

EPA-650/4-74-008

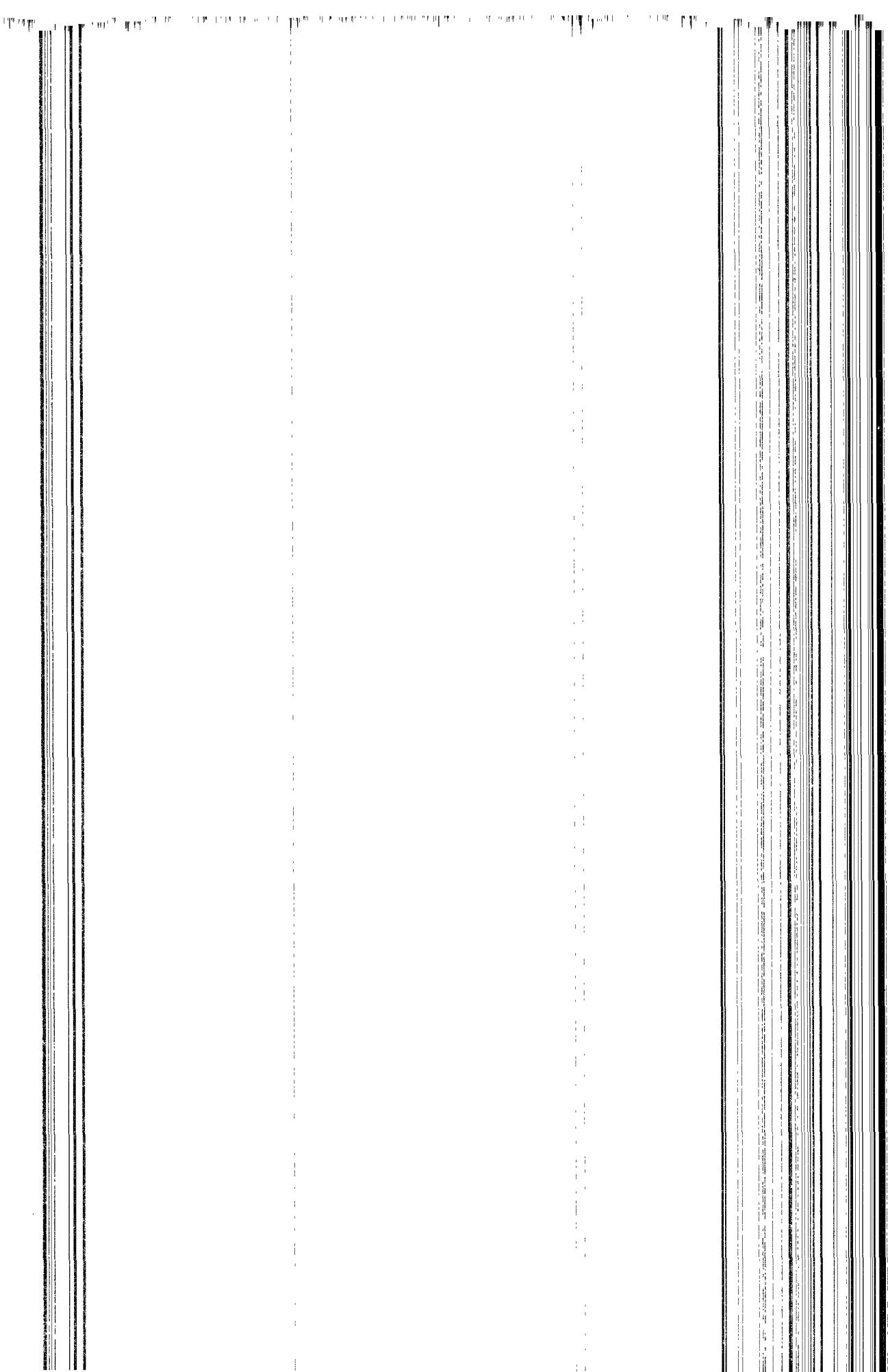
February 1975

Environmental Monitoring Series

USER'S GUIDE FOR HIWAY, A HIGHWAY AIR POLLUTION MODEL



U.S. Environmental Protection Agency
Office of Research and Development
National Environmental Research Center
Research Triangle Park, N.C. 27711



USER'S GUIDE FOR HIWAY, A HIGHWAY AIR POLLUTION MODEL

by

John R. Zimmerman
and
Roger S. Thompson

Program Element 1AA009

NATIONAL ENVIRONMENTAL RESEARCH CENTER
OFFICE OF RESEARCH AND DEVELOPMENT
U.S. ENVIRONMENTAL PROTECTION AGENCY
RESEARCH TRIANGLE PARK, N.C. 27711

February 1975

During the period in which this document was prepared, John R. Zimmerman was assigned to the Environmental Protection Agency by the National Oceanic and Atmospheric Administration, U.S. Department of Commerce.

RESEARCH REPORTING SERIES

Research reports of the Office of Research and Development, Environmental Protection Agency, have been grouped into five series. These five broad categories were established to facilitate further development and application of environmental technology. Elimination of traditional grouping was consciously planned to foster technology transfer and a maximum interface in related fields. The five series are:

1. Environmental Health Effects Research
2. Environmental Protection Technology
3. Ecological Research
4. Environmental Monitoring
5. Socioeconomic Environmental Studies

This report has been assigned to the ENVIRONMENTAL MONITORING series. This series describes research conducted to develop new or improved methods and instrumentation for the identification and quantification of environmental pollutants at the lowest conceivably significant concentrations. It also includes studies to determine the ambient concentrations of pollutants in the environment and/or the variance of pollutants as a function of time or meteorological factors.

EPA REVIEW NOTICE

This report has been reviewed by the Office of Research and Development, Environmental Protection Agency, and approved for publication. Approval does not signify that the contents necessarily reflect the views and policies of the Environmental Protection Agency, nor does mention of trade names or commercial products constitute endorsement or recommendation for use.

DISTRIBUTION STATEMENT

This report is issued by the Environmental Protection Agency to report technical data of interest to a limited number of readers. Copies are available free of charge to Federal employees, current contractors and grantees, and non-profit organizations--as supplies permit--from the Air Pollution Technical Information Center, Environmental Protection Agency, Research Triangle Park, North Carolina 27711. Document is available to the public, for a fee, through the National Technical Information Service, 5285 Port Royal Road, Springfield, Virginia 22161.

Publication No. EPA-650/4-74-008

ABSTRACT

A computer model, called HIWAY, that can be used for estimating the concentrations of nonreactive pollutants from highway traffic is described. This steady-state Gaussian model can be applied to determine air pollution concentrations at receptor locations downwind of "at-grade" and "cut-section" highways located in relatively uncomplicated terrain. For an at-grade highway, each lane of traffic is modeled as though it were a finite, uniformly emitting line source of pollution. For the cut section, the top of the cut is considered an area source. The area source is simulated by using ten line sources of equal source strength. The total source strength equals the total emissions from the lanes in the cut.

The air pollution concentration representative of hourly averaging times at a downwind receptor location is found by a numerical integration along the length of each lane and a summing of the contributions from each lane. With the exception of receptors directly on the highway or within the cut, the model is applicable for any wind direction, highway orientation, and receptor location. The model was developed for situations in which horizontal wind flow occurs. The model cannot consider complex terrain or large obstructions to the flow such as buildings or large trees.

An interactive version of the computer model is available on the Environmental Protection Agency's Users' Network for Applied Modeling of Air Pollution (UNAMAP).

PREFACE

HIWAY is one of the atmospheric dispersion models on both of the UNAMAP (Users' Network for Applied Modeling of Air Pollution) systems. One of these systems is restricted to Environmental Protection Agency users. The other system is available to non-EPA users. The systems are accessed through phone lines and time-share computer terminals. For information on accessing UNAMAP contact: Chief, Data Management, Meteorology Laboratory, U.S. Environmental Protection Agency, Research Triangle Park, N. C. 27711.

Although attempts are made to thoroughly check out computer programs with a wide variety of input data, errors are found occasionally. In case there is a need to correct, revise, or update this model, revisions will be distributed in the same manner as this report. If your copy was obtained by purchase or special order, you may obtain revisions as they are issued by completing the mailing form on the following page. A user can be assured that the latest version of HIWAY is on the UNAMAP system.

Comments and suggestions regarding this document should be directed to Chief, Environmental Applications Branch, Meteorology Laboratory, EPA, Research Triangle Park, N. C. 27711.

ACKNOWLEDGMENTS

The authors greatly appreciate the assistance of Adrian Busse, Lea Prince, Susan Godfrey, and Karl Zeller.

Chief, Environmental Applications Branch
Meteorology Laboratory
U.S. Environmental Protection Agency
Research Triangle Park, N. C. 27711

I would like to receive future revisions to *User's Guide for HIWAY, A Highway Air Pollution Model*. I do not receive EPA documents through the regular mailing list.

Name _____

Address _____

_____ ZIP _____

CONTENTS

<u>Section</u>	<u>Page</u>
LIST OF TABLES	viii
LIST OF FIGURES	viii
ABBREVIATIONS AND SYMBOLS	ix
1. INTRODUCTION	1
2. DESCRIPTION OF MODEL	3
At-grade Highway	3
Cut Section	9
3. DISPERSION FUNCTIONS σ_y AND σ_z	11
4. PREPARATION OF INPUT DATA	17
Card Input Sequence	17
Interactive Operation	17
REFERENCES	19
GLOSSARY	21
APPENDIX A. EXAMPLE PROBLEM	23
Introduction	24
Solution Using the Interactive Version	24
Solution Using the Batch Version	26
APPENDIX B. FORTRAN SOURCE PROGRAM LISTING FOR BATCH VERSION OF HIWAY	35
TECHNICAL REPORT DATA AND ABSTRACT	59

LIST OF TABLES

<u>Table</u>		<u>Page</u>
1	Pasquill Stability Classes	11
2	Values of c and d Used to Calculate θ_p	12
3	Values of g and h Used to Determine σ_z for Downwind Distances Less Than 0.1 km	13
4	Virtual Distances a and b Corresponding to Initial σ_z of 1.5 meters and Initial σ_y of 3.0 meters, Respectively	15
5	Input Data Cards	18
A-1	Example of Interactive Version of HIWAY	27
A-2	Card Input for Example Problem	32
A-3	Example of Batch Version of HIWAY	33

LIST OF FIGURES

<u>Figure</u>		<u>Page</u>
1	Overhead View of the Geometry of an At-grade Highway as Seen by the Computer Model	4
2	Line Source and Receptor Relationships	5
3	Method of Simulating Dispersion from a Cut Section	10
4	Data Points Used to Determine an Estimate of Initial σ_z	14

ABBREVIATIONS AND SYMBOLS

ABBREVIATIONS

EPA	U.S. Environmental Protection Agency
g	grams
hr	hours
km	kilometers
m	meters
mi	miles
sec	seconds
UNAMAP	Users' Network for Applied Modeling of Air Pollution
veh	vehicles

SYMBOLS

A	end point of line source
a	virtual distance for initial σ_z , km
B	end point of line source
b	virtual distance for initial σ_y , km
C(p)	concentration at the perpendicular distance, p, g m^{-3}
c	term to determine θ_p , dependent upon stability, degrees
d	factor to determine θ_p , dependent upon stability, degrees
D	line source length, meters
EF	emission factor, $\text{g veh}^{-1} \text{ mi}^{-1}$
f	point source dispersion function, m^{-2}
g	factor to determine σ_z (depends upon stability and distance range), meters
H	effective source height, meters
h	exponent to determine σ_z (depends upon stability and distance range), dimensionless
L	mixing height, meters
λ	distance from point A to point R,S, meters
p	perpendicular distance of receptor from line source, meters
q_λ	emission rate from line source, $\text{g m}^{-1} \text{ sec}^{-1}$

R	east coordinate , meters
R_A	east coordinate of point A , meters
R_B	east coordinate of point B , meters
R_k	east coordinate of receptor k , meters
S	north coordinate , meters
S_A	north coordinate of point A , meters
S_B	north coordinate of point B , meters
S_k	north coordinate of receptor k , meters
TV	traffic volume , veh hr $^{-1}$
u	wind speed , m sec $^{-1}$
x	downwind distance , meters or km
x_0	normalizing distance , km
y	crosswind distance , meters or km
z	receptor height above ground , meters
β	direction , relative to north , of line from point A to point B , degrees
γ	angle between wind direction and a perpendicular to the line source , degrees
θ	wind direction , relative to north , degrees
θ_p	half angle of horizontal plume spreading , degrees
σ_y	standard deviation of the concentration distribution in the crosswind direction , meters
σ_{yo}	initial σ_y , meters
σ_z	standard deviation of the concentration distribution in the vertical direction , meters
σ_{zo}	initial σ_z , meters
x	concentration , g m $^{-3}$

USER'S GUIDE FOR HIWAY, A HIGHWAY AIR POLLUTION MODEL

1. INTRODUCTION

The National Environmental Policy Act of 1969 requires any Federally funded highway construction project to be preceded by an impact statement analyzing the effect of the proposed roadway on air quality. This report describes a computer program, called HIWAY, for calculating air quality levels of nonreactive pollutants produced by highway automotive traffic at distances of tens to hundreds of meters downwind of the highway in relatively uncomplicated terrain.

In making estimates of pollution concentrations for an "at-grade" highway, highway emissions are considered to be equivalent to a series of finite line sources. Each lane of traffic is modeled as though it were a straight, continuous, finite line source with a uniform emission rate. Air pollution concentrations downwind from a line source are found by a numerical integration along the line source of a simple Gaussian point-source plume. Although most applications of this model will be for ground-level sources and receptors, and for receptors close to the source where mixing height will have almost no effect, the more general case of nonzero source and receptor heights and inclusion of the effects of mixing height can be considered by the model.

The HIWAY model is similar to the line-source equations (5.19 and 5.20) in the *Workbook of Atmospheric Dispersion Estimates* (Turner, 1970) but can also consider finite line sources at any angle to the wind.

An estimate may also be made of air pollution concentrations downwind of a "cut section." To do this, the top of the cut section is considered to be

equivalent to an area source. This area source is simulated by using a series of ten equal line sources such that the total source strength is equal to the total pollution emissions of the highway.

No pollution emissions module is included in the batch (card input) version of the model. A value of the line-source strength, q_g ($\text{g m}^{-1} \text{ sec}^{-1}$), for each lane of traffic must be obtained from a separate computation (Beaton et al., 1972). Line-source strength is generally a function of traffic rate, average vehicle speed, and traffic mix (fraction of heavy-duty vehicles, fraction of late models with emission control devices, etc.). Data input for the HIWAY program can be accomplished in two ways: (1) through batch mode, with data cards that follow the program deck (see Section 4 for format) and (2) through continuous mode, that is, interactively on a time-share computer terminal. The term interactive refers to the information exchange between the user and the computer program in asking and answering questions.

