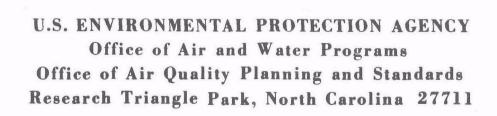
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AIR POLLUTION/LAND USE
PLANNING PROJECT
VOLUME II. METHODS FOR
PREDICTING AIR POLLUTION
CONCENTRATIONS FROM
LAND USE



# AIR POLLUTION/LAND USE PLANNING PROJECT VOLUME II. METHODS FOR PREDICTING AIR POLLUTION CONCENTRATIONS FROM LAND USE

by ·

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### **ABSTRACT**

In order to evaluate or rank land use plans in terms of air quality, it is necessary for planners to be able to project emission density (mass of pollutant per unit of land for any specified time period) using only planning variables, because detailed source characteristics are not available at the time alternative plans are being developed and evaluated. The objective of this study is to analyze the utility of various land use parameters in describing the air quality impacts of land use plans.

Parameters that are tested include land use by zoning class and 2-digit SIC code, employment dwelling units, and square footage of floor space. Variables that are to be explained by these parameters include air quality as represented by the Air Quality Display Model (AQDM), emissions and emission densities, process weight for industrial sources, and energy consumption.

The basic criterion for evaluating the land-use-based emission estimation methods is the ability of the estimates to reproduce regional air quality as represented by the AQDM dispersion model, using the best available point-source inventory information. When data deficiencies prohibit the application of this criterion, standard statistical measures are applied. Statistical techniques used are analysis of variance, multiple regression, and product-moment correlation analysis. Emission inventory and land use data are drawn from the Chicago metropolitan study area.

### 1.0 INTRODUCTION

In order to evaluate or rank land use plans in terms of air quality, it is necessary for planners to be able to project emission density (mass of pollutant per unit of land for any specified time period) using only planning variables, because detailed source characteristics are not available at the time alternative plans are being developed and evaluated. The planning parameters tested in this study include mean emission densities by zoning categories or by 2-digit SIC classification, land utilization, employment, and building size. The variables to be estimated include energy and process throughput; these, in turn, determine fuel combustion and process emissions, respectively. The objectives of the study were (1) to determine what information routinely collected or available in the planning process could be used to quantitatively estimate air quality; and (2) to determine which classification structures or additional parameters should be used in the planning process in order to carry out air quality analyses of land use plans. The tests of utility of each type of classification or each parameter are based on statistical criteria and/or the resulting air quality representation when inserted in the Air Quality Display Model (AQDM) dispersion model. 1 Statistical techniques include analysis of variance, simple correlation, and multiple regression.

It is assumed that manufacturing land is sufficiently distinct in emission characteristics to be analyzed separately from residential and commercial land. Residential and commercial land uses are grouped together due to their similar emission characteristics.

The Chicago Metropolitan Air Quality Control Region was used as a study region because of proximity, availability of data, and the large number of diverse manufacturing sources in the region. Emission inventories for the Chicago region collected by the City of Chicago Department of Environmental Control and the State of Illinois Environmental Protection Agency were used for the study. Using these inventories, we employ a number of alternative strategies to develop land-use-based emission factors. Subsequently, we apply these factors to presently available Chicago land use data to evaluate whether the use of these factors can accurately reproduce estimates of present air quality conditions in the Chicago area.

Section 2 of this report characterizes the emission patterns in the study region and analyzes the variance in manufacturing emissions.

Section 3 tests various methods for explaining this variance and predicting emission patterns using the Chicago emission files as a data base. Section 4 summarizes the results of the study. Appendix A describes the Chicago region in terms of factors influencing present and future emission patterns. The remaining Appendices, B-D, contain technical detail, data, and statistical results supporting the text of Section 3.

### 2.0 AN ANALYSIS OF EMISSION PATTERNS

Air pollution emission patterns and their air quality effects in the Chicago region are discussed in the Report Summary, Volume I. This volume focuses on the stationary source patterns in the Chicago region and, in particular, on the sources of suspended particulate matter. This limitation is purely for convenience, and the methods discussed herein are directly applicable to other pollutant forms emitted from stationary sources.

This section presents a detailed analysis of emission patterns in the study region by zoning class and major industrial sector. The results of using mean emission-density estimators by land use classification to predict pollution concentrations are presented. These results provide the rationale for exploring other methods of estimation, as discussed in Section 3.

### 2.1 CURRENT AIR POLLUTION PROBLEMS IN CHICAGO STUDY REGION

Particulate emissions in an urban area result either from the combustion of fuels containing ash or from industrial plants that produce dust particles during the manufacturing process. High air pollution concentrations in the Chicago area are due primarily to the intense residential and commercial land uses surrounding the central business district (CBD or Loop area of Chicago) and the heavily concentrated industrial areas to the south and southwest of the CBD. Figure 2.1 shows the suspended particulate isopleths (lines of constant concentrations) and the concentration peaks

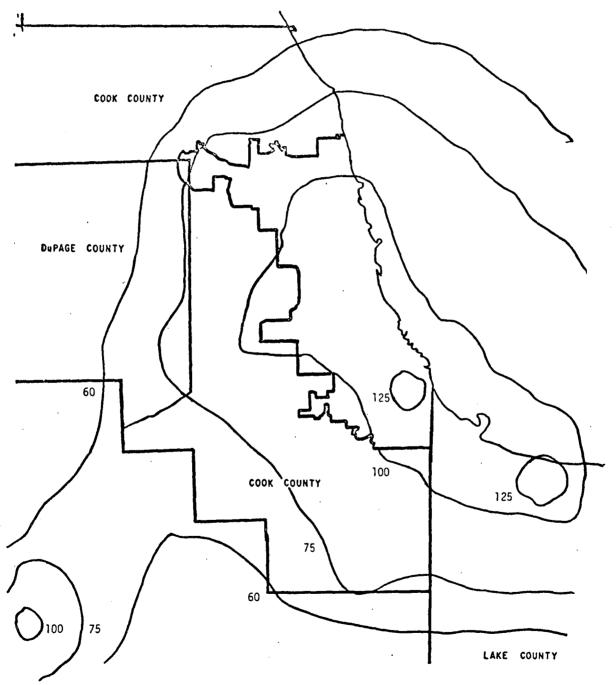


Figure 2.1. Isopleths of suspended particulates using unregulated emission inventory.

resulting from these two intensive land use clusters.

The State of Illinois has enacted emission control regulations (emission standards) designed to achieve the National Ambient Air Quality Standard (75  $\mu g/m^3$  annual geometric mean) by 1975. These regulations are described in Appendix B. Figure 2.2 shows the forecasted air quality with the control regulations in effect. Although the control regulations will have considerable effect in improving air quality, peak areas at or near the standard will exist. Growth in areas surrounding these peaks will contribute to the degradation of air quality in the area and threaten ambient air quality standards. It is for this reason that this study focuses on the three counties surrounding Chicago; namely, Cook, DuPage, and Will. This is a subregion of the 8-county Standard Metropolitan Statistical Area (six counties in Illinois and two in Indiana) and of the 9-county State of Illinois Economic Planning and Statistical Reporting Region as shown in Figure 2.3.

This study divides land use into two major categories—Manufacturing and Residential/Commercial—because of their distinct emission characteristics. Residential and commercial building emissions are a function of the energy consumed and type of fuel used. Energy consumed is, in turn, a function of area climatology, building size, and type of construction. The intense residential/commercial districts of the City of Chicago are rather unique in that a significant number of buildings are still coal heated. A rather severe restriction on the sulfur content of fuels (1% limit) has drastically increased the number of annual conversions from coal to natural gas or oil in recent years due to the large price differential between low-and high-sulfur coal in the Chicago area. This trend is expected to continue to the point where residential/commercial sources will not be

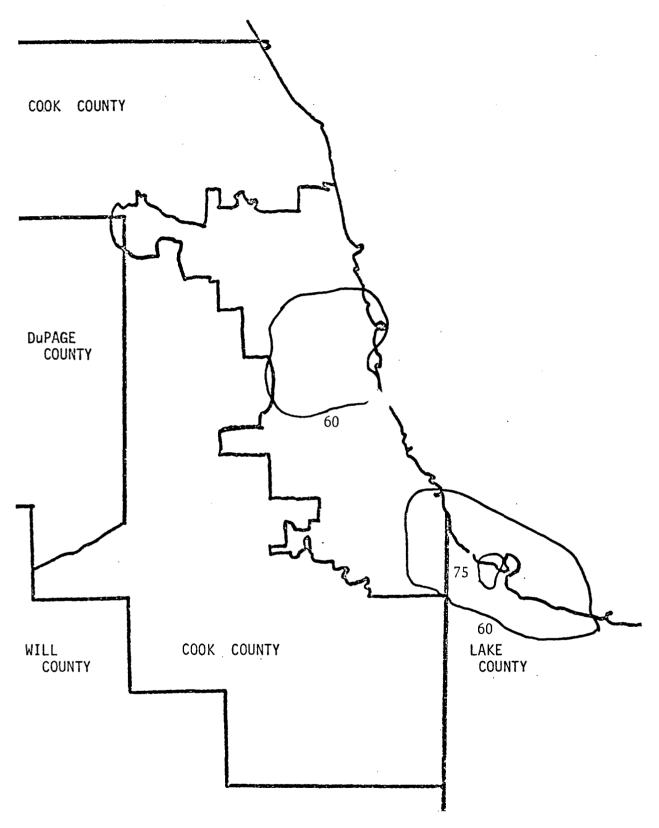


Figure 2.2. Isopleths of suspended particulates with Illinois source control regulations applied.  $(\mu g/m^3 \text{ annual geometric mean})$ 

### CHICAGO REGION

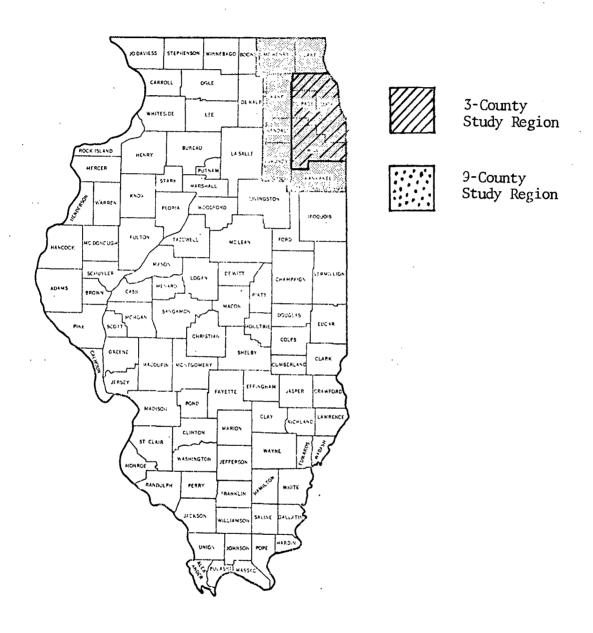


Figure 2.3. State of Illinois, Chicago economic planning and statistical reporting region.

significant contributors to the regional air pollution problem given the availability of low-sulfur fuels. Nonetheless, attempts should be made to estimate this contribution, and a method for making these estimates is discussed in Section 3 of this report.

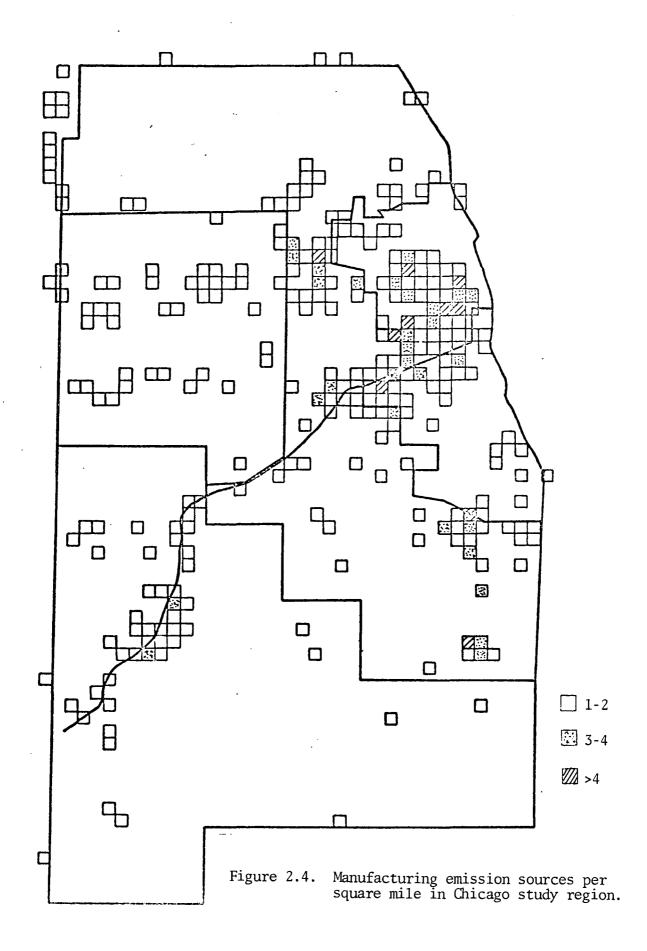
Manufacturing processes and power plants, on the other hand, are now, and are expected to continue to be, major polluting sources, accounting for more than 83% of suspended particulate emissions after source regulation controls are enforced. Manufacturing emissions can be partitioned into emissions due to the nature of the production process itself, due to the combustion of fuels required to carry out the production process, and due to space heating. Manufacturing fuel combustion emissions will continue to be a problem because of the large quantities of fuel consumed. Manufacturers are typically on the low end of the priority list for receiving clean fuel supplies, especially natural gas. The current shortage of clean fuel resources continues to counteract the use of these fuels for manufacturing purposes, however desirable this may be from an air pollution standpoint. Coupled with this shortage of clean fuels is the fact that Illinois is rich in high-sulfur, high-ash bituminous coal reserves and considerable economic pressure exists to utilize these resources. Thus, the planning of manufacturing land use and the location of industrial parks and production facilities that include air pollution considerations are important parts of maintaining air quality standards in a region such as the Chicago Metropolitan Area. Current manufacturing activity in the study region and potential for growth in the area is further described in Appendix A.

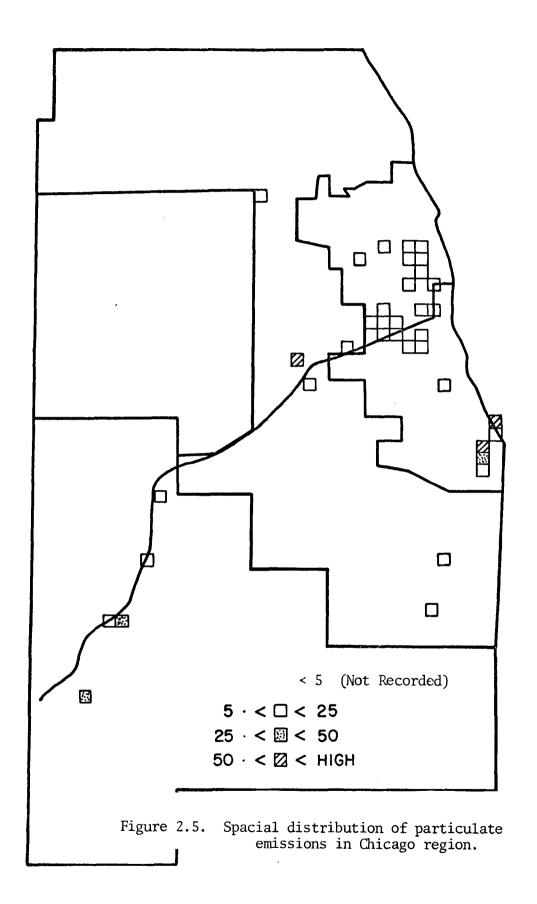
### 2.2 AN ANALYSIS OF VARIANCE IN MANUFACTURING EMISSIONS

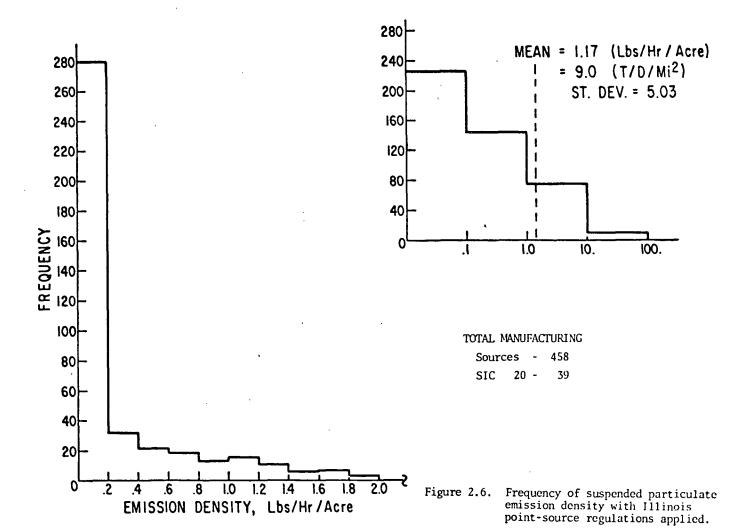
A factor that complicates the analysis of the air pollution impacts of land use plans or development projections is the disaggregated nature of the air pollution problem. Unlike water pollution, there are no centralized processing or treatment plants for which loads can be estimated on an aggregated basis. It is the existence of sources on a diverse geographic plane that constitutes the overall air pollution emission surface of the urban region. Thus, estimation of emissions on a square-mile or square-kilometer grid is required to obtain a realistic picture of air quality.

The spatial distribution of sources from the Chicago emission inventory (see Appendix A) is shown in Figure 2.4, and the resulting particulate emission pattern is shown in Figure 2.5. It is these emission patterns that give rise to the particulate concentration surfaces of Figure 2.1. As can be seen by comparing Figures 2.4 and 2.5, however, it is not the mere existence of a manufacturing source that gives rise to emissions, but also the nature and scale of the production process and space heating requirements. Although high source clusters seem to visually correlate with high emission areas, further explanation of the spatial variance in emissions is required to achieve a realistic estimation of emission patterns in the region.

The need for further analysis can also be viewed statistically as indicated in Figure 2.6 that shows the frequency distribution of industrial source emission densities in the study region. Not only is the standard deviation of this distribution quite high in relation to its average, but the skewness of the distribution causes significant estimation problems if a figure of 1.17 1b/hr/acre is used as an emission density







factor in projecting future air quality. The use of this mean emission density estimate for ranking land use plans was tested by using the AQDM atmospheric dispersion model. Figure 2.7 shows the calculated air quality for suspended particulates as derived by applying a 1.17 lb/hr/acre (9.0 tons/day/mi<sup>2</sup>) emission density factor to the present industrial land use pattern in Chicago. Figure 2.2 indicates suspended particulate air quality estimates based, on the other hand, directly upon the application of standard emission factors to the Chicago Emission Inventory with Illinois source control regulations applied. Comparison of these two figures shows that use of the average emission density factor for industrial lands does produce average air quality estimates that approximate the average air quality over the entire region. However, due to the bias in the estimation of the average emission density factor and the intense clusters of manufacturing land use in the area, pockets of very high concentrations appear in the air quality estimates based upon these factors, as opposed to those based upon the standard emission factors. Thus, if these estimates were used in ranking alternative land use plans, or in trying to identify future potential source clusters in the Chicago area, these average emission density air quality estimates would lead to the belief that air quality standards would not be met under the present conditions of Chicago land use patterns and air quality regulations.

This does not mean that the projections of air quality using these estimators are not a useful tool in ranking the air quality effects of alternative land use plans. Due to the bias of the land use emission density factor estimates, those plans containing a larger percentage of industrial zoned land will, in all probability, be ranked as being likely to produce

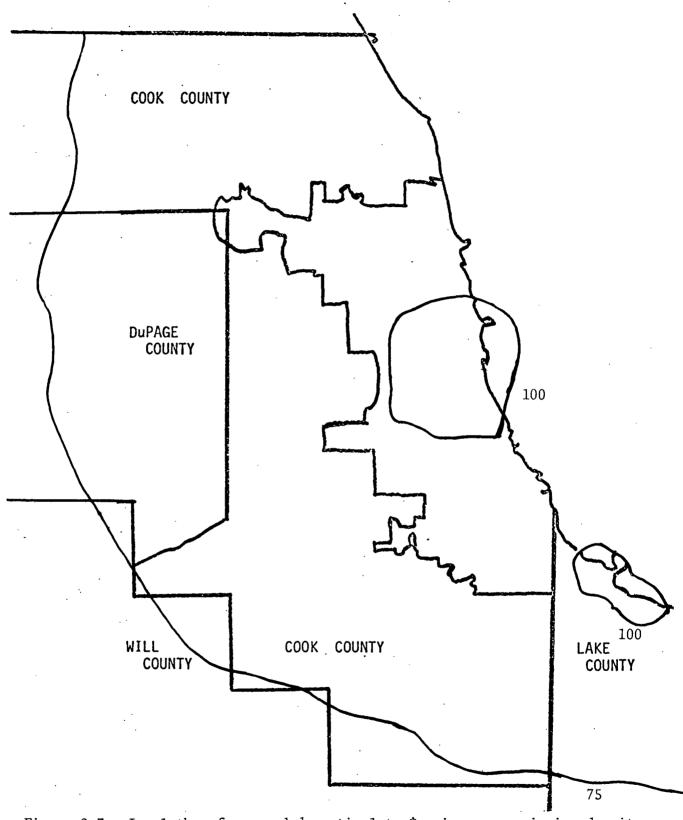


Figure 2.7. Isopleths of suspended particulates\* using mean emission density estimates for manufacturing land (mean = 9.0 T/D/Mi<sup>2</sup> = 1.17 1b/hr/acre) (\* $\mu$ g/m<sup>3</sup> - annual geometric mean)

more significant degradation of air quality than might be justified. We conclude, therefore, that in using the mean estimators for land-use-based emission densities, some further methods must be developed to specifically take into account the skewness and variance of these distributions in projecting future air quality.

