.9786	61.0778	61.1133
PB-210	3.0019	2.1441	0.9700	3.3538	1.3320	0.1551	0.1210	2.5978	1.3261	0.1193	0.1118
PO-210	5.1202	18.4947	56.8097	1.8715	37.7318	27.7983	38.7335	64.5082	90.6859	38.7313	38.7033
RN-222	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
H-3	0.0088	0.0322	5.1564	0.0074	8.0157	0.1500	0.0717	0.0386	0.0094	0.0717	0.0716

ANNUAL POPULATION DOSES(MAN-REMS)

NUCLIDE	ORGAN	DOSE
RA-226	TOT.BODY	0.1535E 02
RA-226	R MAR	0.3616E 01
RA-226	LUNGS	0.1055E-01
RA-226	ENDOST	0.1865E 02
RA-226	S WALL	0.9687E-02
RA-226	LLI WALL	0.7043E 00
RA-226	THYROID	0.1250E 01
RA-226	LIVER	0.1248E 01
RA-226	KIDNEYS	0.1248E 01
RA-226	TESTES	0.1250E 01
RA-226	OVARIES	0.1252E 01
PB-210	TOT.BODY	0.5015E 00
PB-210	R MAR	0.9773E-01
PB-210	LUNGS	0.2760E-03
PB-210	ENDOST	0.6599E 00
PB-210	S WALL	0.2438E-03
PB-210	LLI WALL	0.1519E-02
PB-210	THYROID	0.2476E-02
PB-210	LIVER	0.9866E-01
PB-210	KIDNEYS	0.2074E 00
PB-210	TESTES	0.2442E-02
PB-210	OVARIES	0.2291E-02
PO-210	TOT.BODY	0.8554E 00
PO-210	R MAR	0.8430E 00
PO-210	LUNGS	0.1617E-01
PO-210	ENDOST	0.3682E 00
PO-210	S WALL	0.6907E-02
PO-210	LLI WALL	0.2723E 00
PO-210	THYROID	0.7928E 00
PO-210	LIVER	0.2450E 01

PO-210	KIDNEYS	0.1418E 02
PO-210	TESTES	0.7928E 00
PO-210	OVARIES	0.7928E 00
RN-222	TOT.BODY	0.0
RN-222	R MAR	0.0
RN-222	LUNGS	0.0
RN-222	ENDOST	0.0
RN-222	S WALL	0.0
RN-222	LLI WALL	0.0
RN-222	THYROID	0.0
RN-222	LIVER	0.0
RN-222	KIDNEYS	0.0
RN-222	TESTES	0.0
RN-222	OVARIES	0.0
H-3	TOT.BODY	0.1467E-02
H-3	R MAR	0.1467E-02
H-3	LUNGS	0.1467E-02
H-3	ENDOST	0.1462E-02
H-3	S WALL	0.1467E-02
H-3	LLI WALL	0.1469E-02
H-3	THYROID	0.1467E-02
H-3	LIVER	0.1467E-02
H-3	KIDNEYS	0.1468E-02
H-3	TESTES	0.1467E-02
H-3	OVARIES	0.1467E-02

WORKING LEVELS FOR RN-222 AND ITS SHORT-LIFE PROGENY AT VARIOUS LOCATIONS IN THE ENVIRONMENT
(FRACTION OF EQUILIBRIUM ASSUMED FOR WORKING LEVEL CALCULATIONS=0.700)

