# ASSESSMENT OF INDUSTRIAL HAZARDOUS WASTE PRACTICES IN THE METAL SMELTING AND REFINING INDUSTRY

Volume III

Ferrous Smelting and Refining

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The report is in four volumes: (I) Executive Summary, (II) Primary and Secondary Nonferrous Smelting and Refining, (III) Ferrous Smelting and Refining, and (IV) Appendices

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#### **ABSTRACT**

Investigations of on-land disposal of process and pollution control residuals from the United States metal smelting and refining industry were conducted. This volume presents the results of studies of the U.S. ferrous smelting and refining industry including iron and steel (SIC 3312), iron and steel foundries (SIC 332), ferroalloys (SIC 3313), and primary metal products not elsewhere classified (SIC 3399). Volume II of this report includes the results of investigations of hazardous waste generation and treatment and disposal in the primary and secondary nonferrous smelting and refining industry. Volume I summarizes major findings in both ferrous and nonferrous categories. Characteristics of each industry sector, including plant locations, production capacities, and smelting and refining processes, have been identified and described.

Land-disposed or stored residuals, including slags, dusts, and sludges, have been identified and characterized by physical and chemical properties. State, regional and national estimates have been made of the total quantities of land-disposed or stored residuals and potentially hazardous constituents thereof.

Current methods employed by the ferrous metals industry for the disposal or storage of process and pollution control residuals on land are described. Principal methods include lagoon storage of sludges, and open dumping of slags, sludges and dusts. Methods of residual treatment and disposal considered suitable for adequate health and environmental protection have been provided. Finally, the costs incurred by typical plants in each smelting and refining category for current and environmentally sound residual disposal or storage on land have been estimated.

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# TABLE OF CONTENTS

Section		Page
	ABSTRACT	iti
	ACKNOWLEDGMENTS	iv
	LIST OF FIGURES	٧i
	LIST OF TABLES	vii
I.	CONCLUSIONS	1
11.	INTRODUCTION	3
111.	FERROUS METAL SMELTING AND REFINING	5
	1. Iron and Steel (SIC 3312)	6
	2. Iron and Steel Foundries (SIC 332)	70
	3. Ferroalloys (SIC 3313)	97
	4. Primary Metal Products Not Elsewhere Classified (SIC 3399)	145
	LIST OF REFERENCES	149

# LIST OF FIGURES

Figure No.		Page
1	Flow Diagram For Iron and Steel Making	. 11
2	Foundry Operations	. 74
3	Ferromanganese and Silicomanganese Production	. 101
4	Process and Solid Waste Flow Diagram For Ferronickel Production	. 103

# LIST OF TABLES

Table No.		Page
1	Major United States Steel Ingot Producers, 1972	7
2	State Distribution of United States Iron and Steel Production Capacity, 1974	8
3	EPA Regional Distribution of U.S. Iron and Steel Capacity, 1974	9
4	Production Data For Typical Integrated Steel Plant	15
5	Waste Generation Factors For Iron and Steel Plants	21
6	Yearly Generation of Residuals By Typical Iron and Steel Plant	23
7	Estimated State, Regional and National Land Disposed Wastes From Iron and Steel Production	27
8	Summary Table, Level I, II and III Treatment and Disposal Technology, Iron and Steel	46
9	Cost of Level III Treatment and Disposal Technology, Integrated Steel Mill - Pickle Liquor Sludge	66
10	Cost Summary For Treatment and Disposal Technologies, Iron and Steel	69
11	State, Regional, and National Shipments of Iron and Steel Castings, 1973	71
12	Waste Factors For Iron and Steel Foundries	78
13	Yearly Generation of Waste Residuals by Typical Iron and Steel Foundries	79
14	Estimated State, Regional and National Land Disposed Wastes From Iron and Steel Foundries	80
15	Producers of Ferroalloys in the United States, 1972	98
16	State, Regional and National Distribution of Ferroalloy Plants By Process	99

# LIST OF TABLES (Cont.)

Table No.		Page
17	Waste Generation Factors, Ferroalloy Production	108
18	Yearly Generation of Residuals by Typical Ferroalloy Plants	109
19	Estimated State, Regional and National Solid Waste for the Ferroalloy Industry	110
20	Summary Table, Level I, II and III Treatment and Disposal Technologies - Ferroalloys	116
21	Cost of Level I Treatment and Disposal Technology - Ferromanganese and Silicomanganese	127
22	Cost of Level I Treatment and Disposal Technology - Ferrochrome	130
23	Cost of Level I Treatment and Disposal Technology - Ferronickel	134
24	Cost of Level III Treatment and Disposal Technology - Ferromanganese and Silicomanganese	137
25	Cost of Level III Treatment and Disposal Technology Ferrochrome	138
26	Cost of Level III Treatment and Disposal Technology Ferronickel	139
27	Summary Costs, Ferromanganese and Silicomanganese	141
28	Summary Costs, Ferrochrome	142
29	Summary Costs Ferronickel	143
30	Geographic Distribution of Miscellaneous Primary Metal Product Manufacturing Firms, 1972 (SIC 3399)	146
31	Production of Metal Powders	147
32	Disposition of Residuals From Metal Powder Production	148

#### SECTION I

## **CONCLUSIONS**

The ferrous smelting and refining industry disposes or stores large quantities of process and pollution control residuals on land. These residuals are predominantly inorganic slags, sludges, and dusts containing oxides and other compounds of iron, silicates, and trace metals. The only highly organic sludge encountered is decanter tar sludge from iron and steel industry byproduct coke plants. In addition to slags, sludges and dusts, the iron and steel foundries dispose of significant quantities of waste sand on land. Significant quantities of acid waste pickle liquor and waste oil are produced at iron and steel plants and usually handled by contract disposal services for reclamation or disposal.

The principal potentially hazardous constituents found in ferrous smelting and refining residuals are heavy metals including chrome, copper, zinc, lead, and nickel, and fluorides. Coke plant wastes contain phenols, cyanides, ammonia, oils and greases. Phenol and cyanide appear to a much lesser extent in blast furnace dust and wet scrubber sludges as well. Foundry sands may contain phenol as a result of the use of phenolic binders which are not degraded by process heat. Some mill scales from steel plant rolling mills contain significant amounts of oils and grease.

The predominant practice used in the ferroalloy and iron and steel industries for the disposal of non-recyclable slag and dust residuals is open dumping. Because the iron and steel industry generally dewaters sludges before disposal, sludges are more often open dumped rather than contained in lagoons. The foundry industry produces relatively small quantities of sludge and generally mixes them with waste sands and dusts before land disposal. The ferroalloy industry is more likely to employ lagoons for containment of sludges.

The iron and steel industry generally reclaims iron from slags before land disposal or sale as road ballast or aggregate. A much higher percentage of blast furnace slag is sold because of lower density and greater chemical stability than basic oxygen or electric furnace slag. Approximately 80% of mill scales generated in steel mills is recycled to recover iron value. Blast furnace dust is normally recycled to sinter or blast furnaces while basic oxygen furnace dust is occasionally recycled to sinter. The high zinc content of electric furnace dust and many basic oxygen furnace (BOF) dusts generally makes it impractical to recycle these dusts. The industry is attempting to develop technology for accepting greater quantities of dusts and sludges as sinter or blast furnace inputs. In a similar manner the ferroalloy industry which generally cannot accept dusts as furnace inputs because of trace metal contamination is exploring technology for greater recycling of dusts.

The foundry industry directly recycles significant quantities of most and and reclaims significant quantities of core sand for recycle.

The presence of potentially hazardous constituents in slags, studges, sands, and dusts has been shown including heavy metal and fluorides. Solubility tests described in Appendix B of this report indicates that some of these hazardous constituents may be leached from some wastes. In general, slags were found to solubilize to a lesser extent than sludges or dusts. Process wastes have been categorized as potentially hazardous or not hazardous based on the results of the solubility tests and consideration pf physical (i.e. particle size) and chemical properties.

Practices to protect ground and surface waters in the event of demonstrated significant leaching of potentially hazardous constituents include the use of lined lagoons for storage or permanent disposal of sludges. Leachable sludges which are dredged or pumped from lagoons or settling pits and dumped on land can often be chemically "fixed" so that leaching of heavy metals is prevented according to fixing chemical manufacturers. Alternatively, sealing of soil in disposal areas with bentonite or other sealants should prevent leachate percolation.

For those slags, dusts, sludges, and or other land-disposed or stored solid residues shown to, or suspected to solubilize toxic constituents significantly, then soil sealing of disposal or storage areas would be needed. Collection of runoff from disposal dumps containing slags, sludges or dusts with leachable heavy metals or other potentially hazardous constituents may be needed. Collected runoff would require treatment before discharge or retention and evaporation in lagoons.

Costs for present and environmentally adequate potentially hazardous waste treatment and disposal are given for each smelting and refining category.

#### SECTION II

## INTRODUCTION

This report is the result of study commissioned by the U.S. Environmental Protection Agency to assess "Industrial Hazardous Waste Practices in the Smelting and Refining Industry. Concurrently, the USEPA is pursuing similar studies of other industry categories. This program is intended to provide the USEPA with as detailed and pertinent information on the generation, management, treatment, disposal, and costs related to wastes considered to be "potentially hazardous." Such information will be used by the USEPA in developing guidelines or standards for the management of hazardous wastes.

Throughout this report whenever the terms "hazardous wastes" or "potentially hazardous wastes" are used, it should be kept in mind that no final judgements are intended as to such classification. It is recognized and understood that additional information will be required as to the actual fate of such materials in a given "disposal" or "management" environment before a final definition of "hazardous waste" evolves and is used. As an example, for certain of the waste streams identified in this report, the USEPA is currently supporting other studies designed to investigate leaching characteristics in various soil and moisture conditions.

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#### SECTION III

## FERROUS METAL SMELTING AND REFINING

This section presents the results of investigations and analyses of on-land disposal or storage of process and pollution control residuals from the United States ferrous smelting and refining industry including iron and steel, iron and steel foundries, ferroalloys and ferrous metals not elsewhere classified such as metal powders. Characteristics of each industry sector including plant locations, production capacities and smelting and refining processes have been identified and described.

Land disposed or stored residuals including slags, dusts, sands and sludges have been identified and characterized physically and chemically. State, regional and national estimates have been made of the total quantities of land disposed or stored residuals and potentially hazardous constituents thereof for 1974, 1977, and 1983.

Current methods employed by the ferrous metals industry for the disposal or storage of process and pollution control residuals on land are described. Principal methods include lagoon storage of sludges and open dumping of slags, sludges, dusts and sands. Methods of residual treatment and disposal considered suitable for adequate health and environmental protection have been provided. Finally, the costs incurred by typical plants in each primary smelting and refining industry for current and environmentally sound residual disposal or storage on land have been estimated.

#### 1.0 IRON AND STEEL

#### 1.1 INDUSTRY CHARACTERIZATION

The United States steel industry is very large. The industry ranks third in the nation, behind the automotive and petroleum industries, in the value of its total shipments and, with approximately 487,000 employees, is second only to the automotive industry in the number of people on the direct payroll. Over the decade since 1962, steel industry sales have increased 60%, from sales of \$14.0 to over \$22.0 billion (Ref. 1). Steel mills may range from comparatively small plants to completely integrated steel complexes. Even the smallest of plants will generally represent a fair sized industrial complex. Because of the wide product range, the operations will vary with each facility.

Approximately ninety-two per cent of the 1972 total United States annual steel ingot production was produced by fifteen major steel corporations. This total also represents 22.5% of the world total of 556,875,000 metric tons (625,000,000 tons). Table 1 presents the production breakdown by corporation. Tables 2 and 3 list the number of steel plants by state, EPA regional, and national total iron and steel capacity. The capacity by each of the three major steel producing modes (i.e. basic oxygen furnace, open hearth furnace, and electric furnace) are also given in these tables.

Three basic steps are involved in the production of steel. First, coal is converted to coke. Second, coke is then combined with iron ore and limestone and fired in a blast furnace to produce iron. Third, the iron is purified into steel in either an open hearth or basic oxygen, or furnaces. Electric furnaces remelt and refine predominantly scrap iron and steel. Further refinements include degassing by subjecting the steel to a high vacuum. Molten steel is usually cast into ingot molds but the use of a process called continous casting is increasing steadily. These processes are discussed in more detail in Section 1.2.

Coke plants are operated as parts of integrated steel mills to supply the coke necessary for the production of iron in blast furnaces. Nearly all coke plants today are byproduct plants, i.e., products such as coke oven gas, coal tar, crude and refined light oils, ammonium sulfate, anhydrous ammonia, ammonia liquor, and naphthalene, are produced in addition to coke. A very small portion of coke is also produced in the beehive coke process. A byproduct coke plant consists essentially of the ovens in which bituminous coal is heated, out of contact with air, to drive off the volatile components. The residue remaining in the ovens is coke; the volatile components are recovered and processed in the byproduct plant to produce tar, light oils, and other materials of potential value, including coke oven gas.

Table 1

MAJOR UNITED STATES STEEL INGOT PRODUCERS, 1972

	Metric Tons/Year	Tons/Year
United States Steel	31,750,000	35,000,000
Bethlehem Steel	19,960,000	22,000,000
Republic Steel	9,980,000	11,000,000
National Steel	9,520,000	10,500,000
Armco Steel	7,710,000	8,500,000
Jones & Laughlin Steel	7,280,000	8,000,000
Inland Steel	6,800,000	7,500,000
Youngstown Sheet & Tube	5,440,000	6,000,000
Wheeling Pittsburgh	3,540,000	3,900,000
Kaiser	2,720,000	3,000,000
McLouth	1,819,000	2,000,000
Colorado Fuel & Iron	1,360,000	1,500,000
Sharon	1,360,000	1,500,000
Interlake	907,000	1,000,000
Alan Wood	907,000	1,000,000

Source: Development Document For Proposed Effluent Limitations Guidelines For the Steel Making Segment of the Iron and Steel Manufacturing Point Source Category, U.S. Environmental Protection Agency, February, 1974.

TABLE 2
ESTIMATED STATE DISTRIBUTION OF UNITED STATES IRON AND STEEL PLANTS
AND PRODUCTION CAPACITY, 1974 (METRIC TONS)

State	No. of	Estimated Iron	Estimated	Steel Capaci	ty	Estimated
	Plants	Capacity (Blast	Basic Oxygen	Open Hearth	Electric	Total Steel
•		Furnace)	Furnace	Furnace	Furnace	Capacity
	-	r 200 roo	2 656 700	1 024 000	601 800	A 202 Eau
Alabana	5	5,208,500	2,656,700	1,024,000	601,800	4,282,500
Arizona	1	0	0	0	82,500	82,500
Arkinsas	$\frac{1}{10}$	2 104 700		1 004 700	57,800	57,800
California		2,194,300	1,600,400	1,904,700	674,400	4,179,500
Colorado	1	938,800	1,066,900	0	165,000	1,231,900
Connecticut	1	0	0	0	234,400	234,400
Delaware	1	0	0	0	524,700	524,700
Florida	2	0	0	0	257,600	257,600
Georgia	1	0	0	0	302,000	302,000
Hayoli i	1	0	0	0	20,600	20,600
~ Proois	16	6,906,700	7,261,500	841,800	4,427,000	12,530,300
Indiana	8	15,977,300	15,239,100	5,790,500	1,013,200	22,042,800
Kentucky	4	1,039,700	1,717,900	0	790,400	2,508,300
Maryland	3	5,558,500	2,528,700	2,729,800	343,700	5,602,200
Michigan	5	7,815,600	8,830,800	0	1,382,400	10,213,200
Minnesota	1	0	0	()	209,900	209,900
Mississippi	1	0	0	0	72,800	72,800
Missouri	1	0	0	0	961,900	
New Jersey	2	0	0	0	453,000	453,000
New York	7	4,807,600	5,469,200	0	503,900	5,973,100
North Carolina		()	0	0	213,200	213,200
Ohio	20	17,181,100	11,213,800	8,881,300	4,642,700	24,737,800
Oklahoma	1 1	0	0	0	244,800	244,800
Oregon	2	0	0	()	301,300	301,300
Pennsylvania	42	21,179,600	15,224,000	11,932,400	4,500,500	31,656,900
South Carolina		0	0	0	346,400	
Tennessee	2	0	0	0	122,000	122,000
Texas	9	634,100	0	1,160,600	2,832,200	3,992,800
Utah	1	1,779,500	0	2,483,300	0	2,483,300
Virginia	1	0	Ö	0	71,100	71,100
West Virginia	2	3,106,302	4,062,200	0	106,600	4,168,800
Washington	3	0	0	Ő	536,600	536,600
Totals	158	94,327,600	76,871,200	36,748,400	26,996,400	140,616,000

Source: Iron and Steel Works Directory of the United States and Canada, Iron and Steel Institute, 1974.

TABLE 3

EPA REGIONAL DISTRIBUTION OF U.S. IRON AND STEEL PLANTS AND PRODUCTION CAPACITY, 1974 (METRIC TONS)

EPA Region	No. of Plants	Estimated Iron Capacity (Blast Furnace)		Steel Capacity Open Hearth	Electric Furnace	Estimated Total Steel Capacity
I	1	0	0	0	234,400	234,400
II	10	4,807,600	5,469,200	0	1,481,500	6,950,700
: (I	48	29,844,400	21,814,900	14,662,200	5,021,900	41,499,000
ìV	18	6,248,200	4,374,700	1,024,000	2,706,200	8,104,900
V	50	47,880,700	42,545,200	15,513,500	11,675,100	69,733,800
VI	11	634,100	0	1,160,600	3,134,800	4,295,400
VII	1	0	0	0	961,900	961,900
VIII	2	2,718,300	1,066,900	2,483,300	165,100	3,715,300
IX	12	2,194,300	1,600,400	1,904,700	777,600	4,282,700
Х	5	0	0	0	837,900	837,900
	158	94,327,600	76,871,300	36,748,300	26,996,400	140,616,000

## WASTE CHARACTERIZATION

This section contains descriptions of production technology at iron and steel plants and the resultant byproducts or wastes which are either recycled, handled by contract disposers, or disposed of on site. Estimates are given for the quantities of wastes and potentially hazardous constituents thereof which are disposed of on land, either in lagoons or dumps.

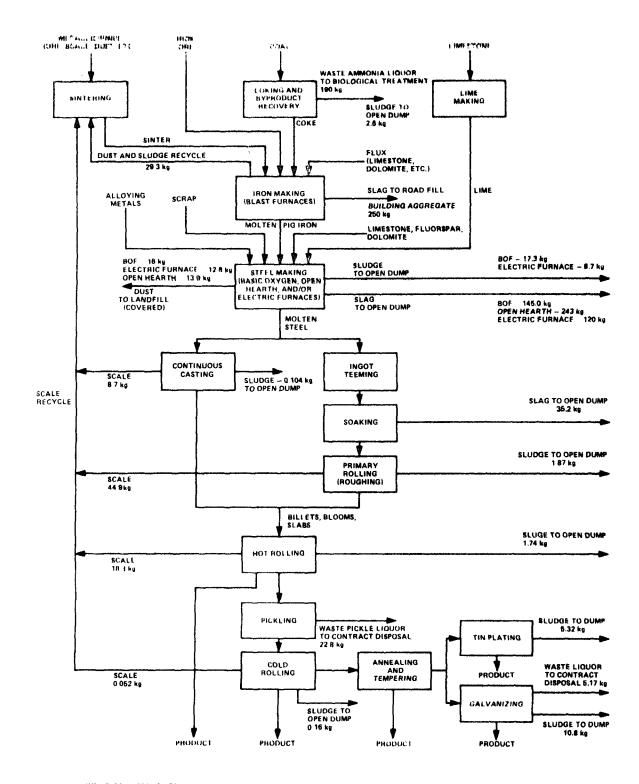
# 1.2.1 Process Descriptions

Integrated steel mills perform all the operations required to convert the principal raw materials of iron ore, limestone, and coal into finished steel products. The principal operations consist of raw material processing, iron making, steel making, primary rolling or roughing, and hot and cold finishing. Additional operations might include forging, annealing, tempering, tin plating and galvanizing. The interrelationships between the operations carried out in a typical large integrated steel plant are shown in the flow diagram of Figure 1. Smaller plants might lack the facilities for some of the operations shown, such as sintering, continuous casting, tin plating and galvanizing. The major operations are described in the following paragraphs.

Sintering. The sintering operation takes natural fine iron ores and metallic fines derived from residues of other steel plant facilities (e.g., flue dust from the blast furnace and scale from hot rolling mills) and fuses them into pieces large enough to be charged into the blast furnaces. In a typical sintering machine the fine material is mixed with coke breeze or powdered coal and spread on a moving bed. The mixture is ignited as it passes under an intense flame. The reaction is sustained by the combustion of the coke or coal as air is drawn downward through the bed. At combustion temperatures, the particles fuse together into a caked layer which is usually quenched with air and broken into pieces of the desired size. Particulates collected by one or more of a variety of emission control systems are generally recycled back into the sintering process. Therefore, no significant amounts of wastes are generated at sintering plants.

Coke and Byproduct Production. Coke serves both as a fuel and as a reducing agent in the making of iron. To produce the required coke, bituminous coal is heated to drive off the volatile components. Two methods of producing metallurgical coke are in use today, the byproduct method and the beehive process, although the beehive process accounts for less than two percent of all metallurgical coke produced.

In the beehive process, the volatile components are burned through the addition of controlled amounts of air into the coking chambers. The heat generated by burning of the combustible volatiles provides energy for maintaining the distillation process.



NUMERICAL VALUES ARE KILOGRAMS OF WASTE PER METRIC TON OF STEEL PRODUCT

Figure 1 FLOW DIAGRAM FOR STEEL MAKING

In the byproduct process, no air is admitted to the coking chambers, the heat for distillation being provided by the combustion of fue, gas in contact with the walls of the coke ovens. The volatiles driven off during distillation are piped from the coke ovens and processed for recovery of useful byproducts. After coking is completed (16 to 24 hours), the hot coke is pushed from the ovens into a waiting car which transfers it to a quenching tower where it is cooled by water sprays.

Iron and Steel Making. In iron and steel making, fluxes are added which combine with impurities to form slag. Fluxes include limestone, lime, dolomite, and fluorspar. Lime is often made onsite at the steel plant by the calcination of limestone. The dusts generated in the required crushing, screening, and handling of the materials are generally collected and recycled.

Blast Furnace. Almost all of the basic iron required for steel making is produced in blast furnaces. Input materials, consisting of iron ore, sinter, coke, and fluxes (primarily limestone), are charged into the top of the furnace. Air preheated to 1400 to 2100 F (760 to 1150 C) is forced into the bottom of the furnace. The coke reacts with the oxygen in the air to produce carbon monoxide which, in turn, reduces the are to metallic iron which settles to the bottom. The molten iron is tapped off into transfer ladles known as submarine cars for transfer to the steel making shop. Slag is drawn off at the surface of the molten metal.

The hot gases leaving the top of the blast furnace have fuel value and are commonly used in the blast furnace stoves to preheat the incoming air and for underfiring the coke ovens. Prior to use, the gases are cleaned by passing them first through a dust catcher to remove the coarser particulates and then through a wet scrubber. Flectrostatic precipitators are also used at some plants. The water from the wet scrubber system is generally piped to a clarifier where the particulates settle to form a sludge or slurry which is subsequently dewatered, often by a vacuum filter system. Thus, the wastes derived from blast furnace operations generally consist of slag, flue dust and sludge.

Steel Making. For making steel, three different furnace types are in use: the basic oxygen furnace (BOF), the electric furnace, and the open hearth furnace. As stated previously, open hearth furnaces are gradually being phased out and being replaced by BOF's. Electric furnaces are particularly well suited for making high quality and alloy steels because of better control on operating conditions such as temperature and oxygen input.

The metal charge to the basic oxygen furnace consists of about 70 percent molten iron and 30 percent cold steel scrap. The open hearth generally operates with a metal charge of 50 percent molten iron and 50 percent scrap, although it can also accept a metal charge of 100 percent scrap. The charge to electric furnaces is predominantly cold scrap.

All three furnaces use limestone and/or fluorspar fluxes to facilitate the removal of impurities as slag.

For control of emissions from basic oxygen furnaces, the use of high energy wet scrubbers appears to be predominant. Of the ten steel plants visited during this program, seven plants had BOF furnaces; and of these plants, six were controlled by wet scrubbers. One plant used a dry electrostatic precipitator preceded by a wet spray system for gas cooling.

Five of the plants visited had electric furnaces. Three of these plants used dry baghouses for dust collection. The other two used a wet scrubber followed by a clarifier and vacuum filter for handling the scrubber water.

Four of the plants had open hearth furnaces and, in all cases, emission control was handled by dry electrostatic precipitators.

Thus, wastes from steel making consist of slag for all furnace types, and dusts and/or sludges, depending on the type of furnace and the associated emission control system. For BOF furnaces, sludges appear to be the most common form of pollution control waste, while for electric furnaces and open hearths dry dust appears to be most common. In addition to the above wastes, particulates called "kish" are released to the air during the pouring of the molten pig iron. In BOF shops, this material is commonly collected in baghouses.

Ingot Molding and Rolling. Molten steel is tapped from the steel making furnaces into teeming ladles and then transferred to a teeming area or to a continous casting area. In the teeming area, the molten steel is poured into ingot molds. Upon solidification, the ingots are placed in soaking pits to bring them to the desired uniform temperature. They are then rolled into billets, blooms, or slabs which are blocks having different shapes and weights. Wastes consist of slag that accumulated at the bottoms of the soaking pits, scale generated in the rolling operations and sludges from treatment of scale pit water.

Continous Casting. In continous casting, the molten steel in the teeming ladles is cast directly into billets, blooms, or slabs, thereby eliminating the need for ingot molds, soaking pits and primary rolling described in the next paragraph. As the castings leave the molds, they are sprayed with cooling water. As a result of coming in direct contact with the steel, this water contains fine scale that is removed as sludge during treatment of the water. Coarser scale accumulates in settling pits.

Rolling. The billets, blooms, and slabs formed in the roughing mill or in the continous caster are sent to the hot rolling mills where they are converted into a wide variety of finished or semi-finished products, including bars, rods, tubes, rails, structured shapes, sheets, and plates. These hot rolling operations produce scale which is collected in pits. Sometimes surface defects in billets, blooms and slabs are removed prior

to rolling by automatic or hand scarfing, an operation in which exygen ther present it limited at the surface. Grinding and chipping are also used for removing surface defects. Thus, scarfing scale and grinding and chipping residues are additional wastes generated at the rolling mills.

hot rolling is often followed by cord-rolling and cold-forming operations. Prior to cold processing, the steed is pickled by passing it through vats of hydrochloric or sulfuric acid solution to clean the surface. Aste pickle liquor is sometimes disposed or treatly on land and, therefore, contitutes a waste of interest to this program. Mentralization of the waste pickle liquor is sometimes accompanied by the formation of sludges which are also land disposed.

In cold rolling, sheet steel becomes hardened and usually requires annealing (i.e. softening by heat treatment). Coils of sheet steel are annealed by heating them in a controlled atmosphere. After cooling, the annealed steel is then generally passed through a temper mill which gives it the desired hardness, flatness, and surface quality. No wastes are generated in the annealing and tempering operations.

Coating and Plating. Further processing of the sheet steel might include coating the surface with nonferrous metal, paint, or other coatings. Two common coating operations, tin plating and galvanizing, are included in the flow diagram of Figure 1. One common method of tin plating involves electrolytic deposition. The steel is first washed and scrubbed and then cleaned in a dilute acid solution. It is then passed through an electrolytic solution, washed, and rinsed. The coated sheets are then heated so the tin flows to form a surface coating of high luster. Finally, the surface is water quenched, electrochemically treated, and coated with oil. In galvanizing, the sheet steel is cleaned, heated, dipped in molten zinc, cooled, and chemically treated. In galvanizing and tin plating, sludges are generated containing residuals from the cleaning lines and from neutralization of the acid rinse water.

# Capacity of Typical Plant

For the typical plant an annual capacity of 2,500,000 metric tons of molten steel was selected. This value is alightly greater than the average ingot steel production for 45 of the major steel making plants in the United States. Facilities at the typical plant consist of a sinter plant, blast furnaces, basic oxygen furnaces, electric furnaces, coke ovens, a continuous caster, primary (or roughing) mills, other hot rolling mills (hot strip, bar, etc.), cold mills, annealing and tempering mills, a tin plating mill and a galvanizing mill. Table 1 gives the annual production figures for each major facility at the typical plant. The figures are generally internally consistent, but in any one plant the relative amounts of products of different types will vary as will the amount of home scrap produced. In addition, intermediate products such as blooms, billets or slabs might be purchased and/or sold in any given year, so that the ratio of weight of finished products-to-weight of steel produced will vary.

TABLE 4 - PRODUCTION DATA FOR TYPICAL INTEGRATED STEEL PLANT

Facility	Product	Annual Amounts (Metric tons)
Coke Ovens	Coke	1,120,000
Blast Furnaces	Iron	1,600,000
Basic Oxygen Furnaces	Steel	2,000,000
Electric Furnaces	Steel	500,000
Soaking Pits	Steel Ingots	1,560,000
Primary Mills	Billets, Blooms, Slabs	1,350,000
Continuous Caster	Billets, Blooms, Slabs	790,000
Hot Rolling Mills	Sheet Steel, Bars, Rods	1,800,000
	Structural Shapes, etc.	
Cold Rolling Mills	Sheet Steel	700,000
Tin Plating Mill	Tin Plated Sheets	100,000
Galvanizing Mill	Zinc Coated Sheets	125,000

# 1.2.1 Description of Waste Streams

This section describes the types of wastes associated with each of the steel making processes previously described. Generation factors for each type of wastes are given as well as an assessment of their potential environmental hazard.

Coke and Byproduct Plants. Wastes generated from coke and byproduct coke plants include waste ammonia liquor, ammonia still lime sludge and decanter tank tar. The relative amounts of these wastes will vary considerably from plant to plant depending on the specific design of the byproduct recovery plant.

Waste Ammonia Liquor. Ammonia is recovered from coke gas by one of two methods. In some plants ammonia is recovered in the form of ammonium sulfate by passing the coke gas through dilute sulfuric acid. This produces a waste ammonia liquor generated at a rate of 190 kg/MT of coke produced or 125 kg/MT of steel produced based on the use of 0.66 MT of coke for 1 ton of steel. Waste ammonia liquor contains significant concentrations of phenol and cyanide and is therefore considered potentially hazardous.

Ammonia Still Lime Sludge. At other plants ammonia is removed initially from the coke oven gas by spray cooling and scrubbing and sold as a concentrated ammonia liquor. Concentration of the liquor is achieved in a ammonia still which produces a waste lime sludge formed as a result of adding milk of lime to decompose ammonium salts. Ammonia still lime sludge along with decanter tank tar to be described is generated at a rate of 0.28 kg/MT of finished steel product (dry weight). This sludge will contain significant concentrations of cyanide, phenol, and oils and greases. In solubility tests described in Appendix B ammonia still lime sludge was found to leach significant concentrations of phenol and cyanide (198 ppm Cn, 20 ppm phenol). It is therefore considered potentially hazardous.

Decanter Tank Tar. The spray cooling of coke oven gases also condenses tars which are sent to a decanter tank where lighter recoverable oil fractions are decanted off. The heavier tar generated at a rate of 2.3 kg/MT steel along with ammonia still lime studge is sent to open dumps. In solubility tests described in Appendix B decanter tank tar was found to leach significant concentrations of phenol (500 ppm) and oil and grease (198 ppm) and is therefore considered potentially hazardous.

Wastes generated from iron and steel making include slags, sludges and dusts. The quantities and nature of these residuals are described in the following paragraphs as well as an assessment of their hazardousness or non-hazardousness.

Blast Furnace. Residuals from blast furnace processing of iron ore to produce molten iron metal include slag, dusts from dry air emissions controls or sludge from wet air emissions controls.

Slag. Blast furnace slag is generated at a rate of 348 kg/MT of iron output from the blast furnace or 250 kg/MT of finished steel. It is normally granulated by quenching the molten slag with water. This produces sand size to large chunks of a hard vesicular slag containing predominantly silica, lime, iron, sulfur and traces of minor metals including chromium, manganese, lead, copper and zinc. In solubility tests described in Appendix B blast furnace slag did not leach toxic constituents in significant concentrations and is therefore not considered potentially hazardous.

Dust. Dust from dry emissions controls on blast furnaces including baghouses and electrostatic precipitators is predominantly iron oxide, silica and lime but contains significant concentrations of chromium, copper, manganese, nickel, lead and zinc. Concentrations of these metals is significantly higher in dusts than in slag. It is generated at a rate of 16.2 kg/MT of blast furnace iron output or 11.7 kg/MT of steel product. In solubility tests described in Appendix B blast furnace dust did not leach toxic heavy metals significantly and is therefore not considered potentially hazardous at this time.

Studge. Studge from wet emissions controls on blast furnaces including wet electrostatic precipitators, venturi scrubbers, and spray towers is also predominantly iron oxide, silica and lime and contains significant concentrations of the trace metals chromium, copper, manganese, nickel, lead and zinc. Concentrations of these metals is significantly higher in studges than in stags. It is generated at a rate of 24.4 kg per metric ton of blast furnace iron output or 17.6 kg/MT of steel (dry weights). In solubility tests described in Appendix B blast furnace studge was not found to leach toxic constituents in significant concentrations and is therefore not considered a potentially hazardous waste.

Basic Oxygen Furnace (BOF). Residuals from BOF processing of iron, scrap and alloying metals to produce steel while reducing carbon sulfur, phosphorus and other impurities, include slag, dusts and sludges.

Slag. A dense slag containing large amounts of silica, iron and lime, minor amounts of sulfur and phosphorus and significant concentrations of the trace metals chromium, copper, manganese, nickel, lead and zinc is generated at a rate of 145 kg/MT of steel output. In solubility tests described in Appendix B blast furnace slag was not found to leach significant concentrations of toxic constituents and is therefore not considered potentially hazardous.

Dust. Fine dust from dry air emissions controls is mainly iron oxide, silica oxide and lime but also contains significant concentrations of trace metals including chrome, copper, manganese, nickel, lead and zinc. Dust is generated at a rate of 16 kg/MT of steel product. Data indicates zinc and lead are more concentrated in dusts and sludges whereas chrome tends to stay with slag. In solubility tests described in Appendix B BOF sludge did not leach appreciable concentrations of toxic constituents. The low solubility of BOF sludge indicates that dust will also not leach

significantly. For this reason BOF dust is not considered potentially nazardous at this time.

Sludge. Sludge from wet control of air emissions from BOF's is also predominantly iron oxides, silica oxide and lime with small but significant concentrations of the trace metals chrome, copper, manganese, nickel, lead and zinc. It is generated at a rate of 17.3 kg/MT of steel product (dry weight). In solubility tests described in Appendix B BOF sludge did not leach significant concentrations of toxic constituents and is therefore not considered potentially hazardous at this time.

Open Hearth Furnaces. Residuals generated from open hearth furnaces include slag, dusts and sludges.

Slag. A dense, hard slag is generated at a rate of 243 kg/MT of steel product. It is mainly iron oxides, silica oxide and lime, with minor amounts of sulfur and phosphorus compounds. Trace metals present in significant concentrations include chromium, copper, manganese, nickel, lead and zinc. In solubility tests described in Appendix B toxic constituents did not leach to a significant extent. Open hearth slag is therefore not considered hazardous at this time.

Dust. Dust from dry emissions control is generated at a rate of 13.7 kg/MT of steel product. It is predominantly iron oxides, silica oxides and lime but contains significant concentrations of chrome, copper, manganese, nickel, lead and zinc. As with BOF furnaces data indicates that lead zinc, and to a lesser extent copper concentrate to a greater extent in dusts whereas chrome stays with the slag. Solubility tests described in Appendix B showed no appreciable leaching of toxic constituents. For this reason open hearth dust is not considered potentially hazardous at this time.

Sludge. None of the plants visited or surveyed during this study used wet emissions controls on open hearth furnaces. Thus no generation factors could be developed or chemical analyses made. The sludge would be similar in composition to dust and would not be expected to leach significantly so as to be considered hazardous.

Electric Furnaces. Residuals from electric furnaces include slag, dust and sludge.

Slag. A dense hard slag is generated at a rate of 120 kg/MT of steel. It is composed principally of iron, silica and calcium compounds with minor amounts of sulfur and phosphorus compounds. Trace metals include chromium, copper, manganese, nickel, lead, and zinc. In solubility tests described in Appendix B toxic constituents did not leach significantly. Electric furnace slag is therefore considered non-hazardous at the present time.

Dust. Dust from dry emissions controls is generated at a rate of 12.8 kg/MT of steel. It is principally iron and silica oxides and lime with significant concentrations of the trace metals chromium, copper, manganese, nickel, lead, and zinc. Zinc, lead and copper are much more concentrated in dusts and sludges than in slag. In solubility tests described in Appendix B lead was found to leach at appreciable concentrations (150 ppm). Electric furnace dust is therefore considered potentially hazardous.

Studge. Studge from wet emissions controls is generated at a rate of 8.7 kg/MT of steel product. It is comprised principally of iron and silica oxides and lime and contains significant concentrations of the trace metals chromium, copper, manganese, nickel, lead and zinc. In solubility tests described in Appendix B electric furnace studge leached chromium (94 ppm) and lead (2.0 ppm) in significant concentrations. Flectric furnace studge is therefore considered potentially hazardous at this time.

Soaking Pits. Soaking pit slag of gravel to boulder size is generated at a rate of 35.2 kg/MT of steel. It is composed principally of iron and contains significant concentrations of trace metals including chromium, copper, manganese, nickel, lead and zinc. In solubility tests described in Appendix B this slag did not leach significant concentrations of toxic metals. It is therefore considered non-hazardous at this time.

Mill Sludges. Mill sludges are produced from a number of steel plant facilities as a result of water pollution control operations. Generation factors for various mill sludges are as follows:

Primary Mills (production of ingots, slabs, billets 1.87 kg/MT steel Continuous Casting Mill - 0.104 kg/MT steel Hot Rolling Mill - 1.74 kg/MT steel Cold Rolling Mill - 0.16 kg/MT steel Tin Plating Mill - 5.32 kg/MT steel Galvanizing Mill 10.8 kg/MT steel

Samples of two of the above types of sludges were obtained and chemically analyzed including hot rolling mill sludge and tin plating mill sludge. Both of these sludges contained significant concentrations of trace metals including chromium, copper, manganese, nickel, lead, zinc and oil and grease.

Solubility tests were not conducted on mill sludges. They are believed to be susceptible to leaching of oil and grease and quite possibly some toxic metals because of the presence of these constituents and fine size of sludge particulates.

Mill Scales Mill scales containing over 50% iron are generated from the following mills:

Primary Mills 44.9 kg/MT steel Continuous Casting Mills 8.7 kg/MT steel Hot Rolling Mills 18.3 kg/MT steel Cold Rolling Mills 0.052 kg/MT steel

Mill scales contain over 50% iron as well as small but significant concentrations of trace metals including chronium, copper, manganese, nickel, lead and zinc. Mill scales can also contain as much as 0.4% oil and grease. Oil and grease can be leached from mill scale and pose a threat of ground water contamination. For this reason mill scales are considered potentially hazardous at this time.

Pickle Liquors. Acid pickle liquors (HCl, H<sub>2</sub>SO<sub>4</sub>) are used in cold rolling mills and galvanizing mills to clean iron and steel metal surfaces. Spent acid is generated at a rate of 22.8 kg/MT steel from cold rolling mills and 5.17 kg/MT steel from galvanizing mills. Waste pickle liquor contains about 4-6% acidity and large concentrations of dissolved and suspended iron. Chromium, copper, nickel, lead and zinc are also present in minor concentration (less than 20 ppm). The high acidity (pH less than 1.0) of waste pickle liquor and resultant solubilization of toxic metal constituents are reasons why waste pickle liquor is considered potentially hazardous.

# 1.2.3 Waste Quantities

During the conduct of this study, intensive sampling and chemical analyses of steel plant residuals were carried out. Ten steel plants located in the North Central and Great Lakes region of the United States provided personnel to obtain daily samples of steel plant production and pollution control residuals, including slags, sludges, dusts, scales, and pickle liquor. These samples were shipped to the Calspan Laboratory at Buffalo, New York, where the daily samples were composited into weekly samples and then chemically analyzed. Steel plant residuals were therefore well characterized as to average chemical content and variability in composition. Results of chemical analyses from the ten steel plants are given in Appendix A.

Table 5 gives generation factors for the various residuals from iron and steel production as well as concentration factors for potentially hazardous constituents. These factors were computed by averaging all available data collected from the 10 iron and steel plants visited on generation rates and chemical analyses data from collected residuals samples of slags, sludges, dusts and other wastes.

Using the residuals generation factors given in Table 5 the yearly amount of residuals generated from a typical integrated steel plant producing 2,500,000 MT of molten steel as described in Table 4 were estimated. Quantities of potentially hazardous constituents were also calculated for the typical integrated plant. These estimates are given in Table 6.

TABLE 5 WASTE GENERATION FACTORS - IRON & STEEL PLANTS

Coke Oven - Sludge   17.6*   12.0     Blast Furnace - Slag   145   16.0     Basic Oxygen Furnace - Kish   10.14   11.72   15.7     Basic Oxygen Furnace - Kish   17.6   17.7   16.0     Basic Oxygen Furnace - Kish   17.7   17.	12	Cu 9 21.9 4 93.2 1 37.4	Concent  Mn  102  3000  8800  3700	ration Ni 5.5	Concentration Factors (ppm)	(md	
Kg/MT         Kg/MT           of Steel Kg/MT         of Steel Vg/MT           Produced of Waste         of Facility           Coke Oven - Sludge         2.6* 5.5           Blast Furnace - Slag         250* 348           Blast Furnace - Dust         11.7* 16.2           Blast Furnace - Sludge         17.6* 24.4           Basic Oxygen Furnace - Slag         145 145 12           Basic Oxygen Furnace - Bust         16.0 16.0 3           Basic Oxygen Furnace - Klsh         0.14 0.14 1	ty		Mn 102 3000 8800 3700	Ni 5.5	ractors (p)	l (md	
Type of Waste or Produced of Facility Processed Output  Coke Oven - Sludge 2.6* 5.5  Blast Furnace - Slag 250* 348  Blast Furnace - Dust 11.7* 16.2  Basic Oxygen Furnace - Slag 145 145 12  Basic Oxygen Furnace - Must 16.0 16.0 3  Basic Oxygen Furnace - Klsh 0.14 1	ty		Mn 102 3000 8800 3700	Ni 5.5 <7.5	-		
Coke Oven - Sludge       2.6*       5.5         Blast Furnace - Slag       250*       348         Blast Furnace - Dust       11.7*       16.2         Blast Furnace - Sludge       17.6*       24.4         Basic Oxygen Furnace - Slag       145       145       12         Basic Oxygen Furnace - Bust       16.0       16.0       3         Basic Oxygen Furnace - Klsh       0.14       0.17       17.7       17.7       17.7	.2 .4		3000 3000 8800 3700	5.5	Pb	Zn	Oil & Grease
Blast Furnace - Slag       250*       348         Blast Furnace - Dust       11.7*       16.2         Blast Furnace - Sludge       17.6*       24.4         Basic Oxygen Furnace - Slag       145       145       12         Basic Oxygen Furnace - Dust       16.0       16.0       3         Basic Oxygen Furnace - Kish       0.14       0.14       1	.2		3000 8800 3700	II .	30.5	96.5	203,070
Blast Furnace - Dust       11.7*       16.2         Blast Furnace - Sludge       17.6*       24.4         Basic Oxygen Furnace - Slag       145       145       12         Basic Oxygen Furnace - Dust       16.0       16.0       3         Basic Oxygen Furnace - Klsh       0.14       0.14       1	.4		8500 3700		21.5	8.2	i i
- Slag 145 145 12 - Dust 16.0 16.0 3 - Kish 0.14 0.14 1	.4		3700	57.6	302	516	ŧ
Basic Oxygen Furnace - Slag1451451Basic Oxygen Furnace - Kish0.140.14		31.3		38.4	1210	11,650	i i
- Dust 16.0 16.0 - Kish 0.14 0.14			41,600	12.2	12.0	16.2	
- Kish 0.14 0.14		202	11,400	115	7350	3350	t f
C1das 17.7		45.7	3810	56.6	137	099	i
- 34uuge 1/.3	17.3 708	174	10,300	130	4190	10,094	;
Open Hearth Furnace - Slag 243 243 2360		49.8	42,710	23.7	57.4	47.9	6
Open Hearth Furnace - Dust 13.7 13.7 568		1130	4810	314	11,650	113,000	l f
Electric Furnace - Slag 120 120 4820		79.0	50,580	53.9	32.7	80.5	4
Electric Furnace - Dust 12.8 1380		1940	42,610	246	24,220	95,710	i i
Electric Furnace - Sludge 8.7 8.7 2690		1130	34,100	421	7900	13,540	

of coke required to produce 1 MT pig iron. Coke oven sludge consists of ammonia still lime sludge and decanter tank tar. Values are averages for data from a number of steel plants. Plus or minus variation for individual plants from averages may be a factor of 2 to 3. \*Approximately 0.72 MT of pig iron required to produce 1 MT of steel (on the average). Approximately 0.66 MT

21

TABLE 5 (Continued)
WASTE GENERATION FACTORS - IRON & STEEL PLANTS

<,

	Generation Factors	Factors							
	Kg/MT of Steel	Kg/MĪ		ဌ	ncentra	stion Fa	Concentration Factors (ppm)	(md	• •
Type of Waste	Produced or Processed	of Facility Output	Çr	ņ	Ě	Ni	Pb	Zn	Oil & Grease
Soaking Pit - Slag	35.2	35.2	373	278	5280	117	760	59.3	!
Primary Mill - Sludge	1.87	1.87							!
Primary Mill - Scale	44.9	44.9	318	449	5410	385	58	32.5	10,180
Continuous Caster - Sludge	0.104	0.104		1			-	- ~	
Continuous Caster - Scale	8.7	8.7	•	-	;	-	-		1
Hot Rolling Mill - Sludge	1.74	1.74	198	232	3280	253	1050	699	45,29
Hot Rolling Mill - Scale	18.3	18.3	208	274	3170	545	154	26.9	42,240
Cold Rolling Mill - Sludge	0.16	0.16	-		 1			1	•
Cold Rolling Mill - Scale	0.052	0.052		-		-			1
Cold Rolling Mill - Waste Pickle Liquor	22.8	22.8*	12.7	7.35	179	19.2	1.1	8.3	
Tin Plating Mill - Sludge	5.32	5.32	2760	2730	1040	250	688	2260	*
Galvanizing Mill - Sludge	10.8	10.8	-	:	;	:	;	1	
Galvanizing Mill - Waste Pickle Liquor	5.17	5.17	ì	i	!	;	1	•	CHARLES AND COMMON PARAMETERS AND COMMON AND

\* Wet weight - all other factors are dry weight.

