# LEAD EXPOSURE ASSOCIATED WITH RENOVATION AND REMODELING ACTIVITIES: 

## ENVIRONMENTAL FIELD SAMPLING STUDY VOLUME II: APPENDICES

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APPENDIX A SUPPORTING TABLES AND FIGURES OF EFSS DATA

## A. 0 SUPPORT TABLES AND FIGURES OF EFSS DATA

## A. 1 DESCRIPTIVE STATISTICS ON SAMPLE WEIGHTS, LEAD LOADINGS, AND LEAD CONCENTRATIONS BY SAMPLE TYPE, IN THE CARPET REMOVAL PHASE

This section presents descriptive summaries on lead exposure data for the various sample types considered in the EFSS carpet removal substudy. These summaries, cited in Chapters 6 and 7A, are presented within six sets of tables, grouped according to the sample type considered:

Total number of samples collected and analyzed: Table CR-1.
Personal and ambient air results: Tables CR-2a, CR-2b.
Pre- and post-activity floor vacuum dust results: Tables CR-3a through CR-3d.
Stainless steel dustfall collector (SSDC) dust sample results using vacuum techniques, collected at 1-hour and 2-hours following the activity: Tables CR-4a through CR-4d.

Pre- and post-activity window sill dust results: Tables CR-5a through CR-5d.
SSDC dust sample results collected at 1-hour following the activity, using vacuum and wipe techniques: Tables CR-6a, CR-6b.

Table CR-1 reports the number of samples planned, the number of samples collected, and the number of analytical results received. The remaining tables present summary statistics, such as the number of samples with nonmissing data values, the arithmetic and geometric means, the standard deviation of the log-transformed data, and the minimum and maximum data values. Within each set of tables, the first table represents statistics over all study data, while subsequent tables include statistics calculated for each study unit. Lead exposure data summarized in these tables include the physical sample weights ( g ) and lead concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) for vacuum samples, lead loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) for vacuum and wipe samples, and lead concentrations ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) for personal air and ambient air samples. The personal air lead concentrations are expressed in terms of task-length average (TLA) exposures for a given worker, defined as the average exposure over the duration of activity.

Sample types are placed within a given set of tables above so that their results can be compared. Therefore, these tables also include differences in sample results between pairs of adjoining samples at a given location. Tables CR-3a and CR-3b consider differences in results between adjoining pre- and post-activity floor dust samples. Tables CR-4a through CR-4d consider differences between 1-hour and 2-hour results from SSDC vacuum dust samples. Tables CR-5a through CR-5d include differences in results between adjoining pre- and postactivity window sill samples, and Tables CR-6a through CR-6b include differences between 1hour vacuum and wipe SSDC sample results. The same statistics are presented for the paired differences as for the individual sample results. However, the statistic identified as the "geometric mean" represents the geometric mean of the ratio between the two adjoining sample results at a given location (e.g., post- vs. pre-activity, 2-hour vs. 1-hour, wipe vs. vacuum).

In addition to the above tables, this section also includes boxplots of lead loading and concentration data for the different types of settled dust samples. Figures CR-1a and CR-1b present lead loading and concentration data, respectively, for the three types of settled dust samples collected prior to the start of carpet removal activity (pre-activity carpet data, window sill data, and floor data). Figures CR-2a and CR-2b contain boxplots for lead loading and concentration data, respectively, for the five types of settled dust samples collected following completion of carpet removal activities (1-hour vacuum from floors and SSDCs, 1-hour wipe from SSDCs, and 2-hour vacuum from SSDCs). Chapter 5 includes a discussion of how to interpret boxplots, as well as the boxplots for personal air and ambient air sample lead loadings.

Table CR-1. Numbers of Field Samples Collected and Results Reported in the EFSS Carpet Removal Substudy, by Study Unit

| Unit ID | Number of Proposed Samples ${ }^{(1)}$ |  | Number of <br> Proposed Samples <br> Collected ${ }^{(2)}$ |  | Number of Extra Samples Collected ${ }^{(3)}$ | Total Number of Samples Collected | Number of Analytical Results Received |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Reg. | QC | Reg. | QC |  |  |  |
| 1-01 | 26 | 9 | 26 | 9 | 2 | 37 | 37 |
| 1-02 | 26 | 9 | 26 | 9 | 0 | 35 | 35 |
| 1-03 | 26 | 9 | 26 | 9 | 0 | 35 | 35 |
| 1-04 | 26 | 9 | 26 | 9 | 0 | 35 | 35 |
| 2-01 | 26 | 9 | 25 | 9 | 0 | 34 | 34 |
| 2-02 | 26 | 9 | 26 | 9 | 0 | 35 | 35 |
| 2-03 | 26 | 9 | 25 | 9 | 1 | 35 | 35 |
| 2-05 | 26 | 9 | 26 | 9 | 0 | 35 | 35 |
| Total | 208 | 72 | 206 | 72 | 3 | 281 | 281 |

(1) A breakdown of the number of proposed samples by sample type is presented in Table 7A-1.
${ }^{(2)}$ Two proposed samples were not collected: both were personal air samples at units where a single R\&R worker performed carpet removal.
${ }^{(3)}$ Extra samples consisted of additional cassette samples necessary for personal air monitoring over the duration of carpet removal activity.

Table CR-2a. Descriptive Statistics (Across All Units) of Lead Concentrations $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right.$ ) Associated with Personal Air and Ambient Air Samples During Carpet Removal

| Sample Type | $\mathbf{N}$ | Arithmetic <br> Mean | Geometric <br> Mean | Log Std. <br> Dev. ${ }^{(1)}$ | Minimum <br> Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| During-Activity Personal <br> Exposure Samples | 14 | 35.87 | 8.44 | 1.77 | 0.86 | 221.3 |
| Pre-Activity Ambient Air <br> Samples | 8 | 0.10 | 0.09 | 0.43 | 0.05 | 0.17 |
| During-Activity Ambient <br> Air Samples | 16 | 1.48 | 0.33 | 1.58 | 0.06 | 13.38 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Results summarize worker exposure over the entire job. Three of the 14 workers in this study had multiple cassette samples taken within non-overlapping time intervals during the activity. For these workers, cumulative results over the entire job were calculated from the multiple samples.

Table CR-2b.
Descriptive Statistics (for Each Unit) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) Associated with Personal Air and Ambient Air Samples During Carpet Removal

| Unit ID | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value | $\begin{gathered} \text { Baseline } \\ \text { (Pre-Activity) } \\ \text { Value } \\ \hline \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Personal Air Sample Results ${ }^{(2)}$ |  |  |  |  |  |  |  |
| 1-01 | 2 | 55.58 | 55.41 | 0.11 | 51.25 | 59.91 |  |
| 1-02 | 2 | 3.81 | 3.67 | 0.40 | 2.77 | 4.86 |  |
| 1-03 | 2 | 7.00 | 6.85 | 0.30 | 5.56 | 8.44 |  |
| 1-04 | 2 | 174.7 | 168.4 | 0.39 | 128.1 | 221.3 |  |
| 2-01 | 1 | 1.48 | 1.48 | . | 1.48 |  |  |
| 2-02 | 2 | 4.56 | 4.08 | 0.68 | 2.52 | 6.60 |  |
| 2-03 | 1 | 7.39 | 7.39 |  | 7.39 |  |  |
| 2-05 | 2 | 0.97 | 0.97 | 0.16 | 0.86 | 1.08 |  |
| Ambient Air Sample Results |  |  |  |  |  |  |  |
| 1-01 | 2 | 2.87 | 1.42 | 1.88 | 0.38 | 5.36 | 0.10 |
| 1-02 | 2 | 0.13 | 0.11 | 0.89 | 0.06 | 0.20 | 0.09 |
| 1-03 | 2 | 0.10 | 0.10 | 0.20 | 0.09 | 0.12 | 0.17 |
| 1-04 | 2 | 6.83 | 1.92 | 2.75 | 0.28 | 13.38 | 0.07 |
| 2-01 | 2 | 0.12 | 0.12 | 0.16 | 0.11 | 0.14 | 0.09 |
| 2-02 | 2 | 0.22 | 0.19 | 0.88 | 0.10 | 0.35 | 0.05 |
| 2-03 | 2 | 1.45 | 1.44 | 0.16 | 1.29 | 1.61 | 0.14 |
| 2-05 | 2 | 0.14 | 0.14 | 0.29 | 0.11 | 0.17 | 0.06 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ For units 1-01 and 2-03, results summarize worker exposure over the entire job. Three of the 14 workers in this study had multiple cassette samples taken within non-overlapping time intervals during the activity. For these workers, cumulative results over the entire job were calculated from the multiple samples.

Table CR-3a. Descriptive Statistics (Across All Units) of Sample Weights, Lead Loadings, and Lead Concentrations Associated with Vacuum Samples from Floors Collected Before Carpet Removal ("pre") and at 1-hour Following Completion of Carpet Removal ("post") (1)

| Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample Weight (g) |  |  |  |  |  |  |
| Pre-activity | 24 | 0.0607 | 0.0304 | 1.1323 | 0.0057 | 0.4536 |
| Post-activity | 24 | 0.1677 | 0.1205 | 0.8087 | 0.0357 | 0.6285 |
| Paired Differences (post minus pre) | 24 | 0.1070 | $3.9666^{(3)}$ |  | -. 2910 | 0.5179 |
| Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |  |  |  |  |  |  |
| Pre-activity | 24 | 84.14 | 14.44 | 1.98 | 1.38 | 564.5 |
| Post-activity | 24 | 591.3 | 130.4 | 1.67 | 6.38 | 6135 |
| Paired Differences (post minus pre) | 24 | 507.1 | $9.03{ }^{(3)}$ |  | -195 | 6132 |
| Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) |  |  |  |  |  |  |
| Pre-activity | 24 | 1336.8 | 475.1 | 1.4 | 36.7 | 9179.2 |
| Post-activity | 24 | 2875.8 | 1081.4 | 1.4 | 71.9 | 20662 |
| Paired Differences (post minus pre) | 24 | 1539.0 | $2.3{ }^{(3)}$ |  | -3554 | 20571 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ Geometric mean of the ratio of the post-activity result to the result of the adjoining pre-activity sample. No measurement units are associated with this value.

Table CR-3b.
Descriptive Statistics (for Each Unit) of Sample Weights (g) Associated with Vacuum Samples from Floors Collected Before Carpet Removal ("pre") and at 1-hour Following Completion of Carpet Removal ("post") ${ }^{(1)}$

| Unit ID | Time | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre | 3 | 0.0112 | 0.0110 | 0.2343 | 0.0090 | 0.0142 |
|  | Post | 3 | 0.1800 | 0.1545 | 0.7018 | 0.0741 | 0.2999 |
| 1-02 | Pre | 3 | 0.0395 | 0.0344 | 0.6261 | 0.0207 | 0.0693 |
|  | Post | 3 | 0.1526 | 0.0993 | 1.1448 | 0.0357 | 0.3419 |
| 1-03 | Pre | 3 | 0.0337 | 0.0216 | 1.1183 | 0.0113 | 0.0784 |
|  | Post | 3 | 0.0851 | 0.0848 | 0.1111 | 0.0747 | 0.0919 |
| 1-04 | Pre | 3 | 0.0299 | 0.0263 | 0.6463 | 0.0132 | 0.0476 |
|  | Post | 3 | 0.3225 | 0.2801 | 0.6707 | 0.1394 | 0.5311 |
| 2-01 | Pre | 3 | 0.0543 | 0.0499 | 0.5330 | 0.0272 | 0.0741 |
|  | Post | 3 | 0.0751 | 0.0746 | 0.1409 | 0.0646 | 0.0856 |
| 2-02 | Pre | 3 | 0.0096 | 0.0089 | 0.4566 | 0.0057 | 0.0142 |
|  | Post | 3 | 0.0802 | 0.0654 | 0.7558 | 0.0390 | 0.1556 |
| 2-03 | Pre | 3 | 0.1691 | 0.0583 | 1.9238 | 0.0100 | 0.4536 |
|  | Post | 3 | 0.1435 | 0.1149 | 0.9053 | 0.0411 | 0.2267 |
| 2-05 | Pre | 3 | 0.1386 | 0.1313 | 0.4234 | 0.0806 | 0.1723 |
|  | Post | 3 | 0.3026 | 0.2186 | 1.0012 | 0.0858 | 0.6285 |
| Paired Differences (Post minus pre) ${ }^{(3)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 3 | 0.1688 | 14.099 |  | 0.0599 | 0.2909 |
| 1-02 |  | 3 | 0.1131 | 2.8810 |  | -. 0336 | 0.3212 |
| 1-03 |  | 3 | 0.0515 | 3.9342 |  | 0.0135 | 0.0775 |
| 1-04 |  | 3 | 0.2926 | 10.670 |  | 0.0918 | 0.5179 |
| 2-01 |  | 3 | 0.0208 | 1.4963 |  | 0.0010 | 0.0374 |
| 2-02 |  | 3 | 0.0706 | 7.3181 |  | 0.0302 | 0.1499 |
| 2-03 |  | 3 | -. 0256 | 1.9713 |  | -. 2910 | 0.2167 |
| 2-05 |  | 3 | 0.1640 | 1.6649 |  | 0.0052 | 0.4656 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ The geometric mean column contains the geometric mean of the ratio of the post-activity result to the result of the adjoining pre-activity sample. No measurement units are associated with this value.

Table CR-3c.
Descriptive Statistics (for Each Unit) of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated with Vacuum Samples from Floors Collected Before Carpet Removal ("pre") and at 1 -hour Following Completion of Carpet Removal ("post") ${ }^{(1)}$

| Unit ID | Time | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre | 3 | 1.70 | 1.67 | 0.23 | 1.38 | 2.16 |
|  | Post | 3 | 146.2 | 107.5 | 0.99 | 41.28 | 295.5 |
| 1-02 | Pre | 3 | 12.45 | 11.43 | 0.52 | 6.70 | 18.78 |
|  | Post | 3 | 35.02 | 28.27 | 0.77 | 16.69 | 68.68 |
| 1-03 | Pre | 3 | 13.97 | 6.30 | 1.52 | 2.61 | 36.68 |
|  | Post | 3 | 108.5 | 36.87 | 1.93 | 6.38 | 292.3 |
| 1-04 | Pre | 3 | 3.19 | 3.09 | 0.29 | 2.61 | 4.34 |
|  | Post | 3 | 2183 | 637.2 | 1.96 | 183.2 | 6135 |
| 2-01 | Pre | 3 | 280.9 | 188.1 | 1.20 | 52.21 | 564.5 |
|  | Post | 3 | 494.7 | 192.1 | 1.70 | 54.87 | 1332 |
| 2-02 | Pre | 3 | 2.86 | 2.86 | 0.01 | 2.85 | 2.89 |
|  | Post | 3 | 185.8 | 103.9 | 1.64 | 15.77 | 316.6 |
| 2-03 | Pre | 3 | 32.49 | 29.89 | 0.52 | 16.66 | 45.77 |
|  | Post | 3 | 167.7 | 119.9 | 1.17 | 30.92 | 240.2 |
| 2-05 | Pre | 3 | 325.5 | 315.2 | 0.30 | 261.4 | 447.5 |
|  | Post | 3 | 1410 | 488.2 | 1.83 | 119.6 | 3857 |
| Paired Differences (Post minus pre) ${ }^{(3)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 3 | 144.5 | 64.50 |  | 39.90 | 293.9 |
| 1-02 |  | 3 | 22.58 | 2.47 |  | -2.09 | 61.98 |
| 1-03 |  | 3 | 94.54 | 5.85 |  | 3.77 | 255.6 |
| 1-04 |  | 3 | 2179 | 205.9 |  | 178.8 | 6132 |
| 2-01 |  | 3 | 213.8 | 1.02 |  | -171 | 767.8 |
| 2-02 |  | 3 | 182.9 | 36.28 |  | 12.92 | 313.7 |
| 2-03 |  | 3 | 135.2 | 4.01 |  | -4.12 | 223.5 |
| 2-05 |  | 3 | 1084 | 1.55 |  | -195 | 3595 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ The geometric mean column contains the geometric mean of the ratio of the post-activity result to the result of the adjoining pre-activity sample. No measurement units are associated with this value.

Table CR-3d.
Descriptive Statistics (for Each Unit) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) Associated with Vacuum Samples from Floors Collected Before Carpet Removal ("pre") and at 1-hour Following Completion of Carpet Removal ("post") ${ }^{(1)}$

| Unit ID | Time | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre | 3 | 152.9 | 152.0 | 0.1 | 133.9 | 172.9 |
|  | Post | 3 | 868.9 | 695.5 | 0.9 | 248.7 | 1372.8 |
| 1-02 | Pre | 3 | 337.0 | 331.7 | 0.2 | 271.1 | 416.4 |
|  | Post | 3 | 304.8 | 284.8 | 0.4 | 200.9 | 467.6 |
| 1-03 | Pre | 3 | 310.2 | 292.6 | 0.4 | 231.4 | 467.9 |
|  | Post | 3 | 1204.0 | 434.9 | 1.9 | 71.9 | 3180.4 |
| 1-04 | Pre | 3 | 126.7 | 117.9 | 0.4 | 90.8 | 198.1 |
|  | Post | 3 | 7469.8 | 2274.7 | 2.0 | 433.5 | 20662 |
| 2-01 | Pre | 3 | 4716.0 | 3773.3 | 0.8 | 1919.3 | 9179.2 |
|  | Post | 3 | 5932.2 | 2575.2 | 1.6 | 730.6 | 15564 |
| 2-02 | Pre | 3 | 342.6 | 320.8 | 0.4 | 203.8 | 500.1 |
|  | Post | 3 | 2910.9 | 1590.3 | 1.4 | 404.2 | 6883.0 |
| 2-03 | Pre | 3 | 1805.6 | 513.1 | 2.4 | 36.7 | 4576.5 |
|  | Post | 3 | 1084.0 | 1043.5 | 0.3 | 752.2 | 1477.2 |
| 2-05 | Pre | 3 | 2903.7 | 2401.1 | 0.7 | 1553.5 | 5552.6 |
|  | Post | 3 | 3231.8 | 2233.8 | 1.2 | 617.5 | 6136.6 |
| Paired Differences (Post minus pre) ${ }^{(3)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 3 | 716.1 | 4.6 |  | 114.8 | 1221.1 |
| 1-02 |  | 3 | -32.2 | 0.9 |  | -170.5 | 196.6 |
| 1-03 |  | 3 | 893.8 | 1.5 |  | -159.5 | 2712.5 |
| 1-04 |  | 3 | 7343.1 | 19.3 |  | 235.5 | 20571 |
| 2-01 |  | 3 | 1216.3 | 0.7 |  | -2319 | 6385.1 |
| 2-02 |  | 3 | 2568.4 | 5.0 |  | 80.3 | 6679.2 |
| 2-03 |  | 3 | -721.6 | 2.0 |  | -3554 | 1440.5 |
| 2-05 |  | 3 | 328.2 | 0.9 |  | -2611 | 4531.7 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ The geometric mean column contains the geometric mean of the ratio of the post-activity result to the result of the adjoining pre-activity sample. No measurement units are associated with this value.

Table CR-4a.
Descriptive Statistics (Across All Units) of Sample Weights, Lead Loadings, and Lead Concentrations Associated with Vacuum Samples from Stainless Steel Dustfall Collectors at 1-hour and 2-hours Following Completion of Carpet Removal ${ }^{(1)}$

| Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample Weight (g) |  |  |  |  |  |  |
| One hour post-activity | 24 | 0.0288 | 0.0223 | 0.6999 | 0.0077 | 0.1127 |
| Two hours post-activity | 24 | 0.0423 | 0.0305 | 0.8151 | 0.0043 | 0.2245 |
| Paired Differences (2-hr minus 1-hr) | 24 | 0.0135 | $1.3682^{(3)}$ |  | -. 0452 | 0.2087 |
| Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |  |  |  |  |  |  |
| One hour post-activity | 24 | 72.68 | 24.33 | 1.50 | 2.61 | 621.0 |
| Two hours post-activity | 24 | 109.8 | 38.63 | 1.50 | 2.61 | 937.8 |
| Paired Differences (2-hr minus 1-hr) | 24 | 37.14 | $1.59^{(3)}$ |  | -193 | 316.8 |
| Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) |  |  |  |  |  |  |
| One hour post-activity | 24 | 2427.8 | 1089.9 | 1.2 | 214.3 | 19839 |
| Two hours post-activity | 24 | 2935.1 | 1264.8 | 1.2 | 280.8 | 29867 |
| Paired Differences (2-hr minus 1-hr) | 24 | 507.4 | $1.2{ }^{(3)}$ |  | -6244 | 10028 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ Geometric mean of the ratio of the two-hour result to the result of the adjoining one-hour sample. No measurement units are associated with this value.

Table CR-4b.
Descriptive Statistics (for Each Unit) of Sample Weights (g) Associated with Vacuum Samples from Stainless Steel Dustfall Collectors at 1-hour and 2-hours Following Completion of Carpet Removal ${ }^{(1)}$

| Unit ID | Time PostActivity | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | 1-hr. | 3 | 0.0499 | 0.0327 | 1.1205 | 0.0127 | 0.1127 |
|  | 2-hrs. | 3 | 0.0548 | 0.0495 | 0.5957 | 0.0249 | 0.0721 |
| 1-02 | 1-hr. | 3 | 0.0435 | 0.0341 | 0.8809 | 0.0141 | 0.0821 |
|  | 2-hrs. | 3 | 0.0361 | 0.0327 | 0.5296 | 0.0234 | 0.0602 |
| 1-03 | 1-hr. | 3 | 0.0206 | 0.0195 | 0.4229 | 0.0122 | 0.0277 |
|  | 2-hrs. | 3 | 0.0276 | 0.0229 | 0.8154 | 0.0091 | 0.0425 |
| 1-04 | 1-hr. | 3 | 0.0269 | 0.0260 | 0.3296 | 0.0178 | 0.0317 |
|  | 2-hrs. | 3 | 0.0465 | 0.0422 | 0.5207 | 0.0311 | 0.0770 |
| 2-01 | 1-hr. | 3 | 0.0190 | 0.0165 | 0.6880 | 0.0079 | 0.0309 |
|  | 2-hrs. | 3 | 0.0232 | 0.0226 | 0.2671 | 0.0192 | 0.0308 |
| 2-02 | 1-hr. | 3 | 0.0172 | 0.0139 | 0.7768 | 0.0077 | 0.0335 |
|  | 2-hrs. | 3 | 0.0235 | 0.0148 | 1.2455 | 0.0043 | 0.0519 |
| 2-03 | 1-hr. | 3 | 0.0264 | 0.0203 | 0.8773 | 0.0098 | 0.0537 |
|  | 2-hrs. | 3 | 0.0981 | 0.0516 | 1.5458 | 0.0103 | 0.2245 |
| 2-05 | 1-hr. | 3 | 0.0266 | 0.0235 | 0.6520 | 0.0114 | 0.0405 |
|  | 2-hrs. | 3 | 0.0286 | 0.0280 | 0.2593 | 0.0212 | 0.0354 |
| Paired Differences (2-hr. minus 1-hr) ${ }^{(3)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 3 | 0.0049 | 1.5139 |  | -. 0452 | 0.0477 |
| 1-02 |  | 3 | -. 0073 | 0.9592 |  | -. 0219 | 0.0093 |
| 1-03 |  | 3 | 0.0070 | 1.1752 |  | -. 0031 | 0.0205 |
| 1-04 |  | 3 | 0.0196 | 1.6208 |  | 0.0001 | 0.0453 |
| 2-01 |  | 3 | 0.0042 | 1.3741 |  | -. 0001 | 0.0117 |
| 2-02 |  | 3 | 0.0063 | 1.0620 |  | -. 0061 | 0.0184 |
| 2-03 |  | 3 | 0.0717 | 2.5482 |  | 0.0005 | 0.2087 |
| 2-05 |  | 3 | 0.0020 | 1.1937 |  | -. 0068 | 0.0179 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ The geometric mean column contains the geometric mean of the ratio of the two-hour result to the result of the adjoining one-hour sample. No measurement units are associated with this value.

Table CR-4c.
Descriptive Statistics (for Each Unit) of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated with Vacuum Samples from Stainless Steel Dustfall Collectors at 1-hour and 2-hours Following Completion of Carpet Removal ${ }^{(1)}$

| Unit ID | Time PostActivity | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | $\begin{aligned} & \text { 1-hr. } \\ & \text { 2-hrs. } \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 103.3 \\ & 80.47 \end{aligned}$ | $\begin{aligned} & 60.55 \\ & 56.31 \\ & \hline \end{aligned}$ | $\begin{array}{r} 1.48 \\ 1.10 \\ \hline \end{array}$ | $\begin{aligned} & 11.65 \\ & 18.25 \\ & \hline \end{aligned}$ | $\begin{aligned} & 205.7 \\ & 163.2 \end{aligned}$ |
| 1-02 | $\begin{aligned} & \text { 1-hr. } \\ & \text { 2-hrs. } \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 18.66 \\ & 14.34 \end{aligned}$ | $\begin{aligned} & 13.88 \\ & 13.07 \end{aligned}$ | $\begin{aligned} & 0.98 \\ & 0.53 \end{aligned}$ | $\begin{aligned} & 5.10 \\ & 7.74 \end{aligned}$ | $\begin{aligned} & 36.51 \\ & 22.39 \end{aligned}$ |
| 1-03 | $\begin{aligned} & \text { 1-hr. } \\ & \text { 2-hrs. } \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{array}{r} 9.44 \\ 13.04 \end{array}$ | $\begin{aligned} & 7.55 \\ & 8.95 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.92 \\ & 1.16 \end{aligned}$ | $\begin{aligned} & 2.61 \\ & 2.61 \\ & \hline \end{aligned}$ | $\begin{aligned} & 13.35 \\ & 25.89 \end{aligned}$ |
| 1-04 | $\begin{aligned} & \text { 1-hr. } \\ & \text { 2-hrs. } \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 282.1 \\ & 437.1 \\ & \hline \end{aligned}$ | $\begin{aligned} & 197.7 \\ & 316.5 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.00 \\ & 0.96 \\ & \hline \end{aligned}$ | $\begin{aligned} & 96.91 \\ & 154.3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 621.0 \\ & 937.8 \end{aligned}$ |
| 2-01 | $\begin{aligned} & \text { 1-hr. } \\ & \text { 2-hrs. } \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 82.21 \\ & 38.96 \end{aligned}$ | $\begin{aligned} & 36.87 \\ & 34.67 \\ & \hline \end{aligned}$ | $\begin{aligned} & 1.53 \\ & 0.57 \\ & \hline \end{aligned}$ | $\begin{aligned} & 13.67 \\ & 23.00 \\ & \hline \end{aligned}$ | $\begin{aligned} & 216.0 \\ & 66.69 \end{aligned}$ |
| 2-02 | $\begin{aligned} & \text { 1-hr. } \\ & \text { 2-hrs. } \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 39.98 \\ & 143.7 \end{aligned}$ | $\begin{aligned} & 10.04 \\ & 40.83 \end{aligned}$ | $\begin{aligned} & 2.10 \\ & 2.37 \\ & \hline \end{aligned}$ | $\begin{aligned} & 2.85 \\ & 3.33 \\ & \hline \end{aligned}$ | $\begin{aligned} & 114.0 \\ & 372.9 \\ & \hline \end{aligned}$ |
| 2-03 | $\begin{aligned} & \text { 1-hr. } \\ & \text { 2-hrs. } \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 34.93 \\ & 117.9 \end{aligned}$ | $\begin{aligned} & 27.72 \\ & 77.76 \end{aligned}$ | $\begin{aligned} & 0.82 \\ & 1.21 \end{aligned}$ | $\begin{aligned} & 13.96 \\ & 22.10 \end{aligned}$ | $\begin{aligned} & 68.60 \\ & 244.7 \end{aligned}$ |
| 2-05 | $\begin{aligned} & \text { 1-hr. } \\ & \text { 2-hrs. } \end{aligned}$ | $\begin{aligned} & 3 \\ & 3 \\ & \hline \end{aligned}$ | $\begin{aligned} & 10.79 \\ & 33.04 \end{aligned}$ | $\begin{array}{r} 9.53 \\ 21.57 \\ \hline \end{array}$ | $\begin{aligned} & 0.59 \\ & 1.23 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.78 \\ & 5.95 \\ & \hline \end{aligned}$ | $\begin{aligned} & 18.82 \\ & 68.58 \end{aligned}$ |
| Paired Differences (2-hr. minus 1-hr) ${ }^{(3)}$ |  |  |  |  |  |  |  |
|  | 1-01 | 3 | -22.8 | 0.93 |  | -42.5 | 6.60 |
|  | 1-02 | 3 | -4.32 | 0.94 |  | -14.1 | 2.65 |
|  | 1-03 | 3 | 3.60 | 1.19 |  | -2.74 | 13.53 |
|  | 1-04 | 3 | 155.0 | 1.60 |  | 57.40 | 316.8 |
|  | 2-01 | 3 | -43.3 | 0.94 |  | -193 | 53.01 |
|  | 2-02 | 3 | 103.7 | 4.07 |  | 0.22 | 259.0 |
|  | 2-03 | 3 | 82.98 | 2.81 |  | 8.14 | 222.5 |
|  | 2-05 | 3 | 22.24 | 2.26 |  | -0.83 | 49.76 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ The geometric mean column contains the geometric mean of the ratio of the two-hour result to the result of the adjoining one-hour sample. No measurement units are associated with this value.

Table CR-4d.
Descriptive Statistics (for Each Unit) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) Associated with Vacuum Samples from Stainless Steel Dustfall Collectors at 1 -hour and 2hours Following Completion of Carpet Removal ${ }^{(1)}$

| Unit ID | Time PostActivity | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | 1-hr. | 3 | 2179.4 | 1852.5 | 0.7 | 917.7 | 3795.5 |
|  | 2-hrs. | 3 | 1327.5 | 1137.9 | 0.7 | 732.9 | 2418.2 |
| 1-02 | 1-hr. | 3 | 408.8 | 407.2 | 0.1 | 361.6 | 444.6 |
|  | 2-hrs. | 3 | 407.5 | 399.9 | 0.2 | 330.9 | 519.7 |
| 1-03 | 1-hr. | 3 | 419.3 | 387.1 | 0.5 | 214.3 | 561.6 |
|  | 2-hrs. | 3 | 412.2 | 390.4 | 0.4 | 287.3 | 609.1 |
| 1-04 | 1-hr. | 3 | 10038 | 7592.7 | 0.9 | 3057.2 | 19839 |
|  | 2-hrs. | 3 | 12972 | 7499.2 | 1.4 | 2004.0 | 29867 |
| 2-01 | 1-hr. | 3 | 3216.1 | 2238.5 | 1.0 | 927.2 | 6990.3 |
|  | 2-hrs. | 3 | 1854.9 | 1532.1 | 0.8 | 746.7 | 3402.4 |
| 2-02 | 1-hr. | 3 | 1357.3 | 722.3 | 1.3 | 299.2 | 3402.4 |
|  | 2-hrs. | 3 | 3922.3 | 2766.9 | 1.1 | 774.4 | 7185.7 |
| 2-03 | 1-hr. | 3 | 1369.9 | 1368.3 | 0.1 | 1277.5 | 1424.7 |
|  | 2-hrs. | 3 | 1565.5 | 1506.2 | 0.3 | 1090.0 | 2145.3 |
| 2-05 | 1-hr. | 3 | 433.7 | 405.9 | 0.5 | 242.2 | 594.3 |
|  | 2-hrs. | 3 | 1018.9 | 769.8 | 1.0 | 280.8 | 1937.3 |
| Paired Differences (2-hr. minus 1-hr) ${ }^{(3)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 3 | -851.9 | 0.6 |  | -2964 | 593.1 |
| 1-02 |  | 3 | -1.2 | 1.0 |  | -72.7 | 99.6 |
| 1-03 |  | 3 | -7.1 | 1.0 |  | -141.8 | 73.0 |
| 1-04 |  | 3 | 2934.6 | 1.0 |  | -1053 | 10028 |
| 2-01 |  | 3 | -1361 | 0.7 |  | -6244 | 1671.6 |
| 2-02 |  | 3 | 2565.0 | 3.8 |  | 475.2 | 3783.4 |
| 2-03 |  | 3 | 195.6 | 1.1 |  | -317.5 | 720.6 |
| 2-05 |  | 3 | 585.2 | 1.9 |  | 38.5 | 1472.7 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ The geometric mean column contains the geometric mean of the ratio of the two-hour result to the result of the adjoining one-hour sample. No measurement units are associated with this value.

Table CR-5a.
Descriptive Statistics (Across All Units) of Sample Weights, Lead Loadings, and Lead Concentrations
Associated with Vacuum Samples from Window Sills Collected Before Carpet Removal ("pre") and at 1-hour Following Completion of Carpet Removal ("post")

| Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample Weight (g) |  |  |  |  |  |  |
| Pre-activity | 16 | 0.2535 | 0.0970 | 1.6046 | 0.0059 | 1.1394 |
| Post-activity | 16 | 0.3087 | 0.1380 | 1.3282 | 0.0195 | 1.6537 |
| Paired Differences (post minus pre) | 16 | 0.0552 | $1.4235{ }^{(2)}$ |  | -. 7865 | 1.4214 |
| Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |  |  |  |  |  |  |
| Pre-activity | 16 | 4208 | 417.5 | 2.32 | 21.58 | 41459 |
| Post-activity | 16 | 4404 | 661.3 | 2.22 | 11.81 | 26581 |
| Paired Differences (post minus pre) | 16 | 196.2 | $1.58{ }^{(2)}$ |  | -14879 | 16392 |
| Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) |  |  |  |  |  |  |
| Pre-activity | 16 | 7396.5 | 2161.8 | 1.7 | 102.0 | 52985 |
| Post-activity | 16 | 7878.4 | 2303.8 | 1.5 | 250.0 | 66776 |
| Paired Differences (post minus pre) | 16 | 481.9 | $1.1{ }^{(2)}$ |  | -6248 | 13791 |

Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Geometric mean of the ratio of the post-activity result to the result of the adjoining pre-activity sample. No measurement units are associated with this value.

Table CR-5b. Descriptive Statistics (for Each Unit) of Sample Weights (g) Associated with Vacuum Samples from Window Sills Collected Before Carpet Removal ("pre") and at 1-hour Following Completion of Carpet Removal ("post")

| Unit ID | Time | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre | 2 | 0.1686 | 0.1685 | 0.0138 | 0.1669 | 0.1702 |
|  | Post | 2 | 0.1162 | 0.1162 | 0.0037 | 0.1159 | 0.1165 |
| 1-02 | Pre | 2 | 0.0618 | 0.0617 | 0.0103 | 0.0613 | 0.0622 |
|  | Post | 2 | 0.2488 | 0.1199 | 1.9222 | 0.0308 | 0.4668 |
| 1-03 | Pre | 2 | 0.1776 | 0.0677 | 2.2901 | 0.0134 | 0.3417 |
|  | Post | 2 | 0.0831 | 0.0661 | 0.9920 | 0.0328 | 0.1334 |
| 1-04 | Pre | 2 | 0.6859 | 0.5145 | 1.1245 | 0.2323 | 1.1394 |
|  | Post | 2 | 1.0033 | 0.7639 | 1.0922 | 0.3529 | 1.6537 |
| 2-01 | Pre | 2 | 0.2120 | 0.1205 | 1.6473 | 0.0376 | 0.3863 |
|  | Post | 2 | 0.5123 | 0.2869 | 1.6731 | 0.0879 | 0.9366 |
| 2-02 | Pre | 2 | 0.0124 | 0.0106 | 0.8232 | 0.0059 | 0.0189 |
|  | Post | 2 | 0.0238 | 0.0234 | 0.2583 | 0.0195 | 0.0281 |
| 2-03 | Pre | 2 | 0.6808 | 0.6797 | 0.0815 | 0.6416 | 0.7200 |
|  | Post | 2 | 0.4092 | 0.3910 | 0.4299 | 0.2885 | 0.5299 |
| 2-05 | Pre | 2 | 0.0292 | 0.0249 | 0.8161 | 0.0140 | 0.0444 |
|  | Post | 2 | 0.0729 | 0.0713 | 0.3033 | 0.0575 | 0.0883 |
| Paired Differences (Post minus pre) ${ }^{(2)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 2 | -. 0523 | 0.6894 |  | -. 0543 | -. 0504 |
| 1-02 |  | 2 | 0.1871 | 1.9418 |  | -. 0305 | 0.4046 |
| 1-03 |  | 2 | -. 0945 | 0.9776 |  | -. 2083 | 0.0194 |
| 1-04 |  | 2 | 0.3175 | 1.4849 |  | -. 7865 | 1.4214 |
| 2-01 |  | 2 | 0.3003 | 2.3808 |  | 0.0503 | 0.5503 |
| 2-02 |  | 2 | 0.0114 | 2.2167 |  | 0.0006 | 0.0222 |
| 2-03 |  | 2 | -. 2716 | 0.5753 |  | -. 3531 | -. 1901 |
| 2-05 |  | 2 | 0.0437 | 2.8580 |  | 0.0131 | 0.0743 |

Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ The geometric mean column contains the geometric mean of the ratio of the post-activity result to the result of the adjoining pre-activity sample. No measurement units are associated with this value.

