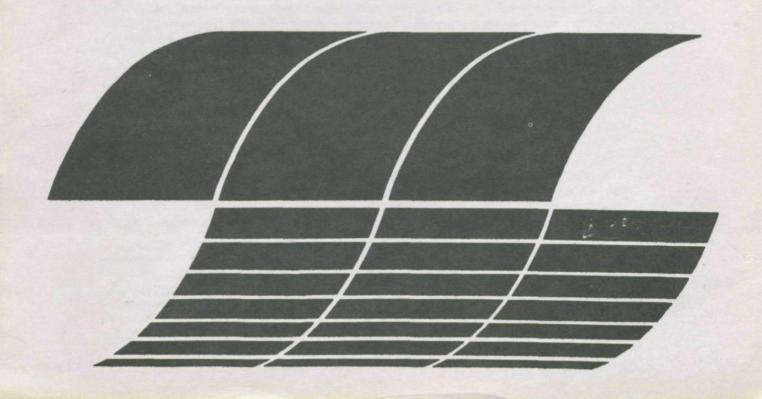
Tennesee Valley Authority Office of Power Emission Control Development Projects Muscle Shoals AL35660 ECDP B-4

Definitive SO_X Control Process Evaluations: Limestone, Double Alkali, and Citrate FGD Processes

Interagency Energy/Environment R&D Program Report



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DEFINITIVE $SO_{\mathbf{x}}$ CONTROL PROCESS EVALUATIONS

LIMESTONE, DOUBLE-ALKALI, AND CITRATE FGD PROCESSES

bу

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ABSTRACT

A detailed comparative technical and economic evaluation of limestone slurry, generic double alkali, and citrate flue gas desulfurization (FGD) processes was made assuming proven technology and using representative power plant, process design, and economic premises. For each process, economic projections were made for a base case (500 MW, 3.5% sulfur in coal, new unit) and case variations in power unit size, fuel type, sulfur in fuel, new and existing power units, waste slurry ponding and filter cake trucking, and sulfur dioxide (SO₂) removal (1.2 lb SO₂ allowable emission per million Btu heat input vs 90%). Capital investment, annual revenue requirements (7000 hr/yr), and lifetime revenue requirements over a 30-year declining operating profile were estimated for the base case and each variation. Investment costs were projected to mid-1979; annual revenue requirements were calculated in projected mid-1980 dollars. Effects of variations in raw material costs, energy costs, maintenance costs, cost of capital, and net sales revenue and operating labor cost escalation were studied.

Depending on unit size and status, fuel type and sulfur content, solids disposal method, and overall project scope, the ranges in estimated capital costs in 1979 dollars are \$71 to \$127/kW for limestone slurry, \$80 to \$130/kW for generic double alkali, and \$105 to \$194/kW for citrate (recovery process). The results can be scaled or altered to reflect other site-specific conditions.

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ABBREVIATIONS AND CONVERSION FACTORS

ABBREVIATIONS

ac	acre	kWh	kilowatt-hour
aft ³ /min	actual cubic feet per	1b	pound
•	minute	L/G	liquid-to-gas ratio in gallons
bb1	barrel		per thousand actual cubic
Btu	British thermal unit		feet of gas at outlet condi-
$o_{\mathbf{F}}$	degrees Fahrenheit		tions
dia	diameter	M	million
FGD	flue gas desulfurization	mi	mile
ft	feet	mo	month
ft ²	square feet	MW	megawatt
ft ³	cubic feet	ppm	parts per million
ga l	gallon	psig	pounds per square inch (gauge)
gpm	gallons per minute	rpm	revolutions per minute
gr	grain	sec	second
hp	horsepower	sft ³ /min	_
hr	hour		minute (60°F)
in.	inch	SS	stainless steel
k	thousand	yr	year
kW	kilowatt		

EPA policy is to express all measurements in Agency documents in metric units. Values in this report are given in British units for the convenience of engineers and other scientists accustomed to using the British systems. The following conversion factors may be used to provide metric equivalents.