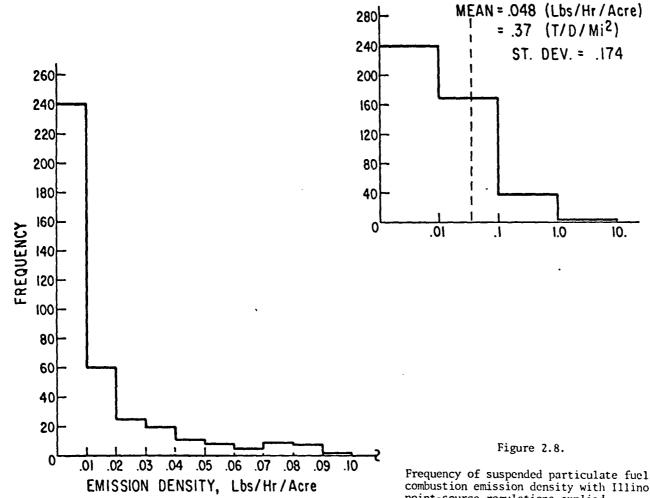
One way to estimate variance is to classify manufacturing sources as process or fuel combustion, as is currently done for control purposes. The dominance of process emissions over fuel combustion emissions is shown by the frequency distributions in Figures 2.8 and 2.9. Examination of the standard deviation of these distributions, compared with the standard deviation of the frequency distribution of the emission densities for the industrial sector as a whole, indicates that almost the entire variance in the emission density estimate is due to the variance of emissions in process sources. Thus, it can be anticipated, that if present industrial land use projections could be disaggregated into process and fuel combustion sources the projected air quality estimates would be somewhat improved. This does not alleviate the need, however, to specifically account for the wide variation in emission densities for industrial process sources.

We conclude that if mean estimators are to be used, a new process of classification must be attempted; the process may require planners to obtain more specific information in order to gain in explanatory power.

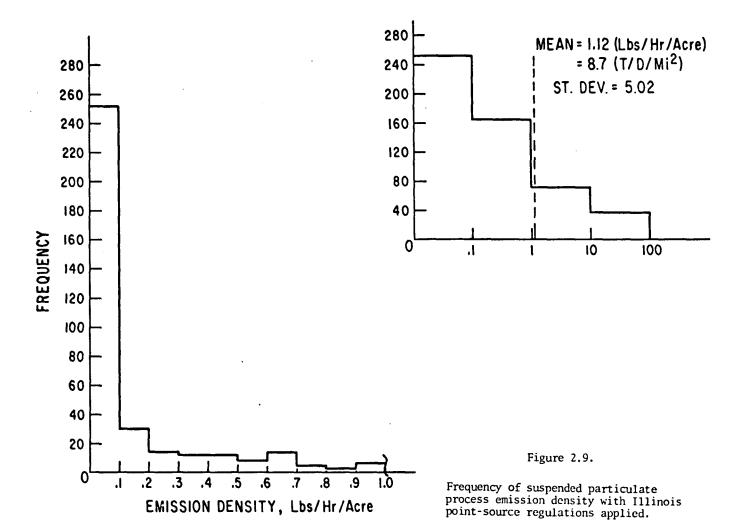
A further explanation using mean estimators was attempted; it groups digit SICs into typical "heavy" and "light" manufacturing land use. A survey<sup>2</sup> of zoning administrators in the Chicago region indicated the following groupings as predominant:

$$G_A^1$$
: Heavy SIC 26 - 33

$$G_{\Lambda}^{2}$$
: Light SIC 20 - 25, 34 - 39.



Frequency of suspended particulate fuel combustion emission density with Illinois point-source regulations applied.



The relevant statistics for this grouping are shown in Tables 2.1, 2.2, and 2.3 for suspended particulate fuel combustion, process, and total manufacturing emission densities, respectively. Again, the dominance of process emission is evident. An analysis of variance between groups indicates that mean process emission densities are significant at the .05 level, but fuel combustion emission densities are not. The significance of process emission densities carries over to total mean emission densities for the two groups.

When the mean estimates are applied to light and heavy manufacturing land use in the Chicago area, a slightly better air quality representation is obtained, as shown in Figure 2.10. A comparison with Figure 2.1 indicates that the peak areas are well represented, but the magnitudes of the peaks remain much too high, indicating a further need for refinement.

A final attempt at mean estimation for manufacturing land was attempted by using the 2-digit SIC classification. Tables 2.4, 2.5, and 2.6 contain the relevant statistics for suspended particulate fuel combustion, process, and manufacturing emission densities, respectively. An analysis of variance between 2-digit SICs shows no significant explanatory power for the emission-density variables. From this result, we are tempted to conclude that knowledge of mean emission densities by 2-digit SIC is of little assistance in predicting emissions and, hence resultant air quality. Land use data by 2-digit SIC was not available to test the resulting air quality representation.

Table 2.1. SUSPENDED PARTICULATE EMISSION DENSITY †
(1bs/hr/acre)

			(,,	• •				
$G_A^1$ (26-33) $G_A^2$ (20-25) $G_A^2$ (24-39)	Unr	egulated S	ource Invent	ory	Regu	lated Sourc	e Inventory	
$G_{A}^{2}$ $\begin{pmatrix} 20-25\\ 24-39 \end{pmatrix}$	Mean	. Median	Std. Dev.	Skewness	Mean	Median	Std. Dev.	Skewness
G <sub>A</sub> <sup>1</sup> (255) G <sub>A</sub> <sup>2</sup> (203)	47.60	.717	472.65	15.48	1.67	.21	6,29	7.63
G <sub>A</sub> (203)	27.24	1.04	164.76	9.63	.54	.04	2.62	8.35
TOTAL	38.57	.92	369.14	18.476	1.17	.104	5.03	9.01
ANOV			4.		F* = 5.65	$DF* = \begin{pmatrix} 1\\454 \end{pmatrix}$		S*(.05)
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	5 - 51gm	ficance le	vel			<u> </u>	'	<u> </u>
	†(by Hea	vy and I	ight Indi	strial Z	oning Cla	ass)		
			:			:		
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Table 2.2. SUSPENDED PARTICULATE FUEL COMBUSTION †

EMISSION DENSITY

(1bs/hr/acre)

		•		(lbs/hr/	ocre)			
GA (26-33)	Unre	gulated So	urce Invento	ory	Regu	ilated Sourc	ce Inventory	,
$G_A^1$ (26-33) $G_A^2$ (20-25) (24-39)	Mean	. Median	Std. Dev.	Skewness	Mean	Median	Std. Dev.	Skewness
GA (255)	.601	.008	6.64	14.13	.058	.005	.208	8.53
$G_A^2$ (203)	.075	.005	.239	5.20	.034	.003	.120	9.53
TOTAL (458)	.370	.006	4.96	18.97	.048	.005	.174	9.44
ANOV	<u> </u>				F* =1.34	$DF^* = 454$		NS
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	*F - F ra	io						
	ĺ	es of free	DFB - Be	}				
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	†(by Hea	vy and I	ight Indi	strial 2	oning Cl	ss)		
	-							
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Table 2.3. SUSPENDED PARTICULATE PROCESS †
EMISSION DENSITY
(1bs/hr/acre)

GA (26-33)	Unre	gulated Sou	rce Invento	ıy	Reg	ulated Sourc	ce Inventor	у
$G_A^2 \left\{ \begin{array}{l} 20-25 \\ 34-39 \end{array} \right\}$	Mean	. Median	Std. Dev.	Skewness	Mean	Median	Std. Dev.	Skewness
G <sub>A</sub> (255)	46.99	.666	472.64	15.48	1.61	.129	6.23	7,63
G <sub>A</sub> <sup>2</sup> (203)	27.16	.998	164.76	9.63	.508	.012	2.61	8.39
TOTAL	38.20	.773	369.12	18.48	1.121	.040	5.02	9.008
ANOV			ý		F* = 5.34	DF* = (154)		S* (.05)
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	DF - Degree	s of freed	DFB - Be	1 1				
<del></del>	S - Signi	ican <u>ce lev</u>						
	†(by Hea	vy and L	ight Ind	ustrial :	Zoning C1	ass)		
			·	·				·

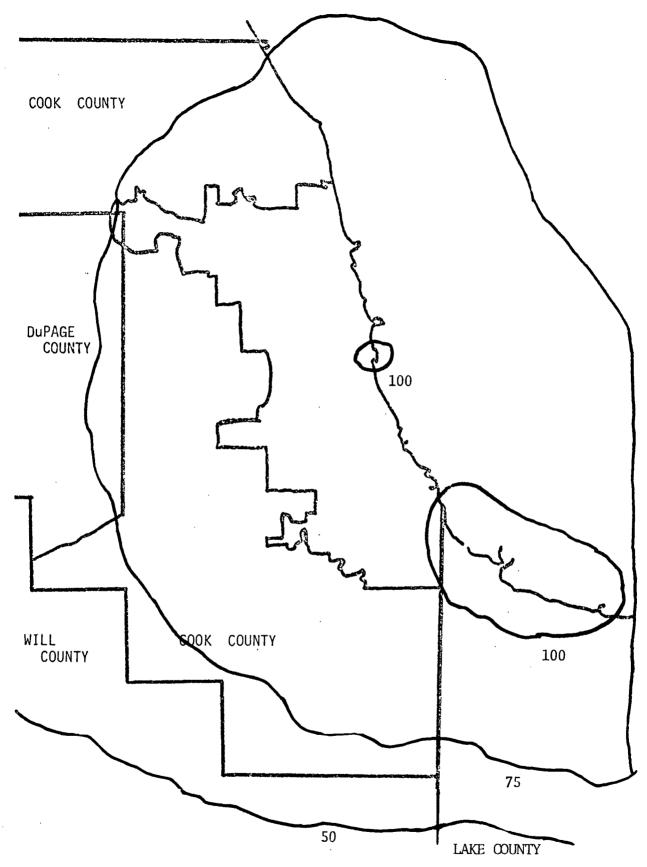


Figure 2.10. Isopleths of suspended particulates\* using mean emission density estimates by manufacturing zoning classification:

Heavy industry = 13.1 T/D/mi<sup>2</sup> = 1.70 1b/hr/acre

Light industry = 4.2 T/D/mi<sup>2</sup> = .55 1b/hr/acre

 $*_{\mu}g/m^3$  annual geometric mean

Table 2.4. SUSPENDED PARTICULATE EMISSION DENSITY † (lbs/hr/acre)

				ir/acrej	·			<del></del>
	Unr	egulated So	ource Invent	tory	R	egulated So	urce Invent	ory
2- Digit SIC (N)	Mean	. Median	Std. Dev.	Skewness	Mean	Median	Std. Dev.	Skewnes
20 (17)	.74	. 09	1.4	2.5	.48	.09	.85	2.4
24 (14)	20.5	3.8	39.5	2.4	.13	.04	. 29	3.2
25 (14)	8.4	2.0	13.0	1.6	.08	.04	.08	.62
26 (20)	29.6	2.4	60.2	2.0	.80	.11	1.88	3.49
27 (9)	50.6	6.4	106.7	2.1	.27	.10	.44	2.15
28 (67)	8.4	.45	29.9	5.66	.95	11	2.74	6.28
29 (35)	17.8	.82	50.6	3.3	4.13	.25	14.12	3.85
30 (13)	2.5	.23	5.3	1.9	.51	.02	1.2	2.54
32 (43)	196.5	1.81	1141.8	6.3	2.35	.61	5.7	4.2
33 (67)	21.2	.65	87.7	6.9	1.36	.35	3.9	6.59
34 (39)	95.7	1.02	362.5	4.2	.63	.16	2.2	5.8
35 (49)	7.8	1.00	34.9	6.5	.88	.04	4.1	6.3
36 (29)	1.7	. 80	2.5	1.9	.21	.02	.39	1.9
37 (12)	51.7	1.6	113.9	2.3	1.72	.02	5.7	3.0
38 (6)	3.5	.26	5.2	.74	.08	.04	.12	1.3
39 (18)	13.1	3.3	21.7	2.1	.14	.03	.27	1.9
TOTAL (458)	38.57	.92	369.14	18.48	1,17	.10	5.03	9.01
ANOV					F=1.229	16 DF=439		NS(.05)
	†(by 2-c	ligit SI	C Code)					

Table 2.5 SUSPENDED PARTICULATE FUEL COMBUSTION EMISSION DENSITY + (1bs/hr/acre)

-	Uni	regulated So	ource Inven	tory	Re	egulated Sou	irce Invento	ory
2- Digit SIC	Mean	. Median	Std. Pev.	Skewness	Mean	Median	Std. Dev.	Skewness
20 (17)	.142	.022	.447	3.7	.049	.016	.095	3.20
24 (14)	.004	0.	.009	2.02	.003	0.	.008	2.27
25 (14)	.016	0.	.026	1.61	.010	0.	.016	1.81
26 (20)	1.64	.01	7.15	4.13	.073	.010	.170	3.44
27 (9)	.036	0.	.088	2.39	.036	0.	.008	2.39
28 (67)	.083	.011	. 263	4.99	.044	.009	.213	6.50
29 (35)	.111	.023	. 224	2.77	.099	.019	.213	2.99
30 (13)	.012	.002	.022	2.40	.011	.002	.002	2.63
32 (43)	2.39	0.	15.42	6.33	.019		.050	4.32
33 (67)	.128	.006	.540	5.59	.082		.327	6.92
34 (39)	.067	.003	. 242	5.53	.064	.003	- 242	5.58
35 (49)	. 101	.004	.301	3.63	.026	.004	.065	4.15
36 (29)	.065	.007	.128	2.23	:042	.003	.080	1.87
37 (12)	. 200	.065	. 255	1.008	.046	.014	.065	1.337
38 (6)	.049	.036	.055	.115	.030	0.	.047	.9
39 (18)	.020	0.	.057	3.57	.008	0.	.014	1.38
TOTAL (458)	.370	.006	4.96	18.97	.048	.005	.174	9.44
ANOV					.473	16 DF=439		NS(.05)
	†(by 2-d	igit SIC	Code)					
	1	i		24			'	

Table 2.6. SUSPENDED PARTICULATE PROCESS

EMISSION DENSITY<sup>†</sup>

(lbs/hr/acre)

	Unre	gulated Sou	irce Invento	ory	Re	gulated Sou	rce Inventor	y
2-Digit SIC (N)	Mean	. Median	Std. Dev.	Skewness	Mean	Modian	Std. Dev.	Skownes
20 (17)	.601	0.	1.39	3.03	.43	0.	.86	2.50
24 (14)	20.46	3.82	39.53	2.42	.125	.035	. 29	3.15
25 (14)	8.38	2.02	13.02	1.62	.071	.021	.083	.69
26 (20)	27.96	2.41	60.41	2.08	.72	.021	1.83	3.55
27 (9)	50.54	6.42	106.7	2.15	. 235	.072	.448	2.20
28 (67)	8.30	.30	29.9	5.67	.906	.024	2.745	6.27
29 (35)	17.7	.75	50.6	3.30	4.032	.173	14.102	3.85
30 (13)	2.55	. 22	5.27	1.96	. 500	.005	1.183	2.58
32 (43)	194.12	1.81	1142.1	6.30	2.33		5.62	4.16
33 (67)	21.1	.62	87.74	6.90	1.27		3.04	6.66
34 (39)	95.61	.883	362.5	4.25	. 564	.126	2.166	5.83
35 (49)	7.67	.871	<b>34.</b> 93	6.46	. 851	.010	4.055	6.28
36 (29)	1.64	.615	2.49	1.915	.1,66	.004	.367	2.16
37 (12) ·	51.45	1.182	113.87	2.25	1.676	0.	5.66	3.01
38 (6)	3.49	.26	5.24'.	.74	.054	0.	.126	1.78
39 (18)	13.08	3.18	21.66	2.05	.134	.006	.276	1.92
TOTAL (458)	38.20	.773	369.13	18.48	1.121	.040	5.021	9.01
:avov					F=1.21	16 DF=439		NS(.05)
	†(by 2-d	igit SIC	Code)					

### 3.0 METHODS FOR ESTIMATING EMISSIONS FROM LAND USE

The analysis of emission density variance described in the preceding section provides the rationale for further investigation into processes and methods for estimating emissions from land use. The description of the current state and potential growth of the Chicago region in Appendix A gives an indication of the parameters that are customarily used and reported in the planning process for forecasting the rate of urbanization and change of settlement patterns of the region. These parameters include rates of change in land use, employment, and productivity for major manufacturing sectors; changes in housing stock and population for residential land; and square footage of floor space for commercial development. section analyzes and tests the utility of certain of these parameters in predicting regional emission and air quality patterns and residential/ commercial land uses. Two criteria were used in evaluating these parameters: (1) the accuracy of the representation of regional air quality produced when the parameter estimates were inserted into the AQDM atmospheric dispersion model, and (2) the reliability of the representation when submitted to standard statistical analyses such as analysis of variance, productmoment correlation, and multiple linear regression.

### 3.1 UNIFORM EMISSION-DENSITY ESTIMATION BY MANUFACTURING ZONING CLASS

The previous section indicated some of the difficulties encountered in using mean emission density estimates by land use class or major industrial sector. The major difficulty stems from the skewness of the emission-density distribution as shown in Figure 2.6. Some improvement is realized if mean emission densities by heavy (HI) and light (LI) industry are used.

In order to obtain a direct comparison between the emission-density approach and the point-source emission factors approach, the AQDM results for each were compared in the <u>uncalibrated</u> model. This merely means that results, before fitting to actual air quality data and adding background concentrations, are to be compared, assuming that the point-source representation is the best attainable with current information. The mean relative error and the standard deviation in the error between air quality concentrations calculated using the point-source representation and those using the emission-density representation are then used to measure the "goodness" of the emission-density representation. Thus:

$$\mu_{R} = \frac{1}{N} \sum_{i} \frac{\Delta \chi_{i}}{\chi_{i}^{PS}}$$
 (3.1)

$$\sigma_{R} = \left[\sum_{N} \frac{\left(\Delta x_{i}\right)^{2}}{N} - \mu_{R}^{2}\right]^{1/2}$$
(3.2)

where

$$\Delta \chi_i = \chi_i^{PS} - \chi_i^{ED}$$
 ,

 $\mu_R$  = the mean relative error ,

 $^{\sigma}_{R}$  = the standard deviation about the mean relative error .

 $\chi_i^{PS}$  = the arithmetic mean air quality concentration calculated at receptor point i using the point-source file ,

 $\mathbf{x}_i^{ED}$  = the arithmetic mean air quality concentration calculated at receptor i using the emission-density representation ,

i = an index of receptor points ,

N = the total number of receptor points.

Using this criterion and the means for heavy and light industry based on the 90% largest source sample (see Appendix A, Section A.4), which are:

$$\tilde{ED}^{HI}$$
 = 18.0 T/D/mi<sup>2</sup> , (means of sample)

$$\bar{ED}^{LI} = 6.0 \text{ T/D/mi}^2$$

The following are obtained:

$$\mu_{R} = -5.86$$

$$\sigma_{\rm p} = 1.48$$

this indicates a severe bias to overprediction. A visual comparison of the resulting air quality is provided in Figures 3.1 and 3.2.