In the interactive version of the model, to be discussed in Section 4 and Appendix A, the user can obtain a crude estimate of line-source emission rate for the pollutant carbon monoxide. If one does not enter emission rates interactively, an estimate of emission rate can be determined by entering a value for vehicle speed and traffic volume per hour for each lane of traffic. This emission rate is representative of that for 1969 model-year automobiles (Ludwig et al., 1970). According to *Compilation of Air Pollutant Emission Factors* (EPA, 1973), this emission factor of $58.7 \text{ g veh}^{-1} \text{ mi}^{-1}$ for a speed of 19.6 mi hr^{-1} is also representative of emissions for the vehicle model mix near the end of 1973. See Table 3.4.1-1 in EPA, 1973.

2. DESCRIPTION OF MODEL

AT-GRADE HIGHWAY

A view of an idealized four-lane at-grade highway is shown in Figure 1. Traffic pollution emissions from each lane are simulated in the computer model by a straight line source of finite length. As shown in Figure 1 for a four-lane highway, the location of the highway is specified by the coordinates at the centerline (from edge to edge) of the highway (points 1 and 2). The ordering of the lanes is from left to right when one looks from point 1 to point 2. One lane or any even number of lanes from 2 to 24 can be used in the model.

The width of the highway and its center strip must also be entered as input data. With this information, the computer program HIWAY will assign a finite uniform line source to each lane of traffic. These line sources are placed at the center of each traffic lane.

A uniform emission rate, q_ℓ , must be specified for each line source. This line-source emission rate can be found if the emission factor, EF ($\text{g veh}^{-1} \text{ mi}^{-1}$), and the traffic volume, TV (veh hr^{-1}), are known:

$$q_\ell (\text{g sec}^{-1} \text{ m}^{-1}) = \frac{EF (\text{g veh}^{-1} \text{ mi}^{-1}) TV (\text{veh hr}^{-1})}{1609.3 (\text{m mi}^{-1}) 3600 (\text{sec hr}^{-1})} \quad (1)$$
$$= 1.726 \times 10^{-7} (EF) (TV)$$

A value of the emission factor for vehicles can be obtained from the most current issue of *Compilation of Air Pollutant Emission Factors* (EPA, 1973). It should be noted that for many pollutants the emission factor varies with vehicle speed.

Calculations

The calculation of concentration is made by a numerical integration of the Gaussian plume point-source equation over a finite length. The coordinates (meters) of the end points of a line source of length D (meters),

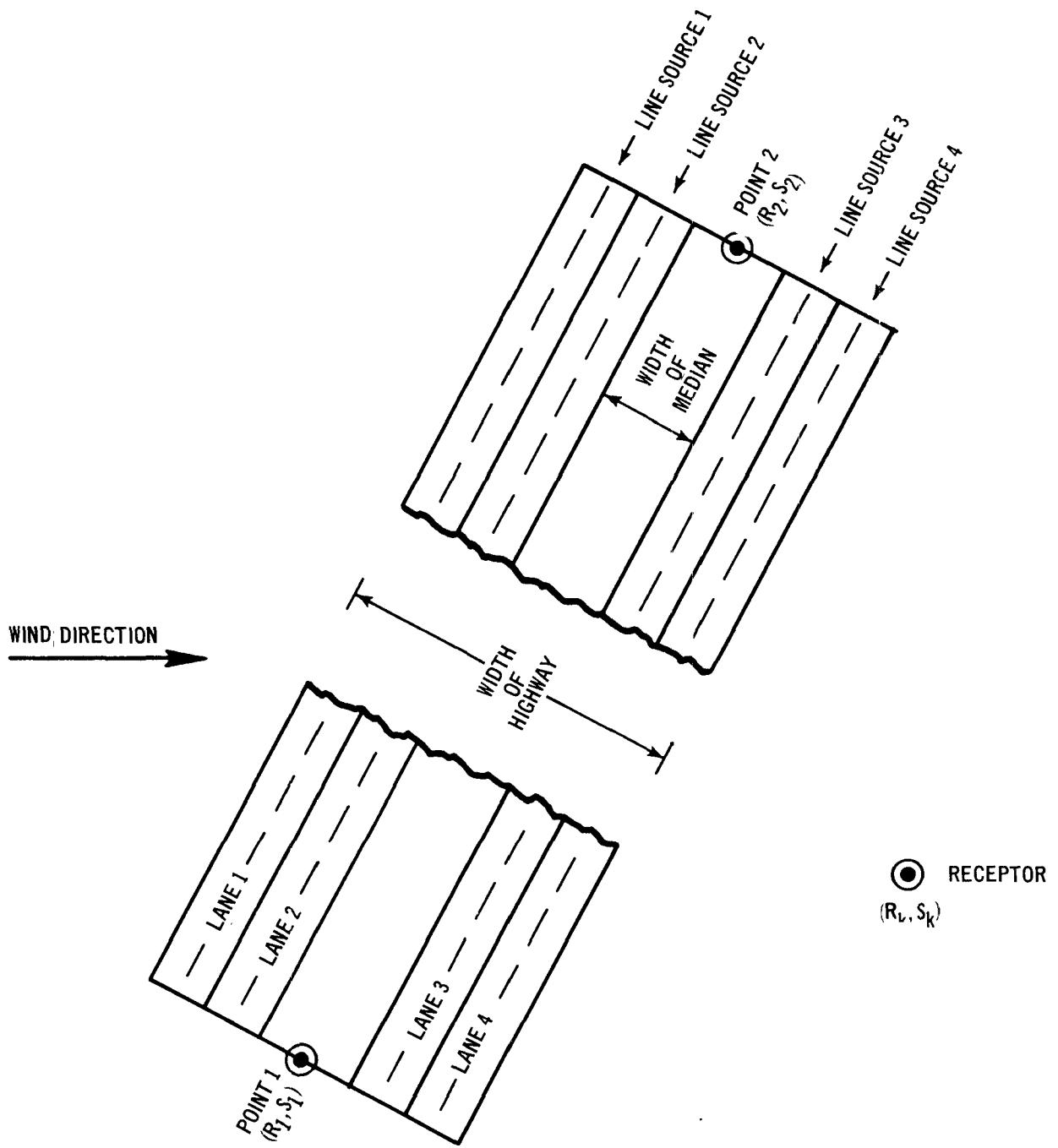


Figure 1. Overhead view of the geometry of at-grade highway as seen by the computer model. The endpoints of the highway are specified by the centerline coordinates, (R_1, S_1) and (R_2, S_2) , while the receptor coordinates are given as (R_k, S_k) . Line sources (four) are indicated by the dashed lines at the center of each lane of traffic.

representing a single lane extending from point A to point B (see Figure 2), are R_A, S_A and R_B, S_B . The direction of the line source from A to B is β (degrees). The coordinates, R, S , of any point along the line at an arbitrary distance, ℓ (meters), from point A are given by:

$$R = R_A + \ell \sin \beta \quad (2)$$

$$S = S_A + \ell \cos \beta \quad (3)$$

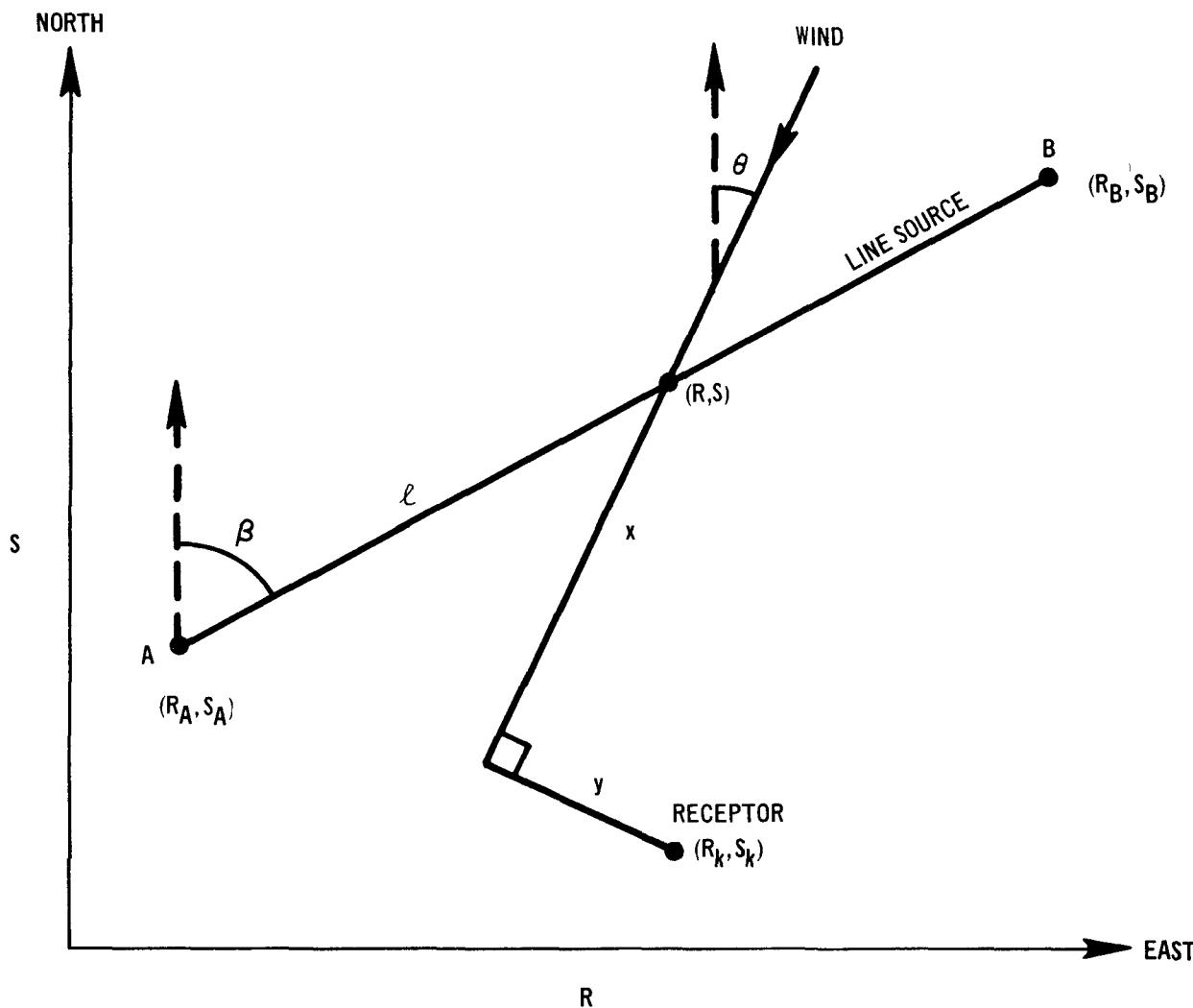


Figure 2. Line source and receptor relationships.

Given a receptor at R_k, S_k , the downwind distance, x (meters), and the crosswind distance, y (meters), of the receptor from the point R, S for any wind direction, θ (degrees), is given by:

$$x = (S - S_k) \cos \theta + (R - R_k) \sin \theta \quad (4)$$

$$y = (S - S_k) \sin \theta - (R - R_k) \cos \theta \quad (5)$$

Since R and S are functions of ℓ , x and y are also functions of ℓ . The concentration, x (g m^{-3}), from the line source is then given by:

$$x = \frac{q_\ell}{u} \int_0^D f d_\ell \quad (6)$$

where:

u = wind speed, m sec^{-1}

D = line source length, meters

f = point source dispersion function (Equations 7 to 9), m^{-2}

For application of this model to a highway segment in relatively open terrain, an approximate estimate of the wind speed, u , at 2 meters height above ground is suitable.

For stable conditions or if the mixing height is ≥ 5000 meters,

$$f = \frac{1}{2\pi\sigma_y\sigma_z} \exp\left[-\frac{1}{2}\left(\frac{y}{\sigma_y}\right)^2\right] \left\{ \exp\left[-\frac{1}{2}\left(\frac{z-H}{\sigma_z}\right)^2\right] + \exp\left[-\frac{1}{2}\left(\frac{z+H}{\sigma_z}\right)^2\right] \right\} \quad (7)$$

where:

σ_y = standard deviation of the concentration distribution in the crosswind direction, meters

σ_z = standard deviation of the concentration distribution in the vertical direction, meters

z = receptor height above ground, meters

H = effective source height, meters

In unstable or neutral conditions, if σ_z is greater than 1.6 times the mixing height, L (meters), the distribution below the mixing height is uniform with height regardless of source or receptor height, provided both are less than the mixing height:

$$f = \frac{1}{\sqrt{2\pi}\sigma_y L} \exp \left[-\frac{1}{2} \left(\frac{y}{\sigma_y} \right)^2 \right] \quad (8)$$

In all other unstable or neutral conditions:

$$\begin{aligned} f = & \frac{1}{2\pi\sigma_y\sigma_z} \exp \left[-\frac{1}{2} \left(\frac{y}{\sigma_y} \right)^2 \right] \left\{ \exp \left[-\frac{1}{2} \left(\frac{z-H}{\sigma_z} \right)^2 \right] \right. \\ & + \exp \left[-\frac{1}{2} \left(\frac{z+H}{\sigma_z} \right)^2 \right] + \sum_{N=1}^{N=\infty} \left[\exp \left[-\frac{1}{2} \left(\frac{z-H-2NL}{\sigma_z} \right)^2 \right. \right. \\ & \left. \left. + \exp \left[-\frac{1}{2} \left(\frac{z+H+2NL}{\sigma_z} \right)^2 \right] + \exp \left[-\frac{1}{2} \left(\frac{z-H+2NL}{\sigma_z} \right)^2 \right. \right. \\ & \left. \left. + \exp \left[-\frac{1}{2} \left(\frac{z+H+2NL}{\sigma_z} \right)^2 \right] \right] \right\} \end{aligned} \quad (9)$$

The infinite series in Equation 9 converges rapidly, and more than four or five sums of the four terms are seldom required.

In each of the three above equations, σ_y and σ_z are evaluated for the given stability class and the distances $x+b$ for σ_y and $x+a$ for σ_z . The virtual distances, a and b (km), are required to produce the initial σ_z and σ_y (σ_{zo} and σ_{yo}), respectively.

If z , H , or both are zero, the resulting simpler forms of Equations 7, 8, and 9 are used by the computer program.

The value of the integral in Equation 6 is approximated by use of the trapezoidal rule. Let $\Delta \ell = D/N$. Then the trapezoidal approximation gives:

$$x = \frac{q_\ell \Delta \ell}{u} \left[\frac{1}{2} (f_0 + f_N) + \sum_{i=1}^{N-1} f_i \right] \quad (10)$$

where f_i is evaluated, as appropriate, from Equation 7, 8, or 9 for $\ell = i\Delta \ell$. The distances x and y are, of course, functions of ℓ .

For a given initial choice of the interval length, $\Delta \ell$, the calculation is then successively repeated with twice the number of intervals, that is, with $\Delta \ell/2$, $\Delta \ell/4 \dots$, until the concentration estimates converge to within 2 percent of the previous estimate. This value is then used as the value of the integral.

The above evaluation of the integral is repeated for each lane of traffic, and the resulting concentrations are summed to represent the total concentration from the highway segment.

Computer Model

The FORTRAN computer program consists of a main program, three subroutines, and two functions. The main program handles input and sets up a separate line source for each lane of traffic. Subroutine DBTLNE does the integration and output of results. This subroutine calls DBTRCX, which evaluates Equations 7, 8, or 9, or simplifications of these equations if H or z is zero. Evaluation of σ_y and σ_z are done by subroutine DBTSIG, which is called from DBTRCX. Functions XVY and XVZ determine virtual distances for a given stability class corresponding to the initial σ_y and initial σ_z , respectively.