TABLE 6
YEARLY GENERATION OF RESIDUALS BY TYPICAL IRON AND STEEL PLANT\*

	Total Quantity	enò	untity o	Quantity of Potentially Hazardous Constituents	ly Hazaro	lous Const		(MT)
	of Waste (MT)	Cr	Cu	Mn	Ni	Pb	Zn	Oil & Grease
Coke Oven - Sludge	6,200	0.062	0.025	0.628	0.034	0.188	0.594	1250
Blast Furnace - Slag	557,000	26.1	12.2	1670	.4.2	12.0	4.57	1
Blast Furnace - Dust	25,900	2.40	2.42	228	1,49	7.83	13.4	;
Blast Furnace - Sludge	39,000	2.19	1.46	144	1.50	47.2	455	! !
Basic Oxygen Furnace - Slag	290,000	374	9.08	12064	3,54	3.48	4.70	, 1
Basic Oxygen Furnace - Dust	280	0.031	0.013	1.07	0.016	0.038	0.185	1
Basic Oxygen Furnace - Sludge	34,600	24.5	6.02	356	4.50	145	349	1
Electric Furnace - Slag	000'09	289	4.74	3035	3.23	1.96	4.83	i
Electric Furnace - Dust	6,400	8.83	12.4	273	1,57	155	613	i i
Electric Furnace - Sludge	4,350	11.7	4.92	148	1,83	34.4	58.9	1
Soaking Pit - Slag	54,900	20.5	15.3	290	6,42	41.7	3.26	
Primary Mill - Sludge	2,520		-		1 \$	1	-	-
Primary Mill - Scale	009,09	19.3	27.2	328	23.3	3.52	1.97	617
Continuous Caster - Sludge	82.2		t I		1			
Continuous Caster - Scale	006*9	-	:	1	ł	}		-
					**************************************			

TABLE 6 (Continued)

YEARLY GENERATION OF WASTE RESIDUALS BY TYPICAL IRON AND STEEL PLANT

0	Total Quantity	en)	antity of	Potentia	Quantity of Potentially Hazardous Constituents (MT)	rdous Cons	tituents	(MI)
Type of Waste	of Waste (MT)	$\mathtt{Cr}$	Cu	Mn	Ni	Pb	uZ	Oil & Grease
Hot Rolling Mill - Sludge	3,130	0.620	0.727	10.3	0.792	3.29	2.10	141
Hot Rolling Mill - Scale 3	32,900	6.85	9.03	104	18.0	5.07	0.886	1392
Cold Rolling Mill - Sludge	112			1			-	
Cold Rolling Mill - Scale	36.4	! !			1		i	!
Cold Rolling Mill - Waste Pickle Liquor	16,000	0.203	0.117	2.86	0.306	0.018	0.132	1.02
Tin Plating Mill - Sludge	532	1.47	1.45	0.553	0.133	0.366	1.20	. <b>(</b>
Galvanizing Mill - Sludge	1,350	i i					•	•
Galvanizing Mill - Waste Pickle Liquor	646	;		:	-		1	

24

\*Quantities calculated from generation and concentration factors given in Table 5 based on annual production figures given in Table 4. Divide by 365 to obtain daily quantities. Multiply by 1.1 to convert to short tons. Using state-by-state production capacities as previously given and waste generation and hazardous constituent factors per unit of product as previously given in Table 5 estimates were made of the state, regional, and national land-disposed wastes and hazardous constituents from iron and steel production. These estimates are given in Tables 7a to 71 for 1974, 1977 and 1983. Extrapolations of waste quantities to 1977 and 1983 were based on an annual growth rate of the steel industry (and accompanying residuals generation) of 2.1% from 1974-1977 and 2.5% from 1974 to 1977. This compares with annual growth of 2.5% predicted by the industry over the same period (Reference 9).

Tables 7a to 7c contain estimates of the total quantity of slags from all sources (blast furnace, BOF, open hearth, electric furnaces, soaking pit) which are or which will be generated in the iron and steel industry in 1974, 1977, and 1983. Although practices may vary widely from plant to plant it is estimated that approximately 90% of generated slag is processed for recovery of contained iron and steel and then sold for use as road fill building aggregate and other purposes. It may be stored for many months before use. The remainder is open dumped.

Tables 7d through 7f gives estimates of sludges generated from all sources in the iron and steel industry for the years 1974, 1977, and 1983. Approximately 55 percent of the total sludge generation originates from wet scrubbers of the blast furnace and is considered non-hazardous. Approximately 70% of blast furnace sludge is recycled to the sinter strand for recovery of iron.

Approximately 20% of the sludge estimated in Tables 7a to 7c originates from wet emissions controls on BOF furnaces, 10% of which is recycled to sinter strands. In total some 75% of estimated sludge generated is from blast furnaces plus BOF furnaces and is not considered potentially hazardous.

The remaining 25% of the sludge estimates given in Tables 7d through 7f consists of sludges from electric furnaces, galvanizing mills, primary and secondary rolling mills, lime pit sludges, and tin mill sludges. These sludges are considered potentially hazardous.

Tables 7g through 7i contain estimates of the total quantities of dust generated by the iron and steel industry for 1974, 1977 and 1983 through dry emissions controls on blast furnaces. Approximately 57% of the state, regional and national estimates consists of blast furnace dust. Approximately 90% of blast furnace dust is recycled to the sinter for iron reclamation with the remainder being placed on land dumps. Blast furnace dust is not considered potentially hazardous.

Approximately 12% of the dust generated in the iron and steel industry is from electric furnaces and is considered potentially hazardous. Electric furnace dust is not presently recycled. The remaining 31% of the dust quantity estimates given in Tables 7g through 7i consist predominantly of BOF dust with a small percentage of open hearth dust. BOF dust and open hearth dust are not considered potentially hazardous.

Tables 7j through 7l contain estimates of quantities of scale generated in the iron and steel industry from hot rolling mill, cold rolling mills, primary mills, and continuous casting mills. It is estimated that 80% of mill scales are recycled for roclamation of iron contait. The presence of high contents of oil and grease prevents complete recycle, and for the same reason causes mill scales to be a danger to the environment and be considered potentially hazardous.

Tables 7m through 7o contain estimates of the quantities of spent pickle liquor (dilute solutions of sulfuric or hydrochloric acid containing iron oxide and iron metal particles and traces of other metals) generated in the iron and steel industry. They are normally disposed of by contract disposal services but may be regenerated for reuse. Pickling liquors are considered potentially hazardous.

Generation of slags, sludges, and dusts follows production patterns. The largest producers of total iron and steel residuals and potentially hazardous wastes from the iron and steel industry are the states of Pennsylvania, Ohio, and Indiana followed by Illinois, Michigan and New York in that order. Alabama, West Virginia, California, and Utah also generate significant quantities of total and hazardous wastes.

## 1.3 TREATMENT DISPOSAL TECHNOLOGY

# 1.3.1. Current Treatment and Disposal Practices

This section will describe the prevalent methods used by the iron and steel industry for the treatment and disposal of all waste types be they considered hazardous or non-hazardous. Sections 1.3.2 through 1.3.4 will present more detailed discussions of the technologies used to treat and/or dispose of those waste streams which are considered to be potentially hazardous. Waste types are discussed with reference to the plant facilities from which they originate.

Coke Plant. Land disposed wastes from the coke plant of an integrated steel facility includes waste ammonia liquor, ammonia still lime sludge and decanter tank tar. All of these wastes are considered potentially hazardous because of the presence of phenols, and cyanides which are susceptible to leaching. The ususal treatment of waste ammonia liquor is input to biological wastewater treatment plants. This is environmentally acceptable since the toxic constituents (phenol, cyanide) will be detoxified in the biological treatment. Sometimes this waste is disposed of in deep wells.

Ammonia still lime sludge and decanter tank tar are normally disposed of by open dumping which is not environmentally acceptable because of the suspectibility to leaching of phenol, cyanide and oils.

Blast Furnace. Residuals from blast furnaces include slag, dust from dry emissions control, or sludge from wet emissions controls. Slag is usually processed for recovery of iron metal before sale as road fill,

Table 7a

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL INDUSTRY TOTAL SLAG, 1974 (METRIC TONS)

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL"	CONSTITUENTS							
_,,,,,,	GENERATED	POTENTIALLY HAZARDOUS	CONSTITUENTS	METHOD	Cr	Cu	F	Mn	Nı	Pb	Zn	
AL ABAMA	2,666,500	o	· o	SOLD AS	1,571 62	110.96	5,309.48	36,521,48	45,29	172.51	47.50	
ARIZONA	12,800	<b> </b>	1	OR BUILDING	48 79	1 58	20.21	518.05	0,87	2.49	0.9	
ARKANSAS	6,900		i i	AGGREGATE	33.38	0 55	14 14	360.52	0 37	0.23	0.5	
CALIFORNIA	1,870,500	[ [		OPEN DUMPED	1.865.20	89.91	3,581.08	36,496.00	39 16	148.06	48.4	
COLORADO	542,800	1	1 1	1	325 82	25 15	1,256 88	8,637 32	10,28	41.17	9.29	
CONNECTICUT	36,000	1 1	{ <b> </b>	1 1	138 41	4.43	57 37	1,464 22	2.44	6 94	2 7:	
DELAWARE	71,800		į <b>!</b>		306 58	744	129 44	3,231 34	4.43	8.80	5.54	
FLORIDA	30,900		1 1	l 1	148 90	244	63.06	1,563 51	1,67	1.01	2.4	
GEORGIA	46 500	ìì	ì Ì		178 37	5 70	73 93	1,886 92	3,14	8.94	3.5	
	1	}	\ \	1 1	11 93	0.20	5 06	125.26	0.13	0.08	0.20	
HAWAII	2,600	(	{ {	[ [		Į.	Į	88,756 10	111.59	401.61	113.3	
ILLINOIS	4,597,700	1		[ ]	4,663 26	250 80	10,158 10	· '		_	1	
INDIANA	9,931,400	} }	/ <b>1</b>	1 1 1	7,260 61	446 80	22,558 00	178,180 00	182.32	711.97	196.1	
KENTUCKY	782 000	1 1	1		823 58	44 44	1,894 40	16,647 20	19 /5	71.84	19 10	
MARYLAND	3 192,900	} }		<b>, ,</b> ,	2 396 25	142 29	6,453 48	52,459 10	58 76	227.84	66.0	
MICHIGAN	4,511,200	[ ]			2 706 97	209 79	10,431 90	71,637 30	86 17	341.56	78.8	
MINNESOTA	25,300	] ]		] ]	121 31	199	51.39	1,273.83	1.38	0.82	2.00	
MISSISSIPPI	8,700	1 1	1 1	i i i	42 06	0.69	1761	441 65	0.47	0.29	0.70	
MISSOURI	147,900	<b>!</b> !	ł <b>i</b>	<b>,</b>	568 12	16 18	235 47	6,009 86	10 01	28.48	112	
MEM TEUREA	62,000	, ,	i I	1 1 1	264 68	6.42	110 89	2 789 73	3.82	7,59	4.8	
NEW YORK	2 /28 300	1 1			1,467 88	122.41	18 841,8	42 111 40	49 00	200.88	43 40	
A CARDINA	20,600	1 1	1 1	) )	157.53	2 02	n2 18	1,293.9#	136	0.84	3 04	
OHIO	11 114 100	{ {	( (	(	10,446 10	bb4 32	2133600	210 113 00	239 37	#93 66	270 BI	
UKLAHUMA	29 400	{	1 1	1 1 1	141 54	2 32	59 96	1,486 36	1 140	0.96	2.3	
DHEGON	48,300	1 1	1 1	1 1	177 96	5 69	73 76	1,882 45	3.13	8 92	35	
PENNSYLVANIA	14 033 500	1 1	1 1	1 1	13 010 20	700 38	29,990 00	270,448 00	298 43	1,141.38	338.8	
S CAROLINA	41,600	} }	}	}	200 24	3 28	84 80	2,102 80	2.24	1.36	3.30	
TENNESSEE	14,800	[ [	l l		70.56	1.15	29.84	740.90	0.79	0.48	1.10	
TEXAS	977,500	1 1		] [	2,362.68	83.27	1,747.62	30,808.40	42.36	134,58	50.61	
UTAH	1,308,400	[	i 1	1 1 1	1,483 85	67 45	2,486 87	28,081.30	28.93	113.06	39.00	
VIRGINIA	10,900	{ }	<b> </b>	}	41.97	1.34	17 40	444.01	0.74	2.10	0.8:	
WASHINGTON	62,500	{ }	l	1 1 1	316 90	10 13	131 35	3,362 33	5.58	15.88	6.20	
W VIRGINIA	1,769,700			! <b>∳</b> i	904 53	67 32	4,401.98	28,851.20	26.12	P6,83	24.51	
EPA REGION	<del>}</del>	} <b>}</b>	<del>  </del>	· · ·		<del>                                     </del>	<del> </del>	<del> </del>	<del>}</del>	<del> </del>		
		} }	<b>\</b>	}		·			١		<b>.</b>	
I	36,000			[	138 41	4 43	67.37	1,464.22	2.44	6.94	2.7	
п	2,790,300	( (	[	[	1.732 56	128.83	6,467.50	44,921.13	52.82	208,45	48.2	
m 	19,078,800			!	16,869 53	918 77	40,991.30	366,433 66	368.48	1,476.95	437.8	
DV	3,816,400	) }	1 1	}	3,158 46	170 69	7,585 66	61,197.96	74 73	267.27	80.0	
<b>X</b>	30,179,600	<b>,</b>	{		25,188 15	1,462 50	66,536.38	549,960.23	618.81	2.349.64	0.000	
721	1,013,800			į į	2,537.60	86.14	1,821 72	32,445.27	44.33	135.78	53.6	
VIII	147,900				568 12	18 16	235 47	6,009.85	10 01	28,48	11.2	
MII	1,861 200	1	1		1,809 67	92 60	3,743 75	36,718 62	39.19	154.23	48 3	
nx ~	1,686 800		1 1	(	1 925 91	91 69	3,606.31	37,137 31	40 16	160.62	478	
x	128,800	l l	[ [		494 86	16 82	205 11	5,234 78	871	24.80	97	
MATIONAL TOTALS	60,526,600		1	i " 1	54 213 26	2,000 43	131,249 48	1,130,622 7	1,279.66	4,763.16	1,300.4	

<sup>\* 90%</sup> OF \$LAG IS PROCESSED FOR RECOVERY OF METALLICE AND THEN SOLD FOR USE AS ROAD FILL, ETC HEMAINDER IS LAND DISPOSED, AND/OR USED AS FLUX SLAGE FROM 81 AST FURNACES, OPEN HEARTH FUNNACES, BASIC COVERN FUNNACES, ELECTRIC FURNACES, AND SOAKING PITS MOT CONSIDERED HAZARDOUS ON THE BASIS OF CALSPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX S

SOURCE CALSPAN CORPORATION

Table 7b
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM IRON AND STEEL INDUSTRY
TOTAL SLAG, 1977 (METRIC TONS)

STATE	TOTAL	TOTAL	TOTAL HAZAHDOUS	DISPOSAL*			í.c	NSTITUENTS			
The second second section is a second section of the second section se	GENERATED	POTENTIALLY HAZARDOUS	CONSTITUENTS	METHOD	C:	Cu	F	Mn	Nı	Pb	Zn
ALABAMA	2,826,500	o	0	SOLD AS	1,865.81	11/62	5,691 66	38,712 50	48.01	182 86	50 45
ARIZONA	13,520		1 1	ROAD BASE	51 70	1 67	21 42	547.01	0.92	2.64	1 02
ARKANSAS	7,350	1 1	ł <b>ł</b>	BUILDING	35 38	0.58	14 99	371 55	0.40	0.24	0.59
CALIFORNIA	1,771,000		1 1	AGGREGATE OR	1,977 11	95 31	3,795 91	38,685 87	41.51	156.93	49.27
COLORADO	575,400	1	1 1	OPEN	345 37	26 66	1,332 29	9,156.56	10.87	43.64	9.80
CONNECTICUT	38,200	<b>(</b>	l I	DUMPED	146 72	4 60	60 81	1,652 07	2.58	7,36	2 90
DELAWAPE	76,130		[ [		324 97	7 89	1.35.14	1,426 22	4 69	¥ 32	5 93
FLORIDA	32,770	[			157 83	2 69	66.84	1,857.32	177	1 07	2 84
GEORGIA	49,230	{			189 07	6 06	78 37	2,000 14	3.33	9.48	3 73
HAWAH	2 625	<b>S</b>	<b>!</b>		12 64	0 21	5 30	132 78	0 14	0 00	0.21
ILLINOIS	4,873 500	1	1	1	4,94106	265 63	10 768 65	94.081 47	118 29	425 70	120 18
INDIANA	10,627,300		}		7,685,54	473 61	23,911 69	188,870 80	193.25	754 69	207.88
KENTUCKY	829 000	1	<b>)</b>	) ]	872 99	47 11	2 008 06	17 646 03	20 84	76 16	20 31
MARYLAND	3 384,500				2,540 03	150 82	6,840 69	5,566 65	62 28	241 51	72 09
MICHIGAN	4 781,900	i	j j	1 1	2,869 39	221 32	11,067.81	76 935 54	90 28	362 05	81 48
MINNE SOTA	26 700	1	]		128 59	2 11	54 46	1 350 26	144	0.87	2 15
MISSISSIPPI	9.256		1	1 1	44 68	0/1	18 88	408 15	0.50	0 30	0.75
MISHOUNE	156 800	) <b>)</b>	1	1 1	602 21	19.25	249 60	6 170 44	10 61	30 19	11 89
VEW JERREY	96.730	1	1		280 66	881	117.04	2 96/11	4 96	8.06	5.12
NEW YORK	2,892,000	,	1		1,555 95	129.76	6,738.01	44.659 28	6193	212.81	46 01
N CAROLINA	2/ 120	1			130 62	2 14	55.32	1,371 62	146	0.89	2 18
OHIO	11 /81.000			{ {	11.072.87	687 58	24,735 10	222,719.78	262 67	94731	286 92
OKLAHUMA	31,180	1	1 1	1 1	160 03	2 48	63 56	1.575 53	1 68	1.02	251
OREGON	49.120				188 63	8.03	78 18	1,995 40	3 32	9.48	373
PENNSYLVANIA	14,876,500	i I	1		13,790 81	1	31,789 72	285,674.90	316 23	1,209,86	359.15
RHODE ISLAND	NA.		[	1 1	NA NA	742 41 NA	1	NA	į i	NA.	t
S CAROLINA	44,060		\ <b>\</b>		(	3 48	NA ma na	2.228 82	NA 2 38	144	NA 3 55
TENNESSEE	(				212 26 74 79	ţ	89 89		0.84	051	1.26
	15,530			1	2 504 44	88 27	31 67 1,852 48	785 35 32,444 90	44 92	142.66	53 72
TEXAS UTAH	1,036,100		<b> </b>	1	<b>§</b>	1	1 '	, ·	30 66	í	41.41
	1,386,900	1	<b> </b>	1 1	1,572 88	71 50	2,636 06	29,766 18	1	119,84	<b>1</b>
VIRGINIA	11,590	1	}	1 1	44 49	1 42	18 44	470.65	0.78	2.23 16 84	0.88
WASHINGTON W VIRGINIA	87,470			1 1	336 91 958 80	71 38	139 23	3,553 47 30 582 27	5 92 27 68	102 64	26 07
EPA REGION	1,875,900			- <del>-</del>	908 90	/136	4,000 10	30 582 27	27 66	102 04	7807
	1	1								1	
I	38,200			1	146 72	4 69	60 81	1,552 07	2 58	7 35	2.90
n	2,957,730				1,836 51	136 56	6 865 55	47,616 39	55 98	220 96	51 13
ш	20,223,620		l <b>l</b>	(	17,659 10	973 90	43,451 00	376 759 69	411 76	1,565 56	464 12
IX.	3,833 465	1	i		3,347 96	180 95	8 040 68	64,869 93	79 23	272 71	84.86
₹	31 990 400				26,699 45	1 550 25	70,527 71	582,957 85	66 6 93	2,490 62	698 61
<b>V</b> I	1 0/4 610	•		1	2 689 85	9131	1,931 03	34 391 98	47.00	143 92	5e 82
VIII	156,800			1	602.21	19 75	249 60	6 170 44	10 61	30 19	1189
YIII	1,962 300				1 918 25	98 16	3 9Aci 37	38 921 /4	4153	163 48	51 21
134	1 /8/ 145		1	1	2,041 45	97 19	3,822 69	39,365 66	42 57	159 86	50.50
x	136,590		<b>.</b>		524 54	18 77	217.41	5,648 87	9 24	26 30	4.36
NATIONAL TOTALS	64 160 880			1	57,466 03	3 189 03	139,124 94	1,198,354 3	1,356 43	5,000.75	1,478.40

\*DISPOSAL PRACTICE FOR 1977 IS EXPECTED TO BE ESSENTIALLY THE SAME AS CURRENT PRACTICE (SEE 1974 SEA) AS LABLET INCLUDE SELAIS FROM BLAST FRIBACES OF IN HEARTH FURNACES BASIC OXYLEN FRIBACES, ELECTRIC FRIBACES AND SOAKING PITS SLAG CONSIDERED NON HAZARIDOUS ON BARIR OF CALRPAN BOLUBIL ILY TESTS OF SCRIPE O IN APPENDIX II

SOURCE LAI SPAN COMPONATION

Table 7c
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL INDUSTRY
TOTAL SLAG, 1983 (METRIC TONS)

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL*	Ĺ			CONSTITUEN	75		
	GENERATED	POTENTIALLY HAZARDOUS	CONSTITUENTS	METHOD	Cr	Cu	F	Mn	Nı	Pb	Zn
ALABAMA	3,279,800	0	0	SOLD AS	1,932 97	136 48	6,604 46	44 921.08	56 71	212 18	54 5
ARIZONA	15 700		1	HOAD BASE	59 99	194	24 85	634 74	1 06	3.06	1 11
ARKANSAS	9,500	1	1 1	BUILDING	41 06	0 67	17 39	431 14	0.46	0.26	9 0
CALIFORNIA	2 054,700			AGGREGATE OR	2,294 20	110 59	4,404 59	44,890 20	48 17	182 10	57 1
COLOHADO	667,700		1 1	OPEN DUMPED	400 78	30 93	1,545 96	10 623 90	12 61	50.84	113
CONNECTICUT	44 300	1 1		<b>! 1</b>	170 26	5 44	70 67	1,800 99	3 00	8 53	3.3
DELAWARE	88,300	]	]	]	377 00	9 15	157 08	3,974 66	5.44	10 82	0.4
FLORIDA	38,000		1		183 14	3 00	77 56	1,923 12	2 05	1.24	3.0
GEORGIA	57,100			1 I	219 40	7 01	90 94	2,320 91	3.87	11,00	4.2
HAWAH	3,000		1 1	! <b>!</b>	14 67	0,24	6 21	154 07	0 16	0 10	62
ILLINOIS	5 866,100				5,735 81	308 23	12,495 69	109,170 00	137 26	493 97	139 4
NDIANA	12 215,600		1 1	1 1	8,918 13	549 56	27,748 50	219,181 40	224 25	875.73	241 2
KENTUCKY	981,900		}	, <u>(</u>	1 013 00	54 86	2,330 11	20,476 06	24 29	88 37	23 5
MARYLAND	3,927,300	]	] <b>]</b>	<b>]</b>	2,947 39	176 01	7,937 78	64,524 69	72 27	290.25	83 6
MICHIGAN	5,548,800			'	3,329 67	256.82	12,831 24	88,113.88	104 76	420.11	94.6
MINNESOTA	31,000				149 21	7 46	63 19	1,566.81	1 67	1 01	2.4
MISSISSIPPI	10 700	i	ĺ		61 73	0 86	21 91	543 23	0.58	0.36	0,0
MISSOURI	182 000				698 79	22.34	289 83	7.392.12	12 31	26.07	13.6
NEW JE HREY	76,300	1		! !	326.66	7.90	1,16.39	3,431.37	4 20	9.34	6.5
NEW YORK	3 365 800				1 805 49	150 56	7 818 63	6182182	60 26	24 / 06	53 3
V CAROLINA	31,500		1	} <b>j</b> j	161 67	249	64 20	159100	170	1 103	2.5
оню	13 670,300	1	1	1 1	12,842 70	68181	28 702 06	258,439 00	293 19	1,099 23	332 9
DK LAHOMA	36,200			<b> </b>	174 09	2 86	73.75	1,828 21	1 96	1 18	2 9
DREGON	67,000		1		218 88	7 00	90.72	2 315 41	3 86	10.97	4.3
PENNEYI VANIA	17 261,200			1	16,002 56	86147	70 888 PF	332,661.00	367.07	1 403 90	416 /
MODE ISLAND		1	!			}				1 1 1 2 2	1
AHOLINA	51 100	ļ			246 30	4 04	104 11	2 586 27	2.16	1.67	41
CENNETSEE	In 000	1	·		86 79	1 12	to 75	911 40	0.97	0.44	1 14
II KAS	1 202,300	i	,		2.906 10	102.43	2 149 57	37 648 33	52 12	165 54	823
JIAN	1 609 300		(		1,825 14	82 97	3,058 85	34 540 00	35 58	139 06	48.0
VIRGINIA	13,400	1	1		51 62	1 65	21 40	546 13	091	2 59	10
NASHINGTON	101 500				389 78	12 46	161 56	4 123 37	687	19 54	77
W VIHGINIA	2 176 700	1	}	<b>!</b>	1 112 57	82.81	5 4 14 44	J5 486 96	32 12	119 10	30 2
- EPA HEGIUN	1 1	1	1 1		···	-				-	†·
1	44 300	l			120.26	5.44	70 67	1 200 00	300	0.67	١,,
ū	3 432,100				170 25 2,131 05	5 44 158 46	7,956 02	1,800 99 55,252 99	3 00 64 96	8 53 256 40	593
ш	23,486,900	)			20,491.22	1,130 09	50,419 87	437,183 35	477.81	1,816.66	538.5
IX	4,448,100			[	3,884 90	209 95	9,330 24	75,273 67	91.93	316.43	
¥	37,120,800				30,98142	1,798 87	81,838 76	676,451.09	761 13	2,890 06	98,4 810,6
VI.	1,247,000				3 121 26	106 96	2,240 71	39,907 86	54 53	167.00	66.9
AUI.	182,000				098 79	72 34	289 63	7,392 12	12 21	36 07	
VIII	2 277 000			Ì		]	]	j ·	ì	l .	13.6
131	2 073,400				2,225 90	11190	4 604 81	46 163 90	48 19	189 /0	50 4
X	168,600				2,368 86 606.66	112 77	4,436 75 252 28	45,879.01 6,438.78	10 73	195 28 30 51	12.6
ATIONAL TOTALS				1			102.00		1		1

\*DISPOSAL PRACTICE FOR 1863 IS EXPECTED TO BE ESSENTIALLY THE SAME AS CURRENT PRACTICE (SEE 1974 SLAG TABLE) INCLUDES SLAGS FROM SLAST FURNACES, OPEN HEARTH FURNACES, BASIC OXYGEN FURNACES, FLECTRIC FURNACES, FADS OAKING PITTS SLAG CONSIDERED NONHAZARDOUS ON BASIS OF CALSPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX B

Table 7d

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM THE IRON AND STEEL INDUSTRY

TOTAL SLUDGE, 1974 (METRIC TONS) DRY WEIGHTS

STATE	TOTAL	TOTAL POTENTIALLY	TOTAL HAZARDOUS	DISPOSAL*	L			CONS	TITUENTS				OIL	PHEN
	DENEMATED	HAZARDOUS	CONSTITUENTS	me mod	Cı	Cu	Mn	Ni	Pb	Zn	Ca	8	GREASE	
ALABAMA	198,300	49,680	1,926.43	OPEN	34 13	16.96	860 38	13.76	309 07	1,999 71	2 68	228.48	4,202.32	38.
ARIZONA	302	76.6	299	DUMP OR	0 25	0 16	347	0 11	0 68	1.04	NA	0 29	5.97	NA.
ARKANSAS	141	36.3	190	RECYCLE	0 15	0.042	2 01	0.06	0 49	074	NA.	0.20	3.87	N/
CALIFORNIA	97,740	24,430	996 28	! !	24 60	15 89	471.58	9 71	190 12	1,200.71	1 13	113.67	1,941 81	16
COLORADO	43,840	10,900	393 86	l l	11 11	4 33	226.84	3 66	\$0.65	39137	G.48	57 73	780.55	•
CONNECTICUT	088,2	478	\$ 68		0 72	047	9 94	0 31	194	2 96	NA	0.81	17 55	N/
DELAWARE	1,600	400	18 13		1 50	0 87	20 17	0.54	4 39	8 64	NA	1.82	30.54	N/
FLORIDA	850	213	7 68	1 1	0 08	0.33	3 68	0 18	2 11	3.24	NA	68.0	14 61	N
GEORGIA	1,400	360	10 96	1	0 93	0.59	12 69	0.38	2 50	3.82	NA	1.05	21.86	N/
HAWAII	87.5	219	1 17	) j	0.06	0.04	0 84	0 03	0.23	0.29	NA	0 07	3.15	N
ILLINOIS	321 300	80,330	3,022 05	1 1	97 82	38 76	1 758 59	30 74	609 96	3,021.82	3.56	420 58	6,065.77	50
INDIANA	735,900	184,000	6,844 98	{	211 23	120 96	3,564,48	64 44	1,365.19	7,503.68	8.23	902.84	13,831.70	117
KENTUCKY	60,640	15 160	512 74		18 77	7 46	346 61	6.04	120 42	502.54	0.54	81.23	969.76	7
MARYLAND	109,060	27,270	2,148 59		38 71	24 48	901 38	16 20	349 30	2,426.56	2.98	236.71	4,567.36	40
MICHIGAN	349,100	87,280	3,275 00		92 18	36 03	1,900 32	30 47	689 00	3,262.47	4 03	479.20	6,878.90	57
MINNESOTA	514	129	4 40	} }	0 56	0 29	7 32	0 17	1 77	2.66	NA	0.73	14.06	N.
MISSISSIPPI	487	122	2 39	} }	0 19	0 10	2 54	0.06	0.61	0 93	NA	0.25	4.87	N.
MISSOURI	3,950	968	34 89		2 96	1 89	40 41	1 23	7 96	12.16	NA	3.34	88.42	N
NEW JERSEY	1,590	. 398	15 68	1	1.30	0.75	17 43	047	3 78	5 76	NA	1.57	31.67	) N
NEW YORK	217,000	54,250	206		56,97	21.62	1,159 47	18 42	410.47	2,000.63	2.48	294 62	4,026.55	36
N CAROLINA	452	113	6 35		0.56	0 27	7 18	0 15	1 74	2 58	NA	0.74	12 10	N/
OHIO	719,200	179 800	7,208 70		167 33	100.26	2,390 30	84 51	1,290 03	6,031.48	8.85	840 96	14,815 10	126
OKLAHOMA	600	150	8 04	1	0.65	0 33	8 54	0 19	2 06	3 12	NA	0.85	16 40	N/
OREGON	1 100	275	10 93		0 92	0.66	12 66	0.38	2 49	3 81	NA	106	21.81	N/
PENNBYLVANIA	901 300	225,300	9,000 13		218 48	130 06	4.311 72	81 64	1,865 19	10.242 10	10 61	1,073 62	18,111,40	156
RHODE ISLAND	204	510	0.03	1	NEGLI	•	0 02	_	NEGLIGIBL		NA	NA	011	N/
S CAROLINA	970	243	10.37	'	091	0.45	11.83	0 25	2.84	4 36	NA	1.20	19.65	N/
TENNESSEE	500	125	401	! ]	0.32	0.17	4 26	0 10	103	156	NA	0.42	8.18	N/
TEXAS	33 650	,			11 60	961	200 71	5 83	67.55	449.43	0 33	29 88	762.09	1
UTAH	61,360	8 4 10	385 45	1	6 85	9 10	213 50	5 41	106 84	1 005 33	0 92	55 03	1 510 50	13
VIRGINIA	260	15,340 65.0	731 38 2 5 7		0.22	0 14	213 50	0.00	0.59	0.96	NA	0.25	5 14	N.
WASHINGTON	1961	65 0 491	258 1946		1.05	1.06	27 54	1168	1.4	1 6.28	NA.	1 86	IN R4	l No
W VIRLINIA	197 100	19 1 101	1 1860 20,	1	117 88	17.76	R16 /0	14.70	20136	: 1 (64.28	1 60	204.55	2 631 11	22
FPA REGION	}		1 1111/2/1			1		1			!		1	,
FEM REGION	1					1	1	1	1	}	1			Ì
1	2 084	521	R 71		0/2	047	9.98	0.11	194	2.98	NA	0 #1	17 66	N/
n	218,590	'A 648	17.74		1.7.27	27 37	1,176 90	18 HG	414.25	2,006.28	2 48	296 19	4 058 /2	,15
20	1 200 520	297 386	12 629 68		316 25	18781	6 083 05	113 17	2,312,81	14,040,49	16.37	1,816 96	25,343.76	216
17	263,600	\$5,906	2,480 93		56 46	26 33	1,264 17	20 91	440.32	2,518.84	3.22	314.26	8,243.36	45
¥	2 126 014	531,639	20,365 13		559 10	296.30	10,621 01	190 33	3,925 96	21,812 13	24 67	2,644 31	41,005.62	361
201	34,391	8,596	396 39	' i	12.40	10 02	211 26	6 17	70 10	453 29	0.33	30 93	782.36	4
था	3 950	988	34 89		295	189	40 41	1 23	7 95	12 16	NA	2 34	66.62	N/
VIII	105,300	28,320	1,125 03		17.96	13.43	442 34	9 06	187 49	1,396 70	1.40	112 76	2,300.05	19
11%	98,130	24 527	1,000.44		24 91	16 09	475 89	985	191 01	1,202 04	1 13	114 03	1 960 73	18
x	3,063	786	30.39		257	1 64	35 20	106	6 92	10.59	NA	291	50 65	N/
NATIONAL TOTALS	4 124,612	1,006,175	37 978 33		1.060 59	576 36	20,320.20	370 98	7.588 74	43,455.48	48 60	5,036 49	80,831 02	602

<sup>\*</sup>APPROXIMATELY 85 PERCENT OF THE TOTAL SLUDGE IS FROM THE WET SCRUBBERS ON THE BLAST FURNACES PROBABLY MORE THAN 70 PERCENT OF THIS IS RECYCLED VIA SINTERING OR OTHER ADGLOMERATING PROCESSES ABOUT 20 PERCENT OF THE SLUDGE IS FROM BABIC OXYGEN FURNACES. ~ 10 PERCENT OF WHICH IS CURRENTLY RECYCLED BLAST FURNACES SLUDGE AND BOF SLUDGE ARE NOT COMBIDERED HAZARDOUS THE REMAINING SLUDGE 128% OF TOTAL GENERATED IS LAND DISPOSED AND COMBIDERED HAZARDOUS THIS CONSISTS OF SLUDGES FROM BLECTRIC FURNACES GALVANIZING MILLS PRIMARY AND SECONDAHY MILLS, DECANTER SLUDGE, LIME PIT SLUDGE AND TIN MILL SLUDGE

NOTE NA DENOTES THAT DATA WERE NOT AVAILABLE

Table 7e ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM THE IRON AND STEEL INDUSTRY TOTAL SLUDGE, 1977 (METRIC TONS) DRY WEIGHTS

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL*				CONST	ITUENTS				Oir	PHENO
	DENERATED	POTENTIALLY HAZARDOUS	HAZARDOUS CONSTITUENTS	METHOD	Cr	Cu	Min	N4	Pb	Zn	Cn	F	GREASE	
AL ABAMA	210,200	52,560	2,042 02	OPEN	36 18	17 98	912 00	14 58	327 62	2,119 60	0.84	242 19	4,454.46	40.1
ARIZONA	320	80	117	DUMP OR	0 27	0 17	3.78	0 11	0 72	111	NA	0.30	6.33	NA.
AHKANSAS	160	38	20	RECYCLE	0.18	0.00	2 14	0.06	0 52	0.78	NA	0.21	4 10	NA
CALIFORNIA	103 610	26,900	1,0ne 0s		26 08	16 84	490 88	10.29	201 53	1,272 78	1.20	120 48	2,058.11	17.
COLORADO	46 570	11,840	417 27		11 78	4 59	242 57	3.87	85.48	414.86	0.61	61.20	636.92	7.
CONNECTICUT	1,990	408	9 20		0 77	0 60	10,54	0 23	2.06	3 14	NA.	0.96	18.61	NA.
DELAWARE	1,700	426	19 21		1 59	0 92	21 36	0 67	4 64	7.06	NA	1.93	38.76	N.A
FLORIDA	900	226	8 14	ļ	0 70	0.35	9.20	0 19	2.23	3,44	NA	0.96	15.40	N/
GEORGIA	1,490	373	1161		0 98	0 63	13 46	0.41	2 65	4.06	NA	7 71	23 17	N/
HAWAII	93	23	1 24		0 07	0.04	0 89	0.03	0 23	0 31	NA	0.08	3 34	N/
ILLINOIS	340,560	85,140	3,203 37		93 09	4108	1,864.11	32 58	846 56	3,203,13	3 77	445.82	6,429 72	53
INDIANA	780,000	195,000	7,255 67		223 91	128 22	3,778 35	68.31	1,436 50	7,963.90	8.73	967.01	14,343 00	124
KENTUCKY	84,280	16,070	543 51	\ \	19 89	791	367 41	6 40	127 84	532.69	0.67	86 10	1,017.34	
MAHYLAND	221,600	55,400	2,277 61		41 03	25.95	965 46	17 17	370 26	2,572 14	3 04	250.91	4,830 79	43
MICHIGAN	370,000	97 500	3 471 50		97 69	38 19	2,014 34	32.29	709 14	3,447.62	4.27	507.95	8,973 73	80
MINNESOTA	545	136	7 30		0.69	0 30	7 78	0 10	1 07	2.84	NA	0 77	14 90	, N
MISSISSIPPI	517	129	2 83		0 20	0 10	2 60	0.06	. 0 00	0 96	NA.	8.27	8 17	N/
MISSOUHI	4,190	1,060	36 98		3 13	2 00	42 84	1 30	8 43	12 86	NA	3.54	73.80	N/
NEW JERSEY	1,680	420	16 67	1	1,37	0.80	18 48	080	4 00	6 10	NA	1.67	22.57	N/
NEW YORK	230 000	57 500	2 126 73		59 33	22 92	1 229 04	19 53	436 10	2 120 66	2 63	312 20	4,268 14	37
N CAROLINA	480	120	8 74		5 50	0 29	7 82	0 15	1.85	2.85	NA.	0.78	12.82	) N
оню	782,300	190,580	7,641 23		177 36	106.27	3,593.72	68 38	1 367 43	8,513 37	9 38	891.42	15,704 00	123
OKLAHOMA	636	159	8 77		D 89	0.36	9 06	0 20	2 19	3 31	NA	0 90	17 38	N/
OREGON	1,170	293	1158		0.98	0.63	13.42	041	2 64	4 04	NA.	1 11	23 12	N/
PENNSYL VANIA	965 400	238 850	9,540 13		231 56	137 87	4,570 42	86.54	1,765 10	10,856 63	11 57	1,248 04	19,196 10	184
HHODE ISLAND	716	54	0.04		NEGLI		0 02		NEGLIGIBI	£	NA	NA	0 12	N/
S CAHOLINA	1 030	258	11 00		0.96	0.48	12.54	0 27	301	4 63	NA	1.27	20.83	N/
DENNESSEE	5.29	132	4.25		0.34	0.18	4.51	0.10	1.09	1 65	NA	0.45	8 67	NA.
TENAS	35 670	8 970	408 57	1	12 30	10 19	212.75	6 28	71 60	476 40	0 36	31 67	807 81	4
U.AH	65 040	16 260	225.27	.	7 26	9 64	226 31	5 73	113 25	1 065 65	0.97	58 33	1,600 08	13
VIRGINIA	276	69	2 /3	1	0 23	0 15	3 16	010	0.62	0 95	NA	0.26	5 45	N/
WASHINGTON	2,080	520	20 63	1	1 75	1 12	23 90	0.72	470	7 19	NA	197	41 17	NA.
W VIRGINIA	166,700	41,680	1.441 88	. 🗼	60 80	34 20	965 BO	15 58	310 95	1,446 14	170	216.83	2,791 31	24
FPA REGION	<del>                                  </del>						<u> </u>	-	<del> </del>	<del></del>	f	ļ ————	+	1
									İ	l	l			١.
1	2 206	562	9 24		0 77	0 60	10.56	0 33	2 06	3 14	NA	0 86	18 73	N/
п	231,680	57,920	2,143 35		60 70	23 72	1,247 52	20.03	439 10	2,126 66	> 2.63	313.96	4,301 71	> 37
111	1,345,876	336,424	13 281 46		336 21	199 09	6,416 22	119 96	2,451.57	14,882 92	>16.31	1,807.97	26,864.40	>232
IV.	279,426	69,867	2,829 80		59.83	27 92	1,329 42	22.16	466.74	2,669.98	> 3.41	333 12	6,567.96	>48
V	2,263,405	563,366	21 579 07		592 84	314 06	11,258 28	201 74	4,181 50	23,120 88	>26 15	2,802 97	43,486 96	>372
AI.	38,458	9,117	419 34		13 16	10 62	223 94	8 63	74 31	480 49	>0.36	32.78	829.29	>4
A311	4,190	1,050	36 98		3 13	2 00	42.84	1 30	8 43	12 89	NA	3 54	73.80	N/
VIII	111 610	27,900	1,192 54		19 04	14.23	458.86	9 60	198 73	1,480 50	1 48	119 53	2,437 00	21
nx.	104,023	26,003	1,060 47		26 42	17 06	504.55	10 43	202 48	1,274 17	>1 20	120.86	2,067.78	> 17
X	3,250	813	32 21		2 73	1 76	37.32	1 13	7 34	11 23	NA	3.00	64.29	N/
ATIONAL TOTALS	4,371,922	1,092,992	42,384,46		1,113.67	610 84	21,530.53	393 21	6,012.26	46,062 84	) 51.53	5,330.67	85,880.90	>724