Table CR-5c. Descriptive Statistics (for Each Unit) of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ )
Associated with Vacuum Samples from Window Sills Collected Before Carpet Removal ("pre") and at 1-hour Following Completion of Carpet Removal ("post")

| Unit ID | Time | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre | 2 | 535.2 | 339.2 | 1.46 | 121.19 | 949.2 |
|  | Post | 2 | 157.9 | 156.8 | 0.17 | 139.05 | 176.7 |
| 1-02 | Pre | 2 | 1850 | 1612 | 0.76 | 942.19 | 2757 |
|  | Post | 2 | 990.0 | 812.3 | 0.92 | 424.12 | 1556 |
| 1-03 | Pre | 2 | 82.46 | 71.67 | 0.77 | 41.69 | 123.2 |
|  | Post | 2 | 393.4 | 392.1 | 0.12 | 361.44 | 425.4 |
| 1-04 | Pre | 2 | 111.5 | 111.2 | 0.09 | 104.06 | 118.9 |
|  | Post | 2 | 1236 | 1012 | 0.92 | 526.05 | 1946 |
| 2-01 | Pre | 2 | 5576 | 4795 | 0.80 | 2730.3 | 8422 |
|  | Post | 2 | 16052 | 13449 | 0.87 | 7289.5 | 24814 |
| 2-02 | Pre | 2 | 64.31 | 48.06 | 1.13 | 21.58 | 107.0 |
|  | Post | 2 | 155.6 | 59.47 | 2.29 | 11.81 | 299.5 |
| 2-03 | Pre | 2 | 25395 | 19668 | 1.05 | 9330.3 | 41459 |
|  | Post | 2 | 16098 | 12217 | 1.10 | 5615.3 | 26581 |
| 2-05 | Pre | 2 | 51.62 | 46.70 | 0.64 | 29.63 | 73.60 |
|  | Post | 2 | 152.9 | 74.08 | 1.91 | 19.14 | 286.7 |
| Paired Differences (Post minus pre) ${ }^{(2)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 2 | -377 | 0.46 |  | -772.5 | 17.86 |
| 1-02 |  | 2 | -860 | 0.50 |  | -1201 | -518 |
| 1-03 |  | 2 | 311.0 | 5.47 |  | 238.22 | 383.7 |
| 1-04 |  | 2 | 1125 | 9.10 |  | 407.19 | 1842 |
| 2-01 |  | 2 | 10475 | 2.80 |  | 4559.2 | 16392 |
| 2-02 |  | 2 | 91.33 | 1.24 |  | -9.77 | 192.4 |
| 2-03 |  | 2 | -9297 | 0.62 |  | -14879 | -3715 |
| 2-05 |  | 2 | 101.3 | 1.59 |  | -54.46 | 257.1 |

Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ The geometric mean column contains the geometric mean of the ratio of the post-activity result to the result of the adjoining pre-activity sample. No measurement units are associated with this value.

Table CR-5d. Descriptive Statistics (for Each Unit) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) Associated with Vacuum Samples from Window Sills Collected Before Carpet Removal ("pre") and at 1-hour Following Completion of Carpet Removal ("post")

| Unit ID | Time | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre | 2 | 3182.3 | 1639.6 | 1.8 | 454.9 | 5909.6 |
|  | Post | 2 | 1042.3 | 1030.4 | 0.2 | 885.0 | 1199.7 |
| 1-02 | Pre | 2 | 4538.6 | 3960.2 | 0.8 | 2321.6 | 6755.5 |
|  | Post | 2 | 1294.0 | 1027.9 | 1.0 | 508.0 | 2080.0 |
| 1-03 | Pre | 2 | 735.5 | 506.2 | 1.3 | 201.9 | 1269.0 |
|  | Post | 2 | 3404.2 | 2833.2 | 0.9 | 1517.0 | 5291.5 |
| 1-04 | Pre | 2 | 412.4 | 271.6 | 1.4 | 102.0 | 722.9 |
|  | Post | 2 | 3304.9 | 1663.9 | 1.9 | 449.4 | 6160.4 |
| 2-01 | Pre | 2 | 27328 | 9411.9 | 2.4 | 1671.9 | 52985 |
|  | Post | 2 | 34308 | 11088 | 2.5 | 1841.0 | 66776 |
| 2-02 | Pre | 2 | 3462.6 | 1791.3 | 1.8 | 499.4 | 6425.9 |
|  | Post | 2 | 2234.3 | 1026.9 | 2.0 | 250.0 | 4218.5 |
| 2-03 | Pre | 2 | 17029 | 13665 | 1.0 | 6867.1 | 27192 |
|  | Post | 2 | 16439 | 14755 | 0.7 | 9191.2 | 23687 |
| 2-05 | Pre | 2 | 2482.6 | 2319.7 | 0.5 | 1598.2 | 3366.9 |
|  | Post | 2 | 999.8 | 946.0 | 0.5 | 676.2 | 1323.3 |
| Paired Differences (Post minus pre) ${ }^{(2)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 2 | -2140 | 0.6 |  | -5025 | 744.8 |
| 1-02 |  | 2 | -3245 | 0.3 |  | -6248 | -241.6 |
| 1-03 |  | 2 | 2668.8 | 5.6 |  | 1315.1 | 4022.4 |
| 1-04 |  | 2 | 2892.4 | 6.1 |  | -273.5 | 6058.3 |
| 2-01 |  | 2 | 6980.0 | 1.2 |  | 169.2 | 13791 |
| 2-02 |  | 2 | -1228 | 0.6 |  | -2207 | -249.4 |
| 2-03 |  | 2 | -590.1 | 1.1 |  | -3504 | 2324.0 |
| 2-05 |  | 2 | -1483 | 0.4 |  | -2691 | -274.9 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ The geometric mean column contains the geometric mean of the ratio of the post-activity result to the result of the adjoining pre-activity sample. No measurement units are associated with this value.

Table CR-6a. Descriptive Statistics (Across All Units) of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated with Vacuum and Wipe Samples from Stainless Steel Dustfall Collectors Collected at 1-hour Following Completion of Carpet Removal ${ }^{(1)}$

| Data Representation | $\mathbf{N}$ | Arithmetic <br> Mean | Geometric <br> Mean | Log Std. <br> Dev. ${ }^{(2)}$ | Minimum <br> Value |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Vacuum | 16 | 85.59 | 23.04 | 1.65 | 2.61 |
| Vape | 16 | 58.84 | 27.06 | 1.31 | 3.19 |
| Paired Difference (Wipe <br> minus vacuum) | 16 | -26.8 | $1.17^{(3)}$ |  | 621.0 |

${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table. Only regular vacuum samples located side-by-side with a wipe sample are included in the calculation of vacuum sample results.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ Geometric mean of the ratio of the wipe result to the result of the adjoining sample collected by vacuum. No measurement units are associated with this value.

Table CR-6b. Descriptive Statistics (for Each Unit) of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated with Vacuum and Wipe Samples from Stainless Steel Dustfall Collectors Collected at 1 -hour Following Completion of Carpet Removal ${ }^{(1)}$

| Unit ID | Sample Type | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Vacuum Wipe | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | $\begin{aligned} & 108.7 \\ & 48.82 \end{aligned}$ | $\begin{aligned} & 48.95 \\ & 35.66 \end{aligned}$ | $\begin{aligned} & \hline 2.03 \\ & 1.18 \end{aligned}$ | $\begin{aligned} & \hline 11.65 \\ & 15.48 \end{aligned}$ | $\begin{aligned} & \hline 205.7 \\ & 82.16 \end{aligned}$ |
| 1-02 | Vacuum Wipe | $\begin{aligned} & 2 \\ & 2 \end{aligned}$ | $\begin{array}{r} 9.74 \\ 21.56 \end{array}$ | $\begin{array}{r} 8.56 \\ 19.29 \end{array}$ | $\begin{aligned} & 0.73 \\ & 0.68 \end{aligned}$ | $\begin{array}{r} 5.10 \\ 11.94 \end{array}$ | $\begin{aligned} & 14.37 \\ & 31.18 \end{aligned}$ |
| 1-03 | Vacuum Wipe | $\begin{aligned} & 2 \\ & 2 \\ & \hline \end{aligned}$ | $\begin{array}{r} 7.48 \\ 35.46 \\ \hline \end{array}$ | $\begin{array}{r} 5.68 \\ 22.06 \\ \hline \end{array}$ | $\begin{array}{r} 1.10 \\ 1.49 \\ \hline \end{array}$ | $\begin{aligned} & 2.61 \\ & 7.70 \\ & \hline \end{aligned}$ | $\begin{array}{r} 12.35 \\ 63.22 \end{array}$ |
| 1-04 | Vacuum Wipe | $\begin{aligned} & 2 \\ & 2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 358.9 \\ & 254.2 \end{aligned}$ | $\begin{array}{r} 245.3 \\ 241.5 \\ \hline \end{array}$ | $\begin{aligned} & 1.31 \\ & 0.46 \\ & \hline \end{aligned}$ | $\begin{aligned} & 96.91 \\ & 174.9 \end{aligned}$ | $\begin{aligned} & 621.0 \\ & 333.6 \\ & \hline \end{aligned}$ |
| 2-01 | Vacuum Wipe | $\begin{array}{r} 2 \\ 2 \\ \hline \end{array}$ | $\begin{array}{r} 116.5 \\ 22.14 \\ \hline \end{array}$ | $\begin{array}{r} 60.54 \\ 22.09 \\ \hline \end{array}$ | $\begin{aligned} & 1.80 \\ & 0.09 \\ & \hline \end{aligned}$ | $\begin{array}{r} 16.97 \\ 20.66 \\ \hline \end{array}$ | $\begin{aligned} & 216.0 \\ & 23.62 \end{aligned}$ |
| 2-02 | Vacuum Wipe | $\begin{array}{r} 2 \\ 2 \\ \hline \end{array}$ | $\begin{array}{r} 58.55 \\ 48.29 \\ \hline \end{array}$ | $\begin{aligned} & 18.83 \\ & 17.82 \\ & \hline \end{aligned}$ | $\begin{array}{r} 2.55 \\ 2.34 \\ \hline \end{array}$ | $\begin{aligned} & 3.11 \\ & 3.41 \\ & \hline \end{aligned}$ | $\begin{aligned} & 114.0 \\ & 93.17 \\ & \hline \end{aligned}$ |
| 2-03 | Vacuum Wipe | $\begin{aligned} & 2 \\ & 2 \\ & \hline \end{aligned}$ | $\begin{aligned} & 18.10 \\ & 32.69 \\ & \hline \end{aligned}$ | $\begin{array}{r} 17.62 \\ 32.46 \\ \hline \end{array}$ | $\begin{array}{r} 0.33 \\ 0.17 \\ \hline \end{array}$ | $\begin{aligned} & 13.96 \\ & 28.81 \\ & \hline \end{aligned}$ | $\begin{array}{r} 22.24 \\ 36.57 \\ \hline \end{array}$ |
| 2-05 | Vacuum Wipe | $\begin{array}{r} 2 \\ 2 \\ \hline \end{array}$ | $\begin{aligned} & 6.78 \\ & 7.51 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.78 \\ & 6.14 \\ & \hline \end{aligned}$ | $\begin{aligned} & 0.00 \\ & 0.93 \\ & \hline \end{aligned}$ | $\begin{aligned} & 6.78 \\ & 3.19 \\ & \hline \end{aligned}$ | $\begin{array}{r} 6.78 \\ 11.82 \\ \hline \end{array}$ |
| Paired Differences (wipe minus vacuum) ${ }^{(3)}$ |  |  |  |  |  |  |  |
| 1-01 |  | 2 | -59.9 | 0.73 |  | -124 | 3.83 |
| 1-02 |  | 2 | 11.83 | 2.25 |  | 6.84 | 16.81 |
| 1-03 |  | 2 | 27.98 | 3.89 |  | 5.09 | 50.87 |
| 1-04 |  | 2 | -105 | 0.98 |  | -287 | 77.96 |
| 2-01 |  | 2 | -94.3 | 0.36 |  | -192 | 3.69 |
| 2-02 |  | 2 | -10.3 | 0.95 |  | -20.8 | 0.30 |
| 2-03 |  | 2 | 14.59 | 1.84 |  | 6.57 | 22.61 |
| 2-05 |  | 2 | 0.72 | 0.91 |  | -3.59 | 5.04 |

[^0]${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ The geometric mean column contains the geometric mean of the ratio of the wipe result to the result of the adjoining sample collected by vacuum. No measurement units are associated with this value.


Figure CR-1a.
Boxplots of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) for Three Types of Dust Samples Taken Prior to Carpet Removal Activities


Figure CR-1b.
Boxplots of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) for Three Types of Dust Samples Taken Prior to Carpet Removal Activities


SSDC $=$ Stainless Steel Dustfall Collectors

Figure CR-2a.

Figure CR-2b.


SSDC $=$ Stainless Steel Dustfall Collectors
Boxplots of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) for Five Types of PostActivity Settled Dust Samples

Boxplots of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) for Four Types of PostActivity Settled Dust Samples

## A. 2 DESCRIPTIVE STATISTICS ON SAMPLE WEIGHTS, LEAD LOADINGS, AND LEAD CONCENTRATIONS BY SAMPLE TYPE, IN THE WINDOW REPLACEMENT PHASE

This section presents descriptive summaries on lead exposure data for the various sample types considered in the EFSS window replacement phase. These summaries, cited in Section 7B and Chapter 6, are presented within six sets of tables, grouped according to the sample type considered:

> Total number of samples collected and analyzed: Table WR-1. Personal and ambient air results: Tables WR-2a, WR-2b.

> Pre- and post-activity floor vacuum dust results: Tables
> WR-3a through WR-31.
> Stainless steel dustfall collector (SSDC) dust sample results using vacuum techniques, collected at 1-hour and 2-hours following the activity: Tables WR-4a through WR-4d.

> Pre-activity window well dust results: Tables WR-5a, WR-5b.
> Interior and Exterior Paint Chip results: Tables WR-6a, WR-6b.

Table WR-1 reports the number of samples planned, the number of samples collected, the number of analytical results received, and the number of analytical results used in the statistical analysis. The remaining tables present summary statistics, including the number of samples with non-missing data values, the arithmetic and geometric means, the standard deviation of the logtransformed data, and the minimum and maximum data values. Within each set of tables, the first table represents statistics over all study data, while subsequent tables include statistics calculated for each study unit. Lead exposure data included in these tables include the physical sample weights ( g ) and lead concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) for vacuum samples, lead loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) for vacuum samples, lead loadings for paint chip samples ( $\mathrm{mg} / \mathrm{cm}^{2}$ ) and lead concentrations ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) for personal air and ambient air samples. The personal air lead concentrations are expressed in terms of task-length average (TLA) exposures for a given worker, defined as the average exposure over the duration of activity.

Similar sample types are placed within a given set of tables above so that their results can be compared. These comparisons are made using the differences in sample results between pairs of adjoining samples at a given location. Tables WR-2a through WR-2l present differences in results between adjoining pre- and post-activity floor dust samples. Tables WR-3a through WR3d present differences between 1-hour and 2-hour results from SSDC vacuum dust samples. The same statistics are presented for the paired differences as for the individual sample results. However, the statistics identified as the "geometric mean" represents the geometric mean of the ratio between the two adjoining sample results at a given location (e.g., post- vs. pre-activity, 2hour vs. 1-hour).

In addition to the above tables, this section also includes boxplots of lead loading and concentration data for the different types of settled dust samples. Figures WR-1a and WR-1b present lead loadings and lead concentrations, respectively, for four pre-activity settled dust samples ( 1 window well, 3 floor). Figures WR-2a and WR-2b present lead loadings and lead concentrations, respectively, for five post-activity settled dust samples ( 3 floor, 2 SSDC). Figure WR-3 presents boxplots of interior and exterior paint chip lead loadings from removed windows. Chapter 5 includes a discussion of how to interpret boxplots.

## Table WR-1. Numbers of Field Samples Collected and Results Reported by Unit in the R\&R/EFSS Window Replacement Phase

| Unit ID | Number of Proposed Samples |  | Number of Proposed Samples Collected ${ }^{(1)}$ |  | Number of Extra Samples Collected ${ }^{(2)}$ |  | Total Number of Samples Collected | Number of Analytical Results Received ${ }^{(3)}$ | Number of Analytical Results Used in Analysis ${ }^{(4)}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Reg. | QC | Reg. | QC | Reg. | QC |  |  |  |
| 1-01 | 42 | 6 | 42 | 6 | 1 | 1 | 50 | 47 | 46 |
| 2-01 | 42 | 6 | 40 | 6 | 8 | 0 | 54 | 50 | 50 |
| 3-01 | 42 | 6 | 39 | 6 | 3 | 0 | 48 | 47 | 46 |
| 4-01 | 42 | 6 | 41 |  | 3 | 1 | 51 | 49 | 49 |

${ }^{(1)}$ The number of proposed samples collected differs from number of proposed samples for units 2-01, 3-01 and 4-01. For unit 201 , one pre- and one post-activity settled dust (floor) sample at 3 feet were not collected. For unit 3-01, two post-activity tarpaulin samples and one post-activity settled dust (floor) sample at 3 feet were not collected. For unit 4-01, one post-activity tarpaulin sample was not collected.
(2) Two additional regular samples were collected at unit 2-01: one post-activity tarpaulin and one exterior paint chip. One additional 2 -hour post-activity settled dust (stainless steel dust collector) sample was collected at unit 3-01. Two additional QC samples, both paint chip field blanks, were collected at units 1-01 and 4-01. Additional personal air monitor samples collected when filled cassettes were replaced account for the other regular samples in this column.
${ }^{(3)}$ Tarpaulin samples were collected but not analyzed. They will be archived.
${ }^{(4)}$ One window well sample from unit 1-01 was deleted from the analysis because it was identified as an outlier. One 2-hour postactivity settled dust (stainless steel dust collector) sample was deleted from analysis because of a protocol deviation. This collector was placed after activity had been completed.

Table WR-2a. Descriptive Statistics (Across All Units) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) Associated With Personal Air, Pre-Activity Area Air, and During-Activity Area Air Samples Collected During Window Replacement

| Sample Type |  | Arithmetic | Geometric <br> Mean | Log <br> Std. <br> Dev. ${ }^{1}$ | Minimum <br> Value | Maximum <br> Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| During-Activity <br> Personal <br> Exposure Samples | 8 | 13.95 | 7.48 | 1.19 | 2.41 | 44.29 |
| Pre-Activity <br> Ambient Air <br> Samples | 4 | 0.83 | 0.30 | 1.58 | 0.10 | 2.86 |
| Post-Activity <br> Ambient Air <br> Samples | 8 | 1.54 | 1.16 | 0.82 | 0.29 | 4.16 |

${ }^{(1)}$ Standard deviation of the log transformed data (expressed in log measurement units).

Table WR-2b. Descriptive Statistics (Within Each Unit) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) Associated With Personal Air, Pre-Activity Area Air, and During-Activity Area Air Samples Collected During Window Replacement

| Unit <br> ID | N | Arithmetic <br> Mean | Geometric <br> Mean | Log Std. <br> Dev. ${ }^{(1)}$ | Minimum <br> Value | Maximum <br> Value | Baseline <br> (Pre-Activity <br> Value) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Personal Air Sample Results |  |  |  |  |  |  |  |
| $1-01$ | 2 | 2.88 | 2.87 | 0.17 | 2.55 | 3.22 |  |
| $2-01$ | 2 | 3.45 | 3.29 | 0.44 | 2.41 | 4.49 |  |
| $3-01$ | 2 | 37.98 | 37.46 | 0.24 | 31.67 | 44.29 |  |
| $4-01$ | 2 | 11.50 | 8.85 | 1.07 | 4.15 | 18.84 |  |
|  |  |  | Ambient Air Sample Results |  |  |  |  |
| $1-01$ | 2 | 0.56 | 0.50 | 0.74 | 0.29 | 0.84 | 0.10 |
| $2-01$ | 2 | 1.00 | 0.55 | 0.48 | 0.68 | 1.33 | 0.10 |
| $3-01$ | 2 | 3.41 | 3.33 | 0.32 | 2.66 | 4.16 | 0.27 |
| $4-01$ | 2 | 1.18 | 1.17 | 0.16 | 1.05 | 1.31 | 2.86 |

[^1]Table WR-3a. Descriptive Statistics (Across All Units) of Sample Weight (g) Associated With Vacuum Samples from Floors Collected Before ("pre") and at One Hour Following Completion of Window Replacement ("post")

| Data <br> Representation | Distance <br> (feet) | $\mathbf{N}$ | Arithmetic <br> Mean | Geometric <br> Mean | Log Std. <br> Dev. ${ }^{(1)}$ | Minimum <br> Value | Maximum <br> Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pre-activity | 0 | 12 | 4.1668 | 0.7219 | 2.5855 | 0.0076 | 20.4911 |
| Pre-activity ${ }^{\left({ }^{(2)}\right.}$ | 3 | 11 | 0.7965 | 0.3436 | 1.8286 | 0.0055 | 2.8148 |
| Pre-activity ${ }^{(3)}$ | 6 | 16 | 0.6935 | 0.1588 | 2.4357 | 0.0008 | 2.9056 |
| Post-activity | 0 | 12 | 3.1297 | 0.7992 | 2.5822 | 0.0058 | 7.1463 |
| Post-activity $y^{(4)}$ | 3 | 10 | 0.9499 | 0.2878 | 2.3679 | 0.0037 | 3.3809 |
| Post-activity ${ }^{(3)}$ | 6 | 16 | 0.9403 | 0.2498 | 2.0747 | 0.0088 | 3.2372 |
| Paired Difference <br> (Post minus Pre) | 0 | 12 | -1.0371 | $1.1070^{(5)}$ | . | -14.7512 | 4.4551 |
| Paired Difference <br> (Post minus Pre) $)^{(3,4)}$ | 3 | 10 | 0.3552 | $1.0335^{(5)}$ | . | -0.3251 | 2.8118 |
| Paired Difference <br> (Post minus Pre) $)^{(3,6)}$ | 6 | 15 | 0.2584 | $1.4730^{(5)}$ | . | -0.8229 | 2.2498 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ One pre-activity floor sample at 3 feet was not collected at unit 2-01.
${ }^{(3)}$ Results include both regular and QC samples.
${ }^{(4)}$ Two post-activity floor samples at 3 feet were not collected: one at unit 2-01 and one at unit 3-01.
${ }^{(5)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(6)}$ One pre-activity/post-activity pair is excluded because the pre-activity sample location differed from the post-activity sample location.

Table WR-3b. Descriptive Statistics (Across All Units) of Lead Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated With Vacuum Samples from Floors Collected Before ("pre") and at One Hour Following Completion of Window Replacement ("post")

| Data Representation | $\begin{gathered} \hline \hline \text { Distance } \\ \text { (feet) } \\ \hline \end{gathered}$ | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pre-activity | 0 | 12 | 58016.8 | 1913.3 | 3.63 | 9.0 | 439845.0 |
| Pre-activity ${ }^{(2)}$ | 3 | 11 | 5424.6 | 490.6 | 3.22 | 2.3 | 29402.0 |
| Pre-activity ${ }^{(3)}$ | 6 | 16 | 3562.0 | 334.3 | 2.99 | 1.7 | 18443.2 |
| Post-activity | 0 | 12 | 35499.4 | 3912.1 | 3.02 | 19.0 | 109740.0 |
| Post-activity ${ }^{(4)}$ | 3 | 10 | 5504.4 | 1293.5 | 2.43 | 56.0 | 12702.0 |
| Post-activity ${ }^{(3)}$ | 6 | 16 | 9357.9 | 878.4 | 3.01 | 10.4 | 54515.0 |
| Paired Difference (Post minus Pre) | 0 | 12 | -22517.3 | $2.0^{(5)}$ | . | -354160.0 | 92013.0 |
| Paired Difference (Post minus Pre) ${ }^{(3,4)}$ | 3 | 10 | 448.8 | $3.5{ }^{(5)}$ | . | -19060.0 | 10856.4 |
| Paired Difference (Post minus Pre) ${ }^{(3,6)}$ | 6 | 15 | 6179.1 | $2.6{ }^{(5)}$ | . | -540.3 | 36071.8 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ One pre-activity floor sample at 3 feet was not collected at unit 2-01.
${ }^{(3)}$ Results include both regular and QC samples.
${ }^{(4)}$ Two post-activity floor samples at 3 feet were not collected: one at unit 2-01 and one at unit 3-01.
${ }^{(5)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(6)}$ One pre-activity/post-activity pair is excluded because the pre-activity sample location differed from the post-activity sample location.

Table WR-3c. Descriptive Statistics (Across All Units) of Lead Concentration ( $\mu \mathrm{g} / \mathrm{g}$ ) Associated With Vacuum Samples from Floors Collected Before ("pre") and at One Hour Following Completion of Window Replacement ("post")

| Data <br> Representation | Distance <br> (feet) | $\mathbf{N}$ | Arithmetic <br> Mean | Geometric <br> Mean | Log Std. <br> Dev. ${ }^{(1)}$ | Minimum <br> Value | Maximum <br> Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Pre-activity | 0 | 12 | 7047.0 | 2650.2 | 1.58 | 228.5 | 33003.6 |
| Pre-activity ${ }^{(2)}$ | 3 | 11 | 5735.5 | 1503.0 | 1.74 | 155.6 | 37114.5 |
| Pre-activity ${ }^{(3)}$ | 6 | 16 | 4243.5 | 2105.1 | 1.37 | 136.0 | 16470.1 |
| Post-activity | 0 | 12 | 11299.6 | 4886.5 | 1.80 | 234.8 | 26874.7 |
| Post-activity ${ }^{(4)}$ | 3 | 10 | 11112.0 | 4494.7 | 2.19 | 31.8 | 32346.0 |
| Post-activity ${ }^{(3)}$ | 6 | 16 | 6898.3 | 3516.2 | 1.25 | 632.4 | 31728.1 |
| Paired Difference <br> Post minus Pre) $^{\text {Pos }}$ | 0 | 12 | 4251.7 | $1.8^{(5)}$ |  | . | -15767.1 |
| Paired Difference <br> $(\text { Post minus Pre) })^{(3,4)}$ | 3 | 10 | 5126.8 | $3.2^{(5)}$ |  | 23378.0 |  |
| Paired Difference <br> $(\text { Post minus Pre) })^{(3,6)}$ | 6 | 15 | 2838.0 | $1.7^{(5)}$ |  | -27343.0 | 31925.8 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ One pre-activity floor sample at 3 feet was not collected at unit 2-01.
${ }^{(3)}$ Results include both regular and QC samples.
${ }^{(4)}$ Two post-activity floor samples at 3 feet were not collected: one at unit 2-01 and one at unit 3-01.
${ }^{(5)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(6)}$ One pre-activity/post-activity pair is excluded because the pre-activity sample location differed from the post-activity sample location.

Table WR-3d. Descriptive Statistics (Within Each Unit) of Sample Weight (g) Associated With Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -- at a Distance of 0 Feet from the Windows

| Unit ID | Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 3 | 0.0514 | 0.0468 | 0.5121 | 0.0347 | 0.0846 |
|  | Post-Activity | 3 | 0.0414 | 0.0212 | 1.4559 | 0.0058 | 0.1024 |
|  | Paired Difference <br> (Post minus pre) | 3 | -0.0100 | $0.4522^{(2)}$ | ${ }^{\cdot}$ | -0.0292 | 0.0178 |
| 2-01 | Pre-Activity | 3 | 1.1503 | 0.2333 | 3.0698 | 0.0076 | 2.8584 |
|  | Post-Activity | 3 | 3.6090 | 1.3251 | 2.4222 | 0.0809 | 5.7063 |
|  | Paired Difference (Post minus pre) | 3 | 2.4588 | $5.6788^{(2)}$ | . | 0.0733 | 4.4551 |
| 3-01 | Pre-Activity | 3 | 3.7352 | 3.4471 | 0.4749 | 2.5883 | 5.9636 |
|  | Post-Activity | 3 | 4.9993 | 4.7908 | 0.3486 | 3.7681 | 7.1463 |
|  | Paired Difference <br> (Post minus pre) | 3 | 1.2641 | $1.3898{ }^{(2)}$ | . | 1.1145 | 1.4951 |
| 4-01 | Pre-Activity | 3 | 11.7303 | 7.2101 | 1.4526 | 1.3725 | 20.4911 |
|  | Post-Activity | 3 | 3.8689 | 3.0337 | 0.9652 | 0.9993 | 5.7399 |
|  | Paired Difference <br> (Post minus pre) | 3 | -7.8613 | $0.4208{ }^{(2)}$ | . | -14.7512 | -0.3732 |

[^2]Table WR-3e. Descriptive Statistics (Within Each Unit) of Sample Weight (g) Associated with Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -at a Distance of 3 Feet from the Windows

| Unit <br> ID | $\begin{gathered} \hline \text { Data } \\ \text { Representation } \\ \hline \end{gathered}$ | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{1}$ | $\begin{gathered} \hline \hline \text { Minimum } \\ \text { Value } \end{gathered}$ | $\begin{gathered} \hline \text { Maximum } \\ \text { Value } \end{gathered}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 3 | 0.0727 | 0.0337 | 1.7291 | 0.0055 | 0.1721 |
|  | Post-Activity | 3 | 0.0550 | 0.0146 | 2.0594 | 0.0037 | 0.1559 |
|  | Paired Difference (Post minus pre) | 3 | -0.0177 | $0.4328{ }^{(2)}$ |  | -0.0352 | -0.0018 |
| $2-01^{(3)}$ | Pre-Activity | 2 | 0.3519 | 0.2769 | 1.0189 | 0.1347 | 0.5691 |
|  | Post-Activity | 2 | 1.8266 | 0.9595 | 1.7812 | 0.2723 | 3.3809 |
|  | Paired Difference (Post minus pre) | 2 | 1.4747 | $3.4655^{(2)}$ |  | 0.1376 | 2.8118 |
| 3-01 ${ }^{(4)}$ | Pre-Activity | 3 | 1.6617 | 1.4741 | 0.5900 | 0.8863 | 2.8148 |
|  | Post-Activity | 2 | 1.1396 | 0.9819 | 0.7911 | 0.5612 | 1.7179 |
|  | Paired Difference (Post minus pre) | 2 | 0.0544 | $0.9204^{(2)}$ |  | -0.3251 | 0.4339 |
| 4-01 | Pre-Activity | 3 | 0.9516 | 0.9422 | 0.1726 | 0.7922 | 1.1187 |
|  | Post-Activity | 3 | 1.1339 | 1.1213 | 0.1808 | 0.9700 | 1.3732 |
|  | Paired Difference (Post minus pre) | 3 | 0.1823 | $1.1901^{(2)}$ |  | -0.1487 | 0.4294 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(3)}$ One set of the pre- and post-activity samples at this unit were not collected due to space and time constraints.
${ }^{(4)}$ The post-activity sample was not collected. Sampler ran out of sampling bottles.

Table WR-3f. Descriptive Statistics (Within Each Unit) of Sample Weight (g) Associated with Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -- at a Distance of 6 Feet from the Windows ${ }^{(1)}$

| Unit <br> ID | Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 4 | 0.0466 | 0.0184 | 2.1805 | 0.0008 | 0.0967 |
|  | Post-Activity | 4 | 0.0500 | 0.0413 | 0.7165 | 0.0224 | 0.0952 |
|  | Paired Difference (Post minus pre) ${ }^{(4)}$ | 3 | -0.0196 | $1.8163^{(3)}$ | . | -0.0438 | 0.0223 |
| 2-01 | Pre-Activity | 4 | 0.0744 | 0.0252 | 1.6986 | 0.0062 | 0.2505 |
|  | Post-Activity | 4 | 0.1002 | 0.0409 | 1.6376 | 0.0088 | 0.2981 |
|  | Paired Difference (Post minus pre) | 4 | 0.0258 | $1.6228{ }^{(3)}$ | . | 0.0009 | 0.0478 |
| 3-01 | Pre-Activity | 4 | 1.1280 | 1.0180 | 0.5600 | 0.4699 | 1.5553 |
|  | Post-Activity | 4 | 1.5855 | 1.3877 | 0.6043 | 0.7324 | 2.7197 |
|  | Paired Difference (Post minus pre) | 4 | 0.4575 | $1.3632^{(3)}$ | . | -0.8229 | 2.2498 |
| 4-01 | Pre-Activity | 4 | 1.5252 | 1.3453 | 0.5583 | 0.7727 | 2.9056 |
|  | Post-Activity | 4 | 2.0256 | 1.6609 | 0.7565 | 0.7517 | 3.2372 |
|  | Paired Difference (Post minus pre) | 4 | 0.5004 | $1.2346{ }^{(3)}$ | . | -0.5511 | 1.9870 |

${ }^{(1)}$ Includes QC samples and regular samples.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(4)}$ One pre-activity/post-activity pair is excluded because the pre-activity sample location differed from the post-activity sample location.

Table WR-3g. Descriptive Statistics (Within Each Unit) of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated with Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -- at a Distance of 0 Feet from the Windows

| Unit ID | Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 3 | 79.4 | 36.4 | 1.58 | 9.0 | 202.9 |
|  | Post-Activity | 3 | 246.4 | 226.9 | 0.50 | 140.0 | 379.1 |
|  | Paired Difference (Post minus pre) | 3 | 167.0 | $6.2^{(2)}$ | . | 113.7 | 211.1 |
| 2-01 | Pre-Activity | 3 | 419.3 | 220.3 | 1.78 | 28.4 | 653.0 |
|  | Post-Activity | 3 | 1191.2 | 389.8 | 2.62 | 19.0 | 1980.5 |
|  | Paired Difference (Post minus pre) | 3 | 771.9 | $1.8{ }^{(2)}$ | . | -9.4 | 1403.8 |
| 3-01 | Pre-Activity | 3 | 35699.2 | 31474.6 | 0.61 | 17727.0 | 60108.0 |
|  | Post-Activity | 3 | 96981.7 | 96448.9 | 0.13 | 84851.0 | 109740.0 |
|  | Paired Difference (Post minus pre) | 3 | 61282.5 | $3.1{ }^{(2)}$ | . | 24743.0 | 92013.0 |
| 4-01 | Pre-Activity | 3 | 195869.0 | 53110.0 | 2.76 | 2342.1 | 439845.0 |
|  | Post-Activity | 3 | 43578.4 | 27459.9 | 1.35 | 6224.0 | 85685.1 |
|  | Paired Difference (Post minus pre) | 3 | -152291.0 | $0.5^{(2)}$ | . | -354160.0 | 3881.9 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.

Table WR-3h. Descriptive Statistics (Within Each Unit) of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated with Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -- at a Distance of 3 Feet from the Windows

| Unit ID | Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{\text {(1) }}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 3 | 15.1 | 10.0 | 1.29 | 2.3 | 26.8 |
|  | Post-Activity | 3 | 884.0 | 255.1 | 2.00 | 56.0 | 2476.4 |
|  | Paired Difference (Post minus pre) | 3 | 868.9 | $25.5{ }^{(2)}$ |  | 39.8 | 2449.6 |
| $2-01^{(3)}$ | Pre-Activity | 2 | 93.5 | 67.7 | 1.20 | 29.0 | 158.0 |
|  | Post-Activity | 2 | 84.7 | 81.5 | 0.39 | 61.7 | 107.6 |
|  | Paired Difference (Post minus pre) | 2 | -8.8 | $1.2^{(2)}$ |  | -50.3 | 32.7 |
| $3-01^{(4)}$ | Pre-Activity | 3 | 8255.4 | 7746.0 | 0.46 | 4623.8 | 11027.0 |
|  | Post-Activity | 2 | 10427.0 | 10427.0 | 0.00 | 10425.0 | 10429.0 |
|  | Paired Difference (Post minus pre) | 2 | 2601.6 | $1.5{ }^{(2)}$ |  | -598.0 | 5801.2 |
| 4-01 | Pre-Activity | 3 | 11557.4 | 5706.5 | 1.45 | 1845.6 | 29402.0 |
|  | Post-Activity | 3 | 10456.0 | 10302.4 | 0.21 | 8324.1 | 12702.0 |
|  | Paired Difference (Post minus pre) | 3 | -1101.3 | $1.8{ }^{(2)}$ |  | -19060.0 | 10856.4 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(3)}$ Both the pre- and post-activity samples at this unit were not collected due to space and time constraints.
${ }^{(4)}$ The post-activity sample was not collected. Sampler ran out of sampling bottles.