The skewness of the distributions involved would ordinarly argue for using the median as an estimation instead of the mean. For this sample:

$$\widehat{ED}^{HI} = 1.3 \text{ T/D/mi}^2$$
 (medians of sample)

$$\widehat{ED}^{LI} = .23 \text{ T/D/mi}^2$$

and

$$\mu_{R} = \cdot 61$$

$$\sigma_{\rm R}$$
 = .08

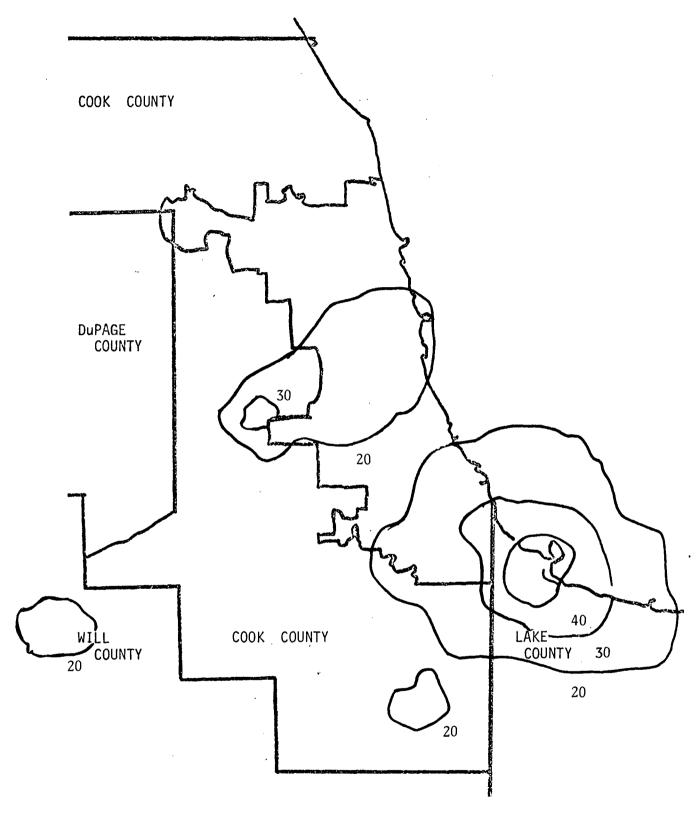


Figure 3.1. Isopleths of suspended particulates\* using point-source representation.

\*( $\mu g/m^3$  - annual arithmetic mean - uncalbirated model)

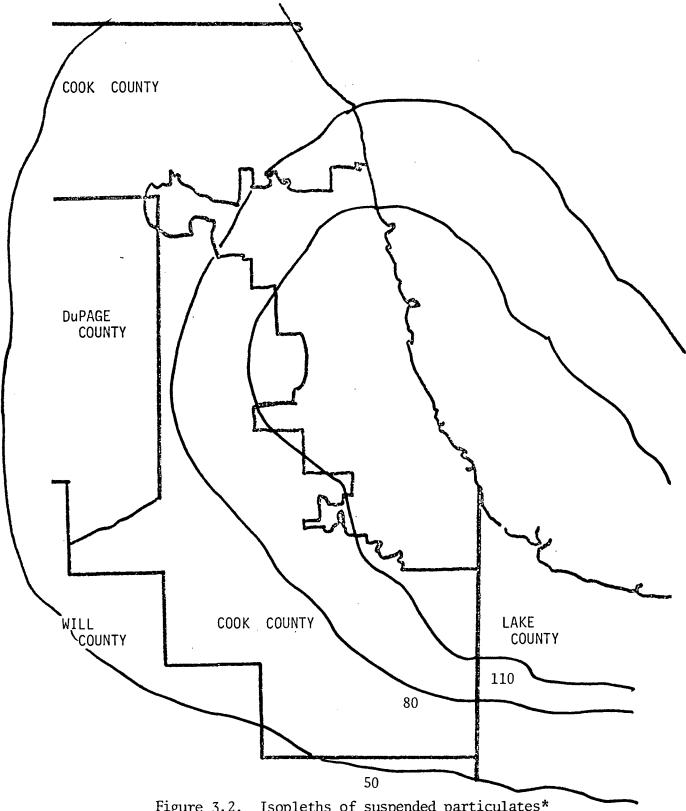


Figure 3.2. Isopleths of suspended particulates\* using mean emission density representation.

(EDHI = 18.0 T/D/mi<sup>2</sup> - EDLI = 6.0 T/D/mi<sup>2</sup>)

\*( $\mu g/m^3$  - annual arithemetic mean - uncalibrated model)

indicating a substantial bias to underprediction. A visual comparison can be made by simultaneously viewing Figures 3.1 and 3.3.

At this point, it is reasonable to ask if a reasonable estimate of air quality concentrations can be made using some emission-density estimates for heavy and light industry. To answer this question, assume that emission-density estimates are free parameters to be chosen so as to achieve a "best fit" in the sense that:

min 
$$\sigma_R$$
 (ED<sup>HI</sup>, ED<sup>LI</sup>) (3.3)  
subject to  $\mu_R$  (ED<sup>HI</sup>, ED<sup>LI</sup>) = 0 .

That is, emission density estimates,  $\tilde{ED}^{HI}$  and  $\tilde{ED}^{LI}$ , are sought which yield the best (least standard deviation), unbiased ( $\mu_R$  = 0) comparison with air quality concentrations as modeled using the point-source information. The analytic solution to this problem is easily worked out (Appendix C), and the results yield:

$$ED^{HI} = 3.53 \text{ T/D/mi}^2 ,$$
 
$$ED^{LI} = .53 \text{ T/D/mi}^2 ,$$
 and 
$$\mu_R = 0 \qquad \text{(by constraint)} ,$$
 
$$\sigma_R = .20$$

The resulting concentration isopleth map is shown in Figure 3.4. Thus, the best fit emission-density representation still leaves a 20% standard deviation in the relative error.

A closer look at the seriousness of this error can be taken if it is assumed that a large relative error in the lower concentration ranges can be tolerated, but, hopefully, the peak concentrations are well represented.

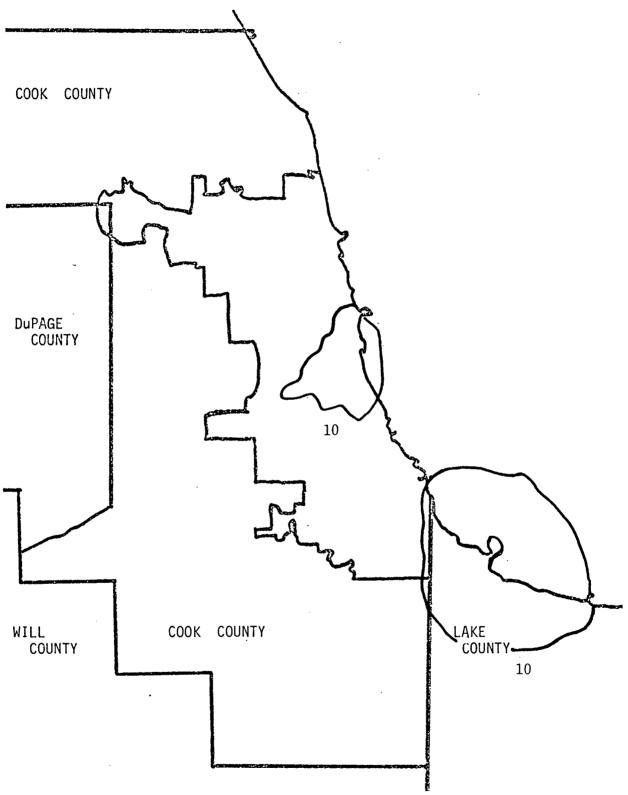


Figure 3.3. Isopleths of suspended particulates\* using median emission density representation.  $(\hat{ED}^{HI} = 1.3 \text{ T/D/mi}^2 - \hat{ED}^{LI} = .23 \text{ T/D/mi}^2)$ 

\*(µg/m $^3$  - annual arithmetic mean - uncalibrated model)

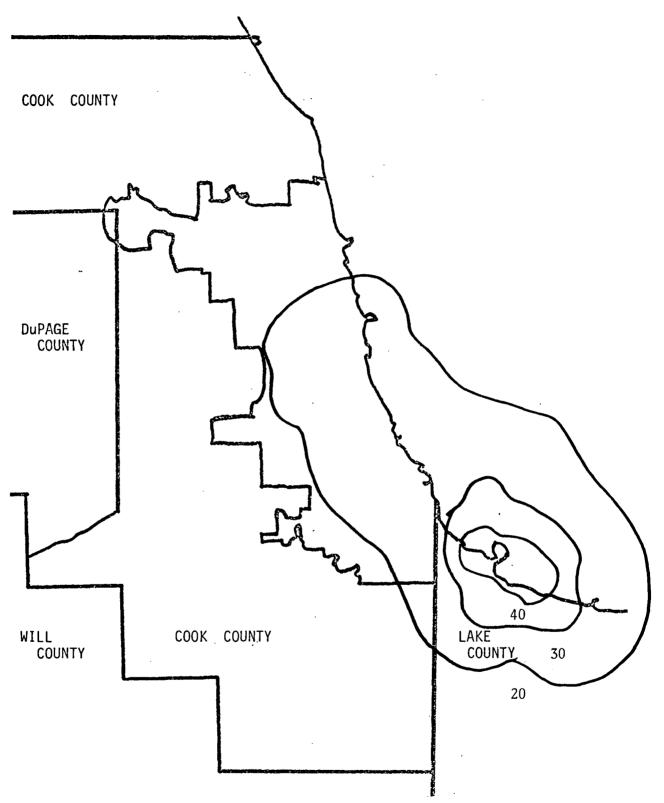


Figure 3.4. Isopleths of suspended particulates\*
using "best fit" emission density representation.

(ED = 3.53 T/D/mi<sup>2</sup> - ED = .53 T/D/mi<sup>2</sup>)

\*( $\mu gm/m^3$  - annual arithmetic mean - uncalibrated model)

Nine receptor points are above 30  $\mu g/m^3$ ; this, when coupled with the normal rural background of 40  $\mu g/m^3$ , can be considered in the critical area of the standard (75 $\mu g/m^3$ ). Using the "best fit" emission-density estimates applied to only these nine points yields:

$$\mu_{R} = .22$$
 ,  $\sigma_{R} = .33$  ,

indicating a strong bias to underprediction, with a large standard deviation of relative error. Thus, it can be concluded that the best fit estimates actually do worse in predicting the higher peak concentrations than lower concentration levels; further, the standard deviation of bias is to underprediction, an undesirable result for estimating peak levels.

Finally, if "best fit" emission density estimates are generated using these nine highest receptor points alone, the results are:

$$\dot{E}_{D}^{HI} = 2.43 \text{ T/D/mi}^2,$$
  
 $\dot{E}_{D}^{LI} = 2.74 \text{ T/D/mi}^2,$ 

where, for the nine highest receptor points,

$$\mu_{\rm R}$$
 = 0 (by constraint).  
 $\sigma_{\rm R}$  = .33 ,

and for all receptor points,

$$\mu_{R} = .86$$
,  $\sigma_{R} = .56$ ,

From these results, it can be concluded that several high receptor points are being influenced by clustered light industrial land use, and even when

these nine points are used to determine best-fit emission-density values, no improvement is observed in the standard deviation of relative error.

All this is at the expense of a substantial bias to overprediction in the remaining receptor points.

It must be concluded, therefore, that (1) either the land use data used for this study is severely in error, or (2) that further explanation is required; e.g., further disaggregation of land use categories, or using intensity measures such as employment density. The land use data was collected from best available sources and is assumed to be sufficiently reliable for purposes of this study. Therefore, the results of this section are assumed to provide the rationale for further investigations as discussed in the next section.

## 3.2 ANALYSIS OF MANUFACTURING EMISSIONS BY

MAJOR INDUSTRIAL SECTOR (2-digit SIC code)

The previous section indicated the need, based on the criteria of air quality representation, for further explanation of manufacturing emissions. Manufacturing land use by heavy and light industry failed to give adequate air quality representation, even when "best fit" emission density estimators were used. The next level of disaggregation is by 2-digit SIC code; however, land use data by 2-digit SIC code was not available in the Chicago area. Therefore, the analysis of this section uses statistical measures to test the utility of various parameters in predicting emissions.

Even if land use were known by 2-digit SIC, the analysis of variance of Section 2 yields discouraging results regarding the use of mean emission-density estimates by the 2-digit classification. This result is reproduced for a subset of major polluting sectors in the Chicago region as shown in

Table 3.1. The variance at the 5% significance level in average emission densities of industries classified by the 2-digit scheme differs only marginally, which, in turn, is due to the large variance of emission density within each 2-digit class. Note, however, that it is the variance in the land variable that is causing this result, since emissions by 2-digit class are significantly different. Thus, justification is provided for attempting to estimate emissions within each 2-digit classification through the use of certain planning parameters. Average employment levels, process weight, and energy are particularly important because they vary significantly among the 2-digit groupings.

In the remainder of this section, the major polluting sectors are investigated in order, as ranked by total controlled emissions. Each sector is characterized with respect to its major contribution to air pollution, process and fuel combustion emission contributions, reductions in emissions achieved by Illinois source control regulations, and the degree of explanation of controlled emissions by employment, land use, process weight, and energy consumption. Descriptions and material presented in the Standard Industrial Cl sification Manual and the Compilation of Air Pollutant Emission Factors are used when necessary to complete the discussion of each 2-digit classification.

Appendix D contains the results of applying correlation and regression analysis to the Chicago emission inventory by 2-digit SIC. In addition to product-moment correlation, four linear regression models are tested for each 2-digit category; these are:

Table 3.1. ANALYSIS OF VARIANCE TEST FOR DIFFERENCE OF MEANS BETWEEN 12 LARGEST POLLUTING SECTORS

Variable	F Value DFB 11 DFW 476	Significance Level
Land	. 54	NS
Employment	4.6	.001
Process Weight	5.2	.001
Energy	2.7	.001
Controlled Emissions	7.2	.001
Controlled Emission Density	1.4	NS

## General Emission Model

$$E^{CT} = A \cdot Pw + B \cdot En + C \cdot Sp + D \cdot Em + E$$
 (3.4)

# Restricted Emission Model

$$E^{CT} = A \cdot Sp + B \cdot Em + C \tag{3.5}$$

# Restricted Process Weight Model

$$Pw = A \cdot Sp + B \cdot Em + C$$
 (3.6)

# Restricted Energy Model

$$En = A \cdot Sp + B \cdot Em + C \tag{3.7}$$

where

E<sup>CT</sup> = controlled emissions (lb/hr)

Pw = process weight flow (t/hr)

En = energy consumption (MBtu/hr)

Sp = space (acres)

Em = employment

and A, B, C, D, and E are linear regression coefficients.

Results of these models are summarized in Table 3.2; the details for the five major polluting sectors are discussed in the remainder of the section. These five sectors account for 272, or 50%, of the sources in the emission inventory file; 76% of the manufacturing land use; 34% of employment; 96.2% of process material flow; 79.9% of energy consumed; and 85% of controlled emissions.

# 3.2.1 SIC 32 Stone, Clay, and Glass Products

Industries in this category manufacture products from materials taken principally from the earth in the form of stone, clay, and sand; such as glass products, cement, structural clay products, pottery; and concrete,

Table 3.2. MULTIPLE REGRESSION R<sup>2</sup> AND INDIVIDUAL VARIABLE CONTRIBUTIONS

		General	Emission	Model		E	stricted mission Model		Proc	stricted ess Weig Model			stricted Energy Model		of Total Emissions	to Process	i due to Fuel Combustion
510	R <sup>2</sup>	₽w	En	Sp	Em	R <sup>2</sup>	Sp	Em	R <sup>2</sup>	Sp	Em	R <sup>2</sup>	Sp	Em			
32	. 57	. 55		.02		.35	.34	.01	_47	.43	.03	.82	.01	. 81	29	97	3
20	.61	.08	.53			.30	. 28	.02				.68	.64	.04	17	70	30
33	.61	. 52	.03		.06	.13		.13	.03		.03	.03		.03	16	90	10
28	.73	.60	.01	.12		.13	,12	.01				.40	.01	. 39	16	82	18
20	.95	.05	.90			.80	,77	.03	.19		,19	.81	.78	.03	7	53	47
35	.93	. 69	.23		.01	.17		.17	.01	.01		.88	.07	. 81	4	65	35
34	.89	.74	.15			.46	.46		.71	.71		.05	.05		3	63	37
21,	.87	, 81	.06			.55	,01	. 54	.51		.51	.17	01	.16	3	80	20
30_	. 67		.44	.42	.01_	.02		.02	.08		.08	.43	.40	.03	1.3	89	11
37	.999	.88	.12			.02	,02		.08	.02	.06	.27		.27	1.1	70	30
39	.999	.999				.05	.05		.06	.06		.30	.30		1,1	82	18
36	.75	. 02	.72		.01	.06		.06	.04	.02	.02	.46		.46	1.0	71	29

gypsum, abrasive and asbestos products. This category accounts for 29% of controlled particulate emissions in the source file; 97% of these emissions are due to the manufacturing processes themselves, while only 3% are due to fuel combustion. This category utilizes 5.5% of the energy consumed or 920 MBtu/hr; of which 833 MBtu/hr are due to the combustion of natural gas. Thus, process emissions are the major air pollution problem in this category.

Estimated uncontrolled process emission factors for various subcategories are shown below:

SIC	Description	Suspended Particulate Emission Factors (1b/ton of finished product)
32	Stone, Glass and Clay	
3211	Flat Glass	2.0
3229	Blown Glass	60.0
3241	Cement	54.0
3251	Brick	180.0
3273	Ready Mix Concrete	0.2
3274	Lime	200.0
3275	Gypsum	132.0
3281	Cut Stone	31.0
3291	Abrasive Products	31.0
3295	Minerals & Earth	77.0
3295	Perlite	21.0
3296	Mineral Wool	50.0
3297	Non-Clay Refractory	225.0

Source: Compilation of Air Pollutant Emission Factors (Revised). U.S. EPA, Office of Air Programs, February 1972.

This category accounts for 61% of process weight flow, amounting to 17,337 tons of material moved per hour. Application of the Illinois control regulations will achieve a reduction in emissions from 88,556 lb/hr to 1330 lb/hr, or 98%. Emissions per ton of process weight will then be .08 lb/T/hr.

Correlation results for this category indicate that controlled emissions are highly correlated (r = .74) with process weight as expected. Since process weight and land are correlated (r = .66), a high correlation (r = .58) between emissions and land is also obtained. Energy and employment are also highly correlated (r = .90).

The general emission model  $R^2$  of .57 is obtained with all five variables entering the equation. However, process weight dominates the explanation contributing an  $R^2$  of .55, while the remaining variables contribute the remaining .02. In the restricted emission model, a multiple  $R^2$  of .35 is obtained primarily from the land variable. For the restricted process weight model, an  $R^2$  of .43 is obtained, again primarily due to the land variable. On the other hand, employment accounts for most of the  $R^2$  of .82 in the restricted energy model. These results indicate that space is the most useful planning variable in predicting controlled emissions in this category.

## 3.2.2 SIC 29 Petroleum Refining and Related Industries

Industries in this category are engaged in petroleum refining, manufacturing of paving and roofing materials, and compounding lubricating oils and greases from purchased materials. This category accounts for 17% of controlled particulate emissions; 70% are due to the manufacturing processes themselves, while 30% are due to fuel combustion. This category utilizes 36% of the energy consumed, or 6036 MBtu/hr; of which 5115 MBtu/hr are due to the combustion of natural gas. Thus, process emissions are the major problem, although fuel combustion must also be considered a problem due to the high volume of fuel consumed.

Estimated uncontrolled process emission factors for the various subcategories are shown below:

SIC	Description	Suspended Particulate Emission Factors (lb/ton of finished product)
29	Petroleum and Coal	
2911	Petroleum Refining	5.5
2951	Paving	45.0
2952	Asphalt Coating	8.5
Source: Op cit		

This category accounts for 17% of the process weight flow amounting to 4755 t/hr. Application of the Illinois control regulations will achieve a reduction in emissions from 5110 lb/hr to 767 lb/hr, or 85%. Emissions per ton of material moved will then be .16 lb/t/hr.

Correlation results for this category indicate that controlled emissions are correlated with energy (r = .73), process weight (r = .44), employment (r = .49), and space (r = .52). Energy is correlated with space (r = .80) and employment (r = .74), but process weight is not correlated with either variable.

The general emission model  $R^2$  is .61, with energy contributing .53 and process weight contributing .08 to the explanation. The restricted energy model  $R^2$  is .68 with space contributing .64 to the explanation. Neither land nor employment contribute to the explanation of process weight. In the restricted emission model, the  $R^2$  is .30 with space contributing .28 to the explanation. Thus, space appears to be the most useful planning variable in explaining emissions from this category.

# 3.2.3 SIC 33 Primary Metal Industries

Industries in this category engage in the smelting and refining of metals from ore, pig, or scrap; in the rolling, drawing, or alloying of metals; and in the manufacture of castings, forgings, and other basic metal products. This category accounts for 16% of controlled particulate emissions; 90% are due to the manufacturing processes themselves, while 10% are due to fuel combustion. This category utilizes 15.3% of the energy consumed, or 2575 MBtu/hr, of which 2365 Mbtu/hr are due to the combustion of natural gas. Thus, process emissions are the major air pollution problem in this category.

Estimated uncontrolled process emission factors for the various subcategories are shown below:

SIC	Description	Suspended Particulate Emission Factors (1b/ton of finished product)
33	Primary Metal Industries	
3312	Blast Furnace	200.35
3313	Electrometallurgical	1180.0
3321	Gray Iron Foundries	17.0
3323	Steel Foundries	66.0
3331	Copper Smelting	135.0
3332	Lead Smelting	162.0
3333	Zinc Smelting	530.0
3334	Aluminum Smelting	295.0
3341	Brass and Bronze Smelting	50.0
3341	Aluminum	1025.0
3341	Lead	110.0
3341	Zinc	103.0
3341	Magnesium	4.0
3352	Rolling Aluminum	135.0
		İ

Source: Op cit

This category accounts for 3.6% of the process weight flow amounting to 1010 tons of material moved per hour. Application of the Illinois control regulations will achieve a reduction in emissions from 9007 lb/hr to 733 lb/hr or 92%. Emissions per ton of process weight will then be .73 lb/T/hr.