<sup>&</sup>quot;DISPOSAL METHODS WILL PROBABLY FOLLOW PRESENT PRACTICES (SEE 1974 TABLE) WITH GREATER TENDENCY TOWARD RECYCLE NOTE: NA DENOTES THAT DATA WERE NOT AVAILABLE

Table 7f
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM THE IRON AND STEEL INDUSTRY
TOTAL SLUDGE, 1983 (METRIC TONS) DRY WEIGHTS

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL*	}			CONST	ITUENTS				OIL	PHENC
er administrative mentalisment	GENERATED	POTENTIALLY HAZARDOUS	HAZARDOUS CONSTITUENTS	METHOD	Cr	Cu	Min	Ni	Ръ	Žn	Cn	p.	GREASE	
ALABAMA	243,980	60,990	2,369.51	OPEN	41.86	20 67	1,058.26	169:	380 16	2,459.64	3 30	281.03	5,100.85	47.0
ANOSIR.	371	93	3 68	DUMP	0.31	0.20	4 27	0 13	0 84	1 26	NA	0.36	7.36	NA
ARKANSAS	174	44	2.33	RECYCLE	0.19	0 10	2 48	0.046	0 60	091	NA	0.25	4.76	NA
CALIFORNIA	120,200	30,060	1,225 43		30.26	19 56	580 06	11 94	233.85	1,476.87	1.39	139.81	2,308.18	19.
COLORADO	54,040	13,510	484 19		13.67	5 33	281 47	4 49	99 19	481 36	0 59	71 01	971 15	8,
CONNECTICUT	2,310	578	10 68	] ]	0.89	0.58	12 23	0.39	2 39	3 65	NA	1.00	21.50	NA
DELAWARE	1 970	493	22 30	} }	185	1 07	24 81	0 67	5 39	8 19	NA	2.24	44.97	NA
FLORIDA	1,040	260	844	( <u> </u>	0 82	0 40	10 68	0 23	2 59	3 99	NA	1 16	17.98	NA
GŁORGIA	1 730	433	1347	( (	1 14	0.73	15 61	0.47	3 07	4 70	NA	1 20	26 89	NA
HAWAII	108	27	1 44		0.08	0.04	103	0 03	0 26	0.345	NA	0.00	3.60	NA
ILLINOIS	396 180	98 790	3 /17 17	} }	108 02	47.67	2 163 07	3/87	750 26	3 716 84	4 36	61731	7,460 90	62.
INDIANA	905,100	226 280	8,419.32	1 1	259 82	148 78	4 384 31	79 27	1 656 63	9.229 63	10 12	1,110 50	16,643 99	144.
KENTUCKY	74,590	18,650	630 67		23 00	9 16	428 33	/ 43	148 12	618 12	0 66	98 91	1,180.50	8
MARYLAND	157,140	JU 290	2,642 77		47 81	30 11	1 108 69	19 93	479 84	2,984 66	3 62	201 16	5,606 64	50.
MIGHICAN	429 400	107 (60	4 028 26		113.36	44 31	2 337 39	17.47	#22 B7	4 000 54	4 95	589 42	8,002 16	70
PINNESOTA	fi 32	10.8	8.47	1	0 68	0 38	9 00	0.20	117	3 29	NA	0 90	17.39	MA
M 88188(PP)	800	ino		1	0 24	012	3 12	0 07	0 7h	1 14	NA	0.31	1.00	NA
M: sacrett	4,860	1 120	4291		3 63	2 37	49 11	191	414	14 94	NA	411	85.64	NA
NEW JERSEY	1,960	488	19 29	) )	1 80	0 03	21 44	0 58	4 66	707	NA	1 23	30.96	NA
NEW YORK	267 000	66,750	2,467 8			28.59	1,426 15	22 00	2 460 66	2,460 65	3 0%	362.36	4,952.06	43
N CAROLINA	556	139	/82		0 44	0 33	9 84	U 1#	2 14	3 30	NA	0.81	14 88	NA
оню	884,600	221 150	8,896 7	, ,	206 81	123 32	4 170 07	79.36	1,586 /4	9,878 72	10.89	1,034 38	18,222 00	156.
OKLAHOMA	/38	185	9.69		0.80	041	10 50	0 24	2 54	3 84	NA	106	20 17	NA
OREGON	1,366	339	13 44		1 14	073	15 57	0 47	3 06	4 69	NA.	1.29	28.82	NA
PENNSYLVANIA	1,108,600	277,150	11.070 15	1 1	266 70	159 98	5,303 42	100 41	2,048 18	12,597 80	13.42	1,320 58	22,277.00	191
RHODE ISLAND	251	63	0.04	1	NEGLIG	BLE	0.02		NEGLIGIBL	E	NA	NA	0.14	NA
S CAROLINA	1 193	298	12.76		1 11	0 56	14 55	0.31	3 49	5 37	NA	1.48	24.17	NA
TENNESSEE	614	164	493		0 40	0.20	5 24	0 12	1 26	191	NA.	0.52	10.06	NA
TEXAS	41,390	10.360	474 10		14.27	11 82	246 88	7 29	83 09	562 dQ	0.40	36 75	937.37	5
UTAH	75 480	18.870	899 60	]	8 42	11 19	262 61	6 65	131 11	1 236 56	1 13	67 59	1,856 70	18
VIRGINIA	320	80	3 17		0 27	0 17	367	0 11	0 72	1 11	NA.	0.30	6.33	NA
WASHINGTON	2,410	603	23 94		2 02	1.29	27 73	0 84	5 15	8 34	NA	2 29	47 77	NA
W VIRGINIA	193,460	48 370	1 673 10	•	70.66	39 68	1,004 66	18 06	340.82	1,678,06	197	251.60	3,238 97	28.
EPA REGION	100,100				70.00		1,554 00	12.00						
			40.75											
ī	2,561	841	10 72		0.89	0.58	12 25	0.38	2.39	3 65	NA	>100	21 73	NA
ti	268,950	87,238	2 487 09 18 411 49		70 44	27 52	1 447 59	23 24	509 52	2 467 72	3 06	364 31	4,991 61	> 43.
m •••	1,561 490	365 363			368 96	231 01	7 446 26	139 20	2 844 75	17,269.82	>18 91	1,965.84	31,172 81	>280.
TV.	324 283	#1 074	1.6160 t. ## 6E0,0C		88 48	12 20	1 642 63	26 71	54104	3,086 17	>3 98	306 55	8,449,32	> 86
V Vi	2,614,912	10 p / 8	20,039 W4		64.7 154	363 43	13 003 84	234 10	4,826 62	36,426 92	>30 34	3,262 51	50,436.84	>432 > s
VI VII	42 302				15 26	12 23	200 86	/69	86 Z 1	657 58	>0.40		962 30	
AUI .	4 860	1 220	4/01		3 63	2 12	46 /1	161	974	14 96	NA	4 11	36 64	NA
	129 620	32.360	1 363 /9		22 06	16 52	b44 08	11 14	130 60	1 / 17 98	1 72	136 /0	2,827 86	24.
n Y	120,679	30 170	1,230,66		30 86	19 79	b86 36	12 10	234 BE	1,478 61	>1 3 <del>9</del>	140 26	2,309 41	> 19.
A	3,766	942	37 38		3 16	2 02	41 30	131	8.51	13 03	NA.	3.68	74 59	NA
ATIONAL TOTALS	6.073.322	1.243.356	49.181.47		1 202 74	708 81	24 993 86	456.28	9,29 / 23	53,450 31	1 60 77	6,194.90	99.422.20	652

<sup>\*</sup>METHODS OF HANDLING SLUDGE WILL PROBABLY FOLLOW CURRENT PRACTICE, BUT WITH INCREASED EMPHASIS ON RECYCLING

NOTE NA DENOTES THAT DATA WERE NOT AVAILABLE

Table 7g
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM IRON AND STEEL INDUSTRY
TOTAL DUST, 1974 (METRIC TONS)

	TOTAL	TOTAL	TOTAL	[	ĺ			co	METITUENT	rs			
STATE	GENERATED	POTENTIALLY HAZARDOUS	HAZARDOUS CONSTITUENTS	DISPOSAL*	Cı	Cu	ķ	Min	NI	70	Ž4	CM	PHENO
LABAMA	117 700	14,060	461	OPEN	20.16	36 46	26.22	1,200.29	11.05	427.53	1,005.05	0.77	0.12
ARIZONA	960	114	19	OR	131	1.86	2.30	40.62	0.23	23.03	91.01	0	
AHKANSAS	946	79	13	RECYCLE	0 92	1.20	1 00	20.36	0.16	16 11	63.67		۰
CALIFORNIA	12,400	8,600	840	1 1	20 14	42.74	36.44	842 48	11 26	499.48	3,039.03	0.32	9.0
COLOHADO	23,200	2,780	/3		8.93	6.32	4.57	203.64	2 04	94.00	210.0	0.4	9.0
CONNECTION	2,700	324	55	1 1	3 72	5.24	8.49	116.04	0.66	65.30	266.30		
DELAWARE	8,050	726	122	1 1	8 33	11 73	14.54	257.54	1.40	148.40	578.49		1 0
FLORIDA	2,950	364	60	1	4 09	5 76	7 14	126,44	0.73	71.88	284.02		0
GEORGIA	3,500	420	70	]	4.80	6 75	9.37	148.24	0.86	84.27	332.90	۰ ا	1 6
HAWAII	250	30	5	( ( )	0.33	0.48	0.57	10 13	0.06	676	22.75	٠,	
LLINOIS	213,350	25,500	1,410	1 1	98 58	127 63	130.50	3,667.29	26.48	1,670,46	6,088,70	1.02	0.1
NDIANA	418,400	50,210	1 740	1 1	101.47	132 61	82.06	4,046.71	48.70	1,882,71	6,300.96	2.37	0.3
CENTUCKY	36,800	4,300	230	1 1	17 17	21 26	21 90	846 77	4 33	296.37	912.54	0.15	0,0
MARYLAND	137,000	16,440	678	) )	34 47	61,24	34.97	1,200.00	16 76	589,22	3,003.22	0.82	0.1
MICHIGAN	193,200	1	808	1 1	49.37	52,76	39.30	2,361.19	16 97	787.62	1,756.06	1.16	0,1
MINNESOTA	2,400	23,180 288	49		3 33	4 00	5.81	103.02	0.50	56.56	231.40	0	1
MISSISSIPPI	850	102	1	1 1	1 16	1.63	2 02	36 72	0.21	20.30	80.23		
MISSOURI	11,100		17		15.20	21.81	26 65	472 18	2 73	268.40	1,080.57		
NEW JERSEY	5,200	1,330	224		7 20	10 13	1	222 34	1.28	126.39	499.43		
NEW YORK	115,100	624	105	1 1 1	24 93	1	12 55	i	9 48	369 32	096.82	0.71	01
	2 460	13,810	294	] ]		24.76	1	104 84	0.60	58 49	236.05	0	
Y CAROLINA		294	50		3 39	477	5 91		45.61	1		I -	1
жно	488,900	58,670	3 060	[	172 00	247 56	211 42	5,896.78	1	2,921 44	16,960 00	2 54	0.4
DKEAHOMA	2,800	136	5/	1	3 89	5 47	6.78	120 19	0 69	68 32	269 96	0	] 9
ONE GON	3,460	414	76	1   1	4 79	4.74	0 36	147 00	0.06	64.07	332.20	0	'
TNNEY! VANIA	606,900	/7,830	3,670		201 04	291 07	236 93	6,807 34	#1 50	3,437.67	19,802.20	3 14	0.5
GEORGE ISLAND				1 1 1			1						Ι.
CARDUNA	4 000	480	81	1 1	5 50	776	9 60	170 06	0 98	98 86	381 96	0	٠
ENNESSEE	1 400	168	26	1 1 1	194	2 73	3 38	59 92	0.36	34.06	134.50	۰	
IE NAS	56 000	6 600	864	1 1	52 82	78 01	89 29	1,538 84	12 42	934 53	4,497 08	0.00	0.0
HAT	54 750	6,570	446	<b>!</b> ! !	17 39	32 06	23 15	378 33	9 80	310 74	2,944.35	0.26	0.0
/IRGINIA	800	96	17	1 1	1 13	1.59	1 97	34 88	0.20	19.83	78 35		
VASHINGTON	6,200	744	126	1 1	8 52	12 00	14 87	263 37	1 52	149 72	591.58	0	0
VIRGINIA	74,850	8,980	147	<b></b>	13.57	11 89	2 95	758 63	5.85	212.21	220.07	0.46	0.0
PA REGION								i	1			1	I
1	2,700	324	55	1	3 72	5.24	6.49	115 04	0.66	65.39	258 39		
п	120,300	14,434	399		32 13	34 88	26 51	1,507 07	10 76	515.71	1,198.25	071	0 1
ш	826,600	99,072	4,634		268.54	367 32	290.36	9,117,27	106.86	4,375.23	24,072.33	4.42	07
rs/	168,150	20,178	987		66 20	87 04	84 54	2,552.07	19.71	1,090.36	4,326.43	0.92	0.1
¥	1,318,250	157,948	6,887		424.84	566.25	468 00	18,073.98	166.36	7,130 79	32,376.71	7.00	1,1
77	58,450	7,014	934		57 63	84 77	87 67	1,667.38	13.27	1,018.96	4,830.71	0.00	0.0
771	11 100	1,330	224		15.28	21.81	26 66	472 16	2 73	268.40	1,080.57	0	"
2201	77,960	9,350	519		23.32	38.38	27.72	661.87	11.84	406.33	3,154.36	0.4	0.0
DX	73,600	8,834	564		29 78	45.06	39 30	893.13	11 54	525.27	3,162,79	0.32	0.0
x	9,860	1,158	195		13 31	18 74	23.22	411 26	2 37	233.79	923.79	0	1
ATIONAL TOTALS	2,663,750	319,642										+	<del></del>

<sup>\*</sup>APPROXIMATELY 57% OF TOTAL GENERATED IS BLAST FURNACE DUST OF WHICH ~ 80% IS RECYCLED APPROXIMATELY 12% OF DUST GENERATED IS FROM ELECTRIC FURNACE AND LAND DISPOSED ELECTRIC FURNACE DUST IS COMBIDERED POTENTIALLY HAZARDOUS REMAINING 31% OF DUST IS FROM OPEN HEARTH AND BOF FURNACES IT IS OPEN DUMPED BUT NOT CONSIDERED HAZARDOUS

<sup>&</sup>quot;VALUES FOR CN, F, AND PHENOL ARE TO BE CONSIDERED AS MINIMUM SINCE DATA WERE NOT AVAILABLE FOR THESE CONSTITUENTS FOR ALL TYPES OF DUST INCLUDED IN THE SUMMATIONS

Table 7h ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL INDUSTRY **TOTAL DUST, 1977 (METRIC TONS)** 

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL*				cor	NSTITUEN	TS			
	GENERATED	POTENTIALLY HAZARDOUS	HAZARDOUS CONSTITUENTS	METHOD	Cr	Cu	Ł	Mn	Ni	Pb	Zn	Ca	PHENO
ALABAMA	124,300	14,920	478	OPEN	29.84	38 84	27 78	1,335.91	12 35	462.97	2,082.96	0.82	0.13
ARIZONA	1,000	120	20	OR	1 39	1 96	2 42	42 96	0.25	24.42	98.48		
ARKANSAS	700	84	14	RECYCLE	0 97	1 37	170	30.06	0 17	17.08	67.49	0	0
CALIFORNIA	76 700	9,290	572	] [	20 83	46 31	36 63	. 893 03	11 92	526.27	3.221.37	0.34	0.04
COLORADO	24,500	2,960	77	}	6 28	6 70	4 8b	300 58	3 16	100.27	222.99	0.16	0.02
COMMECTICUT	2,850	342	5.0		3 96	5 56	6.88	121 94	0.70	60.32	273.90	0	0
DELAWARE	6,400	768	130	1	8 83	12 44	18 41	272 96	1,58	155 19	613.20		
FLORIDA	3,150	378	64	i	4 34	6 11	7 56	134 03	677	76 19	301.06	ه ا	
GEORGIA	3,790	444	75	1 1	509	7 16	8.87	167 14	0.91	89 33	352.97		0
HAWAH	250	30	5	1	0.36	0.48	0.81	10.74	0.61	6 10	24 11		
ILLINOIS	226,200	27,140	1,500	1 1	104 49	135 29	138 33	3.887 33	26.09	1,770 69	6.432.82	1.08	0.16
INDIANA	443,500		1,840	l [	107 55	140 56	86.98	4.289 51	49 50	1,794 27	8,871 10	2.51	0.41
KENTUCKY	37,960	53,220	244		18 20	22 47	23 21	685 58	4 59	314 15	967.29	0.18	0.01
MARYLAND	146,200	4 560 17,420	719		38 53	54 32	37 07	1 336 63	17.76	592 77	3,914,91	0.15	0.0
MICHIGAN	204,800		644	1 1	62 33	55 92	40 60	2,502.86	17 99	834.88	1,001.41	1.23	0.20
MINNESOTA	2,560	24,580		<b>,</b> ,	3 53	4 97	6 18	109.20	0 63	62.07	245.28	0	0.0
WISSISSIPPI	900	306	62		1 23	172	2 14	37.86	0 22	21.52	85.04		
WISSOURI	11 /50	108	18	1 1	16 20	22 80	28.25	500 49	2.89	284.51	1.124.20		
	i .	1,410	237	i i	1	1					.,	i -	} -
NEW JERSEY	5,550	666	112	1 1	7 63	10 74	13,30	235.68	1 36	133,98	528.40	0	0
NEW YORK	122,000	14 640	311	1 1	26 43	26 23	14 80	1,361.81	10.05	412,88	740.75	0.75	0.12
N CAROLINA	2,600	312	53	1 1	3 58	5 06	6.26	110 92	0 64	63.06	249,15	C	0
OHIO	518,200	62,180	3,240		182 46	262 41	224 11	8,249 53	69 55	3,098 73	16,907 64	2.70	0.44
OKLAHOMA	3,000	360	60		4 12	5 80	7 19	127 40	0 74	72 42	286.16	٥	0
DREGON	3,700	444	74	1 1	5 07	7 14	8.85	158 77	0 91	89.12	352,13	0	0
PENNSYLVANIA	643,300	77,200	3,890	1 1	213 10	308 53	250 08	7 215 79	86 45	3,643 82	20,572,33	3.32	0.5
RHODE ISLAND		-	-	ļ ļ		_		-	:	-	_		ļ
S CAROLINA	4,250	510	80		5 83	8 21	10 17	180 25	1 04	102 46	404.87	0	0
TENNESSEE	1,500	180	30	<b>!</b> !	2 06	2 89	3 58	6351	0 37	36 10	142 66	٥	0
TEXAS	58,300	7 000	916		65 99	82 69	94 64	1 631 17	13 17	990 60	4,766,90	0 10	0.0
UTAH	58 900	6,960	473	{	18 43	34 00	24 1-4	40103	19 40	329 40	3 121 00	0.28	0.04
VIRGINIA	860	102	18	1 1	1 20	1 68	2 09	36 97	0 21	21 02	83,06	0	0
WASHINGTON	6,550	786	132	) }	9 04	12 72	15 76	279 18	16	158 70	<b>627.09</b>	0	0
W VIRGINIA	79,350	9 520	156		14 38	12 40	3 13	802.03	6 ∠0	224 94	233.28	0.49	0.0
EPA REGION				]	Ī		1		1	1	1		
t	2 850	342	58		3 95	6 56	6.88	121 94	9.70	69 32	273 90	0	
n .	127 550	15 306	421		34 06	36 97	28 10	1 1407 44	1141	546 6b	1 270 15	0.76	01
ш	875,100	10% 910	491)		274 04	389 37	307 %	314431	5 11 36	4 631 14	25 516 67	4 60	0.7
124	178 160	71 402	1 048	1	70 1H	92 25	89 148	2 105.20	20.90	1 155 77	4 585 99	0 98	0.1
y .	1 396 750	107 426	1 216		450 31	599 15	496 18	17 0,48 4 1	100 77	7.868 64	ال 318 كس (	7 6.2	12
vi	62,000	7 444	940		81 00	80 84	101 63	1.788 62	14 08	1,000 10	6 120 66	0.10	0.0
100 100	11,760	1,410	237		18 20	22 80	28 25	800 49	2 89	284 51	1,124,20	0	3.0
<b>1</b> 210	#2,600	9,910	560		24 71	40 70	29 19	701 59	13 68	429 67	3,343.86	0.43	0.0
	77,950	9,350	597		31 67	47.75	41 65	946 72	12 78	568 79	3,341,96	0.34	ì
DX.	10 250	1 230	206			19 86	1	846 7Z	2 52	i	979.22	0.34	0.0
X	10 2717		708		14 11	19 56	24.61	4 101 100	752	74782	0/8.22		L
NATIONAL TOTALS	2,823,650	338.830	16,298		980 21	1,344 27	1 156 96	15,500 74	356 17	16 567 02	79,874 48	14.8	2.4

<sup>\*</sup>DISPOSAL PRACTICE FOR 1977 IS EXPECTED TO ESSENTIALLY BE THE SAME AS THE CURRENT PRACTICE. BUT WITH A THEND TOWARD INCREASED USE OF SINTERING OR AGG. OMERATING TO ALLOW RECYCLE.
\*\*VALUES FOR CN, F AND PHENOL ARE TO BE CONSIDER TO AS MINIMUM SINCE DATA WERE NOT AVAILABLE FOR THE SI CONSTITUENTS FOR ALL TYPES OF DUST INCLUDED IN THE SUMMATIONS.

Table 7i
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM IRON AND STEEL INDUSTRY
TOTAL DUST, 1983 (METRIC TONS)

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL*				CO	NSTITUENT	'S			
	GENERATED	POTENTIALLY HAZARDOUS	HAZAROOUS CONSTITUENTS	METHOD	Cı	Cu	Me	Nı	Pb	Zn	CN	k	PHENOL
AL ABAMA	144 200	17,300	554	OPEN	34 83	44 24	1,550 16	14 33	525 82	2,417 01	0.96	32.25	0.15
ARIZONA	1,150	138	24	DUMP OR	1 61	2 27	49.84	0 29	20 33	111.96	~0	2,81	~0
ARKANSAS	800	96	17	RECYCLE	1 13	1 59	34 87	0 20	19.82	78.32	~0	1.97	~0
CALIFORNIA	89,000	10,680	664	<b> </b>	34 61	52 57	1,036.25	13 83	810 87	3,738 00	0.40	44.82	0.06
COLORADO	28 600	3,430	90	]	7 29	7,78	348 76	2 61	118 35	258 29	0.17	5.63	0.03
CONNECTICUT	3 300	396	67	i i	4 58	6 45	141 49	0 82	80 43	317 82	~0	7 99	~0
DELAWARE	7 450	894	150		10 25	14 43	316 78	1 83	180 07	711 55	~0	17.88	~0
FLOHIDA	3 650	438	74	1 1	5 03	7 08	155 52	0 90	88 41	349.34	~0	8 78	~0
GEORGIA	4,300	516	87		5 90	8 31	182 34	106	103 66	409 58	~0	10.29	~ 0
HAWAII	300	36	6		0 40	0.67	12 46	0.07	7 08	27 99	~0	070	~0
ILLINOIS	262,400	31,490	1 740	1 1	121 25	156 99	4,510 77	32 67	2,064 67	7,484.50	1.26	180 51	0.20
INDIANA	514,700	61,760	2,140		124.80	163.11	4,977 45	57.44	2,082.03	10,293.82	2.91	100.93	0.47
KENTUCKY	44 000	5 280	283		21 12	26.07	795 53	5 33	364 54	1,122 42	0.19	26.93	0.03
MARYLAND	168,500	20,220	834		42 39	63 03	1,550 88	20 81	687 84	4,542 56	1.01	43 01	0 16
MICHIGAN	237 700	28 b20	147		60 73	64.89	2,904 26	20 87	968 77	2,159 94	1 42	47 11	0.23
MINNESOTA	2 950	164	60	[	4 10	5 77	126 71	0 73	72 03	264 62	~0	7 16	~ 0
MISSISSIPPI	1 060	176	21		142	2 00	43.93	0 26	24 97	W.#	~0	2.48	-0
MISSOURI	11860	1 640	276	[	18 80	26 46	580 76	3 36	330 14	1,304.50	~0	32 78	~0
NEW ILHEEY	6 400	758	130	1 1	# #6	12 48	273 48	1 58	166 44	614.30	~0	18.44	~0
NEW YORK	141,500	16 980	361		30 87	30 44	1 060 27	11 66	478 87	868 55	0.98	17,17	0.14
N CAROLINA	1 000	160	61	1 1	4 17	8.86	128 71	0 74	73 17	209 11	~0	7 26	~0
оню	601 300	72 160	3,760		211 67	304 49	7,251 81	80.70	3,503 37	19,619.24	3.13	260.06	0.61
OKLAHOMA	3 450	414	70		4 78	8 73	147 83	0.85	84.03	332.05	~0	B 34	~0
OREGON	4 250	510	86		5 89	8 29	181 91	106	103.41	406.61	~0	10.27	~0
PENNSYLVANIA	746 500	89 580	4 510	1	247 28	358 01	8,373 03	100.31	4,228.21	23,987.71	3.88	290 19	0 82
S CAROLINA	4,900	588	99		6 77	9 5 3	209 16	1.21	118 90	469.81	~0	11,51	~0
IF NNESSE E	1,750	210	35	]	2 39	3 36	73 70	0.43	41 99	185.54	~0	4 15	~0
TE XAS	67 660	8 120	1 060		64 97	96.96	1,892 77	15 28	1,149 47	5,531.41	0.12	109 82	0 02
HAH	87 350	080	549		21 39	30 43	465 35	12 06	382.21	3,621 56	0.32	28,48	0.06
VIRGINIA	1 000	120	20		1 39	196	42 90	0.25	24 39	96.37	~0	2.42	~0
WASHINGTON	7,600	912	154		10 48	14 76	323 95	187	184 15	727 86	~0	18.28	-0
W VIRGINIA	92 100	11 050	181	↓	16 69	14 38	930 65	7 19	261 08	270.69	0.57	3.63	0.09
EPA REGION	† †		<del>-</del> -			-					<u> </u>		+
Ţ	3,300	396	67		4 58	8,45	141 49	0 82	80 43	317.82	~0	799	~0
П	147,900	17.748	491		39 52	42 90	1.853 70	13 24	634 33	1.473.86	0.88	32 81	0.14
m	1 015,550	121,864	5,695		316 0	451 80	11,214,24	130 19	6 381 53	29.808 98	6 44	367 13	0.87
IV	706 Hb0	24 818	1 214		8143	107.06	3 139 05	24 24	1 341 16	5,321 49	1 14	103 96	0 18
V	1 619 060	184 2h4	E 447		6.73 Bb	690.20	19 771 0	197 31	8,770 87	30.822 12	s 72	675 75	141
וע	71 BKKI	H 10 40	1 147		/O NA	104 28	20/64/	16 11	1.251.32	5 941 /8	0.12	120 13	0.03
VII	14.650	1 640	279	· .	10 00	26 45	580 76	1.16	110 14	1 104 10	. 0	12 /8	0
vin	96 960	11 610	618		28 68	47 21	814 11	14 57	498 56	3,879 84	0 49	34 11	0.08
IX	90 450	10 854	694		36 62	55.41	1 098 55	14 19	646 08	3,877 94	0 40	48 33	0.06
x	11,860	1.422	240		16 37	23.06	505.86	2 92	29756	1,136 27	~0	28 55	~0
NATIONAL TOTALS	3,276,450	393,166	18,910		1,137 43	1,880.85	41,194 23		19.223 97	92,684 59	17 19	1,341,34	2 76

<sup>\*</sup>DISPOSAL PRACTICE FOR 1983 IS EXPECTED TO ESSENTIALLY BE THE SAME AS THE CURRENT PRACTICE, BUT WITH A TREND TOWARD INCREASED USE OF SINTERING OR AGGLOMERATING TO ALLOW RECYCLE.

<sup>\*\*</sup>VALUES FOR CN, F AND PHENOL ARE TO BE CONSIDERED AS MINIMUM SINCE DATA WERE NOT AVAILABLE FOR THESE CONSTITUENTS FOR ALL TYPES OF DUST INCLUDED IN THE SUMMATIONS.

Table 7j ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM THE IRON AND STEEL INDUSTRY **TOTAL SCALE, 1974 (METRIC TONS)** 

STATE	TOTAL	FOTAL POTENTIALLY	TOTAL HAZARDOUS	DISPOSAL*			CONST	TUENTS			OIL
	GENERATED	HAZARDOUS	CONSTITUENTS	METHOD	Cr Cr	Cu	Mn	Ni	Pb	Zn	GREASE
ALABAMA	196,400	39,260	991 9	RECYCLE	56.34	78 46	937 47	84 49	16.72	8.07	3,760 06
ARIZONA	3,780	756	19 1	OPEN DUMP	1 09	151	18 06	1 63	0.32	0.12	72.82
ARKANSAS	1,380	276	88	1 1	0.31	0 42	4 91	0.71	0.19	0.04	37.3
CALIFORNIA	185,080	37,020	944 1	<b>(</b>	52 67	73 27	874 86	80.25	16.13	5.70	3,817.6
COLORADO	56 500	11,300	285 2		16.20	22 56	269 60	24 30	4.81	1.76	1,086.9
CONNECTICUT	10,700	2,140	54.3	]	3 08	4 29	61 31	4 63	0.92	0.33	206.9
DELAWARE	18,300	3,880	100 6	1	4 87	671	79.70	8 40	1.88	0.56	401.0
FLORIDA	3,340	608	31 1	\	0 69	091	1057	1.82	0.51	0.09	141.0
GEORGIA	13,800	2,760	69 9		3 97	5 53	66 09	5 96	1.18	0.43	266.4
HAWAII	720	144	67	<b>i</b>	0.15	0 20	2 28	0.39	011	0.02	30.4
ILLINOIS	562,260	112,440	2,855.1		160 59	223 49	2,666 40	242 91	48.49	17.36	10,913.1
INDIANA	938,000	187,800	4,842 9		264.45	367 35	4,382 72	410 38	83 96	28.76	18,677.0
KENTUCKY	109,500	21,900	561 1		31 06	43 18	515 51	47 63	9.63	3.37	2,154.8
MARYLAND	256,900	61,380	1,297 3	}	73 69	102.62	1,226 14	110 51	21.87	7.84	4,943.7
MICHIGAN	468,300	93,660	2,366 1		134 34	187 08	2,236 40	201 47	39.87	14.48	9,013.0
MINNESOTA	5 000	1,000	319	l l	1 14	1 53	17 83	2 58	0.66	0.14	136.6
MISSISSIPPI	1,730	346	11 1	1 1	0 39	0.53	6.18	0 90	0 24	0.05	47.0
MISSOURI	44,100	8.820	222 7		12 66	17 62	210 49	18 97	3 75	1.36	848 6
NEW JERSEY	15,800	3,160	86 9	i i	4 22	5.81	68 98	7.27	1,63	0.47	346.2
NEW YORK	273,900	54,780	1,3834	1 1	78 58	109 42	1,307 46	117.84	23.32	8.47	5,271.8
N CAROLINA	2,760	562	25 8		0 57	0 76	8 74	151	0.43	0 07	116.7
OHIO	1,150,200	230,040	6.032 8	{ {	324.83	451 32	5,385 53	502 34	102 43	36 30	23,362.4
OKLAHOMA	5,830	1,170	37.2		1 33	1 78	20 80	3 01	0.80	0 16	158.2
OREGON	13,800	2.760	<b>6</b> 9 8	}	3 96	5 5 2	65 93	5 94	1 18	0.43	265.8
PENNSYLVANIA	1,416,600	283,320	7 206 1		404 18	562 41	6,716 97	612 74	122.57	43 68	27,563 7
S CAROLINA	/ 440	1 490	45.1		171	2 30	26 87	182	1.00	021	189 6
1 ENNESSEE	2910	582	186	1 1	0.86	0.89	10 37	1 150	0.40	0.08	78.9
TEXAS	183 000	36 600	924 4		52 51	73 12	873 74	/8 74	15 58	5 66	3,522 4
UTAH	113,900	22 780	5751		32 67	1	1	38 99		3.52	2.191 4
		650	16.5		093	45 49	543 54	140	9 69		
VIRGINIA	3 260	4 920	124.2	}	7.06	1.30	11, 1515	10.58	0.28	0 10	62 6
WASHINGTON W VIRGINIA	24,600 206 100	41 220	984 0	\	58 88	9 H 3 81 91-	978 80	89 07	2 00 17 78	635	4733 3,6872
	206 100				00 80		1 378 80	- "	1//6	0.35	3,0872
EPA HEGION					ì	ļ		]	}	)	1
1	10 100	≥ 140	54.3		3 08	4 29	5131	4 83	0 92	ده د	2069
ø	289,700	57,940	1,470 3		82 80	115 23	1,376 44	125 11	24.95	8.94	5,618,0
m	1,901,160	380,230	9,603,5		542 55	754 99	9,017 16	822 12	164 38	58.63	36,857.8
II.	337,880	67,578	1,754 6		95 39	127 03	1,581 80	147 63	30 11	10.37	6,774 7
¥	3,123,700	624,740	16,127 8		885 35	1,230 77	14,690 88	1,259 68	275.42	96,03	62,101.1
<b>VI</b>	190,210	38,046	970.A		64 16	75.32	899.96	82 46	16.57	5.86	3,718.0
AII.	44,100	8,820	2 <b>22</b> 7	}	12 65	17 62	210.49	18 97	3.75	1 36	848.6
<b>uu</b>	170,400	34,080	860.3		48 87	68 05	813 14	73 29	14 50	5 27	3,278 3
138	189,580	37,920	989 9		53 91	74 98	895 20	82 27	16 56	5 84	3 720.8
x	38,400	7,680	194 0		11.02	16 36	183 34	16.62	3.27	1,19	739.1
NATIONAL TOTALS	6,295,830	1,259,174	32,227 8		1.789.77	2.489 16	29 719 21	2.732.68	550.43	193,82	123,663,7

<sup>\*</sup>IT IS ESTIMATED THAT ~ 80 PERCENT OF THE SCALE IS RECYCLED DIRECTLY OR SOLD FOR EVENTUAL RECYCLE THE REMAINDER IS LAND DISPOSED. OIL CONTENT PREVENTS TOTAL RECYCLE SOURCE CALSPAN CORPORATION

36

Table 7k

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM THE IRON AND STEEL INDUSTRY

TOTAL SCALE, 1977 (METRIC TONS)

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL*			CONST	TUENTS			OIL
	GENERATED	POTENTIALLY HAZARDOUS	HAZARDOUS CONSTITUENTS	METHOD	Cı	Cu	Mn	N <sub>3</sub>	Pb	Zn	GREA
ALABAMA	208,200	41 640	1,051 4	RECYCLE	59 72	83 16	993 72	89.56	17 73	8.44	4,006
ARIZONA	4,010	903	20 1	OPEN DUMP	1 15	1 60	19 15	173	0.34	0.12	77
AHK ANSA'S	1,460	292	9 1		0 33	0 45	5 20	0.75	0 20	0.04	30
CALIFORNIA	196 200	<b>39 240</b>	1 000 /		bb 83	7/ 66	927 36	25 08	17 10	6.04	3,834
COLORADO	59,900	11 980	102 1		17 17	23 92	285 78	25 76	B 10	1 85	1,152
CONNECTION	11,400	2.2MO	5/ b		3 27	4 t5	54 39	4 90	0 97	0.36	219
DELAWARE	19,400	1 1880	106 J		617	7 12	84 48	8.91	1 99	0.58	425
FLORIDA	3,540	708	3 5 0	] [	0 /4	0 97	11 20	193	0 54	0 10	149
GECIRGIA	14,700	2 940	/4.1	1 1	4 21	5 86	70 06	6 31	1.26	0.45	262
HAWAH	760	162	7.1	1 1	0 16	0.21	2 42	0 42	0 12	0.02	32
ILLINOIS	595,900	119 180	3,026 4		170 22	236 89	2,829 56	257.49	51 40	18 39	11,567
INDIANA	994,300	198 860	b 1.33 5		280 31	389 39	4,645 68	435.00	88 98	30.49	19,797
KENTUCKY	116 100	23 220	594 7	1 1	32 92	45 78	546 44	50.49	10 21	3.57	2,284
MARYLAND	272 300	54 460	1,375 1		78 11	108 77	1,299 71	117 14	23.18	8.42	5,240
MICHIGAN	496,400	99 280	2,507 0		142 40	198 31	2,369 52	213 56	42.26	15.35	9,553
MINNESCITA	5 300	1 060	33 8		1 21	1 62	18 90	2 74	0 73	0 15	143
MISSISSIPPI	1 840	368	11.7		0 42	0 56	6 55	0 95	0.25	0.05	49
MISSOURI	46 700	9 340	236.1		13 41	18 67	223 12	20 11	3 98	1 44	899
NEW JERSEY	16,800	3 360	92 1	1 1	4 47	6 16	73 12	7 71	1 72	0 50	367
NEW YORK	290,300	58 060	1 466 4		83.29	115 99	1,385 91	124 91	24.72	8 98	5,588
N CÁROLINA	2,930	586	27 3		0.61	0,80	9 27	1 60	0.46	0.08	123
оню	1,219,200	253,840	6 394 8		344 31	478 40	5 708.66	532 48	108 57	37.41	24,764
OKLAHOMA	6,180	1,240	39 5	] ] .	1.41	1,89	22.06	3 19	0.86	0.17	167
DREGON	14 600	2,920	73 9		4 20	5 85	69 89	6 30	1 25	0.45	281
PENNSYLVANIA	1 501,600	300 320	7 63 / 4	1	428 44	596 16	7 119 99	649 50	129 92	46 30	29,216
HODE ISLAND	NEG				*****	1		17.		46.50	20,210
CAROLINA	7 890	1 5-80	47 H		1 81	2 44	20.48	4.05	1.04	022	201
I NNEBOLE	1 000	010	19 /		0.70	0.04	10 90	159	0.42	0.00	83
EXAB	184 000	18 800	₩/0 H		ho this	1/01	929 10	834/	1662	000	3,753
IIAH	120,700	24 140	Acres n		34 63	44 22	670 15	51 93	10.20	3 73	2,322
/IRGINIA	3,460	p <del>9</del> 0	1/ 4		099	1 38	18 48	149	0 29	011	66
VASHINGTON	26,000	5 200	131 7		7 48	10.42	124.46	11 22	2.22	0.81	501
VIRGINIA	218,800	43 720	1,043 1	1 1	62 42	86 87	2,037 52	94 42	18 85	8.74	3,908
PA REGION			.,5-5 .			- 55.57	-,		1.555	<del>  "</del>	3,500
1	11,400	2.280	57 <b>6</b>		2.27	1	54 39	4.00	0.07		
п	307,100	61,420	1,558 6		3 27 87 76	4.55	1.459 03	4 90 132 62	0.97	0.35	219
m T	2,015,350	403,070	10,179 7		87 76 575 13	122,15 800 30	9,558 18	132 62 871 46	174 23	9.48	5,966
IV	368,280	71 658	1,859 7				1	1		62.15	38,867
<u>v</u>	3 311,100	- 1	17,096 6		101 13	140.51	1,676 70	158.48	31 91	11.00	7,181
VI	201,840	662,220 40,332	1,028 6		936 45	1,304 61	16,672 32	1,441.27	201 04	101 78	65,627
AU. 77		9,340	236 1		67.40	70.85	963 41	87 41	17.67	6.21	3,941
AIII AII	46,700	36 120	2.90 1 911 9		13.41	18 67	223 12	20 11	3.98	1.44	896
DX VIII	180,600				51.00	72 14	861 93	77 89	15 38	5.66	3,476
X X	200,970	40,194 8 120	1,028 1		57 14	79,47	948 92	87 21	17.58	6 18	3,944
	40,600	8 120	200 6		11 66	16 27	194 35	17 52	3 4 7	1.26	783
ATIONAL TOTALS	6,673,740	1,334,754	34,161 3	· I	1,897 17	2,638.52	31,502 35	2,896 67	583 45	205,44	131,083

<sup>\*</sup>THE AMOUNT OF SCALE RECYCLED IS EXPECTED TO INCREASE OVER PRESENT AMOUNTS

Table 71
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM THE IRON AND STEEL INDUSTRY
TOTAL SCALE, 1983 (METRIC TONS)

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL*			CONST	TUENTS			OIL
	GENERATED	POTENTIALLY HAZARDOUS	HAZARDOUS CONSTITUENTS	METHOD	C <sub>1</sub>	Cu	Mn	Nı	Pb	Zn	GREAS
ALABAMA	241,600	48,320	1,220 1	RECYCLE	68.30	96 50	1,153 09	103 93	20.57	7.47	4,849.
ARIZONA	4,650	930	23 5	OR OPEN DUMP	1.34	1.86	22 22	2 00	0.40	0 14	89.1
AHKANSAS	1 890	338	10 8		0 39	0 52	6 04	0 87	0.23	0.06	45.1
CALIFORNIA	227,600	45,520	1,161 2	1 1	64 79	90.12	1,076 08	98 70	19:84	7.01	4,449.6
COLORADO	69,500	13,900	350.8	1 1	19.92	27 75	331 61	29 89	5.91	2 15	1,336.6
CONNECTICUT	13,200	2,640	66.8		3 79	5 28	63 11	5 69	1.13	0.41	254.
DELAWARE	22,500	4,500	123 8	1	5 99	8 26	98 03	10 33	2.31	0 67	493.
FLORIDA	4,110	822	38 3		0 85	1 13	13 00	2 24	0.63	0.11	173.
GEORGIA	17,000	3,400	860	1	4 89	80	81 29	7 33	1.45	0.53	327.
HAWAII	890	178	83	1 1	0 18	0 24	2.80	0 48	0 14	0.02	37.
LLINOIS	691,500	138 300	3,5117	<b> </b>	197 62	2 /4.89	3 /83 36	298 /H	59 64	21.33	13,423.
NDIANA	1,153,800	230,760	t,966 <b>8</b>		320 27	451 ##	6 190 /b	b04 /e	103 25	35.36	22,972
CENTUCKY	134,700	JN 940	690 1		W 21	6.1.12	014 07	en en	11 #8	4 14	2,960.
MARYL AND	315,900	61180	1 695 /	1 1	90 64	128.22	1 500 15	116 97	26 90	977	6,090
AKHIGAN	576,000	115,200	2,909 1		165 24	230 11	2 /49 54	24/81	49 04	17.81	11,088
MINNESOTA	6,150	1,230	39 3	į (	1 40	1 88	21 93	3 18	0 84	0.17	166
MISSISSIPPI	2,130	426	13 6	1 1	0.49	0.65	7 60	1 10	0 29	0.06	57
AISSOURI	64,200	10.840	273 9	1	15 56	21 67	258 91	23.33	4.82	1 68	1,043
IEW JERSEY	19,500	3.900	106 9		6 19	7 15	84 84	8 94	2 00	0.58	425
EW YORK	336,900	67.380	1,701 6	ł I	96.65	134 59	1,608 18	144 94	28 68	10.42	5.484
CAROLINA	3,400	680	31 7	1	0.71	0 93	10.76	1 85	0 52	0.08	143
OHIO	1.414.700	282.940	7,420 4	1 1	399 53	585 12	8 624 20	617 88	125 98	43.41	28,735
KLAHOMA	7,175	1,435	45 8		163	2 14	25 59	371	0 98	0 20	194
REGON	17 000	3,400	85.8	1 1	4 87	8 79	81 10	7 31	1 45	0.63	326
PENNEYI VANIA	1,742,400	348,480	8 862 3		497 15	691 //	6,261 87	20.402	160 76	53,73	33,802
יוייטנו ופו אוני	NEG	,548,480	0 407 3		70/10		6,261 07	703 107	100 /6	04.73	35.55
CANOLINA	9,160	1,832	bbb	] ]	2 10	283	13 04,	4 70	1 24	0.24	233
IENNESSEF	3,580	716	22.8	} }	0.81	109	12 /6	1 85	0 49	0.10	97
AAK 41	226,100	45 020	1,1370		64 59	89 94	10/4 /0	96.86	19 17	8.98	4.332
JTAH	140,000	28,000	/07.3		40 17	56 95	668 55	80 25	11 92	4.33	2.695
IRGINIA	4.000	800	20 2	{ }	1	1	19.1.1	1 72	0 34	0.12	77
VASHINGTON	30,300	6,060	162 8	\ <b>\</b>	1 15 8 68	1 60 12 09	144 42	13.02	2 58	0.12	582
VIRGINIA	253,600	50,720	1,210 3	♦	72 43	100 80	1,203 92	109.56	21 87	7.82	4,535
	203,000			<del> </del>	12-3	100 00	1,203 82	103,50	+	1.02	+
PA REGION	1		}	1	}	1		1			1
I	13,200	2,840	66 8	1	3 79	5 28	63 11	5 <b>69</b>	1 13	0.41	254
п	356,400	71,280	1,808.5		101 84	141 74	1,693.02	153 88	30 68	11.00	6,910
m	2,338,400	467,880	11,8123	1	667 36	928 65	11,091 10	1,011 20	202 18	72.11	45,069
IZ	415,680	83,136	2,158 1	-	117 36	163 05	1,945 62	181 58	37 04	12.76	8,332
¥	3,842,150	768,430	19,837 3	!	1,088 96	1,513 83	18,069 78	1,672 41	338 75	118.10	76,383
<b>VI</b>	233,965	46,793	1,193.6	1	66 61	92 85	1,106.33	101.44	20.38	7.21	4,573
ΔII	54,200	10,840	273 9	1	15 56	21.67	258 91	23 33	4.62	1.68	1,043
<b>v</b> m	209,500	41,900	1,058 1		60 09	83 70	1,000 16	90 14	17.83	5.48	4,032
TX.	233,140	46,628	1,193.0	1	66 31	92 22	1,101 10	101 18	20.38	7.17	4,576
x	47,300	9,460	238.6		13 55	18 88	225 52	20 33	4.03	1.47	908
ATIONAL TOTALS	7,743,935	1,548,787	39,640 2		2.201.43	3.081 87	36,854 86	3,381 18	877.02	238.39	152,106

<sup>\*</sup>THE AMOUNT OF SCALE RECYCLED IS EXPECTED TO INCREASE OVER PRESENT AMOUNTS

ESTIMATED STATE, REGIONAL, AND NATIONAL WASTE FROM THE IRON AND STEEL INDUSTRY PICKLE LIQUOR, 1974 (METRIC TONS) DRY WEIGHTS\* Table 7m

			TOTAL			HAZAR	Sous co	HAZARDOUS CONSTITUENTS	S		
STATE	DISPOSED	TOTAL POT.	HAZARDOUS	DISPOSAL METHOD	ర	3	¥	ž	æ	5	OIL & GREASE
*******											
ALABORA A		1,827	11.41	NEUTRALIZED ON SITE	0.497	0.288	7.005	0.751	0.043	0.323	2.501
CALIFORNIA	7	4.321	6.298	OR BY CONTRACT	0.274	0.159	3.867	0.415	0.024	0.178	1,380
COLORADO	Ŕ	202	0.301	DISPOSAL SERVICE	0.013	0.0076	0.185	0.020	0.001	0.0085	9900
CONNECTICUT	745	745	1.086		0.047	0 027	0.667	0.072	0.004	0.031	0.238
FLORIDA	ñ	5	0.045	-	0.0020	0.0011	0.028	0.0030	0.00017	0.0013	0.010
GEORGIA	5	33	0.045		0.0020	0.0011	0.028	0.0030	0.00017	0.0013	0.010
ILLINOIS	12.56		18.03		0.785	0.455	11.070	1.187	0.068	0.511	3.952
INDIANA	2,28	43,369	63.21		2.754	25	38.815	4.163	0.239	5	13.856
KENTUCKY	(98)	4,667	98.9		0.296	0 172	4.177	0.448	0.026	0.193	1.491
MARYLAND	5.712	5,712	8.325		0.363	0.210	5 112	0.548	0.031	0.236	1.825
MICHIGAN	885.6	9,588	13.97		0.609	0.352	8.581	0.920	0.053	0.396	3.063
MESSISSIPPI	×	33	0.047		0.0020	0.0012	0.029	0.0031	0.00018	0.0013	0.010
MISSOURI		45	0.065		0.0028	0.0016	0.040	0.0043	0.00025	81000	0.014
NEW JERSEY	<b>35</b>	135	0.196		9800.0	9000	0.121	0.013	0.00074	95000	0.043
NEW YORK	8.410	8,410	12.26		0.534	0.309	7.527	0.807	0.046	0.347	2.687
OHIO	28.872	28,872	42.08		1.833	1.061	25.84	2.772	0.159	1.192	9.225
PENNSYLVANIA	12,991	32,991	48.085		2.095	1212	29.526	3.167	0.181	1.362	10.540
RHODE ISLAND	<b>Ξ</b>	141	0.205		0.0089	0.0052	0.126	0.014	0.00077	9500.0	0.045
S. CAROLINA	2	21	0.030		0.0013	0.00076	0.018	0.0020	0.00011	0.00086	0.0066
TENNESSEE	5	23	0.030		0.0013	0.00076	0.018	0.0020	0.00011	0.00086	0.0066
TEXAS	2	23	0:030		0.0013	0.00076	0.018	0.0020	0.00011	0.00086	0.0066
HVIS	732	2,321	3.38		0.147	0.085	2.078	0.223	0.013	0.09	0.742
W. VIRGINIA	17,537	17,537	25.56	•	1.114	0.644	15.696	1.684	960.0	0.724	5.603
EPA REGION											
,,,	2	*	1.291		9900	0.032	0.793	9800	0.0048	0.0368	0.283
Ħ	<b>8</b> , 545	8,545	12.456		0.543	0.314	7.648	0.82	0.0467	0.3526	2.73
8	26.240	56,240	81.97		3.572	2.066	50.334	5.399	0.308	2.322	17.968
<b>B</b> 1	12,630	12,630	18.437		0.802	0.465	11.303	1.212	0.0697	0.5216	4.035
pi l	<b>2</b> ,197	761.79	137.29		5.981	3.462	84.306	9.042	0.519	3.89	30.096
<b>4</b>	Z !	2	0.030		0.0013	0.00076	0.018	0.002	0.0001	0.00086	0.0066
7	•	\$	0.065		0.0028	0.0016	20.0	0.004	0.00025	0.0018	0.014
31	2.528	2,528	3.881		0.16	0.0926	2.263	0.243	0.014	0.1045	0.808
4	4,221	4,321	6.298		0.274	0.156	3.867	0.415	0.027	0.178	1.380
NATIONAL TOTALS	179,411	178,411	261.52		11.391	6.593	160.572	17.223	0.9866	7.408	57.321
		A	T								

\*MULTIPLY BY 5.0 TO CONVERT TO APPROXIMATE WET WEIGHTS. MULTIPLY BY 1.1 TO CONVERT TO SHORT TONS.