	British		Metric			
ac	acre	0.405	hectare	ħa		
bb1	barrels of oil ^a	158.97	liters	L		
Btu	British thermal unit	0.252	kilocalories	kca1		
of	degrees Fahrenheit minus 32	0.5556	degrees Celsius	оС		
ft	feet	30.48	centimeters	cm		
ft ²	square feet	0.0929	square meters	m^2		
ft ³	cubic feet	0.02832	cubic meters	m ³		
ft/min	feet per minute	0.508	centimeters per second	cm/sec		
ft ³ /min	cubic feet per minute	0.000472	cubic meters per second	m^3/sec		
gal	gallons (U.S.)	3.785	liters	l		
gpm	gallons per minute	0.06308	liters per second	l/sec		
gr	grains	0.0648	grams	g		
gr/ft ³	grains per cubic foot	2.288	grams per cubic meter	g/m^3		
hp	horsepower	0.746	kilowatts	kW		
in.	inches	2.54	centimeters	cm		
1b	pounds	0.4536	kilograms	kg		
1b/ft ³	pounds per cubic foot	16.02	kilograms per cubic meter	kg/m ³		
lb/hr	pounds per hour	0.126	grams per second	g/sec		
psi	pounds per square inch	6895	Pascals (Newton per square meter)	pa (N/m^2)		
mi	miles	1609	meters	m		
rpm	revolutions per minute	0.1047	radians per second	rad/sec		
sft ³ /min	standard cubic feet per minute (60°F)	1.6077	normal cubic meters per hour (0°C)	Nm ³ /hr		
ton	tons (short)b	0.9072	metric tons	tonne		
ton, long	tons (long)b	1.016	metric tons	tonne		
ton/hr	tons per hour	0.252	kilograms per second	kg/sec		

a. Forty-two U.S. gallons per barrel of oil.

b. All tons, including tons of sulfur, are expressed in short tons in this report.

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DEFINITIVE SOx CONTROL PROCESS EVALUATIONS - PHASE I

EXECUTIVE SUMMARY

Under the provisions of the Clean Air Act of 1967 and its subsequent amendments, the U.S. Environmental Protection Agency (EPA) has funded research and development on sulfur dioxide (SO₂) removal processes, including the publication of several conceptual design and cost studies. This report is one of a series of flue gas desulfurization (FGD) studies sponsored by EPA to determine comparative costs of some of the more prominent SO₂ removal systems now being offered by vendors. Three processes are evaluated in this report—limestone slurry, generic double alkali, and citrate scrubbing. Process evaluations in subsequent studies will include lime scrubbing, magnesia scrubbing, the Wellman-Lord sodium sulfite process, and the Rockwell International aqueous carbonate process.

PROCESS DEFINITION

A brief description of the three processes in this study and the data sources used as the basis are given below. The process data represent the state of technology in late 1977.

Representative flow diagrams, material balances, plant layouts, and equipment arrangements are included in the report for the base case (new 500-MW coal-fired unit, 3.5% sulfur in fuel, 1.2 1b SO_2 emission per million Btu heat input) of each process. These and detailed equipment descriptions define the systems estimated.

Limestone Slurry Process

Stack gas is scrubbed with a recirculating slurry of limestone and reacted calcium salts in water (pH about 5.8) using a presaturator unit for cooling and humidification and a mobile-bed scrubber for $\rm SO_2$ removal. Limestone feed is wet-ground prior to addition to the scrubber effluent hold tank. Calcium sulfite and sulfate salts are withdrawn to a disposal pond where they settle to a 40% solids sludge. Cleaned stack gas is reheated to $\rm 175^{o}F$. Design is based on data taken from the TVA-EPA-Bechtel Shawnee test program and TVA Widows Creek unit 8.

Generic Double-Alkali Process

Stack gas is cooled and humidified in a presaturator using recycled scrubber effluent and scrubbed in a perforated-plate scrubber with regenerated sodium sulfite(pH about 6.0). A bleedstream of scrubber effluent is reacted with lime to regenerate sodium sulfite and produce calcium sulfite and sulfate salts. After filtering and washing to recover the sodium sulfite solution, the calcium sulfite-sulfate cake is reslurried and pumped to the disposal pond where the salts settle to 40% solids. Makeup soda ash is added at the thickener overflow tank. Cleaned stack gas is reheated to 175°F. The double-alkali design is generalized from several processes currently offered in the United States.