Correlation results for this category indicated that controlled emissions are correlated with process weight (r = .73), and somewhat with employment (r = .35) and energy (.27). However, process weight is poorly correlated with land (r = .05) and employment (r = .17). Energy is somewhat correlated with space (r = .28) but poorly correlated with employment (r = .16).

The general emission model R<sup>2</sup> if .61 with process weight contributing .52 to the explanation, the remainder being due to employment (.06) and energy (.03). Unfortunately, the results for the restricted models show that neither land nor employment is a good predictor of emissions, process weight, or energy. Some other means for estimating these parameters, particularly process weight, is required for this category.

## 3.2.4 SIC 28 Chemicals and Allied Products

Industries in this category produce basic chemicals or products manufactured predominantly from chemical processes. Establishments in this group manufacture three classes of products: (1) basic chemicals; (2) chemical products to be used in further manufacturing processes; and (3) finished chemical products to be used in final consumption. This category accounts for 16% of controlled particulate emissions; 82% are due to the manufacturing processes themselves, while 18% are due to fuel combustion. This category utilizes 11.4% of the energy consumed or 1908 MBtu/hr; 758 MBtu/hr are due to coal use, 146 MBtu/hr are due to the consumption of natural gas. Thus, both process and fuel combustion emissions pose air pollution problems for this category.

Estimated uncontrolled process emission factors for the various subcategories are shown below:

	i	Suspended Particulate Emission Factors
SIC	Description	(1b/ton of finished product)
28	Chemicals and Allied	
2812	Alkalis	6.0
2815	Dyes	0.0
2819	Industrial Inorganic Chemicals	20.0
2821	Plastics	35.0
2822	Synthetic Rubber	15.0
2841	Soap	90.0
2842	Detergents	90.0
2843	Surface Acting Agents	90.0
2851	Paints	2.0
2871	Nitrate Fertilizers	12.9
2871	Phosphate Fertilizers	80.0
2892	Explosives	36.0
2893	Printing Ink	2.0
2895	Carbon Black	2300.0
2899	Chemicals	16.0
Source: Op	cit	

This category accounts for 12.6% of process weight flow amounting to 3569 tons of material moved per hour. Application of the Illinois control regulations will achieve a reduction in emission from 5200 lb/hr to 702 lb/hr, or 86%. Emission per ton of process weight will then be .2 lb/t/hr.

Correlation results for this category indicate that controlled emissions are correlated with process weight (r=.78) and energy (r=.54), and somewhat with space (r=.35) and employment (r=.33). However, process weight is poorly correlated with land (r=0) and employment (r=.01).

Energy, on the other hand, is correlated with both space (r = .52) and employment (r = .63), although employment and space are also correlated (r = .72).

The general emission model  $R^2$  is .73, with process weight contributing .60 and space .12. Since space and process weight are unrelated, a poor  $R^2$  of .13 is obtained in the restricted emission mode. No explanation of process weight is achieved in the restricted process weight model, but energy is somewhat predictable from employment in the restricted energy model. These results indicate that some other means of predicting process weight is required, but employment may be useful in predicting fuel combustion emissions if fuel use can be estimated.

## 3.2.5 SIC 20 Food and Kindred Products

Industries in this category manufacture foods and beverages for human consumption, other food related products such as vegetable and animal fats and oils, and prepared feeds for animals and fowls. This category accounts for 7% of controlled particulate emissions; 53% of these emissions are due to the manufacturing processes, while 47% are due to fuel combustion. This category utilizes 7% of the energy consumed or 1945 MBtu/hr; 1084 MBtu/hr are due to coal use, 66 MBtu/hr due to oil consumption, and 776 MBtu/hr due to the combustion of natural gas. Thus, both process and fuel combustion emissions pose air pollution problems for this category.

Estimated uncontrolled process emission factors for the various subcategories are shown below:

SIC	Description	Suspended Particulate Emission Factors (lb/ton of finished product)
20	Food and Kindred	
2011	Meat Packing Plants	0.3
2013	Sausages	0.3
2015	Poultry	0.3
2036	Fresh Fish	0.1
2041	Flour	23.0
2042	Animal Feed	60.0
2046	Wet Corn Milling	8.0
2061	Cane Sugar	225.0
2085	Distilled Liquors	8.0
2095	Animal Fats	9.0
Source: Op ci	t	

This category accounts for 11.6% of process weight flow, amounting to 524 tons of material moved per hour. Application of the Illinois control regulations will achieve a reduction in emissions from 841 lb/hr to 315 lb/hr or 63%. Emissions per ton of process weight will then be .6 lb/t/hr.

Correlation results for this category indicate that controlled emissions are correlated highly with energy (r = .92) and employment (r = .83); however, energy and employment are related (r = .58), as are space and employment (r = .85). Process weight is somewhat related to employment (r = .44) and space (r = .38).

The general emission model  $R^2$  is .95 with energy contributing .90 and process weight only .05. The restricted emission model  $R^2$  is .80. with space contributing .77, while employment contributes only .03. The restricted process weight model R<sup>2</sup> is only .19, with employment contributing the

entire share of explanation. The restricted energy model R<sup>2</sup> is .81, with space contributing .78, while employment contributes only .03. These results indicate that space is the most useful planning parameter in estimating energy and hence emissions for this category.

# 3.2.6 Summary of Analysis of Manufacturing Emissions

The previous sections have analyzed the five largest polluting sectors in the Chicago study region to determine those parameters best explaining controlled particulate emissions. Contributions to controlled emissions were assumed functions of process weight and energy. This assumption is especially true if the Illinois process regulations constrain both process emissions and emissions due to fuel combustion as described in Appendix B. In the former case, a non-linear (exponential) relationship holds, while the latter relationship is indeed linear. Thus, not only were the parameters of land use and employment tested in a multiple linear model, predicting emissions along with process weight and energy, but these parameters were also tested for power in predicting the process weight and energy variables themselves.

For the five major polluting sectors analyzed in detail, the results are sporadically encouraging. SICs 32, 33, and 28 are dominated by process emissions and SICs 29 and 20 are dominated by fuel combustion emissions. Space is a useful predictor of process weight for SIC 32, and a useful predictor of energy for SICs 29 and 20. Employment is a useful predictor of energy for SICs 32 and 28. Unfortunately, neither land nor employment is a consistently good predictor of process weight flow and further investigations are required beyond the scope of this study.

Similar results for the remaining seven sectors are left to the reader to pursue in Table 3.2 and Appendix D.

## 3.3 ESTIMATION OF EMISSIONS FROM RESIDENTIAL/COMMERCIAL LAND

Emissions from residential and commercial (R/C) land are due primarily to fuel combustion for space heating. Therefore, the variance in emissions can be expected to relate directly to the size and construction of the building, as well as to the efficiency of the heating unit and the type of fuel burned. In this study, the size of the building as measured in total square footage is used to classify commercial buildings, and the number of dwelling units (DU) is used for residential buildings. The distribution of commercial buildings in Chicago by floor space is shown in Figure 3.5. Note that the skewness in this distribution is similar to that which occurred in the scale of manufacturing sources.

Buildings were classified in two ways for analysis purposes:

- 1) Light R/C (LRC)

  <20 DUs for Residential
  <20000 square feet for Commercial
  (Data aggregated on a square mile basis.)
- 2) Heavy R/C (HRC)

  >20 DUs for Residential

  >20000 square feet for Commercial

  (Data retained as point sources.)

Heavy R/C is further divided into intervals of 100 dwelling units or 100,000 sq ft.

It is desirable for planning purposes to know if mean energy use per DU or  $10^3$  ft<sup>2</sup> is a predictor of energy (and hence emissions, given fuel use) in each of the classes indicated. To test this hypothesis for HRC, a sample was drawn from the data for each of the heavy residential (HR) classes, as shown in Table 3.3. The sample was selected so as to achieve a uniform sample size in each of the heavy residential building size classes.

Analysis of variance was used to test the significance of variation in

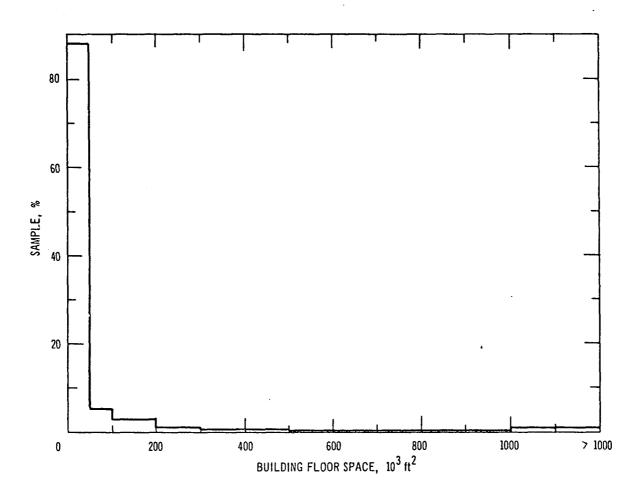


Figure 3.5. Commercial/institutional building size distribution in Chicago.

Table 3.3 SAMPLE DATA FOR HEAVY RESIDENTIAL ENERGY USE

(Single Source Data ≥ 20 DU/Building)

	20 - 100 DU's			]	100 - 200 D	U's	400 DU's			
	Btu x 10 <sup>6</sup> / Day	DU	Btu x 10 <sup>6</sup> / Day/DU	Btu x 10 <sup>6</sup> / Day	DU	Btu x 10 <sup>6</sup> / Day/DU	Btu x 10 <sup>6</sup> /	DU	Btu x 10 <sup>6</sup> / Day/Du	
1.	s	21	.38	53	148	.36	471	1256	.38	
2.	13	27	.48	30	144	121	370	628	.59	
3.	18	43	.38	58	187	.31	247	\$50	.45	
4.	18	40	.45	21	114	.15	226	640	.35	
5.	47	91	. 52	27	103	.26	130	585	.22	
6.	19	71	. 27	53	190	.28	89	413	.21	
	М	e a n	.41	. 1	de a n	.26	Ŋ	lean	.37	
	2	00 - 300	DU's	. 30	00 - 400 DU	's	Grand Mear	1	.37	
1.	106	232	.46	162	338	.48	DFB		4	
2.	181	203	. 89	94	364	.26 ,	BSS		.11	
3.	50	250	.20	170 .	320	.53	DEM		25	
4.	61	250	.24	50	312	.16	WSS		1.08	
5.	72	223	.32	158	324	.49	F		.64 - (NS)	
6.	86	273	.33	170	300	. 57				
	М	e a n	.41	1	Mean	.37				

the mean dwelling unit energy consumption of the building size classes of HR. The results are displayed in Table 3.3 and indicate that means of dwelling unit energy consumption are not materially different at the .05 significance level. Therefore, for this sample, we can conclude that energy estimation can be done on a dwelling unit density basis using .37 x  $10^6$  Btu/day/DU as an estimator. A similar result is obtained for heavy commercial classes (HC) using  $10^3$  ft<sup>2</sup>, as shown in Table 3.4 indicating a mean of .29 MBtu/day/ $10^3$  ft<sup>2</sup> for all buildings greater than 20,000 ft<sup>2</sup>.

The difference of means between heavy (HR) and light (LR) residential for the small sample was tested using analyses of variance. The results are as follows:

LR Mean No. Sample Pts.	.53 MBtu/day/10 <sup>3</sup> ft <sup>2</sup> 25.
HR Mean No. Sample Pts	.37 BMtu/day/10 <sup>3</sup> ft <sup>2</sup>
DFB	1
BSS	.35
DFW	53
WSS	1.44
F	12.96(s)

This result indicates that, for this sample, the hypothesis that the same mean estimator can be used for both light and heavy residential must be rejected. Therefore, we would use  $.53 \times 10^6$  Btu/day/DU as an estimator of light residential buildings and conclude that large residential buildings utilize less heat per dwelling unit than small residential buildings. This could be partially explained if small residential buildings generally were higher in square footage of floor space per DU than large residential buildings, but these data were not available to test this hypothesis.

Table 3.4 SAMPLE DATA FOR HEAVY COMMERCIAL ENERGY USE (Single Source Data 20 x 10<sup>3</sup> Sq. Ft./Building)

	20-	100 x 10 <sup>3</sup>	sq ft	10	00-200 x 10	3 sq ft	20	00-300 x 1	0 <sup>3</sup> sq ft
	Btu x 10 <sup>6</sup> /	10 <sup>3</sup> Sq. Ft.	Btu x <sub>3</sub> 10 <sup>6</sup> /Day/ 10 <sup>3</sup> Sq.Ft.	Btu x 10/ <sup>6</sup> Day	10 <sup>3</sup> Sq.Ft.	Btu x <sub>3</sub> 10/ <sup>6</sup> /Day/ 10 <sup>3</sup> Sq.Ft.	Btu x 10 <sup>6</sup> / Day	10 <sup>3</sup> Sq.Ft.	Btu x <sub>3</sub> 10 <sup>6</sup> /Day/ 10 <sup>3</sup> Sq.Ft.
1.	32	87	.37	46	150	.31	51	296	.17
2.	30	81.	.37	16	110	.14	120	275	.44
3.	14	75	.19	36	120	.30	32	200	.16
4.	24	54	.44	21	112	.19 *	101	240	.42
5.	11	45	. 24	17	130	.13	60	238	. 25
6.	17	<sup>.</sup> 37	.46	30	150	.20	77	230	.33
1	Ме	a n	.35	Mea	n	.21	Mean		.30
								=- <u></u>	. · · · · · · · · · · · · · · · · · · ·
	300-40	0 x 10 <sup>3</sup> s	γft ,	>40	0 x 10 <sup>3</sup> sq	ft	Grand Mean		. 29
1.	51	350	.15	130	420	.31	DFB		4
2.	92	380	. 24	261	768	.34	BSS		105
3.	84	351	. 24	136	631	.22	DI∙W	•	25
4.	117	312	.38	115	637	.18	WSS		.42
5.	165	329	.50	340	510	.67	F		.74 - (NS)
6.	61	350	.17	90	504	.18			
	M e	a n	.28	Mea	n	.31			
7									

A similar result is obtained for commercial buildings, as shown in the following table:

LC Mean No. Sample Pts.	.60 MBtu/day/10 <sup>3</sup> ft <sup>2</sup> 25.
HC Mean No. Sample Pts.	.29 MBtu/day/10 <sup>3</sup> ft <sup>2</sup>
DFB	1.
BSS	1.33
DFW	53.
WSS	1.02
F	66.5

For planning purposes, it is desirable to have energy use a linear function of dwelling units and independent of building size. If this assumption is approximately true, then dwelling unit density or floor area ratio (FAR) can be used. The previous section shows that an average estimator of energy use per unit is sufficient for the large heavy residential and commercial building classes.

Another way to view this result is that energy for HR use is linear with dwelling units per building. Figure 3.6 shows the fit of a simple regression model to the sample data. The result indicates that the regression line

$$Y = .40X - 6.7$$
.

where

Y is Btu  $\times 10^6$ /day

and X is Dwelling Units

is a good estimator of energy use for the small example of heavy residential buildings defined in the previous section.

A simple regression for the entire sample of heavy residential buildings for the City of Chicago that included 1103 sample points is also shown in Figure 3.6. The regression line is given by

$$Y = .59 x - 11.7$$
.

where the units are the same as above. The regression slope for the large sample has shifted upward significantly, indicating a bias in the small sample toward low Btu x  $10^6/\text{day/DU}$  readings.

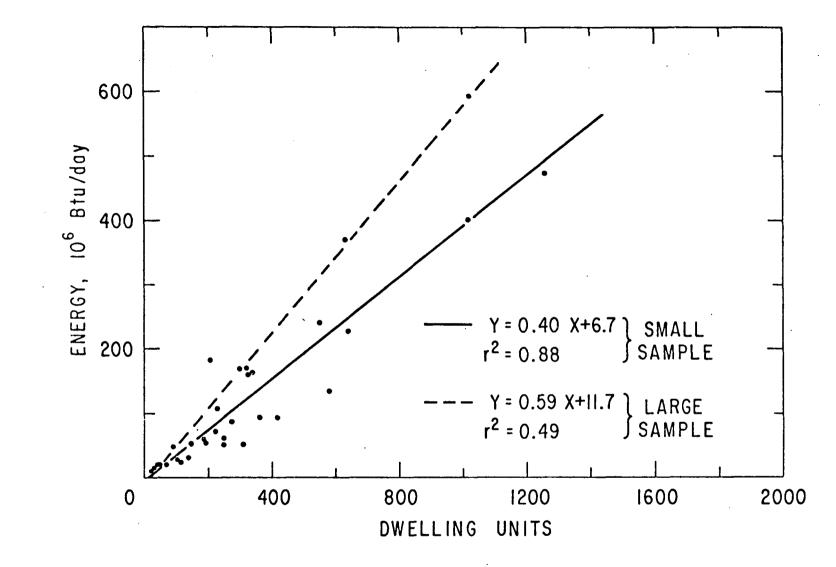


Figure 3.6. Large residential energy use.

The simple regression results for heavy commercial buildings are shown in Fig. 3.7. If building size is known, the simple regression model

$$Y = .30X - 4.2$$

where

Y is 
$$10^6$$
 Btu/day and X is  $10^3$  sq ft

can be used as an estimator. The linear fit is displayed in Fig. 3.6.

A sample regression for the entire sample of heavy commercial buildings for the City of Chicago that included 1373 sample points is also shown in Fig. 3.7. The regression line is given by

$$Y = .19 x + 24.5$$

when the units are the same as above.

The regression slope for the large sample has shifted downward somewhat , indicating a possible bias in the small sample toward high  $10^6~{\rm Btu/day/10}^3~{\rm sq}~{\rm ft}~{\rm readings}$  .

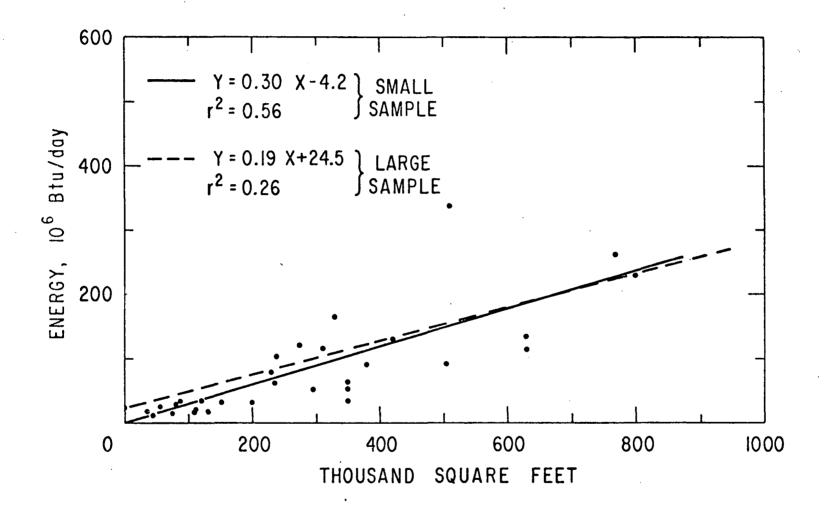


Figure 3.7. Large commercial energy use.

#### 4.0 SUMMARY AND CONCLUSIONS

Comprehensive planning as a control mechanism to maintain regional air quality depends on: (1) the applicability of the plan over time;

- (2) the ability of public administrators to implement the plan; and
- (3) the ability of planners to forecast the air quality effects of land use decisions and policies and to rank land use or effects-assessment plans. The latter element has been addressed in this study.

The basic criterion for evaluating the land-use-based emission estimation methods was the ability of the estimates to reproduce regional air quality as represented by the AQDM dispersion model, using the best available point-source inventory information. When data deficiencies prohibited the application of this criterion, standard statistical measures were applied. Statistical techniques used were analysis of variance, multiple regression, and product-moment correlation analysis. Emission inventory and land use data were drawn from the Chicago metropolitan study area as described in Appendix A.

The following conclusions are drawn from this study:

(1) The major problem with the air quality prediction on the basis of manufacturing land use data is in the wide variance and skewness in emission density distributions; severe distortions in air quality representations occur when mean and median estimates based on land use are employed in the AQDM model.