ESTIMATED STATE, REGIONAL, AND NATIONAL WASTE FROM THE IRON AND STEEL INDUSTRY PICKLE LIQUOR, 1977 (METRIC TONS), DRY WEIGHTS\* Table 7n

	TOTA	TOTA! POT	TOTAL			HAZ	ARDOUS C	HAZARDOUS CONSTITUENTS	YTS		3
STATE	DISPOSED	HAZARDOUS	CONSTITUENTS	DISPOSAL METHOD	ð	3	Mn	ž	£	Zn	GREASE
ALABAMA	8,297	8,297	12.09	NEUTRALIZED ON SITE	0.527	0.305	7.426	0.796	0.046	0.343	2.651
CALIFORNIA	4,580	4,580	8.68	OR BY CONTRACT	0.291	0.168	4.099	0.440	0.025	0.189	1.463
COLORADO	218	218	0.32	DISPOSAL SERVICE	0.014	0.0081	0.196	0.021	0.0012	0.0091	0.070
CONNECTICUT	8	8	1.15	_	0.050	0 0 29	0.707	0.076	0.0043	0.033	0.252
FLORIDA	ង	Ħ	90.0		0.0021	0.0012	0.029	0.0032	0.0002	0.0014	0.011
GEORGIA	Ħ	æ	0.05		0.0021	0.0012	0.029	0.0032	0.0002	0.0014	0.011
ILLINOIS	13,111	13,111	19.11		0.833	0.482	11.734	1.259	0.072	0.541	4.189
INDIANA	45,971	45,971	67.0		2.919	1.689	41.144	4.413	0.253	1.899	14.687
KENTUCKY	4,947	7.8.4	7.21		0.314	0.182	4.428	0.475	0.027	0 204	1.581
MARYLAND	6,054	6,064	8.82		0.384	0.222	5.419	0.581	0.033	0.250	1.934
MICHIGAN	10,163	10,163	14.81		0.645	0.373	9.036	0.976	0.056	0.420	3.247
MISSISSIPP	*	*	0.05		0.0022	0.0012	0.030	0.0033	0.0002	0.0014	0.011
MISSOURI	9	\$	0.07		0.003	0.0017	0.043	0.0046	0.0003	0.002	0.015
NEW JERSEY	143	143	0.21		1600.0	0.0052	0.128	0.014	0.0008	0.0059	0.046
NEW YORK	8,915	8,915	12.99		0.566	0.328	7.979	0.856	0.049	0.368	2.848
OHIO	30,604	30,604	44.61		1.943	1.125	27.391	2.938	0.168	1.264	9.778
PENNSYLVANIA	34,970	34,970	50.97		122.2	1.285	31.298	3.357	0.192	144	11.173
RHODE ISLAND	149	149	0.22		9600.0	0.0055	0.133	0.014	0.0008	0.0062	0.048
S. CAROLINA	22	22	0.03		0.0014	0.0008	0.020	0.0021	0.0001	0.0009	0.007
TENNESSEE	22	22	0.03		0.0014	0.0008	0.020	0.0021	0.0001	0.0009	0.00
TEXAS	22	22	0.03		0.0014	90000	0.020	0.0021	0.0001	0.0009	700.0
UTAH	2,461	2,461	3.56		0.156	0600	2.202	0.236	0.014	0.102	0.786
W. VIRGINIA	18,589	18,589	27.09	->	1.180	0.683	16.637	1.785	0.102	0.768	5.939
EPA REGION											
<b>H</b>	828	626	1.37		0.0595	0.0385	98.0	60.0	0.0051	0.039	0.3
p	6,057	9,067	13.2		0.575	0.333	8.107	0.87	0 0498	0.374	2.594
В	59,614	59,614	86.88		3.785	2.19	53.351	5.723	0.327	2.462	18.04
Ħ	13,387	13,387	19.51		0.850	0.492	11.982	1.282	0.074	0.553	4.275
ы	999,848	99,848	145.53		9.3K	3.669	89.365	9.586	0.549	4.124	31 90:
E E	2	22	0.03	_	0.0014	0.0008	0.020	0.0021	0.0001	0.0009	0 000
茛	94	34	0.07		0.003	0.0017	0.043	0.0046	0.0003	0.002	0.015
TEX.	2,680	2,680	3.91		0.17	960.0	2.398	0.257	0.015	0.111	953 0
Ħ	4,580	089°, <b>↑</b>	89.68		0.291	0.168	4.099	0.44	0.025	0.189	1.463
NATIONAL TOTALS	190,173	190,173	81.772		12.075	6.9915	6.9915 170.208	18.254	1.045	7.855	60.761
					7	1		1			,

\*MULTIPLY BY 5.0 TO CONVERT TO APPROXIMATE WET WEIGHTS. MULTIPLY BY 1.1 TO CONVERT TO SHORT TONS. SOURCE: CALSPAN CORPORATION

ESTIMATED STATE, REGIONAL, AND NATIONAL WASTE FROM THE IRON AND STEEL INDUSTRY PICKLE LIQUOR, 1983 (METRIC TONS), DRY WEIGHTS\* Table 7o

			TOTAL			HAZ	ARDOUS CC	HAZARDOUS CONSTITUENTS	TS		į
STATE	DISPOSED	HAZARDOUS	CONSTITUENTS	DISPOSAL METHOD	ბ	8	.₩	2	£	Zn	GREASE
ALABAMA	9,627	129'6	14.03	NEUTRALIZE ON SITE	0.611	9520	8.616	0.924	0.053	0.398	3.076
CALIFORNIA	5,315	5,315	2.75	OR BY CONTRACT	0.337	0.195	4.757	0.510	0.029	0.219	1.698
COLORADO	25	ž	0.371	DISPOSAL SERVICE	0.016	0.0093	0.228	0.024	0.0014	0.011	0.081
CONNECTICUT	917	917	7		950.0	<b>1</b> 000	0.820	0.088	0.005	0.038	0.293
FLORIDA	8	**	990.0		0.0024	91000	0.034	0.0037	0.0002	0.0016	0.012
GEORGIA	8	8	9500		0.0024	0.0014	0.034	0.0037	0.0002	0.0016	0.012
ILLIMOIS	15,213		71.22		0.966	0.55	13.616	1.460	0.084	0.628	4.861
INDIANA	53,343	53 343	77.75		3.387	1.960	47.742	5.121	0.293	2.203	17.043
KENTUCKY	5,741	5,741	8.37		0.365	1170	5.138	0.551	0.032	0.237	1.834
MARYLAND	7,025		10.24		0.446	200	6.288	0.674	0.039	0.290	2.245
MICHIGAN	11,793	11,783	17.19		0.749	0.433	10.554	1.132	0.065	0.487	3.768
MISSISSIPPI	8	g	0.057		0.0025	0.0014	0.035	0.0038	0.0002	0.0016	0.013
MESSOURI	18	<b>38</b>	800		0.0035	0.002	0.049	0.0053	0.0003	0.0023	0.018
MEW JERSEY	<b>8</b>	<b>18</b>	0.241	-	0.011	0.0061	0.148	0.016	60000	0.0068	0.053
NEW YORK	10,344	10,344	15.08		0.657	0.380	9.258	0.993	0.057	0.427	3.305
040	35,512	35,512	51.76		2.255	1,305	31.784	3.409	0.195	1.467	11.346
PENNSYLVANIA	40,578		27.05		2.577	1.491	36.318	3.896	0.223	1.676	12.965
RHODE ISLAND	E	133	527	-	110.0	0.0064	0.155	0.017	0.001	1,000.0	0.055
& CAROLINA	æ	<b>1</b> C	0.037		9100.0	0.0009	0.023	0.002	0.0001	1100.0	0.0081
TENNESSEE	×	K	0.037		0.0016	00000	0.023	0.002	10000	0.0011	0.0081
TEXAS	×	X	0.037		0.0016	60000	0.023	0.002	0.0001	1100.0	0.0081
<b>HV</b> 15	2,865	2,865	4.16		0.181	9.105	2.556	0.274	0.016	0.118	0.912
W. VIRGINIA	21,571	71.571	31.44	•	1.370	0.793	19.306	2.071	0.119	0.891	6.892
EPA REGION											
-	1,080	1,090	25:		0.069	0.040	0.975	0.105	9000	0.045	0.348
=	10,510	10,510	15.32		0.668	0.386	9.406	1.009	0.579	0.434	3.358
B	689,174	68,174	100.82		4.393	2542	61.912	6.641	0.381	7987	22.102
M	15,534	15,534	22.64		0.986	0.571	13.903	1.490	980.0	0.642	4.963
Þ	115,862	Ξ.	168.87		7.357	1927	103.696	11.122	0.637	£78	37.018
5	£	10	0 037		0.0016	90000	0.023	0.002	0.0001	11000	0.0081
B	55	18	90.08		0.0035	0.002	0.049	0.0053	0.0003	0.0023	0.018
	3,110	3,110	4.53		0.197	0.174	2.783	0.298	0.0174	0.129	0.993
Ħ	5,315	5,315	7.75		0.337	0.195	4.757	0.510	0.029	0.219	1.698
NATIONAL TOTALS	220.675	220.675	321.64		14.013	8.108	197.504	21.182	1.2145	9.114	70.506
			T								

\*MULTIPLY BY 5.0 TO CONVERT TO APPROXIMATE WET WEIGHTS MULTIPLY BY 1.1 TO CONVERT TO SHORT TONS.

road baliast or building aggregate. It may be stored on the ground for many months or years before use for these purposes. Fine dust contains significant concentration of iron and is normally sent to sinter strand to be agglomerated prior to reprocessing for iron recovery. Sludge from wer emissions control is also sent to the sinter facility for agglomeration prior to reprocessing for iron recovery.

All of the blast furnace residuals (i.e. slag, dust, sludge) are considered non-hazardous. Fluorides may leach to the extent of a few parts per million from these materials which is not considered sufficient to pose an environmental threat.

Basic Oxygen Furnace. Residuals from basic oxygen furnaces include slag, dusts from dry emissions controls, sludges from wet emissions controls and kish from metal pouring. Basic oxygen furnace slag is usually open dumped after recovery of metallics. This practice is adequate since basic oxygen furnace slag is not considered potentially hazardous at the present time.

Dusts and sludges from emissions controls are usually open dumped as is kish. This practice is adequate since none of these wastes are considered potentially hazardous at the present time.

Open Hearth Furnaces. Slag from open hearth furnaces is usually open dumped after processing for recovery of metallics. Open hearth dusts from emissions controls are open dumped and are often wetted down before disposal to prevent blowing. At some steel plants open hearth dusts and BOF dusts are recycled to the sinter. Disposal practices are adequate since these wastes are considered non-hazardous at the present time.

Electric Furnaces. Residuals from electric furnaces include slag, dusts from dry emissions controls and sludge from wet emissions control. Slag is usually open dumped after recovery of metallics. A small amount of slag (approximately 10%) is used as road fill or railroad track ballast. These methods are adequate since electric furnace slag is not considered potentially hazardous.

Dusts from dry emissions control and sludge from wet emissions control can leach potentially hazardous heavy metals as previously discussed. Open dumping of these wastes as currently practiced is environmentally inadequate.

Soaking Pits. Slag is the only waste generated at the soaking pits. It is generally broken into chunks and hauled to open dumps. This practice is adequate since this waste is not considered potentially hazardous.

Mill Sludges. This category of residuals includes sludges from various mill operations at an integrated steel plant including primary mills which produce ingots, slabs and other primary steel shapes, continuous casting mills, hot rolling mills, cold rolling mills, galvanizing mills, and tin plating mills. Sludges from these mills are produced as a result of water pollution control operations including oil and grease removal, flocculation and settling of particulates, and pll adjustment.

All of the above sludges are considered potentially hazardous because of possible leaching of hazardous constituents including chromium, copper, nickel, lead, zinc and oil and grease.

Currently the most prevalent management of the above sludges is open dumping except for tin plating sludges which are put in unlined lagoons. These practices are inadequate because of the danger of toxic heavy metal leaching through permeable soils to groundwater.

Mill Scales. Mill scales containing over 50% iron are generated in primary and hot rolling mills, continuous casting mills, and cold rolling mills. Scales from primary and hot rolling mills and continuous casting mills are recycled to the sinter or blast furnace for iron recovery. This practice is environmentally sound since land disposal is precluded.

Scale from cold rolling mills is often highly contaminated with oil which discourages recycle to the sinter because of hydrocarbon emissions in the sinter. Normal disposal is by open dumping. This practice is not environmentally adequate because of the possible movement of oil and grease through permeable soils to groundwaters or surface waters.

Pickle Liquors. Currently the prevalent practice employed by steel plants for handling of waste pickle liquor is the service of outside contract disposal services who generally neutralize the acid before disposal in unlined lagoons. Disposal in unlined lagoons is inadequate if heavy metals leach from the sludge formed from neutralization and percolate through permeable soils to groundwater.

### 1.3.2 Present Treatment and Disposal Technology (Level I)

Coke Plant. Wastes from coking operations and associated byproduct production which are considered potentially hazardous include waste ammonia liquor, ammonia still lime sludge and decanter tank tar. Treatment of ammonia liquor in a biological treatment plant is adequate since destruction of potentially hazardous constituents (i.e. phenol, cyanide) is achieved. Inputs of these wastes to the biological treatment plant must be sufficiently dilute so as to not interfere with normal biological activity. Deep well disposal of waste ammonia liquor is adequate only when done according to EPA guidelines as stated in EPA Administrator's Decision Statement No. 5 dated February 6, 1973 (Reference 10).

Ammonia still lime sludge and decanter tank tar are presently open dumped. This practice is environmentally inadequate because of the danger of toxics including phenol, ammonia, or cyanide leaching and percolating to ground or surface water.

Electric Furnaces. Residuals from electric furnaces which are considered potentially hazardous include emission control dusts and sludges. Present disposal of dusts and sludges is open dumping. This practice is environmentally inadequate because of the danger of heavy metal leaching through permeable soils to groundwater or surface water.

Mill Sludges. Potentially hazardous sludges are generated from water pollution control operations in primary mills, continuous casting mills, hot rolling mills, cold rolling mills, galvanizing mills and tin plating mills. Present treatment and disposal is open dumping which is environmentally inadequate because of the threat of heavy metal and oil or grease leading.

Mill Scales. Potentially hazardous mill scales are generated in primary and hot rolling mills, continuous casting mills and cold rolling mills. The scale from all of these operations excepting cold rolling mills is normally recycled to the sinter for iron recovery and is environmentally adequate. Highly oil contaminated scale from cold rolling mills is presently open dumped. This practice is not environmentally adequate.

Pickle Liquor. Present treatment and disposal technology generally consists of disposal by contract disposal companies who neutralize the acid pickle liquor and leave the neutralization sludge in unlined lagoons. Some steel plants dispose of pickle liquor by deep well disposal. The use of unlined lagoons is not environmentally adequate because of the danger of toxic heavy metal leaching through permeable soils to groundwater or surface waters. Deep well disposal is adequate when done in accordance with EPA guidelines.

### 1.3.3 Best Technology Currently Employed (Level II)

Coke Plant. Level II technology for treatment and disposal of waste ammonia liquor, ammonia still lime sludge and decanter tank tar is the same as Level I and is inadequate except for deep well disposal of pickle liquors which is adequate.

Electric Furnaces. Level II technology for treatment and disposal of potentially hazardous electric furnace dusts and sludges is the same as Level I (i.e. open dumping) and is inadequate.

Mill Sludges. At approximately 5% of the steel plants sludges from primary and hot rolling mills are recycled through the sinter for iron recovery. This precludes land disposal and is therefore environmentally adequate.

Cold rolling mill and galvanizing mill studges are open dumped which is inadequate for environmental protection.

At some plants tin plating mill water treatment sludge is reprocessed for tin recovery. This is environmentally adequate.

Mill Scales. Level II treatment and disposal technology for mill scales from primary mills, continuous casting mills, hot rolling mills, and cold rolling mills is the same as Level I.

Fickle Liquors. At a few steel plants spent pickling liquor is processed for reclamation of sulfuric acid or hydrochloric acid and reuse in the pickling operations. The iron oxide or iron sulfate residues can be recycled for recovery of iron. This practice is environmentally adequate. Deep well disposal of pickle liquors according to EPA guidelines is adequate.

### 1.3.4 Technology to Provide Adequate Health and Environmental Protection (Level III)

Coke Plant. Biological treatment of waste ammonia liquor from the byproduct coke plant will detoxify toxic constituents including phenol, cyanide, and ammonia if present in low concentrations. Solvent recovery and ammonia stripping will normally precede biological treatment of ammonia liquor. Deep well disposal of pickle liquors in accordance with EPA guidelines is adequate for environmental protection.

Sealing of permeable soils at dump sites to prevent leaching of phenol, cyanide, or ammonia from lime sludge or decanter tank tar, or collection and treatment of leachate constitutes Level III treatment and disposal technology.

Electric Furnaces. Sealing of permeable soils at dump sites for disposal of sludge or dust from control of emissions from electric furnaces or collection and treatment of leachate will be necessary for adequate environmental protection.

Mill Sludges. If primary or hot rolling mill sludges are not recycled to the sinter, chemical fixation would be required prior to open dumping. Chemical fixation of cold rolling and galvanizing sludges would be required before open dumping.

Metal reclamation from tin plating sludge would qualify as Level III technology. If this sludge is lagoon disposed, the use of lined lagoons would be needed for adequate environmental protection.

Mill Scales. If mill scales are recycled to the sinter adequate environmental protection is assured. If mill scales are open dumped the use of bentonite or other soil sealants would be required to prevent percolation of toxic heavy metals or oil and grease, or collection and treatment of leachate would be necessary.

Pickle Liquor. Processing of spent pickle liquor to reclaim hydrochloric or sulfuric acid and metallic value (i.e. iron), or deep well disposal according to EPA guidelines is Level III technology.

Tables 8a through 8f summarize features of Levels I, II and III treatment and disposal technologies for potentially hazardous wastes from the iron and steel smelting and refining industry.

Table 8A

Treatment and Disposal Technology Levels

Smelting and Refining Category Iron and Steel SIC 3312

## Byproduct Coke Plant Wastes

	•				
Level III  (Adequate Health and Enviro- mental Protection)	Same as I	Same as I	Same as I	Same as for ammonia liquor; ground sealing of disposal area with bentonite or other sealant for lime and decanter tar sludge if significant leaching of phenol, cyanide or amments	Ammonia liquor - >90% Lime sludge - 0 Decanter tar - 0
(Best Currently Employed)	Same as I	Same as I	Same as I	Biological treatment or deepwell disposal according to EPA guidelines for lime sludge and decanter tar	Same as I
Level I (Prevalent)	Ammonia Liquor - dilute ammonia with traces of phenol and cyanide Lime Sludge - predominantly lime with phenols, cyanide, oil and grease, trace metals.  Tank Tar - tarry sludge; hydrocarbons with oil and grease, phenol, cyanide traces	Waste Ammonia Liquor - 190 Ammonia Still Lime Sludge - 0.6 Decanter Tank Tar - 4.5	Above wastes contain phenol and cyanide, ammonia and oils and greases, trace metals	Ammonia liquor* - biological treatment Line Sludge - open dump Decanter tar - open dump	Ammonia liquor - >90% Lime Sludge - >75% Decanter tar - >75%
Factor	Physical + Chemical Properties	Amount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment/ Disposal Technology	Estimate of # + % of Plants Using Technology

\*Included as land disposed waste only because a few plants dispose in deep wells.

Level III	Same as I	None	None	Compatible	Groundwater surveillance wells and surface runoff monitoring	Negligible
Level II	Same as I	None	Same as I	Compatible	None	Negligible
Level I	Adequate for ammonia liquor; inadequate for lime and tar sludges if significant leaching of phenol, ammonia or cyanide	Ammonia liquor normally is treated without land contact with discharge of treated effluent to receiving stream or sewer. A few plants use deep well disposal.	Lime and decanter tank tar sludges could contaminate ground or surface water if leached.	Compatible	None	Negligible
Factor	Adequacy of Technology	Problems and Comments	b Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

Treatment and Disposal Technology Levels

# Smelting and Refining Category Iron and Steel SIC 3312

## ELECTRIC FURNACE DUST

Level III (Adequate Health and Envisora-	mental Protection) Same as I	Same as I	Same as I	Ground sealing at disposal site	0
(Best Currently Employed)	Same as I	Same as I	Same as I	Same as I	\$0 <b>\$</b> <
Level I (Prevalent) (Be	Colloidal to silt size particles; iron, silica, lime, traces of heavy metals and fluoride	15.0	Contain trace heavy metals including Cr, Cu, , Ni, Pb, Zn and fluoride	open dumped	<b>\$08</b> 5.
Factor	Physical + Chemical Properties	& Amount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment/ Disposal Technology	Estimate of # + % of Plants Using Technology

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Level III	Adequate	None	None	Compatible	Groundwater monitoring Electric furnace dust disposal areas	Negligible
Level II	Same as I	None	Same as I	Compatible	None	Negligible
Level I	Inadequate	Significant leaching of lead from electric furnace dust in solubility tests	Possible contamination of groundwater or surface water	Compatible	None	Negligible
Factor	Adequacy of Technology	Problems and Comments	6 Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance	Energy Requirements

Table 37,

Treatment and Disposal Technology Levels

Smelting and Refining Category Iron and Steel SIC 3312

## ELECTRIC FURNACE SLUDGE

Level III (Adequate Health and Environmental Protection) Same as I	Same as I	Same as I	Chemical fixation if leaching of heavy metals from open dumped sludges	O chemical fixation
Level II (Best Currently Employed) Same as I	Same as I	Same as I	Open Dump	06<
Level I (Prevalent)  Colloidal to silt sire particles; iron, trace metals, fluorides	Electric furnace sludge - 5.8	Contain traces of heavy metals including Cr, Ni, Pb, Zn, Cu, fluoride	Open Dump	06<
Factor Physical + Chemical Properties	S Amount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment/ Disposal Technology	Estimate of # + % of Plants Using Technology

Level III	Adequate	None	None	Compatible	Groundwater monitoring wells	Negligible
Level II	Inadequate	Same as I	Same as I	Compatible	None	Negligible
Level I	Inadequate	Significant leaching of Cr, Pb in solubility tests	Possible contamination of groundwater and surface water	Compatible	None	Negligible
Factor	Adequacy of Technology	Problems and Comments	S Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

Table 8C - (cont'd.)

Table 8D

## Treatment and Disposal Technology Levels

# Smelting and Refining Category Iron and Steel SIC 3312

### PICKLE LIQUORS

Level III  (Adequate Health and Environmental Protection)  Same as II for acid regeneration  Same as I if not regenerated	Same as II	Same as I	Acid regeneration or neutralization with sludge kept in lined lagoons if heavy metals leach to EPA guidelines	10
Level II  (Best Currently Fmployed)  Iron sulfate or oxide salt residues; acid is 100% regenerated	No acid wasted (100% recycle) Residual salts are land dumped only if no market (36.3 kg, FeSO <sub>4</sub> )	Same as I	Acid regeneration or deep well disposal according to EPA guidelines	10
Level I (Prevalent)  Dilute sulfuric or hydrochloric acid with dissolved and particulate iron	Cold rolling mills - 22.8 Galvanizing Mills - 5.17	Acid, trace heavy metals including Cr, Cu, Mn, Ni, Pb, Zn	Outside contract disposal service who neutralize in unlined lagoons	~95 <b>%</b>
Factor Physical + Chemical Properties	G Amount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment/ Disposal Technology	Estimate of # + % of Plants Using Technology

Level III	Adequate	None	None	Compatible	Groundwater monitoring, Well and surface runoff monitoring	Moderate for acid regeneration, negligible for lined lagoon
Level II	Inadequate if land dumped residues leach heavy metals; adequate for acid problem	None	Possible contamination of ground and surface water by residual salts if leached of heavy metals	Compatible	None	Moderate (0.24 kw/MT Steel)
Level I	Inadequate	None	Possible contamination of ground and surface water	Compatible	None	Negligible
Factor	Adequacy of Technology	Problems and Comments	د Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

### Table 8E

Treatment and Disposal Technology Levels

Smelting and Refining Category Iron and Steel SIC 3312
MILL SLUDGES (galvanizing, primary, continuous casting, hot rolling, cold rolling, tin-plating)

Level III (Adequate Health and Enviro-	Same as I	Same as II	Same as I	Primary & hot rolling mill - recycle to sinter or chemical fixation Cold rolling & galvanizing - chemical fixation Tin plating - merel	Primary & hot rolling - <5% recycle, 0 chemical fixation Cold rolling & galvanizing - 0 chemical fixation lin plating - 1.0% tin reclasarion of the dageon
Level II (Best Currently Employed)	Same as I	No sludge waste from primary, hot rolling, or tin plating mill if reprocessed; other factors for other mill sludges same as Level I	Same as I	Primary, continuous casting, f hot rolling mill-recycle to sinter Coldrolling & galvanizing mill-open dump Tin plating mill-tin reclamation	Primary & hot rolling - 5% Cold rolling & galvanizing- 90% Tin plating - 20%
Level I (Prevalent)	Mill sludges are colloidal to silt size aggregated particles, high in iron; trace metals, oils and greases	Galvanizing Mill - 10.8 Primary Mill - 1.87 Continuous Casting - 0.104 Hot Rolling Mills - 1.74 Cold Rolling Mills - 0.159 Tin Plating Mill - 0.532	Contains trace heavy metals including Cr, Cu, Mn, Ni, Pb, Zn and oil and grease	Open dumped except for tin plating sludges which are lagooned	\$06
Factor	Physical + Chemical Properties	s Amount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment/ Disposal Technology	Estimate of # + % of Plants Using Technology

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Level III	Adequate	None	None	Compatible	Groundwater surveillance wells and surface runoff monitoring	Negligible
Level II	Adequate if sludges are recycled - otherwise same as I	Non <b>e</b>	Same as I	Compatible	None	Negligible
Level I	Inadequate if significant leaching of heavy metals	None	Possible contamination of ground or surface water if leached oil and grease or heavy metals percolate through permeable soils	Compatible	None	Negligible
Factor	Adequacy of Technology	Problems and Comments	G Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

Table 8F

Treatment and Disposal Technology Levels

Smelting and Refining Category Iron and Steel SIC 3312

MILL SCALES (Primary mills, continuous casting, hot rolling, cold rolling)

Level III (Adequate Health and Enviro-	mental Protection) Same as I	Same as I	Same as I	Recycle to sinter or ground sealing with bentonite or other sealant if land starosed	O ground sealing
Level II (Best Currently Employed)	Same as I	Same as I	Same as I	Same as I	Same as I
Level I (Prevalent)	Fine sand to small granular size flaky particles - predominantly iron (>60-70%)	Primary Mill - 44.9* Continuous Casting - 8.7* Hot rolling mills - 18.3* Cold rolling mills - 0.052	Contain trace heavy metals including Cr, Cu, Mn, Ni, Pb, Zn, oil and grease	Primary & hot rolling & continuous casting - recycled to sinter or blast furnace Cold rolling mills - open dump	%06<
Factor	Physical + Chemical Properties	9 Amount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment/ Disposal Technology	Estimate of # + % of Plants

\*These scales are not wasted if recycled to sinter or blast furnace ~80% of total scale is recycled.

Using Technology

Level III	Adequate	None	None	Compatible	Groundwater surveillance and surface rumoff monitoring	Negligible
Level II	Same as I	None	Same as I	Compatible	None	Negligible
Level I	Recycling - adequate; inadequate if land dumped and heavy metal leaching occurs	None	Possible contamination of surface or ground water if heavy metals or oils and greases leach	Compatible	None	Negligible
Factor	Adequacy of Technology	Problems and Comments	S Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

### 1.4 COST ALALYSIS

In the last section various treatment and disposal technologies currently employed or considered for adequate health and environmental protection were described. The costs of implementing this technology for a typical integrated iron and steel mill complex are estimated in this section. Costs of land disposal from individual operations such as steel fur makes and rolling mills are also given. The exemplary plant has an annual capacity of 2,500,000 MT of steel and is assumed to operated 350 days per year. Facilities at the plant include the operations given in Table 4 and generate the wastes listed previously in Table 5. All disposal lites are situated on semi-industrial land.

### Dust

Dust results from blast furnace, basic oxygen furnace and electric furnace operations. Dust from the blast furnaces is recycled to the sinter plant. No disposal cost is incurred. The dust from the basic oxygen furnace operations amounts to only 288 MT (222 m<sup>3</sup>)/year. It is not considered hazardous.

Electric Furnace Dust. Dust from the electric furnaces considered potentially hazardous (7,500 MT or 4165 m<sup>3</sup>/yr) is hauled to an on-site dump. This requires 1 hr/day of front loader and truck time plus 40 hrs/yr of bulldozer time at the dump. The dust is piled to a height of 5 m. The dump area is sized to hold 20 years of waste and extends over 1.7 ha.

### Electric Furnace Dust

### Capital Cost

Dust Dump Survey Land Equipment Truck (12.5%) Front Loader (12.5%) Bulldozer (2%)	\$	1,065 6,725 3,125 2,500 320
Total	\$1	3,735
Annual Cost		
Land Construction Amortization Equipment Amortization Equipment Repair and Maintenance Operating Personnel	\$	675 125 945 295 8,045
Energy Fuel Electricity Taxes Insurance	_	995 100 170 135
Total 58	\$1	1,485

### Sludge

Sludge wastes are generated by all operations except by the electric furnaces (where a dry control system is assumed) and the soaking pits.

Coke Oven Sludge. Ammonia still lime sludge (6,160 MT or 5,135 m<sup>5</sup>/yr) is produced at the coke ovens. The sludge is disposed at a dump. One hr/day of frontloader and truck time are needed for loading and transporting the sludge and 50 hrs/yr of bulldozer time at the dump site. The sludge is piled to a height of 5 m. The dump occupies 2.1 hectares and accommodates 20 years of waste sludge.

### <u>Coke Oven Sludge</u> (ammonia still lime sludge)

Capital Cost Sludge Dump Survey		,315
Land	8	3,305
Equipment	_	
Truck (12.5%)		3,125
Front Loader (12.5%)	2	2,500
Bulldozer (2.5%)		400
Total	\$15	,645
Annual Cost		
Land	\$	830
Construction Amortization	•	155
Equipment Amortization		960
Equipment Repair & Maintenance		300
Operating Personnel	S	3,170
Energy	·	,,1/0
Fuel	1	,005
Electricity	•	100
Taxes		210
Insurance		
insurance		155
Total	\$11	,885

Primary and Other Hot Rolling Mill Sludge. The primary and other hot rolling mills produce 5739 MT of sludge per year. The scale wastes generated by these operations are recycled to sinter on the blast furnace. However, about 2 percent of the scale, containing oil contaminants, is skimmed off and disposed with the sludge.

The total yearly waste disposed is about 7,750 MT or 4840  $\rm m^3$ . Loading and hauling require 1 hr/day of front loader and truck time, and 50 hrs/yr of bulldozer time is assigned at the dumpe site. The dump occupies 1.9 ha.

### Primary and Other Hot Rolling Mill Sludge

Capital Cost	
Sludge Dump	
Survey	\$ 1,190
Land	7,515
Equipment	
Truck (12.5%)	3,125
Front Loader (12.5%)	2,500
Bulldozer (2.5%)	400
(2.00.)	
Total	\$14,730
	<u> </u>
Annual Cant	
Annual Cost	d mro
Land	\$ 750
Construction Amortization	140
Equipment Amortization	960
Equipment Repair & Maintenance	300
Operating Personnel	8,170
Energy	
Fuel	1,005
Electricity	100
Taxes	190
Insurance	145
Total	\$11,760

Cold Rolling Mill Sludge. The cold rolling mills produce only 111 MT of sludge annually. For the purpose of costing, the disposal cost of this sludge is combined with that generated by the galvanizing mill.

Tin Plating Mill Sludge. The sludge from the tin plating mill is disposed in a lagoon. The wet sludge (50% solids) produced annually amounts to 1064 MT. The lagoon is sized to hold 20 years of waste. The lagoon characteristics are:

Volume	21,300	m <sup>3</sup>	Circumference	390	m,
Bottom Width	55	m	Dike volume	5,900	m <sub>o</sub>
Top width	67	m	Dike surface	5,540	m <sup>2</sup>
Bottom length	110	m	Total width	81	m
Top length	122	m	Total length	136	m
Total depth	3	m	Required area	1.1	ha
Depth of Excavation	.9	m	-		

### Tin Plating Mill Sludge

Capital Cost	
Lagoon	
Site Preparation	
Survey	\$ 690
Test Drilling	980
Sample Testing	500
Report Preparation	1,500
Construction	
Excavation and Forming	7,845
Compacting	10,910
Fine Grade Finishing	2,490
Soil Poisoning	485
Transverse Drain Fields	1,500
Land	4,350
Total	\$31,250
Annual Cost	
Land	\$ 435
Construction Amortization	2,695
Construction Maintenance & Repair	695
Taxes	110
Insurance	315
Total	\$ 4,250

Galvanizing Mill Sludge. The sludge produced by the galvanizing mill is combined with that from the cold rolling mill. Also included is the small amount of scale waste (36 MT/yr) from the cold rolling mill. The total waste disposed is 1500 MT/yr. Loading, hauling and diposing on land requires about .25 hrs/day of front loader and truck time and a .4 ha sludge dump.

### Galvanizing and Cold Rolling Mill Sludge

Capital Cost	
Sludge Dump	
Survey	\$ 250
Land	1,580
Equipment	
Truck (5%)	1,250
Front Loader (5%)	1,000
Total	\$ 4,080

Annual Cost	
Land	\$ 160
Construction Amortization	30
Equipment Amortization	360
Equipment Repair & Maintenance	115
Operating Personnel	1,890
Energy	
Fuel	240
Electricity	25
Taxes	40
Insurance	 40
Total	\$ 2,900

### Scale

Scale is produced by primary and hot rolling mills and the cold rolling mills. Practically all of the scale of the former is recycled to sinter or blast furnaces. No disposal costs are incurred. Scale from the cold rolling mill is land disposed together with the sludge from that operation. No separate costs are incurred.

### Waste Pickle Liquor

Waste pickle liquor results from cold rolling and galvanizing mill operations. The liquor is treated and disposed of by an outside contractor at a cost of \$10.55/m<sup>3</sup> (\$.04/gal).

No capital costs are incurred. The annual cost is \$149,010.

### Waste Ammonia Liquor

Waste ammonia liquor is normally not land disposed. It is normally detoxified in a biological treatment plant as a minor flow. Occasionally it is disposed of in deep wells. The associated costs of deep well disposal were not ascertained since no land disposal is considered as Levels I, II and III treatment and disposal technology.

### 1.4.2 Cost of Best Technology Currently Employed (Level II).

### Dust

Dust disposal and associated costs are the same for Level II as Level I.

### Sludge

Sludge from the blast furnaces, basic oxygen furnaces and primary and hot rolling mills can be recycled to sinter depending on its composition.

Tin plating mill sludge in some plants has a sufficiently high metal content so that it can be sold to an outside contractor for metal reclamation. We were unable to obtain information on prices paid by reclaimers for the sludge. This treatment method would eliminate the need for the lagoon specified for Level I and its associated costs. Level II treatment for the other sludges is the same as for Level I.

### Waste Pickle Liquor

Acid regeneration is the Level II treatment for waste pickle liquor. Reference 2 indicates a cost of \$13/m of waste treated. This cost is included as an annual cost. It includes the amortization of capital treatment plant investment. Acid regeneration results in an annual cost of \$183,610 which is about a \$35,000 increase over the Level I treatment cost.

Incremental changes resulting from the implementation of Level II technology are shown below.

	Capital Cost	Annual Cost
Slag	<u></u>	-
Dust	-	-
Sludge	(\$31,250)	(\$4,250)
Waste Pickle Li	quor -	34,600
Total	(\$31,250)	\$30,350

- () = savings engendered by sale of tin plating mill sludge and resultant elimination of sludge lagoon.
- 1.4.3 Cost of Technology to Provide Adequate Health and Environmental Protection (Level III)

### Dust

The soil is sealed at the dump used for storing the dust from the electric furnaces. Collection ditches, pump and piping are provided at the dump site.

### Electric Furnace Dust

Capital Cost	
Soil Sealing	\$34,000
Collection ditches	1,970
Pump	9,100
Piping	2,210
Total	\$47,280

Annual Cost		
Construction Amortization	\$ 4,175	
Equipment Amortization	1,800	
Construction Repair & Maintenance	1,080	
Equipment Repair & Maintenance	565	
Energy		
Fuel Electricity	95	
		Insurance
Total	\$ 8,190	

### Sludge

The soil is sealed at the coke oven sludge dump; collection ditches, pump and piping are installed.

### Coke Oven Sludge

Capital Cost Soil Sealing Collection Ditches Pump Piping	\$ 42,000° 2,195 9,300 2,210
Total	\$ 55,705
Annual Cost Construction Amortization Equipment Amortization Construction Repair & Maintenance Equipment Repair & Maintenance Energy Fuel	\$ 5,130 1,835 1,325 575
Electricity Insurance	110 560
Total	\$ 9,535

The sludges from the primary and other hot rolling mills as well as those from the galvanizing and cold rolling mills are chemically fixed prior to land disposal.

### Primary and Other Hot Rolling Mill Sludge

Capital Cost Annual Cost	Not Applicable	
Chemical Fixation	<b>\$6</b> 3,930	
Total	\$63,930	
	64	

#### Galvanizing and Cold Rolling Mill Sludge

Capital Cost Annual Cost

Not Applicable

Chemical Fixation

\$13,175

Total

\$13,175

Level III for tin plating mill sludge disposal consists either of the sale of the sludge to a metal reclaimer or installing a lagoon liner where the sludge is disposed on land. The former entails no cost to the plant. Costs for the latter are shown below.

#### Tin Mill Sludge

Capital Cost Lagoon Liner	\$38,235
Total	\$38,235
Annual Cost Construction Amortization	\$ 4,440
Construction Repair & Maintenance	1,145
Insurance	380

Total

#### Waste Pickle Liquor

Level III treatment of waste pickle liquor consists either of acid regeneration or neutralizing the waste by lime treatment, allow for settling of the sludge in a lined lagoon followed by chemical fixation and land disposal of the sludge. Acid regeneration involves no additional costs beyond those listed under Level II treatment. Costs for the other alternative is shown in Table 9.