An east-north coordinate system is used in the computer model. The width of the highway and of its center strip, the coordinates of the centerline of the highway, and the coordinates of the receptor(s) are input parameters.

It should be noted that in Equations 4 and 5, x and y refer to a coordinate system aligned along the wind vector (x the downwind direction, and y the crosswind direction). That system is distinct from the coordinate system used for locating sources and receptors in the model.

In the basic equations given earlier (Equations 2 to 5), units of the coordinate system have been specified as meters for dimensional balance. However, units of the computer coordinate system, for practicality, are in kilometers. The user may use any convenient highway map unit if he enters an appropriate scaling factor to convert those units to kilometers. For example, if it is desired to use the units of meters for highway coordinates, the scale factor should be entered as 0.001. Section 4 contains a list of the input variables, including a brief description of each of the units by which the input parameters must be expressed. An example of input data, as well as the output of a run made with the example input data, is given in Appendix A.

CUT SECTION

Estimates of air pollution concentrations at locations downwind of a depressed highway (cut section) can be determined by considering the top of the cut section to be an area source of pollution (Figure 3). In the model, this area source is approximated by using ten line sources located at the top of the cut section. The total emission rate for the highway is first found by adding together the emission rates for each individual lane of traffic. Then this emission rate is distributed equally over each of the ten line sources used to simulate the area source at the top of the cut section.

Once this has been done, the procedure used to determine pollutant concentrations downwind of the cut section is entirely similar to the procedure used to determine the concentrations for an at-grade highway. It should be emphasized that these estimates of air pollution concentrations should be made for receptors downwind of the cut section and not for locations inside the cut section itself.

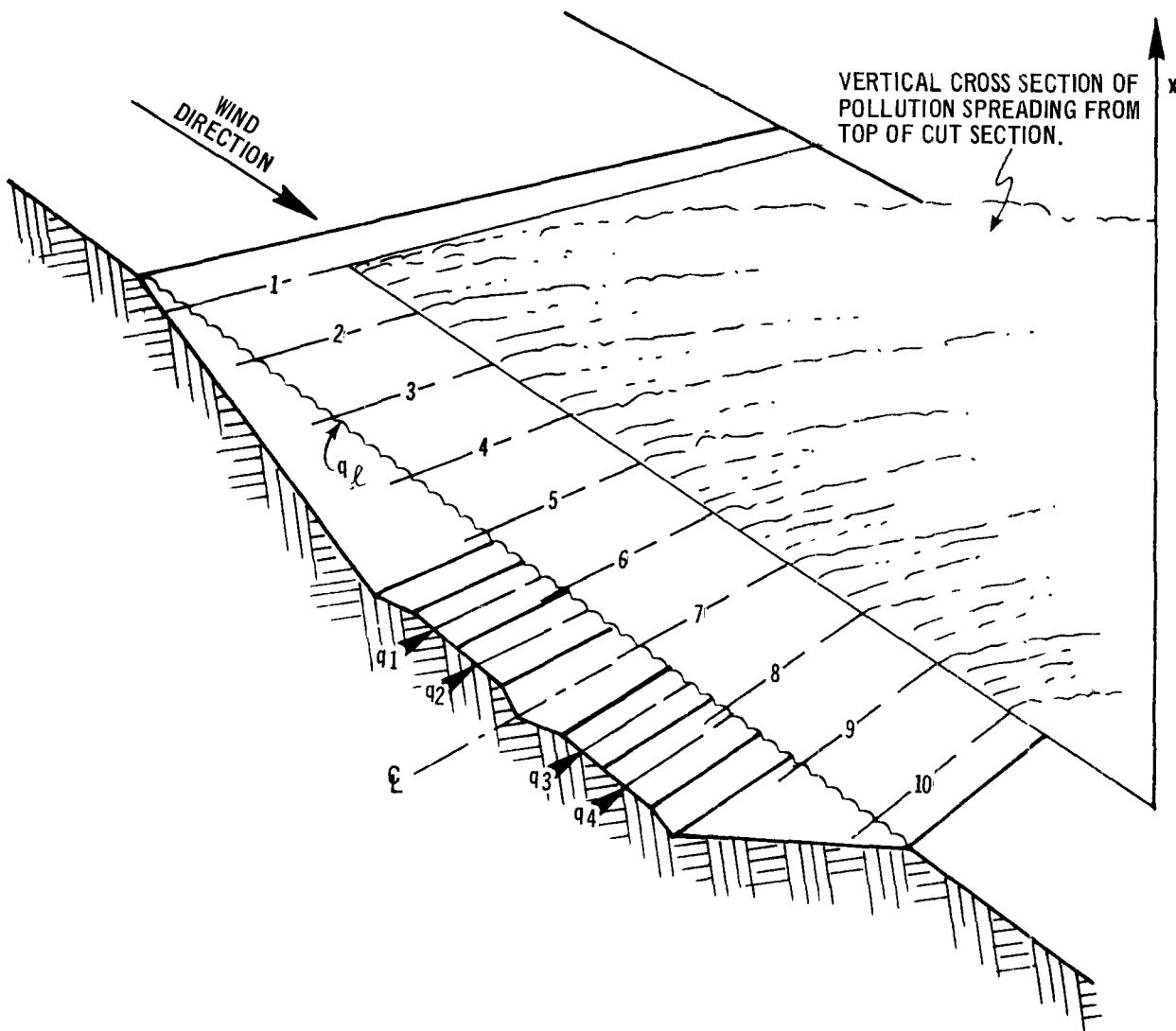


Figure 3. Method of simulating dispersion from a cut section. In this illustration, there are four lanes of traffic in a cut section with pollution emission rates q_1 , q_2 , q_3 , and q_4 . These emission rates are summed up and distributed equally over ten line sources placed at the top of the cut section, i.e., $q_{\Sigma} = (q_1 + q_2 + q_3 + q_4)/(10)$.

3. DISPERSION FUNCTIONS σ_y AND σ_z

The dispersion functions σ_y and σ_z (meters) indicate the amount the pollutant plume has spread (dispersed), after leaving its source. The values for these functions are those of Pasquill (if the virtual distance is taken as zero) as given in graphical form in Turner (1970). Pasquill stability classes are given in Table 1.

Table 1. PASQUILL STABILITY CLASSES

Stability class ^a	description
A (1)	Very unstable
B (2)	Moderately unstable
C (3)	Slightly unstable
D (4)	Neutral
E (5)	Slightly stable
F (6)	Moderately stable

^aThe stability classes are commonly referred to by letter. For input to the computer program, the numbers in parentheses are used.

The horizontal dispersion parameter value is given by

$$\sigma_y = 465.1 (e^{-x/b}) \text{ for } \theta_p \quad (11)$$

where:

x = downwind distance from source to receptor, km

b = virtual distance for initial σ_y , km

θ_p = half angle of horizontal wind spreading, degrees

The factor 465.1 is 1000 m km^{-1} divided by 2π , the number of standard deviations of a Gaussian distribution from the centerline to the point where the distribution falls to 10 percent of its maximum value. The angle θ_p is given by:

$$\theta_p = c + d \text{ in } \left(\frac{x+b}{b} \right)^{\frac{1}{2}} \quad (12)$$

where c and d (degrees) are functions of Pasquill stability class and the normalizing distance, x_0 , is 1 km. Values of the parameters c and d are given in Table 2.

Table 2. VALUES OF c AND d
USED TO CALCULATE θ_p

Stability class	Value, degrees	
	c	d
A (1)	24.167	2.5334
B (2)	18.333	1.8096
C (3)	12.5	1.0857
D (4)	8.333	0.72382
E (5)	6.25	0.54287
F (6)	4.167	0.36191

The vertical dispersion parameter value, σ_z (meters), is given by equations of the form:

$$\sigma_z = g \left(\frac{x + a}{x_0} \right)^h \quad (13)$$

where a is the virtual distance (km) to give the initial σ_z (meters), and g (meters) and h (dimensionless) are functions of stability class and also various ranges of the distance x . When a is zero, the values are the same as those in Figure 3-3 of Turner (1970). Since the values of σ_z for x less than 0.1 km are not given in that figure, the values of the parameters g and h for x less than 0.1 km are given in Table 3. The values corresponding to g and h for x at other distances can be determined by examining the program listing for subroutine DBTSIG (Appendix B).

Turbulence of the air produced by the motion of automobiles results in a rapid mixing of the pollutants near the highway. This is modeled by assuming that an initial spreading of the pollutant plume occurs over the highway. To determine an acceptable initial vertical plume spread, data taken near at-grade sections from various highways were used. When the

Table 3. VALUES OF g AND h USED TO DETERMINE σ_z
FOR DOWNWIND DISTANCES LESS THAN 0.1 km

Stability class	Value	
	g , meters	h , dimensionless
A (1)	122.8	0.9447
B (2)	90.673	0.93198
C (3)	61.141	0.91465
D (4)	34.459	0.86974
E (5)	24.26	0.8366
F (6)	15.209	0.81558

wind direction is less than 75 degrees from the perpendicular to the highway, it has been shown that an approximate expression can be used to determine pollutant concentrations from an infinite line source (Calder, 1973). Solving this expression for σ_z yields:

$$\sigma_z(x) = \sqrt{\frac{2}{\pi}} \frac{q_\ell}{C(p) u \cos \gamma} \quad (14)$$

where:

$\sigma_z(x)$ = the vertical standard deviation of plume distribution
at the downwind distance, x , from the source

$C(p)$ = the measured concentrations at the perpendicular distance,

p (meters), from the highway $\left(x = \frac{p}{\cos \gamma} \right)$, g m^{-3}

γ = the angle between the wind direction and a perpendicular
to the highway, degrees

By making estimates of the line-source emission rate, q_ℓ , and obtaining observed data for air pollution concentrations, a plot of σ_z versus distance was determined (Figure 4). From this analysis, it is seen that an initial σ_z (σ_{z0}) equal to 1.5 meters is a conservative approximation of the vertical

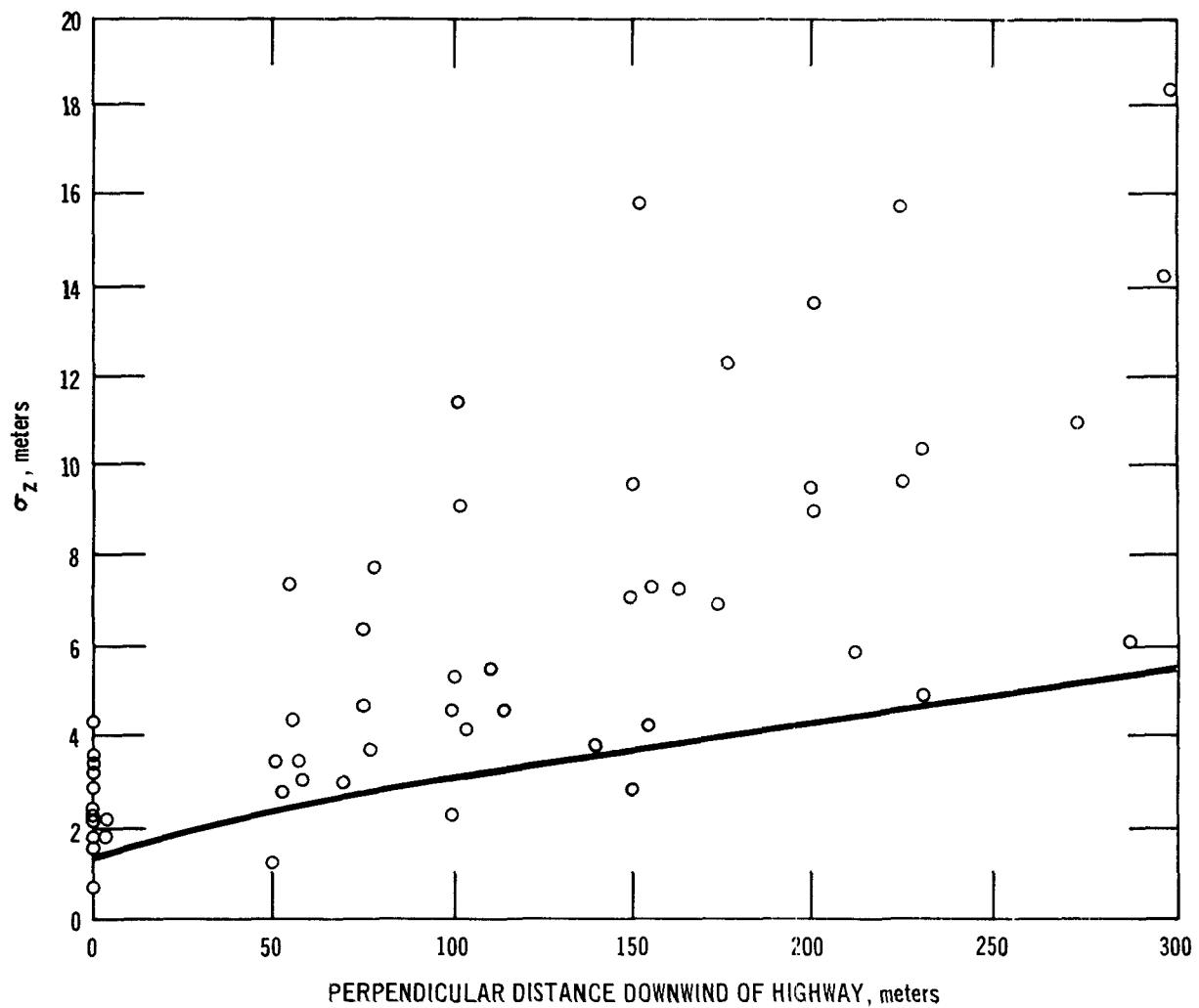


Figure 4. Data points used to determine an estimate of initial σ_z . Also plotted is the $\sigma_z(x)$ curve for neutral stability. The line is the approximate lower bound of the data.

standard deviation of the plume at the downwind edge of the at-grade highway. This is only a tentative value based on a limited amount of data and may be revised as more data become available. This empirical value of σ_{z0} is applied in the operation of the model to each of the line sources placed along each lane of traffic.

For at-grade pollution dispersion, an arbitrary value for initial σ_y (σ_{yo}) of 3 meters (approximately one-half the length of a car) was selected. The value given to σ_{yo} has little effect on the computation of air pollution concentrations when the wind direction has a component perpendicular to the highway. The use of an initial σ_y is to account for a reasonable amount of

cross-highway spreading caused by vehicle-generated turbulence when the wind direction is parallel or nearly parallel to the highway.

The virtual distances, a , corresponding to an initial σ_z of 1.5 meters and the virtual distances, b , corresponding to an initial σ_y of 3.0 meters for each stability class are given in Table 4.