AREA		WORKING LEVEL (POPULATION)
WIND TOWARD	DISTANCE (METERS)	
1	1207	0.0
1	2414	0.0
1	4023	0.0
1	5632	0.0
1	7241	0.0
1	12068	0.779E-06
1	20113	0.0
1	32180	0.0
1	48270	0.198E-07
1	64360	0.851E-06
1	80450	0.490E-05
2	1207	0.0
2	2414	0.0
2	4023	0.0
2	5632	0.0
2	7241	0.0
2	12068	0.0
2	20113	0.196E-05
2	32180	0.523E-06
2	48270	0.146E-05
2	64360	0.494E-06
2	80450	0.345E-06
3	1207	0.0
3	2414	0.0
3	4023	0.0
3	5632	0.0
3	7241	0.0
3	12068	0.0
3	20113	0.0
3	32180	0.0
3	48270	0.406E-05
3	64360	0.383E-05
3	80450	0.124E-05
4	1207	0.0
4	2414	0.0
4	4023	0.0
4	5632	0.0
4	7241	0.0
4	12068	0.0
4	20113	0.136E-05
4	32180	0.104E-05
4	48270	0.160E-05
4	64360	0.986E-05
4	80450	0.124E-04
5	1207	0.0
5	2414	0.0
5	4023	0.0
5	5632	0.0
5	7241	0.0
5	12068	0.119E-05
5	20113	0.132E-05
5	32180	0.0

5	48270	0.186E-06
5	64360	0.114E-06
5	80450	0.522E-05
6	1207	0.0
6	2414	0.181E-04
6	4023	0.0
6	5632	0.0
6	7241	0.0
6	12068	0.0
6	20113	0.0
6	32180	0.525E-06
6	48270	0.348E-06
6	64360	0.755E-05
6	80450	0.535E-05
7	1207	0.0
7	2414	0.0
7	4023	0.0
7	5632	0.0
7	7241	0.0
7	12068	0.0
7	20113	0.0
7	32180	0.157E-05
7	48270	0.572E-06
7	64360	0.105E-05
7	80450	0.157E-06
8	1207	0.0
8	2414	0.0
8	4023	0.0
8	5632	0.0
8	7241	0.0
8	12068	0.0
8	20113	0.266E-05
8	32180	0.273E-05
8	48270	0.816E-06
8	64360	0.424E-06
8	80450	0.0
9	1207	0.0
9	2414	0.0
9	4023	0.0
9	5632	0.0
9	7241	0.0
9	12068	0.0
9	20113	0.0
9	32180	0.179E-04
9	48270	0.0
9	64360	0.911E-06
9	80450	0.0
10	1207	0.0
10	2414	0.0
10	4023	0.0
10	5632	0.0
10	7241	0.0
10	12068	0.163E-04
10	20113	0.0
10	32180	0.333E-05
10	48270	0.971E-06
10	64360	0.503E-06
10	80450	0.503E-06
11	1207	0.0
11	2414	0.0
11	4023	0.0
11	5632	0.0
11	7241	0.0
11	12068	0.107E-04
11	20113	0.962E-06
11	32180	0.0

11	48270	0.847E-06
11	64360	0.427E-06
11	80450	0.767E-08
12	1207	0.0
12	2414	0.0
12	4023	0.0
12	5632	0.0
12	7241	0.0
12	12068	0.0
12	20113	0.226E-05
12	32180	0.0
12	48270	0.898E-06
12	64360	0.252E-06
12	80450	0.324E-06
13	1207	0.0
13	2414	0.0
13	4023	0.0
13	5632	0.0
13	7241	0.0
13	12068	0.0
13	20113	0.296E-06
13	32180	0.0
13	48270	0.847E-07
13	64360	0.399E-07
13	80450	0.584E-06
14	1207	0.0
14	2414	0.0
14	4023	0.0
14	5632	0.0
14	7241	0.0
14	12068	0.0
14	20113	0.0
14	32180	0.260E-06
14	48270	0.138E-06
14	64360	0.967E-06
14	80450	0.179E-05
15	1207	0.0
15	2414	0.0
15	4023	0.0
15	5632	0.0
15	7241	0.0
15	12068	0.0
15	20113	0.0
15	32180	0.0
15	48270	0.149E-06
15	64360	0.254E-06
15	80450	0.118E-05
16	1207	0.0
16	2414	0.0
16	4023	0.0
16	5632	0.325E-05
16	7241	0.0
16	12068	0.0
16	20113	0.0
16	32180	0.0
16	48270	0.984E-07
16	64360	0.267E-06
16	80450	0.471E-05

COLLECTIVE WORKING LEVEL= 0.168E-03

*U.S. GOVERNMENT PRINTING OFFICE: 1980 311-132/3 1-3