The total annual waste liquor amounts to 15,100 MT. This results in the formation of 6,285 MT or 4,910 m  $^3$  of sludge. The selected lagoon size is 10,000 m and it assumed that 4,910 m of sludge are dredged annually. The removed sludge is chemically fixed and hauled to a dump site.

A 236 1/min sturry pump is used for dredging. The pump is operated 350 hrs/yr and 400 hours of labor are assigned to its operation. Loading and hauling of the sludge to the dump site requires 265 hrs/yr of front loader and truck time and 50 hrs/yr of bulldozer time at the sludge dump.

TABLE 9 . COST OF LEVEL III TREATMENT AND DISPOSAL TECHNOLOGY

INTEGRATED STEEL MILL - PICKLE LIQUOR SLUDGE

## Capital Cost

Const	Report Preparation ruction Excavation and Forming		1,200 4,535
	Compacting		6,310
	Fine Grade Finishing		1,705
	Soil Poisoning		345
	Transverse Drain Field		855
	Lagoon Liner	2	20,025
Land	,		2,375
Sludge			
	Survey		625
	Land		3,955
Equipme	ent		
	Slurry Pump	;	13,730
•	Flexible Pipe (100 m)		440
	Front Loader (15%)		3,000
	Truck (15%)		3,750
	Bulldozer (2.5%)		400
	Total	\$ 6	4,365

## TABLE 9 (Continued)

#### Annual Cost

Land	635
Construction Amortization	4,270
Equipment Amortization	3,405
Construction Repair and Maintenance	1,015
Equipment Repair and Maintenance	1,065
Operating Personnel	10,110
Energy Fuel	775
Electricity	90
Chemical Fixation	64,810
Taxes	160
Insurance	645
Total	\$ 86,980
Less Acid Regeneration	(183,610)
Total	( <b>\$96</b> ,930)

( ) = savings

#### The lagoon characteristics are:

Volume	10,000	m	Circumference	277	m,
Bottom width	36	nı	Dike volume	3,410	m <sup>3</sup>
Top width	48	m	Dike surface	3,790	m
Bottom length	72	m	Total width	62	m
Top length	84	m	Total length	98	m
Total depth	3	m	Required area	16	ha
Depth of excavation	1.15	m	•		

The dump is sized to hold 20 years of waste piled to a height of 10 m. It occupies 1.0 ha. The lime treatment facility used to neutralize the waste pickle liquor is considered part of the water treatment system and its cost is not included.

Summary costs for Level I, II and III waste treatments for an integrated steel plant are given in Table 10. Annual costs for Levels I and II disposal of potentially hazardous wastes are estimated as \$7,570,000 which represents less than 0.1% of the estimated 1973 sales value. Annual costs for Level III technology (i.e. adequate for environmental protection) are estimated as \$12,930,000 or 0.15% of estimated 1973 sales value.

68

COST SCAMARY FOR TREATMENT AND DISCOSAL TECHNOLG. . IRON AND SILEL TABLE 10 -

Annual Production: M Waste (Type)	Model Plant e)	2,500,000 MI Amou	in t	Industry 100,92 (MT/MT of Production)	Industry 190,929,000 MT ff of Production)	,000 MT			
Dust Sludge Pickle Liquor	luor		0.003 0.007 0.006						
Unit Waste Disposal	osal Costs:				Level				
	\$/MT of Waste	н	\$/MT of Prod.	\$/MT of Waste	/\$ /\$	\$/Mï of Prod.	\$/MT of Waste	111	\$/NT of Prod.
	\$ 1.83 1.53		\$ 0.005	\$ 1.83 1.53	₩	0.005	\$8.14		\$ 0.02 0.008
udge Capital Cost Annual Cost	3.99 1.87		0.03	3.99		0.03	9.69		0.06
quor Cost Cost	10.55		0.06	13.00	J	0.07	13.00		0.07
Total Capital Cost Total Annual Cost Cum. Industry Waste	Capital Cost Annual Cost Industry Waste Disposal C	\$0.04 0.08 al Costs (\$ Million)	\$0.04 0.08 4111ion)	1 1	<b>\$</b>	\$0.04 0.09	: :		\$0.08 0.13
			Le	Level					
	H			II	I	III			
Dust Sludge Pickle Liquor Total:	\$0.50 3.03 4.03	\$0.50 1.01 6.06 \$7.57	Cap. \$0.50 3.03 	Ann. \$0.50 1.01 7.07 \$7.57	Cap. \$2.02 6.06	\$0.81 5.05 7.07 \$\$2.93			
ice: \$8	1973 Metal Price: \$82.57/MT  Darcant Treatment Cost/Duice of Metric Ton of Production	f Metric	Ton of P	roduction					
			Le	Level					
	I		11		1	III			
Dust Sludge Pickle Liquor Total:	Cap; 0.04 0.05%	Ann. 0.01% 0.01 0.07 0.09%	Cap. 0.01% 0.04 	Ann. 0.01\$ 0.01 0.08	Cap. 0.02% 0.07	Ann. 0.01% 0.06 0.08 0.15%			

#### 2.0 IRON AND STEEL FOUNDRIES

#### 2.1 INDUSTRY CHARACTERIZATION

The three major groupings of ferrous castings are gray and ductife from castings, malleable iron castings, and steel castings. While specific procedures might vary from foundry to foundry, the overall operations for producting castings of all three types are essentially the same and include metal melting and pouring, casting shakeout and cleaning and finishing.

There are about 2000 foundries in the U.S. producing ferrous castings. There is great variability in plant size with monthly capacities ranging from 20 net tons to over 10,000 net tons.\* It is important to note that only about 60 percent of all castings produced in the United States are covered under SIC 332 (Iron and Steel Foundries). The remaining 40 percent are produced under other SIC categories, such as SIC 3714 (Motor Vehicles), SIC 3541 (Machine Tools), etc.

The production data and waste data presented in this report represents only those operations covered under SIC 332 which are within the primary metal smelting and refining industry.

The 1973-74 directory of members of the Gray and Ductile Iron Founders Society, Inc. lists 186 foundries. The monthly average production of these foundries was calculated to be about 1125 MT of finished castings giving an average annual production of 13,500 MT. Using data from "The Metal Casting Industry Census Guide" (1972 Edition, published by Penton Publishing Co., Cleveland, Ohio), the average annual production for all gray and ductile iron foundries (an estimated 1300 to 1500 foundries) was calculated to be about 9,250 MT. Thus, a reasonable capacity figure for a typical gray and ductile iron foundry plant would be about 11,000 net tons per year.

Steel foundries average about 5,440 MT of capacity per year and malleable iron foundries average about 12,700 MT per year.

Table 11 gives state by state, regional, and national shipments of the various type of ferrous castings for 1973. These figures are believed to reflect 1973 capacity. Iron and Steel foundries are concentrated in states heavy in manufacture of iron and steel and automobiles and heavy industrial equipment which are principal consumers of foundry castings.

#### 2.2 WASTE CHARACTERIZATION

This section contains descriptions of production technology at ferrous foundries and the resultant byproducts or wastes which are either recycled directly, reprocessed, or disposed of on land or in lagoons.

\* amount of metal smelted for finished castings exceeds net output of castings products.

TABLE 11
STATE, REGIONAL, AND NATIONAL SHIPMENTS OF IRON AND STEEL CASTINGS, 1973\*
(METRIC TONS)

Sta <b>te</b>	Gray & Ductile	Malleable	Steel	Total Iron &
	Iron Castings	Iron Castings	Casting	Steel Castat.
Alabama	1,543,121	17,237	87,090	1,647,448
Arizona	0	0	58,060	58,060
California	412,769	Q	60,781	473,550
Colorado	98,883	0	5,443	104,326
Connecticut	35,380	8,165	0	43,545
Delaware	0	0	6,350	6,350
Florida	9,072	0	10,886	19,958
Georgia	10,886	0	6,350	17,236
Illinois	1,364,406	118,841	236,775	1,720,022
Indiana	970,688	35,380	72,575	1,078,643
Iowa	368,317	9,072	23,587	400,976
Kansas	10,886	0	59,874	70,760
Kentucky	291,206	0	0	291,206
Lousiana	9,072	0	12,701	21,773
Maryland	72,575	0	6,350	78,925
Massachusetts	59,870	1,814	0	61,684
Michigan	2,597,270	395,533	60,781	3,053,584
Minnesota	170,551	10,886	20,865	202,302
Missouri	63,503	0	49,895	113,398
Nebraska	10,886	0	13,608	24,494
New Jersey	347,452	0	6,350	353,802
New York	822,820	16,329	72,575	911,724
North Carolina	107,048	0	0	107,048
Ohio	2,255,260	128,820	318,422	2,702,502
Oklahoma	34,473	0	10,886	45,359
Oregon	9,979	0	32,659	42,638
Pennsylvania	1,954,980	111,584	221,353	2,287,917
Rhode Island	28,120	3,629	0	31,749

STATE, REGIONAL, AND NATIONAL SHIPMENTS OF IRON AND STEEL CASTINGS, 1977 (METRIC TONS)

TABLE 11 (cont.)

State	Gray & Ductile Iron Castings	Malleable Iron Castings	Steel Castings	Total Iron & Steel Castings
South Carolina	25,401	0	0	25,401
South Dakota	0	0	2,722	2,722
Tennessee	378,296	0	37,195	387,368
Texas	495,323	29,030	42,638	566,991
Utah	196,859	Q	9,072	205,931
Vermont	9,980	907	0	10,887
Virginia	162,386	0	5,443	167,829
Washington	9,072	0	26,308	35,380
West Virginia	74,389	1,814	9,979	86,182
Wisconsin	453,592	46,266	130,635	630,493
EPA Region				
ī	133,350	14,515	0	147,865
11	1,170,272	16,329	78,925	1,265,526
111	2,264,330	113,398	249,475	2,627,203
IV	2,365,030	17,237	141,521	2,523,788
V	7,811,767	735,726	840,053	9,387,546
IV	538,868	29,030	66,225	634,123
VII	453,592	9,072	146,964	609,628
VIII	295,742	0	17,237	312,979
IX	412,769	0	118,841	531,610
X	19,051	0	58,967	78,018
U.S. Total	15,464,771	935,307	1,718,208	18,118,286

<sup>\*</sup> Believed to Reflect U.S. Production Capacity in 1973

Istimates are given for the quantities of wastes and potentially hazardous constituents thereof which are disposed of on land either in lagoons, landfills or open dumps.

#### 2.2.1 Process Descriptions

While specific procedures might vary from foundry to foundry, the overall operations for producing iron castings, malleable iron castings, and steel castings are essentially the same and include: sand preparation, mold and core making, metal melting and pouring, casting shakeout, and cleaning and finishing. The interrelationship between major operations in a typical foundry is shown in Figure 2. Also shown are the major sources of solid wastes. Although not all foundries practice sand reclamation, its use has become sufficiently widespread in the industry to require its inclusion in Figure 2.

Clay bonded molding sands are prepared by mixing silica sand, organic additives, bentonite clay and water together. Some foundries use olivine, zircon, chromite, biasill or other aggregates instead of silica sand. Carbonaceous material in the amount of 2 to 10 percent is also added to the molding sand as may be required to impart special properties. Materials in this category include finely ground bituminous coal, ground corn flower, fuel oil, and finely ground cellulose material.

The molds are made by packing the molding sand around previously made patterns to form the required shapes. For castings having hollows or recesses, cores are required to complete the mold. Since the cores must be removed after the castings have solidified, the core sands have special properties that facilitate their removal. The desired properties are achieved through the use of special binders, the most common of which are: (1) combinations of vegetable, fish and petroleum oils; (2) phenol formaldehyde resin, (3) sodium silicate; (4) phenolic isocyanate; (5) alkyd isocyanate; and (6) mixtures of urea and furfural alcohols. The first item is generally baked to promote hardening, and items 2 and 6 are generally heat-cured. The difference is that baking is done at the rate of approximately one hour per inch of thickness while curing is done in a matter of 30 to 60 seconds at approximately the same temperature. In the case of sodium silicate binders, hardening is achieved by forcing CO, gas through the sand. For the isocyanate binders setting occurs at room temperature through the use of special catalysts. For the ureafurfural alcohol binders, setting is possible at room temperature or higher depending on the type of catalyst used. With the successful use of the newer core binders that do not require high temperatures for setting, it appears that fewer and fewer foundries will continue the practice of core baking.

In addition to special binders, certain other materials are frequently used in preparing core sands. These include: iron oxide, ground corn flour; water soluble compounds of wood sugar; coke pitch; and ground hardwood cellulose. These materials facilitate removal of cores.

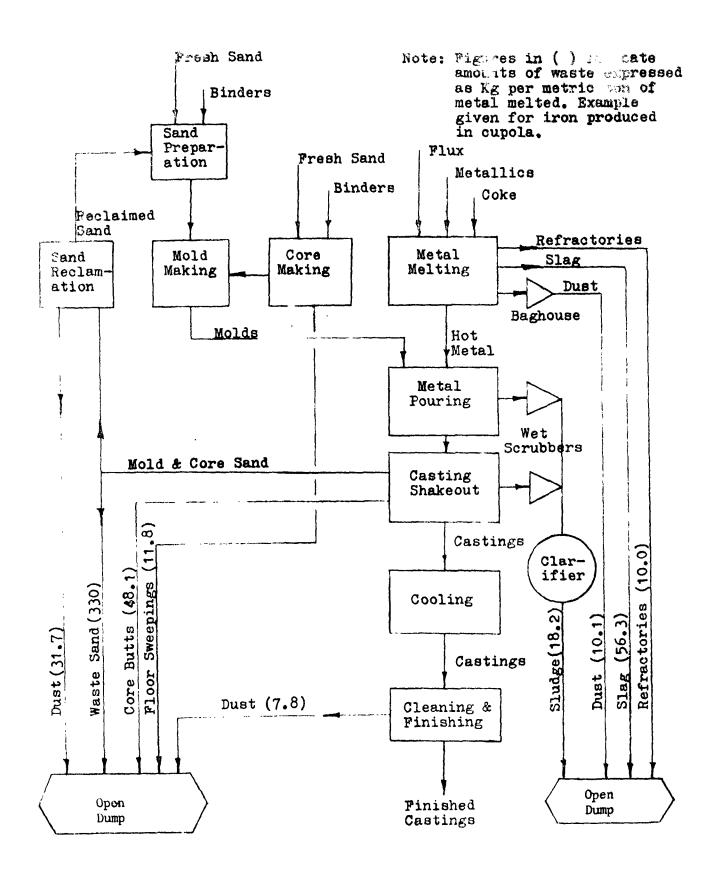


Figure 2 - Foundry Operations
74

Once the cores are formed and cured, they are integrated with the final molds which are then transferred to the metal pouring area. Molten metal of the desired composition is prepared in one of several different types of commonly used furnaces. Charge materials for the cupola furnace usually consist of a flux material, coke, and metallics. Electric arc or induction furnaces do not require coke. Typical fluxes include limestone (CaCO<sub>3</sub>), fluorspar (mostly CaF<sub>3</sub>), and soda ash (Na<sub>2</sub>C)<sub>2</sub>). The metallic charge consists mainly of external scrap and some internally generated scrap. For producing gray and ductile iron castings, cupolas and electric induction furnaces are the most widely used, with cupolas accounting for an estimated 60 to 65 percent of total production. Reverberatory furnaces account for one percent or less of gray and ductile iron castings. Most malleable iron castings are produced in cupolas and electric induction furnaces, although a number of air furnaces are still in operation. Electric arc furnaces account for almost all of the steel castings produced with electric induction furnaces accounting for probably less than 5 percent.

The molten metal is tapped from the furnaces into ladles and poured into the waiting molds. After the castings have solidified they are separated from the molds in the shakeout area. The separated castings are then cooled prior to cleaning and finishing. Cleaning and finishing operations include shot blasting, chipping and grinding.

Following casting shakeout, the mold and core sands are screened. Larger remnants of undisintegrated cores (core butts) and larger chunks of molding sand are transferred to a disposal area. Most of the molding sand, along with the degraded core sand, proceed directly back to molding sand preparation without going through sand reclamation (i.e., this sand is recycled, rather than being reclaimed). In some foundries a portion of this return sand is bypassed through a reclamation system and then returned to either the core or molding sand mixing operation. In the case of no-bake sands, most of the sand from the shakeout may be returned through the sand reclamation unit before recoating. Excess sand is sent to landfill.

#### 2.2.2 Description of Waste Streams

The major types of solid wastes generated at iron and steel foundries were indicated in Figure 2. The general types of waste generated are essentially independent of the type of metal being cast and the type of furnace in use. On the other hand, metal type and furnace type can affect the quantities of waste produced. The numbers in parentheses in Figure 2 indicate the amounts of waste in each category expressed as kilograms of waste per ton of metal melted. The numbers correspond to an average plant producing iron in a cupola. The values are given on the basis of a ton of metal melted rather than on the basis of a ton of finished castings, because yield factors (weight of finished casting/weight of metal melted) vary depending on the foundry and the type of metal cast. For iron (gray, ductile and malleable) the yield factor is generally in the range of 0.6 to 0.7, while for steel values of 0.5 are common. For the purpose of computing total waste quantities for an average iron foundry,

a yield factor of 0.65 would be reasonable. Thus, a typical iron founday would make about 11,000/0.65 = 16,900 tons of metal per year (15,300 metric tons/year).

Whate Sand. As stated previously and shown in Figure 2 there are two types of waste sand. One type is the clay bonded molding sand used in interior parts of the mold. Combined production of the two types of caste sand is 330 kg/MT of cast product. Although these sands have different organic additives as described on page 72 the organic fractions are burned and charred during the pouring of molten metal leaving principally sand coated with carbon residues and traces of metal compounds including copper, lead, chromium and zinc. Solubility tests on spent foundry sand as described in Appendix B did not show significant leaching of heavy metals or phenol. For this reason foundry sands are not considered potentially hazardous at this time.

Core Butts. After the metal pouring process most of the sand is devoid of binder and has little aggregation. Quite often portions of the core sand retain its binder. It is removed as large chunks known as core butts and brought to dumping areas. Core butts are generated at a rate of 48.1 kg/MT of casted metal. Although solubility testing on core butts was not conducted it is not expected to leach to a greater extent than spent sand. Core butts are therefore not considered potentially hazardous at this time.

Dust. Dust is generated at a rate of 31.7 kg/MT of foundry product from the sand reclamation process and from baghouses on metal milling furnaces. Dust will principally be silica oxides and iron oxides with traces of heavy metals including lead, cadmium, copper chromium, nickel, and zinc. Solubility tests on foundry dust as described in Appendix B did not show significant leaching of potentially hazardous metals. For this reason foundry dust is not considered potentially hazardous at this time.

Sludges. Wet scrubbers used to scrub emissions from metal pouring operations produces a wastewater which in turn produces a sludge at a rate of 18.2 kg/MT cast metal product. This sludge will contain iron for the most part along with traces of cadmium, copper, chromium, nickel, lead and zinc. Solubility tests were not conducted on sludges. They would be expected to be of similar composition and nature as furnace dusts however which were studied in solubility tests as described in Appendix B. Since the dusts did not leach significant concentrations of toxic constituents sludge was assumed to be of a similar solubility and therefore is considered as not potentially hazardous at this time.

Slag. Slag from iron and scrap steel furnace smelting is produced at a rate of 56.3 kg/MT of finished iron and steel casting. The gravel size to sand size pieces of slag contains iron, lime and soda ash principally, with small traces of heavy metals including cadmium, copper, chromium, nickel, lead and zinc. Solubility tests as described in Appendix B did not show significant leaching of potentially toxic constituents. For this reason furnace slag from iron and steel foundries is not considered hazardous at this time.

Floorsweepings. Cleanup of floors in core making rooms results in sandy floor sweepings at a rate of 11.8 kg/MT of product. This is assumed similar to other waste sands and therefore non-hazardous at this time. Solubility tests were not conducted on floor sweepings.

Refractories. Broken and weathered brick refractories from metal melting furnaces are generated at a rate of 10 kg/MT of finished castings. These bricks are predominantly highly insoluble fired clay ceramic and are not considered potentially hazardous.

Appendix A gives analyses of iron and steel foundry wastes including sands, dust and slag.

#### 2.2.3 Waste Quantities

Table 12 gives generation factors for the various residuals from iron and steel foundry production as well as concentration factors for potentially hazardous constituents. The waste residual factors given in Table 12 are estimated average values for all foundries in each of the three major foundry categories. In developing the waste factors, consideration was given to the different types of furnaces used in each metal category and to the different types of furnace emission control systems. For example, gray and ductile iron is made in cupola furnaces and electric induction furnaces in the ratio of about 3 to 2. Control for cupola furnace emissions is devided about equally between wet and dry systems, while electric induction furnaces generally require no emission control.

In generating the overall waste factors, the computation of sludges, and dusts and slag accounted for the percentage of castings within a given category made from a specific type of furnace with a specific type of control by weighing the waste factors for specific combinations according to the frequency of their occurrence.

Table 13 presents the amounts of wastes and the amounts of specific potentially hazardous constituents generated annually for an average plant in each of the three major foundry categories. The amounts shown were calculated using the waste factors given in Table 12 and taking the following average annual production figures for finished castings for each type of foundry: (a) gray and ductile iron foundries - 10,000 metric tons, (b) malleable iron foundries - 12,700 metric tons; and (c) steel foundries - 5,400 metric tons.

The quantity of waste generated by ferroalloy plants on a state-by-state basis are given in Table 14 for 1974, 1977, and 1983. The quantities of sludges and dusts are based directly on information derived from a solid waste survey sponsored by the Ferroalloy Association in which the quantities of wastes from furnace emission control were tabulated for each state for each type of ferroalloy. The sludges result from the collection of furnace emissions using wet scrubbing systems. The dusts represent the furnace

TABLE 12
WASTE GENERATION FACTORS, IRON AND STEEL FOUNDRIES, DRY WEIGHTS

	Generation Factor Kg/MT of			Conce	Concentration Factors (ppm)	Factors	(mdd)		
Type of Waste	Finished Casting	рЭ	Cu	$c_{\mathbf{r}}$	Mn	Ni	Pb	Zn	Pheno1
Gray & Ductile Iron Foundries	6 29	0	23.1		1410		9'9	14.7	i
Sludge	32.8	2.0	146	47.6	826	5.3	134	423	1
Dust	65.6	>0.7	79.9		1075		75.5	144.5	!
Sand	009	1	8.5	_	52.9		53.6	0.9	1.1
Refractories	13.8	1	;	i	!	1	i I	1	†
Malleable Iron Foundries									
Slag	55,5	1.0	25.4		1730	10.0	7.4	17.0	!
Sludge	31.9	2.0	146	48.0	749		133	393	!
Dust	64.7	>0.7	79.3		1041		74.3	126	
Sand	009	1	8.3		52.9		53.6	0.9	1.1
Refractories	13.2	1	ŀ	!	!	1	!	i I	1
Steel Foundries									
Slag	122		52	150	5200	1	16	42	
Sludge	36.4	2.3	150	20	375	1	130	250	!
Dust	186		224	105	2806	<b>&gt; 85</b>	187	158	
Sand	780	1		4.8	52.9	28.1	53.6	0.9	
Refractories	53.0	1	!	:	l I	1	-	:	
			1						

TABLL : 3

HTS		Phenoi	0.0066		0.0046
DRY WEIGHTS	ıts	Zn	0.0092 0.1390 0.0948 0.0360	0.0120 0.1590 0.1040 0.0457	0.0277 0.0493 0.159 0.0253
FOUNDRIES,	Constituents	Pb	0.0042 0.0440 0.0495 0.3220	0.0052 0.0539 0.0611 0.4080	0.0105 0.0256 0.188 0.2260
STEEL FOL		Ni	0.0063 0.0017 >0.0180 0.1690	0.0070 0.0018 >0.0230 0.2140	>0.085 0.1180
IRON AND	Potentially Hazardous (MT)	Mn	0.8870 0.2710 0.7050 0.3170	1.218 0.3030 0.8560 0.4030	3.427 0.0739 2.817 0.2230
TYPICAL 1	Potenti (M	Cr.	0.0230 0.0156 0.0396 0.0288	0.0325 0.0194 0.0499 0.0366	0.0989 0.0099 0.1050 0.0202
- BY	Quantity of	Cn	0.0145 0.0479 0.0524 0.0498	0.0179 0.0591 0.6520 0.0632	0.0343 0.0296 0.2250 0.0350
RESIDUALS	ζη	Cd	0.0006 0.0007 >0.0005	0.0007 0.0008 0.0006	0.0007 0.0005 >0.0014
IN OF WASTE	Total Waste Ouantity	(MT)	629 328 656 6000 138	704 405 822 7620 168	659 197 1004 4212 286
YEARLY GENERATION	Type of Waste		Gray & Ductile Iron Foundries  Slag Sludge Dust Sand Refractories a)Based on production of 10,000 MT/yr of finished castings, multiply by 1.1 to convert to short tons	Malleable Iron Foundries  Slag Sludge Dust Sand Refractories b)Based on production of 12,700 MT/yr of finished castings, witiply by 1.1 to convert to short tuns	Steel Foundries <sup>c)</sup> Slag Sludge Sludge Dust Sand Refractories c)Based on production of 5400 MT/yr of finished castings, multiply by 1.1 to convert to short tons

Table 14a
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM IRON AND STEEL FOUNDRIES
TOTAL SLAG, 1974 (METRIC TONS)

STATE	TOTAL DISPOSED	TOTAL POTENTIALLY	TOTAL HAZARDOUS	DISPOSAL METHOD			CONSTI	TUENTS			
	DISPOSED	HAZARDOUS	CONSTITUENTS	METHOD	Cd	Cu	Cr	Mn	Ni	Рь	Z
ALABAMA	122,400	o o	o	LANDFILL	0 122	3 16	5 80	217.7	1 22	0.92	2.
ARIZONA	7,800	1		OR OPEN DUMP	0 006	041	117	40 7	0.08	0.13	0.:
CALIFORNIA	37,500	1 1			0 038	1.10	2 30	84 0	0.38	0.33	0.
COLORADO	7,800	1 1			0 008	0.2	0 37	13 7	0.08	0.06	O.
CONNECTICUT	3,040	1 1		1 1	0 003	0 07	0.12	45	0 03	0.02	0
DELAWARE	860			1 1	0.001	0.04	0 13	44	0.01	0.01	0.
FLORIDA	2,110	1 1			0 002	0.09	0 24	8.5	0.02	0.03	0.
GEORGIA	1,630	<b>\</b>	1	1	0.002	0.06	0.16	5.5	0.02	0.02	0.
ILLINOIS	136,500	1 1			0 137	4 09	8.67	316 1	1.37	1.20	2.
INDIANA	81,000				0.061	2.16	4 09	152 2	0.81	0.63	1.
AWOI	29,900	1	1	1 1	0 029	0.78	1 46	54.5	0.29	0.23	0.
KANSAS	8,860				0 009	0.44	1.24	43 1	0.09	0.13	0.
KENTUCKY	20,680				0 020	048	0.76	29.2	0.20	0.14	0.
LOUISIANA	2,360	\ \			0 002	0 10	0.28	9.8	0.02	0.03	ه ا
MARYLAND	6,010				0 006	0 16	0 32	11.7	0.06	0.06	0.
MASSACHUSETTS	4,370	<b>,</b> ,	1	( )	0 004	0.10	0.16	6.2	0.04	0.03	0.
MICHIGAN	218,200	1			0 218	5 32	9.15	347.3	2.18	1.54	3
MINNESOTA	15,600				0 016	044	090	32 9	0.16	0.13	0.
MISSOURI	11,240	} }			0.011	0 45	1 17	413	0.11	0.14	0.
NEBRASKA	2,600	1 1	1	1	0.003	0 11	030	10.6	0.03	0.14	0
	, , , , ,	1 1			l .	061					0.
NEW JERSEY	25,500	1 1		] .]	0.026	1	1 03	39 3	0.26	0 18	
NEW YORK	69,300			1	0 070	1 88	3 65	135 2	0.70	0.55	1.
N CAROLINA	7,600	[	1 1	[ ]	0 008	0 18 6 13	0.28	10 7	0.08	0.05	· ·
OHIO	211,400	1 1		! !		1	12.66	463 7	2 11	1.81	4.
OKLAHOMA	3,920	t i			0 004	0 13	0.31	11.1	0.04	0.04	0.
OREGON	5 110	1 1		1	0 006	0.25	0.60	23 9	0 05	0.08	0
PLNNSYLVANIA	175,900			1 1	0.176	493	1 87	36.1 /	1 76	1 46	3
HHODE EL MOHH	2.230	( (		, l	0 002	0.37	361	3.7	1.02	001	0
S CAROLINA	1,800	]	1 1	1	0 002	0.04	0.07	26	0 02	0 01	0
S DAKOTA	370				~ 0	0.02	0.05	19	~0	~0	0.
TENNESSEE	31,880	1 (		{	0 032	0.88	1 177	64.0	0 32	0 26	0
TEXAS	42,800			1 1	0 043	1 16	2 27	82.8	0 43	0 34	0
UTAH	15,200	1 1			0 015	0.39	0.70	26 1	0.15	0.11	0.
VERMONT	770		1 1	{	0 001	0.02	0 03	11	0.01	0.01	0.
VIRGINIA	12,270			] ] .	0 012	0.30	0 53	20 1	0.12	0.09	0.
WASHINGTON	4,200				0 004	0 20	0 55	19 3	0.04	0.06	0.
W VIRGINIA	6,750	1	1 1	1 1	0.007	0.20	040	14 /	0.07	0.06	0
WISCONSIN	52,800	<del>  </del>		V	0.053	1 73	3 95	142 2	0.63	0.52	1.
EPA REGION											ļ
I	10,410	1 1	1	)	0.010	0 24	0 39	15 0	0.10	0.07	0
п	94,800			j	0.096	2.49	4.68	174.5	0.96	0.73	1.
m	201,790	] ]	1	)	0 202	5.83	11 25	414.6	2.02	1.66	3.
IY	188,100	1	1	1	0.188	4.89	9 04	338 1	1.86	1 43	3.
¥	715,500	1 1	[ [	ļ i	0.716	19.87	39.42	1,454.4	7 16	5.83	13.
M	49,080	1 1			0 049	1 39	2 82	103 7	0.49	0.41	0.
AII.	62,590	<b>!</b>	1	j	0 062	1 /8	4 17	149 6	0.52	0.53	,
VIII	23,370	{	1	<u> </u>	0.057	0.61	1 12	41 2	0.23	0.17	٥
IX.	45,300			i .	0 046	151	147	124 /	0 46	0.46	1
x	9,310				U 009	0.46	1 24	43.2	0.09	0 14	0
		+ <del>-</del>	44	•		•	•		***************************************	·	20

<sup>\*</sup>FOUNDRY SLAG NOT CONSIDERED HAZARDOUS ON BASIS OF CALSPAN SOLUBILITY YESTS DESCRIBED IN APPENDIX B.

Table 14b
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES
TOTAL SLAG, 1977 (METRIC TONS)

		TOTA:	70741	Dienoe .	<del></del>	T -	<del></del>	CONSTITUEN		1	T 3.
STATE	DISPOSED	POTENTIALLY HAZARDOUS*	TOTAL HAZARDOUS CONSTITUENTS	METHOD	Cd	Cu	Cr	Mn	Ni	Pb	Z,
ALABAMA	135,374	0	ę.	LANDFILL	0.135	3.49	6.41	240.8	1.36	1.02	2
ARI <b>ZON</b> A	8,627	ì i	]	OR OPEN DUMP	0.009	0.45	1.29	45.0	0.00	0.14	0
CALIFORNIA	41,475	1		1	0.042	1.2	2.54	92.9	0.42	0.36	0
COLORADO	8,627	[ [			0.008	0.2	0.41	15.2	0.09	0.07	a
CONNECTICUT	3,362				0 003	0.08	0 13	5.0	0 03	0 02	0
DELAWARE	961	] ]			0.001	0.04	0.14	4.9	0.01	0.01	0
LORIDA	2,334	1		1	0.002	0.10	0.26	9.4	0.02	0.03	1 0
AIDRO ID	1,803	} }	1	} }	0 002	0.07	0 18	6.1	0.02	0.02	0
IL LINOIS	150,969	[ [			0 152	4.52	9.59	349.6	1.52	1.33	1
INDIANA	89,586	]			0.090	2 39	4.52	168.3	0.90	0.70	1
IOWA	33,069				0 032	0.86	1.61	60 3	0.32	0.25	0
KANSAS	9,788				0.010	0.49	1.37	47.7	0 10	0.14	0
KENTUCKY	22,872	[ [			0 022	0.53	0.84	32.3	0.22	0.15	0
LOUISIANA	2,610				0.002	0 11	0.31	10.8	0.02	0.03	0
MARYLAND	6,647				0.007	0.18	0.35	12.9	0.07	0.06	0
MASSACHUSETTS	4,833	}		}	0 004	0 11	0.18	6.8	0.04	0.03	0
MICHIGAN	241,329				0 241	5.88	10.12	384.1	2.41	1.70	3
MINNESOTA	17,254		1		0.018	0.49	1 00	36.4	0.18	0.14	0
MISSOURI	12,431	}		}	0.012	0 50	1.29	45 7	0 12	0 15	0
NEBRASKA	2,876				0.003	0.12	0.33	11.7	0.03	0.03	1
NEW JERSEY	28,203	<b>l</b> .			0.029	0 67	1.14	43 5	0.29	0.20	
NEW YORK	76,646	<b>!</b>			0.077	2.08	4.04	149.5	0.77	0 61	1
N CAROLINA	8,406	1			0.009	0 20	0.31	118	0 09	0.06	0
оніо	233,808				0 233	6.79	14 00	512.8	2 33	2.00	) 4
OKLAHOMA	4,336		(		0 004	0.14	0.34	12.3	0.04	0.04	0
DREGON	5,652				0.006	0 28	0.76	26.4	0.06	0.09	0
PENNSYLVANIA	194,545		)		0.195	5 45	10 92	402 2	1 95	1.60	3
HODE ISLAND	2,466				0 002	0.06	0.09	3.5	0 02	0.01	1 0
CAROLINA	1,991				0.002	0.04	0.08	2.8	0 02	0.01	0
S. DAKOTA	409				~0	0.02	0.06	21	~0	~0	
renne <b>s</b> see	35,259	] ]	]		0.036	0.97	1.91	70 8	0.36	0.29	1 0
TEXAS	47,337	1			0.048	1.28	2.47	91.6	0 48	0.38	0
JTAH	16,811				0.017	0.43	0.77	28.9	0.16	0.12	0
/ERMONT	852				0.001	0.02	0 03	1.2	0.01	0.01	0
VIRGINIA	13,571				0,013	0.33	0.59	22.2	0.13	0.10	) 0
VASHINGTON	4,645		<b>1</b> 1		0.004	0.22	0.61	21.3	0.04	0.07	0
V. VIRGINIA	7,466	[ [	1		0.008	0.22	0.44	16.2	0.08	0.07	0
VISCONSIN	58,397				0.059	1.91	4.37	157.3	0.59	0.58	1
PA REGION						<b> </b>	<b>†</b>		<del> </del>	<del>                                     </del>	$\top$
1	11,513	1 1	1		0.011	0.26	0.43	16.6	0.11	0.08	
п	104,849		<b>f</b> i		0.106	2.75	5.18	193.0	1.06	0.81	1
m	223,180				0.223	6.23	12 44	458.5	2 23	1.84	
177	208,039		]		0.208	5.41	10.00	373.9	2.08	1.58	3
V	791,343		[ ]		0.792	21.98	43 60	1,606 6	7.92	6.45	15
VI.	54,282	1 1	}		0.054	1.54	3 12	114 7	0.54	0.45	1
All	58,165	, , ,	ļ ļ		0.068	197	4 61	165.3	0.58	0.59	;
VIII	25,847		[	l	0.025	0 67	1 24	46 1	0.25	0.39	0
IX.	50,102				0.051	167	3.84	137,9	0.51	0.51	;
*	10,297	} }	1 1	ì	0.010	050	1.37	47.8	0.51	0.15	,
					3.010	0.50	1.37	77.5	3 70	0.15	ļ .

"FOUNDRY SLAG NOT CONSIDERED HAZARDOUS ON HASIS OF CALSPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX 8

Table 14c

# ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES TOTAL SLAG, 1983 (METRIC TONS)

CTATE	TOTAL	TOTAL	TOTAL	DISPOSAL			cc	NSTITUEN	TS		
STATE	DISPOSED	POTENTIALLY HAZARDOUS*	HAZARDOUS CONSTITUENTS	METHOD	Cd	Cu	Cr	Mn	Ni	Pb	Zn
ALABAMA	166,800	0	0	LANDFILL	0.166	4.31	7.90	296.7	1.66	1.25	2.8
ARIZONA	10,600	1 1		OR OPEN DUMP	0 011	0.56	1.59	55.5	0.11	0.18	0.4
CALIFORNIA	61,100			1	0.062	1.50	3.13	114.5	0.52	0.45	1.0
COLORADO	10,600		1	1 1	0.011	0.30	0.60	18.7	0.11	0.08	0.
CONNECTICUT	4,140				0.004	0.10	0.18	61	0.04	0.03	0.0
DELAWARE	1,170				0.001	0.06	0.18	6.0	0.01	0.01	0.0
FLORIDA	2,880	( )			0.003	0.12	0.33	11.6	0.03	0.04	0.
GEORGIA	2,220				0.003	0.08	0.22	7.5	0.03	0.03	0.6
ILLINOIS	186,100	1		1	0.187	5.57	11.82	430.8	1.87	1.64	3.
INDIANA	110,400		l i	1	0.110	2.94	5.57	207.4	1.10	0.86	1.1
IOWA	40,800			]	0.040	1.06	1.99	74.3	0.40	0.31	0.3
KANSAS	12,100				0.012	0.60	1.69	58.7	0.12	0.18	0.4
KENTUCKY	28,190				0.027	0.66	1.04	39.8	0.27	0.19	0.4
LOUISIANA	3,220	1		\ \ \	0.003	0.14	0.38	13.4	0.03	0.04	0.
MARYLAND	8,190				0.008	0.22	0.44	15.9	0.08	0.07	0.
MASSACHUSETTS	5,960				0.006	0.14	0.22	8.4	0.06	0.04	0.0
MICHIGAN	297,400			1 1	0.297	7.25	12.47	473.4	2.97	2.10	4.
MINNESOTA	21,300	1 1		<b> </b>	0.022	0.60	1 23	44.8	0.22	0.18	0.
MISSOURI	15,320				0.015	0.61	159	56.3	0.15	0.19	0.
NEBRASKA	3,540				0.004	0.15	041	14 4	0.04	0.04	0.
NEW JERSEY	34,800	] ]		1 1	0.038	0.83	140	53.6	0.36	0.24	0.1
NEW YORK	94,500				0.095	2 56	4.97	184.3	0.95	0.75	1.3
N CAROLINA	10,400	1	i }	1	0.011	0.24	0.38	14.6	0.11	0.07	0.
ОНЮ	288,100	<b>,</b> (	<b>.</b>	<b> </b>	0.288	8.36	17.26	632.0	2.88	2.47	6.
OKLAHOMA	5,340				0.006	0.18	0.42	15.1	0.06	0.06	0.
OREGON	6,970				0.007	0.34	0.94	32.6	0.07	0.11	0.3
PENNSYLVANIA	239,800	l (	l	ll	0.240	6.72	13.45	496.7	2.40	1.98	4.5
RHODE ISLAND	3,040				0.003	0.07	0.11	4.4	0.03	0.01	0.
S. CAROLINA	2,450				0.003	0.06	0.10	3.4	0.03	0.01	0.0
S. DAKOTA	504			]	~ 0	0.03	0.07	2.6	~0	~0	0.
TENNESSEE	43,450	) j			0.044	1.20	2.36	87.2	0.44	0.35	0.
TEXAS	58,300	<b>,</b>	1	{	0.059	1.58	3.04	112.8	0.59	0.46	1.
UTAH	20,700				0.020	0 53	0.96	35.6	0.20	0.15	0.
	1,050			<b>\</b>	0.001	0.03	0.04	1.5	0.01	0.01	0.
VERMONT	1				0.016	0.41	0.72	27.4	0.16	0.12	0.
VIRGINIA	16,700	j			0.006	0.27	0.72	26.3	0.06	0.12	0.
WASHINGTON	5,730	1 1 1	l	] ]	0.010	0.27	0.54	20.0	0.10	0.08	0.
W. VIRGINIA WISCONSIN	9,200	] [		1 I	0.072	2.36	5.38	193.8	0.72	0.71	1.
	/2,000	<del>  </del>		ļ- <b></b> -	J.072		- 5.55	100.0	ļ	<del> </del>	<del>  ``</del>
EPA REGION		] ] ]				ļ	1		1	I	1
I	14,190	1 1			0.014	0.33	0.53	20.A	0.14	0.10	0.
П	129,300	1 1		}	0.131	3.39	5.38	237.8	1.31	1.00	2.
m	275,060				0.275	7.67	15.33	566.1	2.75	2.26	5.
TV	256,390				0.256	6.66	12.32	460.8	2.56	1.96	4.
¥	975,300				0 976	27.08	53.73	1,982.3	9.76	7.95	18.
Att.	66,860				0.067	1.89	3.84	141.3	0.67	0.56	0.
MI	71,760				0.071	2.43	5.68	203.8	0.71	0.72	1.
VIII	31,804	] ]	]		0.031	0.83	157	56 8	0 31	0.23	0.
130	61,700				0.063	2 08	4 77	170 0	ra 0	0.63	1.0
×	12,700				0.017	0.61	1 60	na v	0.12	0 19	0.4
-	1	1 1 1		1	ì	1	1	į	ı	Į	ě.

<sup>\*</sup>FOUNDRY SLAG NOT CONSIDERED HAZARDOUS ON BASIS OF CALSPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX B

Table 14d
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM IRON AND STEEL FOUNDRIES
TOTAL SLUDGE, 1974 (METRIC TONS)

STATE	TOTAL DISPOSED	TOTAL POTENTIALLY	TOTAL HAZARDOUS	DISPOSAL METHOD			cor	NSTITUENT	8	<del></del>	,
	DISPUSED	HAZARDOUS"	CONSTITUENTS	METHOD	Cd	Cu	Cr	Mn	Ni	Pb	Zn
ALABAMA	61,250	0	0	OPEN DUMP	0.12	8.94	2.92	48.98	0.30	8.19	25.
ARIZONA	2,350	] ]		AND LANDFILL	0.01	0.35	0.12	0.88	NA	0.30	0.1
CALIFORNIA	17,760	<b>,</b> , ,		1	0.04	2.59	0.86	13.54	0.08	2.36	7.
OLORADO	3,900				0.01	0.57	0.19	3 11	0.02	0.52	1.
GNNECTICUT	1,600				0	0.24	0.08	1.31	0.01	0.22	0.
1HAWA I	260	1 1	1		0	0.04	0.01	0.10	NA	0.03	0.
н сонов	800				0	0.11	0.04	0.44	~0	0.10	0.
ALDHOIA	660	1 1 1	1		0	0.10	0.03	0.43	~0	0.09	0.
ILLINOIS	64,450	1 1			0 13	9.44	3.09	48.61	0.29	8.59	25
INDIANA	40,150				0.08	5.87	1,92	31.76	0.20	5.36	16
AWO	14,900	1 1			0.03	2 18	0.71	11.87	0.07	1.99	6.
N/ NSAS	2,800	1 1	1		0.01	0.42	0.14	1.24	~ 0	0.37	0
KENTUCKY	10,800				0.02	1.57	0.51	8.90	0.06	1,44	4
LOUISIANA	850	[			0	0.13	0.04	0.47	~0	0.11	a
MARYLAND	2,950				0.01	0.43	0.14	2.32	0.01	0.39	1.
MASSACHUSETTS	2,300	] ]			0.01	0.33	0,11	1.88	0.01	0.31	0
MICHIGAN	113,250				0.22	16.52	5.40	91 33	0.57	15.14	47
MINNESOTA	7,550				0.02	1.11	0.36	5.83	0.04	1.01	3
v-S\$OURI	4,350			1	0.01	0.64	0.21	2.70	0.01	0.58	1
VFBRASKA	950			1	~0	0.14	0.06	0.54	~ 0	0.13	0
VEW JERSEY	13,100				0.03	1.91	0.62	10.72	0.07	1.75	5
VEW YORK	33,900	1 1	1 1		0.03	4.97	1.62	26.71	0.16	4.54	13
N CAROLINA	3,960	1 1	1 1	. 1	0.07	0.58	0.20	3.27	0.02	0.63	1
OHIO	101,100				0.20	14.79	4.84	77 36	0.46	13.48	40
OKLAHOMA	1,700		1 1		~ 0	0.26	0.08	1 22	0.40	0.23	0
DREGON	1,700		1 1	]		0.26	0.08	0.80	~ 0	0.23	١
PENNSYLVANIA	85,400			<u> </u>	~0	1	1	1			
	· ·	[ [		[ [	0.17	12.49	4.09	66.23	0.40	11 40	34
RHODE ISLAND	1,200				~0	0.17	0.06	0.96	0.01	0.16	0
CAROLINA	960			] ]	~0	0.14	0.04	0.78	0.01	0.13	0.
DAKOTA	100			[	~0	0.02	0.01	0.04	NA	0.01	0.
I F NNESSEE	16,500				0.03	2.27	0.74	12.13	0.07	2.07	6
I I XAS	21,100			]	0.04	3.06	1.01	16.60	0.10	2.82	8.
JTAH	7,660				0.02	1.12	0.36	6 16	0.04	1.02	3.
VERMONT	400			1	~0	0.06	0.02	0.33	~0	0.06	0.
VIRGINIA	6,200	1 1			0.01	091	0.30	5.05	0.03	0.83	2.
VASHINGTON	1,400	1 1	1 1	} }	~0	0.21	0.07	0.68	~ 0	0.18	0.
VIRGINIA	3,200	ļ			0.01	0.47	0.15	2.48	0 01	0.43	1
VISCONSIN	23,800				0.06	3.49	1.14	17.13	0.10	3.18	9.
PA REGION		1 1	1 1								
ı	5,600	1 1			~0	0.80	0.27	4,48	0.03	0.74	2.
n	47,000	<b>1</b> {	[ [		0 10	6.88	2.24	37.43	0.23	6.29	19.
m	98,000	1 1			0 20	14.34	4.69	76.18	0 45	13.08	39,
1327	93,900	1 1	] ]		0.18	13.71	4.48	74.93	0 46	12.55	38
v i	360,300				0.70	51.22	16.75	272.02	1.86	46.74	141.
<b>72</b> 7	23,660 :	1 1			0.04	3.47	1.13	18.29	0.11	3.16	9.
VIII	23,000	1 1		1	0.06	3.38	1.11	16.36	0.06	3.07	8.
VIII	11,660		1 1		0.03	1.71	0.56	9.31	0.06	1.55	4.
ıx.	20,100		1 1		0.06	2.94	0.97	14.42	0.08	2.66	7.
X.	3,100				~ 0	0.46	0.15	1.48	~ 0	0.40	0.1
IATIONAL TOTALS	676,200	4	. ♦	l l	1.40	96 90	32.40	524.90	3.16	90.2	273.