- (2) The use of mean and median estimates in representing air quality through dispersion modeling showed that results are highly sensitive to these estimates, particularly in the critical "hot spot" areas. A derivation of best-fit (minimum variance in relative error) emission density estimates by light and heavy industrial land use classes showed that the least standard deviation in relative error was 20%, with most of the contribution to the error occurring in hot spot regions. From this result, it was concluded that uniform emission density estimates by zoned land use class were insufficient by themselves to adequately represent air quality degradation due to manufacturing emission; measures of use intensity are also required.
- (3) Further attempts to account for the variance in manufacturing emission patterns were made by disaggregating manufacturing land into major industrial sectors by 2-digit SIC categories. Since land use or spatially distributed employment data on this level were not available, the air quality representation of resulting estimates could not be computed. Rather, statistical measures were used to judge the utility of various parameters in estimating emissions. The results showed that land use and employment were sporadically successful in explaining emissions, process weight flow, and energy consumption. However, although process weight frequently explained controlled emissions by 2-digit SIC class (logically, since the Illinois process control regulation is of the Bay Area Curve Class), land use and

employment were poor predictors of process weight. Therefore, it can be concluded that other parameters for estimating process weight flow need to be incorporated into the analyses, perhaps measures of capital intensity; such measures were not available in the data inventory used for this study.

(4) Studies of residential and commercial energy use by building size class in the Chicago area indicated that dwelling unit density and floor area ratio are potentially useful parameters in estimating unit energy consumption. It was noted that a significant difference in unit energy consumption exists between large (high rise) buildings of greater than 20 DUs or 200,000 sq ft and small (low rise) buildings of less than that amount, the former being more efficient. No significant difference in unit energy consumption was observed between size classes of high rise buildings.

# APPENDIX A DESCRIPTION OF THE STUDY AREA

## APPENDIX A

#### DESCRIPTION OF THE STUDY AREA

The purpose of this appendix material is to characterize the Chicago study area in terms of parameters that influence the air quality of the region, both present and future. This description provides a rationale for testing the utility of these parameters in estimating air pollutant emissions from land use, since they are commonly used for forecasting growth and development in the region. The first section characterizes current manufacturing land use in the region, and the second estimates development potential in the next decade. Finally, the data base used in the study is briefly described.

#### A.1 CURRENT MANUFACTURING ACTIVITY IN THE CHICAGO REGION

Chicago has traditionally been a large diverse and basically stable major industrial center as reflected by gross manufactures sales shown in Table A.1. In 1970, Chicago's share of the Gross National Product amounted to 5.28% or \$51.4 billion. Current employment patterns in the major industrial sectors of the region and in the study subregion are shown in Table A.2. The study subregion comprises approximately 90% of the manufacturing employment of the region and 64% of the manufacturing employment of the State of Illinois. The Chicago area is one of the largest electrical equipment manufacturing areas in the nation and the largest manufacturer of household electrical equipment and appliances. This industry is the largest employer in the area with 145,000, but third in total sales volume behind the Primary Metals and Food and Kindred Industries.

TABLE A. 1-MANUFACTURING OUTPUT - 1970 & 1971 - METROPOLITAN CHICAGO (In Millions)

	Gross Manufacturers Sales		Value Added by Manufacture		
•	1971	1970	<u> 1971</u> · ··-	1970	
TOTAL	\$37,989	\$37,299	<b>\$1</b> 8,308	\$18,024	
Primary Metal Industries	6,514	6,539	2,585	2,595	
Food & Kindred Products	5,378	5,159	2,162	2,074	
Electrical Equipment & Supplies	4,174 '	4,194	2,075	2,086	
Fabricated Metal Products	3,835	3,844	2,014	2,019	
Machinery, Except Electrical	3,641	? 724	1,999	2,045	
Chemicals & Allied Products	3,042	2,884	1,651	1,565	
Printing and Publishing	2,428	2,448	1,572	1,585	
Petroleum and Coal Products	1,598	1,478	420	388	
Transportation Equipment	1,383	1,303	639	602	
Paper and Allied Products	1,148	1,110	553	53 <b>5</b>	
Instruments & Related Products	891	894	543	556	
Rubber & Plastic Products	871	799	494	453	
Stone, Clay & Glass Products	805	723	422	379	
Apparel & Related Products	532	518	249	246	
Furniture & Fixtures	521	521	275	275	
Lumber & Wood Products	193	165	95	81	
Leather & Leather Products	145	145	84	84	
Textile Mill Products	103	101	42	42	
Miscellaneous	787	750	434	414	

Source: Chicago Association of Commerce and Industry (CACI), The Year-end Statistical Roundup for 1971.

Table A.2. SUMMARY OF MANUFACTURING PLANTS AND EMPLOYMENT BY MAJOR INDUSTRIAL SECTOR - 1970

· <del></del>			<del></del>		<del></del>					
							SUB-F	EGION		
	S	TATE	REG	REGION		County	DuPage	County	Will	County
2-Digit SIC	Emp.	Units	Emp.	Units	Emp.	Units	Emp.	Units	Emp.	Units
19 20 21 22 23	12561 118787 (D) * 4937 34813	16 1441 3 80 670	(D) 80352 (D) 3493 22266	10 829 3 67 538	1034 71344 (D) 3270 20367	9 734 3 57 499	2218 - - -	- 19 - - -	(D) 893 - - 453	1 19 - - 6
24 25 26 27 28 29	12000 23281 42305 110083 57775 10135	517 490 484 2623 830 99	7614 (D) 33746 91013 44043 4996	277 395 398 1947 660 71	6527 13315 28117 83210 32663 2594	222 346 336 1711 567 58	179 716 1276 2411 614	14 13 13 89 23	126 136 1319 1141 1654 2027	7 6 13 26 17 7
30 31 32 33 34 35	38427 12387 36143 108487 142188 214792	533 132 761 606 2289 2985	(D) 5690 19311 67063 105926 (D)	451 98 383 425 1874 2239	20715 5431 13315 58289 93960 91956	347 94 270 349 1603 1816	2293 - 414 1276 2998 3014	43 - 21 20 102 156	(D) - 1165 2163 1831 (D)	4 - 20 9 22 47
36 37 38 39 Adm.	190831 46476 41556 35332 83857	927 256 358 756 690	144991 30323 (D) 29580 72157 96730	786 177 303 614 550	123635 26247 29421 26936 65311 817985	644 140 271 549 483	5592 218 1170 259 2757	52 8 12 23 24 645	757 221 - (D) 365 28934	7 8 - 6 7 233
/State /Region	100	100	70.4 100	74.9 100	59.4 84.3	63.4 84.7	2.0	4.2 4.9	2.1	1.3 1.8

<sup>\*</sup>D - Denotes figures withheld to avoid disclosure of operations of individual reporting units. Source: County Business Patterns, Illinois, 1970.

Current manufacturing land use for the study area is shown in Figure A.1. The subregion contains a total of 100 square miles of manufacturing land or approximately 5% of the 2130 square miles of surface area. Approximately 41 square miles is devoted to heavy industrial use, while the remainder is devoted to light and general manufacturing uses.

## A.2. MANUFACTURING GROWTH POTENTIAL IN THE CHICAGO STUDY REGION

Total manufacturing activity in the Chicago region is expected to increase at a stable rate over the 10-year period from 1970 to 1980.

The Department of Health, Education and Welfare sponsored research on economic projections for air quality control regions throughout the country. This research was conducted by the U.S. Department of Commerce, Office of Business Economics, Regional Economics Division, and resulted in the publication, "Economic Projections for Air Quality Control Regions." Table A.3 shows the resulting productive growth factors for the Chicago region through 1980. A base year of 1967 is used with projections made for 1970, 1975, and 1980. "Growth factors" for each economic activity are given. For example, the growth factor in Chicago for Food and Kindred Products in 1975 is 114.8 which means that 1975 production will be 1.148 as great as the 1967 production levels in the region.

The Chicago region will continue to dominate manufacturing employment in the State, increasing approximately 11% and accounting for 80% of the statewide increase in manufacturing employment according to the state Office of Planning and Analysis projections. Figure A.2 shows recent manufacturing employment changes in the Chicago region and forecasted employment for 1985 by the Northeastern Illinois Planning Commission. 6

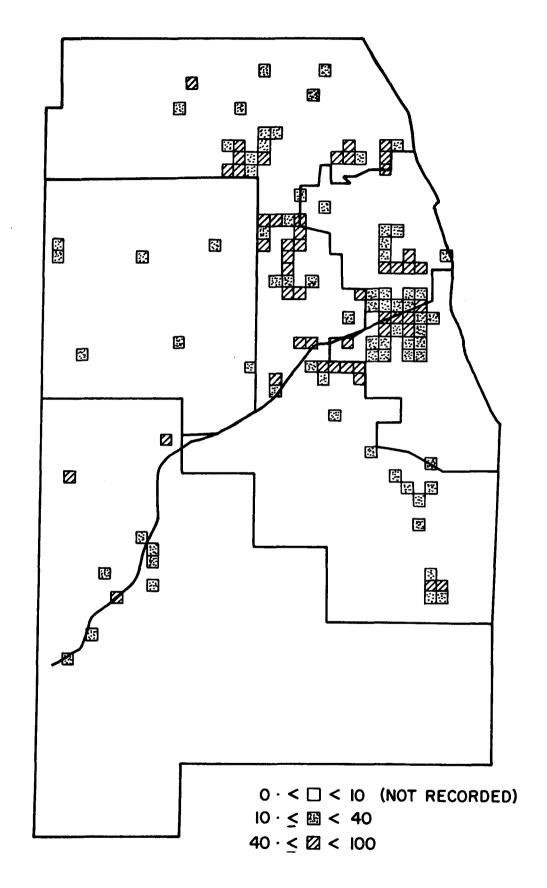


Figure A.1. Total industrial land use in Chicago study region.

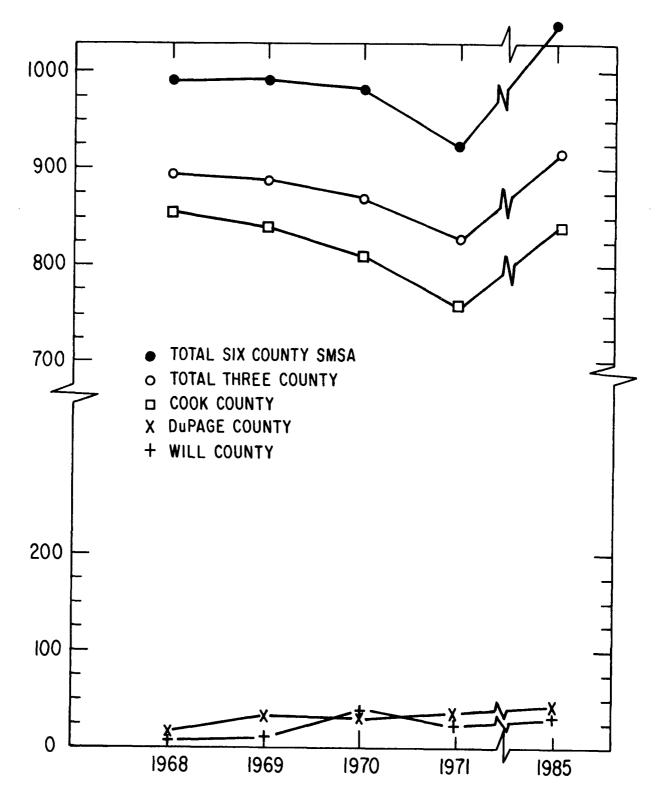
Table A.3

Growth Factors - Chicago Air Quality Control Region\*

(1967 = 100.0)

Item	1970	<u>1975</u>	1980
Manufacturing	108.5	128.5	152.4
Food + Kindred Products	102.5	114.8	128.6
Textile Mill Products	104.1	115.1	127.2
Apparel + Other Textiles	104.2	116.7	130.6
Printing + Publishing	105.2	122.8	143.4
Chemicals + Allied Products	114.7	140.5	172.1
Lumber + Furniture	115.2	134.0	155.8
Machinery, All	108.0	131.1	159.3
Machinery, Excl. Electrical	106.0	123.4	143.6
Electrical Equipment + Supplies	109.8	138.3	174.1
Transportation Equipment	122.4	145.8	173.9
Motor Vehicles + Equipment	147.4	180.2	220.2
Transportation Equipment, Excl.	107.3	125.3	146.2
Other Manufacturing	108.7	128.1	151.2
Paper + Allied Products	109.5	135.2	166.9
Petroleum Refining	131.2	145.6	161.7
Primary Metals	108.9	123.6	140.2
Fabricated Metals + Ordinance	102.0	121.3	144.6
Miscellaneous Manufacturing	112.3	137.2	167.6
Stone, Clay and Glass	108.5	125.7	145.7
Other Misc. Manufacturing	113.3	140.0	173.0

<sup>\*</sup>Source: Economic Projections for Air Quality Control Regions. A report to the National Air Pollution Control Administration, HEW, prepared by the U.S. Dept. of Commerce, Office of Business Economics, June 1970.



Sources: County Business Patterns. U.S. Bureau of Census: 1968-1971. Northeastern Illinois Planning Commission Planning Paper No. 10. Revised, 1972.

Figure A.2. Manufacturing employment trends Chicago SMSA.

Although it is difficult to project the fraction of growth that will result in new development or precisely where this new development will locate, some indications can be derived from land availability in the region. Presumably, this reflects regional planning for public and private transportation facilities, wastewater treatment systems, utilities, etc., as well as other locational advantages for manufacturers inclined to locate in the Chicago region.

Land zoned for manufacturing use in the study region totals approximately 267 square miles. In a ring surrounding the current high peaks of air pollution in the area, 19 square miles of land are currently used for manufacturing, while 84 square miles are zoned for manufacturing use (Figure A.3), a potential increase of 342%.

While the area of land zoned reflects potential manufacturing development as currently planned, no indication is given of the rate at which development is actually taking place. The Chicago Association of Commerce and Industry conducts an annual survey of industrial parks and districts in the metropolitan Chicago area. The summary table of this survey for 1971-72 is shown in Table A.4. This table indicates Will County as the most rapidly developing county in the study region having developed approximately 1 square mile of industrial land in the year under consideration and opening up approximately 1-1/2 square miles in new industrial districts. Suburban Cook County leads in total acreage of industrial development, but a significant withdrawal of lands from industrial use has occurred principally in the southern portion of the County. DuPage County leads in lands available to manufacturing, but is not realizing the rapid industrial growth that is occurring in Will County.

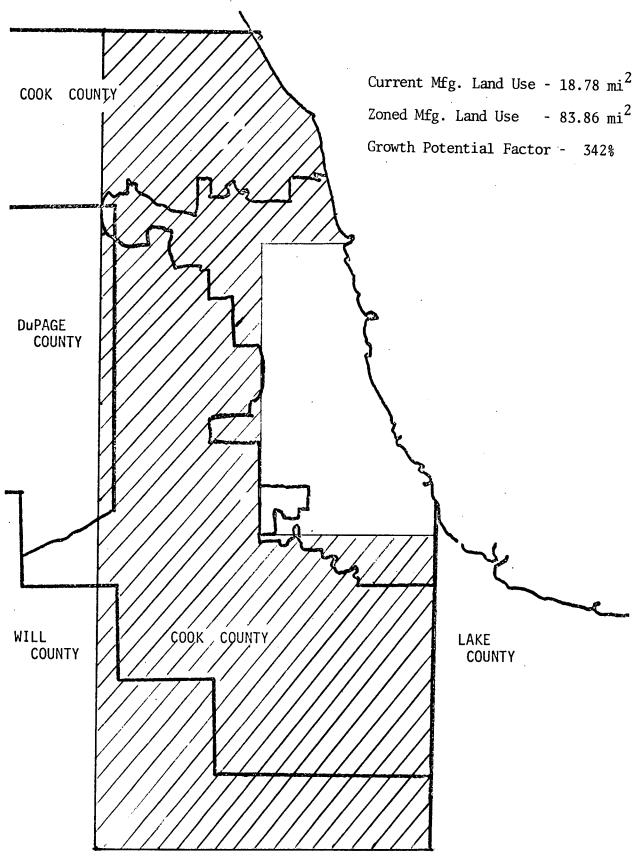


Figure A.3. Potential for Manufacturing Land development in area surrounding region at critical concern.

TABLE A.4. INDUSTRIAL PARKS SURVEY • 1971-1972\*

	Number	of		of acres	No. of acr		Number of	
	industr	al parks	of land i			ed through		or industry
	1972	1971	1972	1971	1972	1971	1972	1971
City of Chicago	37	36	2.826	3,064	2,416	2,355	410	709
Suburban Cook Co., III.	149	156	14,732	17,190	8,295	8,302	6,437	8.888
North Cook	79	83	8.640	8.720	5,274	4,891	3,366	3,829
West Cook	31	29	1.735	1.654	1.483	1,402	252	252
South Cook	39	41	4.377	6,416	1,542	2,009	2,835	4.407
DuPage Co., III.	48	49	10.325	10.560	2,983	3,035	7.342	7.525
Kane Co., III.	26	27	4.123	3.955	948	1,041	3,175	2,914
Lake Co., III.	19	21	2.642	2.846	414	701	2.228	2,145
McHenry Co., III.	ĭ	ī	250	260	0	0	250	260
Will Co., III,	23	18	7.502	6.766	1,687	1.088	5.815	5,678
Lake Co., Ind.	13	12	1.111	1.092	225	257	886	835
Porter Co., Ind.	2	2	770	770	144	144	626	626
Chicago metropolitan								
area	818	319	44,301	46,103	17,116	16,923	27,185	29,183

\*June to June

Source: Chicago Association of Commerce and Industry

#### A.3 DATA BASE FOR THE STUDY REGION

The data base for this study consists of source inventories, land use information by square mile and a permitted-use zoning policy. The data is used for testing the estimation procedures as described in the body of this report. A description and summaries of the data are included here to further characterize the source patterns of the study region.

The regional source inventory file consists of source identification, fuel combustion, process emission, and stack data. A description of the data as recorded in the inventory can be seen in Table A.5. The data were collected as part of the Illinois State Implementation Planning Program during the summer of 1971 by a team of students, who, under the supervision of the Argonne Center for Environmental Studies, surveyed the entire state for manufacturing source information. The Census Bureau publications, "County Business Patterns in Illinois" and the "Directory of Manufacturers," were used to guide the information collection operations. The Illinois State emission inventory contains planning parameters such as land use, employment, energy consumption by type of fuel, and process output data, in addition to emission information.

Emission factor information was used to derive total emissions from data surveyed. No direct emission testing was performed in collecting these data. Information was obtained by secondary source review, telephone contact, or site visit. It should be noted that the City of Chicago supplied combustion information to the State directly, in their own format. Therefore, fuel combustion from manufacturing sources within the City proper was not collected in the survey. The emission factors utilized in the conversion equations were obtained from a report by the U.S. Environmental Protection Agency. 4

TABLE A.5. STATE OF ILLINOIS EMISSION INVENTORY FILE PARAMETERS

Source Identification	Fuel Combustion	Process Emission Source	Stack Data
Source identification number	Boiler capacity (10 <sup>6</sup> BTU/hr)	Emission factor table code	Height (ft)
Source name	Coal (tons/year)	`	Inside diameter (ft)
		Process quantity	
Source street address	Oil (10 <sup>3</sup> gal/ year)		Temperature ( <sup>O</sup> F)
·		Process weight rate (lb/hr)	
City	Oil grade		Velocity (ft/sec)
Zip code	Gas (10 <sup>6</sup> ft <sup>3</sup> / year)	Process name	Gas volume (acf/sec)
Geocode	Heat content:	Emission factor	Number of units
X-Coordinate (Km)	Coal $(10^3 \text{ BTU/lb})$ Oil $(10^3 \text{ BTU/gal})$	Emissions (lb/hr)	
Y-Coordinate (Km)	Gas (BTU/ft <sup>3</sup> )		· ·
Standard land use classification number	Percent ash coal		
	Particulate emission factor		
Lot size (acres)			
Employees	Emissions (1b/hr)		•
Zening			

Tables A.6 and A.7 summarize the source file data by 2-digit SIC code for those classifications for which data existed in the source file. The SIC classes were ranked according to their percentage contribution to total emissions as shown in Table A.8. The top 12 ranking classes were then selected for analysis, accounting for 99% of emissions and 90% of the sources in the file.

In addition to point-source information, the estimation methodology requires land use information by zoning classification. For purposes of this study, manufacturing land use was divided into two categories—heavy industrial (HI) and light industrial (LI). Current land use information for the Chicago region was obtained from the regional planning body, the Northeastern Illinois Planning Commission (NIPC). The land use inventory was collected on a square-mile basis for the Chicago region and computerized as fractions of land area for each land use class.

Finally, the methodology requires that a permitted-use zoning policy be established. This was accomplished by a survey of county zoning administrators. The results indicate that heavy and light industrial activities are most commonly defined as shown in Table A.9.