Table WR-3i. Descriptive Statistics (Within Each Unit) of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated with Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -- at a Distance of 6 Feet from the Windows ${ }^{(1)}$

| Unit ID | Data Representation | N | Arithmetic Mean | Geometric Mean | $\begin{gathered} \hline \text { Log Std. } \\ \text { Dev. }{ }^{(2)} \\ \hline \end{gathered}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 4 | 20.3 | 11.8 | 1.40 | 1.7 | 48.8 |
|  | Post-Activity | 4 | 104.7 | 72.0 | 1.03 | 20.2 | 252.8 |
|  | Paired Difference (Post minus pre) ${ }^{(4)}$ | 3 | 96.5 | $7.2^{(3)}$ | . | 18.5 | 239.7 |
| 2-01 | Pre-Activity | 4 | 41.6 | 40.1 | 0.32 | 25.9 | 51.5 |
|  | Post-Activity | 4 | 70.5 | 41.9 | 1.21 | 10.4 | 190.4 |
|  | Paired Difference (Post minus pre) | 4 | 28.9 | $1.0^{(3)}$ | . | -20.2 | 151.8 |
| 3-01 | Pre-Activity | 4 | 6117.5 | 4048.8 | 1.05 | 1227.2 | 15796.0 |
|  | Post-Activity | 4 | 10641.9 | 9004.5 | 0.74 | 3162.9 | 17136.4 |
|  | Paired Difference (Post minus pre) | 4 | 4524.4 | $2.2{ }^{(3)}$ | . | -540.3 | 11542.8 |
| 4-01 | Pre-Activity | 4 | 8068.4 | 6496.9 | 0.70 | 4272.7 | 18443.2 |
|  | Post-Activity | 4 | 26614.4 | 21937.5 | 0.72 | 9668.8 | 54515.0 |
|  | Paired Difference (Post minus pre) | 4 | 18545.9 | $3.4{ }^{(3)}$ | . | 5369.0 | 36071.8 |

${ }^{(1)}$ Includes QC samples and regular samples.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(4)}$ One pre-activity/post-activity pair is excluded because the pre-activity sample location differed from the post-activity sample location.

Table WR-3j. Descriptive Statistics (Within Each Unit) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) Associated with Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -- at a Distance of 0 Feet from the Windows

| Unit ID | Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 3 | 1136.8 | 776.9 | 1.11 | 260.2 | 2398.8 |
|  | Post-Activity | 3 | 13862.3 | 10711.0 | 0.96 | 3702.4 | 24129.3 |
|  | Paired Difference (Post minus pre) | 3 | 12725.5 | $13.8{ }^{(2)}$ | . | 1303.6 | 23378.0 |
| 2-01 | Pre-Activity | 3 | 1650.1 | 944.1 | 1.40 | 228.5 | 3735.9 |
|  | Post-Activity | 3 | 301.2 | 294.2 | 0.26 | 234.8 | 393.0 |
|  | Paired Difference (Post minus pre) | 3 | -1348.9 | $0.3{ }^{(2)}$ | . | -3501.1 | 47.4 |
| 3-01 | Pre-Activity | 3 | 11469.1 | 9130.8 | 0.80 | 4906.9 | 22651.5 |
|  | Post-Activity | 3 | 20958.7 | 20132.1 | 0.36 | 13483.1 | 26874.7 |
|  | Paired Difference (Post minus pre) | 3 | 9489.6 | $2.2{ }^{(2)}$ | . | -133.2 | 20025.8 |
| 4-01 | Pre-Activity | 3 | 13935.6 | 7366.1 | 1.48 | 1706.4 | 33003.6 |
|  | Post-Activity | 3 | 10076.3 | 8988.3 | 0.57 | 6228.4 | 17236.4 |
|  | Paired Difference (Post minus pre) | 3 | -3859.3 | $1.2^{(2)}$ | . | -15767.1 | 4521.9 |

[^3]Table WR-3k. Descriptive Statistics (Within Each Unit) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) Associated with Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -- at a Distance of 3 Feet from the Windows

| Unit ID | Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 3 | 324.8 | 296.5 | 0.56 | 155.6 | 420.2 |
|  | Post-Activity | 3 | 19535.7 | 17469.5 | 0.57 | 10376.5 | 32346.0 |
|  | Paired Difference (Post minus pre) | 3 | 19210.8 | $58.9^{(2)}$ | . | 9977.8 | 31925.8 |
| $2-01^{(3)}$ | Pre-Activity | 2 | 352.0 | 324.4 | 0.58 | 215.4 | 488.6 |
|  | Post-Activity | 2 | 129.3 | 84.9 | 1.39 | 31.8 | 226.7 |
|  | Paired Difference (Post minus pre) | 2 | -222.7 | $0.26{ }^{(2)}$ | . | -456.7 | 11.3 |
| $3-01^{(4)}$ | Pre-Activity | 3 | 6427.0 | 5254.7 | 0.75 | 3238.4 | 12441.6 |
|  | Post-Activity | 2 | 12325.9 | 10619.4 | 0.79 | 6068.5 | 18583.4 |
|  | Paired Difference (Post minus pre) | 2 | 4304.6 | $1.59^{(2)}$ | . | 2467.4 | 6141.8 |
| 4-01 | Pre-Activity | 3 | 14043.7 | 6056.6 | 1.59 | 1955.5 | 37114.4 |
|  | Post-Activity | 3 | 9200.9 | 9188.0 | 0.065 | 8581.5 | 9771.4 |
|  | Paired Difference (Post minus pre) | 3 | -4842.7 | $1.52^{(2)}$ |  | -27343.0 | 7294.4 |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(3)}$ Both the pre- and post-activity samples at this unit were not collected due to space and time constraints.
${ }^{(4)}$ The post-activity sample was not collected. Sampler ran out of sampling bottles.

Table WR-3I. Descriptive Statistics (Within Each Unit) of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) Associated with Vacuum Samples from Floors Collected Before ("pre") and One Hour Following Completion of Window Replacement ("post") -- at a Distance of 6 Feet from the Windows ${ }^{(1)}$

| Unit ID | Data Representation | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | Pre-Activity | 4 | 953.8 | 641.5 | 1.15 | 136.0 | 2160.4 |
|  | Post-Activity | 4 | 2351.9 | 1741.8 | 0.94 | 688.8 | 4263.7 |
|  | Paired Difference (Post minus pre) ${ }^{(4)}$ | 3 | 1895.0 | $4.0^{(3)}$ | . | -1284.8 | 4127.8 |
| 2-01 | Pre-Activity | 4 | 3289.0 | 1593.7 | 1.70 | 154.0 | 8161.3 |
|  | Post-Activity | 4 | 1189.2 | 1024.0 | 0.61 | 632.4 | 2304.5 |
|  | Paired Difference (Post minus pre) | 4 | -2099.8 | $0.6^{(3)}$ | . | -5856.8 | 484.6 |
| 3-01 | Pre-Activity | 4 | 5950.0 | 3977.4 | 0.94 | 2381.0 | 16345.2 |
|  | Post-Activity | 4 | 7909.2 | 6488.8 | 0.67 | 4318.5 | 17677.3 |
|  | Paired Difference (Post minus pre) | 4 | 1959.2 | $1.6{ }^{(3)}$ | . | 1332.1 | 2483.5 |
| 4-01 | Pre-Activity | 4 | 6781.0 | 4829.3 | 0.94 | 1809.6 | 16470.1 |
|  | Post-Activity | 4 | 16142.9 | 13208.1 | 0.74 | 5691.2 | 31728.1 |
|  | Paired Difference (Post minus pre) | 4 | 9361.9 | $2.7{ }^{(3)}$ | . | 1076.9 | 28448.5 |

${ }^{(1)}$ Includes QC samples and regular samples.
${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(3)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.
${ }^{(4)}$ One pre-activity/post-activity pair is excluded because the pre-activity sample location differed from the post-activity sample location.

Table WR-4a. Descriptive Statistics (Across All Units) of Sample Weights, Lead Loadings, and Lead Concentrations Associated with Vacuum Samples from Stainless Steel Dustfall Collectors at One and Two Hours Following Completion of Window Replacement

| Data Representation | Distance (feet) | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample Weight (g) |  |  |  |  |  |  |  |
| One-hour | 0 | 12 | 4.6002 | 1.2420 | 1.8070 | 0.1095 | 21.7653 |
| One-hour ${ }^{(2)}$ | 6 | 16 | 0.2710 | 0.0428 | 2.1259 | 0.0023 | 1.6381 |
| Two-hour | 6 | 4 | 0.1048 | 0.0522 | 1.5476 | 0.0097 | 0.2056 |
| Paired Differences (2-hr minus 1-hr) | 6 | 4 | 0.0409 | $1.3878^{(3)}$ | 0.5332 | -0.0040 | 0.1123 |
| Lead Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |  |  |  |  |  |  |  |
| One-hour | 0 | 12 | 84604.1 | 24736.3 | 1.67 | 3104.0 | 331410.0 |
| One-hour ${ }^{(2)}$ | 6 | 16 | 770.6 | 240.6 | 1.75 | 15.4 | 4155.0 |
| Two-hour | 6 | 4 | 5252.5 | 519.6 | 2.69 | 40.4 | 20192.0 |
| Paired Differences (2-hr minus 1-hr) | 6 | 4 | 5247.3 | $2.9{ }^{(3)}$ | 0.58 | 37.7 | 20183.7 |
| Lead Concentration ( $\mu \mathrm{g} / \mathrm{g}$ ) |  |  |  |  |  |  |  |
| One-hour | 0 | 12 | 27274.5 | 13826.9 | 1.54 | 489.6 | 87222.4 |
| One-hour ${ }^{(2)}$ | 6 | 16 | 29669.2 | 5620.2 | 1.88 | 114.4 | 335193.5 |
| Two-hour | 6 | 4 | 33634.9 | 9951.8 | 2.15 | 763.1 | 98210.1 |
| Paired Differences (2-hr minus 1-hr) | 6 | 4 | 23553.2 | $2.1{ }^{(3)}$ | 0.94 | -697.9 | 71879.3 |

${ }^{(1)}$ Standard deviations of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Results for both regular and QC samples.
${ }^{(3)}$ Geometric mean of the ratio of the 2 -hour result to the result of the adjoining 1-hour sample. No measurement units are associated with this value.

Table WR-4b. Descriptive Statistics (for Each Unit) of Sample Weight (g) Associated with Vacuum Samples from Stainless Steel Dustfall Collectors at One and Two Hours Following Completion of Carpet Removal

| Unit ID | Data <br> Representation | Distance (feet) | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | One-hour | 0 | 3 | 0.1968 | 0.1812 | 0.5038 | 0.1095 | 0.2999 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 0.0066 | 0.0056 | 0.6380 | 0.0031 | 0.0137 |
|  | Two-hour | 6 | 1 | 0.0097 | 0.0097 | . | 0.0097 | 0.0097 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | -0.0040 | $0.7080^{(3)}$ | . | -0.0040 | -0.0040 |
| 2-01 | One-hour | 0 | 3 | 8.5455 | 4.3343 | 1.3981 | 1.8604 | 21.7653 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 0.9407 | 0.5462 | 1.4693 | 0.0713 | 1.6381 |
|  | Two-hour | 6 | 1 | 0.1836 | 0.1836 | . | 0.1836 | 0.1836 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 0.1123 | $2.5750{ }^{(3)}$ | . | 0.1123 | 0.1123 |
| 3-01 | One-hour | 0 | 3 | 2.8128 | 2.3217 | 0.7399 | 1.2872 | 5.3255 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 0.0233 | 0.0111 | 1.4289 | 0.0023 | 0.0706 |
|  | Two-hour | 6 | 1 | 0.0203 | 0.0203 | . | 0.0203 | 0.0203 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 0.0073 | $1.5615^{(3)}$ | . | 0.0073 | 0.0073 |
| 4-01 | One-hour | 0 | 3 | 6.8456 | 1.3053 | 2.5906 | 0.1107 | 19.3900 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 0.1135 | 0.0992 | 0.6714 | 0.0369 | 0.1578 |
|  | Two-hour | 6 | 1 | 0.2056 | 0.2056 |  | 0.2056 | 0.2056 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 0.0478 | $1.3029^{(3)}$ | . | 0.0478 | 0.0478 |

${ }^{(1)}$ Standard deviations of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Results for both regular and QC samples.
${ }^{(3)}$ Geometric mean of the ratio of the 2-hour result to the result of the adjoining 1-hour sample. No measurement units are associated with this value.

Table WR-4c. Descriptive Statistics (for Each Unit) of Lead Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) Associated with Vacuum Samples from Stainless Steel Dustfall Collectors at One and Two Hours Following Completion of Carpet Removal

| Unit ID | Data Representation | Distance (feet) | $N$ | Arithmetic Mean | Geometric Mean | Log Std. $\text { Dev. }{ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | One-hour | 0 | 3 | 11908.7 | 8417.5 | 0.98 | 4489.1 | 26158.0 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 285.8 | 70.3 | 1.89 | 15.4 | 1039.1 |
|  | Two-hour | 6 | 1 | 40.4 | 40.4 | . | 40.4 | 40.4 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 37.7 | $2.6339^{(3)}$ | . | 37.7 | 37.7 |
| 2-01 | One-hour | 0 | 3 | 83903.3 | 26367.0 | 1.90 | 7361.3 | 233692.9 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 840.4 | 327.8 | 1.48 | 104.2 | 2863.4 |
|  | Two-hour | 6 | 1 | 140.1 | 140.1 | . | 140.1 | 140.1 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 135.5 | $1.3450{ }^{(3)}$ | . | 135.5 | 135.6 |
| 3-01 | One-hour | 0 | 3 | 129459.7 | 60404.1 | 1.54 | 16387.0 | 331410.0 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 166.5 | 105.2 | 1.31 | 16.7 | 365.5 |
|  | Two-hour | 6 | 1 | 637.4 | 637.4 | . | 637.4 | 637.4 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 632.4 | $4.2953{ }^{(3)}$ | . | 632.4 | 632.5 |
| 4-01 | One-hour | 0 | 3 | 113144.7 | 27927.6 | 2.32 | 3104.0 | 313980.0 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 1789.6 | 1382.7 | 0.80 | 619.0 | 4155.0 |
|  | Two-hour | 6 | 1 | 20192.0 | 20192.0 | . | 20192.0 | 20192.0 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 20183.7 | $4.8597^{(3)}$ | . | 20183.7 | 20183.7 |

[^4]Table WR-4d. Descriptive Statistics (for Each Unit) of Lead Concentration ( $\mu \mathrm{g} / \mathrm{g}$ ) Associated with Vacuum Samples from Stainless Steel Dustfall Collectors at One and Two Hours Following Completion of Carpet Removal

| Unit ID | Data Representation | Distance (feet) | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | One-hour | 0 | 3 | 52798.0 | 46459.8 | 0.63 | 24788.0 | 87222.4 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 88953.5 | 12547.8 | 2.43 | 1120.3 | 335193.5 |
|  | Two-hour | 6 | 1 | 4168.2 | 4168.2 | . | 4168.2 | 4168.2 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 3048.0 | $3.7207^{(3)}$ | . | 3048.0 | 3048.0 |
| 2-01 | One-hour | 0 | 3 | 1967.8 | 1413.2 | 1.05 | 489.6 | 3956.8 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 956.8 | 600.1 | 1.28 | 114.4 | 1827.1 |
|  | Two-hour | 6 | 1 | 763.1 | 763.1 | . | 763.1 | 763.1 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | -697.9 | $0.5223^{(3)}$ | . | -697.9 | -697.9 |
| 3-01 | One-hour | 0 | 3 | 32397.0 | 26017.3 | 0.81 | 12730.7 | 62230.8 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 10727.3 | 9505.6 | 0.57 | 5177.3 | 19074.7 |
|  | Two-hour | 6 | 1 | 31398.0 | 31398.0 | . | 31398.0 | 31398.0 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 2 | 19983.4 | $2.7507^{(3)}$ | . | 19983.4 | 19983.4 |
| 4-01 | One-hour | 0 | 3 | 21935.3 | 21396.3 | 0.27 | 16192.9 | 28039.8 |
|  | One-hour ${ }^{(2)}$ | 6 | 4 | 18039.1 | 13938.6 | 0.87 | 5322.2 | 32116.5 |
|  | Two-hour | 6 | 1 | 98210.1 | 98210.1 | . | 98210.1 | 98210.1 |
|  | Paired Differences (2-hr minus 1-hr) | 6 | 1 | 71879.3 | $3.7300^{(3)}$ | . | 71879.3 | 71879.3 |

[^5]Table WR-5a. Descriptive Statistics (Across All Units) of Sample Weights, Lead Loadings, and Lead Concentrations Associated with Vacuum Samples from Window Wells Taken Prior to Window Replacement ${ }^{(1)}$

| Data Parameter | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample Weights <br> (g) | $\begin{array}{r} 11 \\ (12) \\ \hline \end{array}$ | $\begin{array}{r} 4.906 \\ (4.529) \\ \hline \end{array}$ | $\begin{array}{r} 3.029 \\ (2.552) \\ \hline \end{array}$ | $\begin{array}{r} 1.258 \\ (1.338) \\ \hline \end{array}$ | $\begin{array}{r} 0.295 \\ (0.295) \\ \hline \end{array}$ | $\begin{array}{r} 13.576 \\ (13.576) \\ \hline \end{array}$ |
| Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | $\begin{array}{r} 11 \\ (12) \\ \hline \end{array}$ | $\begin{array}{r} 185742.2 \\ (170456.3) \\ \hline \end{array}$ | $\begin{array}{r} 134531.0 \\ (95884.2) \\ \hline \end{array}$ | $\begin{array}{r} 0.94 \\ (1.48) \\ \hline \end{array}$ | $\begin{array}{r} 26786.0 \\ (2311.7) \\ \hline \end{array}$ | $\begin{array}{r} 415342.3 \\ (415342.3) \\ \hline \end{array}$ |
| Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) | $\begin{array}{r} 11 \\ (12) \\ \hline \end{array}$ | $\begin{array}{r} 28476.47 \\ (26293.65) \\ \hline \end{array}$ | $\begin{array}{r} 23482.54 \\ (19336.86) \\ \hline \end{array}$ | $\begin{gathered} 0.653 \\ (0.917) \\ \hline \end{gathered}$ | $\begin{array}{r} 8458.91 \\ (2282.63) \\ \hline \end{array}$ | $\begin{array}{r} 70067.02 \\ (70067.02) \\ \hline \end{array}$ |

${ }^{(1)}$ Results in parentheses summarize values with outlier included.
(2) Standard deviation of the log-transformed data (expressed in log measurement units).

Table WR-5b. Descriptive Statistics (Within Each Unit) of Sample Weights, Lead Loadings, and Lead Concentrations Associated with Vacuum Samples from the Window Wells Taken Prior to Window Replacement ${ }^{(1)}$

| Unit ID | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(2)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample Weights (g) |  |  |  |  |  |  |
| 1-01 | $\begin{gathered} 2 \\ (3) \\ \hline \end{gathered}$ | $\begin{gathered} 0.297 \\ (0.327) \end{gathered}$ | $\begin{gathered} 0.297 \\ (0.324) \end{gathered}$ | $\begin{gathered} 0.0081 \\ (0.1532) \\ \hline \end{gathered}$ | $\begin{gathered} 0.295 \\ (0.295) \\ \hline \end{gathered}$ | $\begin{gathered} 0.298 \\ (0.387) \end{gathered}$ |
| 2-01 | 3 | 2.924 | 2.913 | 0.1071 | 2.613 | 3.237 |
| 3-01 | 3 | 5.525 | 5.304 | 0.3411 | 4.295 | 7.861 |
| 4-01 | 3 | 9.341 | 8.464 | 0.5718 | 4.483 | 13.577 |
| Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |  |  |  |  |  |  |
| 1-01 | $\begin{gathered} 2 \\ (3) \\ \hline \end{gathered}$ | $\begin{array}{r} 44014.3 \\ (30113.4) \\ \hline \end{array}$ | $\begin{gathered} 42687.2 \\ (16150.0) \\ \hline \end{gathered}$ | $\begin{gathered} 0.35 \\ (1.70) \\ \hline \end{gathered}$ | $\begin{aligned} & 33287.6 \\ & (2311.7) \\ & \hline \end{aligned}$ | $\begin{gathered} 54741.0 \\ (54741.0) \\ \hline \end{gathered}$ |
| 2-01 | 3 | 224769.5 | 215579.7 | 0.36 | 145304.8 | 296279.6 |
| 3-01 | 3 | 203828.0 | 178221.1 | 0.65 | 91663.5 | 336049.0 |
| 4-01 | 3 | 223114.3 | 136222.9 | 1.44 | 26786.0 | 415342.3 |
| Lead Concentration ( $\mu \mathrm{g} / \mathrm{g}$ ) |  |  |  |  |  |  |
| 1-01 | $\begin{gathered} 2 \\ (3) \end{gathered}$ | $\begin{gathered} 56582.26 \\ (38482.65) \\ \hline \end{gathered}$ | $\begin{gathered} 54952.43 \\ (19031.35) \\ \hline \end{gathered}$ | $\begin{array}{r} 0.34 \\ (1.85) \\ \hline \end{array}$ | $\begin{aligned} & 43098.31 \\ & (2282.63) \end{aligned}$ | $\begin{gathered} 70067.02 \\ (70067.02) \\ \hline \end{gathered}$ |
| 2-01 | 3 | 20689.59 | 18248.23 | 0.67 | 8458.91 | 27171.01 |
| 3-01 | 3 | 27467.15 | 22990.21 | 0.70 | 15303.16 | 51756.13 |
| 4-01 | 3 | 18535.23 | 17510.97 | 0.43 | 10623.19 | 23130.62 |

[^6]Table WR-6a. Descriptive Statistics (Across All Units) of Sample Weight, Lead Loadings, and Lead Concentrations Associated with Interior and Exterior Paint Chip Samples Collected Following Completion of Window Replacement

| Location | $\mathbf{N}$ | Arithmetic <br> Mean | Geometric <br> Mean | Log Std. <br> Dev. ${ }^{(1)}$ | Minimum <br> Value | Maximum <br> Value |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample Weights (g) ${ }^{(2)}$ |  |  |  |  |  |  |  |

${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
${ }^{(2)}$ Sample weights represent the weight of subsamples used in the chemical analysis. In several instances, two subsamples from the same chip were analyzed. In such cases, the results from the two subsamples were combined to form a single observation.
${ }^{(3)}$ An extra paint chip sample was collected at unit 2-01 from a window where no other samples were collected.

Table WR-6b. Descriptive Statistics (Within Each Unit) of Sample Weight, Lead Loadings, and Lead Concentrations Associated with Interior and Exterior Paint Chip Samples Collected Following Completion of Window Replacement

| Unit ID | Location | N | Arithmetic Mean | Geometric Mean | Log Std. Dev. ${ }^{(1)}$ | Minimum Value | Maximum Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Sample Weights (g) ${ }^{(2)}$ |  |  |  |  |  |  |  |
| 1-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 0.6687 \\ & 0.6765 \end{aligned}$ | $\begin{aligned} & 0.6319 \\ & 0.6396 \end{aligned}$ | $\begin{aligned} & 0.4002 \\ & 0.3979 \end{aligned}$ | $\begin{aligned} & 0.4951 \\ & 0.5073 \end{aligned}$ | $\begin{aligned} & 1.0028 \\ & 1.0127 \end{aligned}$ |
| 2-01 | Exterior <br> Interior | $\begin{gathered} 4^{(3)} \\ 3 \end{gathered}$ | $\begin{aligned} & 0.6291 \\ & 0.5089 \end{aligned}$ | $\begin{aligned} & 0.5978 \\ & 0.5089 \end{aligned}$ | $\begin{aligned} & 0.3504 \\ & 0.0153 \end{aligned}$ | $\begin{aligned} & 0.4964 \\ & 0.5021 \end{aligned}$ | $\begin{aligned} & 1.0110 \\ & 0.5174 \end{aligned}$ |
| 3-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 0.5025 \\ & 0.5052 \end{aligned}$ | $\begin{aligned} & 0.5025 \\ & 0.5052 \end{aligned}$ | $\begin{aligned} & 0.0062 \\ & 0.0062 \end{aligned}$ | $\begin{aligned} & 0.4998 \\ & 0.5016 \end{aligned}$ | $\begin{aligned} & 0.5059 \\ & 0.5072 \end{aligned}$ |
| 4-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 0.5154 \\ & 0.8434 \end{aligned}$ | $\begin{aligned} & 0.5154 \\ & 0.7989 \end{aligned}$ | $\begin{aligned} & 0.0193 \\ & 0.4233 \end{aligned}$ | $\begin{aligned} & 0.5040 \\ & 0.4901 \end{aligned}$ | $\begin{aligned} & 0.5212 \\ & 1.0327 \end{aligned}$ |
| Lead Loadings ( $\mathrm{mg} / \mathrm{cm}^{2}$ ) |  |  |  |  |  |  |  |
| 1-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{gathered} 9.63 \\ 5.897 \end{gathered}$ | $\begin{aligned} & 7.26 \\ & 4.75 \end{aligned}$ | $\begin{aligned} & 1.029 \\ & 0.901 \end{aligned}$ | $\begin{aligned} & 2.284 \\ & 1.6867 \end{aligned}$ | $\begin{array}{r} 16.422 \\ 8.619 \\ \hline \end{array}$ |
| 2-01 | Exterior <br> Interior | $\begin{gathered} 4^{(3)} \\ 3 \end{gathered}$ | $\begin{gathered} 36.948 \\ 0.057 \end{gathered}$ | $\begin{aligned} & 34.33 \\ & 0.055 \end{aligned}$ | $\begin{aligned} & 0.472 \\ & 0.336 \end{aligned}$ | $\begin{array}{r} 17.620 \\ 0.037 \end{array}$ | $\begin{array}{r} 49.651 \\ 0.068 \end{array}$ |
| 3-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 24.911 \\ & 8.368 \end{aligned}$ | $\begin{gathered} 23.991 \\ 8.339 \\ \hline \end{gathered}$ | $\begin{aligned} & 0.345 \\ & 0.103 \end{aligned}$ | $\begin{array}{r} 16.344 \\ 7.440 \\ \hline \end{array}$ | $\begin{array}{r} 31.917 \\ 9.089 \\ \hline \end{array}$ |
| 4-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{gathered} 5.314 \\ 12.976 \end{gathered}$ | $\begin{gathered} 2.436 \\ 10.566 \end{gathered}$ | $\begin{aligned} & 1.815 \\ & 0.815 \end{aligned}$ | $\begin{aligned} & 0.339 \\ & 4.573 \end{aligned}$ | $\begin{aligned} & 12.067 \\ & 23.270 \end{aligned}$ |
| Lead Concentrations (mg/g) |  |  |  |  |  |  |  |
| 1-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 127.11 \\ & 80.43 \end{aligned}$ | $\begin{aligned} & 94.86 \\ & 65.48 \end{aligned}$ | $\begin{aligned} & 1.078 \\ & 0.876 \end{aligned}$ | $\begin{aligned} & 27.41 \\ & 23.90 \end{aligned}$ | $\begin{aligned} & 189.91 \\ & 116.99 \end{aligned}$ |
| 2-01 | Exterior <br> Interior | $\begin{gathered} 4^{(3)} \\ 3 \end{gathered}$ | $\begin{gathered} 139.04 \\ 1.46 \end{gathered}$ | $\begin{gathered} 136.20 \\ 1.45 \\ \hline \end{gathered}$ | $\begin{aligned} & 0.243 \\ & 0.158 \end{aligned}$ | $\begin{gathered} 95.841 \\ 1.21 \\ \hline \end{gathered}$ | $\begin{gathered} 162.11 \\ 1.59 \end{gathered}$ |
| 3-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 196.66 \\ & 122.04 \end{aligned}$ | $\begin{aligned} & 194.83 \\ & 117.26 \end{aligned}$ | $\begin{aligned} & 0.169 \\ & 0.361 \end{aligned}$ | $\begin{gathered} 162.85 \\ 77.35 \end{gathered}$ | $\begin{aligned} & 227.52 \\ & 146.71 \end{aligned}$ |
| 4-01 | Exterior <br> Interior | $\begin{aligned} & 3 \\ & 3 \end{aligned}$ | $\begin{aligned} & 77.23 \\ & 126.71 \end{aligned}$ | $\begin{gathered} 44.44 \\ 117.48 \end{gathered}$ | $\begin{aligned} & 1.549 \\ & 0.480 \end{aligned}$ | $\begin{gathered} 7.71 \\ 72.88 \end{gathered}$ | $\begin{aligned} & 146.01 \\ & 190.33 \end{aligned}$ |

[^7]

Figure WR-1a. Boxplots of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) for Vacuum Dust Samples From the Floors and Window Wells Taken Prior to Window Replacement Activities


Figure WR-1b. Boxplots of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) for Vacuum Dust Samples From Floors and Window Wells Taken Prior to Window Replacement Activities


Figure WR-2a.
Boxplots of Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) for Vacuum Dust Samples From Floors and Stainless Steel Dustfall Collectors Taken One-Hour After Completion of the Window Replacement Activities


Figure WR-2b.
Boxplots of Lead Concentrations ( $\mu \mathrm{g} / \mathrm{g}$ ) for Vacuum Dust Samples From Floors and Stainless Steel Dustfall Collectors Taken One-Hour After Completion of the Window Replacement Activities


Figure WR-3. Boxplots of Lead Loadings ( $\mathrm{mg} / \mathrm{cm}^{2}$ ) for Paint Chip Samples Taken from the Interior and Exterior of the Window Frames After Completion of the Window Replacement Activities

## A. 3 DESCRIPTIVE STATISTICS OF DATA FROM THE CED PHASE

Table CED-1 presents descriptive statistics on lead levels from personal air monitoring of R\&R workers in the CED phase of the EFSS. Lead levels were expressed in terms of task-length averages (TLAs, or average exposure over the duration of activity, in $\mu \mathrm{g} / \mathrm{m}^{3}$ of air) for a given target activity and substrate on which the activity was performed. For each activity/substrate combination, Table CED-1 presents the number of monitoring results, the arithmetic and geometric means, the standard deviation of log-transformed data, and the minimum and maximum observed values. Because these data tended to be lognormally distributed, the geometric means are better indicators of central tendency within the data distributions than are the arithmetic means.

One objective of the CED phase was to study the relationship between lead disturbance generated by performing a target $R \& R$ activity and the distance from the activity at which lead loadings are being measured from settled dust samples. This relationship helps explain potential lead exposures associated with a given activity and was quantified through statistical modeling procedures. Exploratory analysis demonstrated that the relationship between settled dust lead loading and distance from activity was well approximated by the following linear model:

$$
\begin{equation*}
\log (\text { loading })=\bullet{ }_{0}+\bullet{ }_{1}(\text { Distance })+\text { Error } \tag{A-1}
\end{equation*}
$$

where ${ }^{0}{ }_{0}$ and $\bullet{ }_{1}$ are parameters which quantify the linear relationship. This model was fitted separately to data for each experimental unit, or for each combination of individual target activity applications within a study unit.

From the fitted regression lines determined through Model (A-1), estimates are obtained for three indicators of lead disturbance (these indicators are discussed further in Section C. 5 of Appendix C):

- lead disturbance within a 6'x1' gradient from the target activity;
- estimated lead loading in dust that settles from zero to one foot from the target activity; and
- estimated lead loading in dust that settles from five to six feet from the target activity.

For each model fitting, Table CED-2 presents these estimates, in addition to the estimates of ${ }_{0}{ }_{0}$ and - ${ }_{1}$ from the model. One row of Table CED-2 exists for each experimental unit.

A series of figures follow Table CED-2 which present predicted lead disturbance (in log units) as a function of distance from activity, as determined through statistical modeling results. Each figure contains a number of plots representing a particular target activity and substrate:

Figure CED-1: Drilling into wood;
Figure CED-2: Drilling into plaster;
Figure CED-3: Sawing into wood;
Figure CED-4: Sawing into plaster;
Figure CED-5: Wood door modification;
Figure CED-6: Sanding of painted wood;
Figure CED-7: HVAC ductwork removal;
Figure CED-8: Demolition.
The first plot in each figure contains prediction curves for each fit of Model (A-1) within this activity/substrate combination (as given by the dashed lines). Separate fits of the model were made for each occurrence of the activity/substrate in the study (i.e., each experimental unit), as indicated in Table CED-2. Also in this plot are prediction curves of single fits of the "population model" (solid line) and the "two-stage" model (thick-dashed line). Both models, explained in Section C. 4 of Appendix C, predict lead disturbance for the activity/substrate group across the entire CED phase. As both models give nearly equivalent predictions, the solid and thick-dashed lines are nearly plotted on top of each other.

Subsequent plots in Figures CED-1 to CED-8 illustrate the result of fitting model (A-1) to each experimental unit in the study by plotting the observed settled dust lead loadings (in the log domain) versus distance from activity, as well as the fitted prediction curve. These plots are identified by the building and room in which the activity was monitored.

Table CED-1. Summary Statistics for Task-Length Average Personal Worker Lead Levels $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right.$ ) During Each Combination of CED Activity and Substrate

| Task | \# Data <br> Points | Arithmetic <br> Mean | Geometric <br> Mean | Log Std Dev | Minimum <br> Value | Maximum <br> Value |
| :--- | ---: | ---: | ---: | ---: | ---: | ---: |
| Clean/Plaster | 4 | 27.701 | 24.461 | 0.5503 | 14.592 | 53.283 |
| Clean/Wood | 2 | 103.44 | 102.36 | 0.2050 | 88.549 | 118.33 |
| Demolition | 20 | 152.63 | 106.81 | 0.7406 | 33.553 | 947.06 |
| Door Modification/ <br> Wood | 6 | 819.93 | 486.45 | 1.1722 | 112.03 | 2280.4 |
| Drill/Plaster | 6 | 6.9075 | 6.2510 | 0.5181 | 2.6168 | 11.598 |
| Drill/Wood | 7 | 26.324 | 15.147 | 1.2947 | 3.3666 | 50.235 |
| HVAC Removal | 4 | 50.075 | 49.623 | 0.1571 | 40.381 | 58.310 |
| Component <br> Removal/Wood | 2 | 344.01 | 343.84 | 0.0451 | 333.05 | 354.97 |
| Abrasive Sanding | 9 | 544.82 | 332.75 | 1.0110 | 73.645 | 2311.7 |
| Saw/Plaster | 2 | 145.51 | 109.99 | 1.1080 | 50.245 | 240.77 |
| Saw/Wood | 6 | 581.85 | 545.84 | 0.3801 | 397.48 | 967.99 |

Table CED-2. Parameter Estimates $\mathrm{D}_{0}$ and $\mathrm{D}_{1}$ from Model (A-1) Predicting Dust Lead Loadings as a Function of Distance for Each Target Activity Execution

| Target Activity | Substrate | Experimental Units |  | Estimated Intercept | Estimated Slope | Standard Error $\mathrm{D}_{\text {Error }}$ | Estimated $6^{\prime} \times 1^{\prime}$ Pb Loading Gradient ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | Estimated [0-1] Foot SSDC Pb Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | Estimated [5-6] Foot SSDC Pb Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Housing Unit | Room Within Housing Unit |  |  |  |  |  |  |
| Drill | Wood | 1 | 1 | 10.380 | -1.1925 | 1.47741 | 26993.61 | 18816.75 | 48.43 |
|  |  | 1 | 2 | 11.955 | -1.4844 | 2.71843 | 104755.44 | 81025.60 | 48.44 |
|  |  | 1 | 3 | 13.469 | -1.7255 | 1.18628 | 410006.67 | 337003.16 | 60.36 |
|  |  | 2 | 1 | 13.813 | -1.7086 | 0.91359 | 583773.22 | 478061.49 | 93.16 |
|  |  | 2 | 2 | 14.154 | -1.6607 | 1.43482 | 844857.25 | 684354.03 | 169.52 |
|  |  | 3 | 1 | 13.275 | -1.3747 | 2.01080 | 423647.21 | 316579.67 | 327.67 |
|  |  | 3 | 2 | 13.400 | -1.2554 | 1.13787 | 525651.40 | 376064.36 | 706.58 |
|  | Plaster | 1 | 1 | 7.5953 | -1.3107 | 0.77360 | 1516.75 | 1108.23 | 1.58 |
|  |  | 1 | 2 | 10.507 | -1.3807 | 1.48990 | 26488.24 | 19833.98 | 19.92 |
|  |  | 2 | 1 | 11.242 | -1.3615 | 0.64877 | 55979.71 | 41645.92 | 46.03 |
|  |  | 2 | 2 | 13.041 | -2.8209 | 0.78250 | 163361.07 | 153632.09 | 0.12 |
| Saw | Wood | 1 | 1 | 13.297 | -. 75521 | 0.86596 | 780165.95 | 418058.28 | 9578.93 |
|  |  | 1 | 2 | 12.949 | -. 70625 | 1.27843 | 586669.04 | 301508.19 | 8824.58 |
|  |  | 2 | 1 | 12.750 | -. 78775 | 0.38276 | 433427.74 | 238386.68 | 4642.06 |
|  |  | 2 | 2 | 12.420 | -. 96080 | 1.54356 | 256929.19 | 159130.84 | 1304.36 |
|  |  | 3 | 1 | 13.870 | -. 68145 | 0.46151 | 1523083.13 | 765410.31 | 25359.74 |
|  |  | 3 | 2 | 10.500 | -. 11757 | 1.70431 | 156279.63 | 34251.88 | 19027.54 |
|  | Plaster | 1 | 1 | 10.035 | -. 80017 | 1.01382 | 28280.92 | 15704.81 | 287.39 |
|  |  | 2 | 1 | 12.536 | -1.0822 | 2.10227 | 256606.54 | 169909.58 | 759.16 |

Table CED-2. (Continued)

| Target Activity | Substrate | Experimental Units |  | Estimated Intercept | Estimated Slope | Standard <br> Error <br> $\mathrm{D}_{\text {Error }}$ | Estimated $6^{\prime} \times 1^{\prime}$ <br> Pb Loading Gradient ( $\mu \mathrm{g} / \mathrm{ft} \mathrm{t}^{2}$ ) | Estimated [0-1] Foot SSDC Pb Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | Estimated <br> [5-6] Foot SSDC <br> Pb Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Housing Unit | Within Housing Unit |  |  |  |  |  |  |
| Door | Wood | 1 | 1 | 9.2792 | -. 21432 | 0.67524 | 36170.83 | 9642.98 | 3302.36 |
|  |  | 1 | 2 | 10.518 | -. 28567 | 1.17483 | 106102.69 | 32158.29 | 7708.57 |
|  |  | 2 | 1 | 10.273 | -. 21935 | 1.47167 | 96601.78 | 25998.98 | 8682.52 |
|  |  | 2 | 2 | 9.5765 | -. 38191 | 0.97219 | 33944.39 | 11987.57 | 1775.94 |
|  |  | 3 | 1 | 13.183 | -. 63441 | 0.41639 | 818758.77 | 393356.02 | 16488.61 |
|  |  | 3 | 2 | 13.924 | -. 79357 | 0.68776 | 1392338.34 | 769266.98 | 14549.66 |
| Sand | Wood | 1 | 1 | 10.842 | -. 40035 | 1.59203 | 116164.82 | 42139.05 | 5693.01 |
|  |  | 2 | 1 | 13.090 | -. 32664 | 0.72129 | 1273125.24 | 412936.95 | 80650.04 |
|  |  | 3 | 1 | 10.797 | -. 32348 | 0.70356 | 129339.09 | 41738.87 | 8281.43 |
| HVAC | Duct | 1 | 1 | 10.255 | -. 56498 | 1.55988 | 48612.03 | 21714.48 | 1287.96 |
|  |  | 2 | 1 | 5.6465 | -. 13735 | 0.27278 | 1157.86 | 264.70 | 133.20 |
| Demolition | Plaster | 1 | 1 | 7.1450 | -. 10665 | 0.23008 | 5618.30 | 1202.44 | 705.48 |
|  |  | 1 | 2 | 7.3677 | -. 24732 | 0.63808 | 4952.48 | 1403.33 | 407.49 |
|  |  | 2 | 1 | 8.5595 | -. 24404 | 0.37631 | 16430.70 | 4628.28 | 1366.13 |
|  |  | 2 | 2 | 7.4882 | -. 11647 | 0.33018 | 7713.99 | 1686.67 | 942.13 |
|  |  | 3 | 1 | 13.494 | -. 59585 | 1.56133 | 1182861.30 | 546294.38 | 27769.24 |
|  |  | 3 | 2 | 10.291 | -. 17133 | 1.59569 | 110443.37 | 27075.59 | 11496.07 |
|  |  | 3 | 3 | 6.7415 | -. 43914 | 1.24668 | 1790.13 | 685.39 | 76.27 |
|  | Wood/Plaster | 1 | 1 | 6.5466 | 0.10274 | 1.01864 | 5781.13 | 733.92 | 1226.72 |
|  |  | 2 | 1 | 15.326 | -1.0641 | 1.06563 | 4249824.23 | 2788243.68 | 13632.21 |

Target Activity $=$ Drill Substrate $=$ Wood


Figure CED-1.