<sup>\*</sup>FOUNDRY SLUDGE NOT CONSIDERED HAZARDOUS ON BASIS OF CALSPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX B.

Table 14e

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES TOTAL SLUDGE, 1977 (METRIC TONS)

STATE	TOTAL DISPOSED	POTENTIALLY	TOTAL HAZARDOUS	DISPOSAL METHOD			CONS	TITUENTS	) 		
	Distracti	HAZARDOUS*	CONSTITUENTS	MEINOD	Cd	Cu	Cr	Mn	NI	Pto	Zn
ALABAMA	67,740	0	0	OPEN DUMP	0.13	9.89	3.23	54.17	0.33	9.06	27.9
ARIZONA	2,600	]		AND LANDFILL	0.01	0.39	0 13	0.97	NA	0.33	0.6
CALIFORNIA	19,630	} }	1	1	0.04	2.86	0.94	14.98	0.09	2.61	7,8
COLORADO	4,315	l i			0.01	0 63	0 21	3.44	0.02	0.58	1.7
CONNECTICUT	1,770			[ [	~0	0.27	0.09	1,45	0.01	0.24	0.7
DELAWARE	280	]	1		~0	0 04	0.01	0.11	NA	0.03	0.0
FLORIDA	885	1	1		~0	0.12	0.04	0.49	~0	0.11	0.2
GEORGIA	720				~0	0.11	0.03	0.48	~0	0.10	0.2
ILLINOIS	71,280				0.14	10.44	3.42	63.76	0.32	9.50	28,1
INDIANA	44,410				0.09	6.49	2 12	35 13	0.22	5.93	18.1
IOWA	16,480			1	0.03	2.41	0.79	13 13	0.08	2.20	6.7
KANSAS	3,100				0.01	0.46	0.15	1,37	~0	0.41	3.0
KENTUCKY	11,945				0.02	1.74	0.56	9.84	0.07	1.59	5.0
LOUISIANA	940		1	1	~0	0 14	0.04	0.52	~0	0.12	0.3
MARYLAND	3,265				0.01	0.48	0.15	2.57	0.01	0.43	1.3
MASSACHUSETTS	2,545				~ C	0.36	0.12	2.08	0.01	0.34	1.0
MICHIGAN	126,260	1			0.24	18.27	5.97	101.01	0.63	16.74	52.0
MINNESOTA	8,350				0.02	1.23	0.40	6.45	0.04	1.12	3.3
MISSOURI	4,810		l		0.01	0.71	0.23	2.99	0.01	0.64	1.0
NEBRASKA	1,050		i I		~0	0.15	0.06	0.60	^0	0.14	0.3
NEW JERSEY	14,490				0.03	2.11	0.69	11.86	0.06	1.94	6.0
NEW YORK	37,500				0.03	5.50	1.79	29.54	0.18	5.02	15.3
N. CAROLINA	4,370			]	0.01	0.64	0.22	3.62	0.02	0.59	1.6
OHIO	111,820				0.01	16.36	5.36	85.56	0.51	14.91	44.6
OKLAHOMA	1,880				~0	0.28	0.09	1.35	0.01	0.25	0.3
OREGON	1,880				~0	0.28	0.09	0.88	~0	0.25	0.1
PENNSYLVANIA	94,450					13.81		73.25	1	12.81	38.
RHODE ISLAND	1,330			1	0.19	]	4.52 0.07	i	0.44	1	1
S. CAROLINA	1,050				~0	0.19	ļ	1.06 0.86	0.01	0.18	2.0
					~0	0.15	0.04	1	0.01	0.14	0.4
S. DAKOTA	110				~0	0.02	0.01	0.04	NA	0.01	0.0
TENNESSEE	17,140		<b>,</b>		0.03	2.51	0.82	13,42	0.08	2.29	6.9
TEXAS	23,340	İ			0.04	3.42	1 12	18.36	0.11	3.12	9.6
UTAH	8,460				0.02	1.24	0.40	6.81	0.04	1.13	3.0
VERMONT	440				~0	0.07	0.02	0.36	~0	0.06	0.
VIRGINIA	6,860	[			0.01	1.01	0.33	5,59	0.03	0.92	2.5
WASHINGTON	1,550				~0	0.23	0.08	0.75	~0	0.20	0.4
W. VIRGINIA WISCONSIN	3,540 26,326				0.01	0.52 3 86	0.17 1.26	18 95	0.01	0.48 3.49	1.4
EPA REGION	20,320	<del></del>		у	0.00	3.60	1.20	19 90	0.71	348	10.1
			İ		•						l <u>.</u> .
n	6,085		(		~0	0.88	0.30	4.95	0.03	0.82	2.5
- !	59,966				0.11	7.61	2.48	41.40	0.25	0.30	21.4
m	106,396				0.22	15.86	5.19	84.26	0.50	14.47	43.1
TZ	103,850		<b>1</b>		0.20	16.16	4.95	62.87	0.51	13.89	42.1
4	387,445		[ [		0.77	56.65	18.53	300 85	1 84	51.69	156.4
<u>vi</u>	26,160				0.04	3.84	1.25	20.23	0.12	3.49	10.1
M	25,440		1 1		0.06	3,74	1.23	18.08	0.09	3.40	9.0
VIII	12,885	[ ]			0.03	1.89	0.62	10.30	0.07	1.71	5.1
DX .	22,230		[ [		0.06	3.25	1.07	15,95	0.09	2.94	8.4
X	3,430				~0	0.51	0.17	1.64	~0	0.44	1.0
NATIONAL TOTAL	764,875	1	<b>†</b>		1.5	109.4	35.8	580.5	3.5	8,00	301.

<sup>\*</sup>FOUNDRY SLUDGE NOT CONSIDERED HAZARDOUS ON BASIS OF CALSPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX B.

Table 14f
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM IRON AND STEEL FOUNDRIES
TOTAL SLUDGE, 1983 (METRIC TONS)

STATE	TOTAL DISPOSED	TOTAL POTENTIALLY	TOTAL HAZARDOUS	DISPOSAL		<del></del>	CC	MSTITUE	N18		
	Dia Octo	HAZARDOUS*	CONSTITUENTS	ME THOO	Cd	Cu	Cr	Mn	Ni	Pb	Z
ALABAMA	83,480	o	0	OPEN DUMP	0.16	12.19	3.96	66.76	0.41	11.16	34.
ARIZONA	3,200	1		LANDFILL	0.01	0.48	0.16	1.20	NA	0.41	0.
CALIFORNIA	24,190	1 1	1		0.06	3.53	1.16	18.46	0.11	3.22	9
COLORADO	5,320	¦		!	0.01	0.78	0.26	4 24	0.03	0.71	2
CONNECTICUT	2,180				~0	0.33	0.11	1 79	0.01	0.30	0
DELAWARE	340	! !		1	~ 0	0.06	0.01	0.14	NA	0.04	0
FLORIDA	1,000	(	1	1	-0	0.15	0.06	0.60	~0	0.14	10
GEORGIA	890			·	- 0	0 14	0.04	0 59	.0	0.12	0
ILLINOIS	87,850			l	0.18	12.87	4.21	66.26	0.40	11.71	34
INDIANA	64,720	i l		- 1	0.11	8.00	2.62	43.29	0.27	7.31	22
AWO	20,310	1			0.04	2.97	0.97	16.18	0.10	2.71	8
KANSAS	3,820	;	1	;	0.01	0.67	0.19	1.69	~0	0.50	1
KENTUCKY	14,720	1			0.03	2.14	0.70	12.13	0.08	1.96	6.
LOUISIANA	1,160	1	1		~0	0.18	0.06	0.64	~0	0.15	0
MARYLAND	4,020	; 1		i	0.01	0.59	0.19	3.16	0.01	0.53	1.
MASSACHUSETT8	3,135		į Į		~0	0.45	0.15	2.56	0.01	0.42	1
MICHIGAN	154,360		1	.	0.30	22.52	7.36	124 48	0 78	20.64	84
MINNESOTA	10,290	,		1	0.03	1.51	0 49	7 98	0.05	1.38	4
MISSOURI	5,930	! 1	1		0 01	0.87	0.29	3.66	0.01	0.78	2
NEBRASKA	1,295	'	!	1	- 0	0.19	0 07	0.74	- 0	0 18	0
NEW JERSEY	17,860	1	{	ļ <b>1</b>	0.04	2.60	0.85	14 61	0 10	2.39	. 7
NEW YORK	46,210		j		0 10	6 77	2 21	36 41	0 22	8.19	18
N. CAROLINA	5,380	!		! !	0.01	0.79	0 27	4 46	0.03	0.72	1 2
Эніо	137,800				0.27	20 16	6.60	105 44	0.63	18,37	55
JKLAHOMA	2,320			.	. 0	0.34	0.11	1 66	0.01	0.31	0.
JIR GON	2,320	]	] ]	!	. 0	0,34	0.11	1 09	~0	0.30	0.
ENNEY! VANIA	110,400	; <u> </u>			0 2 1	17 02	p b/	90.27	0 55	15.54	48.
HIODE ISLAND	) 640	1	! 1		0	0.21	0.08	1.31	0.01	0 22	0
CAROLINA	1,295	1	1	i j	~0	i 0 19	0.06	1.06	0.01	0.18	0.
DAKOTA	140	, <b>,</b>		; }	~ 0	0.03	0.01	0.06	NA.	0.01	0
TENNESSE E	21,130	1	1		0.04	3.09	1 01	16 53	0.10	2 82	8
TE XAS	28,760		i		0.06	4 21	1 38	22.63	0.14	3.84	11.
JTAH	10,430				0.03	1.53	0.49	8.40	0.06	1.39	4.
VERMONT	546		J		• 0	0.00	0.03	0.45	~0	0.07	0.
/IRGINIA	8,450	i 1			0.01	1.24	0.41	6.88	0.04	1.13	3.
VASHINGTON	1,910				~ 0	0.29	0.10	0.93	~0	0.26	0.
Y. VIRGINIA	4,360				0.01	0.64	0.20	3.38	0.01	0.59	1.
VISCONSIN	32,440				0.07	4.76	1.56	23.35	0.14	4.31	12.
PA REGION			<b></b>	<del>-</del>			-			<del>                                     </del>	+
1	7,500				_						_
n	7,500 64,070			l	·~0	1.09	0.37	6.11	0.04	1.01	3.
m					0 14	9.38	3.05	51.02	0.31	8.57	26.
IZ.	133,570 127,985		]		0.27	19,55	6.30	103.83	0.61	17.83	53.
Δ	477,460			}	0.25	18.69	6.11	102.13	0.63	17.11	52.
VI VI		<b>i</b>			0.95	69.81	22.83	370.76	2.26	63.71	192.
AU A	32,240				0.06	4.73	1.54	24.93	0.15	4.31	12.
i	31,355				0.07	4.61	1.51	22.29	0.11	4.18	11.
VIII	15,890		1 1		0 04	2.33	0 76	12.69	0.08	2.11	6.1
TX.	27,390		1		0.07	4.01	1.32	19.65	0.11	3.63	10.4
×	4,230	.		1	. 0	0.63	0.20	2.02	- 0	0.66	1.
ATIONAL TOTAL	931,660	•	•	}	19	138 8	44.2	715-4	4.3	122 9	372.

<sup>\*</sup>FOUNDRY BLUDGE NOT CONSIDERED HAZARDOUS ON BASIS OF CALEPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX B

Table 14g
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES
TOTAL DUST, 1974 (METRIC TONS)

							cc	METITUENT	8		
STATE	TOTAL DISPOSED	TOTAL POTENTIALLY HAZARDOUS*	TOTAL HAZARDOUS CONSTITUENTS	DISPOSAL METHOD	Cil	Cu	Cı	Mn	Ni	٨	Zr
ALABAMA	133,400	0	ė	OPEN	0.13	13.54	9 03	174.50	4.46	11.84	19.1
ARIZONA	11,960	1 1		LANDFILL	0 02	2 /1	1 28	33 60	1.00	2.22	11
CALIFORNIA	43,300	1 1		1	0.08	6 34	3.22	68 01	1.83	4.87	6.4
COLORADO	8,460				0.01	0.85	0.57	11 02	0.26	0.76	1:
CONNECTICUT	3,250				~0	0.26	0 20	3 46	0.06	0.24	0.
DELAWARE	1,300	1			~0	0.03	0 14	3.67	0.11	0.24	0.
FLORIDA	2,900	] ]			~0	0.56	0 28	7 02	0 20	0.47	0
GEORGIA	2,100	1			~0	0.36	0 20	4 54	0 13	0.30	0
ILLINOIS	158,800	1 1			0 17	20 06	11 97	254 88	6.89	17.14	23.
INDIANA	89,450				0 09	9 50	6 18	121 99	3 16	8 26	13.
AWOI	32,800	1 1			0 03	3.39	2.24	43.68	1.12	2.96	4,
KANSAS	13,150	1 1 .			0 02	2 80	1 36	36.51	1 06	2 35	2.
KENTUCKY	21,550				0.05	1 77	1 33	23 17	0.56	1.59	3
LOUISIANA	3,300				0 01	0.66	0 32	807	0.24	0.54	0.
MARYLAND	6,700		]		0.01	0 74	0.47	ļ	0.25	0.84	0
MASSACHUSETTS	4,550	<b>,</b>	}		Į.	0 37	ļ.	9 45	į.	ļ	0
MICHIGAN	1				~0	(	0.28	4 90 272 76	0.12	0.34	33
MICHIGAN MINNESOTA	234,600				0.22	2101	15 01		6.74	18.65	2
	17,760				0 02	2 08	1 29	26 49	0.70	1.79	1
MISSOURI	15,000				0.02	2 72	1 39	33.93	0.98	2.25	2
NEBRASKA	3,800	1 1	1		0.01	0.70	0.36	874	0 26	0.58	0
NEW JERSEY	27,000				0 03	2 41	1 72	31 31	0.77	2.14	3
NEW YORK	77,100		1		0.06	8.48	5 42	108.73	2.84	7 35	11
N, CAROLINA	7,900	1 1	1		0.01	0.66	0 49	8.52	0.20	0.58	1
оню	242,300		1	' l	0.26	29 34	17.87	373 76	10 00	25.18	36
OKLAHOMA	4,800				0.01	0.72	0.40	9 04	0.25	0.80	0
DREGON	7,500		1		0.01	1.59	0 76	19.69	0.58	1.30	1
PENNSYLVANIA	198,700				0 21	22.88	14.29	292 35	7.73	19,73	29
RHODE ISLAND	2,350		j		~0	0.19	0 15	2 5 2	0.06	0.17	0
S. CAROLINA	1,900				~0	0 15	0 12	202	0.05	0.14	0
DAKOTA	550		(		~0	0.13	0.08	158	0.06	0,10	0
<b>TENNESSEE</b>	35,650				0 04	4 03	2.54	5162	1 36	3.48	5
TEXAS	47,850	<b>i</b> i			0.05	5.17	3 33	66 35	173	4,49	6
HATL	16,450			}	0 02	1 62	1 10	20 91	0.53	1,42	2
VERMONT	800	1 1 1			~0	0.07	0 06	0.86	0.02	0.06	0
/IRGINIA	13,150		1	l	0 01	1.24	0.09	16 07	0.40	1.09	ļ,
VASHINGTON	6,100	) )			0 01	1 28	0 62	15 95	0.47	1.06	ď
N. VIRGINIA	7,700				0 0 1	0 93	0 57	1183	0 32	0.80	1
VISCONSIN	64,000		}	•	0 07	9 13	5 15	115 30	3 20	7,72	
EPA REGION	-						1			<u> </u>	<del> </del>
											1
1	10,060		1 1		. 0	0 89	0.68	1173	0.70	0.#1	1
11	104,100		1		0 11	10 89	7 14	140 04	3.61	9.49	16
III	227,650				0 24	26 62	16 56	333.37	8 81	22,50	33
IV.	206,400		1 1		0.50	21.06	13 99	271 38	6.95	18,40	30
¥	806,800				0.83	91 12	87.47	1185.16	30.89	78.74	118
虹	56,750		ļ		0.07	6 54	4 06	83.46	2 22	5.63	8
AIL	64,550		] ]		0.06	9.67	5 34	121 84	3 40	8.14	9
<b>VIII</b>	25,450		ļ		0.03	2 60	1 73	33 51	0.86	2.27	3
IX.	55, <b>250</b>				0.07	8 05	4 50	101 61	2 83	6 79	8
x	13,600				0.02	2 87	1.38	35 64	1 06	2.36	2
NATIONAL TOTAL	1,589,400		•		17	179 5	111,8	2297 8	60 7	168.1	230

<sup>\*</sup>IRON AND STEEL FOUNDRY DUSTS NOT CONSIDERED HAZARDOUS BASED ON SOLUBILITY TESTS BY CALSPAN AND DESCRIBED IN APPENDIX B SOURCE. CALSPAN CORPORATION

Table 14h
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM IRON AND STEEL FOUNDRIES
TOTAL DUST, 1977 (METRIC TONS)

STATE	TOTAL	TOTAL	TOTAL	DISPOSAL			<del></del>	MSTITUEN	<del></del>	T	
	DISPOSED	POTENTIALLY HAZARDOUS	HAZARDOUS CONSTITUENTS*	METHOD	Cd	ο.	٥	Mn	Ni	76	Zı
ALABAMA	147,500	o	0	LANDFILL	0.14	14.98	9.90	193.00	4.93	13.10	21.0
ARIZONA	13,200	] ]	1	OR OPEN DUMP	0.02	3.00	1.42	37.16	1.11	2.46	2.
CALIFORNIA	47,900	1		1	0.06	5 91	3.56	75.22	2.02	5.06	7.
COLORADO	9,360		i i	•	0.01	0.94	0.63	12.19	0.31	0.83	1.
CONNECTICUT	3,600			l	~0	0.29	0.22	3.82	0.00	0.27	0.
DELAWARE	1,450				~0	0.03	0.15	4.06	0.12	0.27	a
FLORIDA	3,200		j		~0	0 62	0 31	7 76	0.22	0.52	0.
GEORGIA	2,300	1 1	ì	1	~0	0.40	0.22	5 02	0 14	0.33	0
ILLINGIS	175,600		[ .	l	0 19	22 19	13.24	281 88	7.62	18.96	26.
INDIANA	98,950			· (	0 10	10.50	6.84	134.92	3.50	9.14	14.
IOWA	36,300				0.03	3 76	2.48	48.29	1.24	3.27	5
KANSAS	14,650	!!!			0 02	3 16	1.50	39 27	1 16	2.60	2
KENTUCKY	21850			l	0.02	196	1.47	26 55	0.61	1.76	3.
LOUISIANA	3,660	1 1			0.01	0 72	0.35	8 93	0.27	0.60	0
MAHYLAND	7,400		1 1		0 01	0 82	0 52	10 46	0.29	071	1.
MASSACHUSETTS	5,000	)	) )	1	~0	041	0.31	5.42	0 13	0.38	0
MICHIGAN	259,360				0 24	23 24	16.60	301.87	7.45	20.63	37.
MINNESOTA	19,650	1 1	]		0.02	2 30	1.43	29.30	0.77	1.98	2.
MISSOURI	16,600	1 1	i i	\ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \	0.02	3.00	1.54	37.53	1.06	2.49	2
NEBRASKA	4,000	1 1 1	1 1	(	0.01	9.77	0.340	9.67	0.28	0.64	0
NEW JERSEY	29,900	1		İ	0 03	2 67	1.90	34 63	0.85	2.37	4
NEW YORK	86,300	1 1	} }	} ;	0.09	9.38	5.99	120 26	3.14	8.13	12
N CAROLINA	8,750				0.01	0.72	0.54	9.42	0.22	0.64	1
оню	268,000	1 1 1	1 1	1	0.28	32.45	19.76	413.38	11.06	27.86	39
OKLAHOMA	6,300	1 1 1	1	- (	0.20	0.80	0.44	10.00	0.28	0.66	0
OREGON	8.300				0.01	1.75	0.84	21.78	0.84	1,44	1.
PENNSYLVANIA	219,800	) ) )	) 1	1	0.23	25 31	15.90	323.34	8.56	21.82	32
RHODE ISLAND	2,600	1 1 1	1 1		V.23		0.17	2.79	0.07		0
S CAROLINA	2,100				~0	0.21	0.17	2 23		0.19	0.
S. DAKOTA	600	1 1 1	1 1	1		1	}	1 75	0.06	0.15	0
TENNESSEE	39,400				~0	0.14	0.07	57.09	0.06	0 11	1
TEXAS	52,700			J	0.04	4.48	2.81	73.38	1.50	3.85	5
UTAH	18,200	{	1		0 06	6 72	3.68	23.13	1.91	4,97	7.
VERMONT	900		] ]		0 02	179	1 22	0.96	0.50	1.57	2. 0.
VIRGINIA	14,550		1 1	}	~0	0.08	0.06		0.02	0.07	ı
WASHINGTON	8,750		, ,		0.01	1.37	0.10 0. <del>89</del>	17.77 17.64	0.44	1,21	0.
W VIRGINIA	8,500				0.01	1.03	0.63	13.08	0.52	0.88	1.
WISCONSIN	/0,800	}	) }	- • 1	0.01	10.10	5.70	127.52	3.54	8.54	10.
FPA REGION	. 5,256	1 + 1	+	<b>'</b> (		10.13		127,02	3.07	0.04	10.
1	17 100		1	Ì	-0	0.98	0.75	12 98	0.31	0.90	1.
n n	116 160		[ ]	ļ	0.12	12 04	7.90	154 89	3.99	10.80	16.
m	261,700				0.27	20 58	17.21	368,70	9.74	24,89	36.
TX	227,200		} }		0.22	23.29	15,47	300,07	7.00	20.36	33.
<u> </u>	892,300				0.92	100.78	63.56	1288.67	23.94	87.00	130.
<u>v</u>	61,660		] ]		9.08	7.23	4.48	92,31	2.48	6.23	9.
VII	71,400		1 1	}	0.09	10.70	5.91	134,78	3.76	9.00	10.
AIII	28,150				0.03	2.88	1.91	37.07	0.95	2.51	4.
IX.	61,100		1 1		0.08	8.90	4.96	112.38	3.13	7.51	9.
1	15,000	1 1			0.02	3.17	1.53	39.42	1.16	2.61	2.
NATIONAL TOTAL	1,736,750				1.8	196.5	123.7	2641 3	67.1	171.5	254.

\*IRON AND STEEL FOUNDRY DUSTS NOT CONSIDERED HAZARDOUS BASED ON SOLUBILITY TESTS BY CALSPAN AND DESCRIBED IN APPENDIX B SOURCE. CALSPAN CORPORATION

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES TOTAL DUST, 1983 (METRIC TONS)

						y	[	NSTITUEN	T		
\$TATE	TOTAL DISPOSED	TOTAL POTENTIALLY HAZARDOUS*	TOTAL HAZARDOUS CONSTITUENTS*	DISPOSAL METHOD	Cd	Cu	Cr	Mn	Ni	Pb	Zn
ALABAMA	181,800	0	o o	LANDFILL	0 18	18 46	12 31	237 84	6.08	16 14	26 6
ARIZONA	16,300			OR OPEN DUMP	0 03	3 69	1.74	45 80	1 36	3.03	2 5
CALIFORNIA	59,000	1 1		t	0 07	7 28	4 39	92 70	2.49	6 23	87
COLORADO	11,500				0 01	1 16	0.78	15 02	0 38	1 02	1.6
CONNECTION	4.400	1 1			\ O	0.36	0.27	4 10	0 11	0 33	0.6
DELAWARE .	1,800				. 0	0.04	0 19	5 00	0 15	0 3.3	0 2
Adillori	1,460	}	} }		. 0	0.76	o te	9 67	0 27	0 64	0.6
OF OPERIOR	2 HPO			İ	0	0.49	0.27	6 19	0 18	041	0.4
HEINOIS	218,500				0.23	27 14	18.32	147 37	9 39	23 36	32 (
INDIANA	121,900	[ [			0 12	12 95	8 42	166 27	4 31	11 26	17 6
IOWA	44,700				0.04	4 62	3 05	59 51	1 53	4 03	6.5
KANSAS	17,900				0 03	3 90	185	48 40	143	3 20	2 8
KENTUCKY	29,400				0 03	2 4 1	181	31 58	0 75	2 17	4 2
LOUISIANA	4,500				0.01	0.89	0.44	11 00	0 33	0 74	07
MARYLAND	9,100		]		001	1 01	0.64	12 88	0 34	087	1:
MASSACHUSETTS	6,200				~0	0.50	0 38	6 68	0 16	0 46	0 9
MICHIGAN	319,600				0.30	28 64	20 46	371 77	9 19	26 42	45 (
MINNESOTA	24,200				0 03	2 84	1 78	38 11	0 95	2 44	3 !
MISSOURI	20,450				0 03	3 71	1 89	46 25	1 34	3 07	3
NEBRASKA	4,900				0 01	0 95	0 48	1191	0.34	0 79	0.1
NEW JERSEY	36,800		'		0.04	3 28	2 34	42 68	1 05	2 92	5
NEW YORK	105,100			ì	011	11 56	7 39	148 20	3.87	10 02	15.
N CAROLINA	10,800				0.01	0.89	0 67	11 61	0 27	0.79	1
оню	330,250		:		0 35	39 99	24 36	509 43	13 63	34.32	48
OKLAHOMA	6,560	1 1	1 1	Ī	0.01	0 98	0 55	12 32	0.34	0.82	0.9
OREGON	10,200	1 1		1	0 01	2 17	104	26 84	0.79	1.77	1.5
PENNSYLVANIA	270,800	1 1			0 29	31 19	19.48	398 47	10 54	26.89	39.
RHODE ISLAND	3,200				~0	0 26	0.20	3 43	0.08	0.23	0.
S CAROLINA	2,600	!	1 1		~0	0 20	0 16	2 75	0 07	0.19	0:
S DAKOTA	750				~ 0	0 18	0.08	2 15	0 07	0 14	0
TENNESSEE	48,600		1 1	1	0 04	5 49	3 46	70 36	1 85	4 74	7
TEXAS	64,950				0 07	7 05	4 54	90 44	2 36	6 12	9.1
HATU	22,400	, , ,	, ,		0.03	2 21	1 50	28 50	0 72	194	3 :
VERMONT	1,090		1 1		~ 0	0 10	0 07	1 17	0 03	0.08	0
VIRGINIA	17,900			1	0.01	1 69	0 12	21 90	0 55	1 49	2
WASHINGTON	8,300				0 01	1 74	0.85	21 74	0 64	1 44	1.
W VIRGINIA	10,500		{		0 01	1 27	0.78	16 12	0 44	1 09	11
WISCONSIN	87,250		[ [		0 10	12 44	7 02	167 15	4 36	10.52	130
EPA REGION						† <del>-</del>		t	<del> </del>	<del> </del>	
t	14,900				~ 0		0.02	15 98			
- 1			1 1		_	121	0.93	1	0.38	1 10	2.1
П	141,900				0 15	1	9.73	190 88	4.92	12.93	20
ш	310,150				0 33	35 19	21 21	454 37	12.01	30.67	45.5
A IA	279,950				0.27	28 70	19 07	369 90	9.47	25.08	41 (
- 1	1,099,860				1 13	124 20	78 33	1588 10	41.83	107 32	160.8
ΔI	76,000		] ]		0 10	8 91	5 52	113 76	3.03	7 67	11.
प्रा	88,000				0 11	13 18	7 28	166 07	4 63	11 09	13.
Am	34,700	]	}		0.04	3 54	2 36	46 67	1.17	3.09	6 (
nx .	76,300				0 10	10 97	613	138 50	3.86	9.25	113
X	18,650				0 03	3.91	1.88	48 58	1,43	3.22	2.1
NATIONAL TOTAL	2,139,100	• •	• 1		23	244.7	162 4	3131 8	82.7	211.4	313.7

<sup>\*</sup>IRON AND STEEL FOUNDRY DUSTS NOT CONSIDERED HAZARDOUS BASED ON SOLUBILITY TESTS BY CALSPAN AND DESCRIBED IN APPENDIX B

# Table 14j ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDARIES TOTAL SAND, 1974 (METRIC TONS)

CTATE	TOTAL	TOTAL	TOTAL	DISPOSAL	T		co	NSTITUEN	rs		
STATE	DISPOSED	POTENTIALLY HAZARDOUS*	HAZARDOUS CONSTITUENTS	METHOD	Си	Cr	Mn	Ni	Pb	Zn	PHENOL
ALABAMA	1,131,900	0	0	ALL OPEN	9 38	5 39	59 90	31.75	60.63	6.73	1.21
ARIZONA	50,200	1 1	1	DUMP OR	9.42	0.24	2.66	1.41	2.69	0.30	0.05
CALIFORNIA	332,000	1 1	i i	LANDFILL	2 75	1.58	17.57	9.31	17.78	1.97	0.35
COLORADO	71,600			1	0 59	0 34	3.79	2.01	3.84	0.43	0.08
CONNECTICUT	29,700				0 25	0.14	157	0.83	1.59	0.18	0 03
DELAWARE	5,500				0 05	0 03	0.29	0 15	0.29	0.03	0.01
FLORIDA	15,500				0 13	0 07	0.82	0.44	0.83	0.09	0.02
GEORGIA	12,900	1 1			0.11	0.06	0.58	0.36	0.69	0.08	0.01
ILLINOIS	1,211,400	1 1		l i	10 04	5 77	64.10	33.98	64.89	7.20	1.30
INDIANA	744,500				6.17	3 54	39 40	20.88	39.88	4.42	0.80
IOWA	276,000				2 23	1 31	14 81	7.74	14 79	1.64	0.30
KANSAS	59,200	]			0.49	0.28	3.13	1.66	3.17	0.36	0.06
KENTUCKY	197,100	} }			1.63	0.94	10.43	5 53	10.56	1.17	0.21
LOUISIANA	17,100		1		0.14	80.0	0.91	0.48	0.92	0.10	0.02
MARYLAND	54,600	j j i		j	0 45	0 26	2.89	1.53	2.93	0.32	0.06
MASSACHUSETTS	41,800		[ [		0.35	0.20	2.21	1.17	2.24	0.25	0.04
MICHIGAN	2,086,900				17.29	9 93	110.40	58.54	111.80	12.40	2.24
MINNESOTA	141,100	j			1.17	0 67	7 47	3 96	7.56	0.84	0.15
MISSOURI	<b>#86,100</b>			[	0.71	0.41	4.56	2.42	4.81	0.51	0.09
NEBRASKA	19,100				0 16	0.09	1.01	0.54	1.03	0.11	0.02
NEW JERSEY	240,700		<b>j</b> j		199	1.15	12.74	6.75	12.89	1.43	0.26
NEW YORK	631,200		1	1	5.23	300	33 40	17 70	33.81	3.75	0.67
N. CAROLINA	72,500		1 1		0 60	0.35	3.84	2.03	3.88	0.43	0.08
OHIO	1,892,000				15 68	9 00	100 10	53.07	101 30	11 24	2.02
OKLAHOMA	32,700		1 1		0.27	0 16	1.73	0.92	1.75	0.19	0.04
OREGON	35,000		1 1	ı	0.29	0 17	1.85	0.98	1 88	0.21	0.04
PENNSYLVANIA	1,592,700	] ]	<b>j</b> j	1	13.20	7.58	84 28	44.68	85.32	9 47	1.70
RHODE ISLAND	21,600		i l		0.18	0 10	1.14	0 61	1.16	0 13	0.02
S CAROLINA	17,200			1	0 14	0.08	091	0.48	0.92	0.10	0.02
S. DAKOTA	2,400	] ]		i	0.02	0.01	0 12	0.07	0.13	0 01	0
TENNESSEE	288,200			1	2 39	1.37	15.25	8.09	15.44	1.71	0.31
TEXAS	392,400			1	3.25	1.87	20.77	10 01	21.02	2.33	0.42
UTAH	141,100		j j		1 17	0.67	7.47	3 96	7.56	0.84	0.15
VERMONT	7,400				0.06	0.04	0.39	0.21	0.40	0.04	0.01
VIRGINIA	114,600	1	ļ ļ		0.95	0.56	6.07	3.22	8.14	0.68	0.12
WASHINGTON	28,900	1 1	J J	}	0.24	0.14	1.53	0.81	1.55	0.17	0.03
W. VIRGINIA	60,300	<u> </u>	] ]	1	0 50	0.29	3.19	1.69	3.23	0.36	0.06
WISCONSIN	452,300			<b>↓</b>	3 75	2.15	23.94	12.69	24.23	2.89	0.48
EPA REGION	<del>   </del>					t					
1	100,500				0.84	0 48	5.31	2.82	5,39	0.60	0.10
п	871,900	1 1			7.22	4.15	46.14	24.45	46.70	5.18	0.93
ш	1,827,700	1 1			15.15	8.71	96.72	51.27	97.91	10.86	1.95
IV.	1,725,300				14.38	8.26	91.83	48.68	92.95	10.31	1.86
<b>T</b>	6,528,200	1 1			54.10	31.06	354.41	183.12	349.66	38.79	8.99
<b>V</b> I	442,200		1 1		3.66	2.11	23.31	11,41	23.69		0.00
707	440,400				3.66	2.11	23.31	12.36	23.60	2.62	0.48
Am	215,100					1 !				2.61	0.47
ıx İ	382,200		1 1		1.78	1.02	11.38	6.04	11.53	1.28	0.23
X	63,900				3.17 0.53	1.82 0.31	20.23 3.38	10.72 1.79	20.47 3.43	2.27 0.38	0.40 0.07
NATIONAL TOTAL	12,607,400										
WILLIAM TOTAL	12,007,900	• 1	<b>♦</b> I	1	104.40	80.00	667.10	352.70	675.30	74.90	13.50

<sup>\*</sup>FOUNDRY SANDS NOT CONSIDERED HAZARDOUS ON BASIS OF CALSPAN SOLUBILITY YESTS DESCRIBED IN APPENDIX B.

Table 14k
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FROM IRON AND STEEL FOUNDRIES
TOTAL SAND, 1977 (METRIC TONS)

STATE	TOTAL DISPOSED	TOTAL POTENTIALLY	TOTAL HAZARDOUS	DISPOSAL		- <del></del>	7	NSTITUE		<del></del>	·
		HAZARDOUS*	CONSTITUENTS	METHOD	Cu	C,	Mn	Ni	Pb	Zn	PHENO
ALABAMA	1,251,800	0	0	LANDFILL	10 37	5.96	66.26	35.12	67 06	7.44	1.34
ARIZONA	55,520		1	OR OPEN DUMP	0.22	0 27	2 94	1 56	2 98	0.33	0.06
CALIFORNIA	367,200	i i		1	3 04	1.75	19.43	10.30	19.66	2.18	0.39
COLORADO	79,200	<b>}</b>	1	1	0 65	0 38	4.19	2.22	4.26	0.48	0.00
CONNECTICUT	32,800		i I		0.28	0 15	1 74	0 92	1 76	0.20	0.03
DELAWARE	6,100			1	0.06	0 03	0 32	0.17	0.32	0.03	0.01
FLORIDA	17,100		( <b>(</b>	(	0 14	80.0	0.91	0.49	0.92	0 10	0.02
GEORGIA	14,300	,			0 12	0.07	0.75	0 40	0 76	0.09	0.01
ILLINOIS	1,339,800		1		11 10	6.38	70 89	37.58	71.77	7.96	1.44
INDIANA	823,400		1 1	1	6.82	3 92	43 58	23.09	44 11	4.89	0.80
IOWA	305,300		}		2 47	1.45	16 15	8.56	16 36	1.81	0.33
KANSAS	65,500	<u> </u>		İ	0.54	0.31	3.46	1.84	361	0.39	0.07
KENTUCKY	218,000		]		1.80	1.04	11.54	6.12	11.68	1.29	0.23
LOUISIANA	19,000		1 1		0.16	0.09	101	0.63	1.02	0.11	0.02
MARYLAND	60,400	1	<b>j</b>		0.50	0.29	3.20	1.89	3.24	0,36	0 07
WASSACHUSETTS	46,200				0.39	0 22	2.44	1 29	2 48	0.30	0.04
WICHIGAN	2,308,100				19 12	10.98	122 10	64 74	123 65	13 71	2.48
WINNESOTA	158,100	1	} {	1	1.29	0.74	8.26	4.38	8.36	0.93	0.17
MISSOURI	95,200	1			0.79	0.45	5.20	2 68	5 10	0.53	0.17
NEBRASKA	21,100		1		0.78	0.10	1.12	0.60	1 14	0.12	0.02
NEM TEHSEA	286,200	l l		l	2.20	1 27	14 09	7.47	14 26	1 58	0.02
NEW YORK	698,100				5.78	1		19 58	37 39	4 15	0.74
N CAROLINA	80,200		1 1		0.66	0.39	36.94	2.45	4.29	0.48	0.00
OHIO CAROLINA	1			1 1		1 5.55	1				
OKLAHOMA	2,092,500 36,200	<u> </u>	i i		17.34 0.30	9.95	110.61	58 70 1 02	112 04	12 43	2.23 0.04
DREGON	38,700	.	1   1		0,32	0 18	2 05	1.08	208	0.21	0.04
PENNSYLVANIA	1,761,500		\ <b>\</b>			1				i	1
RHOOF ISLAND	23,900	[	{ { I		14.60	8 38	93 21	49 42	94 36	10.47	1 89
CAROLINA	19 000	j j			0 20	0 11	1 26	0.67	1 28	0 14	0.02
	, ,,,,,,,,,	ļ	l		0 15	0 09	1 01	0 53	1 02	0 11	0.02
DAKOTA	700	į			0.02	0.01	013	0.08	0 14	0.01	0
TENNESSEE TEXAS	J18,700 434,000		: 1		2 64	1 152	16.87	8 95	17 08	1 89	0.34
		' I	' [		3 59	2.07	22 97	11 07	23 26	2 58	0 46
JIAH	156,000	1	1 <b>j</b>		1 29	0.74	8.26	4 38	8 36	0 93	0 17
VERMONT	8,200	- 1	1		0.07	0.04	043	0 23	0 44	0 ()4	0 01
VIRGINIA	126,800				1,05	0 60	6 71	3 56	6 79	0 75	0.13
WASHINGTON	32,000	ļ			0 27	0 15	1 69	0.90	1 71	0.19	0.03
VIRGINIA	66,700	l			0 55	0.32	3.53	1.87	3.57	0.40	0.07
VISCONSIN	500,200			· · · · · ·	4 15	2 38	26.48	14 04	27,80	2.96	0.53
PA REGION	,	j	! <b>!</b> !			i	1		!		1
I	111,100	ļ		j	0 83	0 53	5 87	3 12	5 96	0 66	0 11
п	984,300	1			7.99	4 59	3.03	27 04	51 65	5 73	1 03
m	2,021,500	1	<b>!</b> !		16.76	9 63	106 40	56.70	108.29	12.01	2.16
TX	1,919,100	1	<b> </b>	i	15 90	9 14	101 56	53.84	102.80	11.40	2.06
A	7,220,100	ì	1	Ì	59.83	34 35		202 53	386.72	42.90	7.73
AI.	489,200	)		Ì	4 06	2 33	25.89	12.62	26.20	2.90	0.53
AII	487,100				3 97	2.31	26 78	13.87	26.10	2.89	0.52
AII	237,900	1		Ì	1 97	1.13	12.59	6.58	12.75	1.42	0.25
TX.	422,720	1	<b>, ,</b>	1	3.61	2 01	22.37	11.86	22.64	2.51	0.44
X	70,7 <b>00</b>				0 59	0 34	3 74	1 98	3 79	0.42	0.08
ATIONAL TOTAL	13,943,720				115,6	66.4	737 B	390 1	746.9	82.8	14.9

<sup>\*</sup>FOUNDRY SANDS NOT CONSIDERED HAZARDOUS ON BASIS OF CALEPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX B

Table 141
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES
TOTAL SAND, 1983 (METRIC TONS)