TABLE A.6. MANUFACTURING DATA SUMMARIES

by 2-digit SIC code

SIC Code	Land (acres)	Employ-	Process Weight (t/hr)	Energy (MBtu/hr)	Coal (l·Btu/hr)	0i1 (Ætu/hr)	Gas (l·Btu/lır)	UC Emissions (1b/hr)	CT Emissions (1b/hr)	UC PR	UC FC	CT PR	CT FC	# Source
20.0	785+50	9576 • "A	523.88	1945.21	1084.41	66.56	775.72	840.61	314.94	29	78	53	46	21
55.6	17.00	415-40	2.41	14.07	0.00	4.00	14 - 92	76.83	4.21	100	ð	94	6	•
27. P.	48.48	483.90 2407.19	9.00	4 • 4 :	v. an	4 • 4 7 1 4 • 1 1	9•21 10•16	86 • 0 90 • 18 ج	0.45 17.03	9 99	100	88	100	1 16
24. V	172 · 00	4154.00	0.50 561.50	65 • 8 • 385 • 2 •	0.01 150.60	7•09 53•84	5q • 76 180 • 0R	217.40	5.31 127.02	99 49	1 50	67 89	. 33	16 25
27.0	32 • 70 12289 • 79	4204 • 70 20370 • 70	2.77 3563.23	53.31 1988.1	0.00 757.84	Ø • ØØ 145 • 88	53+3 <u>1</u> 992+77	1981.72	9.84 701.56	1 1 0 5 9	9	9 <i>0</i>	10 17	12
3278 3278	35.3+30 64-546	5287.00 4257.00	4754.66 104.74	6035.8° 255.3°	0.00 0.00	884+14	5114.66 237.58	5110.02 485.36	767.37 59.27	94 98	5 1	69 89	36	48 15
31.0	15 • 4N	300.00	11 · 14 /2	39.5	ย ดก	11.86	27 • 24	5.35	5.35	Ø	100	2	190	• 1
32.2	4725.80	4998 • 20	17337.85	920.0:	36.86	46.14	833.65	88563.56	1337.62	98	2	87	3	. 5p
377	1421.44	2456 1.00	1009.74	2574.51	0.40	197.60	2365.65	9006.73	732·86	98	1	98	9	83
34/0	1979.98	19650.00	64.04	1325.76	4.57	107.83	1211•33	2938.79	140.40	98	2	63	36	56
35.0	1749+37 643+48	34042.20	121.76	776.30	227.38 5.27	151 • 64	320·31 184·83	1799.53 424.71	160.68	54 93	<b>♦</b> 5 6	65 71	35 28	56 31
37.2	50	6976 • 30	28.51	555.4.	124.60	9 • 75	87.90	699.77	5,1.42	36	64	70	30	12
3 - , 60	1 44.90	327	4.10	54.5	0.00	44.62	11.82	28.21	5.43	72	ž7	12	88	6
3772	105.47	5203.10	53.84	34.71	5.02	4 • 4 g	25 - 17	312.26	49.72	98	Ź	96	3	5.5
14.S_		194307.00	22284.42	16807.05	2396.61	1814 • 79	12497.94		4520.80	94	5	82	17	544

TABLE A.7. MANUFACTURING DATA PERCENTAGES by 2-digit SIC code

SIC Code	Land	Employ- ment	Process Weight	Energy	. Coa1	0i1	Gas	UC Emissions	CT Emissions	Sources	
 20	2.25	4.93	1.85	11.57	45.25	3.65	6.21	0.70	6.97	4	
22	0.05	0.21	0.01	0.08	0.00	0.00	0.11	0.06	0.09	1	
23	0.13	0.25	0.00	0.03	0.00	0.25	0.00	0.00	0.01	0	
24	1.22	1.24	0.49	0.15	0.00	0.78	0.08	0.24	0.38	3	
25	0.55	2.14	0.00	0.39	0.00	0.39	0.47	0.18	0.12	3	
26	1.89	3.31	1.99	2.29	6.29	2.97	1.44	1.08	2.81	5	
27	0.10	3.19	0.01	0.32	0.00	0.00	0.43	1.66	0.22	2	
28	41.13	10.48	12.62	11.35	31.62	8.04	7.94	4.36	15.52	15	
29	12.43	2.72	16.81	35.91	0.00	48.72	40.92	4.28	16.97	7	
30	2.11	2.19	0.37	1.52	0.00	1.36	1.84	0.41	1.31	3	
31	0.10	0.15	0.00	0.24	0.00	0.65	0.22	0.00	0.05	0	
32	15.06	3.60	61.30	5.47	1.54	2.54	6.67	74.25	29.43	9 -	
33	5.17	12.61	3.57	15.32	0.00	10.89	18.93	7.55	16.21	15	
34	6.29	10.12	0.24	7.91	0.19	5.94	9.69	2.46	3.11	10	
35	5.64	17.52	0.43	4.20	9.49	8.36	2.56	1.51	3.55	10	
36	2.11	12.24	0.05	1.38	0.22	2.23	1.48	0.36	0.92	6	
37	2.87	8.74	0.07	1.32	5.20	0.54	0.70	0.59	1.12	2	
38	0.57	1.69	0.00	0.34	0.00	2,46	0.09	0.02	0.12	1	
39	0.34	2.68	0.19	0.21	0.21	0.25	0.20	0.26	1.10	4	

Table A.8. SIC CLASSES BY PERCENTAGE CONTRIBUTIONS TO TOTAL EMISSIONS

No.	2-Digit SIC Code	% of Controlled SP* Emis.	Cumulative % of Cont. SP Emis.	No. of Sources	% of Sources	Cumulative % of Sources
1	32	29.4	29.4	50	9	9
2	29	17.0	46.4	40	7	16
3	33	16.2	62.6	83	15	31
4	28	15.5	78.1	79	14	45
5	20	7.0	85.1	21	4	49
6	35	3.6	88.7	- 56	<sub>10</sub>	59
7	34	3.1	91.8	56	10	69
8	26	2.8	94.6	25	5	74
9	30	1.3	95.9	15	3	77
10	37	י ד	97.0	12	2	79
11	39	1	98.1	20	4	83
12 _	36	.9	99.0	31	6	89
13	24	.4	99.4	16	3	92
14	27	.2	99.6	12	2	94
15	25	.1	99.7	16	3	97
16	38	.1	99.8	6	1	98
17	22	.1	99.9	4	1	99
18	31	.05	99.95	1	0	99
19	23	.01	99.96	1	0	99
Other	-	.04	100.00	-	0	99

Table A.9. ACTIVITIES BY ZONING CLASS

	Heavy Industry		Light Industry
SIC	Description	SIC	Description
26	Paper and Allied Products	20	Food and Kindred Products
27	Printing, Publishing, and Allied Industries	21	Tobacco Manufactures
28	Chemicals and Allied Products		Textile Mill Products
29	Petroleum Refining and Related Industries	23	Apparel & Other Finished Product Made from Fabrics & Similar Materials
30	Rubber and Miscellaneous Plastic Products	24	Lumber & Wood Products, Except Furniture
31	Leather and Leather Products	25	Furniture and Fixtures
32	Stone, Clay & Glass Products	34	Fabricated Metal Products, Except Ordnance, Machinery, & Trans- portation Equipment
33	Primary Metal Industries	35	Machinery, Except Electrical
		36	Electrical Machinery, Equipment, and Supplies
		37	Transportation Equipment
		38	Professional, Scientific, and Controlling Instruments; Photo- graphic and Optical Goods;
•		39	Watches and Clocks Miscellaneous Manufacturing Indus

# APPENDIX B

# SUMMARY OF STATE OF ILLINOIS

# PARTICULATE EMISSION CONTROL REGULATIONS

#### APPENDIX B

#### SUMMARY OF STATE OF ILLINOIS

#### PARTICULATE EMISSION CONTROL REGULATIONS

In implementing the federal guidelines for the State of Illinois, the Illinois Pollution Control Board adopted a set of comprehensive air pollution control regulations designed to limit emissions of sulfur dioxide, particulate matter, nitrogen oxides, carbon monoxide, and hydrocarbons from stationary sources throughout Illinois.

An additional provision that would have effectively banned coal for residential or commercial use in the Chicago area by mid-1975 was not included in the package due to a temporary restraining order. This order was entered against the Board by a Cook County circuit court judge, who termed the ban unconstitutional as presently structured.

The new regulations represent a major effort by the state to control the air contaminants, and to form the heart of the Illinois program for meeting federal standards and combatting air pollution. Except for controls on particulate matter, the state previously did not have emission limits on these air pollutants.

Specifically, in regard to particulate air contaminants, the program:

1) Significantly tightens limits on the emission of particulate matter from such operations as steel mills, oil refineries,

- electric power plants, cement plants, and corn wet-milling facilities.
- 2) For the first time, requires sophisticated new equipment to control emissions from coke ovens.
- Greatly strengthens existing standards for emissions from incinerators.
- 4) Adopts a statewide nondegradation standard to prevent the unnecessary deterioration of air that is now clean, and to prevent new sources of pollution from being located in inappropriate places.
- 5) Institutes a statewide requirement of operating permits for all pollution sources as an aid to enforcement.
- 6) Requires sources to monitor their emissions, to keep detailed records, to adequately maintain their equipment, and to make regular reports to the state.
- 7) Specified particulate emission standards and limitations for new and existing emission sources, for incinerators, and for fuel combustion emission sources.

The air pollution regulations are designed to enable the state to meet the national ambient air quality standard by 1975.

In the case of Illinois manufacturing sources, emission standards are divided into fuel combustion and process regulations. Fuel emission regulations in the Chicago major metropolitan area require that no person shall cause or allow the emission of particulate matter into the atmosphere from any existing fuel combustion source to exceed 0.1 pound of particulate matter per million Btu of actual heat input in any one-hour period.

For process emission sources, no person shall cause or allow the emission of particulate matter into the atmosphere in any one-hour period from any existing process emission source in excess of the allowable emission rates specified in Table B.1, either alone or in combination with the emission of particulate matter from all other similar new or existing process emission sources at a plant or premises. Interpolated and extrapolated values of the numbers in Table B.1 for process weight rates up to 30 tons per hour shall be determined by using the equation:

$$E = 4.10 (P)^{0.67}$$
 (B.1)

and interpolated and extrapolated values of the data for process weight rates in excess of 30 tons per hour shall be determined by using the equation:

$$E = [55.0 (P)^{0.11}] - 40.0$$
 , (B.2)

where E = allowable emission rate in pounds per hourand P = process weight rate in tons per hour.

The process weight regulation in the Illinois Implementation Plan was modeled after the Bar Area Curve developed by the Bay Area Pollution Control District in San Francisco. This process weight regulation was based on well-controlled process industries found there. The Bay Area Curve rises to an allowable emission of 40 pounds per hour with increasing size of operation, and then allowable emissions increase at a reduced rate above 40 pounds per hour with increasing size of operation. The Bay Area Curve, as applied to the State of Illinois regulation, can be seen in Figure B.1. The Bay Area regulation is quite stringent for sources with a combination of large process weight rate and large emission factors,

TABLE B.1

Illinois Standards for Existing Process Emission Sources

Process Weight Rate Pounds Per Hour	Process Weight Rate Tons Per Hour	Allowable Emission Rate Pounds Per Hour
100	0.05	0.55
200	0.10	0.87
400	0.20	1.40
600	0.30	1.83
800	0.40	2.22
1,000	0.50	2.58
1,500	0.75	3.38
2,000	1.00	4.10 .
4,000	2.00	6.52
6,000	3.00	8.56
8,000	4.00	10.40
10,000	5.00	12.00
20,000	10.00	19.20
30,000	15.00	25.20
40,000	20.00	30.50
50,000	25.00	35.40
60,000	30.00	40.00
70,000	35.00	41.30
80,000	40.00	42.50
90,000	45.00	43.60
100,000	50.00	44.60
200,000	100.00	51.20
300,000	150.00	55.40
400,000	200.00	58.60
500,000	250.00	61.00
600,000	300.00	63.10
700,000	350.00	64.90
800,000	400.00	66.20
900,000	450.00	67.70
1,000,000	500.00	69.00

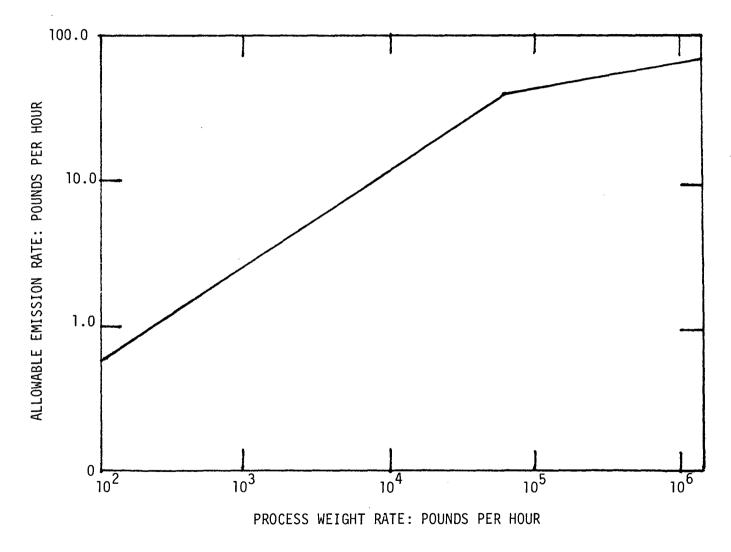


Figure B.1. State of Illinois allowable emission rate for point-source control

such as the SIC class 32 (stone, clay, and glass industries). It is noticeably lenient for sources with small emission factors and large process weight, such as SIC 28 (chemicals and allied) and SIC 29 (petroleum).

# APPENDIX C

DERIVATION OF BEST-FIT EMISSION-DENSITY
ESTIMATORS BY MANUFACTURING ZONING CLASS

## APPENDIX C

# DERIVATION OF BEST-FIT EMISSION-DENSITY ESTIMATORS BY MANUFACTURING ZONING CLASS

This appendix provides the derivation of the equations for determining those emission-density estimates by manufacturing zoning class that best represents air quality as calculated by the Air Quality Display Model (AQDM) dispersion model, using best available point-source emission inventory information in the Chicago region. For purposes of calculation with AQDM, the air quality is determined at 237 receptor locations in the region, yielding 237 points at which to compare the representation achieved by using detailed point-source information with that achieved using an emission-density representation by land use class.

For purposes of this study, two manufacturing classes are considered, heavy industry (HI) and light industry (LI). Two estimates of emission density are sought, ED<sup>HI</sup> and ED<sup>LI</sup>, that best represent air quality in the sense of minimizing the standard deviation in the relative error in calculated air quality between the point-source (PS) representation and the emission-density (ED) representation, and simultaneously achieve a zero mean relative error (umbiased). In this appendix, the emission-density formulation of the AQDM dispersion model is derived, after which the best-fit equations are displayed.

If it is assumed that the region is divided into geographic grid squares indexed by  $\ell$ , that k is an index of receptor points, and that m is an index of land use or zoning class, then the pollutant concentration  $X_k$  at receptor point k, is given by:

$$X_{k} = \sum_{m} \sum_{\ell} \alpha_{\ell k}^{m} ED_{\ell}^{m} A_{\ell}^{m} , \qquad (C.1)$$

where  $X_k$  is the pollutant concentration at receptor point k,

 $\alpha_{\text{lk}}^{\text{m}}$  is the dispersion model transfer coefficient describing the contribution of a unit emission from land use class m in grid square  $\ell$  to the concentration at location k (assumed independent of emissions),

 $\mathrm{ED}_{\ell}^{\mathrm{m}}$  represents the expected emission density in tons/day/acre for land use class m in grid square  $\ell$ ,

 $A_{\ell}^{m}$  is the specified percentage of land designated for land use class m in grid square  $\ell$ ,

If it is further assumed that the emission density,  $\mathrm{ED}^{m}_{\ell}$ , is a variable to be estimated uniformly over the entire region by land use class m, then the following emission-density formulation of the dispersion equation results:

or 
$$X_{\mathbf{k}} = \sum_{\mathbf{m}} \sum_{\ell} \alpha_{\ell \mathbf{k}}^{\mathbf{m}} A_{\ell}^{\mathbf{m}} ED^{\mathbf{m}}$$
 (C.2)

or 
$$X_k = \sum_{m} ED^m \sum_{\ell} \alpha_{\ell k}^m A_{\ell}^m$$
 (C.3)

where  $X_k = \sum_{m} P_k^m ED^m$ 

$$P_{k}^{m} = \sum_{\ell} \alpha_{\ell k}^{m} A_{\ell}^{m}$$
 (C.4)

For the case where m = HI, LI, we have:

$$\chi_{k} = P_{k}^{HI} \cdot ED^{HI} + P_{k}^{LI} \cdot ED^{LI} \qquad (C.5)$$

Let  $\begin{matrix} \text{PS} \\ x_k^{\text{PS}} \end{matrix} \quad \text{be the calculated concentration at reception} \\ \text{point } k \text{ using the point-source formulation} \end{matrix}$ 

and  $x_k^{ED}$  be the calculated concentration at reception point k using the emission-density formulation (eq. B.5).

Then the relative error is given by

$$\varepsilon_k = \frac{\chi_k^{PS} - \chi_k^{ED}}{\chi_k^{PS}}$$

$$= \frac{\chi_{k}^{PS} - \left(P_{k}^{HI} \cdot ED^{I} + P_{k}^{LI} \cdot ED^{LI}\right)}{\chi_{k}^{PS}}$$

$$= 1 - \left(\frac{P_k^{HI}}{X_k^{PS}}\right) ED^{HI} - \left(\frac{P_k^{L^{\intercal}}}{X_k^{PS}}\right) ED^{LI}$$

$$= 1 - \hat{P}_{k}^{HI} \cdot ED^{HI} - \hat{P}_{k}^{LI} \cdot ED^{LI} , \qquad (C.6)$$

where 
$$\hat{P}_{k}^{HI} = \frac{P_{k}^{HI}}{PS}$$

and 
$$\hat{P}_{k}^{LI} = \frac{P_{k}^{LI}}{PS},$$

and the mean relative error is:

 $\stackrel{*}{\text{ED}}^{\text{LI}} = N \sum_{k} \hat{P}_{k}^{\text{LI}} \sum_{k} \hat{P}_{k}^{\text{HI}}^{2}$ 

$$\mu_{R} = 1 - \frac{ED^{HI}}{N} \sum_{R} \hat{p}_{R}^{HI} - \frac{ED^{LI}}{N} \sum_{R} \hat{p}_{R}^{LI}$$
(C.7)

and the standard deviation of the relative error is:

$$\sigma_{R} = \frac{\sum_{k}^{\Sigma} \epsilon_{k}^{2}}{N} - \mu_{R}^{2}$$
 (C.8)

To select the best-fit umbiased emission-density estimators,  $^{**HI}$  and  $^{**LI}$ , the following minimization problem must be solved:

min 
$$\sigma_R$$
 (C.9)  
s.t.  $\mu_R = 0$ .