Figure CED-1. (Continued)


Figure CED-1. (Continued)

Target Activity = Drill Substrate = Plaster


Figure CED-2.


Figure CED-2. (Continued)

Target Activity=Saw Substrate=Wood


Figure CED-3.


Figure CED-3. (Continued)


Figure CED-3. (Continued)

Target Activity=Saw Substrate=Plaster


Figure CED-4.


Target Activity $=$ Saw Substrate $=$ Plaster Unit $=$ Baltimore(2) Room $=1$


Figure CED-4. (Continued)

Target Activity=Door Substrate=Wood


Figure CED-5.


Figure CED-5. (Continued)


Figure CED-5. (Continued)

Target Activity=Sand Substrate=Wood


Figure CED-6.


Figure CED-6. (Continued)

Target Activity = HVAC Substrate = Duct


Figure CED-7.


Target Activity $=$ HVAC Substrate $=$ Duct Unit $=$ Baltimore(2) Room $=1$


Figure CED-7. (Continued)

Target Activity = Demolition Substrate = Plaster


Figure CED-8.


Figure CED-8. (Continued)


Target Activity $=$ Demolition Substrate $=$ Plaster Unit $=$ Denver Room $=2$


Figure CED-8. (Continued)

Target Activity $=$ Demolition Substrate $=$ Wood/Plaster Unit $=$ Baltimore(1) Room $=1$ Target Activity $=$ Demolition Substrate $=$ Wood/Plaster Unit $=$ Baltimore(2) Room $=1$



Figure CED-8. (Continued)

## A. 4 DESCRIPTIVE STATISTICS OF DATA FROM THE CLEANUP INVESTIGATION

Section 7D presents design and results of an investigation of the effects of cleanup procedures on lead levels in settled dust that remain for occupants to encounter. For each combination of R\&R activity and cleanup method, the following tables describe the collected data:

Table CI-1: Lead loadings in paint chip samples taken from surfaces disturbed by R\&R activity

Table CI-2: Lead loadings in post-activity settled dust samples taken prior to cleanup
Table CI-3: Lead loadings in post-cleanup settled dust samples

Table CI-4: Lead loadings in next-day SSDC vacuum-dust samples.

Table CI-1. Descriptive Statistics for Measured Lead Loadings ( $\mathrm{mg} / \mathrm{cm}^{2}$ ) in Paint Chip Samples Taken from Surfaces Disturbed by R\&R Activity in the Cleanup Investigation

| R\&R <br> Activity | Cleanup <br> Method | $\mathbf{N}^{(1)}$ | Arithmetic <br> Mean | Geometric <br> Mean | Log <br> Std. Dev. | Minimum | Maximum |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Drilling | Broom | 3 | 1.77 | 0.32 | 2.42 | 0.08 | 5.15 |
| Drilling | Vacuum | 3 | 4.72 | 1.31 | 2.86 | 0.05 | 9.17 |
| Abrasive <br> Sanding | Broom | 3 | 7.19 | 1.91 | 2.97 | 0.06 | 12.60 |
| Abrasive <br> Sanding | Vacuum | 3 | 14.27 | 14.17 | 0.14 | 12.17 | 15.84 |

${ }^{(1)}$ One result exists for each experimental unit (i.e., each time the activity/cleanup method combination was performed).

Table CI-2. Descriptive Statistics for Measured Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) in PostActivity Settled Dust Samples Taken Prior to Cleanup in the Cleanup Investigation

| R\&R <br> Activity | Cleanup Method | Distanc e from Activity (ft.) | $\mathbf{N}^{(1)}$ | Arithmetic Mean | Geometric Mean | Log Std. Dev. | Min. | Max. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Drilling | Broom | 0 | 3 | 141773 | 26739 | 2.38 | 5332 | 411270 |
|  |  | 3 | 3 | 425 | 176 | 1.93 | 22.3 | 1013 |
|  |  | 6 | 3 | 203 | 65 | 2.60 | 3.3 | 392 |
| Drilling | Vacuum | 0 | 3 | 253005 | 73508 | 2.81 | 2869 | 444986 |
|  |  | 3 | 3 | 471 | 312 | 1.08 | 144 | 1074 |
|  |  | 6 | 3 | 287 | 146 | 1.83 | 17.7 | 463 |
| Abrasive Sanding | Broom | 0 | 3 | 3021341 | 653201 | 3.34 | 13831 | 5096250 |
|  |  | 3 | 3 | 3177 | 715 | 2.26 | 121 | 9075 |
|  |  | 6 | 3 | 17405 | 1376 | 3.71 | 30.6 | 50500 |
| Abrasive Sanding | Vacuum | 0 | 3 | 371105 | 202540 | 1.60 | 34421 | 762190 |
|  |  | 3 | 3 | 8443 | 5277 | 1.37 | 1150 | 16374 |
|  |  | 6 | 3 | 796 | 491 | 1.43 | 96.9 | 1452 |

${ }^{(1)}$ One result exists for each experimental unit (i.e., each time the activity/cleanup method combination was performed).

Table CI-3. Descriptive Statistics for Measured Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) in PostCleanup Settled Dust Samples Taken in the Cleanup Investigation

| R\&R Activity | Cleanup Method | Distanc e from Activity <br> (ft.) | $\mathrm{N}^{(1)}$ | Arithmetic Mean | Geometric Mean | Log <br> Std. <br> Dev. | Min. | Max. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LEAD LOADINGS IN DUST-VACUUM SAMPLES |  |  |  |  |  |  |  |  |
| Drilling | Broom | 0 | 3 | 93 | 42 | 1.79 | 6.2 | 219 |
|  |  | 3 | 6 | 66 | 24 | 1.72 | 3.3 | 256 |
|  |  | 6 | 3 | 22 | 12 | 1.40 | 3.3 | 53 |
| Drilling | Vacuum | 0 | 3 | 217 | 52 | 2.52 | 3.8 | 582 |
|  |  | 3 | 6 | 89 | 40 | 1.52 | 4.5 | 318 |
|  |  | 6 | 3 | 40 | 27 | 1.13 | 9.0 | 85 |
| Abrasive Sanding | Broom | 0 | 3 | 3941 | 235 | 3.53 | 12 | 11720 |
|  |  | 3 | 6 | 2936 | 232 | 2.29 | 33 | 16918 |
|  |  | 6 | 3 | 1794 | 336 | 2.38 | 82 | 5212 |
| Abrasive Sanding | Vacuum | 0 | 3 | 3731 | 388 | 2.92 | 53 | 11041 |
|  |  | 3 | 6 | 114 | 62 | 1.32 | 7.6 | 373 |
|  |  | 6 | 3 | 306 | 161 | 1.36 | 65 | 769 |
| LEAD LOADINGS IN DUST-WIPE SAMPLES |  |  |  |  |  |  |  |  |
| Drilling | Broom | 0 | 3 | 266 | 166 | 1.27 | 46 | 579 |
|  |  | 6 | 3 | 202 | 124 | 1.33 | 30 | 427 |
| Drilling | Vacuum | 0 | 3 | 805 | 360 | 1.84 | 50 | 1857 |
|  |  | 6 | 3 | 166 | 123 | 1.03 | 41 | 312 |
| Abrasive Sanding | Broom | 0 | 3 | 2995 | 1074 | 1.80 | 255 | 8131 |
|  |  | 6 | 3 | 2830 | 829 | 2.04 | 149 | 7854 |
| Abrasive Sanding | Vacuum | 0 | 3 | 905 | 808 | 0.60 | 425 | 1402 |
|  |  | 6 | 3 | 432 | 303 | 1.07 | 108 | 904 |

${ }^{(1)}$ At zero and six feet from activity, one result exists for each experimental unit (i.e., each time the activity/cleanup method combination was performed). At three feet from activity, two dust-vacuum results and one dust-wipe result exist for each experimental unit.

Table CI-4. Descriptive Statistics for Measured Lead Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) in Next-Day SSDC Vacuum-Dust Samples Taken in the Cleanup Investigation

| R\&R <br> Activity | Cleanup Method | Distanc e from Activity (ft.) | $\mathbf{N}^{(1)}$ | Arithmetic Mean | Geometric Mean | Log <br> Std. <br> Dev. | Min. | Max. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Drilling | Broom | 0 | 3 | 92 | 57 | 1.16 | 25 | 216 |
|  |  | 6 | 2 | 48 | 46 | 0.47 | 33 | 64 |
| Drilling | Vacuum | 0 | 3 | 119 | 95 | 0.79 | 53 | 234 |
|  |  | 6 | 3 | 42 | 40 | 0.37 | 31 | 61 |
| Abrasive <br> Sanding | Broom | 0 | 3 | 79 | 60 | 0.99 | 20 | 138 |
|  |  | 6 | 3 | 261 | 155 | 1.33 | 41 | 588 |
| Abrasive Sanding | Vacuum | 0 | 3 | 28 | 27 | 0.34 | 19 | 36 |
|  |  | 6 | 3 | 13 | 12 | 0.60 | 5.9 | 17 |

${ }^{(1)}$ One result exists for each experimental unit (i.e., each time the activity/cleanup method combination was performed). For drilling/broom cleanup, results for only two experimental units were available.

APPENDIX B
DATA PROCESSING AND OUTLIER DETECTION

## B. 0 DATA PROCESSING AND OUTLIER DETECTION

## B. 1 DATA PROCESSING

The following subsections discuss how the requirements for data processing were met in the EFSS. Specifically, these discussions address data storage, data transfer, data tracking, database verification, and necessary data manipulations prior to the statistical analysis.

## B.1.1 Data Storage, Transfer, and Tracking

All requirements concerning the storage, tracking, and transfer of the study data were followed in the EFSS as specified in the Quality Assurance Project Plan (QAPjP). Within several overnight shipments, MRI provided Battelle with the analytical study data in hard-copy listings and on diskette in Lotus spreadsheet format. These listings represented results for specific analytical batches. Battelle has stored the original data listings and diskettes in a locked file cabinet, along with the original completed field data logs for which Battelle is responsible. Battelle has made backup diskettes of the data spreadsheet files; these backups are currently stored in the office of the database manager. The study database created by Battelle from the MRI data files is stored on the hard disk of the database manager, and relevant data for statistical summary and analysis are located on a network hard disk accessible by Battelle statisticians.

Battelle was responsible for entering data from the field sample logs into the study database. After verifying the accuracy of the data entry (Section B.1.2), Battelle merged these data with the analytical data sent by MRI in creating the study database.

Data tracking has been done in accordance with the QAPjP. All dates corresponding to significant events in the collection, laboratory analysis, and transfer of the data are recorded in the Battelle study database. Tracking programs confirmed that all data corresponding to collected field samples and laboratory samples were included in the study database.

## B.1.2 Data Verification

Prior to entering data into the study database, Battelle verified the correctness and accuracy of study data in the following ways:

- Battelle staff hand-entered data from the field sampling logs, using double data entry techniques and hand-checking to ensure that accurate data were entered.
- When a batch of analytical data was received from MRI, Battelle compared the submitted hard-copy data listings with listings made of the contents of the Lotus spreadsheets. This verification procedure included spot-checking of calculations.
- Information used to identify the records in the electronic database were compared with similar information from the sample field logs, to verify overall data consistency.

Battelle staff members reviewed any discrepancies found in the data verification procedure, making any necessary corrections to the database as a result. In this review, Battelle notified MRI of any data issues that needed to be brought to their attention.

## B.1.3 Data Manipulation

The QAPjP for the EFSS notes that data values for variables to be included in the statistical analysis may need to be transformed based on their underlying distributional forms. Statistical analyses and/or data summary were performed on three data variables: physical sample weight, lead concentration, and lead loadings. Battelle statisticians examined the distribution of these variables and concluded that within each study phase, statistical analyses were more appropriately applied to the log-transformed data values. The data transformation issue is further discussed in Section 5.2.

## B. 2 OUTLIER DETECTION

Outliers are loosely defined as data values which do not coincide with preconceived assumptions on the data distribution for the given parameter. The assumptions are usually functions of the observed distribution of the parameter data, given the underlying distribution has some known form (e.g., lognormality). When data values are identified as outliers, they are generally reviewed for accuracy, and any erroneous data are corrected or are omitted from statistical analyses. Numerous outliers can imply that the assumptions on the data distribution are not appropriate, and special care should be taken in applying appropriate methodologies in the statistical analyses.

In each phase of the R\&R study, outlier analyses were conducted using three methods:

- logic checks,
- formal statistical tests, and
- graphical review.

The outlier analyses were applied to sample weight, lead concentration, and lead loading data. The above methods flagged data values for individual samples, as well as pairs of samples (i.e., samples taken from adjoining areas and having results with some expected intrinsic relationship) whose results were inconsistent in some way. The findings of the outlier analyses are presented below for each study phase.

## B.2.1 Logic Checks

As a first step in the outlier detection process, logic checks were performed to flag results which ran contrary to intuition or some underlying criterion. One check flagged those individual sample results having non-positive lead loadings. Within each phase, no results were flagged for this reason. Another set of checks within the window replacement and carpet removal phases flagged sample pairs in the following way:

- One hour/two hour settled dust sample pairs: Flag those pairs where a stainless steel dustfall collector (SSDC) sample collected two hours following the activity had a lower lead loading than the adjoining SSDC sample collected one hour following the activity.
- Pre-activity/post-activity floor dust sample pairs: Flag those pairs where a floor dust sample collected post-activity had a lower lead loading than the adjoining floor dust sample collected prior to start of the activity.

Note that only lead loadings were included in the above two types of logic checks. Lead concentrations were not considered, as it is possible that $R \& R$ activity could result in either higher or lower lead concentrations in settled dust over time, according to how dust is distributed as a result of the activity.

## Results

Table B-1 contains a list of sample pairs which failed one of the two logic checks in the carpet removal phase. In this phase, five of the 24 pre-/post-activity sample pairs resulted in a higher sample lead loading for the pre-activity sample than for the post-activity sample. Two of these five samples had the post-activity sample loading decrease by more than $50 \%$. It is suspected that these five results are due to normal spatial variability, as the field sample logs revealed no unusual circumstances with sample collection for these pairs.

Seven of the 24 one-/two-hour post-activity sample pairs in the carpet removal phase resulted in a higher sample lead loading for the one-hour sample than for the two-hour sample. Of these seven samples, five had the one-hour sample location closer to the activity than the adjoining two-hour sample location. This finding supports the notion that these violations to the logic checks may be the result of spatial variability. The largest deviation between one- and twohour results was found with a sample pair from unit 2-01, where the one-hour result (216.0 $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) was nearly ten times larger than the two-hour result ( $23.0 \mu \mathrm{~g} / \mathrm{ft}^{2}$ ). This deviation was nearly five times greater than the next largest deviation and therefore was considered a candidate for review.

Table B-1 also contains a list of sample pairs which failed one of the two logic checks in the window replacement phase. None of the four one-/two-hour post-activity SSDC sample pairs resulted in a higher sample lead loading for the one-hour sample than for the two-hour sample. However, 9 of the 34 pre-/post-activity sample pairs resulted in a higher sample lead loading for the pre-activity sample than for the post-activity sample. Of these, the two samples with the largest negative difference were reported to MRI for further investigation but no problem was
uncovered in the laboratory analysis. These sample pairs were both taken from unit 4-01. It is suspected that all other results are due to normal spatial variability, as the field sample logs revealed no unusually circumstances with sample collection for these pairs.

Table B-1. Sample Pairs in the Carpet Removal and Window Replacement Phases Whose Lead Loadings Were Flagged by Logic Checks

1. Pre-Activity/Post-Activity Floor Dust Sample Pairs: Pre-activity lead loading larger than post-activity lead loading

| Unit ID | Location | Distance from Activity | Pre-Activity Sample |  | Post-Activity Sample |  | (Post-activity result) - (preactivity result) | Ratio of Pre-activity to postactivity results |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | $\begin{gathered} \text { Sample } \\ \text { ID } \\ \hline \hline \end{gathered}$ | Lead Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | $\begin{gathered} \text { Sample } \\ \text { ID } \\ \hline \hline \end{gathered}$ | Lead Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |  |  |
| Carpet Removal Phase |  |  |  |  |  |  |  |  |
| 1-02 | Hall (L2) |  | 60058 | 18.78 | 60056 | 16.69 | -2.09 | 0.89 |
| 2-01 | Hall (L2) |  | 62091 | 226.0 | 62031 | 54.87 | -171.1 | 0.24 |
| 2-03 | Kitchen (L1) |  | 60411 | 35.04 | 62221 | 30.92 | -4.12 | 0.88 |
| 2-05 | Foyer (L1) |  | 60701 | 267.7 | 60691 | 125.8 | -141.9 | 0.47 |
| 2-05 | Kitchen (L3) |  | 60746 | 447.5 | 60796 | 252.4 | -195.2 | 0.56 |
| Window Replacement Phase |  |  |  |  |  |  |  |  |
| 2-01 | 1 (BED2) | 6 | 60482 | 51.46 | 60332 | 50.97 | -0.49 | 0.99 |
| 2-01 | 2 (BED2) | 3 | 60477 | 157.95 | 60432 | 107.62 | -50.33 | 0.68 |
| 2-01 | 1 (HAL) | 0 | 60487 | 28.39 | 60362 | 19.0 | -9.39 | 0.67 |
| 2-01 | 1 (HAL) | 6 | 60522 | 50.60 | 60402 | 30.42 | -20.18 | 0.60 |
| 3-01 | 1 | 3 | 60302 | 11027.00 | 60577 | 10429.00 | -598.00 | 0.95 |
| 3-01 | 10 | 6 | 60612 | 3703.20 | 60322 | 3162.90 | -540.30 | 0.85 |
| 4-01 | 13 (BED1) | 0 | 60494 | 439845.0 | 60504 | 85685.11 | -354159.89 | 0.19 |
| 4-01 | 13 (BED1) | 3 | 60569 | 29402.00 | 60424 | 10342.00 | -19060.00 | 0.35 |
| 4-01 | 17(LVG1) | 0 | 60559 | 145420.0 | 60439 | 38826.0 | -106594.00 | 0.27 |

2. One-hour/Two-hour Post-Activity SSDC Sample Pairs:

One-hour lead loading larger than two-hour lead loading

| Unit ID | Location | 1-hr. Post-Activity Sample |  | 2-hr. Post-Activity Sample |  | $\begin{gathered} \text { (1-hr. } \\ \text { result) - } \\ \text { (2-hr. } \\ \text { result) } \end{gathered}$ | Ratio of 1 hr. to 2-hr. results |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Sample ID | Lead Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | Sample ID | Lead Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |  |  |
| Carpet Removal Phase |  |  |  |  |  |  |  |
| 1-01 | Bathroom (L2) | 60017 | 205.7 | 60006 | 163.2 | -42.5 | 0.79 |
| 1-01 | Kitchen (L3) | 60010 | 92.61 | 60002 | 59.94 | -32.7 | 0.65 |
| 1-02 | Hall (L3) | 60064 | 36.50 | 60070 | 22.39 | -14.1 | 0.61 |
| 1-02 | Hall (L1) | 60061 | 14.37 | 60054 | 12.89 | -1.48 | 0.90 |
| 1-03 | Kitchen (L3) | 60101 | 13.35 | 60099 | 10.61 | -2.74 | 0.79 |


| $2-01$ | Hall (L2) | 62006 | 216.0 | 62116 | 23.00 | -193.0 | 0.11 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $2-05$ | Foyer (L1) | 60771 | 6.78 | 60751 | 5.95 | -0.83 | 0.88 |

## B.2.2 Formal Statistical Tests

The primary statistical approach to outlier detection was the fitting of simple linear models to estimate how individual data points deviate from the central tendency of the observed data distribution. While the specific methods differed across the three study phases, this basic approach was taken in each phase.

## Methodology

In the carpet removal phase, the following analysis of variance model was fitted to the $\log$-transformed data $\mathrm{Y}_{\mathrm{i}}(\mathrm{i}=1, \ldots, \mathrm{n})$ :

$$
\begin{equation*}
Y_{i} \quad \mu \quad i, \tag{B-1}
\end{equation*}
$$

where $\mu$ represents an overall mean value and $\cdot{ }_{i}$ represents deviation from the mean. For each model fit, the absolute value of each studentized residual was compared to the upper (1-- /2n)*100 percentile of the Student-t distribution, where n is the number of residuals and • is the overall significance level. Those observations whose studentized residuals exceeded this percentile (in absolute value) were declared outliers at the - level. This test takes a Bonferroni approach, implying that the overall error rate in falsely identifying an observation as an outlier is no higher than • .

In the window replacement phase, the Grubbs outlier test was used. In the Grubbs test, the most extreme of the log-transformed data (maximum or minimum) was subtracted from the mean value, and the corresponding absolute difference was divided by the standard deviation of the log-transformed data. If the absolute value of this statistic exceeded the critical value tabulated in Grubbs (1950), the data point was declared an outlier. This procedure yields similar results to the method used in the carpet removal phase.

In the CED phase, the Grubbs test was applied to the residuals in some modelled relationship. The primary step in the outlier detection process consisted of flagging data points that differ statistically from some underlying statistical relationship with a series of covariates. Two models from Section C. 4 of Appendix C were considered in this outlier test according to the type of data considered: Model (CED-1) for personal air lead concentrations, and Model (CED3) for SSDC sample lead loadings. The minimum and maximum residuals (divided by their standard error) from the model fit were compared against critical values tabulated by Grubbs (1950). A data point was flagged as an outlier if its residual exceeded the critical values at either the $\cdot=0.05$ or 0.10 level.

Each formal outlier test was run at the 0.05 and 0.10 significance levels. Significance at a lower • level denotes a more severe outlier.

## Carpet Removal Phase Results

In the carpet removal phase, the study data were partitioned into several data classifications, and Model (B-1) was fitted separately to data within each classification. These classifications and their associated samples sizes are as follows:

Vacuum samples (for sample weight, loading, and concentration):

- Regular pre-activity floor dust samples ( $\mathrm{n}=40$ );
- QC (side-by-side) pre-activity floor dust samples ( $\mathrm{n}=8$ );
- Pre-activity carpet dust samples ( $\mathrm{n}=24$ );
- Regular 1-hr. post-activity samples ( $\mathrm{n}=64$ );
- Regular 2-hr. post-activity samples ( $\mathrm{n}=24$ );
- QC (side-by-side) 1-hr. post-activity samples ( $\mathrm{n}=16$ );
- QC (side-by-side) 2-hr. post-activity samples ( $\mathrm{n}=8$ ).

Vacuum samples (for sample weight and concentration only):

- Field blanks ( $\mathrm{n}=8$ for sample weight, $\mathrm{n}=7$ for concentration).


## Wipe samples (for sample loading):

- Regular 1-hr. post-activity samples ( $\mathrm{n}=16$ );
- QC (side-by-side) 1-hr. post-activity samples ( $\mathrm{n}=8$ ).


## Air samples (for sample loading):

- Pre-activity ambient air samples ( $\mathrm{n}=8$ );
- During-activity ambient air samples ( $\mathrm{n}=16$ );
- During-activity personal air samples ( $\mathrm{n}=14$ ).

Table B-2 indicates that only one data point was flagged as an outlier at the $\bullet=0.10$ level: the lead concentration in a 2-hour post-activity vacuum sample taken from a stainless steel dustfall collector at unit 1-04. Its value of $29,867 \mu \mathrm{~g} / \mathrm{g}$ was over four times higher than the next largest lead concentration among the 2 -hour samples. In addition, four data points were declared outliers at the $\cdot=0.20$ level:

- The vacuum field blank taken at unit 1-02 had a lead concentration of $173.2 \mu \mathrm{~g} / \mathrm{g}$, compared to a range of $509-1376 \mu \mathrm{~g} / \mathrm{g}$ among the other seven vacuum field blanks in the study.
- The ambient air sample taken during the activity in unit 1-04 was $13.38 \mu \mathrm{~g} / \mathrm{m}^{3}$, while the highest reading among the other units was $5.36 \mu \mathrm{~g} / \mathrm{m}^{3}$. The pre-activity (baseline) ambient air sample result for this unit was not larger than that for the other units.

However, the two personal air sample results for this unit were the highest in the study, both falling above the OSHA worker action level of $30 \mu \mathrm{~g} / \mathrm{m}^{3}$.

Table B-2. Data Values in the Carpet Removal Phase Identified as Outliers by Formal Statistical Tests

| $\begin{aligned} & \text { Unit } \\ & \text { ID } \end{aligned}$ | Instr. <br> Batch | Sample Prep Batch | $\begin{gathered} \text { Sample } \\ \text { ID } \end{gathered}$ | Sample Medium | Sample Type | Location | Parameter | Sample value | Level | Hi/Lo |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-02 | E10193A | 602 | 60089 | Vacuum | Field blank | --- | Lead conc. | $173.2 \mu \mathrm{~g} / \mathrm{g}$ | 0.20 | Low |
| 1-04 | V11013A | 605 | 60106 | Ambient air | During activity | Bedroom \#3 | Sample loading | $13.38 \mu \mathrm{~g} / \mathrm{m}^{3}$ | 0.20 | High |
| 1-04 | E10213A | 604 | 60143 | Vacuum | 2-hr postactivity (SSDC) | Bathroom \#1 <br> (L1) | Lead conc. | 29867 Hg/g | 0.10 | High |
| 2-01 | E10213A | 604 | 62011 | Vacuum | 1-hr postactivity (SSDC) QC side-byside samples only) | Hall (L3) | Sample weight | 0.0009 g | 0.20 | Low |
| 2-01 | E11303A | 607 | 60991 | Vacuum | 1-hr postactivity (window sill) | Bedroom \#1 | Lead conc. | $66776 \mu \mathrm{~g} / \mathrm{g}$ | 0.20 | High |

- The sample weight for a one-hour post-activity QC side-by-side sample, taken from a stainless steel dustfall collector in unit 2-01, where the weight of 0.0009 g fell below the next lowest weight of 0.0058 g among these QC side-by-side samples.
- A lead concentration of $66,776 \mu \mathrm{~g} / \mathrm{g}$ for a one-hour post-activity vacuum sample from a window sill, compared to a range of $71.86-23,687 \mu \mathrm{~g} / \mathrm{g}$ for the other postactivity window sill dust samples.

The field sample logs indicated no special citations which would indicate why these samples had unusually low or high results, and MRI reported no problems in the laboratory analysis after further investigation. Thus, they were included in the statistical analysis.

## Window Replacement Phase Results

Outliers detected in the formal statistical tests on window replacement data are presented in Table B-3. As in the carpet removal phase, the study data were initially partitioned into several data classifications. Grubbs test was run separately on data within each classification. These classifications and their associated sample sizes were as follows:

Table B-3. Data Values in the Window Replacement Phase Identified as Outliers by Formal Statistical Tests

| Unit ID | Instr. <br> Batch | Samp. <br> Prep. <br> Batch | Sample <br> ID | Sample <br> Medium | Sample <br> Type | Parameter | Sample <br> Value | Level | Hi/Lo |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $1-01$ | E11153A | 614 | 60230 | Vacuum | Window Well | Loading <br> Lead Conc. | 2311.65 <br> 2282.63 | 0.10 <br> 0.05 | Low |
| $4-01$ | E02104A | 620 | 60359 | Paint chip | Exterior | Loading <br> Lead Conc. | 7.711 <br> 7.711 | 0.05 <br> 0.05 | Low |
| $1-01$ | E11173A | 616 | 60257 | Paint chip | Exterior | Lead Conc. | 27.409 | 0.05 | Low |
| $1-01$ | E11153A | 614 | 60237 | Vacuum | Pre-activity <br> floor at 3 feet | Sample <br> Weight | 0.0055 | 0.10 | Low |

Vacuum floor dust samples (for sample weight, loading, and concentration):

- Regular pre-activity samples at 0 feet ( $\mathrm{n}=12$ );
- Regular pre-activity samples at 3 feet ( $\mathrm{n}=12$ );
- Regular pre-activity samples at 6 feet including QC (side-by-side) samples ( $\mathrm{n}=16$ );
- Regular 1-hr. post-activity samples at 0 feet ( $\mathrm{n}=12$ );
- Regular 1-hr. post-activity samples at 3 feet ( $\mathrm{n}=12$ );
- Regular 1-hr. post-activity samples at 6 feet including QC (side-by-side) samples ( $\mathrm{n}=16$ );

Vacuum Stainless Steel Dust Collector (SSDC) samples (for sample weight, loading, and concentration):

- Regular 1-hr. post-activity samples at 0 feet ( $\mathrm{n}=12$ );
- Regular 1-hr. post-activity samples at 6 feet including QC (side-by-side) samples ( $\mathrm{n}=16$ );
- Regular 2-hr. post-activity samples at 6 feet $(\mathrm{n}=4)$;

Vacuum Window Well dust samples (for sample weight, loading, and concentration):

- Pre-activity window well samples ( $\mathrm{n}=12$ );

Vacuum samples (for sample weight and concentration only):

- Field blanks ( $\mathrm{n}=8$ for sample weight, $\mathrm{n}=7$ for concentration).


## Paint chip samples (for sample weight, loading, and concentration):

- Interior ( $\mathrm{n}=12$ );
- Exterior ( $\mathrm{n}=12$ );

Air samples (for sample loading):

- Pre-activity ambient air samples ( $\mathrm{n}=4$ );
- During-activity ambient air samples $(\mathrm{n}=8)$;
- During-activity personal air samples ( $\mathrm{n}=8$ ).

Table B-3 presents those window replacement data that were identified as outliers by the formal statistical test. Only three samples were flagged as outliers at the $\bullet=0.05$ level: the lead concentration for a window well sample taken at unit 1-01, the lead loading and concentration for an exterior paint chip sample taken at unit 4-01, and the lead concentration for an exterior paint chip sample at unit 1-01. In addition, one data point was declared an outlier at the $\cdot=0.10$ level: the sample weight for a pre-activity 3-foot floor dust sample taken at unit 1-01.

The field sample logs indicated no special citations which would indicate why these samples had unusually extreme results. These results were reported to MRI for further investigation. For the window well sample, MRI reported the presence of insects in the sample; for the two paint chip samples, MRI reported substrate in the sample.

## CED Phase Results

Outliers detected in the formal statistical tests are presented in Table B-4. Three data points were identified as outliers relative to the fitted model, two of which were associated with demolition activities. No indication was given from the field sample logs as to why these three results may have been unusual. Also, these data points were not identified in other outlier procedures, and MRI reported no problems with the laboratory analyses of these samples. As a result, they were included in statistical analyses.

Table B-4. Data Values in the CED Phase Identified as Outliers by Formal Statistical Tests

| Unit ID | Instr. <br> Batch | Sample Prep Batch | $\begin{gathered} \text { MRI } \\ \text { ID } \\ \hline \end{gathered}$ | Sample Medium | Activity | Parameter | Data Value | - Level | Hi/Lo |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Balt. (1) | E04044A | 625 | 60709 | SSDC Wipe | HVAC | Loading | 285.66 | 0.10 | Low |
| Balt. (2) | V04134A | 630 | 60884 | Personal Exp. | Demolition | Loading | 947.05 | 0.05 | High |
| Denver (3) | E05264B | 634 | 60853 | SSDC <br> Vacuum | Demolition | Loading | 53845 | 0.10 | High |

## B.2.3 Graphical Review

The aim of graphical review of data for outlier detection was to visually observe those data points which deviated from the general distribution of all data points. Two plotting procedures were used to check for outliers in each of the three phases:

- the exploratory plotting and regression fitting procedure, and
- the single sample and simultaneous plotting procedure.

Exploratory plotting and regression fitting was applied to the carpet removal and window replacement phases, while single sample and simultaneous plotting were used in the window replacement and CED phases. A description of each of these procedures follows.

Exploratory Plotting and Regression Fitting: The exploratory plotting procedure characterizes the overall relationship between the results of settled dust samples that are paired in some way (e.g., wipe/vacuum sample pairs), flagging those samples whose results deviate substantially from this observed relationship.

The relationship between paired sample results is observed by creating a scatterplot of the log-transformed results of one sampling approach versus the other (e.g., wipe versus vacuum), fitting a linear regression equation to the points in the plot, and flagging those points which deviate substantially from the fitted line. Data points are flagged if the studentized residual exceeds a value of two in absolute value. The results of one or both samples represented by a given flagged point in the plot are then labeled as potential outliers.

Single Sample and Simultaneous Plotting: For single (i.e., unpaired) sample results, descriptive plots, including lognormal probability plots of lead concentration, lead loading and sample weight, and scatterplots were used to identify unusual observations.

Scatterplots were created of log-transformed loadings versus log-transformed weights or concentrations grouped into appropriate categories (e.g., by distance from activity). Possible confounding factors which could explain extreme results, such as dwelling unit, were then examined. In cases where such a factor was deemed to explain deviations, the observation was not included as an outlier. An example of a simultaneous scatterplot used to identify outliers in the single sample case is presented in Figure B-1 for paint chip sample results in the CED study. Note the high variability among Baltimore(1) samples, which excludes the observation associated with a low loading and low concentration from consideration. Dwelling unit in this case is a confounding variable. In addition, dilution factors could explain some extreme values. For example, an observation appearing as an outlier in a plot of lead concentration versus weight may not appear as an outlier in a plot of lead loading versus weight.

$\circ \circ \circ$ Baltimore Unit $1 \diamond \circ \circ$ Baltimore Unit $2 * * *$ Denver Units

Figure B-1. Scatterplot of Paint Chip Log Lead Loadings versus Paint Chip Log Lead Concentrations for the Demolition CED Activities

Only data associated with "regular" samples were included in the exploratory plotting procedure for the 1-hour vs. 2-hour and vacuum vs. wipe comparisons (i.e., results for samples with a field QC purpose, such as side-by-side samples, were not included). Some of the scatterplots reviewed in this outlier analysis are found throughout this report. The regression fittings were conducted separately within the same data categories that were considered in the formal statistical tests procedure.