STATE	TOTAL DISPOSED	TOTAL POTENTIALLY	TOTAL HAZARDOUS	DISPOSAL METHOD	<u></u>		- C	ONSTITUE	N 18		<b></b>
	Diar Ose D	HAZARDOUS"	CONSTITUENTS	ME THOS	Cu	Cr	Mn	Ni	Рь	Zn	PHEN
ALABAMA	1,542,800	0	0	ANDFILL	12 78	7.35	81.64	43.28	82.64	8.17	1.8
ARIZONA	68,400	1		OR GPEN DUMP	0 57	0 33	3.63	1.92	3.67	0.41	0.0
CALIFORNIA	452,500		' (		3 75	2.16	23.96	12.69	24.23	2.59	0.4
COLORADO	97,600				0 80	0.46	5.17	2 74	5.23	0.59	0.1
CONNECTION	40,500				0.34	0.19	2 14	1 13	2.17	0.26	0.0
DELAWARE	7,500	;	. 1		0 07	0.04	0.40	0.20	0.40	0.04	0.0
FLORIDA	21,100				0 18	0.10	1.12	0.60	1 13	0.12	0.0
GEORGIA	17,600			. (	0 15	90.0	0 93	0.49	0.94	0.11	0.0
ILLINOIS	1,651,100				13 68	7.86	87.37	46 31	88.45	9.81	1.3
INDIANA	1,014,800	'	İ		8 41	4.83	53.70	28 46	53.14	6.02	11
10 <b>WA</b>	376,200	. ]	ł		3.04	1 79	19.91	10.55	20.16	2.24	0.4
KANSAS	80,700	1	-	i	0 67	0 38	4 27	2 26	4 32	0.48	0.0
KENTUCKY	268,600	İ		. 1	2 22	1 28	14.22	7.54	14.39	1 59	0.3
LOUISIANA	23,300	]	1		0 19	0.11	1.24	0 65	1 25	0.14	. 0.0
MARYCAND	74,400	. ]	1		0.61	0 35	3 94	2.09	3.99	0.44	0.0
MASSACHUSETTS	57.000	İ	1		0 48	0 27	3 01	1 59	3 05	0.34	0.0
MICHIGAN	2,844,400			j	23 57	13.53	150 48	79 79	152.38	16.90	3.
MINNESOTA	192,300	1	1	1	1 59	0.91	10.18	5 40	10.30	1 14	0.:
MISSOURI	117,400	]	1	1	0.98	0.56	6 22	3 30	6.28	0.70	0.
NEBRASKA	26,000	- 1	1	- 1	0 22	0 12	1.38	0.74	1.40	0 15	0.0
NEW JERSEY	328 100				2 71	1 57	17,36	9 20	17 57	1.95	0.:
NEW YORK	860,300		l	i	7.13	4 10	45 52	24.13	46.08	5.11	0.1
N CAROLINA	98.800	·		1	0.82	0.48	5.23	2 77	5.29	0.59	0.
ОНІО	2,578,800				21 37		138.44	72 33	138.07	15.32	2.
OKLAHOMA	44,600			1	0 37	0.22	2.36	1.25	2 39	0.26	0.0
OREGON	47,700			1	0.40	0.23	2.52	1 34	2.56	0.29	0.1
PENNSYLVANIA	2,170,800		- 1	(	17 99	10 33	114.87	60.90	116.29	12.91	2.5
RHODE ISLAND	29,400	j	1		0.25	0.14	1.55	0.83	1.58	0.18	0.0
S CAROLINA	23,400			ŀ	0.23	0.11	1,24	0.65	1.25	0.14	0.4
S DAKOTA	3,270		j .	)	0.03	0.01	0.16	0.10	0.18	0.01	1
TENNESSEE	392,800			ì	3 26	187	20.79	11 03	21 04	2.33	ì
TEXAS	534,800 ;	1	į.	<b>\</b>	4 43	2 55	28.31	13.64	28.65	3.17	0.4
UTAH	192,300	j		ŀ		1	0	1	1	1.14	i
VERMONT	10 100	1	.	1	1 59 0.08	0 91	10.18 0.53	5 40 0 29	10.30	0.05	0.3
VIRGINIA	156,200			1	1 29	0.05	0 53 8 27	4 39	0.55 8.31	0.05	1.0
WASHINGTON	39,400			1	0 33	0 19	8 27 2 09			0.23	0
W VIRGINIA	82,200	1		İ	0.68	0.40	4.35	1 10 2.30	2.11	0.23	0.0
WISCONSIN	816,500	1	1	ļ	5 11	2.93	32.63	17,30	33.03	3.67	0.0
	••••	ļ	,	· · · · · · · · · · · · · · · · · · ·	911	2.83	34.03	17.30	33.03	3.07	0.1
EPA REGION		•	] :				!	1	ı		ł
1	137,000	1	<u> </u>		1 14	0.65	7.24	3.84	7.35	0.82	0.
11	1,188,400	1	]		9 84	5 66	62 89	33 39	63.65	7 06	1:
mı	2,491,100		'		20.65	11 87	131 83	69 88	133 45	14 80	2 (
IΛ	2 096 500	1	. 1	,	19.60	11 26	125 16	86 35	126 69	14.06	21
v	8,897 900	1	·		73 74	42 33	470 79	249 59	476 59	52 87	9 5
VI	602,700	[			4.99	2 88	31 91	15 66	23 29	3.57	0.6
ΔII	600,300	1	.		4.89	2 85	31.77	16.85	32 17	3.56	0.6
MII	293 170	1			2 4 3	1 39	15 51	8 23	15 72	1 74	0.3
IX	520,900	j	, ) )		4.32	2.48	27.57	14.61	27.90	3.09	1.0
x	87,100	ļ			0.72	0 42	4.61	2.44	4.68	0.52	0.1
NATIONAL TOTAL	16,915,070	1	1		<del></del>		909 3	+		+	<del> </del>

<sup>\*)</sup> DUNDHY SANDS NOT LONSIDERED HAZARDOUS ON BASIS OF CALSPAN SOLUBILITY TESTS DESCRIBED IN APPENDIX B

Table 14m

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES REFRACTORIES, 1974 (METRIC TONS)

STATE	TOTAL DISPOSED	TOTAL POTENTIALLY HAZARDOUS	DISPOSAL METHOD
ALABAMA	29,320	o	ALL
ARIZONA	3,410		DISPOSED OF IN
CALIFORNIA	9,960		OPEN DUMP
COLORADO	1,850	}	OR LANDFILLS
CONNECTICUT	670		
DELAWARE	370		1
FLORIDA	780		1 1
GEORGIA	540		1 1
ILLINOIS	36,910	1	1
INDIANA	19,870		(
IOWA	7,240		1
KANSAS	3,690		1 1
KENTUCKY	4,520		{
LOUISIANA	890		
MARYLAND	1,500		
MASSACHUSETTS	960		1
MICHIGAN	49,950		
MINNESOTA	4,040		
MISSOURI	3,920		} }
NEBRASKA	970		
NEW JERSEY	5,760		}
NEW YORK	1	]	
	17,280		] ]
N CAROLINA	1,660		[ [
OHIO	55,680		
OKLAHOMA	1,170		} }
OREGON	2,070	ł	
PENNSYLVANIA	45,060		
RHODE ISLAND	490		[ [
8. CAROLINA	390		}
S. DAKOTA	160		
TENNESSEE	8,060		] ]
TEX AS	10,840		1
UTAH	3,590		
VERMONT	170		
VIRGINIA	2,840		1
WASHINGTON	1,690		
W. VIRGINIA	1,770		1 1
WISCONSIN	15,430		L
EPA REGION			
1	2,290		1
П	23,040		}
m	61,630	1	
121	45,260		1
V	181,880		
זא	12,700		
<b>V</b> III	15,820	1	
AIII	b,600	1	
ıx.	13,790	[	l
X	3,760		
		<del></del>	<del> </del>
NATIONAL TOTAL	355,270	₹	Ì

Table 14n

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES REFRACTORIES, 1977 (METRIC TONS)

\$TATE	TOTAL DIRPOSED	TOTAL POTENTIALLY HAZARDOUS	DISPOSAL METHOD
ALABAMA	32,428	0	ALL
ARIZONA	3,771		DISPOSED OF IN
CALIFORNIA	11,038		OPEN DUM
COLORADO	2,046		OR LANDFILL
CONNECTICUT	741		
DELAWARE	409	1	1 1
FLORIDA	863		) <b> </b>
GEORGIA	597		
ILLINOIS	40,822		! !
INDIANA	21,976		
IOWA	8,007		
KANSAS	4,081		
KENTUCKY	4,999	1	
LOUISIANA	984		
MARYLAND	1,659	ļ ļ	1 [
MASSACHUSETTS	1,062		
MICHIGAN	55,245	1	
MINNESOTA	4,468		) [
MISSOURI	4,336		i i
NEBRASKA	1,073	<b>, ,</b>	1 1
NEW JERSEY	6,371	1	
NEW YORK	19,112		l l
N CAROLINA	1,836	İ	i i
OHIO	61,582		
OKLAHOMA	1,294		\ <b>\</b>
OREGON			1 1
PENNSYLVANIA	2,289 49,825		
RHODE ISLAND	542		
8. CAROLINA	431	<b>.</b>	
S. DAKOTA	177	) ]	) }
TENNESSEE			
1	8,903		
TEXAS	11,768		Ì
UTAH	3,971	j	
VERMONT	188		
VIRGINIA	3,141		
WASHINGTON W VIRGINIA	1,889		
WISCONSIN	1,958		1
	17,066		<u> </u>
EPA REGION	-		
1	2,533	l	
n	25,482		
TET	66, <b>99</b> 2	{	
122	50,068	1	
¥	201,159		
¥ZL.	14,046		
VIII	17,497		
Am	6,194		
DK.	14,809	(	
I	4,159		
NATIONAL TOTAL	392,929	<u>t</u>	····

Table 140
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FROM IRON AND STEEL FOUNDRIES REFRACTORIES, 1983 (METRIC TONS)

STATE	TOTAL DISPOSED	TOTAL POTENTIALLY HAZARDOUS	DISPOSAL METHOD
ALABAMA	39,963	0	ALL
ARIZONA	4,648		DISPOSED OF IN
CALIFORNIA	13,603		OPEN DUMP
COLORADO	2,822		OR LANDFILL
CONNECTICUT	913		
DELAWARE	504		
FLORIDA	1,063		
GEORGIA	736		
ILLINOIS	50,308		
INDIANA	27,083	į	
IOWA	9,868		
KANSAS	5,029		1
KENTUCKY	6,181		
LOUISIANA	1,213		
MARYLAND	2,045		1 1
MASSACHUSETTS	1,308		
MICHIGAN	68,082		
MINNESOTA	5,506		
MISSOURI	5,343		
NEBRASKA	1,322		
NEW JERSEY	7,851		
NEW YORK	23,563		
N. CAROLINA	2,263		1
OHIO	75,892		
OKLAHOMA	1,595		į į
OREGON	2,821	1	
PENNSYLVANIA	61,403		
RHODE ISLAND	668		
S. CAROLINA	532		
S. DAKOTA	218		
TENNESSEE	10,972		
TEXAS	14,502		
HATU	4,893	<b>)</b>	İ
VERMONT	232		
VIRGINIA	3,871		i
WASHINGTON	2,303		
W VIRGINIA	2,413		
WISCONSIN	21,031		<b>*</b>
EPA REGION			
	3,121		
n	31,403		
ш	70,235		
DZ .	61,689		
7	247,902		
VI	17,310		
Δu	21,583		
MIN	7,633		
DX	18,251		
x	5,125		
NATIONAL TOTAL	484,233		* ************************************
	107,533	<b>4</b>	

emissions collected by dry control systems. The amounts of individual constituents were calculated by multiplying the total waste figures by the concentration values derived from laboratory analyses of waste samples collected at several plants.

An alternative approach for compiling sludge and dusts values for each state might be to multiply the waste generation factors given in Table 12 by the production figures on a state-by-state basis. This approach was not used since state production figures were not directly available for each type of ferroalloy and the numbers of plants using each type (wet/dry) of control system was not known.

The waste slag quantities were calculated by multiplying the slag generation factors obtained from plant visits (see Table 12) by the state production figures for each type of ferroalloy as estimated from the sludge and dust values obtained from in the ferroalloy survey and from furnace emission data contained in Reference 7. The sums of the sludge and dust values were divided by the furnace emission factors for each ferroalloy category for each state to obtain production estimates. The state production estimates for each ferroalloy were then summed and compared with published national figures. The individual state figures were then adjusted as appropriate so that the national figures agreed. The slag constituent values for each state were obtained by multiplying the total slag values for each alloy type by the concentration values determined through the analyses of collected slag samples, and summing over all alloys.

#### 2.3 TREATMENT AND DISPOSAL TECHNOLOGY

#### 2.3.1 Current Treatment and Disposal Practices

Slag. Slag which originates from the metal smelting furnaces is open dumped. This practice is considered environmentally adequate at this time in the absence of significant leaching of toxic constituents as ascertained in solubility tests as described in Appendix B.

Waste Sand. Waste sand from cores and molds may either be reclaimed for making new molds or disposed of in open dumps. Open dumping is considered environmentally acceptable at this time in the absence of significant leaching of toxic constituents as ascertained in solubility tests described in Appendix B.

Core Butts. Core butts containing non-degraded sands and binders are also open dumped. Although solubility tests were not conducted on core butts they are not considered potentially hazardous at this time. Solubility testing on core butts is needed to confirm non-leachability.

Sludges. Sludges originating from wet scrubbing of furnace emissions is generally mixed with dry sands, dusts or other dry wastes and open dumped along with these wastes. This practice is considered environmentally adequate at this time in the absence of significant leaching of toxic constituents as ascertained in solubility tests described in Appendix B.

Dusts. Dusts originating from sand reclaiming or control of emissions from furnaces are open dumped. This practice is considered environmentally acceptable at this time in the absence of significant leaching of toxic constituents as ascertained in solubility tests described in Appendix B.

Refractories. The broken, or eroded brick refractories from furnaces are open dumped and are considered non-hazardous. Open dumping is considered environmentally acceptable.

Floor Sweepings. Sweepings from the core making room are principally sand and are not considered potentially hazardous at this time. Solubility tests were not conducted on sweepings but are needed to confirm designation as non-hazardous.

Since all of the wastes from iron and steel foundries are considered non-hazardous at this time Levels I, II and III technology need not be addressed at this time.

#### 2.4 COST ANALYSIS

Because none of the iron and steel foundry wastes have been considered potentially hazardous based on available evidence at this time there are no costs attributable to hazardous waste disposal.

#### 3.0 PRIMARY SMELTING AND REFINING OF FERROALLOYS (SIC 3313)

#### 3.1 INDUSTRY CHARACTERIZATION

Ferroalloy is the generic term for alloys consisting of iron and one or more other metals. Ferroalloys are used in steel production as alloying elements and deoxidants.

The major types of ferroalloys produced are ferromanganese, silicon manganese, ferrosilicon, ferrochrome and silvery iron. The 1972 production of the ferroalloys and percent of total ferroalloy production for that year are as follows: (Reference 6)

Ferromanganese	726,416 MT	32%
Silicomanganese	139,014	6%
Ferrosilicon	763,305	33%
Ferrochrome	319,611	14%
Silvery Iron	147,940	6 %
Other	206,294	9%

Total U.S. ferroalloy production in 1971 and 1972 was 2,114,733 and 2,292,153 MT respectively. Production of the above alloys comprises over 90% of the industry. Ferroalloys produced in minor quantities (approximately 9% of total) are ferronickel, ferrophosphorus, ferrotitanium, ferrocolumbian, ferrotungsten and ferromolybdenum.

U.S. producers of ferroalloys are listed in Table 15. Table 16 gives ferroalloy plants by process by state, EPA region and nationally. There is insufficient information available to estimate state by state and regional production capacities. Total value of U.S. ferroalloy shipments in 1973 was \$720,542,000 (Ref. 8).

#### 3.2 WASTE CHARACTERIZATION

This section contains descriptions of production technology at ferroalloy plants and the resultant byproducts or wastes which are either recycled directly or disposed of on land. Estimates are given for the quantities of wastes and potentially hazardous constituents thereof which are disposed of on land either in lagoons or open dumps.

#### 3.2.1 Process Descriptions

Because of the common coproduction of ferromanganese and silicomanganese within the same plants and close similarities in production technology these ferroalloys will be treated together. Production of ferrosilicon, ferrochrome, and ferronickel will be dealth with separately.

Ferromanganese and Silicomanganese. The assumed plant has a daily capacity of 236 metric tons (260 short tons) of ferromanganese and 74 metric tons (82 short tons) of silicomanganese. Ferromanganese is produced in two furnaces. The silicomanganese is produced in a single

TABLE 15. PRODUCERS OF FERROALLOYS IN THE UNITED STATES IN 1972

Producer	Plant location	Product 1	Type of furnace
Agrico Chemical Co	Pierce, Fla	FeP	Electric.
- <del>-</del>	(Calvert City, Ky)	FeCr. FeCrSi.	
Lirco Alloys & Carbide	Calvert City, Ky Charleston, S.C.	FeMn, FeSi.	ъ.
Lireo Attoys & Carbide	Mobile, Ala	SiMa.	Do.
labama Metallurgical Corp.	Selma, Ala	FeSi	<b></b>
Bethiehem Steel Corp	Johnstown, Pa		Do. Blast,
	Woodstock, Tenn	FeMn.	
Chromium Mining & Smelting Co.		FeMa, SiMa, FeCr, FeSi, FeCrSi.	Electric.
limax Molybdenum Co	Langeloth, Pa	FeMo	Aluminothermic.
Diamond Shamrock Corp	Kingwood, W. Va	FeMn	Electric.
MC Corp.	Pocatello, Idaho	FeP	Do.
•	(Cambridge, Ohio)	FeB, FeCb, FeTi, FeV, FeCr,	
	Graham, W. Va	FeV. FeCr.	
Poote Mineral Co	Keokuk, Iowa	FeCrSi, FeSi,	Do.
00.0	Vancoram, Ohio	silvery iron.	
	Wenatchee, Wash Buffalo, N.Y	other.	
Janua Furnace Corp	Ruffalo N V	Silvery iron	Blast.
lanna Nickel Smelting Co	Riddle, Oreg	FeNi	Electric.
looker Chemical Corp	Columbia, Tenn	FeP.	Do.
	Beverly, Ohio	P-C- P-C-01 P-01	
nterlake Steel Corp		FeCr, FeCrSi, FeSi, SiMn.	Do.
Kawecki Chemical Co	Easton, Pa	FeCb	Aluminothermic.
Mobil Chemical Co	Nichols, Fla	FeP	Electric.
Colybdenum Corp. of America	Washington, Pa	FeMo, FeW, FeCb,	Electric and
•		FeB.	siuminothermic.
Monaanto Chemical Co	(Columbia, Tenn) Soda Springs, Idaho)	FeP	Electric.
N L Industries, Inc	Niagara Falls, N.Y	FeTi, other	Do.
New Jersey Zinc Co	Palmerton, Pa	Spln	Do.
ten seracy mine more management in	(Brilliant, Ohio		20.
		FeCr. FeSi, FeB,	
Ohio Ferro-Alloys Corp	Powhatan, Ohio	FeMn, SiMn,	Do,
	Tacoma, Wash	other.1	
Reading Alloys	Robesonia, Pa	FeCb, FeV	4 hamila oth
Keading Alloys	Newfield, N.J.	Patt Part Can	Aluminothermic.
Shieldalloy Corp	Newneld, N.J	FeV, FeTi, FeB,	Do.
		FeCb, NiCb, CrMo, other.*	
	(Tarpon Springs, Fla)	•	
Stauffer Chemical Co	{Mt. Pleasant, Tenn}	FeP	Electric.
	Mt. Pleasant, Tenn		
Panagas Allaum Cara	Bridgeport, Als	FeSi	D.,
Leznessee Alloys Corp	Kimball, Tenn		Do.
Tennessee Valley Authority	Muscle Shoals, Ala	FeP	Do.
Tenn-Tex Alloy Chemical Corp. of	Houston, Tex	FeMn, SiMn	Do.
Houston.	/Allan 307 37a		
	[Alloy, W. Va	FeB, FeCr, FeCrSi,	
	Ashtabula, Ohio	FeCb, FeSi,	
Union Carbide Corp	Marietta, Ohio	FeMn. Feft.	Dσ.
	Niagara Palla, N.Y	FeW, FeV.	20.
	Portland, Oreg	SiMn, other.	
	Sheffleid, Ala	Citate' Cenar.	
U.S. Steel Corp	Clairton, Pa.	FeMn	Blast.
our name corp	McKeesport, Pa	4 77 475 Man	ar read to
Woodward Iron Co	Woodward, Ala	FeSt, FeMn, SiMn.	Electric.

<sup>&</sup>lt;sup>1</sup> CrMo, Chromium molybdenum; FeMn, ferromanganese; Spin, spiegeleisen; SiMn, silicomanganese; FeSi, ferrosilicon; FeP, ferrophosphorus; FeCr, ferrochromium; FeMn ferromolybdenum; FeNi, ferronickel, FeTi, ferrotitanium; FeW, ferrotingsten; FeV, ferrovanadium; FeB, ferroboron, FeCt, ferrocolumbium; NiCb, nickel columbium; Si, silicon metal.

<sup>1</sup> Includes Aisifer, Simanai, zirconium alloys, ferrosilicon boron, aluminum silicon alloys, and miscellaneous ferroalloys.

Source: Minerals Yearbook, Volume I, U.S. Dept. of Interior, 1972

TABLE 16
STATE, REGIONAL, AND NATIONAL DISTRIBUTION OF FERROALLOY PLANTS BY PROCESS

	No. of	Plant Distribution By Process		
State	Plants	BF	<u>A</u>	E
Alabama	6	0	0	6
Florida	3	0	0	3
Idaho	2	0	0	2
Iowa	1	0	0	1
Kentucky	1	0	0	1
Montana	1	0	0	1
New Jersey	1	0	1	0
New York	4	1	0	3
Ohio	8	0	0	8
Oregon	2	0	0	2
Pennsylvania	8*	3	4	2
South Carolina	1	0	0	1
Tennessee	6	0	0	6
Texas	1	0	0	1
Washington	2	0	0	2
West Virginia	3	0	0	3

Region	No. of	Plant Distribution By Process		
	Plants	BF	<u>A</u>	E
1	0	0	0 .	0
2	5	0	1	3
3	11*	3	4	5
4	17	0	0	17
5	8	0	0	8
6	1	0	0	1
7	1	0	0	1
8	1	0	0	1
9	0	0	0	0
10	<u>6</u>	<u>0</u>	<u>0</u>	6
Nation	50	3	5	42

BF = Blast Furnace

5.44

A = Aluminothermic

E = Electric Furnace

<sup>\*</sup>One plant employs both aluminothermic and electric furnace processes

furnace. Annual production is given as 81,100 metric tons (89,400 short tons) of ferromanganese and 25,400 metric tons (28,000 short tons) of silicomanganese on the basis of an 11.3 month operating year for each of the three furnaces.

Raw materials for the production of standard ferromanganese (80% Mm and 6.5% C, with the balance mostly iron) consist of manganese ore, coke, mill scale and melted ferromanganese. The input materials are sized, mixed together and introduced into the furnaces directly over the molten bath. An overall flow sheet is shown in Figure 3. The furnaces are of the open submerged-arc type having three vertical Soderberg-type electrodes arranged in a triangle. The ends of the electrodes protrude 5 to 6 feet below the molten bath material. A paste, consisting of coke and pitch, is fed into the electrode shells from the top. As the paste descends, it is baked into a solid mass by the heat of the furnace.

The molten ferromanganese collects at the bottom of the furnace and is tapped into ladles for transfer to a cooling area. Slag is decanted from the top of the ladles, and the product is poured into a cooling bed in layers, a process called layer casting. The solidified product is broken into pieces and sized for sale. The ferromanganese slag is rich in manganese and most of it is used as charge material for silicomanganese production.

The silicomanganese is also made in an open submerged-arc furnace whose general operation is similar to that of the ferromanganese furnaces. The process flow diagram is shown in Figure 3. Input materials for silicomanganese production consist of coal, coke, manganese ore, ferromanganese slag, quartz, mill scale, dolomite, and remelt. The molten silicomanganese is tapped from the furnace into ladles, and the slag is decanted off. The product is cast into layers prior to final sizing. The slag cannot be recycled within the plant so most of it is sold to contractors for use as road fill. Some is sent to an on-site disposal area.

The air emissions for all three furnaces are controlled by wet scrubber systems. The emissions scrubwater from the ferromanganese furnaces with solids amounting to 150.6 kg/MT of product is lime treated and clarified.

Ferrosilicon. There are three major types of ferrosilicon produced in the United States: 75% FeSi, 50% FeSi, and 16-22% FeSi, where the percentages indicate the amount of silicon in the product. The 16-22% FeSi type is commonly called silvery pig iron and accounts for about 20 percent of the total ferrosilicon production.

Most of the ferrosilicon produced in the United States is made in electric submerged-arc furnaces. An average furnace size might be about 15 megawatts with a daily capacity of 37 MT (41 tons) to 65 MT (72 tons), depending on whether the furnace produces 75% FeSi or 50% FeSi. The energy required for 75% FeSi production is about 75% greater than that required for 50% FeSi production. Specifically, the production of 75% FeSi requires only 5.5 mw-hr per MT. Input materials for ferrosilicon production consist of quartzite, scrap steel, coal, and coke.

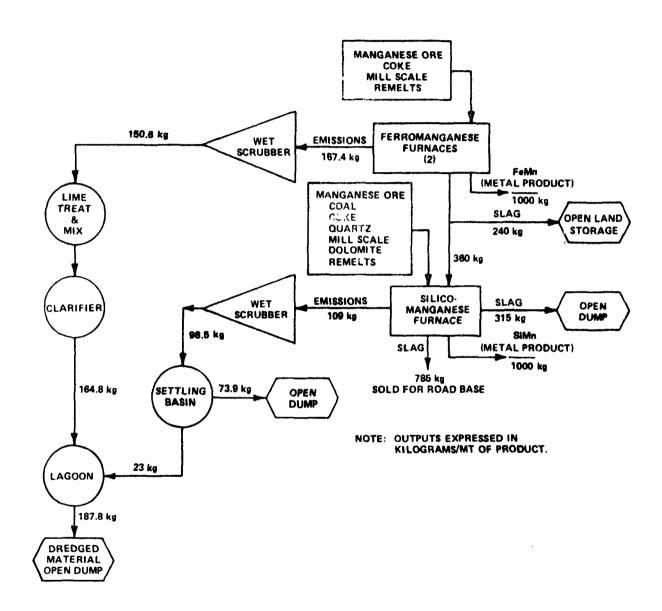


Figure 3 FERROMANGANESE AND SILICOMANGANESE PRODUCTION

Ferrochrome Production. Ferrochrome is made in two grades, high carbon (HC) and low carbon (LC). Most of the ferrochrome produced in the United States is of the high carbon type. Input materials consist of chromium ore, quartzite, limestone, coal and coke. The electrical energy required to produce (HC) ferrochrome averages about 4.6 megawatt-hours per metric ton of product. Furnace emissions average 168 kg of particulates per metric ton of product (335 lb/ton) for either high or low carbon ferrochrome. An average ferrochrome furnace might be rated at 20 megawatts. Thus, the average furnace would produce about 104 metric tons (115 short tons) of ferrochrome per day.

Ferronickel. There is only one ferronickel producing plant in the United States located at Riddle, Oregon. Nickel ore is mined at the top of a mountain and transported to the plant by tram cars.

The plant operates around-the-clock producing approximately 23,600 metric tons (26,000 short tons) of ferronickel (50% Fe, 50% Ni) annually. Reduction of the nickel ore is accomplished by mixing the melted nickel ore with ferrosilicon (48% silicon). The required ferrosilicon is produced in the same plant at the rate of about 20,620 metric tons (22,730 short tons) per year.

The sequence of operations for producing ferronickel consists of ore mining and preparation, melting, reduction, and refining. A flow diagram is presented in Figure 4. The mined ore is first dried and then screened into three fractions. The coarser, low grade rock is diverted to a reject ore pile for possible use in the future if an economical process for nickel extraction can be developed. The ore fraction in the 5/16" to 3/4" range is crushed and temporarily stored. The-5/16" fraction is further screened to remove the fines which are stored separately. The coarser retained ore fractions are calcined and the fines are roasted. The coarse and fine fractions are then transferred to hot ore bins from which they are gravity fed to the furnaces. Ore melting is carried out in four 20,000 KVA electric furnaces. The molten nickel ore is tapped into ladles and vigorously mixed with ferrosilicon which acts as the reducing agent. Mixing is accomplished by transferring the molten mixture back and forth between two ladles. During the reduction process, a fraction of the ferronickel is removed from the ladle at regular intervals and introduced into two small electric furnaces for refining. Other input materials for the refining operations are limestone, dolomite, fluorspar, iron ore, and coarse concentrates from the skull plant.

The skull plant processes slag from the refining furnaces, metal spills and residues from the ladles (called skulls) to produce concentrates of high metal content that are recycled to the refining furnaces and to the ferrosilicon furnace. A hammer mill pulverizes the input materials and the coarser metal-rich fraction is removed magnetically. The finer tailings are slurried with water and piped to a tailings pile.

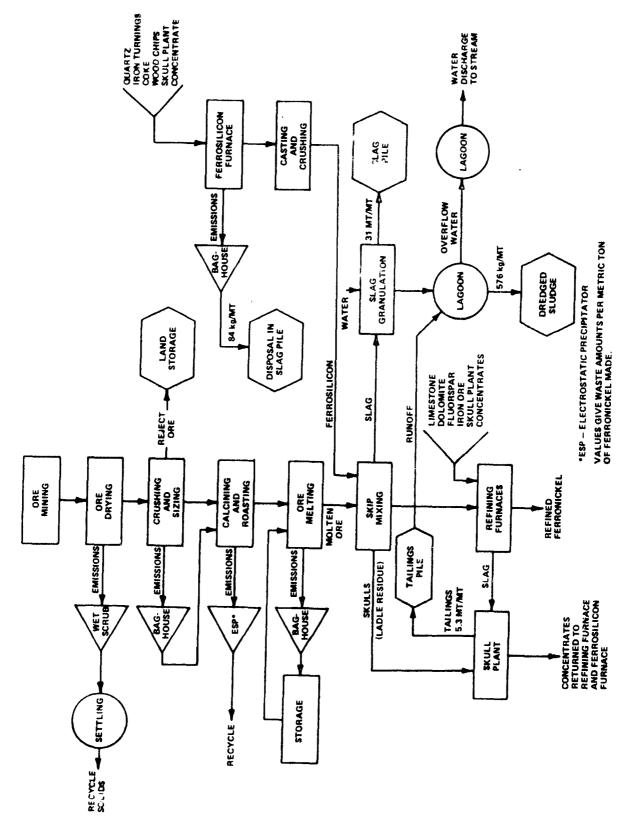


Figure 4 PROCESS AND SOLID WASTE FLOW DIAGRAM FOR FERRONICKEL PRODUCTION

Ferrosilicon is produced in a 15,000 KVA electric furnace with input materials consisting of quartz, iron turnings, coke, wood chips, and skull plant concentrates. All ferrosilicon produced is cast, crushed and used for reduction of the nickel ore.

The molten slag generated during the reduction of the nickel ore is granulated by high pressure water sprays and transferred to the slag pile by conveyor belt. The fines derived from granulation of the slag are carried in the water stream to settling ponds (or lagoons).

## 3.2.2 Description of Waste Streams

## Ferromanganese and Silicomanganese

Slags. A dense vesicular slag is generated from ferromanganese production at a rate of 600 kg/MT ferromanganese product. Approximately 360 kg/MT of the 600 kg/MT generated is used as an input to the silicamanganese furnace. The remaining 240 kg/MT is stored on the ground for possible future use in silicomanganese production.

In the production of silicomanganese a glassy textured slag is generated at a rate of 1100 kg/MT of silicomanganese product. Of this amount approximately 785 kg/MT product is sold for road base with 315 kg/MT product disposed of in open dumps.

Major constituents of ferromanganese and silicomanganese slag are manganese, manganese oxide, silica, alumina, calcium oxide and magnesium oxide. Trace metals in these slags include chromium, copper, lead and zinc.

In solubility tests described in Appendix B there was no leaching of toxic heavy metals at greater than 0.2 ppm from either ferromanganese or silicomanganese slag. For this reason in addition to the dense nature of the slags, ferromanganese and silicomanganese slags are not considered hazardous at this time.

Dusts and Sludges. Depending on whether wet or dry emissions controls are used on furnaces, dusts or sludges are produced. Figure 3 illustrates emissions control residuals using wet scrubbers. Emissions from the ferromanganese furnaces are generated at a rate of 167.4 kg/MT of product. Ninety percent of these emissions or 150.6 kg/MT product are captured in wet scrubbing systems. The scrubber water is lime treated and clarified. Underflow sludge from the clarifier is generated at a dry weight rate of 164.8 kg/MT product and settled in a lagoon.

Emissions from the silico-manganese furnace are generated at a rate of 109 kg/MT silicomanganese product. Ninety percent of the emissions are captured in wet scrubbers as shown in Figure 3 and sent to a settling basin at a rate of 98.5 kg/MT product. Solids are collected in the settling basin, dredged several times per week and trucked to an on-site open dump at a rate of 74 kg/MT product.

Overflow from the settling basin carries 23 kg of dry solids /MT product to the lagoon. Solids from the lagoon are periodically dredged and open damped at a rate of 187.8 kg/MT of product.

In solubility tests described in Appendix B, dusts and sludges from silicomanganese emissions control leached lead at approximately 1.3 ppm. Ferromanganese dusts leached 110 ppm zinc and 560 ppm lead. For these reasons, along with the fine particulate nature of these wastes, sludges and dust, residuals from ferromanganese and silicomanganese production are considered potentially hazardous at this time.

## Ferrosilicon

Dust. The production of ferrosilicon generates no slag. Therefore, control of furnace emissions produces the only significant solid waste. While dry-and-wet emissions control systems are utilized, dry type systems are more prevalent. Furnace emissions average about 450 kg/MT (900 lb/ton) for 75% FeSi and 225 kg/MT (450 lb/ton) for 50% FeSi. Thus, for furnaces controlled by baghouse collection systems the average quantity of collected dry dust will vary between 405 kg/MT product and 202.5 kg/MT product depending on the type of FeSi being made. An overall hooding and capture efficiency of 90 percent is assumed. The collected dusts are trucked to a land disposal area for open dumping.

In solubility tests described in Appendix B there was no leaching of toxic heavy metals greater than 0.3 ppm from ferrosilicon baghouse dust. Sludge would be expected to behave similarly. For this reason dusts and sludges from ferrosilicon production are not considered potentially hazardous at this time.

## Ferrochrome

Slag. In ferrochrome production the slag-to-product ratio is estimated to vary from 1.5 to 2.0. Therefore the slag generation factor is approximately 1750 kg/MT of ferrochrome product. The slag occurs in dense 4 to 6 inch diameter clumps and has a vesicular surface. The slag is either open dumped or processed to produce two or more fractions and sold for use in road building.

In solubility tests described in Appendix B, there was insignificant leaching of toxic constituents from ferrochrome slag. This slag is therefore not considered potentially hazardous at this time.

Dust. Available data show that both wet and dry emissions controls systems are used in ferrochrome production. If the furnace emissions are controlled by a dry system 151 kg of dust per MT of ferrochrome product will be collected on the assumption that the overall hooding and collection efficiency is 90%. The collected dust is usually trucked to an on-site dump for final disposal.

In solubility tests described in Appendix B it was found that dusts from ferrochrome production leached over 100 ppm chrome and around 1 ppm lead. For this reason dust from ferrochrome emissions control is considered potentially hazardous at this time.

Sludge. For a wet collection system operating at an overall capture efficiency of 90%, the same weight of particulates would be contained in the scrubber water as were captured by the dry system. The scrubber water would be piped to a settling basin to allow the particulates to settle. An estimated 97% or 146.5 kg/MT product of the solids would be retained in the settling basin. Accumulated bottom sediments in the settling basin would be pumped out or clammed out periodically and dumped on adjacent land areas.

As discussed previously ferrochrome dust released chrome and lead in solubility tests. Sludge would be expected to behave similarly and is therefore considered potentially hazardous at this time.

## Ferronickel

Slag. Granulated slag from the reduction operation is generated at a rate of 31 MT/MT production, a very high ratio of waste to product. Accumulation of this slag since the plant began operation in 1954 has produced a huge slag pile covering many acres and extending up to a height of 100 feet or greater. A very small fraction of the slag is purchased by a local contractor for road base.

Solids are carried from the slag granulation operation into a large lagoon (approximately 12 acres) at a rate of 697 kg/MT ferronickel product (see Figure 4). Sludge amounting to 576 kg/MT product is dredged once a year from the lagoon and open dumped on land adjacent to the lagoon. Overflow from the settling lagoon is diverted to a second lagoon which is not dredged.

In solubility tests described in Appendix B zinc leached from slag at 2.0 ppm and lead at 1.0 ppm. The fines from this slag (i.e. sludge) however, did not leach toxic heavy metal constituents beyond 0.3 ppm in the solubility tests. For this reason slag and slag fines (sludge) are not considered hazardous at this time.

Skull Plant Tailings. Tailings from the skull plant as shown in Figure 4 are generated at the high rate of 5.3 MT/MT product. The tailings are piped to the tailings pile at the rate of 360 MT (400 short tons) per day. Water runoff from the tailings pile is diverted to the lagoon which receives slag granulation water. Since the skull plant began operation the skull plant tailings pile has grown to an impressive area and height but is dwarfed by the mountainous slag pile.

In solubility tests described in Appendix B, skull plant tailings leached copper and zinc at approximately 50 ppm. For this reason skull plant tailings are considered potentially hazardous at this time.

<u>busts</u>. Dusts collected during ore preparation including drying, crushing, calcining and roasting are fed to the furnaces so no significant solid waste accumulates from control of emissions from these operations.

Dusts from the electric turnace are captured in baghouses and recycled to the furnaces with the exception of dust collected from the ferrosilicon furnace. The ferrosilicon dusts are collected at the rate of 84 kg/MT product, wetted to prevent blowing, and disposed of in the slag pile.

In solubility tests described in Appendix B ferrosilicon furnace dust did not leach any toxic heavy metals greater than 0.3 ppm and is therefore considered non-hazardous.

## 3.2.3 Waste Quantities

A number of ferroalloy plants were visited and samples of waste residuals obtained for subsequent chemical analyses. These analyses are given in Appendix A. From these analyses and data provided by individual plants on quantities of wastes, waste generation and constituent concentration factors were developed. These factors are given in Table 17. Using the generation and concentration factors in Table 17 the yearly generation of waste residuals from typical plants have been estimated. These estimates are given in Table 18 for typical plants producing the various ferroalloys (FeMn, SiMn, FeSi, FeCr, FeNi). Based on plant capacities, data supplied by individual plants, and chemical analyses of collected samples, estimates of the total quantities of land disposed wastes and potentially hazardous constituents thereof have been made on state by state, EPA regional, and national levels. This data is tabulated in Table 19 for 1974, 1977 and 1983. Estimates for growth in ferroalloy capacity by 1983 is approximately 4%. Inherent error in estimated waste quantities does not warrant meaningful increased 1977 and 1983 projections at this growth rate.

Oregon with only two ferroalloy plants generates the greatest amount of slag and sludge than other states with ferroalloy industries. This is a result of the ferronickel plant which generates very large quantities of waste per unit of product. Ohio which has 8 ferroalloy plants generates the second largest quantity of slag and sludge and the greatest quantity of dusts.

### 3.3 TREATMENT AND DISPOSAL TECHNOLOGY

## 3.3.1 Current Treatment and Disposal Practices

## Ferromanganese and Silicomanganese

Slag. Slag from the ferromanganese furnace which is not used as charge material in silicomanganese production (approximately 40% of total slag) is stored on land for possible future use. Approximately 30% of residual slag from silicomanganese furnaces which is not able to be sold as road fill is open dumped. Open dumping or sale as roadfill are environmentally adequate since ferromanganese and silicomanganese slags are not considered potentially hazardous at this time.

WASTE GENERATION FACTORS - FERROALLOY PRODUCTION, DRY WEIGHTS Table 17

	CEMEBATION			CONCE	CONCENTRATION FACTORS (ppm)	ACTORS (p	pm)		
TYPE OF WASTE	FACTOR Kg/MT	රි	ర	ઢ	Mn	Ë	Pb	>	Zn
FERROMANGANESE SLAG SLUDGE	240 164.8		100 18	310 50	525,000 20,000	1 1	10 5,000	1 1	20 35,000
SILICOMANGANESE SLAG SLUDGE	1,100 98.5	1 1	27	8 8	70,000 200,000	1 1	20 20 25,000		20 10,000
FERROSILICON SLAG SLUDGE DUST	338	- 1	1 1 29	2,180	_ _ 1,500	_ _ 3,250	!	1 1 1	1,300
FERROCHROME SLAG DUST	1,750	Į į	3,710 3,390	71 28	290	1 1	12 300	1	65 14,000
FERRONICKEL SLAG TAILINGS DUST SLUDGE	31,000 5,300 84 576	104 47 82 159	321 380 160 2,140	50 21 2,180 23	1,100 500 1,500 2,000	1,850 1,330 3,250 4,100	1111	1   1   1   . 	100 500 1,300

YEARLY GENERATION OF RESIDUALS BY TYPICAL FERROALLOY PLANTS, DRY WEIGHTS Table 18

	TOTAL WASTE	OO/	ANTITY OF F	QUANTITY OF POTENTIALLY HAZARDOUS CONSTITUENTS (MT)	HAZARDOUS	CONSTITUEN	TS (MT)	
TYPE OF WASTE	QUANTITY (MT)	3	ర	ກິວ	Mn	Ž	Pb	Zn
FERROMANGANESE <sup>2)</sup>								
SLAG	7,200	ı	0.72	2.23	3,780	1	0.07	0.14
SLUDGE  a) PRODUCTION CAPACITY OF  .30,000 MT/YEAR	4,944	1	0.089	0.247	6.86 6.	1		173
SILICOMANGANESE <sup>b)</sup>								
SLAG	44,000	ı	1.19	1.01	3,080	I	0.088	0.88
SLUDGE b) PRODUCTION CAPACITY OF 40,000 MT/YEAR	3,940	I	0.177	0.323	788	I	98.5	39.4
FERROSILICOW <sup>c)</sup>								
SLAG	0	I	ı	ı	i	ı		1
c) PRODUCTION CAPACITY OF 40,000 MT/YEAR	13,520	-	2.16	29.48	20.28	43.94	ı	17.58
FERROCHROME <sup>d)</sup>								
SLAG	61,250	ı	722	1.04	17.8	ı	0.735	3.98
DUST d) PRODUCTION CAPACITY OF 35,000 MT/YEAR	5,285	l	17.92	0.285	38.1	ı	1.586	74.0
FERRONICKEL*)								
SLAG	732,000	26	<b>522</b>	37	802	1,350	ŧ	73
TAILINGS	125,000	5.9	48	2.6	62	166	1	23
DUST	1,980	0.16	0.32	4.3	3.0	.6.4	ı	2.6
SLUDGE  9) PRODUCTION CAPACITY OF	13,600	2.2	8	0.31	27.2	56	1	1.7

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FOR THE FERROALLOY INDUSTRY TOTAL SLAG – 1974, 1977, 1983 (METRIC TONS) Table 19a

		Ā	4					LSM00	COMSTITUENTS				
STATE	TOTAL*) DISPOSED	POTENTIALLY HAZARDOUS	HAZARDOUS CONSTITUENTS	DIBOSAL	3	გ	ბ	ð	ş	ž	e	>	ā
ALABANKA	27,100	0	0-	LAND DISPOSED. SOLD	ž	\$	0.7	9.0	1900	4 2	0.5	1	0.5
KENTUCKY	137,000		-	CAND DISPOSED. SOUD	\$	\$	2	ē	22,700	ž	5	<b>\$</b>	9,
NEW JERSEY	3,200			ON-STE DISPOSAL SOME SOLD	ş	¥	4	•	4	۵	۵.	•	
NEW YORK	8,900			SOLD FOR ROAD CONSTRUCTION	\$	\$	1.91	6.2	in .	á .	ş	\$	ž
0	177,600		^	METAL RECOVERY SOLD, LAND DISPOSED	ş	¥	37.1	ŧē	23,000	ş	ē.	¥	10.8
ONEGON	787,900		are remain as	CAND DEPOSED. SOLD	ž	-	ž	3	9,500	2	63	ž	S. P.
S. CAROLMA	140,700			PROCESSED TO REMOVE METALS THEN SOLD	ž	ş	Ş	72	\$	<u> </u>	91	1	=
TENNESSEE	86,180			LAMO DESTORED. SOLD	<b>§</b>	ş	<b>6</b>	3.5	4,560	ş	ŭ	\$	ī
TEXAS	006,11			LAND DEPOSED. SOLD	\$	ž	2	<b>2</b>	9,090	į	2	į	4.0
W. VIRGINIA	45,780			LAND DESPOSED, SOLD	<b>≨</b>	ž	<b>8</b>	4	068	ş	0.2	<b>3</b>	2.0
BPA REGION													
Ħ	12,100			-	ş	ž		0.2	ıo.	ž	\$	ş	\$
Ħ	45,700				\$	Ž	200	70	9	¥ Z	20	\$	2.0
<b>2</b> 9 1	369,900				ď.	ž	5	19.5	29,201	ž	4.5	ź	17.9
<b>⊳</b>	177,500				ş	ž	33	5	23,000	۲ ۲	1.5	<b>≨</b>	801
<b>5</b>	17,300				Ž.	₹	- 2	5.4	060'6	ž	0.7	ş	70
<b>3</b>	0				0	0	0	0	•	•	0	•	•
*	787,900		-		ş	-	¥	3	9,500	~	0,3	¥	78.5
NATIONAL TOTALS	1,410,400	-	-		ş	-	1542	2	71,486	2	6.7	\$	6
			*										

MINICLUDES SLAG SOLD, BUT NOT SLAG USED ON SITE FOR PRODUCING OTHER ALLOYS
 LAGGE FOT CHARARDIAS AT THIS TIME AS
 ARZBULT OF SOLUBLITY TESTING CONDUCTED BY CALSPAN
 AND DESCRIBED IN APPENDIX B.