This can be solved explicitly using the Lagrange multiplier technique to give the following result:

$$\stackrel{**}{\text{ED}}^{\text{HI}} = -N \sum_{k} \hat{P}_{k}^{\text{LI}} \sum_{k} \hat{P}_{k}^{\text{HI}} \cdot \hat{P}_{k}^{\text{LI}}$$

$$\frac{-\sum_{k} \hat{P}_{k}^{\text{HI}} \sum_{k} \hat{P}_{k}^{\text{LI}} \hat{P}_{k}^{\text{LI}}}{D} \qquad (C.10)$$

$$\frac{-\sum_{k} \hat{p}_{k}^{HI} \sum_{k} \hat{p}_{k}^{HI} \cdot \hat{p}_{k}^{LI}}{k}$$
 (C.11)

where

$$D = \sum_{k} \hat{p}_{k}^{LI} \sum_{k} \hat{p}_{k}^{LI} \sum_{k} \hat{p}_{k}^{HI}^{2}$$

$$- \sum_{k} \hat{p}_{k}^{HI} \sum_{k} \hat{p}_{k}^{HI} \cdot \hat{p}_{k}^{LI}$$

$$- \sum_{k} \hat{p}_{k}^{HI} \sum_{k} \hat{p}_{k}^{LI} \sum_{k} \hat{p}_{k}^{HI} \cdot \hat{p}_{k}^{LI}$$

$$- \sum_{k} \hat{p}_{k}^{HI} \sum_{k} \hat{p}_{k}^{HI}^{2}$$

$$- \sum_{k} \hat{p}_{k}^{HI} \sum_{k} \hat{p}_{k}^{HI}^{2} \qquad (C.12)$$

# APPENDIX D

CORRELATION AND MULTIPLE
LINEAR REGRESSION RESULTS

Table D.1. CORRELATION TABLE - SIC 32 Stone, Clay & Glass Products

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.13	.66	. 94	.15	.58
Employment		-	10	.90	.82	004
Process Weight			-	14	06	.74
Energy				-	.62	05
Coal					-	01
Controlled Emissions						-

τ	L
•	Ξ
ι	,

CORPEL AND PERMES AMONG EMISSIONS AND PREDICTORS

FILE	CCRRES ICREA	TION DATE = 95/0	3/731			SIC 32 Stone, Clay	ε & Glass	
	SURATERA	CASES	MĘAN	STD DEV	•	Products	•	
	440085	5,9	94.5159	242.9510		Space (acres)	•	
	FVNHAV	50	139.9300	275.8376		Employment		
	145724	52	346.7568	869.3699		Process Weight (t/h	ır)	
	VA6785	5.9	18.4 403	44.5452		Fnergy (MRtu/hr)		
	V4-726	5.9	W.7 172	5 • 1955		Coal (Mitu/hr)		
	V4=317	5.4	1771 • 2 712	4905.0156		Uncontrolled Emissi	ons (lbs/hr)	
	ANNUA	5.78	56.4153	29.8296		Controlled Emission	s (lbs/hr)	
• • • •	• • • • • • •	• • • • • • •	· · · · · PULTIPL	E REG	RESSIO	N + + + + + + +	• • • • • • • •	• • • • • •
DEFF DE	NT VARIABLE	VARPUR	•					
			Su	MMARY TABLE	E			
/A-146L	ε		MHLTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	8	9E T 4
1447.4			7.74242	Ø:55119	0.55119	0.74242	8.6559.6	2.44253
1842.2			2.75319	0.56729	8.01610	ؕ58377	2.01914	3.15587
1457.3			V.75404	0.56858	0.00129	-0.00427	0.02039	1.18774
447.6			ؕ75562	0.57096	0.70238	-0.01025	-0.61915	-3-17754
. 4 14 7 . 45			0.75605	0.57162	0.00066	-0.04769	-0.05294	-20.26918
(CONT TA	NT3						15.70910	
(FEF-13F)	OF WARIABLE	BOCHAV	•					
			SUI	MMARY TABLE				
VA- JARI I	f		MULTIPLE R	R SQUARE	KSQ CHANGE	SIMPLE R	В	BEIA
V49172			0.58377	0.34078	0.34078	0.583/7	0.07297	0.59432
14-9-3			0.58932	0.34729	J.00651	-0.00427	-0.00880	-0.78137
1775537	(, t )						20.44644	
	T VARIABLE.	VAR704						
			SU	MMARY TABLE				
18A1 CAV	•		MULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	н	BETA
VA-912			0.65752	0.43234	J.43234	0.65/52	2.43851	0.68146
V4-1 ) 3			0.68250	0.46581	0.03347	-0.09611	-0.58151	-0.18450
TCC55TA1	1, ( )						197.56742	••••
2651.1211	AT VAPIABLE	VA4075						
			SU	MMARY TAULE				
18 41 CAV	•		MULTIPLE R	R SQUARE	KSQ CHANGE	SIMPLE R	в	HETA
V42013			0.40432	0.81779	0.81779	0.90432	0.13440	0.41435
VAPCO2			0.90756	0.82367	0.00589	0.70432	-0.01291	-0.01133
(COSTATA	,Т)		55.70.75	5.00.501	********	- <b>70</b> - <b>54</b> - <b>5</b>	0.81032	000,1130

**05/03/73** 

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Table D.2. CORRELATION TABLE - SIC 29 Petroleum Refining and Related Industries

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.76	.01	.80	<del>-</del>	.52
Employment		-	.02	.74 `	-	.49
Process Weight	·		-	.24	-	.44
Energy				-	-	.73
Coal	-	,			-	-
Controlled Emissions				• ,		-

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COMPET THO	PEQPE:	S AMO	G EMISSIONS AND	PPEDICTORS			05/03/73	PAGE 22	
FILE COPP	F٩	(CREA	TION DATE . 05/0	3/73)			SIC 29 Petrole	um Refining and Industries	
٧	A P + A B	LE	CASES	MEAN	STD DEV		_ iciaeca	mastries	
.,	42782		40	97.5750	237,4664		Space (acres)	<del></del>	
	A4263		40	132.0758	193.6956		Employment		
	447%4		4.71	118.8666	185.2731	-	Process Weight (	t/hr)	
	44225		4 /	150.8974	455.3191	_	Energy (MBtu/hr)		
	62226		4.9	0.0	0.0		Coal (MBtu/hr)		
	AUZZZ		40	127.7504	375.8899		Uncontrolled Emi:	ssions (lbs/hr)	
	FRANK		40	19 • 18 • 1	31.9510		Controlled Emiss	ions (1bs/hr)	
• • • • •				* * * * MULTIPL	€ R E G	RESSIO	N • • • • •		
DEPFIDENT V	APIAB	LE	RNNAAV				-		
				· su	MMARY TABL	E			
PRESIDE				4ULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R -	8	BETA
V49775				0.73045	0.53355		a . 730451	0.04667	2 44524
14-2.4				Ø • 78164	Ø.61096	0.53355 0.07741	Ø+73Ø45 Ø+4468	0.04944	2+66504 2+2672
/AF273				0+78175	0.61113	0.00017	0.48836	8.97489	49654.5
124715				ؕ78192	P • 61140		0.52646	-0.00418	-0.03186
(CONSTANT)				10135		D. DNWC/	0.25040	6.92699	-1.44.316.0
SEREMOENT VA	I ABI	f	VAROOS						
				Sur	MARY TABLE	•			
1441444				FUETIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	В	BETA
44.4352				0.52646	0.2//16	0.27716	0.52646	0.04944	0.36742
V42573				0.54389	0.29582	0.01867	0.48836	0.03458	0.20466
100 50 14911								9.19211	
DESCRIBING VA	₽ IAºL	.F	VAR004			• •			
				SUY	MMARY TABLE				
VAPIABLE				FULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	*	BETA
V4F 153				0.02242	0.00053	0.00050	-0.02242	-0.06383	-0.06614
SLUSAN				0.04418	0.00195	0.00145	0.00780	0.74558	0.05842
4503518334				5557120	,	0.00112	3.00.00	122.55007	0107042
DEPENDENT VA	-1A31	f	VAR005					122.000	
				SUA	MMARY TABLE				
VAPTABLE				PULTIPLE R	H SQUARE	KSQ CHANGE	SIMPLE R	в	HETA
441.003				0.80114	0.64182	0.64132	0.80114	1.13056	0.57399
VA9002				0.82456	0.67990	0.03808	0.13485	0.70343	0.29946
(60%5TANT)				0.02430	0.0,,,,,	0.05.00	34.3.07	-44.46049	
10,50516011									

Table D.3. CORRELATION TABLE - SIC 33 Primary Metal Industries

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.28	.05	.10	-	.14
Employment		-	.17	.16	-	.35
Process Weight	·		-	.07	<u>-</u> .	.72
Energy				-	-	.27
Coal					-	-
Controlled Emissions						-

t	1	
į	•	

HCOPHEL AND REGRES AMONG EMISSIONS AND PREDICTORS

FILF	CONFE2 ((	CHEATION DATE = 45/	793/731			SIC 33 Primary Mc	atul Industrias	
	VA: IABLE	CASES	MIAN	STD DEV		oro oo trimary ra	cear moustries	
	44.14.5	Ç = 01, 3	7.1 2.0	0,0 22,		C		
	VAPREZ	A 3	19.51.54	51 • 6155		Space (acres)		
	4844XJ	ЯA	295 - 11 07	688.4092		Imployment		
	A N. S. S. A. A.	83	12+1/55	45.8586		Process Weight (t/	/hr)	
	4444X5	P7	31.0192	130.1583		Phergy (MBtu/hr)		
	146726	8.9	Ø • e	0.0		Coal (MBtu/hr)		
	142247	83	108+5:48	529.7297		Uncontrolled Emiss	sions (lbs/hr)	
	V442/8	яз	8 • R; 97	14.8433		Controlled Emission	ons (lbs/hr)	
			**** MULTIPL	E REGI	RESSION		••••••	• • • • •
DEPEN	CENT VARIABL	E • • VAPØØ8						
			รบ	MMARY TABLE	E			
14411	RLF		MULTIPLE R	R SQUARE	RSO CHANGE	SIMPLE R	8	ŞĘŤĀ
1601	_		<b>4.072278</b>	0.52241	0.52241	g • 72278	0.21824	3.67.26
			0.76043	0.57825	0.05584	Ø • 35 • 9 •	0.03434	5.20122
14-1.1			ؕ78293	0.61297	0.03472	0.26951	Ø • Ø2135	7-19713
/A-",			ؕ78359	0.61401	0.00103	0.14314	0.02965	7 - 13356
			4.478333	0.01401	0.00103	0.14314	4.84349	(11 22 20
10000	1 4 1 1 1						4104349	
CERENO	ENT VARIABLE	VAR008						
			SUM	MARY TABLE				
VASIAE	1 1		MULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	н	BETA
44°()3			0.35494	0.12599	0.12598	0.35494	0.00737	0.34165
VA2702			0.35786	0.12806	0.00208	0.14314	0.01366	0.04149
(CONST	ANTE		003710		0.00200	0011311	6.38850	0.04.47
CEPEND	ENT VARIABLE	VAROD4						
			SUM	IMARY TABLE				
VAPIAB	u e		MULTIPLE R	K SQUARE	RSQ CHANGE	SIMPLE R	8	Ht 1 &
VA>223	i		0.16864	0.02851	0.02851	U.16884	0.01125	0.16384
CL P.T			0.10054	0.02376	0.02071	0.10001	8.84553	
CERTAN	ENT VASTABLE	VA2005						
			SUM	MARY TABLE				
SALSAK	LF		MULTIPLE R	R SOUARE	RSQ CHANGE	SIMPLE R	в	HETA
VAPO03			0.16295	0.02655	0.02655	0.16295	0.02772	0.14659
VA-332			0.1/234	0.02970	0.00315	0.09949	0.14/39	0.05845
100451	ANTI					- •	19.95876	* * * * *
							- · · · · ·	

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Table D.4. CORRELATION TABLE - SIC 28 Chemicals and Allied Products

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.72	-0 .	. 52	.61	.35
Employment		-	.01	.63	.77	.33
Process Weight			:	. 34	.40	.78
Energy	·			-	.83	. 54
Coa1					<u>-</u>	.61
Controlled Emissions				·		-

FILE COPPES (CREATION DATE = 05/03/73)  VARIABLE CASES MEAN STD DEV  VARIA	
VARIABLE         CASES         MEAN         STD OEV           VARIAR         79         163.4150         1127.7778         Space (acres)           VARIAR         79         257.8479         763.4949         Employment           VARIAR         79         45.1801         223.5915         Process Weight (t/hr.)	
VAP/74 79 257.8479 763.4949 Employment VAP/74 79 45.1801 223.5915 Process Weight (t/hr.)	
VAP774 79 45.1801 223.5915 Process Weight (t/hr)	
vanozis 79 9.5936 41.9244 Coal (MBtu/hr)	
VARGET 79 65.8388 267.4426 Uncontrolled Emissions (lhs/l	)
VAPZUR 79 8.8806 19.6010 Controlled Emissions (lbs/hr)	
• • • • • • • • • • • • • • • • • • •	
SERFICENT VARIABLE. VARIOUR	
SUMMARY TABLE	
VARIABLE R SQUARE RSQ CHANGE SIMPLE R	B BETA
7•76765 A•58929 B•58929 A•76765 B•	.9504.6 276.69
	00362 2.22927
	05526 2.11823
	.02865 3.03157
	.00386
(CGNETANT)	. 10266
DEPENDENT VARIABLE VARIOS	
SUMMARY TABLE	
MILTIPLE R R SQUARE RSQ CHANGE SIMPLE R B	BETA
VAPOD2 0.34615 0.1[982 0.11982 0.34615 0.1	00383 0.22055
	UU448 U.17463
	04823
DEPFNOTAT VARIABLE VAROO4	
SUMMARY TABLE	
VAPIABLE R R SQUARE RSQ CHANGE SIMPLE R B	BETA
VAP 773 0.01151 0.00013 0.001151 0.0	0.02405
(CDISTANT) 43.5	92893
SERENDENT VARIABLE. VAROOS	
SUMMARY TABLE	·
VAPIANIC SIMPLE R B	HETA
	13822 0.52296
9A> 972 0.63312 0.40161 0.00988 0.51922 U.	0.14310
(CONSTRA) 13-4	14117

Table D.5. CORRELATION TABLE - SIC 20 Food and Kindred Products

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.85	. 38	.88	.90	.88
Employment		-	.44	.84	.83	.83
Process Weight			-	.23	.23	.43
Energy				-	.96	.92
Coa1				~	-	.95
Controlled Emissions						-

• • • •	GPPES (CF  V4P732  V4P237  V4P274  V4P275  V4P277  V4P277  V4P277  V4P288	CASES  21 21 21 21 21 21 21 21 21 21	MF/N 33.59! 2 456.00 0 24.94.7 92.63 4 51.63 5 40.02 0 14.99 1	5TD DEV 68.2297 758.7634 74.9341 262.3921 232.2444 144.0113	-	SIC 20 Food and  Space Employment Process Weight (t/ Energy (ABtu/hr)		
OEPE-DEN	V&PZ72 V&LZ37 V&LZ37 V&LZ37 V&LZ37 V&LZ37 V&LZ37 V&RZ37	21 21 21 21 21 21	33.59! 2 456.60 0 24.94.7 92.63 4 51.63 5 40.02 0 14.99 1	68:2297 758:7634 74:9341 262:3921 232:2444 144:0615	-	Space Employment Process Weight (t/		
OEPE DEN	VAF-207 VAF-276 VAF-276 VAF-276 VAF-277 VAF-2768	21 21 21 21 21	456 • 70' 0 24 • 94 • 7 92 • 63   4 51 • 63' 5 40 • 02   0 14 • 99   1	758.7634 74.9341 262.3921 232.2444 144.0615	-	Employment Process Weight (t)	/hr)	
OEPE DEN	VAF-207 VAF-276 VAF-276 VAF-276 VAF-277 VAF-2768	21 21 21 21 21	456 • 70' 0 24 • 94 • 7 92 • 63   4 51 • 63' 5 40 • 02   0 14 • 99   1	758.7634 74.9341 262.3921 232.2444 144.0615	-	Employment Process Weight (t)	hr)	
OEPE DEN	482724 484775 482775 48277 48778	21 21 21 21	24.94.7 92.63 4 51.63 5 40.02 0 14.99 1	74+9341 262+3921 232+2444 144+0615	-	Process Weight (t/	hr)	
OEPE DEN	VAHOVS VA⊐036 VA⊐027 VAHOSS	21 21 21	92.63 4 51.63 5 40.02 0 14.99 1	262+3921 232+2444 144+8615			*** )	
OEPE-DEN	VARZVE VARZVE • • • • •	21	40.02 0 14.99 1	144.0615	-			
OEPE- DEN	V48888		14.99 1			Coal		
OEPE DEN		21		22 2224		Uncontrolled Emiss	sions (lbs/hr)	
DEPENDEN	· · · · · ·	• • • • • • • •		37.7325		Controlled Emission	ons (lbs/hr)	
DEPENDEN	T VARTABLE.		· · · · MILTIPL	E REGI	RESSION	• • • • • • •	• • • • • • • • •	
		• VARØØ8				•		
			Sui	MMARY TABLE	Ε			•
VARIABLE			MULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	В.,	BETA
144276			0.94801	0.89873	0.89873	0.94801	0.14468	65508.6
V 4 4 7 7 4			0.97242	0.94560	0.04687	.0.43300	0.12272	2.24367
VA4223			0.97277	0.94628	0.00068	0.83140	-0.00276	-2-5553
VALX15			0.97299.	0.94670	0.00042	0.91830	0.01222	3.08498
444415			0.97310	0.94693		0.88056	-0.02149	-2.23885
(CONSTAN	7)		· · · · · · · · · · · · · · · · · · ·				5.31777	
LESCADI AL	VAPTABLE.	, VAUGOS						
			SUM	IMARY TABLE	•			
31811-AV			MULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	В	BETA
VASSOS			0.88056	0.//538	0.77538	U.88U56	0.34488	0.62363
V45773			0.89527	0.80151	0.02613	0.83140	0.01509	0.30354
(CONSTANT	,						-3.41244	0.30371
DEPENDENT	VAPIABLE.	, VARUO4						
		• • • • • • • • • • • • • • • • • • • •	SUM	MARY TABLE	•			
VAPIANIF			MULTIPLE R	R SQUARE	KSQ CHANGE	SIPPLE R	н	BETA
					2 10201	0 / 1071	0.04339	0.43921
VARGOS CCUUSTANT	)		0.43921	0.19291	0.19291	0.43921	5.16/1/	0.43721
- GEPF YOUN	VAPIANCE.	. VARUOS						
			SUM	IMAKY TABLE	:			
VADIABLE			MULTIPLE R	R SHUARE	RSQ CHANGE	SIMPLE R	в	HETA
VA - 202			0.88212	0.77920	0.77920	0.88272	2.36663	0.61539
V45003			0.89860	0.80749	0.02828	0.83672	0.10922	0.31583
CONSTANT	)		2,3,000	*			-36.68071	

Table D.6. CORRELATION TABLE - SIC 35 Machinery, Except Electrical

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.81	07	.89	.85	.36
Employment		-	07	.90	.83	.41
Process Weight			-	05	04	.83
Energy				-	.95	.44
Coal			,		-	.42
Controlled Emissions	•					· <u>-</u>

FILE		•	NO PREDICTORS			05/03/73	PAGE +2	
	COPPEC	ICREATION DATE - MS	///3/73)			SIC 35 Machinery Electrics	, Except	
	<b>√∆</b>	BLE CASFS	MEAN	STD DEV	, ·	Electrica		
	/AF XX		31.5959	66+6823	1	Space (acres)		
	144.4%	3 56	607,8928	1091.9629		Employment		
	VAPPE	4 54	2 • 1 7 3 2	12.0812		Process Weight (t		
	124021	5 54	12.6124	38 • 9831		Energy (MBtu/hr)		
	144771	5 54	4.0604	20.6633		Coal (MBtu/hr)		
	14543	7 56	32.1167	96.2852	•	Uncontrolled Emis	sions (lbs/hr)	
	AVONS		2.8693	7.9479		Controlled Emissi		
		• • • • • • • • •	• • • • • HULTIPL	E REG	R E B S I O	N + + + * + + + + + + + + + + + + + + +		
ErE.	PENT VARIAB	SLE VARROS						
			Si	MMARY TABL	Ε			
4474	B! E		MILTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	В	BETA
£ = 2, 1	4		0.83193	0.69211	0.69211	0.83193	0.56625	2.96045
447,	5	•	9.96966	0.92287		0.44187	0.04605	2.22587
A-11	3		9.96544	0.93207		0.41023	0.00169	2.23272
4-2,	-		0.96567	0.93251	0.00045	Ø++2875	0.02772	3.07207
4-1			ؕ96574	0.93265		0.36038		
	c Tabit)		1,136374	6.53563	#100014	0.36036	-0.003n9 0.01368	-1.92591
PF*;()(	CHT VAMIARE	E VAR998						
			SUM	MARY TAHLE				
21A81	, F		MILTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	В	BETA
2003			0.41023	0.16829	0.16829	0.41023	0.00252	0.34594
			0.41280	0.17041	0.00212	0.46038	0.00942	0.07906
			0.41200	0.11041	0.00212	0.36030		0.01.00
	C 9. T 3						1.05091	
	£4. T )						1.04043	
r ns ta	ENT VAPTABL	.F VAPON4		· .		-	1.04043	
ensti Penbl	FRT VAPTABL	F VAPO04	SUA	IMARY TAULE			1.04041	
151651	FRT VAPTABL	F VAP004	M JET IPEE P	IMARY TAULE R SQUARE	RSQ CHANGE	SIMPLE R	B	HETA
(5 15 17)   PEND   -   PEND    PEND	FRT VAPTABL	F VAPON4	MJLTIPLE P 0.01567	IMARY TAULE R SQUARE 0.00573				
CNSTA PENDI PENBI PENBI PENBI PENBI	FUT YAPINKL	F VAPON4	M JET IPEE P	IMARY TAULE R SQUARE	RSQ CHANGE	SIMPLE R	B -0.00768	-0.04238
CNSTA PENDI PENBI PENBI PENBI PENBI	FUT YAPINKL	.F VAPON4	MJLTIPLE P 0.01567	IMARY TAULE R SQUARE 0.00573	RSQ CHANGE	SIMPLE R -0.07567	В	
CNST/ PENDI PENDI POOR POOR POOR	FUT YAPINKL		MJLTIPLE P 0.01567	IMARY TAULE R SQUARE 0.00573	RSQ CHANGE	SIMPLE R -0.07567	B -0.00768 -0.00045	-0.04238
(CNST) (PEND) (PEND) (PEND) (POD) (POD)	FUT VAPTABL		MILTIPLE P 0.07567 0.07933	IMARY TAULE R SQUARE 0.00573	RSQ CHANGE	SIMPLE R -0.07567	B -0.00768 -0.00045	-0.04238
CNST/ (PEND) (PEND) (PENDZ (PODZ (PODZ)	FUT VAPTAGE (F 44T)		MILTIPLE P 0.07567 0.07933	MARY TABLE R SQUARE 0.00573 0.00629	RSQ CHANGE	SIMPLE R -0.07567	B -0.00768 -0.00045	-0.04238
16419 16419 16419 16419 16419 18419	FUT VAPTAGE (F 44T)		MILTIPLE P 0.0/567 0.0/933 SUM MILTIPLE R 0.90052	MARY TABLE R SQUARE 0.00573 0.00629  MARY TABLE R SQUARE 0.81094	RSQ CHANGE 0.00573 0.00057  RSQ CHANGE 0.81094	SIMPLE R -0.07567 -0.07540  SIMPLE R 0.90052	B -0.00768 -0.00045 2.69111 B	-0.04238 -0.04093 851A 0.52128
PEADI PEADI PEADI PEADI PEADI PEADI	FUT VAPIABL (F 41,T) (MT VAPIABL		MILTIPLE P 0.0/567 0.0/933 SUM MILTIPLE R	MARY TABLE R SOUARE 0.00573 0.00629  MARY TABLE R SQUARE	RSQ CHANGE U.00573 U.00057	SIMPLE R -0.0/567 -0.0/540 SIMPLE R	B -0.00768 -0.0045 2.69111	-0.04238 -0.04093