## Carpet Removal Phase Results

Table B-5 presents those paired samples which have been flagged in the exploratory plotting and regression fitting procedure for the carpet removal phase. The pre-activity/postactivity pairs that were flagged had much larger post-activity results relative to their pre-activity results. One pair occurred in unit 1-04, which had high lead levels in all samples. In the wipe/vacuum pair that was flagged (unit 2-01, location L2) the vacuum sample loading was higher than the wipe sample loading. Note that the loading and concentration associated with the 1-hr post-activity vacuum sample were also much higher than that for the 2 -hr post-activity sample at the same location. This unexpected result of observing higher loadings for a 1 -hr
sample compared to a $2-\mathrm{hr}$ sample was flagged in the logic check procedure above. The other two 1-hr/2-hr sample pairs that were flagged had much higher results for the 2-hour sample.

Table B-5. Sample Pairs in the Carpet Removal Phase Identified as Outliers by Graphical Review and Regression Analysis

## 1. Pre-Activity/Post-Activity Floor Dust Sample Pairs

| Unit ID | Location | Parameter | Pre-Activity Sample |  | Post-Activity Sample |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sample ID | Result | Sample ID | Result |
| 2-05 | Bathroom (L2) | Sample wgt. | 60666 | 0.1629 g | 60676 | 0.6285 g |
| 1-04 | Bathroom \#1 (L1) | Lead loading | 60128 | $2.61 \mu \mathrm{~g} / \mathrm{ft}^{2}$ | 60148 | 6,135 $\mathrm{gg} / \mathrm{ft}^{2}$ |
|  |  | Lead conc. | 60128 | $90.78 \mu \mathrm{~g} / \mathrm{g}$ | 60148 | 20,662 $\mu \mathrm{g} / \mathrm{g}$ |

## 2. One-hour/Two-hour Post-Activity SSDC Sample Pairs

| Unit ID | Location | Parameter | Pre-Activity Sample |  | Post-Activity Sample |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Sample ID | Result | Sample ID | Result |
| 2-03 | Bathroom (L2) | Sample wgt. | 62216 | 0.0158 g | 60436 | 0.2245 g |
| 2-01 | Hall (L2) | Lead loading | 62006 | $216.0 \mu \mathrm{~g} / \mathrm{ft}^{2}$ | 62116 | $23.0 \mu \mathrm{~g} / \mathrm{ft}^{2}$ |
|  |  | Lead conc. | 62006 | $6990 \mu \mathrm{~g} / \mathrm{g}$ | 62116 | $746.7 \mu \mathrm{~g} / \mathrm{g}$ |
| 2-02 | Sun room (L3) | Lead loading | 60486 | $2.85 \mu \mathrm{~g} / \mathrm{ft}^{2}$ | 60466 | $54.82 \mu \mathrm{~g} / \mathrm{ft}^{2}$ |
|  |  | Lead conc. | 60486 | $370.2 \mu \mathrm{~g} / \mathrm{g}$ | 60466 | $3807 \mu \mathrm{~g} / \mathrm{g}$ |

3. Wipe/Vacuum SSDC Sample Pairs

|  |  |  | Wipe Sample | Vacuum Sample |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Unit <br> ID | Location | Parameter | Sample ID | Result |  |
| $2-01$ | Hallway (L2) | Lead loading | 62186 | $23.62 \mu \mathrm{~g} / \mathrm{ft}^{2}$ |  |

## Window Replacement Phase Results

Table B-6 presents those results in the window replacement phase which have been flagged in the single sample and simultaneous plotting procedure.

None of the paired samples for the 2-hour versus 1-hour comparisons were identified as outliers. In addition, those paired samples for the pre-activity versus post-activity floor dust comparisons identified as outliers did not differ from outliers detected in the logic check. Therefore, paired samples are not included in Table B-6.

Table B-6. Sample Results in the Window Replacement Phase Identified as Outliers by Graphical Review and Regression Analysis

| Unit ID | Instr. <br> Batch | Sample Prep. Batch | $\begin{aligned} & \text { Sample } \\ & \text { ID } \end{aligned}$ | Sample Medium | Sample Type | Componen t ID | Parameter | Sample Value | Comment |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | E11153A | 614 | 60230 | Window Well | Vacuum | 2 (DEN) | Loading Conc. | $\begin{aligned} & 2311.65 \\ & 2282.63 \end{aligned}$ | Low value for loading, concentration. |
| 1-01 | $\begin{aligned} & \text { E11153A } \\ & \text { E11153A } \end{aligned}$ | $\begin{aligned} & 614 \\ & 614 \end{aligned}$ | $\begin{aligned} & 60233 \\ & 60184 \end{aligned}$ | Window Well | Vacuum | $\begin{aligned} & 2 \text { (KIT) } \\ & 2 \text { (BAT) } \end{aligned}$ | Loading <br> Conc. <br> Weight <br> Loading <br> Conc. <br> Weight | $\begin{gathered} 33287.56 \\ 43098.31 \\ .2950 \\ 54740.95 \\ 70067.02 \\ .2984 \end{gathered}$ | Unusually high concentrations and loadings for a low sample weight. |
| $\begin{aligned} & 1-01 \\ & 4-01 \\ & 4-01 \\ & \hline \end{aligned}$ | E11173A E02104A E02104A | $\begin{aligned} & 616 \\ & 620 \\ & 620 \\ & \hline \end{aligned}$ | $\begin{aligned} & 60257 \\ & 60344 \\ & 60359 \\ & \hline \end{aligned}$ | Paint chip | Exterior | $\begin{gathered} 2 \text { (DEN) } \\ 17 \text { (LVG1) } \\ 13 \text { (BED1) } \\ \hline \end{gathered}$ | Loading <br> Loading <br> Loading | $\begin{aligned} & 2.28 \\ & 3.54 \\ & 0.34 \\ & \hline \end{aligned}$ | Low values for concentrations and loadings. |
| 4-01 $4-01$ | E02104A | 620 620 | $\begin{aligned} & 60339 \\ & 60359 \end{aligned}$ | Paint chip | Exterior | 20 (LVG1) <br> 13 (BED1) | Weight Conc. Weight | $\begin{aligned} & 0.5211 \\ & 146.01 \\ & 0.5212 \end{aligned}$ | High weights: 60339 has an unusually low concentration compared to a high weight. |

## CED Phase Results

Although several observations appeared at the extremes of these plots for SSDC samples, distance from activity provided reasonable evidence for such deviations. For paint chip samples several observations also appeared at the extremes of these plots. However, dwelling unit provided reasonable evidence for such deviations. No observations for either the SSDC or paint chip samples deviated substantially from the linear relation expected between log transformed concentrations and loadings.

Paired samples included the nine vacuum/vacuum side-by-side pairs and the twelve vacuum/wipe side-by-side pairs. No outliers were detected when considering the relationship between paired samples.

## B.2.4 Outlier Summary

Outliers were considered serious contenders for rejection from statistical analyses when they either failed two or more of the outlier checking procedures (logic checks, graphical review or formal statistical tests) or Battelle's field log sheets revealed some sampling protocol deviation. Only one outlier in the three phases of the R\&R study was deleted from the statistical analyses. A breakdown of outlier analysis results within each phase is as follows:

## Carpet Removal

10 sample pairs and 5 additional single samples were flagged by at least one of the above three analysis methods. Examination of the sample $\log$ sheets revealed no immediate explanation for any of the results, and no problems were uncovered with these results as a result of laboratory analysis. Therefore, none of these flagged results were removed from the statistical analysis.

## Window Replacement

9 sample pairs and 8 additional single samples were flagged by at least one of the above three analysis methods. Examination of the sample log sheets and review of laboratory analysis documentation revealed no immediate explanation for any of the extreme results. However, one of these flagged results has been removed from the statistical analysis. The window well sample (MRI ID 60230) was flagged in both the graphical review and formal statistical test. In addition, this result appeared inconsistent with other measurements within the same unit and the same window. Thus, this sample was removed from the analyses.

## CED

Three samples were identified as possible outliers by formal statistical tests. No outliers were flagged by either graphical review or logic checks. Examination of the sample log sheets revealed no immediate explanation for these three results, and no results were excluded from statistical analysis.

## APPENDIX C <br> STATISTICAL METHODS AND MODELS IN THE EFSS

## C. 0 STATISTICAL METHODS AND MODELS IN THE EFSS

In this appendix, the approaches to statistical analysis of the EFSS data are presented in detail. Section C. 1 presents statistical models used in the carpet removal and window replacement phases to characterize the statistical relationship between lead exposure and predictor variables. The approach to estimating components of variation on the lead exposure data within these two phases is presented in Section C.2. Section C. 3 contains the method used in the window replacement phase to estimate the effect of distance from activity on settled dust sample lead loadings. Section C. 4 presents statistical methods used to characterize lead disturbance associated with various $\mathrm{R} \& \mathrm{R}$ activities in the CED phase. Section C. 5 presents the approach to estimating lead disturbance within a 6 x 1 ' dustfall gradient in an effort to compare potential lead hazards in settled dust across CED activities. Section C. 6 presents the methodology used to calculate $95 \%$ confidence intervals for the 50th, 75 th, and 95 th percentile of worker personal exposure results and for the percentage of results above the OSHA permissible exposure limit of $50 \mu \mathrm{~g} / \mathrm{m}^{3}$. Finally, Section C. 7 presents the meta-analysis methodology for combining the surface preparation results with results obtained from sources independent from the $R \& R$ study.

## C. 1 MODELS IN THE CARPET REMOVAL AND WINDOW REPLACEMENT PHASES TO EVALUATE FACTORS OR MEASUREMENTS IN RELATION TO LEAD EXPOSURE

## Methods

In the carpet removal and window replacement phases, a common statistical modeling approach was used to express the distribution of lead in dust and air as a function of pre-activity lead levels and/or other activity characteristics. Lead measurements were initially classified as to the type of exposure represented and the approach to collecting the sample (personal worker exposures, ambient air exposures, loadings from SSDC dust samples, etc.). A set of covariates were identified as potential predictors of the lead measurements within each classification. A statistical model evaluated the significance of the association between lead measurements and the covariates. A reduced form of the model was used to characterize variability (Section C.2).

For the carpet removal data, the common model form across data categories was generally loglinear, characterizing a linear relationship between the natural logarithm lead exposure measurement and a series of $p(\cdot 1)$ log-transformed covariates and duration of activity. The model form was

$$
\begin{equation*}
\log \left(Y_{i j}\right) \quad \log (\mu) \quad{ }_{k 1}{ }_{k} \log \left(X_{k i j}\right) \quad T_{i} \quad H_{i} \quad L_{j(i)}, \tag{C-1}
\end{equation*}
$$

where $\mathrm{Y}_{\mathrm{ij}}$ is the lead exposure measurement for the sample taken at the $\mathrm{j}^{\text {th }}$ location within the $\mathrm{i}^{\text {th }}$ study unit, $\mu$ represents the (unknown) geometric mean lead measurement across the study phase, $\mathrm{X}_{\mathrm{kij}}$ represents the value associated with the $\mathrm{j}^{\text {th }}$ location within the $\mathrm{i}^{\text {th }}$ study unit of covariate $\mathrm{X}_{\mathrm{k}}$, - ${ }_{k}$ is the (unknown) multiplicative effect of covariate $X_{k}$ on the lead loading, $T_{i}$ is the duration of
carpet removal (minutes) in the ith unit, • is the (unknown) additive effect of activity duration on the log lead measurement, $\mathrm{H}_{\mathrm{i}}$ represents the random effect of the $\mathrm{i}^{\text {th }}$ study unit (normally distributed with mean zero and variance $\cdot{ }_{u}{ }^{2}$ ), and $L_{j(i)}$ represents the random effect of the $j^{\text {th }}$ sample location within the $\mathrm{i}^{\mathrm{th}}$ study unit (normally distributed with mean zero and variance $\cdot{ }_{\mathrm{L}}{ }^{2}$ ). Only data corresponding to "regular" (i.e., not side-by-side) samples were included in these model fits. The MIXED procedure in the SAS® System was used to fit model (C-1) to each category of lead loading data, resulting in estimates for the model parameters $\mu,{ }_{1}, \ldots,{ }_{\mathrm{p}},{ }^{\bullet},{ }_{\mathrm{u}}{ }^{2}$, and ${ }_{\mathrm{L}}{ }^{2}$ for a given category.

For the carpet removal phase, Table C-1 lists the data categories and the covariate group considered within each category. Each data category considered a specific group of covariates $X_{k}$ in model ( $\mathrm{C}-1$ ). According to the model, each covariate $\mathrm{X}_{\mathrm{k}}$ has a multiplicative effect on the (untransformed) lead loading, with the parameter ${ }^{\circ}{ }_{k}$ representing the extent of the effect associated with covariate $X_{k}$. Thus, a test of whether ${ }^{*}{ }_{k}$ is significantly different from zero indicates whether the covariate $X_{k}$ is significantly associated with the lead exposure measurement in the given data category. Similarly, a test of whether • is significantly different from zero indicates whether the duration of carpet removal activity is significantly associated with lead exposure.

In the window replacement phase, a model similar to Model (C-1) was fitted to lead measurements. Due to the small numbers of data points within each category of lead measurement considered, each fit of the model included only one covariate. Therefore, the model took the form

$$
\begin{equation*}
\log \left(Y_{i j}\right) \quad \log (\mu) \quad{ }_{k} \log \left(X_{\text {kij }}\right) \quad H_{i} \quad L_{j(i)}, \tag{C-1a}
\end{equation*}
$$

where the notation is interpreted in the same manner as for Model ( $\mathrm{C}-1$ ). The only exception was for ambient air lead concentrations, where the pre-activity ambient air lead concentration for the study unit was included as a covariate within each fit of model (WR-2). Multiple covariates were considered within each data category; the model was fitted a number of times equal to the number of covariates considered for the data category. Table C-2 lists the data categories and the covariates considered in the various model fits within the category. The MIXED procedure in the SAS® System was used to fit each model.

## Results

Results of fitting the various models in Table C-1 on carpet removal data (models (CPT-1) to (CPT-4)) are presented in Table C-3. This table presents estimates and associated standard errors for model parameters $\mu, \beta_{1}, \ldots, \beta_{\mathrm{p}}$, and • . The estimated parameters ${ }^{\mathrm{k}}{ }_{\mathrm{k}}$ and $\bullet$ were generally not significantly different from zero at the 0.05 level, implying that their associated covariates were not statistically associated with the lead loading of the sample type of interest. However, the models were fit to a small number of data points that generally had high variability, resulting in statistical tests with low power to detect differences from zero.

Results of fitting the models in Table C-2 on window removal data (models (WR-1) to (WR-5)) are presented in Tables C-4a through C-4d. These table presents model parameter estimates and their standard errors. Table C-4a presents results from fitting model (WR-1) with different covariates to personal exposure data. Table C-4b contains results from fitting model (WR-2) with different covariates to area air data. Results from fitting models (WR-3) and (WR-4) with different covariates to SSDC settled dust lead loading data are found in Table C-4c. Finally, Table C-4d presents results from fitting model (WR-5) with different covariates to lead amounts disturbed in a 6'x1' dustfall gradient. The estimated parameters ${ }^{\circ}{ }_{k}$ were generally not significantly different from zero at the 0.05 level.

## Table C-1. Data Categories and Covariates Considered in Fitting Model Form (C-1) to Lead Loading Data in the Carpet Removal Phase

| Model ID <br> Number | Data Category | Covariates Included in the Model |  |
| :---: | :---: | :---: | :---: |
| (CPT-1) | Personal Worker Exposures ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) | $X_{1}$ $X_{2}$ $X_{3}$ | Geometric mean lead loading in carpet in the $\mathrm{i}^{\text {th }}$ unit. Geometric mean lead loading in pre-activity floor dust samples in the $\mathrm{i}^{\text {th }}$ unit. <br> Geometric mean lead loading in pre-activity window sill dust samples in the $\mathrm{i}^{\text {th }}$ unit. |
| (CPT-2) | Area Airborne Exposures $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ | $\begin{aligned} & X_{1 i}: \\ & X_{2 i}: \\ & X_{3 i}: \\ & X_{44}: \end{aligned}$ | Geometric mean lead loading in carpet in the $\mathrm{i}^{\text {th }}$ unit. Geometric mean lead loading in pre-activity floor dust samples in the $\mathrm{i}^{\text {th }}$ unit. <br> Geometric mean lead loading in pre-activity window sill dust samples in the $\mathrm{i}^{\text {th }}$ unit. <br> Lead loading in the pre-activity area air sample in the $\mathrm{i}^{\text {th }}$ unit. |
| (СРТ-3) | 1-hour post-activity lead loadings from floors or SSDCs ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | $X_{1}$ $X_{2}$ X | Geometric mean lead loading in carpet in the $\mathrm{i}^{\text {th }}$ unit. Lead loading in the adjacent pre-activity floor dust sample ( $\mathrm{j}^{\text {th }}$ location within $\mathrm{i}^{\text {th }}$ unit). <br> Geometric mean lead loading in pre-activity window sill dust samples in the $\mathrm{i}^{\text {th }}$ unit. |
| (СРТ-4) | 1-hour post-activity lead loadings from window sills ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | $X_{1 i}$ $X_{2 i}$ \% $X_{3 i j}$ | Geometric mean lead loading in carpet in the $\mathrm{i}^{\text {th }}$ unit. Geometric mean lead loading in pre-activity floor dust samples in the $i^{\text {th }}$ unit. <br> Lead loading in the adjacent pre-activity window sill dust sample ( $j^{\text {th }}$ location in the $i^{\text {th }}$ unit). |

Table C-2. Data Categories and Covariates Considered in Fitting Model Form (C-1a) to Lead Loading Data in the Window Replacement Phase

| Model ID Number | Data Category | Number of Model Fits | Covariates Considered Among the Model Fits <br> (For a given data category, each covariate was included in only one model fit, with the exception of area airborne exposures, where covariate $X_{7 i j}$ was included in every fit of Model (WR-2)) |
| :---: | :---: | :---: | :---: |
| (WR-1) | Personal Worker Exposures ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) | 7 | $X_{1 i j}$ : Pre-act. floor dust lead loading at 0 ft . from window. <br> $X_{\text {2ij }}$ : Pre-act. floor dust lead loading at 3 ft . from window. <br> $X_{3 i j}$ : Pre-act. floor dust lead loading at 6 ft . from window. <br> $X_{\text {4ij }}$ : Pre-act. window well dust lead loading. <br> $X_{5 i j}$ : Lead content of paint chips collected from the interior sash/frame of the window. <br> $X_{6 i j}$ : Lead content of paint chips collected from the exterior sash/frame of the window. <br> $X_{7}$ : Pre-activity ambient air lead loading in the ith unit. |
| (WR-2) | Area Airborne <br> Exposures ( $\mu \mathrm{g} / \mathrm{m}^{3}$ ) | 6 | $X_{1 i j}$ : Pre-act. floor dust lead loading at 0 ft . from window. <br> $X_{\text {2ij }}$ : Pre-act. floor dust lead loading at 3 ft . from window. <br> $X_{3 i j}$ : Pre-act. floor dust lead loading at 6 ft . from window. <br> $X_{4 i j}$ : Pre-act. window well dust lead loading. <br> $X_{5 j}$ : Lead content of paint chips collected from the interior sash/frame of the window. <br> $X_{6 i j}$ : Lead content of paint chips collected from the exterior sash/frame of the window. <br> $X_{7}$ : Pre-activity ambient air lead loading in the $\mathrm{i}^{\text {th }}$ unit (included in every model fit to area airborne exposure data). |
| (WR-3) | 1-hour post-activity lead loadings from SSDCs at zero feet from window ( $\mu \mathrm{g} / \mathrm{f} \mathrm{t}^{2}$ ) | 6 | $X_{1 i j}$ : Pre-act. floor dust lead loading at 0 ft . from window. <br> $X_{\text {2ij }}$ : Pre-act. floor dust lead loading at 3 ft . from window. <br> $X_{3 i j}$ : Pre-act. window well dust lead loading. <br> $X_{4 i j}$ : Lead content of paint chips collected from the interior sash/frame of the window. <br> $X_{5 i j}$ : Lead content of paint chips collected from the exterior sash/frame of the window. <br> $X_{6 i}$ : Pre-activity ambient air lead loading in the $i^{\text {th }}$ unit. |
| (WR-4) | 1-hour post-activity lead loadings from SSDCs at six feet from window ( $\mu g / f t^{2}$ ) | 6 | $X_{1 i j}$ : Pre-act. floor dust lead loading at 3 ft . from window. <br> $X_{\text {2ij: }}$ : Pre-act. floor dust lead loading at 6 ft . from window. <br> $X_{3 i j}$ : Pre-act. window well dust lead loading. <br> $X_{4 i j}$ : Lead content of paint chips collected from the interior sash/frame of the window. <br> $X_{5 i j}$ : Lead content of paint chips collected from the exterior sash/frame of the window. <br> $X_{6 i}$ : Pre-activity ambient air lead loading in the $i^{\text {th }}$ unit. |

## Table C-2. Data Categories and Covariates Considered in Fitting Model Form (C-1a) to Lead Loading Data in the Window Replacement Phase

| (WR-5) | Estimated lead amount in $6^{\prime} \times 1^{\prime}$ gradient from window | 7 | $X_{1 i j}$ : Pre-act. floor dust lead loading at 0 ft . from window. <br> $X_{2 i j}$ : Pre-act. floor dust lead loading at 3 ft . from window. <br> $X_{3 i j}$ : Pre-act. floor dust lead loading at 6 ft . from window. <br> $X_{4 i j}$ : Pre-act. window well dust lead loading. <br> $X_{5 i j}$ : Lead content of paint chips collected from the interior sash/frame of the window. <br> $X_{6 i j}$ : Lead content of paint chips collected from the exterior sash/frame of the window. <br> $X_{7}$ : Pre-activity ambient air lead loading in the $i^{\text {th }}$ unit. |
| :---: | :---: | :---: | :---: |

Table C-3. Parameter Estimates (and Standard Errors) from Fitting Statistical Models to Evaluate Factors Relating to Lead Disturbance in Carpet Removal Data

Standard errors of model parameter estimates are in parentheses.

| Model Parameter ${ }^{(1)}$ | Estimates from Modeling Personal-Air Lead Conc. (Model CPT-1) | Estimates from Modeling <br> Ambient Air Lead Conc. <br> (Model CPT-2) | Estimates from Modeling PostActivity Floor Dust Lead Loading (Model CPT-3) | Estimates from Modeling 1-hr. Post-Activity SSDC Dust Lead Loading (Model CPT-3) | Estimates from Modeling PostActivity Window Sill Dust Lead Loading (Model CPT-4) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mu$ | $\begin{gathered} 1.521 \\ (5.104) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline-3.666 \\ & (6.591) \\ & \hline \end{aligned}$ | $\begin{aligned} & \hline 5.623 \text { * } \\ & (2.383) \\ & \hline \end{aligned}$ | $\begin{gathered} 1.761 \\ (2.586) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 3.552 \\ (2.890) \\ \hline \end{gathered}$ |
| - ${ }_{1}$ | $\begin{gathered} 0.219 \\ (0.679) \\ \hline \end{gathered}$ | $\begin{gathered} 0.089 \\ (0.497) \\ \hline \end{gathered}$ | $\begin{array}{r} -0.139 \\ (0.314) \\ \hline \end{array}$ | $\begin{gathered} 0.078 \\ (0.339) \\ \hline \end{gathered}$ | $\begin{gathered} -0.328 \\ (0.392) \\ \hline \end{gathered}$ |
| ${ }^{2}$ | $\begin{gathered} -0.831 \\ (0.487) \\ \hline \end{gathered}$ | $\begin{aligned} & -0.472 \\ & (0.373) \\ & \hline \end{aligned}$ | $\begin{gathered} 0.289 \\ (0.209) \\ \hline \end{gathered}$ | $\begin{array}{r} -0.198 \\ (0.216) \\ \hline \end{array}$ | $\begin{gathered} 0.173 \\ (0.281) \\ \hline \end{gathered}$ |
| - 3 | $\begin{array}{r} -0.120 \\ (0.492) \\ \hline \end{array}$ | $\begin{gathered} 0.010 \\ (0.421) \\ \hline \end{gathered}$ | $\begin{gathered} -0.463 \\ (0.231) \\ \hline \end{gathered}$ | $\begin{gathered} -0.099 \\ (0.251) \\ \hline \end{gathered}$ | $\begin{gathered} 0.591 * \\ (0.241) \\ \hline \end{gathered}$ |
| ${ }^{4} 4$ |  | $\begin{gathered} 0.021 \\ (0.018) \\ \hline \end{gathered}$ |  |  |  |
| - | $\begin{gathered} 0.020 \\ (0.024) \\ \hline \end{gathered}$ | $\begin{gathered} -0.421 \\ (1.666) \\ \hline \end{gathered}$ | $\begin{gathered} 0.021 \\ (0.011) \\ \hline \end{gathered}$ | $\begin{gathered} 0.020 \\ (0.012) \\ \hline \end{gathered}$ | $\begin{gathered} 0.009 \\ (0.013) \\ \hline \end{gathered}$ |

* Estimate is significantly different from zero at the $\cdot=0.05$ level.
${ }^{(1)}$ Model parameters $\cdot{ }_{k}$ correspond to covariates in the order given in Table C-1.

Table C-4a. Parameter Estimates (and Standard Errors) from Fitting Model (WR-1) to Evaluate Factors Relating to Lead Disturbance for Personal Exposure Samples in the Window Replacement Phase ${ }^{(1)}$

| Covariate | Model Parameter |  |
| :--- | :---: | :---: |
|  | $\boldsymbol{\mu}$ | $\boldsymbol{1}_{1}$ |
| Pre-activity Floor Lead Loading (0 feet) | $-0.0372(1.07)$ | $0.271(0.130)$ |
| Pre-activity Floor Lead Loading (3 feet) | $0.122(0.833)$ | $0.313(0.125)$ |
| Pre-activity Floor Lead Loading (6 feet) | $0.264(0.953)$ | $0.298(0.147)$ |
| Window Well Lead Loading | $-6.64(12.1)$ | $0.739(1.03)$ |
| Interior Paint Chip Lead Loading | $1.81(0.656)$ | $0.253(0.286)$ |
| Exterior Paint Chip Lead Loading | $1.75(1.81)$ | $0.109(0.695)$ |
| Pre-activity Ambient Air Lead Concentration | $2.36(0.899)$ | $0.284(0.492)$ |

${ }^{(1)}$ Standard errors of model parameter estimates are in parentheses. See Model (C-1a) for parameter interpretation.
Note: None of the estimates are significantly different from zero at the 0.05 level.

Table C-4b. Parameter Estimates (and Standard Errors) from Fitting Model (WR-2) to Evaluate Factors Relating to Lead Disturbance for During-Activity Area Air Samples in the Window Replacement Phase ${ }^{(1)}$

| Covariate | Model Parameter |  |  |
| :--- | :---: | :---: | :---: |
|  | $\boldsymbol{\mu}$ | $\boldsymbol{P}_{1}{ }^{(2)}$ | $\boldsymbol{e}^{(3)}$ |
|  | $-8.12(9.45)$ | $0.0708(0.367)$ | $0.713(0.797)$ |
| Exterior Paint Chip Lead Loading | $-1.07(0.984)$ | $0.610(0.388)$ | $0.821(0.510)$ |
| Interior Paint Chip Lead Loading | $0.234(1.11)$ | $0.0978(0.580)$ | $0.0458(0.368)$ |
| Pre-activity Floor Lead Loading (0 feet) | $-3.16^{(4)}(0.819)$ | $-0.518^{(4)}(0.186)$ | $0.355^{(4)}(0.0810)$ |
| Pre-activity Floor Lead Loading (3 feet) | $-2.40^{(4)}(0.652)$ | $-0.394(0.164)$ | $0.344^{(4)}(0.0784)$ |
| Pre-activity Floor Lead Loading $(6$ feet $)$ | $-2.88^{(4)}(0.756)$ | $-5.44^{(4)}(0.190)$ | $0.404^{(4)}(0.0921)$ |

${ }^{(1)}$ Standard errors of model parameter estimates are in parentheses. See Model (C-1a) for parameter interpretation.
${ }^{(2)}$ Parameter estimate for pre-activity area air.
${ }^{(3)}$ Parameter estimate for listed covariate.
${ }^{(4)}$ Estimate is significantly different from zero at the $\cdot=0.05$ level.

Table C-4c. Parameter Estimates (and Standard Errors) from Fitting Models (WR3) and (WR-4) to Evaluate Factors Relating to Lead Disturbance for SSDCs at Zero and Six Feet from Windows Being Removed ${ }^{(1)}$

| Covariate | Model Parameter |  |
| :--- | :---: | :---: |
|  |  |  |
| Zero feet |  | $\boldsymbol{\mu}_{1}$ |
| Window Well Lead Loading | $-1.82(5.61)$ | $1.02(0.474)$ |
| Interior Paint Chip Lead Loading | $10.1(0.533)$ | $0.0785(0.226)$ |
| Exterior Paint Chip Lead Loading | $10.8(1.05)$ | $-0.289(0.374)$ |
| Pre-activity Floor Lead Loading (0 feet) | $8.69(1.10)$ | $0.188(0.132)$ |
| Pre-activity Floor Lead Loading (3 feet) | $7.90(0.851)$ | $0.325^{(2)}(0.123)$ |
| Pre-activity Ambient Air Lead Concentration | $10.3(0.668)$ | $0.169(0.365)$ |
|  | Six feet |  |
| Window Well Lead Loading | $4.35(2.45)$ | $0.120(0.630)$ |
| Interior Paint Chip Lead Loading | $5.45(0.891)$ | $0.0923(0.361)$ |
| Exterior Paint Chip Lead Loading | $6.44(1.22)$ | $-0.382(0.427)$ |
| Pre-activity Floor Lead Loading (3 feet) | $3.64(1.52)$ | $0.270(0.219)$ |
| Pre-activity Floor Lead Loading (6 feet) | $4.39(1.52)$ | $0.195(0.229)$ |
| Pre-activity Ambient Air Lead Concentration | $6.33(0.750)$ | $0.659(0.410)$ |

[^8]Table C-4d. Parameter Estimates (and Standard Errors) from Fitting Model (WR-5) Evaluate Factors Relating to Estimated Total Lead Disturbance in a Six-foot by One-foot Gradient Perpendicular to Windows Being Removed ${ }^{(1)}$

| Covariate | Model Parameter |  |
| :---: | :---: | :---: |
|  | $\mu$ | - 1 |
| Total Lead |  |  |
| Window Well Lead Loading | $\begin{array}{r} 0.276 \\ (5.22) \\ \hline \end{array}$ | $\begin{gathered} 0.906 \\ (0.441) \\ \hline \end{gathered}$ |
| Interior Paint Chip Lead Loading | $\begin{gathered} 11.4^{(2)} \\ (0.984) \\ \hline \end{gathered}$ | $\begin{gathered} -0.269 \\ (0.351) \\ \hline \end{gathered}$ |
| Exterior Paint Chip Lead Loading | $\begin{gathered} 10.7^{(2)} \\ (0.528) \\ \hline \end{gathered}$ | $\begin{aligned} & 0.0871 \\ & (0.225) \\ & \hline \end{aligned}$ |
| Pre-activity Floor Lead Loading (0 feet) | $\begin{aligned} & 9.38^{(2)} \\ & (1.02) \\ & \hline \end{aligned}$ | $\begin{gathered} 0.189 \\ (0.122) \\ \hline \end{gathered}$ |
| Pre-activity Floor Lead Loading (3 feet) | $\begin{gathered} 8.59^{(2)} \\ (0.750) \\ \hline \end{gathered}$ | $\begin{aligned} & 0.326^{(2)} \\ & (0.109) \\ & \hline \end{aligned}$ |
| Pre-activity Floor Lead Loading (6 feet) | $\begin{gathered} 9.47^{(2)} \\ (0.933) \\ \hline \end{gathered}$ | $\begin{array}{r} 0.228 \\ (0.142) \\ \hline \end{array}$ |
| Pre-activity Ambient Air Lead Concentration | $\begin{array}{r} 11.1^{(2)} \\ (0.617) \\ \hline \end{array}$ | $\begin{gathered} 0.249 \\ (0.337) \\ \hline \end{gathered}$ |

${ }^{(1)}$ Standard errors of model parameter estimates are in parentheses. See Model (C-1a) for parameter interpretation.
${ }^{(2)}$ Estimate is significantly different from zero at the $\cdot=0.05$ level.

## C. 2 ESTIMATING COMPONENTS TO TOTAL VARIABILITY IN LOGTRANSFORMED LEAD LOADING DATA IN THE CARPET REMOVAL AND WINDOW REPLACEMENT PHASES

The models in Section C.1, used to evaluate the relationship of pre-activity lead measurements and activity characteristics to lead exposures in a given data category, contained random effects to characterize unit-to-unit variability (denoted by $\bullet{ }_{u}{ }^{2}$ ) and within-unit (i.e., location-to-location) variability (denoted by ${ }^{\circ}{ }_{\mathrm{L}}{ }^{2}$ ) in the response variable (log-transformed lead loadings). In addition, a third variance component can be characterized when results from side-by-side QC samples within a sampling location are available for analysis. This third component, denoted by $\cdot{ }_{R}{ }^{2}$, represents variability present in results within a sampling location at a given study unit, and could be estimated for floor dust and SSDC samples. Estimating these three variance components provides information on how one variance component dominates another relative to the total variability in the response.

The covariates within the models in Section C. 1 generally were not significantly associated with lead measurements. As a result, reported estimates of the three variance
components were obtained after fitting the following model to data within each of the data categories in Tables C-1 and C-2:

$$
\begin{equation*}
\log \left(y_{i j k}\right) \quad \log (\mu) \quad H_{i} \quad L_{\lambda i)} \quad k(i j) \tag{C-2}
\end{equation*}
$$

where $\mathrm{Y}_{\mathrm{ijk}}$ is the $\mathrm{k}^{\text {th }}$ replicate lead loading at the $\mathrm{j}^{\text {th }}$ location in the $\mathrm{i}^{\text {th }}$ unit, $\mu$ is an estimate of the study-wide geometric mean, $\mathrm{H}_{\mathrm{i}}$ is a random effect of the $\mathrm{i}^{\text {th }}$ unit (normally distributed with mean zero and variance $\cdot{ }_{u}{ }^{2}$ ), $L_{j(i)}$ is a random effect of the $j^{\text {th }}$ location in the $i^{\text {th }}$ unit (normally distributed with mean zero and variance ${ }^{\circ}{ }_{\mathrm{L}}{ }^{2}$ ), and ${ }_{\mathrm{k}(\mathrm{ji})}$ is a random effect of the $\mathrm{k}^{\text {th }}$ replicate within the $\mathrm{j}^{\text {th }}$ location in the $\mathrm{i}^{\text {th }}$ unit (normally distributed with mean zero and variance $\cdot{ }_{\mathrm{R}}{ }^{2}$ ). Note that for data categories without side-by-side QC sample data (e.g., personal and ambient air exposures, window-sill dust lead loadings), the variance component ${ }^{2}{ }^{2}$ cannot be estimated.

Restricted maximum likelihood estimation techniques were applied to estimate the variance components ${ }_{\mathrm{u}}{ }^{2},{ }_{\mathrm{L}}{ }^{2}$, and $\bullet_{\mathrm{R}}{ }^{2}$ (where appropriate) using the MIXED procedure in the SAS® System. For the sample types where no side-by-side QC samples were collected, $\bullet{ }_{R}{ }^{2}$ was set to zero. The total variability in log-transformed lead loadings within the data category was then assumed to be $\bullet{ }_{\mathrm{u}}{ }^{2}+\bullet{ }_{\mathrm{L}}{ }^{2}+\bullet{ }_{\mathrm{R}}{ }^{2}$. To determine the extent to which a single variance component dominated total variability, ratios of each variance component to total variability were expressed in percentage terms.

The results of fitting the variance component Model (C-2) to lead measurements are presented in Section 7A-2.2.4 for the carpet removal phase and Section 7B-2.2.4 for the window replacement phase.

## C. 3 MODELING THE RELATIONSHIP BETWEEN LEAD EXPOSURE AND DISTANCE FROM ACTIVITY AREA IN THE WINDOW REPLACEMENT PHASE

The sampling design of the window replacement phase specified that for each window being removed, a settled dust sample from a SSDC be collected at one hour after completion of the activity at two distances from the window (zero feet and six feet). It was desired to determine whether distance from the activity could explain the lead loadings found in the SSDC dustfall samples. The statistical model used to evaluate this relationship was

$$
\begin{equation*}
\log \left(Y_{i j}\right) \quad \log (\mu) \quad d_{i j} \quad H_{i} \quad L_{j(i)} \tag{C-3}
\end{equation*}
$$

where $d_{i j}$ represents the distance from the window of the $j^{\text {th }}$ location within the $i^{\text {th }}$ study unit, $\beta$ is the (unknown) additive effect of $\mathrm{d}_{\mathrm{ij}}$ on the $\log$ lead measurement $\log \left(\mathrm{Y}_{\mathrm{ij}}\right)$, and the remaining model parameters are interpreted in the same manner as model (C-1a) in Section C.1. Thus, a test of whether the parameter - is significantly different from zero indicates whether the distance is significantly associated with the SSDC lead loadings.