NA - DATA NOT AVAILABLE P - CONSTITUENT KNOWN TO BE PRESENT, BUT AMOUNT NOT KNOWN

SOUNCE CALIFFAN CORPORATION

Table 19b
ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE
FOR THE FERROALLOY INDUSTRY
TOTAL DUST — 1974, 1977, 1983 (METRIC TONS) — DRY AND WET

								CONSTITUENTS	VENTS				
STATE	TOTAL	POTENTIALLY HAZARDOUS	HAZARDOUS COMSTITUENTS	DISPOSAL	3	రి	ŭ	ત	ذ	ž	e	>	uZ
ALABAMA	99 #	0	•	LAND	¥	0.2	03	4.5	, w	87.9	ž	\$	2.7
KENTUCKY	8	14,300	986	LAND	90	6	249	7 61	Ď	K S	8	¥ 0	<b>9</b>
NEW JERSEY	1	ď Z	ş	ON-SITE DUM	*	ş	a	n	•	۵.	a.	 Q.	۵
NEW YORK	008.5	2,900	10	ON-SITE DUMP	¥	ξ.	0 2	e C	7	1	\$	<b>≨</b>	<b>-</b>
OHEO	80.30	19,500	%		\$	2.3	5	<b>8</b>	Ä	98	\$	ž	<b>88</b> 6
OREGON	2.000	0	0	WETTED AND DUMPED ON SLAG PILE	\$	0.2	E 0	<b>*</b>	3.6	49	1	¥	2.6
S. CAROLINA	9.100	9,100	857	LANDFILL	60	A A	363	8 0	181	\$	8	50	454
TENNESSEE	10,900	10,900	1103	LAND	ž	ž	5	0	8	1	ĸ	ş	81
WASHINGTON	15.400	0	o	LAND	\$	60	90	6	n A	811	\$	٧ ٧	4.7
W. VIRGINIA	907 1	15,400	871	LAND	<b>\$</b>	1.2	2.5	31.2	371	8	5.2	₹ 2	37.1
EPA REGION							<del>!</del>						
Ħ	2,300	2,900	8.7		\$	S A	0.2	0 3	-	<u> </u>	ş	¥	£.
Ħ	94.400	15,400	178	_	į	1 2	2.5	31.2	174	167	5.2	ž	37.1
a	90,300	34,300	98.20		1.5	6.0	612	Ŕ	2822	233	8	60	543 1
<b>&gt;</b>	104,100	19,500	%		ž	2.3	5.1	60	ī	9'68	Ş	ž	48.6
B	•	•	•		0	•	0	0	0	0	•	0	0
B	•	0	0	-	0	•	0	0	i)	•	•	0	0
×	17,400	0	6		¥ ¥	0.5	0.9	12.2	8.4	18.3	ž	A N	7.3
NATIONAL TOTALS	302,100	75,100	3730		1.5	4.9	129	8	N N	431	ĕ	60	32
						1	+	1	1				

NA = DATA NOT AVALLABLE
P = CONSTITUENT KNOWN TO BE PRESENT, BUT AMOUNT NOT KNOWN
SOURCE. CALEPAN CORPORATION

111

Table 19c

ESTIMATED STATE, REGIONAL, AND NATIONAL SOLID WASTE FOR THE FERROALLOY INDUSTRY TOTAL SLUDGE — 1974, 1977, 1983 (METRIC TONS) DRY WEIGHT \*

							*	AZARDO	HAZARDOUS CONSTITUENTS	ITUENT			
STATE	TOTAL	TOTAL POTENTIALLY HAZARDOUS	TOTAL HAZARDOUS CONSTITUENTS	DISPOSAL	8	ပိ	õ	3	5	ž	£	>	5
ALABAMA	16,600	16,600	195	LAGOONS	4M	1.0	1.9	28.5	82,	39.2	14.5	ĭ	25
HOMA	10,960	16,900	<b>4</b>	LAGOOMS	ğ	ď	ž	2	1	ž	¥	1	ž
HEW JERSEY	\$	ž	<b>\$</b>	LAGOONS	ď Z	<b>4</b>	۵.	<b>L</b>	a	۵.	۵.		4
0.440	36.800	38,800	7202	LAGOONS	9.5	4.0	219	2	ž	9	ĸ	3	60
OREGON	142,200	142,200	9	TAILINGS PILE & LAGOON	ş	8.0	E	12	2	B	2	<b>1</b>	<u>3</u>
S. CAROLINA	3,900	3,900		LAGOON	4.0	ş	<b>15</b>	2	2,5	<b>½</b>	9	ร	19.5
TERMENSEE	•	•	0	ı	•	•	0	•	•	0	o	0	0
TEXAS	3,300	3,300	\$	LAGOOMS	ş	ď	5.	0.2	65.3	<u>خ</u>	16.3	<b>1</b>	7
WASHINGTON	•	•	0	ı	•	٥	0	0	•	٥	0	0	•
W. VIRGINIA	•	0	0	ı	•	0	0	•	•	•	•	0	0
EPA REGION													
E	1	ž	<b>3</b>		Š	4	۵.	a	•	•	•		٠
B	•	0	0		•	0	0	0	0	0	٥	•	•
23	20,500	20,500	748		0.4	1.0	<u> </u>	2	25	8	18.4	¥	22
Þ	35,800	35,800	202		0.5	9.0	219	2	<b>8</b>	9	12.6	63	ŝ
Ħ	3,300	3,300	ž	•	¥	ď.	0	0.2	65.3	ď.	16.3	ş	=
B	10,900	10,900	Ą		ž	¥	ž	ž	¥	ď.	¥	ž	\$
×	142,700	142,200	683	-	¥.	8.0	٤	Ä	163	22	2	į	192
MATIONAL TOTALS	212,700	212,700	3.065		60	0.6	454	4.2	1509	772	178	F 0	1165

SOURCE - CALSPAN CORPORATION

NA = DATA HOT AVAILABLE
P = CONSTITUENT KNOWN TO BE PRESENT, BUT ANOUNT NOT KNOWN
• TO CONVERT TO APPROXIMATE WET WEIGHTS MULTIPLY BY 2.5

Sludges and Dusts. At the present time lime treated scrubwater from ferromanganese furnace emissions control and wet scrubber sludge from silicomanganese emissions control is settled in lagoons or settling basins. Settled sediments are periodically dredged and dumped on land. Dusts are either directly dumped on land or wetted before dumping to prevent blowing. The present methods of disposing of sludges or dusts are considered inadequate because of the danger of leaching of lead and zinc.

## Ferrosilicon

<u>Dusts and Sludges</u>. Collected dust from ferrosilicon furnaces is usually trucked to on-site open dump areas. Dust is wetted down to prevent blowing from the truck while being transported. If wet emissions control is used a sludge is generated which is open dumped. Open dumping of dust or sludge is environmentally acceptable since they are not considered hazardous at this time.

## Ferrochrome

Slag. Electric furnace slag is open dumped or sold for use in road building. These practices are environmentally adequate since solubility tests indicated that ferrochrome furnace slag is non-hazardous at this time.

Dusts and Sludge. Either dusts or scrubber water is generated from emissions control on ferrochrome electric furnaces depending on the method of air pollution control practiced. Dusts are open dumped while scrubber waters are put in unlined lagoons with periodic dredging of settled sediments. Dredged sediments are open dumped. Current practices of dust and sludge disposal are considered inadequate because of the possibility of chrome and lead leaching.

## Ferronickel

Slag. Granulated slags from reduction furnaces are presently open dumped. This practice is adequate since ferronickel slag is not considered hazardous at this time.

Skull Plant Tailings. Skull plant tailings are currently open dumped. This practice is not considered adequate because of evidence of zinc and copper leaching at approximately 50 ppm in solubility tests.

Sludges. Sludges result from settling of slag granulation water and skull plant tailing water in an unlined lagoon. The sludges are dredged from the lagoon and open dumped. The sludge from slag granulation is not considered potentially hazardous while that from skull plant tailings is considered potentially hazardous. Since they accumulate in the same lagoon, the entire sludge volume must be considered hazardous at this time and the use of an unlined lagoon as not acceptable.

<u>Dust</u>. The only land disposed dust from ferronickel production is the emission control dust from the associated ferrosilicon furnace. This dust is open dumped on land, an environmentally acceptable practice since ferrosilicon dust is not considered potentially hazardous at this time.

Levels of treatment and disposal technology for those ferroalloy wastes which are considered potentially hazardous are discussed in the following sections.

## 3.3.2 Present Treatment and Disposal Technology (Level I)

## Ferromanganese and Silicomanganese

Sludges and Dust. Lime treated scrubwater from ferromanganese furnace emissions controls and wet scrubber sludge from silicomanganese emissions control is settled in lagoons or settling basins. Settled sediments are dredged and open dumped. Dusts are either open dumped directly or wetted before open dumping. These practices are inadequate because of the possibility of heavy metal leaching and subsequent percolation through permeable soils to groundwater.

## Ferrochrome

Dusts and Sludges. Dusts are open dumped and scrubber waters are settled in unlined lagoons with periodic dredging of settled sediments. Dredged sediments are open dumped. These practices are inadequate because of the possibility of heavy metal leaching and subsequent percolation through permeable soils to groundwater.

## Ferronickel

Skull Plant Tailings. Skull plant tailings are presently open dumped. This is not adequate since solubility tests indicate leaching of zinc and copper which could percolate through permeable soils to groundwater.

Sludges. Sludges from skull plant tailings water accumulates in a lagoon along with sludge from slag granulation water. Sludge is periodically dredged and open dumped. The lagoon is unlined. The use of an unlined lagoon and open dumping of dredged sludge are considered inadequate because of the danger of heavy metal leaching through permeable soils to groundwater.

## 3.3.3 Best Technology Currently Employed (Level II)

### Ferromanganese and Silicomanganese

Sludges and Dusts. Level II technology is the same as Level I (i.e. open dumping of dust and dredged sludge).

## Ferrochrome

Dusts and Sludges. Level II technology is the same as Level I (i.e. open dumping of dust and dredged sludge).

## Ferronickel

Skull Plant Tailings. Level II technology is the same as Level I (i.e. open dumping).

Sludges. Level II technology is the same as Level I (i.e. lagoon settling and open dumping of dredged sludge).

3.3.4 <u>Technology To Provide Adequate Health And Environmental</u> Protection (Level III)

## Ferromanganese and Silicomanganese

Sludges and Dust. The use of lined lagoons would be required for settling of sludges. Dredged sludges would need chemical fixation before dumping on land to prevent heavy metal leaching. Ground upon which dusts are disposed would require soil sealing to prevent percolation of potentially hazardous constituents.

## Ferronickel

Skull Plant Tailings. The ground area for disposal of skull plant tailings would require sealing with bentonite or other sealant to prevent percolation of leachate. Runoff water would be collected and diverted to the lagoon.

Sludges. The lagoon receiving sludge from the skull plant tailings pile and slag granulation would require a lining. Dredged lagoon sediments would be dried and disposed of in sealed soil areas.

Tables 20a through 20e summarize features of Levels I, II and III treatment and disposal technology for those wastes from the ferroalloy industry which are considered potentially hazardous at this time.

## 3.4 COST ANALYSIS

In the last section, various treatment and disposal technologies currently employed or considered for adequate health and environment protection were described. The costs for implementing this technology for typical plants is considered in this section. Costs are given separately for plants producing ferromanganese and silicomanganese, ferrosilicon, ferrochrome, and ferronickel.

Table 20a

Treatment and Disposal Technology Levels

Smelting and Refining Category Ferromanganese SIC 3313

## Sludge

Factor Physical + Chemical Properties	Level I (Prevalent) Colloidal to silt size particles; lime, silica, iron	Level II (Best Available) Same as I	Level III (Adequate Health and Enviro- mental Protection) Same as I
Hount of Waste (kg/MT Product)	150.6	Same as I	Same as I
Fac <b>tors</b> Affecting Haz <b>ar</b> dousness	Contains trace heavy metals including $Cz$ , $Cu$ , $Pb$ , $2n$	Same as I	Same as I
Treatment/ Disposal Technology	Sludge - lagoons with dredged material open dumped	Same as I	Sludge - lines lagoon with chemical fixation of sludge
Estimate of # + % of Plants Using Technology	>75%	>75%	0

	Level III	Adequate	None	Ncne	Compatible	Groundwater and surface runoff monitoring	Negligible
Table 20a - (cont'd.)	Level II	Same as I	Same as I	Same as I	Compatible	Same as I	Negligible
	Level I	Inadequate	Lead and zinc leached in solubility tests	Possible contamination of ground or surface water	Compatible	None	Negligible
	Factor	Adequacy of Technology	Problems and Comments	Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

Table 20b

Treatment and Disposal Technology Levels

Smelting and Refining Category Silicomanganese SIC 3315

## Scrubber Sludge

Level III (Adequate Health and Enviromental Protection) Same as I	Same as I	Same as I	Lined lagoons and chemical fixation if heavy metals leached	0
Level II (Best Available) Same as I	Same as I	Same as I	Same as I	>75\$
Level I (Prevalent) Colloidal to silt size particles; silica, iron, magnesium, manganese	985	Contains trace heavy metals including Cr, Cu, Pb, Zn, Mn	Lagooned with dredged material open dumped	>75 <b>%</b>
Factor Physical + Chemical Properties	H Amount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment/ Disposal Technology	Estimate of # + % of Plants Using Technology

		Level III	Adequate	None	None	Compatible	Groundwater surveillance wells, surface runoff monitoring	Negligible
•	Table 20b (Cont.)	Level II	Same as I	Same as I	Same as I	Compatible	None	Negligible
		Level I	Inadequate if heavy metals are significantly leached	Lead leached in solubility tests	Possible contamination of ground or surface water	Compatible	None	Negligible
•		Factor	Adequacy of Technology	Problems and Comments	U Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

Table 20c

Treatment and Disposal Technology Levels

eg eg
3
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Dust

Level III (Adequate Health and Enviro- mental Protection)	Same as I	Same as I	Same as I	Dust - land sealing and diversion of runoff if heavy metals leach significantly Sludge - lined lagoons and chemical fixation if heavymetals leach	significantly 0
Level II (Best Available)	Same as I	Same as I	Same as I	Same as I	>75%
Level I (Prevalent)	Dust-colloidal to silt size particles Sludge-colloidal to silt size particles	Dust - 168 Sludge - 146	Presence of heavy metals including Cr, Cu, Pb, Zn, Mn	Dust - open dumped  Sludge - unlined lagoon with dredged sediments dumped on land	>75%
Factor	Physical - Chemical Properties	Nount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment Disposal Technology	Estimate of # + % of Plants Using Technology

<sup>\*</sup>Dust from dry air pollution control system; sludge from wet air pollution control system.

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Level III	Adequate	None	None	Compatible	Groundwater surveillance wells, surface runoff monitoring	Negligible
Level II	Same as I	Same as I	Same as I	Compatible	Same as I	Negligible
Level I	Inadequate if heavy metals are significantly leached	Chrome and lead leached from dust in solubility tests	Possible contamination of ground or surface water	Compatible	None	Negligible
Factor	Adequacy of Technology	Problems and Comments	15 Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

Table 20d

Treatment and Disposal Technology Levels

Smelting and Refining Category Ferronickel SIC 3313

## Skull Plant Tailings

Level III (Adequate Health and Enviro-	Mental Protection) Same as I	Same as I	Same as I	Ground sealing and diversion of runoff if heavy metals leached	0
Level II (Best Available)	Same as I	Same as I	Same as I	Same as I	1 (100%)
Level I (Prevalent)	Sand to gravel size, lime, magnesium, iron, silica	5,300	Presence of heavy metals including Co, Cr, Cu, Zn, Mn, Ni	Open dump	1 (100%)
Factor	Physical + Chemical Properties	S Amount of Waste (kg/MT Product)	Factors Affecting Hazardousness	Treatment/ Disposal Technology	Estimate of # + % of Plants Using Technology

	Level III	Adequate	None	None	Compatible	Groundwater surveillance wells, surface runoff monitoring	Negligible
Table 20d (Cont.)	Level II	Same as I	Same as I	Same as I	Compatible	Same as I	Negligible
	Level I	Inadequate if heavy metals are significantly leached	Copper and zinc leached in solubility tests	Possible contamination of ground or surface water	Compatible	None	Negligible
	Factor	Adequacy of Technology	Problems and Comments	S Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

Table 20e

## Treatment and Disposal Technology Levels

# Smelting and Refining Category Ferronickel SIC 3313

Sludge from Slag Granulation Water and Skull Tailings Water

Factor	Level I (Prevalent)	Level II (Best Available)	Level III (Adequate Health and Enviro-
Physical + Chemical Properties	Silt to sand size particles; silica, iron	Same as I	mental Protection) Same as I
The state of Waste (kg/MT Product)	576	Same as I	Same as I
Factors Affecting Hazardousness	Presence of trace metals including Co, Cr, Cu, Zn, Mn, Ni	Same as I	Same as I
Treatment/ Disposal Technology	Unlined lagoon with dredged sludge dumped on land	Same as I	Lined lagoons with sealing of sludge disposal area
Estimate of # + % of Plants Using Technology	1 (100%)	1 (100%)	0

Level III	Adequate	None	None	Compatible	Groundwater surveillaspce Wells, surface runoff monitoring	Negligible
Level II	Same as I	Same as I	Same as I	Compatible	None	Negligible
Level I	Inadequate if heavy metals are significant leached	Solubility tests indicate that sludge from skull plant tailings will leach copper and zinc	Possible contamination of ground or surface water	Compatible	None	Negligible
Factor	Adequacy of Technology	Problems and Comments	S Non-Land Environmental Impact	Compatibility With Existing Facilities	Monitoring & Surveillance Methods	Energy Requirements

## 3.4.1 Cost of Present Treatment and Disposal Technology (Level I)

Ferromanganese and Silicomanganese. The typical plant produces 81,000 MT of ferromanganese and 25,400 MT of silicomanganese operating about 345 days/year.

Effluents from both operations go to a lagoon. It has a volume of 10,700 m and allows for 4 days of residence. Its design characteristics are:

		3
Volume	10,700	m
Bottom width	38	m
Top width	50	m
Bottom length	75	m
Top length	87	m
Total depth	3	m
Depth of excavation	1.15	
Circumference	286 3,546	m,
Dike volume	3,546	ma
Dike surface	3,921	m <sup>2</sup>
Total width	63	m
Total length	101	m
Required area	.65	ha

The daily inflow into the lagoon contains 40.6 MT of solids which form about 29 m of sludge. This requires that the lagoon is dredged about 1.9 times/yr assuming that it is dredged when half filled with sludge. This requires about 380 hours of dragline time based on a capacity of 27 m /yr of frontloader and truck time. The lagoon is located on semi-industrial land.

Scrubber water from the silicomanganese furnace flows through a concrete-lined settling pit before entering the lagoon. The pit is sized to allow a settling time of 30 minutes. About 38.7 Mi of solids are removed weekly from the pit and trucked to the on-site dump. This operation is estimated to require 80 hours of truck and backhoe time/yr.

Capital and annual costs of Level 1 treatment and disposal technology are given in Table 21.

Ferrochrome. The selected plant produces 62,790 MT of ferrochrome/year operating 345 days. Two types of wastes are generated. One is furnace slag (non-hazardous) which is open dumped or sold for use in road building. The other consists of wastes collected by air emission control systems considered hazardous. Both dry and wet systems are employed for handling the latter waste, and costs are developed for both systems.

TABLE 21

COST OF LEVEL I TREATMENT AND DISPOSAL TECHNOLOGY
FERROALLOYS - FERROMANGANESE AND SILICOMANGANESE

C.	ar	οi	t	a l	Co	st

		Sludge
Lagoon		
Site Preparation		
Survey		\$ 375
Test Drilling		490
Sample Testing		250
Report Preparation		1,200
Construction		2,200
Excavation & Forming		4,715
Compacting		6,560
Fine Grading		1,765
Soil Poisoning		355
Transverse Drain Fields		580
Land		2,570
Sump		3,870
Equipment		
Truck (1.1)		8,250
Front Loader (1.1)		6,600
Dragline (20%)		14,000
Bulldozer (30%)		2,305
Dump		
Survey		1,350
Land		8,545
	TOTAL	\$63,780

## TABLE 21 (Cont.)

## Annual Cost

		Sludge
Land		\$ 1,110
Amortization Construction		
Equipment		2,495 4,955
Operating Personnel		20,110
Repair and Maintenance		
Construction		53\$
Equipment		1,560
Energy		
Fue1		2,310
Electricity		230
Taxes		280
Insurance		
(Slag Sale)		640
	TOTAL	\$34,225

The dry system results in the collection of 15.7 MT of dust/day with a density of 500 Kg/m. The dust is transported to an ensite dump, which requires 2 hrs/day of frontloader and truck time.

In the wet system, the scrubber water is piped to a lagoon. The lagoon, like all other waste disposal facilities is assumed located on semi-industrial land. Inflow into the lagoon is at a rate of 80 l/sec. The lagoon size allows for 4 days detention. Its characteristics are:

		3
Volume	27,650	m
Bottom width	63	m
Top width	75	m
Bottom length	126	m
Top length	138	m
Total depth	3	m
Depth of excavation	.85	m
Circumference	438	m,
Dike volume	6,872	m
Dike surface	6,282	m <sup>2</sup>
Total width	90	m
Total length	153	m
Required area	1.4	ha

About 15.2 MT of solids settle in the lagoon daily which form 12.7 m of sludge. Dredging is required only once every three years. On the average, 4,150 m of sludge are dredged annually which represents 220 hours of frontloader and truck time.

The sludge dump is designed to accommodate lagoon sludge dredged over a 20-year period.

Capital and annual costs of Level I treatment and disposal technology are given in Table 22.

Ferrosilicon. Since there are no hazardous wastes believed associated with ferrosilicon production at this time, there are no costs associated with hazardous waste treatment and disposal.

Ferronickel. The model plant produces 23,600 MT of ferronickel operating 365 days/year. Ferrosilicon required for the reduction of nickel is produced in the same plant at a rate of about 20,620 MT/yr. The only wastes associated with ferronickel production which is believed hazardous is skull plant tailings and associated sludge.

Tailings from the skull plant are piped to a tailings pile. Solids accumulate at a rate of about 360 MT/day. The water from the tailings slurry drains into a lagoon which also receives water and solids from slag granulation. The tailings have an estimated density of 1,300 kg/m $^3$ . Thus, about 275 m $^3$  of solids form daily and 100,375 m $^3$  annually. The accumulation over a 20-year period amounts to about 2,000,000 m $^3$ . This will require a 7 ha area given that the tailings are built-up to a height of 30 m.

TABLE 22

COST OF LEVEL I TREATMENT AND DISPOSAL TECHNOLOGY

FERROALLOYS - FERROCHROME PLANT - DRY COLLECTION SYSTEM

## Capital Cost

		Dust
Equipment		
Truck (35%)		\$ 8,750
Front Loader (35%)		7,000
Bulldozer (5%)		1,000
Dump		
Survey		1,380
Land		8,740
	TOTAL	\$26,870

## Annual Cost

		Dust	
Land		\$	875
Amortization			
Construction			160
fiqui p <b>ment</b>		2	<b>,</b> (s6's
Operating Personnel		10	, 265
Repair and Maintonance			
Construction			
Equipment			840
Energy			
Fue1		2	,000
Electricity			200
Taxes			220
Insurance			270
	TOTAL	\$23	,495

## TABIL 22 (Cont.)

## FERROCHROME PLANT - WET COLLECTION SYSTEM

## Capital Cost

		Sludge
Lagoon		
Site Preparation		
Survey		\$ 875
Test Drilling		980
Sample Testing		500
Report Preparation		1,500
Construction		
Excavation & Forming		9,140
Compacting		12,715
Fine Grading		2,825
Soil Poisoning		545
Transverse Drain Fields		2,070
Land		5,535
Equipment		
Truck (10%)		2,500
Front Loader (10%)		2,000
Bulldozer (1%)		200
Drag Line (10%)		7,000
Dump		
Survey		505
Land		3,230
	TOTAL	\$52,120

## TABLE 22 (Cont.)

## Annual Cost

		Sludge	
Land		\$ 875	
Amortization Construction Equipment		3,670 1,860	
Operating Personnel		7,145	
Repair and Maintenance Construction Equipment		820 585	
Energy Fuel Electricity		820 80	
Taxes		220	
Insurance		520	
	TOTAL	\$16,595	

Solids carried into the settling lagoons accumulate at an estimated rate of 13,600 MT/yr. The sludge formed has a wet density of 1,260 Kg/m $^3$  and a dry density of 1,390 Kg/m $^3$ . Most of the solids settle in the first of two lagoons (Lagoon A). The overflow from Lagoon A goes to the second lagoon (Lagoon B). The characteristics of the lagoons are:

	1.16,3011	Δ	Lagoon	В
Volume	პი, <b>0</b> 60	<sub>m</sub> 3	95,000	$m^3$
Bottom width	1.79		152	
Top width	147	m	160	m
Bottom length	278	m	304	m
Top length	236	m	312	m
Circumference	879	m	955	m
Depth	2	ın		m
Depth of excavation	.25	m z	.25 10,863	m z
Dike volume	9,990	$m_2^3$	10,863	$m_2^2$
Dike surface	9,893	m <sup>2</sup>	10,758	m <sup>2</sup>
Total width	160	m	173	m
Total length	299	m	325	m
Required area	4.8	ha	5.6	ha

Lagoon A is dredged once per year at which time about  $10,800 \text{ m}^3$  of sludge is removed. This requires about 400 hours of dragline time. The sludge is then deposited on adjacent land. The transport is estimated to require 520 hours of frontloader and truck time annually.

In a dry state, sludge removed amounts to  $9,785 \text{ m}^3/\text{yr}$  or  $195,700 \text{ m}^3$  in 20 years. This will require a 2 ha area if the built-up is to 10 m.

All dust except those from the ferrosilicon furnace are recycled. The latter are not considered hazardous and therefore have no hazardous waste disposal costs attributed to their disposal.

Altogether, about 680,000 m<sup>3</sup> of solids are deposited on land each year. This is estimated to require 6,800 hrs of bulldozer time yearly for spreading, shaping and compacting. Capital and annual costs of Level I treatment and disposal technology are given in Table 23.

## 3.4.2 Cost of Best Technology Currently Employed (Level II)

Ferromanganese and Silicomanganese. Technology and costs for Level II are the same as those for Level I.

 $\overline{\text{Ferrochrome}}$ . Technology and costs for Level II are the same as those for Level I.

Ferronickel. Technology and costs for Level II are the same as those for Level I.

## TABLE 23

## COST OF LEVEL I TREATMENT AND DISPOSAL TECHNOLOGY

## FERROALLOYS - FERRONICKEL PLANT

## Capital Cost

	Sludge	Tailings
Lagoon A		
Site Preparation		
Survey	\$ 3,000	
Test Drilling	900	
Sample Testing	250	
Report Preparation	1,500	
Construction	,	
Excavation & Forming	13,285	
Compacting	18,480	
Fine Grading	4,450	
Soil Poisoning	1,090	
Transverse Drain Fields	6,625	
Land	8,400	
Lagoon B		
Site Preparation	7 500	
Survey Test Drilling	3,500 900	
•	250	
Sample Testing Report Preparation		
Construction	1,500	
	14 450	
Excavation & Forming	14,450 20,095	
Compacting Fine Grading	4,840	
Soil Poisoning	1,185	
Transverse Drain Fields	7,960	
Land	9,800	
Land	3,000	
Tailing's Dump		
Survey		4,375
Land		12,250
Sludge Dump		
Survey	1,250	
Land	3,500	
	,,,,,,	
Equipment		
Truck (35%)	6,565	
Front Loader (35%)	3,230	
Bulldozer (55%)	545	7,615
Belt Conveyor	شعيد المام	
Dragline (20%)	14,000	
TOTAL	\$153,390	\$24,240
134	**************************************	

## TABLE 23 (Cont.)

## Annual Cost

		Sludge	Tailings
Land		\$ 2,170	\$ 1,225
Amortization			
Construction		12,220	510
Equipment		4,190	1,210
Operating Personnel		16,920	11,565
Repair and Maintenance			
Construction		2,775	-
Equipment		1,320	<b>3</b> 80
Energy			
Fue 1		1,945	915
Electricity		195	90
Taxes		545	305
Insurance		1,535	240
	TOTAL	\$43,815	\$16,440

## 3.4.3 Cost of Technology to Provide Adequate Health and Environmental Protection (Level III)

Ferromanganese and Silicomanganese. The lagoon is lined and the accumulated sludge is removed by pumping instead of dredging. The sludge is chemically fixed prior to being deposited at the slag dump. The slurry pump is operated about 720 hrs/yr, and 1,000 labor hours are assigned for its operation. The use of the slurry pump eliminates the use of the dragline.

Capital and annual costs are given in Table 24.

Ferrochrome. The lagoon is lined, and the sludge or slurried dust is removed by pumping instead of dredging. The sludge is chemically fixed prior to being deposited at the dump. The dump surface is sealed and collection ditches installed, together with a pump and piping. The slurry pump is operated about 300 hrs/yr and 450 hrs are assigned for its operation. The use of the slurry pump eliminates use of the dragline. Capital and annual costs are given in Table 25.

Ferronickel. Both lagoons are lined and the accumulated sludge is removed from Lagoon A by pumping instead of dredging. The slurry pump used for this purpose is operated about 765 hrs/yr and 1,000 labor hours are assigned for its operation. The use of the slurry pump eliminates the need for the dragline.

The pumped sludge is deposited on a sealed .25 hectare area adjacent to Lagoon A for drying. The runoff is collected in ditches and then flows by gravity into Lagoon B. The dried sludge is then hauled to dump where the ground has been sealed.

The tailings from the skull plant are deposited on sealed ground and collection ditches are constructed at the dump site. The capital and annual costs of Level III treatment and disposal technology are given in Table 26.

Tables 27 through 29 summarize the capital and annual costs for Levels 1, II and III treatment and disposal technologies for hazardous land disposed waste from the U.S. ferroalloys industry. Costs are given per metric ton of dry and wet wastes (i.e. sludges) and per metric ton of product. Cumulative total industry costs for each ferroalloy sector to meet Levels I, II and III treatment and disposal technology are also given. Costs for each type of waste and total costs for each ferroalloy sector are also expressed as percentages of product selling prices.

Estimated 1973 annualized industry costs for Levels I and II treatment and disposal technology of potentially hazardous wastes from ferromanganese and silicomanganese production are \$250,000 or 0.2% of estimated national sales value. The industry cost of Level III treatment and disposal technology (adequate for environmental protection) is estimated as \$1,310,000 or 0.8% of estimated national sales value.

## COST OF LEVEL III TREATMENT AND DISPOSAL TECHNOLOGY

## FERROALLOYS - FERROMANGANES AND SILICOMANGANESE PLANT

## Capital Cost

		Sludge
Construction Lagoon Liner		\$21,440
Equipment Slurry Pump Piping, Flexible (Dragline)		13,730 440 (14,000)
	FOTA	\$21,610

#### Annual Cost

		Sludge
Land		-
Amortization Construction Equipment (1)		\$ 2,485 25
Operating Personnel (1)		4,835
Repair and Maintenance Construction Equipment (1)		6 <b>45</b> 10
Energy Fuel (1) Electricity		(435) 15
Taxes		-
Insurance (1)		215
Chem. Fixation		134,180
	TOTAL	\$141,975

<sup>(1)</sup> Costs shown are net costs, i.e. costs of new equipment less dragline associated costs which are no longer incurred.

TABLE 25

## COST OF LEVEL III TREATMENT AND DISPOSAL TECHNOLOGY

## FERROALLOYS - FERROCHROME PLANT

# Capital Cost

		Sludge
Construction Lagoon Liner		\$47,630
Equipment Slurry Pump Pipe, Flexible (Dragline)		13,730 440 (7,000)
	TOTAL	\$54,800

### Annual Cost

		Sludge
Land		~
Amortization Construction Equipment (1)		\$ 5,525 1,140
Operating Personnel (1)		2,370
Repair and Maintenance Construction Equipment (1)		1,430 360
Energy Fuel (1) Electricity		(175) 10
Taxes		-
Insurances (1)		550
Chem. Fixation		54,780
	TOTAL	\$65,990

<sup>(1)</sup> Costs shown are net costs, i.e. costs of new equipment less dragline associated costs which are no longer incurred.

TABLE 26

# COST OF LEVEL 111 TREATMENT AND DISPOSAL TECHNOLOGY

## FERROALLOYS - FERRONICKEL PLANT

# Capital Cost

		Sludge	Tailings
Construction			
Lagoon (A) Liner		\$180,080	
Lagoon (B) Liner		212,655	
Equipment			
Slurry Pump		13,730	
Piping, Flexible		440	
Sludge Drying Area			
Land Sealing		5,000	
Collection Ditches		760	
Pipe Rigid		1,730	
Dumps			
Survey			
Land			
Land Sealing		40,000	140,000
Collection Ditches		2,145	4,010
Pump and Piping		11,140	18,210
	TOTAL	\$453,680	\$162,220

# TABLE 26 (Cont.)

# Annual Cost

		Sludge	Tailings
Land		-	-
Amortization Construction Equipment		\$51,115 2,075	\$16,705 2,895
Operating Personnel		4,590	-
Repair and Maintenance Construction Equipment		13,220 650	4,320 910
Energy Fuel Electricity		(455) 95	- 325
Taxes		where	_
Insurance		4,535	1,620
	TOTAL	\$75,825	\$26,775

TABLE 27. SUMMARY COSTS - FERROMANGANESE AND SILICOMANGANESE

Anr	Annual Froduction:	Model Plant		81,000/25,400 MT	,	Indust	Industry 620,977/167,002 MT	/167,002	MT	
	Waste (Type)	ype)		Amount (	Amount (MT/MT of Production)	Producti	ou)			
	Sludge	ø)		0.15 (Avg.)	(8.)					
Cu	Cum. Unit Waste Disposal Costs:	posal Cost	;;l			[ 9.79.]				
Was	Waste (Type)	\$/MT of Waste	H	\$/MT of Prod.	\$/MT of Waste	11	\$/MT of Prod.	\$/MT of Waste	111	\$/MT of Prod.
Slu	Sludge	Dry	Wet		Dry	Wet		Dry	Wet	
141	Capital Cost Annual Cost Total Capital Cost Total Annual Cost	\$4.00 2.15	\$1,60	\$0.60 0.32 0.60 0.32	\$4.00 2.15	\$1.60 0.86 	\$0.60 0.32 0.60 0.32	\$5.36 11.06	\$2.14	\$0.80 1.66 0.80 1.66
Cur	Cum. Industry Waste Disposal		Costs (\$ Million)	Million) Level	rg.					
¥a.s	Waste (Type)	h		II			III			
	Sludge	Cap. \$0.47	Ann. \$0.25	Cap.	Ann. \$0.25	Cap.	Ann. \$1.31			
	Total	0.47	0.25	0.47	0.25	0.63	1.31			
197	1973 Metal Price:	\$199.20/MT	[ (avg.)							
Per	Percent Treatment Cost/Price of Metric Ton of Production	ost/Price	of Metric	Ton of Pro	duction					
				Level	1,					
Was	Waste (Type)	I Cap.	Ann.	II Cap.	Ann.	Cap.	III Ann.			
Slu	Studge	0.3%	0.2%	0.3%	0.2%	0.4%	0.8%			
	Total	0.3	0.2	0.3	0.2	0.4	0.8			

TABLE 28. SUMMARY COSTS - FERROCHROME

Annual Production:	Model Plant	t 62,790 MT	MT (	Industry	7 426,846 MT	46 MT			
Waste (Type)	ype)		Amount (	Amount (MT/MT of Production)	roduction	1)			
Sludge	e.		0.08						
Cum. Unit Waste Disposal Costs:	posal Costs:				Level				
Waste (Type)	\$/MT of Waste	H	\$/NT of Prod.	\$/MT of Waste	11	\$/MT of Prod.	\$/MT of Waste	III	\$/MT of Prod.
Sludge Capttal Cost Annual Cost	bry \$9.91 3.15	Wet \$3.96 1.26	\$0.83 0.26	bry \$9.91 3.15	Wet \$3.96 1.26	\$0.83 0.26	bry \$20.33 15.70	Wet \$8.13 6.28	\$1.70 1.32
Cum. Industry Waste Disposal	Disposal Co	sts (\$ Million)	illion)						
			Level	<b>=</b>					
Waste (Type)	Ι		II			111			
	Cap.	Ann.	Cap.	Ann.	Cap.	Am.			
Sludge	\$0.35	\$0.11	\$0.35	\$0.11	\$0.73	\$0.56			
1973 Metal Price:	\$365.20/MT								
Percent Treatment Cost/Price of	ost/Price of		Metric Ton of Production	duction					
			Level	-					
Waste (Type)	H		II			III			
	Cap.	Ann.	Cap.	Ann.	Cap.	Ann.			
Sludge	0.23%	0.07%	0.23%	0.07%	0.47%	0.36%			

TABLE 29. SUMMARY COSTS - FERRONICKEL

Annual Production: Model Plant	Model Plant	23,600 NT	Tiv -	Industry	23,600	Industry 23,600 MT (est.)			
Waste (Type)	ype)		Arount	(MT/MT of Production)	roduction	n)			
Sludge Tailings	e ngs		0.58						
Cum. Unit Waste Disposal Costs:	posal Costs:								
					revel				
Waste (Type)		-			II			III	
	\$/MT of Waste		S/Mf of Prod.	\$/NT of Waste		\$/MT of Prod.	\$/MT of Waste		\$/MT of Prod.
Sludge	Dry	Wet		Dry	Wet		Dry	Wet	
[8]		\$4.51	\$6.50	\$11.28	\$4.51	\$6.50	\$44.63	\$7.85	\$25.72
Annual Cost Tailings	3.22	1.29	1.86	3.22	1.29	1.86	8,80	3.52	5.07
	0.18	;	1.03	0.18	1	1.03	1.42	\$ <b>8</b>	7 90
Annual Cost	0.13	;	0.70	0.13	;	0.70	) (F)		2000
Total Capital Cost	i	!	7.53	;	i	7.53		į	
Total Annual Cost	;	;	2.56	i i	;	2.56	! ! 5	i i	23.55
Cum. Industry Waste Disposal	- 1	Costs (\$ Million)	llion)						
			Level	T (					
Waste (Type)	<b></b>		II			III			
Sludge Tailings	Cap. \$0.15 0.02	Ann. \$0.04 0.02	Cap. \$0.15 0.02	Ann. \$0.04 0.02	Cap. \$0.61	Ann. \$0.12			
Total	0.17	90.0	0.17	90.0	0.80	0.16			
1973 Metal Price: \$	\$1,430/MT:(est)	t)							
Percent Treatment Cost/Price	- 1	Metric T	of Metric Ton of Production	duction					
			Level	-					
Waste (Type)	H		II			Iti			
	Cap.	Ann.	Cap.	Ann.	Cap.	Ann.			
Sludge Tailings	0,45% 0.07	0.13%	0.45%	0.13%	1.80%	0.35%			
Total	0.52	0.18	0.52	0.18	2.35	0.48			

Assuming that wet systems are used for emissions control for ferrochrome production the industry annualized costs for Levels I and II treatment and disposal technology are estimated as \$110,000 or 0.07% of estimated national sales. The industry annual cost of Level III technology using wet emissions controls is estimated as \$560,000 or 0.36% of 1973 national sales.

The estimated annual cost for Level I and II treatment and disposal technology for potentially hazardous waste from the one United States ferronickel plant is \$60,000 or 0.18% of estimated 1973 sales value. Estimated annual costs for Level III treatment and disposal technology are \$160,000 or 0.48% of estimated national sales.

#### 4.0 PRIMARY METAL PRODUCTS NOT ELSEWHERE CLASSIFIED (SIC 3399)

This SIC category includes a number of miscellaneous metal products and associated manufacturing processes including production of ferrous and non-ferrous metal powders, metal paste, and ferrous and non-ferrous nails, brads, wire and staples. Table 30 shows the geographic distribution of industries in this and category as of 1972.

Brads, nails, tacks, spire the similar items are manufactured from metal by machining, extructon and other similar processes. Solid wastes will consist principally of the absolutions, clippings and other metal remnants. These wastes are relevered for scrap and therefore do not constitute a solid or hazardous. See problem.

Metal powders are produced by a variety of processes as summarized in Table 31. The raw materials for production is either solid metal or chemical compounds of metals - generally exides of metals.

The three predominant practices for powder production are atomization, gaseous reduction and electrolysis. Atomization is the most widely employed method for manufacturing or melting metal powders, such as tin, lead, zinc, cadmium and aluminum. Atomization consists essentially in forcing a thin stream of molten metal through a small orifice and then bombarding it with a stream of compressed gas, which causes the metal to disintegrate and solidify into finely divided particles. Usually the gas stream is directed through a nozzle, partly submerged in the molten metal, in such a manner as to draw the metal up through the nozzle to the tip. Solidification of the metal occurs instantaneously upon contact with the gas stream. The product is then removed by means of a suction system and collected in baghouses or cyclone dust collectors.

Electrolytic production methods for metal powders consist of electrolytic deposition from solution and electrolytic deposition from fused salts. These methods are most suitable for manufacture of extremely pure powders of a variety of metals including copper, i.on, silver, nickel, manganese and chromium.

Gaseous reduction is employed for the manufacture of commercial quantities of iron and copper powders, the most common metal powders, and less common metal powders including nickel, cobalt, tungsten and molybdenum. Hydrogen, carbon monoxide or some other reducing gas is used to reduce metallic compounds, usually oxides, to fine metal powders.

Because either pure metal or metal oxides are used as raw materials for metal powder production there is little waste. Dust, slag or sludge residues contain high metallic content and are reprocessed. Table 32 which summarizes residual disposition for one of the largest metal powder producers in the United States illustrates the dominant practice of residual recycle.

GEOGRAPHIC DISTRIBUTION OF MISCELLANEOUS PRIMARY METAL PRODUCT MANUFACTURING FIRMS, 1972 (SIC 3399)

Geographic Area	Total No. of Establishments	No. with 20+ Employees	Value of Ind. Shipments
U.S. Total	161	101	\$341M
N.E. Region	56	35	153
New England Div.	8	7	25
Connecticut	3	3	9
Middle Atlantic Div	. 48	28	128
New York	9	5	9
New Jersey	14	8	63
Pennsylvani <b>a</b>	25	15	57
N. Central Region	55	34	91
Ohio	14	9	19
Illinois	10	5	10
S. Region	28	18	64
S. Atlantic Div.	6	3	8
E.S. Central Div.	14	9	37
Tennessee	6	4	17
W.S. Central Div.	8	6	20
W. Region	<b>)</b> )	14	33
Mountain Div.	5	4	. 9
Pacific Div.	17	10	24

Source: Census of Manufacturing 1972

TABLE 31 PRODUCTION OF METAL POWDERS

Raw material	Blate	· • • •	i Frinciple igvolved	Product
		Machining Bess mer plants Screening best man	Tearing	Mg Cu and Al alloys Au, Cu, and alloys
		Stan.p mill. Hametag mg z ** v ills		Al, Cu, and alloys Al, Cu, and alloys
		Eddy mills	Hovere working	Fo Cu
	Bolid	Grinding sponge	ĺ	Fe
		Grinding Cleavable metals	Fracturing of clea- vage planes	Bi, Sb, etc.
Metal		Grinding brittle elec- trolytic metals	Intercrystalline	Fe
		Grinding brittle metals made fine by hot was	fracturing	Ni-Fe alloys
		Atomization by air blast or steam	Spraying	Al Pb Pb alloys
	Molten	Granulation by stir-	Graining	Al Pb alloys
	Vapor	Condensation at nor- mal or low pressure	Condensation	Zn, Mg
	Solid	Reduction by hydro- gen or other gases at temperatures be- low melting point	Reduction	W, Mo Ni, Co Fe Fe, Cu
		Chemical precipitation	Precipitation	Pt, Pd Sn
Chemical	Solution	Electrodeposition as a powder	Electrolysis	Cu, Fe, etc.
	(las	Carbonyl process	Thermal decomposition	Fe Ni, Ni-Fe alloys

Source: Treatise on Powder

Metallurgy, Vol. I, Interscience Publishers, NY, 1949

- TABLE 32 DISPOSITION OF RESIDUALS FROM METAL POWDER PRODUCTION

	Type of Powder	Av. Production per year	Process Type	Dust Quantity-Disposition per year	Waste Residue Sludge or Slurry Quantity-Disposition per year	Other Quantity-Dispositio
	Copper	6500 tons	Electrolytic	150 tons	50 tons	N.I.
148			Deposition	Reprocessed by Re-Cycle	Reprocessed by Re-Cycle	
	Copper Base Alloy	400 tons	Water Atomization	N:1	2 tons Reprocessed	Slag, 15 tons Reprocessed
	Tin	160 tons	Air Atomization	3 tons Reprocessed	Nil	Dross, 8 tons Reprocessed
	Solder	150 tons '	Air Atomization	3 tons Reprocessed	12.72	Dross, 20 tens Reprocessed
					,	

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