Table D.7. CORRELATION TABLE - SIC 34 Fabricated Metal Products, Except Ordnance, Machinery, and Transportation Equipment

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.01	.84	.23	.98	.68
Employment		-	02	.05	03	. 04
Process Weight	·		-	.19	.86	86
Energy				-	.20	.48
Coal					-	.67
Controlled Emissions					·	-

		,	EMISSIONS AND	,			05/03/73	_		
FILE C	OBBEG	CHEATIC	N DATE = 05/0	13/73)			SIC 34 Fabricat		Products, Machinery	
	PAIMAY	ιLΕ	CASES	MEAN	STD DEV			ortation	Equipment	
	VAFRE	,	54	35.2486	162.0347		Space (acres)			
	VALUAT		56	351.0356	972.5554		Employment			
	VARZZA		54	1.2150	3.7497		Process Weight (t	/hr)		
	444334		54	23.7278	87.6151		Energy (MBtu/hr)			
	VA2286		54	0.0829	p.6053		Energy (MBtu/hr) . Coal (MBtu/hr)			
	<b>∀ A</b> ≃ 7. 2.7		54	52.4783	252.7663		Uncontrolled Emis	sions (1	bs/hr)	
	VAHOUE		56	2.5071	5.1106	•	Controlled Emissi			
• • • •	• • • •	• • • •	• • • • • • •	· · · · MULTIPL	E REGA	ESSION			• • • • • •	• • • • •
PERE DE P	T VARTAR	LE.	VARBUR							
				SU	MMARY TABLE					
ear labile				TULTIPLE R	R SQUARE	RSO CHANGE	SIMPLE R	-	8	BETA
12000				v • 86218	Ø.74335	0.74335	Ø+86218		1.50905	1+107
1447.5				V.00C1X	0.84714	0.10379	0.47983		0.01883	3.355
14-7.6				2.93748	0.87887	0.03174	0.66539		-6.46685	•ø•765
-					_	- • ·				
51344				7 • 9 <b>4 1 8 7</b>	0.88713.	0.00x25 0.00054	0+67944 0+04447		8.81331	254+6 854+6
165763		_		0.94216	0.88767	• במטח• ש	Ø • Ø • • • · /		a.00012 0.23685	7.653
ICS46TA4	7,			,	•				6.53683	
DEPENDEN	T VAPIABI	F 1	/AROOB							
				2014	IMARY TABLE					
APTABLE				*ULTIPLE R	R SQUARE	RSO CHANGE	SIMPLE R		B	HETA
40002				0.67944	0.46163	0.46163	0.6/944		0.02142	0.6790
A4993				0.68047	0.46305	0.00141	0.04447		0.00020	0.037
CONSTANI	т)			<b>0.0001</b> 1	0010307	0.00141	0.07777		1.68241	0.031
er ar hat s	T VAPIAH		VAP 004							
,,,,,	, Av-14-	1 % 4 4	¥ A. 17:74	·	MMARY TABLE					
VAR TARLE				WELLPEF K		RSQ CHANGE	SIMPLE R		8	BEIA
VAR002				J.84179	0.70861	0./0961	0.84179		0.01949	U.842
VA-072				0.84225	0.70939	0.00078	-0.01939		-0.00011	-0.021
ICC 4STAN	7)			7.04725	0.10439	0.00078	-0.01934		0.56596	-0.021
DESCHOEN	BAISAV T	lf	VAR005							
				SU	MARY TABLE					
A-TABLE				NULTIPLE R	R SQUARE	HSQ CHANGE	SIMPLE R		в	861A
142672				0.23005	- 0.05292	0.05292	W 3 WWF		0.12/15	
							0.23005		0.12415	0.229
/APODS CONSTAN	* 1			0.23415	0.05483	0.00140	0.04596		0.00393 17.97187	0.043

108

Table D.8. CORRELATION TABLE - SIC 26 Paper and Allied Products

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	. 1,4	.11	02	02	.03
Employment		-	.72	.40 `	.30	.74
Process Weight			-	.16	05	.90
Energy				-	.88	.35
Coal					-	.19
Controlled Emissions				. •		-

COMBEL	AND REGR	ES AMO	NG EMISSIONS AND	PPEDICTORS		,	05/03/73	PAGE 52	
FILE	CORREC	(CPE A	TION DATE = M5/M	3/731			SIC 26 Paper and	Allied Products	
	VAPTA	BLE	CASES	MFAN	STD DEV				
	14221	2	25	23.7320	48.9834		Space (acres)		
	11.27		25	257.2400	244.3931		imployment		
	VA-7V		25	22.4631	101-5388		Process Weight (t/	hr)	
	VA#74		25	15.4079	31.9324		Energy (MBtu/hr)	,	
	VARRY		25	6.0272	30.1360	•	Coal (MBtu/hr)	•	
	74020		25	51.7551	142.9213		Uncontrolled Emiss	ions (lhs/hr)	
	AVEVA		25	5.0808	11.2124		Controlled Emission		
	V,	• • •		MU; TIPL	_	RESSID		, , , , , , , , , , , , , , , , , , ,	
		015	VADGGO		_			,	
DEPERE	HT VAHTAL	4CE	VARØØS			_			
				Su	MMARY TABLE				
1451466	. ξ			WLTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	В	BETA
1241 6				Ø € 9 Ø Ø 9 Ø Ø 9 Ø Ø 9 Ø Ø 9 Ø Ø 9 Ø Ø 9 Ø Ø 9 Ø	0.81068	0.81.068	0.99038	0.09833	0.89849
12-11-6				8 • 93057	A.86595	0.05527	0.19341	0.09428	1.25341
142				93262	Ø • 86979	0.00383	0.03127	-0.01522	-7-166643
4-663				V • 93312	0.87072	0.02293	0 • 73719	0.00256	2884548 4888548
1647,5	_			Ø+93327	0.87100	0.00028	9.34927	-0.01381	-4.00.3234
(CONTA	(** 1 )							5.55953	
DEFENDE	ST VAPIA	:Lf	VARGOS						
				SU	MMARY TABLE				
AV5 1 V GE	r			OLTIPLE R	K SQUARE	RSQ CHANGE	SIMPLE R	н	BETA
142693				0.73719	0.54344	0.54344	0.73719	0.03905	0.74668
A2552				0.74044	0.54425	0.00481	0.03127	-0.01602	-0.07000
CCNSTA	117)					0.00.00		-4.58419	
DEPENDA	*1 V421A*	115	VAR 204						
				SU	MMARY TABLE				
18 4 1 4 A V	¢.			NULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	н	BETA
VAF503 {CC45TA	u <b>1)</b>			0.71538	0.51173	0.51178	0./1538	0.33981 -64.69324	0.71538
Cependi	NT VARIAT	: E	VAROOS	•					.=
				SU	MARY TABLE				
VAPTABL	F			AULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	8	H- I A
VA2003				0.40012	0.16009	0.16009	0.40012	0.06112	0.41035
14-557				0.40104	0.16568	0.00559	-0.01979	-0.04919	-0.01545
(CC),STA	41)							0.85312	
								·	

.

Table D.9. CORRELATION TABLE - SIC 30 Rubber & Miscellaneous Plastic Products

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.71	.17	.63	-	09
Employment		-	28	.31	<u>-</u>	16
Process Weight	·		-	.35	-	.30
Energy				-	<del>-</del>	.67
Coal					-	-
Controlled Emissions	•					-

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CONSEL THO N	EGRES AMO	THE EMISSIONS AND	PREDICTORS			05/03/73	PAGE 57	
FILE COPPE	G ICREA	1719N DATE - 45/83	/73)			SIC 30 Rubber & Plastic		
VA	PIABLE	CASES	MEAN	STD DEV		1105110	"	
74	P782	15	44.1640	74.6698		Space (acres)		
	40/3	15	283+5332	405.7395		limployment		
	6224	15	6.9827	16.2064		Process Weight (1	(/hr)	•
	PROS	15	17.0220	31.5517		Energy (MBtu/hr)		
	P775	15	0.0	0.0	•	Coal (MBtu/hr)		
	2227	15	32.3573	92.2821	*	Uncontrolled Emis	sions (lbs/hr)	
	RZER	15	3.9513	9.6917	-	Controlled Emiss	ions (1bs/hr)	
• • • • • •			• • • • MULTIPL	E PEGI	R E S S 1 0	N • • • • •		
SEPESSERT VA	FIAHLE·	VAPUOR						
			Su	MMARY TABLE	Ε			
VARIFEE			FULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	В	BETA
1447/5			₽∙66565	0.44309	0.44309	Ø+66565	0.36978	1.21485
1 A 4 1 1 2			0.92747	0.86020	0.41712	-0.08526	-0.12091	=1.046.32
16-3			0.93188	0.86840	0.00419	-A • 15536	0.03311	a.13159
(CONSTANT)							2.11550	
							-	
				•				
DEPENDENT VAN	IASt F	VAROOR						
			SUM	MARY TABLE				
71841541			MILTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	н	HETA
712003			0.15536	0.02414	0.02414	-0.15536	-0.00444	-0.18955
16.14.32			0.15911	0.02532	0.00118	-0.08526	0.03623	0.04846
455 (STANT)							4.94154	
SEPENDENT VAN	TABLE	VA2034						
			SUM	MARY TABLE	•			
112414AV			FULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	в	8E1A
142403			0.28063	0.07875	0.07875	0.28063	0.01267	0.31720
VA2332			0.28302	0.08010	0.00135	0.17194	-0.01125	-0.05164
(CONSTANT)					******		3.89726	
							20001211	
DEPTIOENT VAR	IAGLE	VARTOS			•			
			SUM	MAKY TAULE				
ANDIARE			ULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	В	HETA
VAROO2			0.62742	0.39366	0.39366	0.62142	0.34392	0.81391
742773			0.654/9	0.42876	0.03510	0.30987	-0.02056	-0.26433
(CINSTANT)			3,33,11,				7.66147	
100.1315.113								

Table D.10. CORRELATION TABLE - SIC 37 Transportation Equipment

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.45	22	.19	. 28	13
Employment		-	25	.51	.60	03
Process Weight			-	16	12	.94
Energy				<u>.</u>	.93	.19
Coal			,		-	.23
Controlled Emissions						-

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FILE								
	COPPES (CRE	ATION DATE . ME	5/73/731			SIC 37 Transportat	ion Equipment	
	VARTABLE	CA9£9	MEAN	STD DEV	•	•		•
	AVBAND	12	75.0417	112.2263		Space (acres)		
	1448K3	12	1414.6665	1552 - 3781		Employment		
	122776	12	1.7092	5.4622	** .	Process Weight (t/h	r)	-
	122765	12	18.5525	30.3073		Energy (\Btu/hr)	• ,	
	VAP 2.16	-12	10.3533	30.8047		Coal (MBtu/hr)	*	
	VAN287	ié	58.3141	77.9441			(1) A >	
	VAPOZB	12	4.2017	8.6579		Uncontrolled Emissi Controlled Emission:		
		• • • • • • •		PLE REG	RESSIOI			
JEHF LAE	TOT VARTABLE	VAHUUR						
				SUMMARY TABL	E			
/ASTERL	Ę.		FILTIP	LE R R SQUARE	RSQ CHANGE	SIMPLE R	В	BETA
/A50/4			7.97	645 0.87694	0.87694	0 • 93645	1.57035	5166.5
1457.5			9.99			0.18794	0.05792	2.2027
, A - 7			9 • 9 9 0 • 9 9			0.55704	0.03759	P+1337
								5.6395
ALLA, 3	. • .		0.99	781 0.99563	2.02054	-0.02956	0.00017	6.6305
CSNSTA	NT)						-0.18679	
FPF 41)FM	T VAZIANIF	VARODS						
				SUMMARY TABLE				
APIAGLE			MOLTIPE	ER R SQUARE	RSQ CHANGE	SIMPLE R	н	BETA
42 172			0.131	0.01722	0.01722	-0.13124	-0.01144	-0.14835
47003			0.135	48 0.01835	0.00113	-0.02956	0.00021	0.03//3
CLISTAN	T )						4.76285	
_ 4 4	•					•		
EPENGEN	T VAPIANET	VA9094						
				SUMMARY TABLE				
APTABLE			MILTIPL	ER R SQUARE	RSQ CHANGE	SIMPLE R	В	BETA
42333			0.245	93 0.06048	0.06048	-0.24593	-0.00064	-0.18328
62712			0.215	0.07564	0.01515	-0.22126	-0.10672	-0.13813
CONSTAN	1)						3.12599	•
•	·							•
EPFYDEY	T VAPIANLE	VA-1705						
				SUMMARY TABLE				
APIABLE			MULTIPL	ER R SQUARE	RSQ CHANGE	SIMPLE N	н.	8614
A2653			0.514	27 0.26667	0.26661	0.51427	0.01051	()_5 (#4.1
A2693 A2692			0.514 0.516		0.2644 <i>1</i> 0.0022 <i>1</i>	0.5142 <i>1</i> 0.19079	0.01051 ~0.01444	0.53851 -0.05346

Table D.11. CORRELATION TABLE - SIC 39 Miscellaneous Manufacturing Industries

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space		.28	24	. 55	.57	22
Employment		-	07	.10	0	07
Process Weight			_	10	05	.99
Energy				-	. 28.	09
Coal					-	03
Controlled Emissions						<u>-</u>

CORRET	AND RESPES AND	NG EMISSIONS AND	PPEDICTORS			05/03/73	PAGE 67	
FILE	COPPES COREA	TION DATE - 05/0	3/73)			SIC 39 Misc. Manu	facturing Industries	,
	VARTABLE	CASES	MEAN	STD DEV	•			
	VAF202	29	5.2735	5.2509		Space		
	ENGENA	54	260.1499	203.8884		Employment		
	VA4224	27	0569.5	11.9097		Process Weight (t/)	ir)	
	¥442K5	20	1.7380	2.7630		linergy (MBtu/hr)		
	VAH2V6	2%	0.2510	1.1225		Coal (MBtu/hr)		
	VA-277	29	15.6130	29.5590	_	Uncontrolled Emissi	ons (lbs/hr)	
	VARPER	20	2.4860	10.0567		Controlled Emission	ns (lbs/hr)	
			*** HU  TIPL	E REG	RESSIO	N • • • • • • •	• • • • • • • •	• • • • •
DEFF 1.0F	** VAPIABLE .	VALUUR				•		
			su	MMARY TABL	E			
/AHIZEL	€		+ ULTIPLE R	R SQUARE	RSO CHANGE	SIMPLE R	В	BFT▲
1447.4			(1499949	Ø+99897	0.99897	a+99949	0.84573	1.0015
1647.6			0.99967	0.99934	0.00037	-0.03291	0.14948	3.6166
164715			1+99969	0.99938	0.00004	-0.09413	0.01935	2.0452
va42.3			0 • 99969	. 0.99939	. 0.00001	-0.06667	8.80818	6555.4
14-1.2			V • 99969	0.99939	0.00000	-0.22242	0.00417	1569.5
1CG-16TA	NT)						0.09052	•
				÷				
OFPERUIP	NT VARIABLE	800HAV						
			SU	MAKY TABLE	<del>!</del>			
) 1641 94V	f		COLTIPLE R	R SQUARE	KSQ CHANGE	SIMPLE R	в	BETA
VAPOOZ LCONSTAN	NT)		0.22242	0.04947	0.04947	-0.22 <b>242</b>	-0.42598 4.73243	-0.2224
OFPENDEN	T VARIABLE	VAP 004						
			SUM	MARY TABLE				
AND I VBL E	•		FULTIPLE R	R SQUARE	KSQ CHANGE	SIMPLE R	н	BETA
VAPODZ CONSTAN	(f)		0.23719	0.05626	0.05626	-0.23719	-0.53797 5.52897	-0.23719
CEPFNOFN	IT VAPTABLE	VAROO5						
			SUN	IMARY TAULE				
VAPTABLE	:		FULTIPLE R	R SQUARE	RSQ CHANGE	SIMPLE R	н	BETA
¥44332 ¥44333 {€645788			0.54902 0.55181	0.30142 0.30450	0.30142	0.54902 0.10038	0.29739 -0.00078 0.37328	0.56518

Table D.12. CORRELATION TABLE - SIC 36 Electrical Machinery, Equipment and Supplies

	Space	Employment	Process Weight	Energy	Coal	Controlled Emissions
Space	-	.15	11	.08	.11	.01
Employment		-	.14	.68	.13	.24
Process Weight	·		-	.21	07	.81
Energy				-	.47	.27
Coal					-	.20
Controlled Emissions	·					-

						: :		
				•				
COMPEL A	AND PEGRES AMO	ONG EMISSIONS AND	PREDICTORS			: 05/03/73	PAGE 72	
FILE C	COPRES (CRE)	ITION DATE # 95/03	/731				Machinery, Equipment,	
	VARIABLE	CASES		STD DEV		and Suppli	es equipment,	
			MFAN	-				
	A <b>P</b> # A & & \$	31 31	21.4949 766.9675	22.4546 766.8181		Space		
	AT5480	31	0.4719	1.275		Employment Process Weight (t/h	ır)	
	449765	31	7.4864	13,1412		Energy (MBtu/hr)	·	
	742775 74227	31 31	0 • 1 700 1 3 • 7002	ؕ9465		Coal (MBtu/hr)	(I) B >	
	ATSAVA	31	1.3345	21+6211 2+5488		Uncontrolled Emissi Controlled Emission		
• • • •	• • • • • •		· · · · HUL TP	LE REG	R E S S 1 0	N	• • • • • • •	• • • • • •
CE+4 1.04 1	T VA-TABLE	RNKHAV						
				SUMMARY TABL	Э.	•		
.ASIABLE	Ī.		My.TTpLE	R R SQUARE	RSQ CHANGE	SIMPLE R	8	9514
16-7,6			1.8106			0.81861	1.71354	1.85566
18-503			* • 8 <sub>4</sub> ዓ ቁ ነ • 8 ዓ ቁ ጻ			0.19773	0.87124	3,32355
14-11-5			1.8654			ؕ23904 ؕ27151	0.00073 +0.0422	492594
12-1.8			4.8470			0.00777	9.99815	≠0+21763 2+05395
105-10141	.7 }						0.03368	
SEPFNOFNT	VAPIABLE	VAPOOR						
			•	SUMMARY TABLE	:			
A80 1 V 61 1			MULTIPLE	R R SQUARE	RSQ CHANGE	SIMPLE R	9	HETA
142673			C.23904		0.05714	0.23904	0.00081	0.24328
989592 460557857	1)		C.24069	0.05/93	0.00014	0.00111	-0.00323 0.78347	-0.02846
							•	
SERFYSELT	3 JAATAAV	VAPUN4						
				UMMARY TABLE			ú	REIA
AVAIVELE			MULTIPLE	R R SQUARE	RSQ CHANGE	SIMPLE K	₿	
VAP 993			(.13580		0.01844	0.13580	0.0 1026 -0.00782	0.15633 -0.13/91
SCC 421211 TRATENT	13		( , 19239	0.03701	0.01857	-0.11453	0.44004	-0.13/31
SEPEROFIA	VARIABLE	¥44005			1			
			5	UMMARY TABLE				
1481 5AV			MULTIPLE	R R SQUARE	HS4 CHANGE	SIRPLE R	н	BETA
VAPCO3			(.67482		0.46215	0.67982	0.01171	10.68301
VARCOZ COMSTANT	,		(.68015	0.46260	0.00045	0.08029	-0.01255	-0.02145
II, III , IANI	•						-1.22231	

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  Revised, 1972.

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# 16. ABSTRACT

In order to evaluate or rank land use plans in terms of air quality, it is necessary for planners to be able to project emission density (mass of pollutant per unit of land for any specified time period) using only planning variables, because detailed source characteristics are not available at the time alternative plans are being developed and evaluated. The objective of this study is to analyze the collisty of various land use paramters in describing the air quality impacts of land use plans.

Parameters that are tested include land use by zoning class and 2-digit SIC code, employment dwelling units, and square footage of floor space. Variables that are to be explained by these parameters include air quality as represented by the Air Quality Display Model (AQDM), emissions and emission densities, process weight for industrial sources, and energy consumption.

7. KEY WORDS AND DOCUMENT ANALYSIS								
DESCRIPTORS	b.IDENTIFIERS/OPEN ENDED TERMS	c. COSATI Field/Group						
Land Use Planning and Zoning Local Government Air Pollution Control Agencies Area Emission Allocations								
8. DISTRIBUTION STATEMENT Unlimited	19. SECURITY CLASS (This Report)  20. SECURITY CLASS (This page)	21. NO. OF PAGES  22. PRICE						

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