Results of fitting model (C-3) to the SSDC lead loadings in the window replacement phase are presented and discussed in Section 7B-2.2.3.

## C. 4 MODELS IN THE CED PHASE TO EVALUATE FACTORS OR MEASUREMENTS IN RELATION TO LEAD EXPOSURE

Section 7C presents the results of several statistical models for lead exposure data from the CED phase of the EFSS. These models were used to:

- characterize the statistical relationship between personal exposure to airborne lead and predictor variables such as target activity, substrate, and pre-activity lead levels; and
- explain the lead loading in settled dust as a function of distance, target activity, substrate, and pre-activity lead levels.

This section presents the statistical methodology upon which the results of Section 7C were based.

Like the models in Section C.1, the characterization of the distributions of lead in air, settled dust, and paint in the CED phase are based on linear models that describe the natural logarithm of the observed lead loadings as a function of one or more covariates, or predictor variables. The models also characterize total variability in the response as a function of several sources of variability, such as worker-to-worker variability and unit-to-unit variability.

The MIXED procedure in the $\mathrm{SAS}^{\circledR}$ System was used to fit the models to relate the measured lead loadings to appropriate explanatory variables. This procedure accommodates both fixed and random effects factors, as well as a variety of statistical dependence structures.

In describing the model fitting procedure, the following terms are used:
Subunit -- a portion of a dwelling unit where a specific CED activity was performed. This can be an entire room or a portion of a room.

Experimental unit -- the occurrence of a specific CED activity (i) within a subunit (k) of a dwelling unit ( j ). This is generally represented by $E U_{\mathrm{ijk}}$.

Table C-5 provides a summary of the statistical models applied to CED data. These models were generally fit separately to each combination of target activity and substrate. The models appear in the order that they are referenced in Section 7C.

Table C-5. Statistical Models Considered in the CED Phase to Characterize Lead Loadings

| Model | Response Variable ${ }^{(1)}$ | Model Fit Separately By | Predictor Variables | Variance Components |
| :---: | :---: | :---: | :---: | :---: |
| CED-1 | $\log \left(\mathrm{PEM}_{\mathrm{ijk}}\right)$ | Activity/Substrate | None | $\stackrel{\text { Unit }}{\bullet} \stackrel{\text { Worker }}{ }$ |
| CED-2 | $\log \left(\mathrm{PEM}_{\mathrm{ijk}}\right)$ | Activity | Substrate | - Worker - Error |
| $\begin{aligned} & \text { CED-3 } \\ & \text { CED-4 } \end{aligned}$ | $\log$ Dust $_{\text {ijk }}$ ) | Exper. Unit | Distance | - ${ }^{\text {ntercept }}$ - Slope - Error |
| CED-5 | $\log$ Dust $_{\text {jikk }}$ ) | Activity/Substrate | Distance | - ${ }_{\text {Intercept }}{ }^{\text {- }}$ Slope ${ }^{\text {- }}$ Error |
| CED-6 | $\log \left(\right.$ Dust $\left._{\text {ijk }}\right)$ | Activity | Distance, Substrate | - $_{\text {Intercept }}{ }^{\text {- }}$ Slope ${ }^{\text {- }}$ Error |
| CED-7 | $\log \left(\mathrm{PEM}_{\mathrm{ijk}}\right)$ | Activity | Substrate, Paint | - Worker - Error |
| CED-8 | $\log$ Dust $_{\text {ijk }}$ ) | Activity | Distance, Substrate, Paint | - Intercept ${ }^{\text {- }}$ Slope - Error |

${ }^{(1)}$ PEM $=$ personal exposure monitor result $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$.
Dust $=$ dust lead loading $\left(\mu \mathrm{g} / \mathrm{tt}^{2}\right)$.

Each model in Table C-5 is presented in further detail in the following subsections, along with estimates of model parameters obtained from fitting the models.

## C.4.1 Variance Components Associated with Worker Personal Exposure Levels

## Model

To characterize the components of variability in personal exposure measurements, the following model was fit separately for each combination of target activity and substrate (denoted by subscript i):

$$
\begin{equation*}
\log \left(\mathrm{PEM}_{\mathrm{ijk}}\right)=\mu_{\mathrm{i}}+\text { Unit }_{\mathrm{j}}+\operatorname{Task}_{\mathrm{k}}\left(\text { Unit }_{\mathrm{j}}\right)+\text { Worker }_{\mathrm{l}}+\mathrm{e}_{\mathrm{ijk} \mid} \tag{CED-1}
\end{equation*}
$$

where
$\mathrm{PEM}_{\mathrm{ijk}}$ is the personal exposure measurement $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ for the $\mathrm{l}^{\text {th }}$ worker within subunit k of the $\mathrm{j}^{\text {th }}$ dwelling unit;
$\mu_{\mathrm{i}}$ is the mean of the $\log (\mathrm{PEM})$ responses over the activity;
Unit ${ }_{\mathrm{j}}$ is a random effect attributable to the $\mathrm{j}^{\text {th }}$ dwelling unit, having standard deviation

- Unit;
$\operatorname{Task}_{\mathrm{k}}\left(\mathrm{Unit}_{\mathrm{j}}\right)$ is a random effect attributable to the occurrence of subunit k within dwelling unit j , having standard deviation ${ }^{-}$Task(Unit) ;

Worker $_{1}$ is a random effect attributable to the $\mathrm{l}^{\text {th }}$ worker performing the activity, having standard deviation ${ }^{\bullet}$ Worker ; and
$\mathrm{e}_{\mathrm{ijk} \mathrm{l}}$ is a random term representing replicate variability and measurement error, having standard deviation ${ }^{\bullet}$ Error

The four random effects are each assumed to be independent from each other and have a normal distribution with mean zero. In addition, the random effect Worker $_{1}$ is assumed to be crossed with Unit ${ }_{\mathrm{j}}$ and $\mathrm{Task}_{\mathrm{k}}\left(\mathrm{Unit}_{\mathrm{j}}\right)$.

In the above model, ${ }^{\bullet}{ }_{\text {Unit }}$ is interpreted as a measure of heterogeneity that exists between different dwelling units and is estimable only if multiple dwelling units were considered. The component - Task(Unit) is interpreted as a measure of the variability that exists between occurrences of activity (i) in multiple subunits (k) within dwelling unit ( j ), and is estimable only if data for multiple subunits exist. The component ${ }^{-}{ }_{\text {Worker }}$ is interpreted as a measure of heterogeneity between different workers performing the same activity, and is estimable only when data for multiple workers at a given activity are present.

## Results

For each activity, Table C-6 presents estimates of the geometric mean and those variance components which were estimable as a result of fitting model (CED-1) to log-transformed personal exposure data.

Table C-6. Estimated Variance Components and Geometric Mean Resulting from Fitting Model (CED-1) to Personal Exposure Results for a Given CED Activity/Substrate Combination

Model (CED-1): $\log \left(\right.$ PEM $\left._{\mathrm{ijk}}\right)=\mu_{\mathrm{i}}+$ Unit $_{\mathrm{j}}+$ Task $_{\mathrm{k}}\left(\right.$ Unit $\left._{\mathrm{j}}\right)+$ Worker $_{\mathrm{l}}+\mathrm{e}_{\mathrm{ijk} 1}$

| CED Activity | Substrate | Model parameter estimates |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | Geometric Mean | - Worker | - Unit | - Task(unit) | - |
| Drilling | Plaster Wood | $\begin{array}{r} \hline 6.76 \\ 15.15 \\ \hline \end{array}$ | $\begin{aligned} & \hline 0.434 \\ & 0.000 \\ & \hline \end{aligned}$ |  |  | $\begin{aligned} & \hline 0.313 \\ & 1.295 \\ & \hline \end{aligned}$ |
| Sawing | Plaster Wood | $\begin{aligned} & 109.99 \\ & 545.84 \\ & \hline \end{aligned}$ | 0.000 |  |  | $\begin{aligned} & 1.108 \\ & 0.380 \end{aligned}$ |
| Sanding (hand) <br> Sanding (power) | Wood <br> Wood | $\begin{aligned} & 254.06 \\ & 570.82 \\ & \hline \end{aligned}$ | 0.000 | 0.860 |  | 0.589 |
| Door Modification | Wood | 590.29 | 0.896 |  |  | 0.847 |
| Component Removal | Wood | 343.84 |  |  |  | 0.045 |
| HVAC | Duct | 49.62 |  | 0.147 |  | 0.101 |


| Demolition | Plaster | 107.83 |  | 0.463 | 0.451 | 0.475 |
| :--- | :--- | ---: | :--- | :--- | :--- | :--- |
| Cleanup | Plaster | 24.46 |  |  |  | 0.550 |
|  | Wood | 102.36 |  |  |  | 0.205 |

## C.4.2 Differences in Worker Personal Exposure Lead Levels that are Attributable to Substrate (Plaster Versus Wood)

Model (CED-1) in the previous subsection was fitted to personal exposure lead levels for a given combination of CED activity and substrate to estimate variance components in these levels. For three of the activities (drilling, sawing, and cleanup), separate modeling results were obtained for wood and plaster substrates (Table C-6). For these activities, it is desired to estimate differences in modeled worker exposure lead levels that are attributable to wood versus plaster substrates.

## Model

The following model was fit separately for drilling, sawing, and cleanup activities to characterize differences due to substrate:

$$
\begin{equation*}
\log \left(\mathrm{PEM}_{\mathrm{ijk}}\right)=\mu_{\mathrm{i}}+\cdot \bullet \text { Plaster }_{\mathrm{ijk}}+\text { Worker }_{\mathrm{l}}+\mathrm{e}_{\mathrm{ijk} \mid}, \tag{CED-2}
\end{equation*}
$$

where
PEM $_{\mathrm{ijkl}}$ is the personal exposure lead concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ for the $\mathrm{l}^{\text {th }}$ worker within subunit k of the $\mathrm{j}^{\text {th }}$ dwelling unit;
$\mu_{\mathrm{i}}$ is the mean of the $\log (\mathrm{PEM})$ responses over the activity;

- ${ }_{i}$ measures the additive effect on the $\log (\mathrm{PEM})$ response that results from performing the $\mathrm{i}^{\text {th }}$ CED activity on plaster;

Plaster $_{\mathrm{ijk}}=1$ if $\mathrm{EU}_{\mathrm{ijk}}$ corresponds to performing an activity that disturbed a painted plaster surface, and equals zero otherwise;

Worker $_{1}$ is a random effect attributable to the $\mathrm{l}^{\text {th }}$ worker performing the activity, having standard deviation • Worker(i); and
$\mathrm{e}_{\mathrm{ijk} \mathrm{l}}$ is a random term representing replicate variability and measurement error, having standard deviation ${ }^{\bullet}$ Error(i).

The two random effects are each assumed to be independent from each other and have a normal distribution with mean zero. Note that those random effects included in model (CED-1) but not in model (CED-2) were associated with variance components which were not estimable for any of these three CED activities.

In model (CED-2), ${ }^{\bullet}$ Worker (i) is interpreted as a measure of heterogeneity between different workers performing the ith activity, and the error term ${ }^{\text {Error (i) }}$ represents replication and measurement error.

## Results

For drilling, sawing, and cleanup activities, Table C-7a presents estimates of model parameters resulting from fitting model (CED-2) to log-transformed personal exposure data.

Table C-7a. Parameter Estimates from Fitting Model (CED-2) to Personal Exposure Results for Drilling, Sawing, and Cleanup Activities

$$
\text { Model (CED-2): } \log \left(\text { PEM }_{\mathrm{ijk}}\right)=\mu_{\mathrm{i}}+\bullet \bullet \text { Plaster }_{\mathrm{ijk}}+\text { Worker }_{\mathrm{l}}+\mathrm{e}_{\mathrm{ijkl}}
$$

| CED Activity (i) | Parameter estimates (standard errors in parentheses) |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
|  | $\boldsymbol{\mu}_{\mathbf{i}}$ | $\bullet_{\mathbf{i}}$ | $\bullet^{2.696}$ Worker (i) | $\bullet_{\text {Error (i) }}$ |
| Drilling | 2.696 <br> $(0.416)$ | -0.798 <br> $(0.529)$ | 0.428 | 0.938 |
| Sawing | 6.302 <br> $(0.232)$ | -1.602 <br> $(0.465)$ | 0.000 | 0.570 |
| Cleanup | 4.991 <br> $(0.391)$ | -1.703 <br> $(0.248)$ | 0.538 | 0.252 |

Note that model (CED-1) provides separate estimates of $\bullet$ Worker and $\bullet$ Error for plaster and wood substrates, while model (CED-2) provides a common estimate for these two variance components over both substrates. As a result, model (CED-2) can be considered a reduced version of model (CED-1), as it has two fewer parameters. A likelihood ratio testing procedure has been applied to assess the adequacy of the model (CED-2) over model (CED-1). The results of this testing procedure are presented in Table C-7b.

Table C-7b. Results of the Likelihood Ratio Testing Procedure for Comparing Model (CED-2) Relative to Model (CED-1)

| CED <br> Activity | $-2^{*} \log (\mathrm{~L})$ |  |  | Likelihood Ratio Test Statistic | Degrees of Freedom | P- <br> Value |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Model (CED-1): <br> Plaster | Model (CED-1): Wood | $\begin{gathered} \text { Model } \\ \text { (CED-2) } \end{gathered}$ |  |  |  |
| Drilling | 8.2874 | 22.0721 | 35.0591 | 4.6996 | 2 | 0.095 |
| Sawing | 3.7361 | 6.3087 | 12.7690 | 2.7242 | 2 | 0.256 |
| Cleanup | 5.6944 | 0.3614 | 6.1779 | 0.1221 | 2 | 0.941 |

The results of the likelihood ratio testing procedure demonstrate no statistical differences between the two models at the 0.05 level of significance for any of the three CED activities. Therefore, model (CED-2) provides an adequate description of the data while estimating the substrate effect on worker personal exposures to airborne lead.

## C.4.3 Association Between Potential Lead Hazard to Occupants and CED Activity/Substrate Combinations

The goal of the statistical analysis of lead loadings in settled dust samples from stainless steel dustfall collectors (SSDCs) is to characterize the potential lead hazard to occupants that may result from the dust and debris generated by a given CED activity. SSDCs were placed at varying distances from a surface being disrupted by an activity, in order to measure the amount of lead generated by each CED activity. As a result, the effect that distance has on potential lead exposure to occupants that results from a specific CED activity can be estimated.

## Model

For a given experimental unit $E U_{i j k}$ (i.e., the occurrence of activity $i$ within subunit $k$ of dwelling unit j ), the relationship between lead loadings from SSDC samples and distance from activity was expressed by the following linear regression model:
where
$\log \left(\right.$ Dust $\left._{\mathrm{ijk}}\right)$ is the log-transformed dust lead loading $\left(\mu \mathrm{g} / \mathrm{ft}^{2}\right)$ associated with the $\mathrm{l}^{\text {th }}$ SSDC sample occurring at $\mathrm{EU}_{\mathrm{ijj}}$;

-     * ${ }_{0(\mathrm{jik})}$ is the unknown intercept term;
- ${ }_{1(\mathrm{ijk})}$ is the unknown slope term, relating the change in $\log \left(\right.$ Dust $\left._{\mathrm{ijkk}}\right)$ associated with a unit change in distance;

Distance $_{\mathrm{ijkk}}$ is the distance that the $\mathrm{l}^{\mathrm{th}} \mathrm{SSDC}$ has been placed from the surface being disrupted by the activity in $\mathrm{EU}_{\mathrm{ijj}}$; and

Error $_{\mathrm{ijkl}}$ is a random term representing replicate variability and measurement error, having standard deviation ${ }^{\text {E }}$ Error(ijk).

Note that model (CED-3) expresses the untransformed lead loading data as an exponential function:

$$
\begin{equation*}
\text { Dust } \left._{\mathrm{ijk} \mid}=\exp \left\{\cdot{ }^{*}{ }_{0(\mathrm{jik})}\right\} \bullet \exp \left\{\bullet{ }^{*}{ }_{1(\mathrm{j}, \mathrm{k})} \bullet \text { Distance }_{\mathrm{ijk}}\right\}\right\}^{\bullet} \mathrm{e}_{\mathrm{ijkl}} \tag{CED-4}
\end{equation*}
$$

where $\mathrm{e}_{\mathrm{ijkl}}$ represents multiplicative error in the model.

Although model (CED-3) implies separate fits to data for each experimental unit $E U_{\mathrm{ijk}}$, our goal is to determine an overall relationship between lead loadings and distance from activity for an entire CED activity/substrate combination. Two approaches were used to achieve this goal:

1. Two Stage Model Approach. Fit model (CED-3) independently to data for each experimental unit $E U_{\mathrm{ijk}}$. We then assume that the vectors of parameter estimates $\left({ }^{*}{ }_{0(\mathrm{ijk})},{ }^{\wedge^{*}}{ }_{1(\mathrm{ijk})}\right)$ obtained from each fit are a set of independent and identically distributed observations from a multivariate normal distribution with mean $\left(\bullet{ }_{0 i}, \bullet{ }_{1 i}\right)$ and covariance matrix $\cdot{ }^{*}$. The mean and covariance matrix are estimated based on the observed parameter estimates.
2. Population Model Approach. The following random effects model is fit separately for each combination of CED activity and substrate (denoted by i):

$$
\begin{equation*}
\log \left(\text { Dust }_{\mathrm{ijk}}\right)=\bullet_{0 \mathrm{i}}+^{\bullet}{ }_{1 \mathrm{i}}^{\bullet} \text { Distance }_{\mathrm{ijk} \mid}+\mathrm{R}_{0 \mathrm{j} \mathrm{k}}+\mathrm{R}_{1 \mathrm{ijk}} \bullet \text { Distance }_{\mathrm{ijk} \mid}+\mathrm{e}_{\mathrm{ijk} \mid}, \tag{CED-5}
\end{equation*}
$$

where, in addition to the terms in model (CED-3),

- ${ }_{0 \mathrm{i}}$ is the population average intercept for activity i ;
- ${ }_{1 \mathrm{i}}$ is the population average slope relating $\log \left(\right.$ Dust $\left._{\mathrm{ijkl}}\right)$ to Distance $_{\mathrm{ijkl}}$ for activity i ,
$\mathrm{R}_{0 \mathrm{ijk}}=\left(\bullet{ }_{0(\mathrm{ijk})}{ }^{\bullet}{ }_{0 \mathrm{i}}\right)$ is a random effect representing the difference between $\bullet{ }_{0 \mathrm{i}}$ and
- **(jij) (the intercept for $\mathrm{EU}_{\mathrm{ijk}}$ under model (CED-3));
$\mathrm{R}_{1 \mathrm{ijk}}=\left(\bullet{ }^{*}{ }_{1(\mathrm{jik})} \bullet_{1 \mathrm{i}}\right)$ is a random effect representing the difference between ${ }^{1 \mathrm{i}}$ and - ${ }_{1(\mathrm{ijk})}$ (the slope for $\mathrm{EU}_{\mathrm{ijk}}$ under model (CED-3)); and
$\mathrm{e}_{\mathrm{ijkl}}$ is the error term associated with this model.
Across experimental units, the vectors $\left(\mathrm{R}_{0 \mathrm{ijk}}, \mathrm{R}_{1 \mathrm{ijk}}\right)$ are assumed to be independent and bivariatenormally distributed with mean $(0,0)$ and covariance ${ }^{\text {Ri. }}$. In addition, the error term $\mathrm{e}_{\mathrm{ijkl}}$ is assumed to be normally distributed with mean zero and standard deviation ${ }^{\bullet}$ Error (i).


## Results

Both approaches were applied to the settled dust data for each CED activity/substrate combination to obtain an overall estimate of the linear relationship between log-transformed lead loading and distance from activity. The results are given in Table C-8.

Table C-8 shows that the slope and intercept estimates and their associated standard errors are very consistent between the two statistical approaches for each CED activity/substrate combination. As a result, the population model approach (i.e., fitting model (CED-5)) was taken in the final characterization.

The estimated relationship between lead loading and distance for a given CED activity was later used to quantify the amount of lead disturbed in a 6'x1' dustfall gradient from the surface being disrupted. The dustfall gradient approach is presented in Section C.5.

Table C-8. Estimates of the Intercept and Slope (and Associated Standard Errors) from the Two Stage and the Population Models of Settled Dust Lead Loading as a Function of Distance

|  |  |  | Two Stage Approach |  | Population Model Approach |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Target Activity | Substrate | Number of $\mathrm{EU}_{\mathrm{ijk}}$ 's | $\left(\operatorname{se}\left({ }^{0 \boldsymbol{i}}{ }_{0 \mathrm{i}}\right)\right)$ | $\left(\operatorname{se}\left(\cdot^{1 i}{ }_{1 i}\right)\right)$ | $\stackrel{\bullet 0 i}{\left(\operatorname{se}\left({ }^{\circ}{ }_{0 i}\right)\right)}$ | $\stackrel{\bullet}{\left(\operatorname{se}\left(\cdot{ }_{1 i}\right)\right)}$ |
| Drilling | Plaster | 4 | $\begin{array}{r} 10.596 \\ (1.133) \\ \hline \end{array}$ | $\begin{array}{r} -1.718 \\ (0.368) \\ \hline \end{array}$ | $\begin{array}{r} 10.484 \\ (1.096) \\ \hline \end{array}$ | $\begin{gathered} -1.671 \\ (0.344) \\ \hline \end{gathered}$ |
| Drilling | Wood | 7 | $\begin{array}{r} 12.921 \\ (0.497) \end{array}$ | $\begin{array}{r} -1.486 \\ (0.083) \\ \hline \end{array}$ | $\begin{aligned} & 12.877 \\ & (0.602) \end{aligned}$ | $\begin{gathered} -1.472 \\ (0.121) \\ \hline \end{gathered}$ |
| Sawing | Plaster | 2 | $\begin{array}{r} 11.286 \\ (1.250) \\ \hline \end{array}$ | $\begin{gathered} -0.941 \\ (0.141) \\ \hline \end{gathered}$ | $\begin{array}{r} 11.249 \\ (1.203) \\ \hline \end{array}$ | $\begin{gathered} -0.929 \\ (0.247) \\ \hline \end{gathered}$ |
| Sawing | Wood | 6 | $\begin{aligned} & 12.631 \\ & (0.472) \\ & \hline \end{aligned}$ | $\begin{array}{r} -0.668 \\ (0.117) \\ \hline \end{array}$ | $\begin{array}{r} 12.631 \\ (0.474) \\ \hline \end{array}$ | $\begin{array}{r} -0.668 \\ (0.117) \\ \hline \end{array}$ |
| Abrasive Sanding | Wood | 3 | $\begin{array}{r} 11.576 \\ (0.757) \\ \hline \end{array}$ | $\begin{array}{r} -0.350 \\ (0.025) \\ \hline \end{array}$ | $\begin{array}{r} 11.522 \\ (0.737) \\ \hline \end{array}$ | $\begin{array}{r} -0.342 \\ (0.047) \\ \hline \end{array}$ |
| Door Modification | Wood | 6 | $\begin{array}{r} 11.126 \\ (0.795) \\ \hline \end{array}$ | $\begin{gathered} -0.422 \\ (0.098) \\ \hline \end{gathered}$ | $\begin{array}{r} 11.099 \\ (0.707) \\ \hline \end{array}$ | $\begin{array}{r} -0.417 \\ (0.094) \\ \hline \end{array}$ |
| HVAC Removal | Duct | 2 | $\begin{gathered} 7.951 \\ (2.304) \\ \hline \end{gathered}$ | $\begin{gathered} -0.351 \\ (0.214) \\ \hline \end{gathered}$ | $\begin{gathered} 8.080 \\ (2.207) \\ \hline \end{gathered}$ | $\begin{array}{r} -0.375 \\ (0.226) \\ \hline \end{array}$ |
| Demolition | Plaster | 9 | $\begin{array}{r} 9.218 \\ (1.062) \\ \hline \end{array}$ | $\begin{array}{r} -0.320 \\ (0.114) \\ \hline \end{array}$ | $\begin{gathered} 8.775 \\ (0.839) \\ \hline \end{gathered}$ | $\begin{array}{r} -0.263 \\ (0.071) \\ \hline \end{array}$ |

## C.4.4 Differences in the Relationship Between Lead in Settled Dust and Distance that can be Attributed to Substrate (Plaster Versus Wood)

Model (CED-5) in the previous subsection was fitted to SSDC lead loadings for a given combination of CED activity and substrate to characterize the relationship between lead loading and distance from the activity. For two of the activities (drilling and sawing), separate modeling results were obtained for wood and plaster substrates. For these activities, it is desired to estimate differences in the relationship with distance that is attributable to wood versus plaster substrates.

## Model

The following model was fit separately for drilling and sawing activities to characterize differences due to substrate:

$$
\begin{aligned}
& +\left[1-\text { Plaster }_{\mathrm{ijk}}\right]\left[\mathrm{R}^{(\mathrm{W})}{ }_{\text {oijk }}+\mathrm{R}^{(\mathrm{W})}{ }_{1 \mathrm{ijk}} \bullet \text { Distance }_{\mathrm{ijk}}\right]+\text { Plaster }_{\mathrm{ijk}}\left[\mathrm{R}^{(\mathrm{P})}{ }_{\text {oijk }}\right. \text { CED-6 } \\
& \left.+\mathrm{R}^{(P)}{ }_{1 \mathrm{jk}} \cdot \text { Distance }_{\mathrm{ijk}}\right]+\mathrm{e}_{\mathrm{ijk} \mathrm{l}} \text {, }
\end{aligned}
$$

where
$\log \left(\right.$ Dust $\left._{\mathrm{ijk}}\right)$ is the log-transformed dust lead loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) associated with the $\mathrm{l}^{\text {th }}$ SSDC sample occurring at $\mathrm{EU}_{\mathrm{ij} \mathrm{j}}$;

- ${ }^{(W)}{ }_{0 \mathrm{i}}$ is the population average intercept for activity i when performed on wood surfaces;
- ${ }^{(\mathrm{W})}{ }_{1 \mathrm{i}}$ is the population average slope relating $\log \left(\right.$ Dust $\left._{\mathrm{ijk}}\right)$ to Distance $_{\mathrm{ijkl}}$ for activity i when performed on wood surfaces;

Distance $_{\mathrm{ijkk}}$ is the distance that the $\mathrm{l}^{\mathrm{th}} \mathrm{SSDC}$ has been placed from the surface being disrupted by the activity in $\mathrm{EU}_{\mathrm{ijk}}$;

Plaster $_{\mathrm{ijk}}=1$ if $\mathrm{EU}_{\mathrm{ijk}}$ corresponds to performing an activity that disturbed a painted plaster surface, and equals zero otherwise;

- ${ }^{(\text {P-W }}{ }_{0 \mathrm{i}}$ is the population average difference in intercept attributable to substrate (PlasterWood) for activity i ;
- ${ }^{(P-W)}{ }_{1 \mathrm{i}}$ is the population average difference in slope relating $\log \left(\right.$ Dust $\left._{\mathrm{i} j \mathrm{k} k}\right)$ to Distance $\mathrm{i}_{\mathrm{ijk} 1}$ attributable to substrate (Plaster-Wood) for activity i;
$\mathrm{R}^{(\mathrm{W})}{ }_{0 \mathrm{jikk}}=\left(\bullet{ }^{*}{ }_{0(\mathrm{jik})} \bullet{ }^{(\mathrm{W})}{ }_{0 \mathrm{i})}\right.$ is a random effect which explains the difference between $\bullet{ }^{(\mathrm{W}}{ }_{0 \mathrm{i}}$ and - ${ }_{0(\mathrm{ijk})}$ (the intercept in model (CED-3) for $\mathrm{EU}_{\mathrm{ijk}}$ );
$\mathrm{R}^{(\mathrm{W})}{ }_{0 \mathrm{ijk}}=\left(\bullet{ }^{*}{ }_{1(\mathrm{jik})} \bullet{ }^{(\mathrm{W})}{ }_{1 \mathrm{ij}}\right)$ is a random effect which explains the difference between $\bullet{ }^{(\mathrm{W})}{ }_{1 \mathrm{i}}$ and - ${ }_{1(\mathrm{jijk})}\left(\right.$ the slope in model (CED-3) for $\left.\mathrm{EU}_{\mathrm{ijk}}\right)$;
$\mathrm{R}^{(\mathrm{P})}{ }_{0 \mathrm{ijk}}=\left(\bullet{ }_{0(\mathrm{jjk})} \bullet^{(\mathrm{P})}{ }_{0 \mathrm{i}}\right)$ is a random effect which explains the difference between $\bullet{ }^{(\mathrm{P})}{ }_{0 \mathrm{i}}$ and - ${ }_{0(\mathrm{jijk})}$;
$\mathrm{R}^{(\mathrm{P})}{ }_{0 \mathrm{ijk}}=\left(\bullet{ }^{*}{ }_{1(\mathrm{jijk})}{ }^{\bullet}{ }^{(\mathrm{P})}{ }_{1 \mathrm{i}}\right)$ is a random effect which explains the difference between $\bullet{ }^{(\mathrm{P})}{ }_{1 \mathrm{i}}$ and - ${ }_{1(\mathrm{j} \mathrm{j} \mathrm{k}}$; and
$\mathrm{e}_{\mathrm{ijkl}}$ is the error term.

The vectors of random effects $\left(\mathrm{R}^{(\mathrm{W})}{ }_{0 \mathrm{ijk}}, \mathrm{R}^{(\mathrm{W})}{ }_{\text {lijk }}\right)$ are assumed to be independent and bivariatenormally distributed with mean $(0,0)$ and covariance matrix ${ }^{\mathrm{R}(\mathrm{W})}$. The vector random effects $\left(\mathrm{R}^{(\mathrm{P})}{ }_{0 \mathrm{ijk}}, \mathrm{R}^{(\mathrm{P})}{ }_{1 \mathrm{ijk}}\right)$ are assumed to be independent and bivariate-normally distributed with mean $(0,0)$ and covariance matrix ${ }^{{ }_{R}(P) i}$. The error term $\mathrm{e}_{\mathrm{ijkl}}$ is assumed to be normally distributed with mean zero and standard deviation ${ }^{\bullet}$ Error (i).

## Results

Table C-9a presents the parameter estimates that result from fitting model (CED-6) to lead loading data separately for drilling and sawing activities.

Table C-9a. Parameter Estimates from Fitting Model (CED-6) to Settled Dust Lead Loadings for Drilling and Sawing Activities

Model CED-6:

$$
\begin{aligned}
& \text { Distance } \left.e_{i j k}\right]+e_{i j k 1}
\end{aligned}
$$

| CED <br> Activity | - ${ }^{(W)}{ }_{0}$ | - ${ }^{(1)}{ }_{1 i}$ | - ${ }^{(P-W)}{ }_{0 i}$ | - ${ }^{(P-W)}{ }_{1 i}$ | $\begin{aligned} & \mathbf{R}^{(W)}{ }_{\text {oijk }} \\ & \text { Std Dev. } \end{aligned}$ | $\begin{gathered} \mathbf{R}^{(\mathrm{W})}{ }_{1{ }_{1 i \mathrm{j}}} \\ \text { Std Dev. } \end{gathered}$ | $\begin{gathered} \mathbf{R}^{(\mathrm{P})_{0 i j k}} \\ \text { Std Dev. } \end{gathered}$ |  | - Error (i) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Drilling | $\begin{aligned} & 12.884 \\ & (0.558) \\ & \hline \end{aligned}$ | $\begin{gathered} -1.474 \\ (0.110) \\ \hline \end{gathered}$ | $\begin{array}{r} -2.536 \\ (1.175) \\ \hline \end{array}$ | $\begin{array}{r} -0.133 \\ (0.321) \\ \hline \end{array}$ | 0.543 | 0.000 | 1.490 | 0.422 | 1.402 |
| Sawing | $\begin{array}{r} 12.631 \\ (0.553) \\ \hline \end{array}$ | $\begin{gathered} -0.668 \\ (0.127) \\ \hline \end{gathered}$ | $\begin{array}{r} -1.350 \\ (1.342) \\ \hline \end{array}$ | $\begin{array}{r} -0.271 \\ (0.254) \\ \hline \end{array}$ | 0.501 | 0.179 | 1.282 | 0.000 | 1.253 |

Note that model (CED-5) provides separate estimates of $\bullet$ Error for plaster and wood substrates, while model (CED-6) provides a common estimate over both substrates. As a result, model (CED-6) can be considered a reduced version of model (CED-5), as it has one fewer parameter. A likelihood ratio testing procedure has been applied to assess the adequacy of the model (CED-6) over model (CED-5). The results of this testing procedure are presented in Table C-9b.

Table C-9b. Results of the Likelihood Ratio Testing Procedure for Comparing Model (CED-6) to Model (CED-5)

|  | -2*log(L) |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CED <br> Clivity | Model (CED- <br> 6): <br> Plaster | Model (CED- <br> 6): <br> Wood | Model (CED- <br> 5) | Likelihood <br> Ratio Test <br> Statistic | Degrees of <br> Freedom | P-Value |
| Drilling | 69.8120 | 135.3740 | 208.0132 | 2.8272 | 1 | 0.093 |
| Sawing | 36.6159 | 102.2258 | 139.8868 | 1.0451 | 1 | 0.307 |

The results of the likelihood ratio testing procedure demonstrate no statistical differences between the two models at the 0.05 level of significance for either CED activity. As a result, model (CED-6) provides an adequate description of the data while estimating the substrate effect on potential occupant exposures to lead in settled dust.

## C.4.5 Investigating the Substrate Effect on Worker Personal Exposure Monitoring Results after Adjusting for the Effects of Pre-activity Paint Lead Loading

For three CED activities (drilling, sawing, and cleanup), model (CED-2) presented in Section C.4.2 investigated the difference in worker exposure to airborne lead that is attributable to substrate effects (wood versus plaster). The results of that analysis demonstrated a potential substrate effect, although it was not statistically significant at the 0.05 level. One cause for the substrate effect was higher paint lead loadings on wood surfaces in comparison to plaster surfaces. By adjusting model (CED-2) to include an effect of paint lead loading, we can investigate whether this cause is appropriate.

## Model

The following random effects model, fit separately to each of the three activities (denoted by i ), was used to measure differences in the response of worker exposure to airborne lead that are attributable to substrate after adjusting for the effect of paint lead loading:

$$
\begin{equation*}
\log \left(\text { PEM }_{\mathrm{ijk}}\right)=\mu_{\mathrm{i}}+\bullet_{0 \mathrm{i}}^{\bullet} \text { Paint }_{\mathrm{ijk}}+\cdot{ }_{\mathrm{i}} \text { Plaster }_{\mathrm{ijk}}+\text { Worker }_{l}+\mathrm{e}_{\mathrm{ijk}}, \tag{CED-7}
\end{equation*}
$$

where the model terms have the same interpretation as in model (CED-2), with the following addition:
${ }^{-}{ }_{0 i}$ measures the effect of paint lead loading on the $\log (\mathrm{PEM})$ response for activity i .

## Results

Table C-10 presents the parameter estimates and associated standard errors from model (CED-7).

Table C-10. Parameter Estimates from Fitting Model (CED-7) to Personal Exposure Results for Drilling, Sawing, and Cleanup Activities

Model CED-7: $\log \left(\right.$ PEM $\left._{\mathrm{ijk}}\right)=\mu_{\mathrm{i}}+{ }^{\bullet}{ }_{0} \bullet$ Paint $_{\mathrm{ijk}}+{ }^{\bullet}{ }_{1 \mathrm{i}}$ Plaster $_{\mathrm{ijk}}+$ Worker $_{\mathrm{l}}+\mathrm{e}_{\mathrm{ijk}}$

| CED Activity | Parameter estimates (standard errors in parentheses) |  |  | - Worker (i) | - Error (i) |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | $\mu_{i}$ | - 0 | ${ }^{1 i}$ |  |  |
| Drilling | 1.916 (0.593) | 0.109 (0.064) | -0.374 (0.602) | 0.079 | 0.938 |
| Sawing | 6.238 (0.508) | 0.009 (0.061) | -1.556(0.597) | 0.000 | 0.623 |

## C.4.6 Investigating the Substrate Effect on the Relationship Between Lead Loading in Settled Dust and Distance After Adjusting for the Effects of Pre-Activity Paint Lead Loading

For two CED activities (drilling and sawing), model (CED-6) presented in section C.4.4 investigated the difference in lead loadings from SSDC samples that is attributable to substrate (wood versus plaster). The results of that analysis demonstrated a potential substrate effect, although it was not statistically significant at the 0.05 level, indicating higher lead loadings in settled dust for activities which disturbed a lead-painted wood surface. One cause for the substrate effect was higher paint lead loadings on wood surfaces in comparison to plaster surfaces. By adjusting model (CED-2) to include an effect of paint lead loading, we can investigate whether this cause is appropriate.