Table 4. VIRTUAL DISTANCES a AND b
CORRESPONDING TO INITIAL σ_z OF 1.5 METERS
AND INITIAL σ_y OF 3.0 METERS, RESPECTIVELY

Stability class	Distance, km	
	a	b
A (1)	0.00944	0.00863
B (2)	0.01226	0.0132
C (3)	0.01736	0.0210
D (4)	0.02722	0.0348
E (5)	0.03590	0.0471
F (6)	0.05842	0.0733

There are very few published measurements of air quality downwind of a cut section. Nevertheless, the available data indicate that the cut-section configuration tends to increase the dispersion of the air pollution originating from the cut section. This is particularly true when wind speeds are light, for then the release of heat from combustion, the long travel time of the pollutant to the receptor, and mechanical turbulence produced by the cut-section highway aid the dispersion. Thus, for the cut-section case, based upon very limited data, the initial σ 's for wind speeds less than 1 m sec^{-1} were set at 10 meters for σ_y and 5 meters for σ_z . It was assumed that for wind speeds greater than 3 m sec^{-1} the cut section did not enhance the initial dispersion and that it was the same as for the at-grade highway: 3 meters for σ_y and 1.5 meters for σ_z . For speeds between 1 and 3 m sec^{-1} , the initial sigmas are linearly interpolated. These initial σ 's are assumed for each of the ten lanes used to represent the cut. The initial values of σ_y and σ_z (meters) are found from:

$$\left. \begin{array}{l} \sigma_{yo} = 3 \\ \sigma_{zo} = 1.5 \end{array} \right\} \text{for } u > 3 \text{ m sec}^{-1} \quad (15)$$

$$\left. \begin{array}{l} \sigma_{yo} = 10 - 7 \left(\frac{u - 1}{2} \right) \\ \sigma_{zo} = 5 - 3.5 \left(\frac{u - 1}{2} \right) \end{array} \right\} \text{for } 1 < u < 3 \text{ m sec}^{-1} \quad (16)$$

and

$$\left. \begin{array}{l} \sigma_{yo} = 10 \\ \sigma_{zo} = 5 \end{array} \right\} \text{for } u < 1 \text{ m sec}^{-1} \quad (17)$$

4. PREPARATION OF INPUT DATA

CARD INPUT SEQUENCE

The arrangement of data on the input cards for the batch mode of operation is given in Table 5. The coordinates of the roadway are in the center of the highway (from edge to edge). The ordering of the lanes is from left to right when looking from point 1 to point 2.

INTERACTIVE OPERATION

The HIWAY model has been placed on the Environmental Protection Agency's (EPA) Users' Network for Applied Modeling of Air Pollution (UNAMAP) computer system and is accessible to EPA users. The model is also on the UNAMAP system available to all users. For information on this system contact: Chief, Data Management, Meteorology Laboratory, U.S. Environmental Protection Agency, Research Triangle Park, N. C. 27711.

The self-explanatory listing produced by the model on a remote computer terminal is shown in Appendix A to illustrate the operation of the model in an interactive mode. The computer communicates to the user in upper case letters, while the user replies in lower case letters. To initiate the program, the user issues the command, *hiway*.

Operation of the model in an interactive mode is similar to batch mode operation. To determine emission rates for the pollutant carbon monoxide, however, the user can elect the option to use the internally generated emission rates for carbon monoxide that are representative of the emissions for the vehicle model mix near the end of 1973. This applies a correction factor for vehicle speed.

Table 5. INPUT DATA CARDS

Name	Columns	Format	Form	Variable	Units
Card type 1 (1 card)					
Head	1-80	20A4	AAAA	Alphanumeric data for heading	-
Card type 2 (1 card)					
REP1	1-10	F10.0	XXXX.XXX	East coordinate, point 1	Map units
SEP1	11-20	F10.0	XXXX.XXX	North coordinate, point 1	Map units
REP2	21-30	F10.0	XXXX.XXX	East coordinate, point 2	Map units
SEP2	31-40	F10.0	XXXX.XXX	North coordinate, point 2	Map units
H	41-50	F10.0	XX.X	Height of line source	Meters
WIDTH	51-60	F10.0	XX.	Total width of highway	Meters
CNTR	61-70	F10.0	XX.	Width of center strip	Meters
XNL	71-80	F10.0	X.	Number of traffic lanes	-
Card type 3 (up to 3 cards)					
QLS	1-80	F10.0	.XXXXXXXXXX	Emission rate for each lane	$\text{g sec}^{-1}\text{m}^{-1}$
Card type 4 (1 card; can be blank for at grade)					
CUT	1-10	F10.0	X.	1, if cut; 0, if at grade	-
WIDTC	11-20	F10.0	XX.	Width of top of cut section	Meters
Card type 5 (1 card)					
THETA	1-10	F10.0	XXX.	Wind direction	Degrees
U	11-20	F10.0	XX.X	Wind speed	m sec^{-1}
HL	21-30	F10.0	XXXX.	Height of mixing layer	Meters
XKST	31-40	F10.0	X.	Pasquill stability class	-
Card type 6 (1 card)					
GS	1-10	F10.0	X.	Scale factor ^a	-
Card type 7 (any number of cards)					
XXRR	1-10	F10.0	XXXX.XXX	East coordinate of receptor ^b	Map units
XXSR	11-20	F10.0	XXXX.XXX	North coordinate of receptor	Map units
Z	21-30	F10.0	XX.	Height (above ground) of receptor	Meters

^aThe scale factor converts map units to kilometers.

If map units in kilometers, scale factor = 1.0

If map units in meters, scale factor = 0.001

If map units in feet, scale factor = 0.000305

If map units in miles, scale factor = 1.61

^bTo begin again with another set of data, a value of 9999. is punched for XXRR (card type 7) following the last receptor card.

REFERENCES

- Beaton, J.L., A.J. Ranzieri, and J.B. Skog (1972). Motor Vehicle Emission Factors for Estimates of Highway Impact on Air Quality. In: Air Quality Manual, Vol. 2. California Department of Public Works, Division of Highways. Sacramento, California. Report No. FHWA-RD-72-34. April 1972. 58 p.
- Calder, K.L. (1973). On Estimating Air Pollution Concentrations from a Highway in an Oblique Wind. *Atmos. Environ.* 7: 863-868, September 1973.
- EPA (1973). Compilation of Air Pollutant Emission Factors, 2nd Ed. U.S. Environmental Protection Agency. Research Triangle Park, North Carolina. Publication No. AP-42. April 1973.
- Holzworth, G.C. (1972). Mixing Heights, Wind Speeds, and Potential for Urban Air Pollution throughout the Contiguous United States. U.S. Environmental Protection Agency. Research Triangle Park, North Carolina. Publication No. AP-101. 1972. 118 p.
- Ludwig, F.L., W.B. Johnson, A.E. Moon, and R.L. Mancuso (1970). A Practical Multipurpose Diffusion Model for Carbon Monoxide. Stanford Research Institute. Menlo Park, California. Contracts CAPA-3-68 and CPA 22-69-64. 184 p.
- Pasquill, F. (1961). The Estimation of the Dispersion of Windborne Material. *Meteorol. Mag.* 90(1063): 33-49, 1961.
- Turner, D.B. (1970). Workbook of Atmospheric Dispersion Estimates. U.S. Environmental Protection Agency. Research Triangle Park, North Carolina. Publication No. AP-26. 1970. 84 p.

GLOSSARY

Several frequently used terms have become part of the jargon used by air quality dispersion modelers, and these terms are defined briefly in this section. For a more complete discussion of the concepts implied by these terms, the reader should consult the references cited.

Stability class: Atmospheric stability ranked according to classes, which are given in indexes *A* through *F* (or 1 through 6), as shown in Table 1 (Pasquill, 1961). Class *A* is very unstable and is found when skies are clear and sunny, while class *F* is moderately stable and occurs under calm conditions on clear nights.

Mixing height: The height to which pollutants are actively mixed. The air close to the earth's surface generally becomes unstable after sunrise, resulting in a zone of vigorous atmospheric mixing in the layer of air at ground level. The height of this layer increases after sunrise and reaches a maximum about 4:00 p.m. (Holzworth, 1972). For most locations close to the pollution source, the mixing height will have very little influence on the calculation of pollution concentration. When the receptor is located at a great distance from the pollution source and the travel time of the pollutant from source to receptor location is long, the mixing height will be the limiting height to which pollution will spread vertically.

Receptor: A location for which it is desired to predict pollutant concentrations. When a model is being validated, it is necessary to obtain model predictions at the receptor locations for which air quality data are measured.

Emission rate of a line source: An estimate of the amount of pollution being generated by a line source (e.g., lane of automobile traffic). To determine this value, two pieces of information are required: (1) the volume of traffic and (2) the emission factor, which is dependent on vehicle speed. The emission rate can then be determined by

$$q_L = (CV) (EF) (TV)$$

where:

q_ℓ = line source emission rate, g sec⁻¹ m⁻¹

EF = emission factor, g veh⁻¹ mi⁻¹

TV = traffic volume, veh hr⁻¹

CV = conversion constant = 1.726×10^{-7} , mi hr m⁻¹ sec⁻¹

σ_y and σ_z : The standard deviation of concentration distribution in the horizontal and vertical planes, respectively. The values of σ_y and σ_z will increase with downwind distance from the source of pollution as the dimensions of the pollution plume increase. This increase in pollution plume dimension is caused by atmospheric turbulence. The intensity of atmospheric turbulence is in turn related to atmospheric stability. The plume growth will be greatest in an unstable atmosphere (more turbulence) and least when the atmosphere is stable.

APPENDIX A. EXAMPLE PROBLEM

INTRODUCTION

In order to clarify the procedure for using both the batch and interactive (continuous) versions of the HIWAY model, the following test problem is solved using both versions.

Given: Length of highway - 5 km.

Orientation - east-west.

Number of lanes - four.

Road width (edge to edge) - 46 meters.

Median width - 30 meters.

Emission rate in each lane from south to north - 0.0112, 0.0103,
0.0106, and 0.0156 g sec⁻¹ m⁻¹.

Wind direction - 42 degrees.

Wind speed - 3.7 m sec⁻¹.

Stability class - 3.

Find: The expected concentration at receptors along a line perpendicular to the center of the highway segment at distances 1, 5, 10, 30, and 50 meters from the downwind edge of the roadway (1) if the road is an at-grade section, and (2) if the road is a cut section with the top of the cut being 50 meters in width.

SOLUTION USING THE INTERACTIVE VERSION

Assuming that you have already logged on the computer, etc., type in the name *hiway* as indicated in Table A-1. You are then given the choice of receiving a description of the model. Following that, enter the input parameters as the model calls for them. Most of them are self-explanatory; however, a few comments are in order:

1. When entering the mixing height never use the value 0.
2. If you do not want the effect of a limit to vertical mixing in your calculation, use a large enough mixing height so that there is no chance of its influencing your results, such as 5000 meters.

3. When entering the receptor coordinates , remember that this program is valid only downwind of the line source. A receptor location defined on the line source will not give a valid answer. If you are interested in the concentration at the edge of the highway , use a downwind distance greater than 0.1 meter from the edge of the highway and the result will be valid.
4. The coordinates for the ends of the roadway segment are assumed to be in the center of the road (from edge to edge).
5. The ordering of emission rates is for lanes in order from left to right when looking from point 1 to point 2.

The results for the at-grade section are given following the entry of receptor coordinates. For convenience , the center of the roadway has been placed 0.023 km north of the origin in this example so that the edge of the road is on the axis and the y coordinate of the receptor is the distance from the edge of the road. The roadway and receptors could have been placed at any location.

The option to run the model for a new receptor location (LOC) , change the road type (TYPE) , or to end the program (END) is given after the results.

In the second part of the problem , the road type (cut) , the width (50 meters) , and the location of the road (to again place the edge of the road at a y coordinate value of zero) are changed. The results for the cut section are shown following the entry of data. Note that the concentrations are in micrograms per cubic meter (UGM/M**3) . The part per million (PPM) column is a conversion from micrograms per cubic meter for the pollutant carbon monoxide. The part per million column would be incorrect for any other pollutant.

If you decide to continue and change the receptor locations (LOC) , remember that the receptors must remain downwind from the downwind edge of the roadway .

SOLUTION USING THE BATCH VERSION

The batch version requires at least seven input cards. Depending upon the number of receptor points and number of problems to be run, there may be more. The format for each card is given in Table 5. Table A-2 lists the input for the example problem; Table A-3 lists the results. Note that for the cut section the sixth and seventh fields (columns 51 to 70) in card type 2 were left blank. Also note that the card with 9999. for the variable XXRR is only used if more than one set of input data are used. A card like this does *not* follow the last set of input data. As in the interactive version, the parts per million column is only valid if carbon monoxide is the pollutant being modeled.

Table A-1. EXAMPLE OF INTERACTIVE VERSION OF HIWAY

hiway

DO YOU WANT A DESCRIPTION OF THE EPA "HIWAY" MODEL
BEFORE APPLYING IT? (YES OR NO)

yes

1. THE EPA "HIWAY" MODEL COMPUTES INERT POLLUTANT CONCENTRATIONS IN THE VICINITY OF A ROADWAY ON A SHORT TERM BASIS (HOURLY AVERAGES) USING THE GAUSSIAN PLUME FORMULATION. IF MORE THAN ONE ROADWAY IS PRESENT, SUPERPOSITION APPLIES. THE MODEL CAN BE USED FOR AT GRADE AND CUT SECTIONS FOR RECEPTOR DISTANCES OF TENS TO HUNDREDS OF METERS DOWNWIND OF THE LINE SOURCE IN RELATIVELY UNCOMPLICATED TEPPAIN.
 2. THE COORDINATE SYSTEM IS ARRANGED SUCH THAT THE X-AXIS INCREASES FROM WEST TO EAST WHILE THE Y-AXIS INCREASES FROM SOUTH TO NORTH. THE UNITS RELATED TO HIGHWAY MEASUREMENTS ARE INDICATED BY A SCALE FACTOR OF USER UNITS TO KILOMETERS. THE MOST FREQUENTLY USED FACTORS ARE:

UNITS	SCALE FACTOR
KILOMETERS	1.0
METERS	0.001
FEET	0.000305
MILES	1.61
- SCALE FACTOR UNITS APPLY EXCEPT WHEN OTHER UNITS ARE SPECIFICALLY REQUESTED.
3. THE EMISSION DATA IS DEPENDENT ON VEHICLE SPEED, TYPES AND NUMBER OF VEHICLES, AND EMISSION CONTROL DEVICES. THE PROGRAM WILL GENERATE AN EMISSION RATE BASED ON AN ESTIMATE OF AVERAGE ROADWAY SPEED AND VOLUME OF TRAFFIC. ALTERNATIVELY, THE USER CAN ELECT TO SPECIFY HIS OWN EMISSION RATES IN GRAMS PER SECOND-METER. THE LATTER APPROACH IS HIGHLY PREFERABLE SINCE THE INTERNALLY GENERATED RATE IS BASED UPON A SPECIFIC AUTOMOBILE MIX (END OF 1973) WHICH DOES NOT APPLY ACCURATELY TO MOST CASES. EMISSIONS (GM/SEC/M) ARE ENTERED IN ORDER FROM LEFT TO RIGHT WHEN LOOKING FROM ROAD END PT 1 TO END PT 2.
 4. ROAD COORDINATES ARE THE ENDPOINTS OF THE HIGHWAY CENTER LINE. WIND DIRECTION IS DERIVED BY MEASURING CLOCKWISE(EAST) FROM DUE NORTH. (E.G., WIND FROM NORTH IS 0 DEGREES; EASTERLY WIND IS 90.)
 5. THE PROGRAM CONTAINS THE OPTION TO EVALUATE ANY NUMBER OF RECEPTOR LOCATIONS AND/OR TYPES OF ROADS.
 6. YOU MUST SEPARATE MULTIPLE INPUTS WITH COMMAS.
 7. FOR MOST APPLICATIONS, THE HEIGHTS OF THE RECEPTOR AND SOURCES ARE ASSUMED TO BE THE SAME.