## Model

The following model was used to measure differences in lead loadings from SSDCs that are attributable to substrate within drilling and sawing activities (denoted by i), after adjusting for the effect of paint lead loading:

$$
\begin{align*}
& \log \left(\text { Dust }_{\mathrm{ijk}}\right)=\cdot{ }^{(\mathrm{W})}{ }_{\mathrm{Oi}}+\cdot{ }^{(\mathrm{W})}{ }_{1 \mathrm{i}} \cdot \text { Distance }_{\mathrm{ijk}}+\text { Plaster }_{\mathrm{ijk}}\left[0^{(\mathrm{P}-\mathrm{W})}{ }_{\mathrm{i}}+\cdot{ }^{(\mathrm{P}-\mathrm{W})}{ }_{1 \mathrm{i}} \cdot\right.  \tag{CED-8}\\
& \text { Distance } \left._{i j k l}\right]+\cdot{ }^{\bullet} \text { Paint }_{i j k}+\left[1-\text { Plaster }_{\mathrm{ijk}}\right]\left[R^{(\mathbb{W})}{ }_{0 j \mathrm{jk}}+\mathrm{R}^{(\mathrm{W})}{ }_{1 \mathrm{ijk}} \cdot\right. \\
& \text { Distance } \left._{i \mathrm{ijk}}\right]+ \text { Plaster }_{\mathrm{ijk}}\left[\mathrm{R}^{(P)}{ }_{\text {ojk }}+\mathrm{R}^{(P)}{ }_{1 \mathrm{ijk}}{ }^{\bullet} \text { Distance } \mathrm{e}_{\mathrm{ijk}}\right]+\mathrm{e}_{\mathrm{ijkl}} \text {, }
\end{align*}
$$

where the model terms have the same interpretation as in model (CED-6), with the following addition:

- ${ }_{i}$ measures the effect of paint lead loading on the log-transformed lead loading for activity i.


## Results

Table C-11 presents the parameter estimates that result from fitting model (CED-8) to drilling and sawing activity data.

## Table C-11. Parameter Estimates from Fitting Model (CED-8) to SSDC Lead Loading Data for Drilling and Sawing Activities

## Model CED-8:


 $R^{(P)_{1 j k}} \cdot$ Distance $_{i j k]}+\mathrm{e}_{\mathrm{ijk}}$

| CED <br> Activity | - ${ }^{(W)}{ }_{0}$ | - ${ }^{(W)}{ }_{1 i}$ | - ${ }^{(P-W)}{ }_{0 i}$ | - ${ }^{(P-W)}{ }_{1 i}$ | - ${ }^{\text {i }}$ | $\begin{aligned} & \mathbf{R}^{(\mathrm{W})}{ }_{\text {oijk }} \\ & \text { Std Dev. } \end{aligned}$ | $\begin{gathered} \mathbf{R}^{(\mathrm{W})}{ }_{1 i \mathrm{ijk}} \\ \text { Std Dev. } \end{gathered}$ | $\mathbf{R}^{(P)}{ }_{0 \text { Dijk }}$ <br> Std Dev. | $\mathrm{R}^{\mathbf{R}^{(\mathrm{P})}{ }_{1 \mathrm{lijk}}}$ | - Error (i) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Drilling | $\begin{aligned} & 10.991 \\ & (0.980) \\ & \hline \end{aligned}$ | $\begin{array}{r} -1.480 \\ (0.314) \\ \hline \end{array}$ | $\begin{array}{r} -0.730 \\ (1.329) \\ \hline \end{array}$ | $\begin{array}{r} -0.160 \\ (0.412) \\ \hline \end{array}$ | $\begin{gathered} 0.258 \\ (0.114) \\ \hline \end{gathered}$ | 0.520 | 0.047 | 1.415 | 0.363 | 1.301 |
| Sawing | $\begin{array}{r} 11.554 \\ (0.724) \\ \hline \end{array}$ | $\begin{array}{r} -0.668 \\ (0.128) \\ \hline \end{array}$ | $\begin{array}{r} -0.595 \\ (1.359) \\ \hline \end{array}$ | $\begin{array}{r} -0.268 \\ (0.278) \\ \hline \end{array}$ | $\begin{gathered} 0.148 \\ (0.066) \\ \hline \end{gathered}$ | 0.488 | 0.186 | 1.260 | 0.000 | 1.236 |

## C. 5 QUANTIFYING LEAD DISTURBANCE IN A 6' X 1' DUSTFALL GRADIENT

As stated earlier, the goal of the statistical analysis of settled dust lead-loadings is to determine the potential occupant exposure to lead which results from each R\&R activity. Fitting the models in Sections C. 3 and C. 4 resulted in a prediction curve for each R\&R activity. This curve predicts the average amount of lead in settled dust that is expected to fall within different distance intervals. For the $\mathrm{i}^{\text {th }}$ activity, this curve has the following form:

$$
\text { Lead in Dust }\left(\mu \mathrm{g} / \mathrm{tt}^{2}\right)=\exp \left(\cdot{ }_{0 i}\right) \cdot \exp \left(\cdot{ }_{1 i} \cdot \text { Distance }\right)
$$

and is estimated by estimating the model parameters ${ }^{0}{ }_{0 \mathrm{i}}$ and ${ }^{1 \mathrm{i}}$. By integrating two areas underneath this estimated curve, we obtain two estimates of lead disturbance:

- area underneath the curve from zero to one foot distance from the activity (i.e., an estimate of the expected lead-loading of an SSDC located adjacent to the activity).
- area underneath the curve from five to six feet distance from the activity.

The measure that was chosen to represent the potential occupant exposure to lead in settled dust for each CED Activity is a $6^{\prime} \times 1^{\prime}$ gradient lead-loading, which is obtained by integrating the area underneath the estimated curve from zero to six feet distance from the activity.

The parameter estimates ${ }^{\wedge}{ }_{0 i}$ and ${ }^{\wedge}{ }_{1 \mathrm{i}}$ are obtained from a random effects regression model. We assume that they jointly follow a multivariate normal distribution with mean $\left(\bullet_{0 \mathrm{i}}\right.$ and $\left.\bullet_{1 \mathrm{i}}\right)$ and covariance $\bullet .{ }_{\mathrm{i}}$. To obtain an estimate of the $6^{\prime} \times 1^{\prime}$ gradient lead-loading (and associated
standard error) for each CED activity we used the Multivariate Delta Method (Bishop, Fienberg and Holland 1975, page 492):

If $\left(\mathrm{X}_{1}, \mathrm{X}_{2}\right)$ follow a multivariate normal distribution with mean $\left(\bullet_{1},{ }_{2}\right)$ and variance • , then a continuous and differentiable function of $\mathrm{X}_{1}$ and $\mathrm{X}_{2}, \mathrm{f}\left(\mathrm{X}_{1}, \mathrm{X}_{2}\right)$ has the following asymptotic distribution:
$f\left(X_{1}, X_{2}\right)$ is asymptotically distributed with mean $f\left(\bullet{ }_{1},{ }_{2}\right)$ and variance $\left[\mathrm{df} / \mathrm{d}\left(\bullet{ }_{1},{ }_{2}\right)\right] \bullet\left[\mathrm{df} / \mathrm{d}\left(\bullet_{1},{ }_{2}\right)\right]{ }^{\prime}$.

In our estimates of the $6^{\prime} \times 1^{\prime}$ gradient lead-loading (and associated standard error) for each CED activity, $\mathrm{f}\left({ }_{0 \mathrm{oi}},{ }_{\mathrm{ij}}\right)$ has the following form:

$$
f\left(\hat{(0 ; ~}_{0 ;} \hat{1}_{1 i}\right) \hat{0}_{0}^{6} \exp \left(\hat{( }_{0 i} \hat{\quad}_{1 i} x\right) d x \frac{\exp \left(\hat{0}_{0 i} \quad 6 \hat{1}_{1 i}\right) \exp \left(\hat{0}_{0 i}\right)}{\hat{1}_{1 i}}
$$

and $\left[\mathrm{df} / \mathrm{d}\left(\bullet_{0 \mathrm{i}},{ }_{1 \mathrm{i}}\right)\right]$ has the following form:

The estimated $6^{\prime} \times 1$ ' gradient lead-loadings for each CED activity/subtask combination was estimated as $\mathrm{f}\left({ }^{\wedge}{ }_{0 \mathrm{i}},{ }_{1 \mathrm{i}}\right)$ and their associated standard deviations were estimated as the square root of $\left[\mathrm{df} / \mathrm{d}\left({ }^{\wedge}{ }_{0 i},{ }_{1 \mathrm{i}}\right)\right] \bullet\left[\mathrm{df} / \mathrm{d}\left({ }^{\wedge}{ }_{0 \mathrm{i}},{ }_{1 \mathrm{i}}\right)\right]$. The estimated $[0-1]$ and [5-6] foot SSDC and their associated standard deviations were estimated by adjusting the limits of integration on the function $\mathrm{f}\left(\bullet_{0 \mathrm{i}} \bullet_{\mathrm{li}}\right)$ and adjusting df/d $\left({ }_{0 \mathrm{i}}{ }^{\bullet}{ }_{1 \mathrm{i}}\right)$ accordingly.

## C. 6 METHODOLOGY UNDERLYING NORMAL DISTRIBUTION THEORY CONFIDENCE INTERVALS, CONFIDENCE INTERVAL FOR A PERCENTILE, AND CONFIDENCE INTERVAL FOR THE PROPORTION LESS (GREATER) THAN A SPECIFIED VALUE

This section discusses the methodology underlying the calculation of confidence intervals on distribution percentiles and on the probability of being less (greater) than a specified level. This methodology is applied to the (natural) logarithms of personal exposure lead concentrations ( $\mu \mathrm{g} / \mathrm{m}^{3}$ of air). Since air volume is proportional to sampling time, these loadings are effectively adjusted for sampling time. Confidence intervals are constructed for each R\&R activity.

The confidence interval procedures are based on components of variance models having either one, two, or three variance components. The appropriate model was determined by those variance components that could be estimated from the available data. The variance components within these models are as follows:

Model \#1
(one variance component): Worker-to-worker

## Model \#2

(two variance components): Unit-to-unit
Worker-to-worker within units

```
Model #3
(three variance components): Unit-to-unit
Worker-to-worker within units
Replicate variability within workers
```

The only activity where three variance components can be estimated is demolition.
For each activity where the two- and three-variance component models are appropriate, it is assumed that the data sets are (approximately) balanced or nearly balanced (i.e., the number of workers within units is (approximately) the same across units and the number of replicate determinations within workers is (approximately) the same across workers within units). If the data sets are only nearly balanced, we use the harmonic mean of levels (e.g. workers within units) in the confidence interval calculations.

## Models

The forms of the variance component models are as follows:

## One Variance Component Model:

$$
\mathrm{Y}_{\mathrm{k}}=\mu+\mathrm{e}_{\mathrm{k}} \quad \mathrm{k}=1, \ldots, \mathrm{n} \quad \mathrm{Y}_{\mathrm{k}} \bullet \quad \operatorname{ind} \mathrm{~N}\left(\mu, \cdot{ }_{\mathrm{e}}{ }^{2}\right)
$$

## Two Variance Components Model:

$$
\begin{aligned}
& \mathrm{Y}_{\mathrm{ij}}=\mu+\mathrm{h}_{\mathrm{i}}+\mathrm{w}_{\mathrm{j}(\mathrm{i})} \mathrm{i}=1, \ldots, \mathrm{I} ; \mathrm{j}=1, \ldots, \mathrm{~J} \\
& \mathrm{~h}_{\mathrm{i}} \bullet \text { ind } \mathrm{N}\left(0,{ }_{\mathrm{h}}{ }^{2}\right) ; \quad \mathrm{w}_{\mathrm{j}(\mathrm{i})} \bullet \\
& \text { ind } \mathrm{N}\left(0,{ }^{2}{ }^{2}\right)
\end{aligned}
$$

## Three Variance Components Model:

$$
\begin{array}{ll}
\mathrm{Y}_{\mathrm{ijk}}=\mu+\mathrm{h}_{\mathrm{i}}+\mathrm{w}_{\mathrm{j}(\mathrm{i})}+\mathrm{e}_{\mathrm{ijk}} & \mathrm{i}=1, \ldots, \mathrm{I} ; \mathrm{j}=1, \ldots, \mathrm{~J} ; \mathrm{k}=1, \ldots, \mathrm{n} \\
& \mathrm{~h}_{\mathrm{i}} \bullet \text { ind } \mathrm{N}\left(0, \bullet{ }_{\mathrm{h}}{ }^{2}\right) ; \\
& \mathrm{w}_{\mathrm{j}(\mathrm{j})} \bullet \text { ind } \mathrm{N}\left(0,{ }^{2}{ }^{2}\right) ; \\
& \mathrm{e}_{\mathrm{ijj}} \bullet \text { ind } \mathrm{N}\left(0,{ }^{{ }^{2}}{ }^{2}\right)
\end{array}
$$

## C.6.1 Normal Theory Two-Sided 100(1-•) Percent Confidence Interval on the p-th Distribution Percentile

One objective of the analysis of personal exposure data is to compare (across activities) potential lead exposures associated with each R\&R activity. This is done by summarizing the distribution of personal exposure data for each activity by a single summary statistic, and estimating the error associated with the statistic. This statistic has been taken to be the 75th percentile of the distribution. The same methods were used to estimate the 50th and 95th percentiles as well. This section presents the statistical approach taken to calculate confidence intervals on these estimated distribution percentiles.

The (1-•)* $100 \%$ two-sided confidence intervals calculated in this section are based on the noncentral Student-t distribution. The methods for calculating these confidence intervals are as follows, according to the variance component model applied to the personal exposure data for a given $R \& R$ activity:

## A. One Variance Component

$$
\begin{array}{ll}
Y_{k}(k 1, \ldots, n) & \text { ind } N\left(u,{ }_{e}^{2}\right) \\
\bar{Y} \cdot \frac{1}{n_{k 1}}{ }^{n} Y_{k} & \bar{Y} . N\left(\mu,{ }_{e}^{2} / n\right) \\
s^{2} \frac{1}{(n 1)_{i 1}}{ }_{i}^{n}\left(Y_{i} \bar{Y} .\right)^{2} & s^{2}{ }_{e}^{2} X^{2} /
\end{array}
$$

where • =n-1 d.f.
Let $\mu+\bullet{ }_{\mathrm{p}}{ }_{\mathrm{e}}$ denote the p-th percentile of the normal distribution, $0 \bullet \mathrm{p} \cdot 1 ; \bullet{ }_{\mathrm{p}}={ }^{-1}(\mathrm{p})$. We wish to place a $100(1-\bullet)$ percent two-sided confidence interval on $\mu+{ }_{\mathrm{p}}^{\bullet}{ }_{\mathrm{e}}$. Determine $\mathrm{k}_{1}$, $\mathrm{k}_{2}$ such that

$$
P\left(\bar{Y} . k_{1} s \mu_{\text {pe }} \bar{Y} . k_{2} s\right) 1
$$

Determine $\mathrm{k}_{1}, \mathrm{k}_{2}$ such that

$$
\begin{aligned}
& P\left(\bar{Y} . k_{1} s>\mu_{p e}\right) / 2 \\
& \mathrm{P}\left(\overline{\mathrm{Y}} . \mathrm{k}_{2} \mathrm{~s}<\mu_{\mathrm{pe}}\right) / 2
\end{aligned}
$$

Rearranging these inequalities implies that

$$
k_{1} \frac{1}{\sqrt{n}} t^{\prime} ; / 2 \quad p \sqrt{n}
$$

is the lower 100•/2 percentile of the noncentral $t$ distribution with $\bullet$ d.f. and noncentrality - ${ }^{\bullet}$. n. Similarly

$$
k_{2} \frac{1}{\sqrt{n}} t^{\prime} ; 1 / 2 \quad p \sqrt{n}
$$

is the upper 100• $/ 2$ percentile of the noncentral $t$ distribution with $\bullet$ d.f. and noncentrality - ${ }_{\mathrm{p}}{ }^{\bullet}$ n. A $100(1-\bullet)$ percent two-sided confidence interval on $\mu+{ }^{\circ}{ }_{\mathrm{p}}{ }^{\bullet}{ }_{\mathrm{e}}$ is thus

$$
\left(\bar{Y} . \frac{1}{\sqrt{n}} t^{\prime} ; / 2 \quad p^{\sqrt{n}} s, \bar{Y} \cdot \frac{1}{\sqrt{n}} t_{; 1 / 2}^{\prime} \quad p^{\sqrt{n}} \quad s\right)
$$

where $\mathrm{t} .\left({ }_{\mathrm{p}}^{\bullet} \mathrm{n}\right)$ represents the noncentral t -distribution with $\bullet=\mathrm{n}-1$ d.f and noncentrality parameter $\cdot{ }_{\mathrm{p}} \bullet \mathrm{n}$, and where $\cdot{ }_{\mathrm{p}}={ }^{-1}(\mathrm{p})$.

## B. Two Variance Components

$$
\begin{aligned}
& Y_{i j}, i=1, \ldots, I ; j=1, \ldots, J \\
& \mathrm{Y}_{\mathrm{ij}}=\mu+\mathrm{h}_{\mathrm{i}}+\mathrm{w}_{\mathrm{j}(\mathrm{i})} \\
& \mathrm{h}_{\mathrm{i}} \cdot \operatorname{ind} \mathrm{~N}\left(0, \bullet{ }_{\mathrm{h}}{ }^{2}\right) ; \mathrm{w}_{\mathrm{j}(\mathrm{i})} \bullet \mathrm{N}\left(0, \bullet{ }_{\mathrm{w}}{ }^{2}\right) ; \mathrm{h}_{\mathrm{i}}, \mathrm{w}_{\mathrm{j}(\mathrm{i})} \text { are independent } \\
& \mathrm{Y}_{\mathrm{ij}} \bullet \mathrm{~N}\left(\mu, \bullet{ }_{\mathrm{h}}{ }^{2}+\bullet{ }_{\mathrm{w}}{ }^{2}\right) \bullet \mathrm{N}\left(\mu,{ }^{2}\right)
\end{aligned}
$$

The mean square among units is MSH, with I-1 df.

$$
\text { MSH } \quad \frac{\mathrm{J}}{\mathrm{I} 1}{ }_{i 1}^{1}\left(\bar{Y}_{\mathrm{i}} \cdot \overline{\bar{Y}}_{\mathrm{Y} . .}\right)^{2} \quad \text { MSH } \quad\left(\begin{array}{lll}
\mathrm{J}_{\mathrm{h}}^{2} & { }_{w}^{2}
\end{array}\right) \quad{ }_{11}^{2} /(\mathrm{I} 1)
$$

The mean square among workers within units is MSW, with $\mathrm{I}(\mathrm{J}-1)$ d.f.

$$
\text { MSW } \frac{1}{l(J 1)}{ }_{i 1 j_{j 1}}^{J}\left(Y_{i j} \overline{\bar{Y}}_{\mathrm{i}} \cdot\right)^{2} \quad \text { MSW } \quad \begin{gathered}
2 \\
w
\end{gathered}
$$

Let

| 2 | 2 | 2 |
| :---: | :---: | :---: |
|  | h | w |
| 2 | ${ }_{\mathrm{h}} / \mathrm{l}$ | ${ }_{\mathrm{w}}^{2} / \mathrm{J}$ |
| $r$ | ${ }_{\mathrm{h}} /{ }^{2}$ |  |

Then $\bullet{ }^{2},{ }^{2}$, and r are estimated as

$$
\begin{aligned}
& \text { ^2 } \frac{1}{J} \text { MSH }\left(\frac{J 1}{J}\right) \text { MSW } \\
& \text { ~2 } \frac{1}{\mathrm{IJ}} \mathrm{MSH} \text {, with I } 1 \text { d.f. } \\
& \text { ̂ } \frac{1}{\mathrm{~J}}\left(\frac{\mathrm{MSH}}{\mathrm{MSW}}\right) \frac{1}{\mathrm{~J}}
\end{aligned}
$$

In analogy with the one variance component case (Section A), we wish to place a 100(1-• ) percent two-sided confidence interval on the p -th percentile of the distribution of Y , namely $\mu+\bullet{ }_{\mathrm{p}}^{\bullet}$, where ${ }^{\bullet}{ }_{\mathrm{p}}=\bullet^{-1}(\mathrm{p})$. Determine $\mathrm{k}_{1}, \mathrm{k}_{2}$ such that

$$
\mathrm{P}\left(\overline{\overline{\mathrm{Y}}} . . \quad \mathrm{k}_{1}{ }^{\wedge} \quad \mu \quad \mathrm{p} \quad \overline{\overline{\mathrm{Y}}} . . \quad \mathrm{k}_{2}{ }^{\wedge}\right) \quad 1
$$

Determine $\mathrm{k}_{1}, \mathrm{k}_{2}$ such that

$$
\begin{array}{llll}
P(\overline{\bar{Y}} . . & k_{1}{ }^{\wedge}>\mu & p) & / 2 \\
P(\overline{\bar{Y}} . . & k_{2}{ }^{\wedge}<\mu & p) & / 2
\end{array}
$$

Rearranging these inequalities implies that

$$
/ 2 \quad \mathrm{P}\left(\frac{\frac{\mu \overline{\overline{\mathrm{Y}}} . .}{} \mathrm{p}^{-}}{\hat{\jmath} /}<\mathrm{k}_{1-} \hat{n}\right)
$$

Assume that ${ }^{\wedge} \wedge$ on the right hand side of this inequality is approximately equal to $\bullet / \bullet$. This is asymptotically correct. Then

$$
\mathrm{k}_{1} \quad \frac{1}{/} \mathrm{t}_{11 ; / 2}^{\prime}\left(\mathrm{p}^{-}\right)
$$

the lower $100 \cdot / 2$ percentile of the noncentral $t$ distribution with I-1 d.f. and noncentrality parameter $\mathrm{p}^{-}$. Estimate •/• by

$$
\hat{\wedge}\left[\frac{\frac{1}{J} \mathrm{MSH}\left(\frac{\mathrm{~J} 1}{J}\right) \mathrm{MSW}}{\frac{1}{\mathrm{IJ}} \mathrm{MSH}}\right]^{1 / 2} \quad\left[\mathrm{IJ}\left(\frac{\hat{r}}{\mathrm{~J} \hat{\mathrm{r}}} 11\right)\right]^{1 / 2}
$$

Similarly

$$
/ 2 \quad \mathrm{P}\left(\frac{\frac{\mu \overline{\overline{\mathrm{Y}}} . .}{} \mathrm{p}^{-}}{\hat{\jmath} /}>\mathrm{k}_{2 \bar{\wedge}} \hat{\wedge}\right)
$$

As above, assume that ${ }^{\wedge}$ on the right hand side of this inequality is approximately equal to - /• . Then

$$
\mathrm{k}_{2} \frac{1}{/} \mathrm{t}_{11 ; 1 / 2}\left(\mathrm{p}^{-}\right)
$$

is the upper $100 \cdot / 2$ percentile of the noncentral $t$ distribution with I-1 d.f. and noncentrality parameter $\mathrm{p}^{-}$. As above,

$$
\wedge \wedge\left[\operatorname{IJ}\left(\begin{array}{ll}
\hat{r} & 1 \\
J \hat{r} & 1
\end{array}\right)\right]^{1 / 2}
$$

## C. Three Variance Components

This case is an extension of the two variance component case.
$Y_{\mathrm{ijk}}, \mathrm{i}=1, \ldots, \mathrm{I} ; \mathrm{j}=1, \ldots, \mathrm{~J} ; \mathrm{k}=1, \ldots, \mathrm{n}$
$\mathrm{Y}_{\mathrm{ijk}}=\mu+\mathrm{h}_{\mathrm{i}}+\mathrm{w}_{\mathrm{j}(\mathrm{i})}+\mathrm{e}_{\mathrm{ijk}}$
$h_{i} \bullet \operatorname{ind} N\left(o, \bullet{ }_{h}{ }^{2}\right) ; \mathrm{w}_{\mathrm{j}(\mathrm{i})} \bullet \mathrm{N}\left(\mathrm{o}, \bullet{ }_{\mathrm{w}}{ }^{2}\right) ; \mathrm{e}_{\mathrm{ijk}} \bullet \mathrm{N}\left(\mathrm{o}, \bullet{ }_{\mathrm{e}}{ }^{2}\right) ; \mathrm{h}_{\mathrm{i}}, \mathrm{w}_{\mathrm{j}(\mathrm{i})}, \mathrm{e}_{\mathrm{ijk}}$ are independent
$\mathrm{Y}_{\mathrm{ijk}} \cdot \mathrm{N}\left(\mu,{ }_{\mathrm{h}}{ }^{2}+\bullet{ }_{\mathrm{w}}{ }^{2}+\bullet{ }_{\mathrm{e}}{ }^{2}\right) \cdot \mathrm{N}\left(\mu,{ }^{2}\right)$

The mean square among units is MSH, with I-1 d.f.

$$
\text { MSH } \quad \frac{J n}{11}_{i 1}^{1}\left(\bar{Y}_{i . .} \quad \overline{\bar{Y}} \ldots\right)^{2} \quad \text { MSH } \quad\left(\mathrm{Jn}_{\mathrm{h}}^{2} \quad \mathrm{n}_{\mathrm{w}}^{2} \quad{ }_{\mathrm{e}}^{2}\right) \quad{ }_{11}^{2} /\left(\begin{array}{ll}
(1)
\end{array}\right.
$$

The mean square among workers within units is MSW, with $\mathrm{I}(\mathrm{J}-1)$ d.f.

$$
\text { MSW } \quad \frac{n}{I(J 1)}_{i 1 j_{j 1}}^{J}\left(\bar{Y}_{i j} . \quad \bar{Y}_{i . .}\right)^{2} \quad \text { MSW } \quad\left(n_{w}^{2} \quad e\right) \quad{ }_{l(J 1)}^{2} / l(J 1)
$$

The mean square among replicate determinations within workers is MSE, with $\mathrm{IJ}(\mathrm{n}-1)$ d.f.

Let

$$
\begin{array}{ccccc}
2 & 2 & 2 & 2 & \\
& { }_{h} & { }_{w} & e \\
2 & { }_{h}^{2} / I & { }_{\mathrm{w}}^{2} / \mathrm{e} & & \\
{ }_{\mathrm{e}} & 2 / \mathrm{IJn}
\end{array}
$$

- ${ }^{2},{ }^{2}$ are estimated as

$$
\begin{aligned}
& \text { ^2 } \frac{\mathrm{MSH}}{\mathrm{Jn}}\left(\frac{\mathrm{~J} 1}{\mathrm{~J}}\right) \frac{\mathrm{MSW}}{\mathrm{n}}\left(\frac{\mathrm{n} 1}{\mathrm{n}}\right) \text { MSE } \\
& \therefore 2 \frac{1}{\mathrm{Jnn}} \mathrm{MSH} \text {, with I } 1 \text { d.f. }
\end{aligned}
$$

In analogy with the previous case of two variance components (Section B), we wish to place a $100(1-\bullet)$ percent two sided confidence interval on the p -th percentile of the distribution of Y, namely $\mu+{ }_{\mathrm{p}}{ }^{\bullet}$, where ${ }^{\mathrm{p}}{ }_{\mathrm{p}}={ }^{-1}(\mathrm{p})$. Determine $\mathrm{k}_{1}, \mathrm{k}_{2}$ such that

$$
\mathrm{P}\left(\overline{\overline{\mathrm{Y}}} \ldots \mathrm{k}_{1}{ }^{\wedge} \quad \mu_{\mathrm{p}} \quad \mathrm{p} \quad \overline{\overline{\mathrm{Y}}} \ldots \mathrm{k}_{2}{ }^{\wedge}\right) \quad 1 \quad / 2
$$

In direct analogy with the two variance component case,

$$
\begin{aligned}
& \mathrm{k}_{1} \frac{1}{(/)} \mathrm{t}_{11}^{\prime} ; / 2(\mathrm{p}-) \\
& \mathrm{k}_{2} \frac{1}{(/)} \mathrm{t}_{11}^{\prime} ; 1 / 2(\mathrm{p}-)
\end{aligned}
$$

Estimate • /• by

$$
\wedge\left[I J\left(\frac{\frac{\mathrm{MSH}}{\mathrm{~J}}\left(\frac{\mathrm{~J} 1}{\mathrm{~J}}\right) \mathrm{MSW} \text { (n 1) MSE }}{\mathrm{MSH}}\right)\right]^{1 / 2}
$$

If $\mathrm{n}=1$ this reduces to the expression for $\wedge^{\wedge}$ in the two variance component case.

## C.6.2 Normal Theory Two-Sided 100(1-•) Percent Confidence Interval on $\mathrm{P}(\mathrm{Y}>\mathrm{a})$

The theory presented in this section is used to calculate a (1-• )* $100 \%$ two-sided confidence interval on the probability that a given random variable $Y$ exceeds a pre-specified threshold value (a), based on assumptions on its underlying distribution. In the EFSS, this method is applied to obtaining confidence intervals on the proportion of workers whose personal exposure sample results exceed the OSHA permissible exposure limit of $50 \mu \mathrm{~g} / \mathrm{m}^{3}$.

Assume that

$$
\mathrm{Y} \mathrm{~N}\left(\mu,{ }^{2}\right)
$$

and let

$$
\mathrm{q} \quad \mathrm{P}(\mathrm{Y}>\mathrm{a}) \quad 1 \quad\left(\frac{\mathrm{a} \mu}{}\right)
$$

Then

$$
\mathrm{p} \quad 1 \mathrm{q} \quad\left(\frac{\mathrm{a} \mu}{}\right)
$$

This implies that

$$
\text { a } \mu \quad \text { p }
$$

where ${ }^{p} \quad{ }^{1}(p)$.
We wish to place a two-sided $100(1-\bullet)$ percent confidence interval on p , and therefore equivalently on $q \cdot 1-\mathrm{p}$. This is the inverse problem to that considered in the previous section.

For each value of $\mathrm{p}, 0<\mathrm{p}<1$, a two-sided $100(1-\bullet)$ percent confidence interval on $\mu+\bullet{ }_{\mathrm{p}}^{\bullet}$ is $\left(\bullet{ }_{1}(\mathrm{p}),{ }_{\mathrm{u}}(\mathrm{p})\right)$ where

$$
\begin{aligned}
& \text { (p) } \bar{Y}\left(\frac{1}{/}\right) t_{; / 2}^{\prime}\left({ }_{p} /\right)^{\wedge} \\
& \text { (p) } \bar{Y} \quad \frac{1}{(/)} t_{; 1 / 2}^{\prime}(p /)^{\wedge}
\end{aligned}
$$

As in the previous section, •/• and • can be expressed as follows, given the variance components model being considered:

One Variance Component: / $\sqrt{\mathrm{n}}, \mathrm{n} 1$
Two Variance Components: $\quad\left[\begin{array}{cc}2 & 2 \\ h & w \\ \hline{ }_{h}^{2} / I & { }_{w} / \mathrm{IJ}\end{array}\right]^{1 / 2}, \quad \mathrm{I} 1$
Three Variance Components: $/\left[\begin{array}{ccc} & 2 & 2 \\ h & { }_{w} & { }^{2} \\ \hline{ }_{h} / l & { }_{w}^{2} / J J & { }_{e}^{2} / I J n\end{array}\right]^{1 / 2}, \quad 11$
and • /• are estimated as discussed previously.
If $\bullet$ is the true (unknown) value of p such that a $\bullet \mu+\bullet . \bullet$, then with probability at least 1-•, the value a will fall within the confidence interval for $\mu+\bullet . \bullet$ The 1-• confidence interval on $\mathrm{p} \cdot \mathrm{P}(\mathrm{Y}<\mathrm{a})$ is thus $\left\{\mathrm{p}:{ }_{1}(\mathrm{p}) \cdot \mathrm{a} \bullet \bullet{ }_{\mathrm{u}}(\mathrm{p})\right\}$. The boundaries $\bullet{ }_{1}(\mathrm{p}),{ }_{\mathrm{u}}(\mathrm{p})$ are each increasing functions of $p$. Therefore, the lower and upper confidence bounds for $p$ are

$$
\begin{aligned}
& \mathrm{p}_{1} \min _{\mathrm{p}} \mathrm{u}^{(\mathrm{p})} \mathrm{a} \min _{\mathrm{p}}\left\{\mathrm{t}_{; 1 / 2}^{\prime}(\mathrm{p}-)\right. \\
& \left.\frac{\mathrm{a} \overline{\mathrm{Y}}}{\sim}(-)\right\} \\
& \mathrm{p}_{\mathrm{u}} \max _{\mathrm{p}} \quad{ }_{1}(\mathrm{p}) \quad \mathrm{a} \\
& \max _{\mathrm{p}}\left\{\mathrm{t}^{\prime} ; / 2(\mathrm{p}-)\right. \\
& \left.\frac{\mathrm{a} \overline{\mathrm{Y}}}{n}(-)\right\}
\end{aligned}
$$

The degrees of freedom, $\bullet$, are $\bullet=\mathrm{n}-1$ in the one variance component case; $\cdot=\mathrm{I}-1$ in the two and three variance component cases (balanced design).

The upper and lower confidence bounds on $q \cdot 1$-p are obtained directly from $p_{1}$ and $p_{u}$. Namely

```
q| 1 pu
qu}1\mp@subsup{p}{l}{
```


## C. 7 MODELS USED TO ESTIMATE MEAN EXPOSURE LEVELS ACROSS STUDIES IN COMBINING OTHER SOURCES OF SURFACE PREPARATION DATA

The individual data points were available for all surface preparation studies located in the search for other sources of data. Therefore within-study and between-study variability could be estimated directly from the data rather than approximated by statistical meta-analytic techniques. To characterize the components of variability in personal worker exposures the following model was fit separately for interior and exterior dry surface preparation:

$$
\begin{equation*}
\log \left(\text { PEM }_{i j}\right)=\mu+\text { Study }_{i}+\text { Worker }_{j} \tag{OS-1}
\end{equation*}
$$

where
$\mathrm{PEM}_{\mathrm{ij}}$ is the personal exposure lead concentration $\left(\mu \mathrm{g} / \mathrm{m}^{3}\right)$ for the jth worker in the ith study
$\mu$ is the mean of the $\log (\mathrm{PEM})$ responses
Study $_{\mathrm{i}}$ is the random effect of the ith study (normally distributed with mean zero and variance ${ }_{\mathrm{s}}^{2}$ )

Worker ${ }_{j}$ is a random effect of the jth Worker (normally distributed with mean zero and variance ${ }_{\mathrm{W}}^{2}$ ).

Parameter estimates for each model fit are presented in Table 7E-4 of Volume 1. Estimates of the 75th and 95th percentiles of the distribution and confidence intervals for the geometric mean, 75th and 95th percentile were calculated according to the methodology presented in Section C. 6 of Appendix C. Likewise, estimates of the percent of workers exceeding the OSHA PEL and their associated 95th confidence interval were calculated according to the methodology presented in Section C. 6 of Appendix C.

APPENDIX D QUALITY CONTROL

## D. 0 QUALITY CONTROL

To ensure that the sampling and analysis protocols employed in the EFSS produced data of sufficient quality, a number of different quality control (QC) samples were included in the study design for each study phase. Field QC samples were intended to help assess variability introduced by the sampling method and to detect potential biases from field sources such as sample transfer and handling. The types of field QC samples collected in this study were:

- Field blanks: Lead-free samples prepared in the laboratory and transported to the field, to assess potential bias or contamination. Field blanks consisted of a sample collection medium (dust bottle, wipe, filter cassette, paint chip collection vial) removed from packaging, connected to any necessary sampling device (vacuum, air pump) and immediately removed, then packaged without actually taking a dust sample. At a given study unit, one field blank of each sampling media to be used on that day was taken prior to $R \& R$ activities and field sampling.
- Field side-by-side samples: Vacuum and wipe samples collected in areas adjoining "regular" sample areas, to determine variability due to the sample collection process.

In addition, laboratory QA/QC measures were implemented during the analysis of the field samples.

Section D. 1 of this appendix presents a statistical summary of the field blank data. Tables of the side-by-side sample results, along with results for adjoining regular samples, are presented in Section D. 2 (a discussion of side-by-side sample results is found in Section 6.4). Results of laboratory QA/QC sample analysis that deviated from data quality objectives are summarized in Section D.3.

## D. 1 FIELD BLANKS

The following field blanks were collected within each phase of the EFSS:

- Carpet removal: Four field blank samples were collected at each of the eight study units prior to carpet removal activities, one for each sample type considered in this phase (vacuum, wipe, personal air, and ambient air);
- Window replacement: Three field blank samples were collected at each of the four study units prior to window replacement activities, one for each sample type considered in this phase (vacuum, personal air, and ambient air);
- CED phase: at a given study unit, one field blank sample was collected for each sample medium to be employed on that day (vacuum, wipe, personal air, paint chip).

Field blank results for all sample types were reported in terms of lead content (i.e., $\mu \mathrm{g}$ lead per sample). In addition, vacuum field blank samples were reported in $\mu \mathrm{g}$ lead per gram of dust in the sample.

Tables D-1a through D-1c present the results of analysis on the field blank samples for the carpet removal, window replacement, and CED phases, respectively. The results ( $\mu \mathrm{g} / \mathrm{sample}$ ) for all three phases were generally close to the analytical detection limit associated with the given sample medium, despite the frequency to which detected results were observed within the field blanks. Detected results are primarily the result of instrument sensitivity. These tables indicate that no apparent bias in sample collection and handling was observed as a result of reviewing the field blank data.

Table D-1a. Descriptive Summaries of Field Blank Sample Results Within the Carpet Removal Phase

|  | Sample Types |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Vacuum |  | Wipe | Personal Air | Ambient Air |
|  | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} / \mathrm{g}$ | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} /$ sample |
| Arithmetic Mean (S.E.) | $\begin{gathered} 2.19 \\ (1.09) \\ \hline \end{gathered}$ | $\begin{aligned} & \hline 679.5 \\ & (374) \\ & \hline \end{aligned}$ | $\begin{gathered} \hline 2.72 \\ (0.58) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 0.215 \\ (0.250) \\ \hline \end{gathered}$ | $\begin{gathered} \hline 0.209 \\ (0.073) \\ \hline \end{gathered}$ |
| Minimum/ Maximum Result | $\begin{gathered} 0.450 / \\ 3.12 \end{gathered}$ | $\begin{aligned} & 173.2 / \\ & 1,376 \end{aligned}$ | $\begin{aligned} & 2.34 / \\ & 3.94 \end{aligned}$ | $\begin{gathered} 0.093 / \\ 0.831 \end{gathered}$ | $\begin{aligned} & 0.110 / \\ & 0.312 \end{aligned}$ |
| \% Not Detected Results | 62.5\% | 57.1\% ( $\mathrm{n}=7$ ) | 50\% | 0\% | 0\% |

Note: This summary is based on analysis of $n=8$ field blank samples.

Table D-1b. Descriptive Summaries of Field Blank Sample Results Within the Window Replacement Phase

|  | Sample Types |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Vacuum |  | Paint Chip | Personal Air | Ambient Air |
|  | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} / \mathrm{g}$ | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} /$ sample |
| Arithmetic <br> Mean (S.E.) | $2.09(0.58)$ | 1259.81 <br> $(1422.82)$ | 6.08 <br> $(0.01)$ | $0.080(0.006)$ | 0.102 <br> $(0.050)$ |
| Minimum/ <br> Maximum <br> Result | $1.72 /$ | $45.008 /$ | $6.07 /$ | $0.075 /$ | $0.047 /$ |
| \% Not <br> Detected <br> Results | $50 \%$ | 3263.33 | 6.09 | 0.089 | 0.151 |

Note: Summaries for vacuum, personal air, and ambient air are based on analysis of $n=4$ field blanks. Summaries for paint chip are based on analysis of $n=2$ field blanks (at units 1-01 and 4-01).

Table D-1c. Descriptive Summaries of Field Blank Sample Results Within the CED Phase

|  | Sample Types (Number of Samples) |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  | Dust Vacuum$(\mathrm{N}=4)$ |  | $\begin{gathered} \text { Paint Chip } \\ (\mathrm{N}=2)^{(1)} \end{gathered}$ | $\begin{gathered} \text { Personal Air } \\ (\mathrm{N}=5) \end{gathered}$ | Dust Wipe $(\mathrm{N}=4)$ |
|  | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} / \mathrm{g}$ | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} /$ sample | $\mu \mathrm{g} /$ sample |
| Arithmetic Mean (S.E.) | $\begin{gathered} 11.31 \\ (10.335) \end{gathered}$ | $\begin{gathered} 0.0013 \\ (0.000483) \\ \hline \end{gathered}$ | $\begin{gathered} 10.19 \\ (6.537) \end{gathered}$ | $\begin{gathered} 0.1568 \\ (0.0921) \end{gathered}$ | $\begin{gathered} 4.461 \\ (0.7213) \end{gathered}$ |
| Minimum/ Maximum Result | $\begin{aligned} & 2.33 / \\ & 20.85 \end{aligned}$ | $\begin{gathered} 0.0006 / \\ 0.0017 \end{gathered}$ | $\begin{aligned} & 5.57 / \\ & 14.81 \end{aligned}$ | $\begin{gathered} 0.075 / \\ 0.276 \end{gathered}$ | $\begin{aligned} & 3.519 / 1 \\ & 5.277 \end{aligned}$ |
| \% Not Detected Results | 25\% |  | 0\% | 0\% | 75\% |

## D. 2 FIELD SIDE-BY-SIDE SAMPLES

Side-by-side QC samples were collected for various dust vacuum and wipe samples throughout the three EFSS phases. Section 6.4 contains a detailed discussion of the results of the statistical analysis of the side-by-side sample data relative to their adjoining regular sample results.

Tables D-2a through D-2c contain sample weights, lead concentrations, and lead loadings within pairs of dust samples, where pairs constituted a side-by-side sample and its adjoining regular sample. The first set of columns in the table contain results for the sample from each pair that was collected first, the second set of columns are for the sample collected second, and the third set of columns indicate summaries of differences between the two samples in a pair.

Within a pair, the regular sample was usually (but not always) taken prior to the side-byside sample in all three phases. At the same time, when vacuum collection methods were used, lower lead loadings were usually observed within the sample collected second. These facts suggest that some bias may be introduced to the second sample area when the first sample is collected. This issue is discussed further in Section 6.3.

Table D-2a. Sample Loadings, Concentrations, and Weights for Each Sample Pair Defined by a Regular Dust Sample and an Adjoining Side-by-Side QC Sample, in the R\&R Carpet Removal Phase

| Unit ID | Sample Taken First in the Pair |  |  |  |  | Sample Taken Second in the Pair |  |  |  |  | Difference in Results (First Sample Minus Second Sample) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MRI ID | Time Col. | Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | Conc. ( $\mu \mathrm{g} / \mathrm{g}$ ) | Sample Weight (g) | MRI ID | Time Col. | Loading $\left(\mu \mathrm{g} / \mathrm{ft}^{2}\right.$ ) | Conc. ( $\mu \mathrm{g} / \mathrm{g}$ ) | Sample Weight ( g ) | Loading $\left(\mu \mathrm{g} / \mathrm{ft}^{2}\right.$ ) | Conc. ( $\mu \mathrm{g} / \mathrm{g}$ ) | Sample Weight ( g ) | Time (min.) |
| Vacuum Dust Sampling from Floor Surfaces (Pre-Activity) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1-01 | 60022 | 09:49 | 32.42 | 493.38 | 0.0657 | 60020 | 09:59 | 1.56 | 172.92 | 0.0090 | 30.86 | 320.46 | 0.0567 | 10 |
| 1-02 | 60065 | 08:26 | 6.69 | 323.43 | 0.0207 | 60067 | 08:34 | 5.28 | 225.83 | 0.0234 | 1.41 | 97.60 | -0.0027 | 8 |
| 1-03 | 60105 | 09:01 | 2.61 | 231.37 | 0.0113 | 60048 | 09:08 | 2.61 | 272.34 | 0.0096 | 0.00 | -40.97 | 0.0017 | 7 |
| 1-04 | 60145 | 08:25 | 2.61 | 52.08 | 0.0502 | 60129 | 08:35 | 2.61 | 198.06 | 0.0132 | 0.00 | -146.0 | 0.0370 | 10 |
| 2-01 | 62036 | 09:26 | 564.52 | 9179.19 | 0.0615 | 62051 | 09:37 | 121.21 | 1864.77 | 0.0650 | 443.31 | 7314.4 | -0.0035 | 11 |
| 2-02 | 62336 | 15:20 | 2.85 | 500.07 | 0.0057 | 60556 | 15:29 | 11.51 | 1211.79 | 0.0095 | -8.66 | -711.7 | -0.0038 | 9 |
| 2-03 | 60986 | 14:09 | 45.77 | 4576.50 | 0.0100 | 62246 | 14:16 | 5.96 | 960.48 | 0.0062 | 39.81 | 3616.0 | 0.0038 | 7 |
| 2-05 | 60746 | 08:46 | 447.54 | 5552.61 | 0.0806 | 60741 | 08:57 | 347.85 | 3229.81 | 0.1077 | 99.69 | 2322.8 | -0.0271 | 11 |
| Vacuum Dust Sampling from Floor Surfaces (1-hour Post-Activity) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1-01 | 60021 | 14:31 | 655.33 | 1227.89 | 0.5337 | 60008 | 14:39 | 295.49 | 985.29 | 0.2999 | 359.84 | 242.60 | 0.2338 | 8 |
| 1-02 | 60062 | 10:59 | 68.68 | 200.87 | 0.3419 | 60066 | 11:07 | 36.45 | 358.38 | 0.1017 | 32.23 | -157.5 | 0.2402 | 8 |
| 1-03 | 60100 | 12:05 | 26.88 | 359.80 | 0.0747 | 60098 | 12:12 | 20.93 | 426.23 | 0.0491 | 5.95 | -66.43 | 0.0256 | 7 |
| 1-04 | 60131 | 11:41 | 2290.80 | 10532.4 | 0.2175 | 60142 | 11:49 | 230.24 | 433.52 | 0.5311 | 2060.6 | 10099 | -0.3136 | 8 |
| 2-01 | 62016 | 14:33 | 1332.30 | 15564.3 | 0.0856 | 62056 | 14:42 | 351.28 | 5593.63 | 0.0628 | 981.02 | 9970.6 | 0.0228 | 9 |
| 2-02 | 60461 | 18:05 | 224.93 | 1445.57 | 0.1556 | 60491 | 18:12 | 232.09 | 4227.51 | 0.0549 | -7.16 | -2782 | 0.1007 | 7 |
| 2-03 | 60451 | 19:28 | 452.15 | 2132.78 | 0.2120 | 62096 | 19:35 | 231.86 | 1022.76 | 0.2267 | 220.29 | 1110.0 | -0.0147 | 7 |
| 2-05 | 60726 | 12:20 | 167.83 | 1822.26 | 0.0921 | 60796 | 12:30 | 252.37 | 2941.38 | 0.0858 | -84.54 | -1119 | 0.0063 | 10 |
| Vacuum Dust Sampling from Stainless Steel Dustfall Collectors (1-Hour Post-Activity) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1-01 | 60010 | 14:48 | 92.61 | 3795.49 | 0.0244 | 60009 | 14:56 | 8.87 | 1528.49 | 0.0058 | 83.74 | 2267.0 | 0.0186 | 8 |
| 1-02 | 60064 | 11:15 | 36.50 | 444.64 | 0.0821 | 60071 | 11:26 | 40.27 | 291.63 | 0.1381 | -3.77 | 153.01 | -0.0560 | 11 |
| 1-03 | 60101 | 12:19 | 13.35 | 481.88 | 0.0277 | 60097 | 12:26 | 8.60 | 411.48 | 0.0209 | 4.75 | 70.39 | 0.0068 | 7 |
| 1-04 | 60137 | 11:57 | 128.46 | 7216.85 | 0.0178 | 60135 | 12:05 | 94.58 | 8520.45 | 0.0111 | 33.88 | -1304 | 0.0067 | 8 |
| 2-01 | 62041 | 14:50 | 13.67 | 1730.76 | 0.0079 | 62011 | 14:57 | 3.06 | 3397.78 | 0.0009 | 10.61 | -1667 | 0.0070 | 7 |
| 2-02 | 60486 | 18:19 | 2.85 | 370.18 | 0.0077 | 60446 | 18:26 | 4.11 | 596.09 | 0.0069 | -1.26 | -225.9 | 0.0008 | 7 |
| 2-03 | 62111 | 19:42 | 24.30 | 1786.54 | 0.0136 | 62231 | 19:46 | 68.60 | 1277.54 | 0.0537 | -44.30 | 509.00 | -0.0401 | 4 |
| 2-05 | 60781 | 12:05 | 19.78 | 464.23 | 0.0426 | 60736 | 12:12 | 18.82 | 464.62 | 0.0405 | 0.96 | -0.39 | 0.0021 | 7 |

Table D-2a. (Continued)

|  | Sample Taken First in the Pair |  |  |  |  | Sample Taken Second in the Pair |  |  |  |  | Difference in Results (First Sample Minus Second Sample) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Unit ID | MRIID | Time Col. | Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | Conc. $(\mu \mathrm{g} / \mathrm{g})$ | Sample Weight (g) | MRIID | Time Col. | $\begin{gathered} \text { Loading } \\ \left(\mu \mathrm{g} / \mathrm{ft}^{2}\right) \\ \hline \end{gathered}$ | Conc. ( $\mathrm{mg} / \mathrm{g}$ ) | Sample Weight (g) | $\begin{gathered} \text { Loading } \\ \left(\mu \mathrm{g} / \mathrm{ft}^{2}\right) \\ \hline \hline \end{gathered}$ | Conc. ( $\mathrm{mg} / \mathrm{g}$ ) | Sample Weight (g) | Time (min.) |


| Vacuum Dust Sampling from Stainless Steel Dustfall Collectors (2-Hours Post-Activity) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-01 | 60002 | 15:11 | 59.94 | 831.38 | 0.0721 | 60003 | 15:16 | 17.81 | 415.10 | 0.0429 | 42.13 | 416.28 | 0.0292 | 5 |
| 1-02 | 60070 | 11:56 | 22.39 | 371.96 | 0.0602 | 60068 | 12:04 | 30.30 | 157.40 | 0.1925 | -7.91 | 214.56 | -0.1323 | 8 |
| 1-03 | 60102 | 12:59 | 2.61 | 168.67 | 0.0155 | 60099 | 13:05 | 10.61 | 340.10 | 0.0312 | -8.00 | -171.4 | -0.0157 | 6 |
| 1-04 | 60144 | 12:43 | 219.14 | 7046.30 | 0.0311 | 60136 | 12:49 | 196.50 | 7528.74 | 0.0261 | 22.64 | -482.4 | 0.0050 | 6 |
| 2-01 | 62021 | 15:31 | 66.69 | 3402.40 | 0.0196 | 62001 | 15:39 | 12.23 | 1547.47 | 0.0079 | 54.46 | 1854.9 | 0.0117 | 8 |
| 2-02 | 60466 | 19:17 | 54.82 | 3806.60 | 0.0144 | 60506 | 19:24 | 3.01 | 567.55 | 0.0053 | 51.81 | 3239.1 | 0.0091 | 7 |
| 2-03 | 60421 | 20:35 | 86.94 | 1461.19 | 0.0595 | 62106 | 20:37 | 32.49 | 1511.07 | 0.0215 | 54.45 | -49.88 | 0.0380 | 2 |
| 2-05 | 60696 | 12:54 | 68.58 | 1937.32 | 0.0354 | 60671 | 13:00 | 13.22 | 297.06 | 0.0445 | 55.36 | 1640.3 | -0.0091 | 6 |
| Wipe Dust Sampling from Stainless Steel Dustfall Collectors (1-Hour Post-Activity) |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 1-02 | 60076 | 11:00 | 23.23 |  |  | 60074 | 11:03 | 11.94 |  |  | 11.29 |  |  | 3 |
| 1-03 | 60111 | 11:58 | 7.70 |  |  | 60113 | 12:00 | 4.64 |  |  | 3.06 |  |  | 2 |
| 1-04 | 60126 | 11:45 | 174.87 |  |  | 60124 | 11:47 | 188.56 |  |  | -13.69 |  |  | 2 |
| 2-01 | 62186 | 14:20 | 23.62 |  |  | 62191 | 14:25 | 16.18 |  |  | 7.44 |  |  | 5 |
| 2-02 | 62196 | 18:21 | 93.17 |  |  | 60606 | 18:26 | 392.87 |  |  | -299.7 |  |  | 5 |
| 2-03 | 62276 | 19:19 | 74.11 |  |  | 62261 | 19:21 | 28.81 |  |  | 45.30 |  |  | 2 |
| 2-05 | 60806 | 11:43 | 11.82 |  |  | 62151 | 11:45 | 2.42 |  |  | 9.40 |  |  | 2 |

Table D-2b. Sample Loadings, Concentrations, and Weights for Each Sample Pair Defined by a Regular Dust Sample and an Adjoining Side-by-Side QC Sample, in the R\&R Window Replacement Phase

|  | Sample Taken First in the Pair |  |  |  |  | Sample Taken Second in the Pair |  |  |  |  | Difference in Results (First Sample Minus Second Sample) |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Unit ID | MRI ID | Time Col. | Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | Conc. ( $\mu \mathrm{g} / \mathrm{g}$ ) | Sample Weight (g) | MRI ID | Time Col. | Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | Conc. ( $\mu \mathrm{g} / \mathrm{g}$ ) | Sample Weight (g) | Loading $\left(\mu \mathrm{g} / \mathrm{ft}^{2}\right)$ | Conc. ( $\mu \mathrm{g} / \mathrm{g}$ ) | Sample Weight (g) | Time (min.) |
| Vacuum Dust Sampling from Floor Surfaces (Pre-Activity) ${ }^{(1)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2-01 | 60522 | 08:37 | 50.60 | 8161.29 | 0.0062 | 60472 | 08:45 | 25.85 | 3271.77 | 0.0079 | 24.75 | 4889.5 | -0.0017 | 8 |
| 3-01 | 60367 | 08:19 | 1227.20 | 2611.62 | 0.4699 | 60252 | 08:27 | 3743.45 | 2462.15 | 1.5204 | -2516.25 | 149.47 | -1.0505 | 8 |
| 4-01 | 60454 | 09:50 | 18443.2 | 16470.1 | 1.1198 | 60469 | 09:59 | 4272.70 | 3279.63 | 1.3028 | 14171 | 13190 | -0.1830 | 9 |
| Vacuum Dust Sampling from Floor Surfaces (Post-Activity) ${ }^{(1)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2-01 | 60402 | 17:22 | 30.42 | 2304.55 | 0.0132 | 60392 | 17:30 | 10.40 | 1181.25 | 0.0088 | 20.02 | 1123.3 | 0.0044 | 8 |
| 3-01 | 60592 | 13:49 | 12770.0 | 4695.37 | 2.7197 | 60587 | 13:52 | 9498.10 | 4945.64 | 1.9205 | 3271.9 | -250.27 | 0.7992 | 3 |
| 4-01 | 60484 | 14:20 | 54515.0 | 17547.0 | 3.1068 | 60509 | 14:25 | 23850.0 | 31728.1 | 0.7517 | 30665 | -14181.1 | 2.3551 | 5 |
| Vacuum Dust Sampling from Stainless Steel Dustfall Collectors (Post-Activity) ${ }^{(1)}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2-01 | 60457 | 17:43 | 206.50 | 424.72 | 0.4862 | 60352 | 17:49 | 187.39 | 114.40 | 1.6381 | 19.11 | 310.33 | -1.1519 | 6 |
| 3-01 | 60537 | 13:30 | 148.39 | 11414.6 | 0.0130 | 60597 | 13:34 | 135.43 | 19074.6 | 0.0071 | 12.96 | -7660.03 | 0.0059 | 4 |
| 4-01 | 60399 | 13:40 | 4155.00 | 26330.8 | 0.1578 | 60549 | 13:50 | 1185.10 | 32116.5 | 0.0369 | 2969.9 | -5785.73 | 0.1209 | 10 |

[^9]Table D-2c. Loadings for Each Sample Pair Defined by a Regular Dust Sample and an Adjoining Side-by-Side QC Sample, Both Collected by Vacuum Techniques, in the R\&R CED Phase

| Activity | Sample Taken First in the Pair |  |  | Sample Taken Second in the Pair |  |  | Difference in Loadings ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | MRI ID | Time Collected | Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) | MRI ID | Time Collected | Loading ( $\mu \mathrm{g} / \mathrm{ft}^{2}$ ) |  |
| 1372 N. Carey Street, Baltimore, MD |  |  |  |  |  |  |  |
| Wall Demolition, 2nd Floor Bathroom | 61159 | 10:15 | 2671.70 | 60969 | 10:22 | 1365.40 | 1306.3 |
| Wall Demolition, 3rd Floor Bathroom | 61799 | 15:08 | 817.26 | 61669 | 15:15 | 1297.50 | -480.24 |
| Wall Demolition, Kitchen | 61849 | 13:27 | 3438.80 | 61834 | 13:30 | 2521.80 | 917.00 |
| 960 Lipan Street, Denver, CO |  |  |  |  |  |  |  |
| Door, Baseboard, Frame Removal, Bedrooms | 60448 | 15:06 | 48944.5 | 60403 | 15:18 | 23794 | 25150.5 |
|  | 60483 | 15:50 | 75693 | 60413 | 15:55 | 25652 | 50041 |
| Wall Demolition, Kitchen | 60418 | 17:01 | 138631 | 60443 | 17:07 | 11968 | 126663 |
| Window Sanding, Dining Room | 60633 | 15:47 | 918.29 | 60848 | 15:51 | 1140.2 | -221.91 |
|  | 60878 | 15:56 | 1187.70 | 60843 | 16:00 | 1241.8 | -54.10 |
| Wall Demolition, Dining Room | 61213 | 11:06 | 45.25 | 61198 | 11:14 | 98.64 | -53.39 |

## D. 3 SUMMARY OF LABORATORY QA/QC FINDINGS

In their data reports, MRI summarized the results of analyzing laboratory QA/QC samples within each instrumental and sample preparation batch. In the carpet removal phase, environmental samples were analyzed across eight instrumental analysis batches and nine sample preparation batches Samples in the window replacement samples were analyzed across nine instrumental analysis batches and thirteen sample preparation batches. Samples in the CED phase were analyzed across 16 instrumental analysis batches and 13 sample preparation batches.

In all three phases, the results of analyzing initial calibration verification and continuing calibration verification samples in each instrumental analysis batch were within the protocol criteria of $\pm 10 \%$. This indicates that the analytical instrument was properly calibrated for all of the sample analyses.

Table D-3a through D-3c report the status of meeting data quality objectives within batches in the carpet removal, window replacement, and CED phases, respectively. These tables also show the number of field samples, duplicate samples, and field blanks analyzed in each of the instruments analysis batches. Most of the incidents where data quality objectives were not met occurred in analysis of NIST standard reference material (SRM) 1646.

## Table D-3a. Summary of Conclusions Made in Analysis of Laboratory QA/QC Samples in the Carpet Removal Phase

| Instrument Analysis Batch | Total Number of Field Samples Analyzed | Sample Preparation Batch | Notes |
| :---: | :---: | :---: | :---: |
| Personal Air (MCE Filter) Cassettes |  |  |  |
| V10293A $\text { V11013A }{ }^{(1)}$ | 20 Field Samples <br> 7 Field Blanks <br> 3 Field Samples 0 Field Blank | 605 | Percent recovery for NIST SRM 1646 was $71 \%$, which was below the lower control limits. Historical data continued to be monitored throughout the study. Percent recovery for NIST SRM 2704 was $90 \%$, meeting the data quality objectives. |
| V10283B | 19 Field Samples 8 Field Blanks | 606 | Percent recovery for NIST SRM 1646 was $77.5 \%$, which falls below the lower control limit as published in the QAPjP. Historical data continued to be monitored through the study, and no further corrective action was deemed necessary. Percent recovery for NIST SRM 2704 was $105 \%$, which meets the data quality objectives. |
| Dust Wipe Samples |  |  |  |
| E07223A | 24 Field Samples 8 Field Blanks | 601 | Percent recovery for NIST SRM 2704 and NIST SRM 1646 were $93.5 \%$ and $102.2 \%$, respectively, meeting the data quality objectives. |
| E10193A | 32 Field Samples 2 Field Blanks | 602 | Percent recovery for NIST SRM 1646 was $75.3 \%$ for batch 602 , which falls between the lower warning limit and the lower control limit as published in the QAPjP. Historical data continued to be monitored through the study, and no further corrective action was deemed necessary. Percent recovery for NIST SRM 2704 was $94.6 \%$, meeting data quality objectives. |
| Dust Vacuum Samples |  |  |  |
| E10213A | 36 Field Samples 1 Field Blank <br> 36 Field Samples 2 Field Blanks | $\begin{aligned} & 603 \\ & 604 \end{aligned}$ | Percent recoveries for the NIST SRM 1646 were $71.7 \%$ for batch 603 and $75.0 \%$ for batch 604 , both of which fall below the lower control limits as published in the QAPjP. Historical data continued to be monitored through the study, and no further corrective action was deemed necessary. Percent recoveries for the NIST SRM 2704 were $97.1 \%$ for batch 603 and $86.9 \%$ for batch 604, both of which meet data quality objectives. |
| E10263A | 34 Field Samples 2 Field Blanks <br> 38 Field Samples 2 Field Blanks | $\begin{aligned} & 607 \\ & 608 \end{aligned}$ | Percent recoveries for NIST SRM 1646 were $94 \%$ for batch 607 and $86 \%$ for batch 608. Percent recoveries for NIST SRM 2704 were $104 \%$ for batch 697 and $98 \%$ for batch 608. All of these results meet data quality objectives. |
| E11303A ${ }^{(2)}$ | 5 Field Samples 0 Field Blanks <br> 2 Field Samples 0 Field Blanks | $\begin{gathered} 617 \\ 607^{(3)} \end{gathered}$ | Percent recoveries in batch 617 were 87.3\% for the NIST SRM 1646 and $87.4 \%$ for NIST SRM 2704. Both of these results meet data quality objectives. |

[^10]
## Table D-3b. Summary of Conclusions Made in Analysis of Laboratory QA/QC Samples in the Window Replacement Phase

| Instrument Analysis Batch | Total Number of Field Samples Analyzed | Sample Preparation Batch | Notes |
| :---: | :---: | :---: | :---: |
| Personal and Ambient Air (MCE Filter) Cassettes |  |  |  |
| V11223A <br> V11233 ${ }^{(1)}$ | 26 Field Samples 4 Field Blanks 1 Field Sample | 610 | The percent recovery for NIST SRM 1646 was $78.1 \%$, which falls between the lower warning and control limits. For NIST SRM 2704 the percent recovery was $104.1 \%$, which meets the data quality objectives. |
| V02034A | 10 Field Samples 0 Field Blanks | 621 | Percent recovery for NIST SRM 1646 was $78.2 \%$, which fall between the lower warning and control limits. For NIST SRM 2704 the percent recovery was $87.6 \%$, which meets the data quality requirements. |
| Paint Chip Samples |  |  |  |
| E11173A | 19 Field Samples 3 Duplicates 1 Field Blank | 615 | Percent recoveries for NIST SRM 1579 were 97.6, 93.4, and $99.7 \%$, meeting the data quality objectives. Percent recoveries for AIHA SRMs were 103, 95, and 105\% for AIHA 1 and 101, 93 , and $102 \%$ for AIHA 2. All of these results meet the data quality objectives. |
| Dust Vacuum Samples |  |  |  |
| E11153A | 49 Field Samples 3 Field Blanks | $\begin{aligned} & 612 \\ & 614 \end{aligned}$ | Percent recovery for NIST SRM 1646 was $87.3 \%$ for batch 612 and $78.1 \%$ for sample batch 614. The result for bath 614 fall between the lower warning and control limits. Percent recoveries for NIST SRM 2704 was $97.6 \%$ for batch 612 and $88.22 \%$ for batch 614 , both of which meet data quality objectives. |
| E11163A ${ }^{(2)}$ | 39 Field Samples 0 Field Blank | $\begin{aligned} & 613 \\ & 614 \end{aligned}$ | The percent recovery for the NIST SRM 1646 was $100 \%$ for batch 613, and for NIST SRM 2704 it was 102\%. Both of these results meet the data quality objectives. |
| E11303A ${ }^{(3)}$ | 8 Field Samples 1 Duplicate | $\begin{aligned} & 617 \\ & 618 \end{aligned}$ | The percent recovery for the NIST SRM 1646 was $87.3 \%$ for batch 617 and $83.6 \%$ for batch 618 . The recoveries for NIST SRM 2704 were 87.4 and $93.7 \%$ for batches 617 and 168 , respectively. All of these results meet the data quality objectives. |
| E02254A | 31 Field Samples 1 Field Blank | $\begin{aligned} & 619 \\ & 622 \end{aligned}$ | The result for the NIST SRM 1646 was $99.0 \%$ for batch 619 and $96.7 \%$ for batch 622. The percent recoveries for NIST SRM 2704 were 102 and $95.3 \%$ for batches 619 and 622, respectively. All of these results meet the data quality objectives. |

${ }^{(1)}$ The samples from instrument batches V11223A and V11233A were combined when assessing data quality objectives.
${ }^{(2)}$ Instrument analysis batch E11163A included the reanalysis of one sample from sample prep batch 614.
${ }^{(3)}$ Instrument analysis batch E11303A included two samples from the carpet removal phase.

## Table D-3c. Summary of Conclusions Made in Analysis of Laboratory QA/QC Samples in the CED Phase

| Instrument Analysis Batch | Total Number of Field Samples Analyzed | Sample <br> Preparation Batch | Notes |
| :---: | :---: | :---: | :---: |
| Personal Air (MCE Filter) Cassettes |  |  |  |
| V03314A | 39 Field Samples 2 Field Blanks | 629 | Data quality objectives met. |
| V04134A | 22 Field Samples <br> 1 Field Blank | 630 | Percent recovery for NIST SRM 1646 was $75.4 \%$, which falls between the lower warning limit and lower control limit as published in the QAPjP. |
| V05264A | 29 Field Samples <br> 2 Field Blanks | 635 | Percent recovery for NIST SRM 1646 was $72.7 \%$, which falls below the lower control limit as published in the QAPjP. Historical data continued to be monitored through the study, and no further corrective action was deemed necessary. |
| Dust Wipe Samples |  |  |  |
| V04264A E04254A E04214A | 4 Field Samples 9 Field Samples 6 Field Samples 2 Field Blanks | 631 | Percent recovery for NIST SRM was $77.2 \%$, which falls between the lower warning limits and the lower control limit as published in the QAPjP. |
| E05254A | 14 Field Samples <br> 2 Field Blanks | 638 | Percent recovery for both NIST SRM 2704 and NIST SRM 1646 were $63.2 \%$ and $50.7 \%$, respectively, which does not meet the data quality objectives. Historical data continued to be monitored throughout the study, and no further corrective action was deemed necessary. |
| Paint Chip Samples |  |  |  |
| E03294A <br> V04264B ${ }^{(1)}$ | 39 Field Samples <br> 4 Duplicates <br> 2 Field Blanks <br> 2 Field Samples | 628 | Data quality objectives met. |
| E05264A | 22 Field Samples <br> 3 Duplicates | 636 | Data quality objectives met. |
| Dust Vacuum Samples |  |  |  |
| E04044A | 79 Field Samples 13 Duplicates | $\begin{aligned} & 624 \\ & 625 \end{aligned}$ | Percent recovery for NIST SRM 1646 was $78.5 \%$ for batch 624 , which falls between the lower warning limit and the lower control limit as published in the QAPjP. The result for batch 625 was $65.6 \%$, which does not meet the data quality objectives. Historical data continued to be monitored through the study, and no further corrective action was deemed necessary. |
| E04134A <br> E04184B ${ }^{(2)}$ <br> V04264A ${ }^{(2)}$ | 83 Field Samples 12 Duplicates 1 Field Blank 1 Field Sample 1 Duplicate 1 Field Sample 1 Duplicate | $\begin{aligned} & 626 \\ & 627 \end{aligned}$ | The result for the NIST SRM 1646 was $67.3 \%$ for batch 626, which falls below the lower control limits as published in the QAPjP. Historical data continued to be monitored through the study, and no further corrective action was deemed necessary. The result for the NIST SRM 2704 was $75.3 \%$ for batch 626, which falls between the lower warning limit and the lower control limit as published in the QAPjP. |
| $\begin{aligned} & \text { E05264B } \\ & \text { E06014B }{ }^{(3)} \end{aligned}$ | 75 Field Samples 5 Duplicates 4 Field Blanks 2 Field Samples | $\begin{aligned} & 633 \\ & 634 \end{aligned}$ | The result for the NIST SRM 1646 was $78.4 \%$ for batch 634, which falls between the lower warning limit and the lower control limit as published in the QAPjP. |

${ }^{(1)}$ Rerun samples from Instrumental Analysis Batch No. E03294A (over range).
${ }^{(2)}$ Rerun samples from Instrumental Analysis Batch No. E04134A.
${ }^{3}$ ) Samples moved from Instrumental Analysis Batch No. E05264B.

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| 15. Supplementary Notes <br> In addition to the authors listed above, the following key staff members were major contributors to the study: Halsey Boyd, David Burgoon, Beth Burkhart, Paul Feder, Pam Hartford, Mary Kayser, Steve Naber, Nick Sasso, and Shawn Shumaker of Battelle; and Jack Balsinger, Derrick Bradley, John Jones, and Gary Wester of MRI. |  |  |  |  |
|  |  |  |  |  |
| 16. Abstract (Limit 200 words) <br> The U.S. Environmental Protection Agency, in response to the Residential Lead Based Paint Hazard Reduction Act of 1992 (Title X), conducted a study of lead exposure associated with renovation and remodeling ( $R \& R$ ) activities. This report presents the results of a literature review and one of the principle data collection efforts of the study: the Environmental Field Sampling Study (EFSS). The EFSS collected 90 personal air samples and 556 settled dust samples to assess potential exposure to workers and occupants from selected R\&R activities. Task length average exposures measured by personal air samplers on $R \& R$ workers were greater than $100 \mu \mathrm{~g} / \mathrm{m}^{3}$ for paint removal, interior demolition, and sawing, and greater than $49 \mu \mathrm{~g} / \mathrm{m}^{3}$ for interior surface preparation and central heating system maintenance/repair. Lead loadings from stainless steel dust collectors were measured as indicators of the amount of lead disturbed and made available by the R\&R activity for exposure to occupants. With the exception of carpet removal and drilling into plaster, all activities monitored in the EFSS deposited significant amounts of lead, ranging from $218 \mu \mathrm{~g} / \mathrm{ft}^{2}$ for sawing lead-painted plaster to $42,900 \mu \mathrm{~g} / \mathrm{ft}^{2}$ for paint removal. Other exposure modifiers, as well as sampling methodology issues, are discussed in the report. |  |  |  |  |
|  |  |  |  |  |
| 17. Document Analysis |  |  |  |  |
| a. Descriptors <br> Lead-based paint, lead hazards, renovation and remodeling, field study, wipe and vacuum dust-lead sampling, dust-lead, personal exposure samples, worker certification, dustfall sampling <br> b. Identifiers/open-ended Terms Lead, renovation and remodeling, worker exposure, Title $X$, dustfall <br> c. COSATI Field/Group |  |  |  |  |


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[^0]:    ${ }^{(1)}$ Only results for regular samples (i.e., no side-by-side QC samples) are represented in this table. Only regular vacuum samples located side-by-side with a wipe sample are included in the calculation of vacuum sample results.

[^1]:    ${ }^{(1)}$ Standard deviation of the log transformed data (expressed in log measurement units).

[^2]:    ${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
    ${ }^{(2)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.

[^3]:    ${ }^{(1)}$ Standard deviation of the log-transformed data (expressed in log measurement units).
    ${ }^{(2)}$ Geometric mean represents ratio of the post-activity result to the result of the corresponding pre-activity sample. No measurement units are associated with this value.

[^4]:    ${ }^{(1)}$ Standard deviations of the log-transformed data (expressed in log measurement units).
    ${ }^{(2)}$ Results for both regular and QC samples.
    ${ }^{(3)}$ Geometric mean of the ratio of the 2-hour result to the result of the adjoining 1-hour sample. No measurement units are associated with this value.

[^5]:    ${ }^{(1)}$ Standard deviations of the log-transformed data (expressed in log measurement units).
    ${ }^{(2)}$ Results for both regular and QC samples.
    ${ }^{(3)}$ Geometric mean of the ratio of the 2-hour result to the result of the adjoining 1-hour sample. No measurement units are associated with this value.

[^6]:    ${ }^{(1)}$ Results in parentheses summarize values calculated with outlier included.
    ${ }^{(2)}$ Standard deviation of the log-transformed data (expressed in log measurement units).

[^7]:    (1) Standard deviation of the log-transformed data (expressed in log measurement units).
    ${ }^{(2)}$ Sample weights represent the total weight of the subsamples taken from each paint chip collected. In several instances, two subsamples from the same chip were analyzed. In such cases, the results from the two subsamples were combined to form a single observation.
    ${ }^{(3)}$ An extra paint chip sample was collected at unit 2-01 from a window where no other samples were collected.

[^8]:    ${ }^{(1)}$ Standard errors of model parameter estimates are in parentheses. See Model (C-1a) for parameter interpretation.
    ${ }^{(2)}$ Estimate is significantly different from zero at the $\cdot=0.05$ level.

[^9]:    ${ }^{(1)}$ Collected approximately six feet from a window that was removed.

[^10]:    ${ }^{(1)}$ One sample preparation batch was divided into two instrument analysis batches.
    ${ }^{(2)}$ This instrument analysis batch consisted of five carpet samples and four window samples.
    ${ }^{(3)}$ Two samples from sample prep batch 607 were reanalyzed due to dilution problems in the original analysis.