Table A-1 (continued). EXAMPLE OF INTERACTIVE VERSION OF HIWAY

```

DO YOU WANT A DESCRIPTION OF THIS VERSION OF "HIWAY"? (YES OR NO)
no
ENTER SCALE FACTOR (USER UNITS/KILOMETER).
1 ENTER LINE(ROAD) ENDPOINTS. (ORDERED PAIRS:X1,Y1,X2,Y2)
2.5,-023,-2.5,023
ENTER EMISSION HEIGHT. (METERS)
0
ENTER WIND DIRECTION (DEG). NORTH IS ZERO.
42
ENTER WIND SPEED (METERS/SEC).
3.7
ENTER MIXING HEIGHT (METERS).
1000
ENTER PASQUILL-TURNER STABILITY CLASS (1-6).
3
ENTER THE NUMBER OF LANES.
4
DO YOU WISH TO ENTER YOUR OWN EMISSION RATES? (YES OR NO)
yes
ENTER LINE SOURCE STRENGTH VECTOR. (A VALUE FOR EACH LANE)
.0112,.0103,.0106,.0156
IS THIS A CUT SECTION? (YES OR NO)
no
ENTER HIWAY WIDTH (METERS).
46
ENTER WIDTH OF CENTER STRIP (METERS).
30
ENTER NUMBER OF RECEPTOR LOCATIONS NEEDED. (MAXIMUM OF 25)
5
ENTER RECEPTOR COORDINATE SETS. (X&Y IN SCALE FACTOR UNITS;Z IN METERS)
0,-.001,0,0,-.005,0,0,-.010,0
0,-.030,0,0,-.050,0

```

Table A-1 (continued). EXAMPLE OF INTERACTIVE VERSION OF HIWAY

HIWAY VERSION: 74250
 ENDPOINTS OF THE LINE SOURCE
 2.500, .023 AND -2.500, .023
 EMISSION HEIGHT IS 0.000 METERS
 EMISSION RATE (GRAMS/SECOND*METER) OF 4 LANE(S)
 .112-01 .103-01 .106-01 .156-01
 WIDTH OF AT-GRADE HIGHWAY IS 46.000 METERS
 WIDTH OF CENTER STRIP IS 30.000 METERS
 WIND DIRECTION IS 42. DEGREES
 WIND SPEED IS 3.7 METERS/SEC
 STABILITY CLASS IS 3
 HEIGHT OF LIMITING LIN IS 1000.0 METERS
 THE SCALE FACTOR IS 1.0000 USER UNITS/KM.

RECEPTOR LOCATION	HEIGHT Z (M)	UGM/M**3	CONCENTRATION PPM*
X .0000	-.0010	.0000	4449.
.0000	-.0050	.0000	3831.
.0000	-.0100	.0000	3294.
.0000	-.0300	.0000	2184.
.0000	-.0500	.0000	1669.

* PPM CONCENTRATIONS CORRECT FOR CARBON MONOXIDE ONLY.

Table A-1 (continued). EXAMPLE OF INTERACTIVE VERSION OF HIWAY

YOU HAVE THE OPTION TO RUN THE MODEL FOR A NEW RECEPTOR LOCATION
(LOC), OR TO CHANGE THE ROADWAY TYPE, OR TO END THE PROGRAM.
ENTER LOC, OR TYPE, OR END.

type
ENTER LINE(ROAD) ENDPOINTS. (ORDERED PAIRS:X1,Y1,X2,Y2)
2.5,.025,-2.5,.025
ENTER EMISSION HEIGHT. (METERS)

0 ENTER WIND DIRECTION (DEG). NORTH IS ZERO.

42 ENTER WIND SPEED (METERS/SEC).

3.7 ENTER MIXING HEIGHT (METERS).

1000 ENTER PASQUILL-TURNER STABILITY CLASS (1-6).

3 ENTER THE NUMBER OF LANES.

4 DO YOU WISH TO ENTER YOUR OWN EMISSION RATES?(YES OR NO)
yes
ENTER LINE SOURCE STRENGTH VECTOR.(A VALUE FOR EACH LANE)
.0112,.0103,.0106,.0156
IS THIS A CUT SECTION? (YES OR NO)
yes
ENTER WIDTH OF TOP OF CUT. (METERS)

50 ENTER NUMBER OF RECEPTOR LOCATIONS DESIRED. (MAXIMUM OF 25)

5 ENTER RECEPTOR COORDINATE SETS.(X&Y IN SCALE FACTOR UNITS;Z IN METERS)
0,-.001,0,0,-.005,0
0,-.010,0,0,-.030,0
0,-.050,0

Table A-1 (continued). EXAMPLE OF INTERACTIVE VERSION OF HIWAY

HIWAY VERSION: 74250
 ENDPOINTS OF THE LINE SOURCE
 2.500, .025 AND -2.500, .025
 EMISSION HEIGHT IS .000 METERS
 EMISSION RATE (GRAMS/SECOND*METER) OF 4 LANE(S)
 112-01 103-01 106-01 156-01
 WIDTH OF TOP OF CUT SECTION IS 50.000 METERS
 WIND DIRECTION IS 42. DEGREES
 WIND SPEED IS 3.7 METERS/SEC
 STABILITY CLASS IS 3
 HEIGHT OF LIMITING LIN IS 1000.0 METERS
 THE SCALE FACTOR IS 1.0000 USER UNITS/KM.

RECEPTOR LOCATION	HEIGHT	CONCENTRATION		
X	Y	Z (M)	UGM/M**3	PPM*
.0000	-.0010	.0000	3894.	3.388
.0000	-.0050	.0000	3452.	3.003
.0000	-.0100	.0000	3040.	2.645
.0000	-.0300	.0000	2107.	1.833
.0000	-.0500	.0000	1636.	1.423

* PPM CONCENTRATIONS CORRECT FOR CARBON MONOXIDE ONLY.

ENTER LOC, OR TYPE, OR END.
end

Table A-2. CARD INPUT FOR EXAMPLE PROBLEM

AT-GRADE SECTION		EXAMPLE FOR HIWAY USERS MANUAL									
		-2.5	.023	-2.5	.023	-2.5	.023	-2.5	.023	-2.5	.023
1	12 34 56 78 90 12 34 56 78 90 12 34 56 78 90 12 34 56 78 90 12 34 56 78 90 12 34 56 78 90	.0112	.0103	.0106	.0156	.0106	.0156	.0106	.0156	.0106	.0156
2	42	3.7	1000	3							
3	1	-0.001	.0								
4	1	-0.005	.0								
5	1	-0.010	.0								
6	1	-0.030	.0								
7	1	-0.050	.0								
8	9999	CUT-SECTION									
9	2	2.5	.025	-2.5	.025	-2.5	.025	-2.5	.025	-2.5	.025
10	12	.0112	.0103	.0106	.0156	.0106	.0156	.0106	.0156	.0106	.0156
11	1	50									
12	42	3.7	1000	3							
13	1	-0.001	.0								
14	1	-0.005	.0								
15	1	-0.010	.0								
16	1	-0.030	.0								
17	1	-0.050	.0								

Table A-3. EXAMPLE OF BATCH VERSION OF HIGHWAY

@XGT HIWAYBATCH.KZ

AT-GRADE SECTION EXAMPLE FOR HIWAY USERS MANUAL

HIGHWAY VERSION: 74250
 ENDPOINTS OF THE LINE SOURCE
 2.500. •.C23 AND -2.500. •.023
 EMISSION HEIGHT IS •.000 METERS
 EMISSION RATE (GRAMS/ SEC) OF 4 LANE(S)
 •.112-.51 •.103-.01 •.106-.01 •.156-.01
 WIDTH OF AT-GRADE HIGHWAY IS 46.0 M
 WIDTH OF CENTER STRIP IS 30.0 M
 WIND DIRECTION IS 42. DEGREES
 WIND SPEED IS 3.7 METERS/SEC
 STABILITY CLASS IS 3
 HEIGHT OF LIMITING LID IS 1000.0 METERS
 THE SCALE OF THE COORDINATE AXES IS 1.0000 USER UNITS/KM.

RECEPTOR X	LOCATION Y	HEIGHT Z(M)	CONCENTRATION UGM/METER*3	PPM *
•.0000	- •.C21C	•.0000	4449.	3.871
•.0000	- •.C05C	•.0000	3831.	3.333
•.0000	- •.C10D	•.0000	3294.	2.866
•.0000	- •.030C	•.0000	2184.	1.900
•.0000	- •.050D	•.0000	1669.	1.452

* PPM CONCENTRATIONS CORRECT FOR CARBON MONOXIDE ONLY.

Table A-3 (continued). EXAMPLE OF BATCH VERSION OF HIGHWAY

CUT-SECTION EXAMPLE FOR HIWAY USERS MANUAL

HIGHWAY VERSION: 74250
 ENDPOINTS OF THE LINE SOURCE
 2.500. •C25 AND -2.500. • .025
 EMISSION HEIGHT IS •000 METERS
 EMISSION RATE (GRAMS/SECOND*METER) OF 4 LANE(S)
 •112-01 •103-01 •106-01 •156-01
 WIDTH OF TOP OF CUT SECTION IS 50.000 M
 WIND DIRECTION IS 42. DEGREES
 WIND SPEED IS 3.7 METERS/SEC
 STABILITY CLASS IS 3
 HEIGHT OF LIMITING LID IS 1000.0 METERS

THE SCALE OF THE COORDINATE AXES IS 1.0000 USER UNITS/KM.

RECEPTOR LOCATION X Y Z	HEIGHT Z(M) •0000 •0010 •0050 •0100 •0300 •0500	CONCENTRATION UGM/METER**3 3894. • 3452. • 3040. • 2107. • 1636. •	PPM *
•0000	- •0010	•0000	3.388
•0000	- •0050	•0000	3.003
•0000	- •0100	•0000	2.645
•0000	- •0300	•0000	1.833
•0000	- •0500	•0000	1.423

* PPM CONCENTRATIONS CORRECT FOR CARBON MONOXIDE ONLY.

**APPENDIX B. FORTRAN SOURCE PROGRAM LISTING
FOR BATCH VERSION OF HIWAY**

```

C   HIWAY 1
C   THIS PROGRAM CALCULATES THE CONCENTRATION FROM A LINE SOURCE
C   COMMON /SOL/ QLN(25),HLN(25), RAQ(25), SAQ(25), RBQ(25), SBQ(25),
*  SYON,SZON,CON(50)
C   COMMON /REC/ RRI(51),SR(51),ZR(51)
C   COMMON /WEA/ THETA,U,KST,HL
C   COMMON /PUTY/ XXRR(51),XXSR(51),OLS(25),HEAD(20),IWRI
C   DIMENSION Z(51)
C   IVER=74250
C   IRDE=5
C   IWRI=6
C   READ HEADER CARD
C   READ(IRO,500,END=190)HEAD
500  FORMAT(2DA4)
      WRITE(IWRI,510)HEAD
510  FORMAT('C',12.4)
      WRITE(IWRI,520)VERS
520  FORMAT('C',HIWAY VERSION:' ,I6)
      READ(IRO,540,END=190)REP1,SEP1,REP2,SEP2,H,WIDTH,CNTR,XNL
      FORMAT(8F10.0)
      REP1,SEP1 ARE THE COORDINATES OF AN END POINT OF THE LINE
      SOURCE IN SOURCE COORDINATES.
      REP2,SEP2 ARE THE COORDINATES OF THE OTHER END POINT OF THE
      LINE SOURCE IN SOURCE COORDINATES.
      H IS THE EFFECTIVE EMISSION HEIGHT OF THE SOURCE IN METERS.
      WIDTH IS THE HIGHWAY WIDTH (M) FOR AT GRADE
      CNTR IS THE WIDTH OF THE CENTER STRIP (M)
      XNL IS THE NUMBER OF LANES FOR THE AT-GRADE HIGHWAY.
      WRITE(IWRI,550)REP1,SEP1,REP2,SEP2
      FORMAT("ENDPOINTS OF THE LINE SOURCE",/,,
* F9.3,*,F9.3,*,*,F9.3)
      NL=NL
      WRITE(IWRI,560)H
      FORMAT(1EMISSON HEIGHT IS',F8.3,' METERS')
      WRITE(IWRI,570)NL
      FORMAT("EMISSION RATE (GRAMS/SECOND * METER ) OF ',I4,' LANES",)
      READ(IRO,540)OLS(I),I=1,NL
      FORMAT(1EMISSON RATE (GRAMS/SECOND * METER ) OF ',I4,' LANES",)
      HIWAY 1
      HIWAY 2
      HIWAY 3
      HIWAY 4
      HIWAY 5
      HIWAY 6
      HIWAY 7
      HIWAY 8
      HIWAY 9
      HIWAY 10
      HIWAY 11
      HIWAY 12
      HIWAY 13
      HIWAY 14
      HIWAY 15
      HIWAY 16
      HIWAY 17
      HIWAY 18
      HIWAY 19
      HIWAY 20
      HIWAY 21
      HIWAY 22
      HIWAY 23
      HIWAY 24
      HIWAY 25
      HIWAY 26
      HIWAY 27
      HIWAY 28
      HIWAY 29
      HIWAY 30
      HIWAY 31
      HIWAY 32
      HIWAY 33
      HIWAY 34
      HIWAY 35
      HIWAY 36
      HIWAY 37

```

```

C      QLS IS THE LINE SOURCE STRENGTH (GRAMS/SECOND-METER)          HIWAY 38
      WRITE(IWRI,580)(QLSI),I=1,NL)                                25 HIWAY 39
      FORMAT(8E12.3)                                              26 HIWAY 40
      READ(IRD,540)CUT,WIDTC                                         27 HIWAY 41
C      CUT SECTION.                                                 HIWAY 42
C      WIDTC IS THE WIDTH OF THE TOP OF THE CUT SECTION (M)        HIWAY 43
      IF (CUT.EQ.0.)GOTO40                                         28 HIWAY 44
C      DQLS IS THE CUT SECTION SOURCE STRENGTH                      HIWAY 45
      DQLS=0.                                                       29 HIWAY 46
      DO 20 I=1,NL                                                 30 HIWAY 47
      DQLS=DQLS+QLSI(I)                                           31 HIWAY 48
      XNDL=10.                                                       32 HIWAY 49
      NL=2XNDL                                                       33 HIWAY 50
      DQLS=DQLS/XNDL                                             34 HIWAY 51
      WRITE(IWRI,590)WIDTC                                         35 HIWAY 52
      FORMAT(1*WIDTH OF TOP OF CUT SECTION IS*,F10.3,*M*)          36 HIWAY 53
      DO 30 I=1,NL                                                 37 HIWAY 54
      QLS(I)=DQLS                                                 38 HIWAY 55
      WIDT=WIDTC                                                 39 HIWAY 56
      XNL=XNDL                                                       40 HIWAY 57
      CNTR=0.                                                       41 HIWAY 58
      GO TO 50                                                       42 HIWAY 59
      WRITE(IWRI,600)WIDTH,CNTR                                     43 HIWAY 60
      FORMAT(1*WIDTH OF AT-GRADE HIGHWAY IS*,F10.1,*M*,/,           44 HIWAY 61
             * WIDTH OF CENTER STRIP IS*,F10.1,*M*)                  45 HIWAY 62
      READ(IRD,540)THETA,U,KST                                     46 HIWAY 63
      KST=KKST                                                       47 HIWAY 64
C      THETA IS THE WIND DIRECTION IN DEGREES.                      HIWAY 65
C      U IS THE WIND SPEED IN METERS PER SECOND.                   HIWAY 66
C      KST IS THE STABILITY CLASS.                                 HIWAY 67
C      HL IS THE HEIGHT OF THE LIMITING LID.                      HIWAY 68
      WRITE(IWRI,610)THETA,U,KST,HL                               48 HIWAY 70
      FORMAT(1*WIND DIRECTION IS*,F7.0,*DEGREES*,/,*WIND SPEED IS*,   HIWAY 71
             *F7.1,*METERS/SEC*,/,*STABILITY CLASS IS*,F7.0,*HEIGHT OF LIMITING
             *LID IS*,F8.1,*METERS*)                                  HIWAY 72
      READ(IRD,540)GS                                         49 HIWAY 73
C      GS IS THE MEASURE BETWEEN COORDINATES (KM).                  HIWAY 74

```

```

WRIT E(IWRI,620)G$      50 HIWAY 75
FORMAT(* THE SCALE OF THE COORDINATE AXES IS * ,F10.4,* USER UNITS/
* KM.* // )      51 HIWAY 76
WRIT E(IWRI,630)      52 HIWAY 77
FORMAT(1 HD *, RECEPTOR LOCATION      53 HIWAY 78
* * X*,1GX*,Y      54 HIWAY 81
* * Z(M)      55 HIWAY 82
HEIGH T      56 HIWAY 83
UGM/METER* *3      57 HIWAY 84
PPM * *)      58 HIWAY 85
CONCENTRATION *,      59 HIWAY 86
      60 HIWAY 87
      61 HIWAY 88
      62 HIWAY 89
      63 HIWAY 90
      64 HIWAY 91
      65 HIWAY 92
      66 HIWAY 93
      67 HIWAY 94
      68 HIWAY 95
      69 HIWAY 96
      70 HIWAY 97
      71 HIWAY 98
      72 HIWAY 99
      73 HIWAY100
      74 HIWAY101
      75 HIWAY102
      76 HIWAY103
      77 HIWAY104
      78 HIWAY105
      79 HIWAY106
      80 HIWAY107
      81 HIWAY108
      82 HIWAY109
      83 HIWAY110
      84 HIWAY111

DL = -5.5)* CNT R+(-1)* ALIM-L* b+A)*WL
DU = DL *0 .001/DIST
RA ( ID )= RA+DELS*DUM
NLIM=NL/2
ALIM=NLIM
DO 1 ID ID=1,NLIM
AL ID
DL = -5.5)* CNT R+(-1)* ALIM-L* b+A)*WL
DU = DL *0 .001/DIST
RA ( ID )= RA+DELS*DUM
RB ( ID )= RB+DELS*DUM
SA ( ID )= SA-DELR*DUM
SB ( ID )= SB-DELR*DUM

```

```

QL(N ID)=QLS(ID)
HL N ID)=H
CO NT INUE
NS =N LIM+ 1
AS =NS
DO 120 ID=NS+N L
A=ID
DL =D .5.*C NTR+(D .5+A -AS)*WL
DU M DL *C .C 01 /DIST
RA Q ID)=RA +DELS*DUM
RB Q ID)=RB +DELS*DUM
SA Q ID)=SA -DELR*DUM
SB Q ID)=SB -DELR*DUM
QL N ID)=QL S(ID)
HL N ID)=H
CO NT INUE
K=NL
IC HK=1
NE 1
RE AD (IRD *540,END=150)XXRR(N),XXSR(N),Z(N)
IF (X XRR(N).GE. 99 99.) GO TO 170
IF (N=5)160,140,140
WR IT E(IWRI,640)
FORMAT(1HC,"THE NUMBER OF RECEP TORS IS LIMITED TO 50. YOU HAVE AT 108
* TERMINATED TO READ THE 51ST. COMPUTATIONS WILL BE MADE FOR 50.",)
150 IC HK=2
GO TO 170
RR (N)=XXRR(N)*65
SR (N)=XXSR(N)*65
ZR (N)=Z(N)
N=N+1
GO TO 130
170 NE N+1
DO 180 I DUM=1..N
180 CO M ID UM=0.
C K IS NUMBER OF LINE SOURCES
C N IS NUMBER OF RECEP TORS

```

```
CALL DBTLINE(K,N)
WRITER(TWRI,650)
FORMAT(1HO,*,PPM) CONCENTRATIONS CORRECT FOR CARBON MONOXIDE ONLY
*.*.
60 TO (10,190).1CHK
CALL EXIT
END
22 COMMENT CARDS 9 CONTINUATION CARDS 34 NUMBERED STATEMENTS
```

```

SUBROUTINE DBTLNE(NQ, NR)
CO MM ON / SOL/ QLN(25), HLN(25), RAG(25), SAQ(25), RBQ(25), SBQ(25),
* SY ON, S ZON, CON(50)
CO MM ON / REC/ RRI(51), SR(51), ZR(51)
CO MM ON / WE A/ THE TA, U, KST, HL
CO MM ON / PUT/ XRR(51), XXSR(51), QLS(25), HEAD(20), IWRI
DI ME NS IDN XST(11), YST(11)
X( R, S) = (R-RREC)*SINT + (S-SREC)*COST
X IS UP WIND DISTANCE OF R, S FROM RREC, SREC
Y( R, S) = (S-SREC)*SINT - (R-RREC)*COST
Y IS CROSSWIND DISTANCE OF R, S FROM RREC, SREC
TR = THE TA/57. 2958
SI NT = SIN(TR)
CO ST = COS(TR)
PI NE 0.02
UZ =U
XY YL =X W(S YON, KST)
XV ZL =X VZ(S ZON, KST)
DO 4 65 NC=1, NR
RR EC =R RI NC
SR EC =S RI NC
Z=ZR( NC)
DO 4 70 N=1, NQ
R1 = RAQ(NS)
S1 = SAQ(NS)
R2 = RBQ(NS)
S2 = SBQ(NS)
Q1 = QLN(NS)
H = HL(NS)
X1 = X(R1, S1)
X2 = X(R2, S2)
IF (X1) 35 .45, 45
IF (X2) 40 .45, 45
RC = 0.
60 T0 470
45 IF (X1-100. 146, 46, 47
46 IF (X2-100. 149, 49, 47
1 HIWAY156
2 HIWAY157
3 HIWAY159
4 HIWAY160
5 HIWAY161
6 HIWAY162
7 HIWAY163
8 HIWAY164
9 HIWAY165
10 HIWAY166
11 HIWAY167
12 HIWAY168
13 HIWAY169
14 HIWAY170
15 HIWAY171
16 HIWAY172
17 HIWAY173
18 HIWAY174
19 HIWAY175
20 HIWAY176
21 HIWAY177
22 HIWAY178
23 HIWAY179
24 HIWAY180
25 HIWAY181
26 HIWAY182
27 HIWAY183
28 HIWAY184
29 HIWAY185
30 HIWAY186
31 HIWAY187
32 HIWAY188
33 HIWAY189
34 HIWAY190
35 HIWAY191
36 HIWAY192

```

```

47 WRITE(IWRT,48)
48 FORMAT(1HD," THIS RECEPTOR IS 100KM OR MORE FROM SOURCE ")
49 GO TO 465
50 DELR = R2 - R1
51 DELS = S2 - S1
52 Y1 = Y(R1,S1)
53 Y2 = Y(R2,S2)
54 IF(Y1-Y2) 100,255,10C
      10C COST + 0.0001135,105,105
      11C SINT - E*SCUM1145,145,135
      12C R2 - 0.00011125,115,115
      13C R1 - 0.00011125,115,115
      14C RLOC = S1 + (DELS/DELR)*R1
      15C RLLOC = RREC
      16C SLLOC = SLP * (RLOC - R1) + S1
      17C GO TO 200
      18C IF(DELR + 0.0001175,165,165
      19C IF(DELR - 0.0001170,170,175
      20C RLLOC = R1
      21C SLLOC = (RLOC - RREC) * COST/SINT + SREC
      22C GO TO 200
      23C IF(DELS + 0.0001180,180,180
      24C IF(DELS - 0.0001185,190,190
      25C SLLOC = S1

```

```

RL OC = (SL OC - SREC) * SIN T/COST + RREC      71 HIWAY230
60 T0 200                                         72 HIWAY231
TA TH = SIN T/COST                               73 HIWAY232
C   TA TH IS TANGENT (THETA)                      HIWAY233
SL P = DELS/DELR
C   SLP IS SLOPE OF LINE SOURCE.                  HIWAY234
RL OC = (RREC/TATH + S1 - SLP*R1 - SREC)/TATH - SLP 74 HIWAY234
SL OC = (RL OC - RREC)/TATH + SREC               75 HIWAY235
C   RLOC, SLOC IS LOCUS OF UPWIND VECTOR FROM RECEPTOR AND LINE AR 76 HIWAY237
C   EXTENSION OF LINE SOURCE.                      HIWAY238
HIWAY239
77 HIWAY240
78 HIWAY241
79 HIWAY242
80 HIWAY243
81 HIWAY245
82 HIWAY246
83 HIWAY247
84 HIWAY248
85 HIWAY249
86 HIWAY250
87 HIWAY251
88 HIWAY252
89 HIWAY253
90 HIWAY254
91 HIWAY255
92 HIWAY256
93 HIWAY258
94 HIWAY259
95 HIWAY260
HIWAY261
96 HIWAY262
97 HIWAY263
98 HIWAY264
99 HIWAY265
100 HIWAY266

C   TA TH IS TANGENT (THETA)
IF (XLOC >= 1255.255,205
    XLOC IS POSITIVE IF LOCUS IS UPWIND.
IF (S2-S1) > 1210,210,215
    XL OC = X(RLOC,SLOC)
IF (XLOC < 1255.255,205
    XLOC IS POSITIVE IF LOCUS IS UPWIND.
IF (S2-S1) < 1210,210,215
    SL AX = S1
    SM IN = S2
    60 T0 220
    SM AX = S2
    SM IN = S1
    IF (R2-R1) > 225,225,230
    RM AX = R1
    RM IN = R2
    GO T0 235
    RM AX = R2
    RM IN = R1
    SEE IF UPWIND LOCUS IS ON LINE SOURCE.
235  IF (RLOC-RMIN) > 255,240,240
240  IF (RMAX-RLOC) > 255,245,245
245  IF (SLOC-SMIN) > 255,250,250
250  IF (SMAX-SLOC) > 255,260,260
255  INDIC = 1
    INDIC = 1 FOR NO LOCUS ON LINE SOURCE.

C   XA = X1
    YA = Y1
    XB = X2
    YB = Y2
    GO T0 300

```

```

260      INDIC = 2 FOR LOCUS ON LINE SOURCE.
C        XA = X1
          YA = Y1
          XB = XLOC
          YB = 0.
300      DISX = XB - XA
          DISY = YB - YA
          DISI = SQR( (DISX*DISX + DISY*DISY) )
          DISI IS LENGTH(KM) OF LINE CONSIDERED.
C        IF (DISI) 310, 305, 310
305      CURR = 0.
60      TO 435
       DD1 = DISI*1000./20.
C        ONE-HALF IS INCLUDED IN THE 2C.
C        DDI IS ONE-HALF TIMES 1/10 OF DISI (M).
C        DX = DISX/10.
          DY = DISY/10.
          PREV = 0.
KNTRL = 1
XT = XA
YT = YA
KNT = 0
DO 355  I = 1,11
      STORE EACH XT,YI.
C        XT(I) = XI
          YT(I) = YI
          XZ = XI + XVZL
          XY = XI + XVYL
          CALL DBTRCX(UZ,Z,H,HL,XZ,YI,KST,AN,M,SY,SZ,RC)
          G0 TO 315, 335), KNTRL
          IF RC IS ZERO, CONTINUE UNTIL RC IS POSITIVE.
C        IF (RC) 350, 350, 320
315      IF (I-1) 325, 330
320      KNTRL = 2
          G0 TO 345
          RESET POINT A TO LAST ONE PREVIOUS.

```

```

101      HIWAY267
102      HIWAY268
103      HIWAY269
104      HIWAY270
105      HIWAY271
106      HIWAY272
107      HIWAY273
108      HIWAY274
109      HIWAY275
110      HIWAY276
111      HIWAY277
112      HIWAY278
113      HIWAY279
114      HIWAY280
115      HIWAY281
116      HIWAY282
117      HIWAY283
118      HIWAY284
119      HIWAY285
120      HIWAY286
121      HIWAY287
122      HIWAY288
123      HIWAY289
124      HIWAY290
125      HIWAY291
126      HIWAY292
127      HIWAY293
128      HIWAY294
129      HIWAY295
130      HIWAY296
131      HIWAY297
132      HIWAY298
133      HIWAY299
134      HIWAY300
135      HIWAY301
136      HIWAY302
137      HIWAY303

```

```

330   XA = XST(I-1)
      YA = YST(I-1)
      KNTRL = 2
      GO TO 345
      IF (RC) 340, 340, 345
      RESET POINT B IF REACH ZERO CONCENTRATION.
340   XB = XI
      YB = YI
      GO TO 360
      KNT = KNT + 1
345   XI = XI + DX
      YI = YI + DY
      COUNTINUE
350   IF (KNT) 370, 370, 365
      IF (KNT -6) 300, 300, 390
      IF GET TO 370 • CONC. FROM THIS SEGMENT IS 0.
355   COUNTINUE
360   IF (KNT) 370, 370, 365
      IF (KNT -6) 300, 300, 390
      GO TO (375, 380, 385), INDIC
365   RC = 0.
      GO TO 460
      FIRST = 0.
370   GO TO 450
      RC = FIRST
375   GO TO 460
      COUNTINUE
380   DO A TRAPEZOIDAL INTEGRATION FROM A TO B IN TEN STEPS.
      IT IS LIKELY THAT A OR B HAVE BEEN REDEFINED.
385   DIS = FIRST
      GO TO 460
      COUNTINUE
390   DO A TRAPEZOIDAL INTEGRATION FROM A TO B IN TEN STEPS.
      IT IS LIKELY THAT A OR B HAVE BEEN REDEFINED.
400   DISX = XB-XA
      DISY = YB-YA
      DISI = SQRT(DISX*DISX + DISY*DISY)
      DED = DISI*100.
      DED IS 1/10 DISI IN METERS.
410   DX = DISX/10.
      DY = DISY/10.
      SUM = 0.
      XDUM = XA
      YDUM = YA
      GO TO 320
      COUNTINUE
131  HIWAY304
132  HIWAY305
133  HIWAY306
134  HIWAY307
135  HIWAY308
      HIWAY309
136  HIWAY310
137  HIWAY311
138  HIWAY312
139  HIWAY313
140  HIWAY314
141  HIWAY315
142  HIWAY316
143  HIWAY317
144  HIWAY318
      HIWAY319
145  HIWAY320
146  HIWAY321
147  HIWAY322
148  HIWAY323
149  HIWAY324
150  HIWAY325
151  HIWAY326
152  HIWAY327
      HIWAY328
      HIWAY329
153  HIWAY330
154  HIWAY331
155  HIWAY332
      HIWAY333
156  HIWAY334
      HIWAY335
157  HIWAY336
158  HIWAY337
159  HIWAY338
160  HIWAY339
161  HIWAY340

```

```

XZ = XDUM + XVZL          162 HIWAY341
XY = XDUM + XYYL          163 HIWAY342
CALL DBTRCX(UZ,Z•H•HL,XZ•XY, YDUM•KST,AN•M•SY•SZ•RC) 164 HIWAY343
SUM = SUM + RC/2.          165 HIWAY344
DO 405 I = 1•9             166 HIWAY345
XDUM = XDUM + DX          167 HIWAY346
YDUM = YDUM + DY          168 HIWAY347
XZ = XDUM + XVZL          169 HIWAY348
XY = XDUM + XYYL          170 HIWAY349
CALL DBTRCX(UZ,Z•H•HL,XZ•XY, YDUM•KST,AN•M•SY•SZ•RC) 171 HIWAY350
SUM = SUM + RC             172 HIWAY351
XDUM = XDUM + DX          173 HIWAY352
YDUM = YDUM + DY          174 HIWAY353
XZ = XDUM + XVZL          175 HIWAY354
XY = XDUM + XYYL          176 HIWAY355
CALL DBTRCX(UZ,Z•H•HL,XZ•XY, YDUM•KST,AN•M•SY•SZ•RC) 177 HIWAY356
SUM = SUM + RC/2.          178 HIWAY357
C INTEGRATED VALUE IS CURR.          HIWAY358
CURR = SUM * DEDD          179 HIWAY359
ILIM = 1C                  180 HIWAY360
C FIRST ESTIMATE COMPLETED HERE.          HIWAY361
410 PREV = CURR             181 HIWAY362
C EVALUATE FOR POINTS IN BETWEEN THOSE ALREADY EVALUATED.
DED = DEDD/2.               182 HIWAY364
XDUM = XA + DX/2.          183 HIWAY365
YDUM = YA + DY/2.          184 HIWAY366
DO 415 I = 1•ILIM          185 HIWAY367
XZ = XDUM + XVZL          186 HIWAY368
XY = XDUM + XYYL          187 HIWAY369
CALL DBTRCX(UZ,Z•H•HL,XZ•XY, YDUM•KST,AN•M•SY•SZ•RC) 188 HIWAY370
C NOTE ADD THESE TO RC'S FOUND ABOVE.          HIWAY371
SUM = SUM + RC             189 HIWAY372
XDUM = XDUM + DX          190 HIWAY373
YDUM = YDUM + DY          191 HIWAY374
CURR = SUM * DEDD          192 HIWAY375
C SECOND ESTIMATE COMPLETED HERE. ALSO FOURTH, SIXTH, ETC.
TEST = ABS((CURR-PREV)/CURR) 193 HIWAY377

```

```

C      IF (TEST-PIN)435.420.420
      IF (TEST-PIN)435.420.420
420    ILIM = ILIM * 2
      PREV = CURR
      EVALUATE POINTS IN BETWEEN.
      DELD = DELD/2.
      DX = DX/2.
      DY = DY/2.
      XDUM = XA + DX/2.
      YDUM = YA + DY/2.
DO 425  I = 1,ILIM
      XZ = XDUM + XYZL
      XY = XDUM + XVL
      CALL DBTRC(X(UZ,Z,H,HL,XZ,XY,YDUM,KST,AN,M,SY,SZ,RC)
      SUM = SUM + RC
      XDUM = XDUM + DX
      YDUM = YDUM + DY
425    CURR = SUM * DELD
      THIRD ESTIMATE COMPLETED HERE. ALSO FIFTH,SEVENTH, ETC.
      TEST = ABS((CURR+PREV)/CURR)
      IF (TEST-PIN)435.430.430
430    ILIM = ILIM * 2
      DX = DX/2.
      DY = DY/2.
      TO 410
      AT 435 HAVE FINAL VALUE OF INTEGRATION IN CURR.
435    GO TO 440,445,455,INDIC
440    RC = CURR
      GO TO 460
      FIRST = CURR
445    INDIC = 3
450    XA = XLOC
      YA = 0.
      XB = X2
      YB = Y2
      GO TO 300
      RC = FIRST + CURR

```

48 460 CON(NC)=CON(NC)+RC*QL
 470 CONTINUE
 CO(NC)=1. DE+5*CON(NC)
 QLSS=0.0087*CON(NC)
 WRIT E1 TWRI*660)XXRR(NC)*XXSR(NC)*ZR(NC)*CON(NC),CLSS
 FORM AT (1H ,3(F10.4,2X),F10.0,F10.3)
 660 CONTINUE
 RETURN
 END

32 COMMENT CARDS 1 CONTINUATION CARDS 74 NUMBERED STATEMENTS

```

SUBROUTINE DBTRCX (U,Z,H,HL,X,XY,Y,KST,AN,M,SY,SZ,RC)
  THIS IS THE 1972 VERSION OF DBTRCX.
  SUBROUTINE DBTRCX CALCULATES CHI/Q CONCENTRATION VALUES • DB TRCX
  CALLS UPON SUBROUTINE DBTSIG TO OBTAIN STANDARD DEVIATIONS .
  THE INPUT VARIABLES ARE . . .
    U WIND SPEED (M/SEC)          1 HIWAY424
    Z RECEPTOR HEIGHT (M)        2 HIWAY425
    H EFFECTIVE STACK HEIGHT (M) 3 HIWAY425
    HL HEIGHT OF LIMITING LID (M) 4 HIWAY426
    X DISTANCE RECEPTOR IS DOWNWIND OF SOURCE (KM) 5 HIWAY427
    XY X+VIRTUAL DISTANCE USED FOR A SOURCE APPROX. (KM) 6 HIWAY428
    Y DISTANCE RECEPTOR IS CROSSWIND FROM SOURCE (KM) 7 HIWAY429
    KST STABILITY CLASS         8 HIWAY430
    THE OUTPUT VARIABLES ARE . . .
    AN THE NUMBER OF TIMES THE SUMMATION TERM IS EVALUATED 9 HIWAY431
    AND ADDED IN.          10 HIWAY432
    RC RELATIVE CONCENTRATION (SEC/M**3) 11 HIWAY433
    IWR1 IS CONTROL CODE FOR OUTPUT 12 HIWAY434
    IWR1 = 6
    THE FOLLOWING EQUATION IS SOLVED —
    RC = (1/(2*PI*SIGMA Y*SIGMA Z)) * (EXP (-C. 5*(Y/SIGMA Y)**2))
    (EXP (-C. 5*((Z-H)/SIGMA Z)**2)) + EXP (-C. 5*((Z+H)/SIGMA Z)**2)
    PLUS THE SUM OF THE FOLLOWING 4 TERMS K TIMES (N=1..K) —
    TERM 1- EXP (-C. 5*((Z-H-2NL)/SIGMA Z)**2)
    TERM 2- EXP (-C. 5*((Z+H-2NL)/SIGMA Z)**2)
    TERM 3- EXP (-C. 5*((Z-H+2NL)/SIGMA Z)**2)
    TERM 4- EXP (-C. 5*((Z+H+2NL)/SIGMA Z)**2)
    THE ABOVE EQUATION IS SIMILAR TO EQUATION (5.8) P 36 IN
    WORKBOOK OF ATMOSPHERIC DISPERSION ESTIMATES WITH THE ADDITION
    OF THE EXPONENTIAL INVOLVING Y.
    IF THE SOURCE IS ABOVE THE LID, SET RC = 0., AND RETURN .
    IF (H-HL) > 302.304          3 HIWAY455
 302  IF (Z-HL) > 300.30          4 HIWAY456
 304  IF (Z-HL) > 306.306         5 HIWAY457
 306  WRITE(IWR1, 307)           6 HIWAY458
 307  FORMAT (1HO, 'BOTH H AND Z ARE ABOVE THE MIXING HEIGHT SO A RELIABL
    *E COMPUTATION CAN NOT BE MADE.') 7 HIWAY459
    HIWAY460

```

```

30      RC=0.
      RETURN
      IF X IS LESS THAN 1 METER, SET RC=0, AND RETURN. THIS AVOIDS
      PROBLEMS OF INCORRECT VALUES NEAR THE SOURCE.
      IF (X < 0.001) 30, 310
      CALL DBTSIG TO OBTAIN VALUES FOR SY AND SZ
      CALL DBTSIG (X,XY,KST,SY,SZ)
      SY = SIGMAY, THE STANDARD DEVIATION OF CONCENTRATION IN THE
      Y-DIRECTION (M)
      SZ = SIGMAZ, THE STANDARD DEVIATION OF CONCENTRATION IN THE
      Z-DIRECTION (M)
      C1 = 1.
      IF (Y) 5, 400, 5
      YD = 1000. * Y
      YD IS CROSSWIND DISTANCE IN METERS.

      DUM = YD / SY
      TEHP = 0.5 * DUM * DUM
      IF (TEMP < -5.0.) 16, 30, 30
      C1 = EXP (TEMP)
      IF (KST = 4) 14, 01, 401, 403
      IF (HL = 50.00) 17, 403, 403
      19, 401, 403
      IF STABLE CONDITION OR UNLIMITED MIXING HEIGHT.
      USE EQUATION 3.2 IF Z = 0, OR EG 3.1 FOR NON-ZERO Z.
      C2 = 2.* SZ * SZ
      IF (Z) 30, 404, 406
      C3 = H * H / C2
      IF (C3 - 50.) 405, 30, 30
      A2 = 1. / EXP (C3)
      WADE EQUATION 3.2.
      RC = A2 / (3.14159 * U * SY * SZ * C1)
      H = 1
      RETURN
      A2 = 0.
      A3 = 0.
      CA = Z + H
      CB = Z * H
      8 HIWAY461
      9 HIWAY462
      10 HIWAY465
      11 HIWAY466
      11 HIWAY467
      11 HIWAY468
      11 HIWAY469
      11 HIWAY470
      12 HIWAY471
      12 HIWAY472
      13 HIWAY473
      14 HIWAY474
      14 HIWAY475
      15 HIWAY476
      15 HIWAY477
      16 HIWAY478
      17 HIWAY479
      18 HIWAY480
      19 HIWAY481
      20 HIWAY482
      20 HIWAY483
      20 HIWAY484
      21 HIWAY485
      22 HIWAY486
      23 HIWAY487
      24 HIWAY488
      25 HIWAY489
      26 HIWAY490
      26 HIWAY491
      27 HIWAY492
      28 HIWAY493
      29 HIWAY494
      30 HIWAY495
      31 HIWAY496
      32 HIWAY497

```

```

C3 = CA*CA/C2          33 HIWAY498
C4 = CB*CB/C2          34 HIWAY499
IF (C3-50.) 407,408,408 35 HIWAY500
IF (C3-50.) 409,411,411 36 HIWAY501
IF (C4-50.) 409,411,411 37 HIWAY502
A3 = 1./EXP(C4)          38 HIWAY503
WADE EQUATION 3.1.      39 HIWAY504
RC = (A2 + A3)/16.28318*U*SY*SZ*C1) 40 HIWAY505
N = 2                   41 HIWAY507
RE TURN
C   IF SIGMA-Z IS GREATER THAN 1.6 TIMES THE MIXING HEIGHT.
C   THE DISTRIBUTION BELOW THE MIXING HEIGHT IS UNIFORM WITH
C   HEIGHT REGARDLESS OF SOURCE HEIGHT.
C   IF (SZ/HL - 1.6) 9,8
C   WADE EQUATION 3.5.
C   RC = 1./ (2.5066*U*SY*HL*C1)
C   N = 3
RE TURN
C   INITIAL VALUE OF AN SET = 0.
AN = 0.
IF (N > 3) 34,C=40:
C   IF STATEMENTS 40,16,17, CALCULATE SOURCE HEIGHT CONCENTRATION
C   IN WHICH THE SMOOTHING FUNCTION IS 50% OF THE PREVIOUS
C   VALUES ARE USED IN A CYCLIC MANNER. INTERMEDIATE
C   STATEMENTS ARE PRINTED AT THE END OF EACH CYCLE.
C   PRINTS A DOCUMENT OF THE EXPONENTIAL FUNCTION IS NEVER GREAT THAN .501. IF "AN" BECOMES GREATER THAN .45, A LINE OF OUTPUT IS
C   PRINTED INFORMING OF THIS.
C   CALCULATE MULTIPLE EDDY REFLECTIONS FOR RECEPTOR HEIGHT Z.
A1 = 1./ (6.28318*U*SY*SZ*C1)
C2 = 2.*SZ*SZ
A2 = 0.
A3 = 0.
CA = Z+H
CB = Z+H
C3 = CA*CA/C2
C4 = CB*CB/C2
40

```

```

      IF ( C3=5.0,160,80,80
A2 =1./EXP(C3)
IF (C4=50.,)90,110,110
A3 =1./EXP(C4)
SUM=0.
THL = 2.* HL
AN=AN+1.

120   A4 = 0.
      A5 = 0.
      A6 = 0.
      A7 = 0.

      C5 = AN* THL
      CC = CA-C5
      CO = CB-C5
      CE = CA+C5
      CF = CB+C5
      CS = CC* CC /C2
      CD = CD* CD /C2
      CE = CE* CE /C2
      CF = CF* CF /C2
      IF (C6=50.,)130,150,150
      A4 =1./EXP(C6)
      IF (C7=50.,)160,180,180
      A5 =1./EXP(C7)
      IF (C8=50.,)190,210,210
      A6 =1./EXP(C8)
      IF (C9=50.,)220,240,240
      A7 =1./EXP(C9)
      T=A4+A5+A6+A7
      SUM=SUM+T
      IF (T>0.01)1250,120,120
      RC =A1*(A2+A3+SUM)
      M = 5
      RETURN

130   A4 =1./EXP(C6)
150   IF (C7=50.,)160,180,180
160   A5 =1./EXP(C7)
180   IF (C8=50.,)190,210,210
190   A6 =1./EXP(C8)
210   IF (C9=50.,)220,240,240
220   A7 =1./EXP(C9)
240   T=A4+A5+A6+A7
      SUM=SUM+T
      IF (T>0.01)1250,120,120
      RC =A1*(A2+A3+SUM)
      M = 5
      RETURN

250   C   CALCULATE MULTIPLE EDDY REFLECTIONS FOR GROUND LEVEL RECEIVER H
      A1 = 1./(6.28318*SY*SZ*C1)
      A2 = 0.

      56 HIWAY535
      57 HIWAY536
      58 HIWAY537
      59 HIWAY538
      60 HIWAY539
      61 HIWAY540
      62 HIWAY541
      63 HIWAY542
      64 HIWAY543
      65 HIWAY544
      66 HIWAY545
      67 HIWAY546
      68 HIWAY547
      69 HIWAY548
      70 HIWAY549
      71 HIWAY550
      72 HIWAY551
      73 HIWAY552
      74 HIWAY553
      75 HIWAY554
      76 HIWAY555
      77 HIWAY556
      78 HIWAY557
      79 HIWAY558
      80 HIWAY559
      81 HIWAY560
      82 HIWAY561
      83 HIWAY562
      84 HIWAY563
      85 HIWAY564
      86 HIWAY565
      87 HIWAY566
      88 HIWAY567
      89 HIWAY568
      90 HIWAY570
      91 HIWAY571

```

```

C2 = 2.*SZ*SZ          92 HIWAY572
C3 = H*H/C2           93 HIWAY573
IF (C3-50.) 360.*410.*410    94 HIWAY574
360 A2 = 2.*EXP(C3)      95 HIWAY575
410 SUM = 0.             96 HIWAY576
THL = 2.*HL            97 HIWAY577
420 AN = AN + 1.        98 HIWAY578
A4 = 0.*               99 HIWAY579
A5 = D.*               100 HIWAY580
C5 = AN*THL            101 HIWAY581
CC = H-C5              102 HIWAY582
CE = H + C5            103 HIWAY583
C6 = CC*CC/C2          104 HIWAY584
C8 = CE*CE/C2          105 HIWAY585
IF (C6-50.) 430.*480.*430    106 HIWAY586
430 A4 = 2.*EXP(C6)      107 HIWAY587
480 IF (C8-50.) 490.*540.*540    108 HIWAY588
490 A6 = 2.*EXP(C8)      109 HIWAY589
540 T = A4 + A6          110 HIWAY590
SUM = SUM + T           1.1 HIWAY591
IF (T-0.01) 550.*420.*420    112 HIWAY592
550 RC = A1 * (A2 + SUM)    113 HIWAY593
M = 4                  114 HIWAY594
RETURN                 115 HIWAY595
END                   116 HIWAY596

```

56 COMMENT CARDS 1 CONTINUATION CARDS

41 NUMBERED STATEMENTS

```

SUBROUTINE DBTSIG (X,XY,KST,SY,SZ)
DIMENSION XA(7),XB(2),XD(5),XE(8),XF(9),AA(8),BA(8),AB(3),BB(3),
* A(6),BD(6),AE(9),BE(9),AF(10),BF(10)
DATA XA/.5,.4,.3,.2,.15,.1/
DATA XB/.4,.2/
DATA XD/.3,.1,.3,.1,.3/
DATA XE/.4,.2,.1,.4,.2,.1,.3,.1/
DATA XF/.6,.3,.15,.7,.3,.2,.1,.7,.2/
DATA AA/.453,.85,.346,.75,.258,.89,.21,.7,.41,.179,.52,.17,.22,.158,.08,.122,.8/
DATA BA/.2,.166,.1,.7283,.1,.4,.94,.1,.2644,.1,.1262,.1,.09332,.1,.0542,.0,.9447/
DATA AB/.109,.3,.30,.98,.4,.83,.90,.67,.3/
DATA BB/.1,.0971,.0,.98332,.0,.93198/
DATA AD/.44,.053,.36,.650,.33,.504,.32,.093,.32,.093,.32,.093,.32,.093,.32,.093,
DATA BD/.0,.51179,.0,.56589,.0,.60486,.0,.64463,.0,.81066,.0,.86974/,
DATA AE/.47,.618,.35,.420,.26,.97,.24,.703,.22,.53,.4,.21,.628,.23,.331,
* 24.26 /
DATA BE/.0,.29592,.0,.37615,.0,.46713,.0,.50527,.0,.57154,.0,.63077,.0,.75660,
* 0,.1956,.0,.8366/
DATA AF/.74,.219,.27,.074,.22,.651,.17,.836,.16,.187,.14,.823,.13,.953,
* 14.457,.15,.209,
DATA BF/.0,.21716,.0,.27436,.0,.32681,.0,.41507,.0,.46490,.0,.54563,.0,.53227,
* 0,.68465,.0,.78437,.0,.81558,
60 T0 (10,20,30,40,50,60),KST
C      STABILITY A (10)
10      TH = (.24,.167 - 2.5334*ALOG(XY)),/57.2358
IF (X.GT.-3.11) GO TO 69
DO 11 ID = 1,7
IF (X.GE.XA(ID)) GO TO 12
11      CONTINUE
ID = 8
12      SZ = AA(ID) * X ** BA(ID)
C      STABILITY B (20)
20      TH = (.18,.333 - 1.8096*ALOG(XY))/57.2958
IF (X.GT.35.) GO TO 69
DO 21 ID = 1,2
IF (X.GE.XB(ID)) GO TO 22
21      CONTINUE
GO TO 71
22      ID = 8
SZ = AA(ID) * X ** BA(ID)
23      STABILITY C (20)
24      TH = (.18,.333 - 1.8096*ALOG(XY))/57.2958
IF (X.GT.35.) GO TO 69
DO 25 ID = 1,2
IF (X.GE.XB(ID)) GO TO 26
25      CONTINUE
GO TO 71
26      ID = 8
SZ = AA(ID) * X ** BA(ID)
27      STABILITY D (20)
28      TH = (.18,.333 - 1.8096*ALOG(XY))/57.2958
IF (X.GT.35.) GO TO 69
DO 29 ID = 1,2
IF (X.GE.XB(ID)) GO TO 30
29      CONTINUE
GO TO 71
30      ID = 8
SZ = AA(ID) * X ** BA(ID)

```

```

21  CONTINUE
ID = 3
SZ = AB(ID) * X ** BB(ID)
60 T 0 70
      STABILITY C { 30 }
C   TH = { 12.5 - 1.0857 * AL06(XY) } / 57.2958
SZ = 61.141 * X * Q.91465
60 T 0 70
      STABILITY D { 40 }
C   TH = { 8.3333-0.72382 * AL06(XY) } / 57.2958
DO 41 ID = 1,5
IF (X.GE.XD(ID)) GO TO 42
CONTINUE
41 ID = 6
SZ = AD(ID) * X ** BD(ID)
60 T 0 70
      STABILITY E { 50 }
C   TH = { 6.25 - 0.54287 * AL06(XY) } / 57.2958
DO 51 ID = 1,8
IF (X.GE.XE(ID)) GO TO 52
CONTINUE
51 ID = 9
SZ = AE(ID) * X ** BE(ID)
60 T 0 70
      STABILITY F { 60 }
C   TH = { 4.1667 - 0.36191 * AL06(XY) } / 57.2958
DO 61 ID = 1,9
IF (X.GE.XF(ID)) GO TO 62
CONTINUE
61 ID = 10
SZ = AF(ID) * X ** BF(ID)
60 T 0 70
SZ = 5000.
69 T 0 71
IF (SZ.GT.5000.) SZ = 50.00.
70 SY = 1000. * XY * SIN(TH) / (2.15 * COS(TH))
RE TURN

```

END
 6 COMMENT CARDS 5 CONTINUATION CARDS 19 NUMBERED STATEMENTS

```

FUNCTION XWY (SY0,KST)
GO TO (1,2,3,4,5,6),KST
XY Y = (SY0/213.)**1.1148
1   RETURN
XY Y = (SY0/155.)**1.097
2   RETURN
XY Y = (SY0/103.)**1.092
3   RETURN
XY Y = (SY0/68.)**1.076
4   RETURN
XY Y = (SY0/50.)**1.086
5   RETURN
XY Y = (SY0/33.5)**1.093
6   RETURN
END

0 COMMENT CARDS    0 CONTINUATION CARDS    6 NUMBERED STATEMENTS
  1 HIWAY672
  2 HIWAY673
  3 HIWAY674
  4 HIWAY675
  5 HIWAY676
  6 HIWAY677
  7 HIWAY678
  8 HIWAY679
  9 HIWAY680
10 HIWAY681
11 HIWAY682
12 HIWAY683
13 HIWAY684
14 HIWAY685
15 HIWAY686

```

```

FUNCTION XYZ (SZ0•KST)
DIMENSION SA(7),SB(2),SD(5),SE(8),SF(9),AA(8),AB(3),AD(6),AE(9),
* AF(10),CA(8),CB(3),CD(6),CE(9),CF(10),
DATA SA /13.95,21.40,29.3,37.67,47.44,71.16,104.65,
DATA SB /20.23,40./
DATA SD /12.09,32.09,65.12,1.34,3,251,2/
DATA SE /3.534,8.698,21.628,33.489,49.757,79.07,109.3,141.86,
DATA SF /4.093,10.93,13.953,21.627,26.976,46.0,54.83,68.84,83.25,
DATA AA /122.8,158.08,170.22,179.52,217.41,258.89,346.75,453.85,
DATA AB /90.673,98.483,109.3/
DATA AD /34.459,32.093,32.093,33.504,36.85,44.0,53,
DATA AE /24.26,23.331,21.628,21.628,22.534,24.7C,3,26.97,35.42,
* 47.61,8/
DATA AF /15.209,14.457,13.953,13.953,14.82,3.16,1.87,1.7,83E,22.651,
* 27.074,34.219,
DATA CA /1.0585,0.9486,0.9147,0.8879,0.7909,0.7095,0.5786,0.4725,
DATA CB /1.073,1.017,0.9115,
DATA CD /1.1498,1.2336,1.5527,1.6533,1.7671,1.9539,
DATA CE /1.1953,1.2202,1.3217,1.5854,1.7497,1.9791,2.1407,2.6585,
* 3.379,3/
DATA CF /1.2261,1.2754,1.4606,1.5816,1.8348,2.151,2.4092,3.6599,
* 3.6448,4.6049,
GO TO (10,20,30,40,50,60),KST
C      STABILITY A(10)
10     DO 11 ID = 1,7
      IF (SZ0•LE,SA(ID)) GO TO 12
11     CONTINUE
      ID = 8
12     XYZ = SZ0/AA(ID)*CB(ID)
      RETURN
C      STABILITY B (20)
20     DO 21 ID = 1,2
      IF (SZ0.LE,SB(ID)) GO TO 22
21     CONTINUE
      ID = 3
22     XYZ = (SZ0/SB(ID))*CB(ID)
      RETURN
1   HIWAY687
2   HIWAY688
3   HIWAY689
4   HIWAY690
5   HIWAY691
6   HIWAY692
7   HIWAY693
7   HIWAY694
8   HIWAY695
9   HIWAY696
10  HIWAY697
11  HIWAY698
12  HIWAY700
13  HIWAY701
14  HIWAY702
14  HIWAY703
15  HIWAY704
16  HIWAY705
16  HIWAY706
17  HIWAY707
18  HIWAY708
18  HIWAY709
19  HIWAY710
19  HIWAY711
20  HIWAY712
21  HIWAY713
22  HIWAY714
23  HIWAY715
24  HIWAY716
25  HIWAY717
26  HIWAY718
27  HIWAY719
27  HIWAY720
28  HIWAY721
29  HIWAY722
30  HIWAY723

```

```

C      STABILITY C (30)
30    XVZ = (SZ0/61.141)**1.0933
RE TURN
C      STABILITY D (40)
40    DO 41 ID = 1*5
      IF (SZ0.LE.SD(ID)) GO TO 42
      CONTINUE
      ID = 5
      XVZ = (SZ0/AD(ID))**CD(ID)
RE TURN
C      STABILITY E (50)
50    DO 51 ID = 1*8
      IF (SZ0.LE.SE(ID)) GO TO 52
      CONTINUE
      ID = 9
      XVZ = (SZ0/AE(ID))**CE(ID)
RE TURN
C      STABILITY F (60)
60    DO 61 ID = 1*9
      IF (SZ0.LE.SF(ID)) GO TO 62
      CONTINUE
      ID = 10
      XVZ = (SZ0/AF(ID))**CF(ID)
RE TURN
END

```

6 COMMENT CARDS

5 CONTINUATION CARDS

16 NUMBERED STATEMENTS

```

HIWAY724
31 HIWAY725
32 HIWAY726
33 HIWAY727
34 HIWAY728
35 HIWAY729
36 HIWAY730
37 HIWAY731
38 HIWAY732
39 HIWAY733
40 HIWAY734
41 HIWAY735
42 HIWAY736
43 HIWAY737
44 HIWAY738
45 HIWAY739
46 HIWAY740
47 HIWAY741
48 HIWAY742
49 HIWAY743
50 HIWAY744
51 HIWAY745
52 HIWAY746
53 HIWAY747
54 HIWAY748

```

TECHNICAL REPORT DATA (Please read Instructions on the reverse before completing)		
1. REPORT NO. EPA-650/4-74-008	2.	3. RECIPIENT'S ACCESSION NO.
4. TITLE AND SUBTITLE USER'S GUIDE FOR HIWAY: A HIGHWAY AIR POLLUTION MODEL		5. REPORT DATE February 1975
6. PERFORMING ORGANIZATION CODE		
7. AUTHOR(S) John R. Zimmerman,* and Roger S. Thompson		8. PERFORMING ORGANIZATION REPORT NO.
9. PERFORMING ORGANIZATION NAME AND ADDRESS National Environmental Research Center Office of Research and Development U.S. Environmental Protection Agency Research Triangle Park, N.C. 27711		10. PROGRAM ELEMENT NO. 1AA009
11. CONTRACT/GRANT NO.		
12. SPONSORING AGENCY NAME AND ADDRESS		13. TYPE OF REPORT AND PERIOD COVERED Final report
		14. SPONSORING AGENCY CODE
15. SUPPLEMENTARY NOTES *On assignment from the National Oceanic and Atmospheric Administration, U.S. Department of Commerce		
16. ABSTRACT A computer model, called HIWAY, that can be used for estimating the concentrations of nonreactive pollutants from highway traffic is described. This steady-state Gaussian model can be applied to determine air pollution concentrations at receptor locations downwind of "at-grade" and "cut-section" highways located in relatively uncomplicated terrain. For an at-grade highway, each lane of traffic is modeled as though it were a finite, uniformly emitting line source of pollution. For the cut section, the top of the cut is considered an area source. The area source is simulated by using ten line sources of equal source strength. The total source strength equals the total emissions from the lanes in the cut. The air pollution concentration representative of hourly averaging times at a downwind receptor location is found by a numerical integration along the length of each lane and a summing of the contributions from each lane. With the exception of receptors directly on the highway or within the cut, the model is applicable for any wind direction, highway orientation, and receptor location. The model was developed for situations in which horizontal wind flow occurs. The model cannot consider complex terrain or large obstructions to the flow such as buildings or large trees. An interactive version of the computer model is available on Environmental Protection Agency's Users' Network for Applied Modeling of Air Pollution (UNAMAP).		
17. KEY WORDS AND DOCUMENT ANALYSIS		
a. DESCRIPTORS Air pollution Turbulent diffusion Highway transportation Meteorology Mathematical models Computer models	b. IDENTIFIERS/OPEN ENDED TERMS Dispersion Air quality simulation model	c. COSATI Field/Group
18. DISTRIBUTION STATEMENT Release unlimited		19. SECURITY CLASS (This Report) Unclassified
		20. SECURITY CLASS (This page) Unclassified
		21. NO. OF PAGES 74
		22. PRICE