Citrate Process

Stack gas is cooled and humidified in a presaturator using recycled liquor and scrubbed in a packed-tower scrubber with regenerated citrate solution (pH about 4.5). A bleedstream of presaturator recycle liquor is neutralized with lime and discarded to control chlorides in the system. Scrubber effluent is reacted with hydrogen sulfide (H₂S) to produce elemental sulfur and regenerate the citrate scrubbing solution. Sulfur is separated by air flotation, melted, and stored in liquid form to be sold. Part of the sulfur is combined with natural gas and steam to form H₂S for use in the reduction process. Makeup soda ash and citric acid are added to replace losses due to handling and oxidation of sulfite to sulfate. Sodium sulfate crystals are purged from the system and discarded. Cleaned stack gas is reheated to 175°F. Conceptual design for the generalized citrate process is based primarily on the U.S. Bureau of Mines system. Design differences in the Bureau of Mines demonstration unit have been noted.

MAJOR DESIGN AND COST FACTORS

The base case for evaluating the three processes is a new, 500-MW, coal-fired power unit located in the Midwest (Illinois, Indiana, Kentucky area). The project schedule begins in mid-1977 with a 3-year construction period ending mid-1980. The midpoint of construction costs is mid-1979; revenue requirements are estimated in mid-1980 dollars.

Other important design and cost assumptions used in the evaluations are:

- The coal has a heating value of 10,500 Btu/lb and contains 16% ash.
- \bullet SO₂ removal reduces emissions to 1.2 1b SO₂ per million Btu heat input.
- Stack gas is reheated to 175°F.
- Both ponding and trucking disposal at a site 1 mile from the FGD facilities are evaluated for the limestone and double-alkali processes. Thirty-day storage and a base value of \$40 per short ton for sulfur have been used for the citrate process.

- The use of a fully developed design is assumed. No redundancy is included; only spare pumps are included. A second pond transport line is included in disposal cases. An orderly and well-managed design and construction program is assumed.
- Revenue requirements are estimated on 7,000-hour annual operation.

RESULTS

Summaries of capital investment, annual revenue requirements, and lifetime operating costs for all cases estimated are displayed in Tables S-1, S-2, and S-3, respectively.

Capital Investment

In order of increasing investment, the base case process ranking is (1) limestone slurry, (2) generic double alkali, and (3) citrate.

Except for the waste-disposal-by-trucking cases, limestone has the lowest capital investment and citrate has the highest for each variation. The limestone trucking alternative capital investment is 2.4% higher than the double-alkali case because limestone FGD produces more waste solids and requires a larger investment in the feed preparation area.

Capital investment for the existing power unit variation is greater than the new power unit variation at each plant size with the exception of the limestone 200-MW cases. For the existing limestone 200-MW unit the decrease in cost due to decrease in pond size based on a remaining life of 20 years slightly outweighs the increase in labor charges required for retrofit.

 $\rm SO_2$ removal of 90% compared with $\rm SO_2$ removal equal to 1.2 1b $\rm SO_2$ emission per million Btu heat input increases base case capital investment by 3.5% to 4.2%.

Base case projections described here represent a proven FGD system designed with no redundancy and operating at minimum required removal capacity on flue gas from 3.5% sulfur coal. As an indication of how the project scope and corresponding investment could vary, the effects of changes in process design and indirect charges on the limestone base case estimate are shown in Table S-4. Changes such as 50% redundancy, 90% SO₂ removal, 6% sulfur in coal, increased stoichiometry, greater entrainment in the cleaned gas, and a larger contingency charge can double the investment requirement for the limestone slurry process. Similar effects on investment needs can be expected in the double-alkali and citrate processes with changes in project scope.

TABLE S-1. SUMMARY OF TOTAL CAPITAL INVESTMENT REQUIREMENTS^{a,b}

		Limestone pi	rocess	Generic dou alkali proc	ess	Citrate process		
	Years remaining	Total capital investment,		Total capital investment,		Total capital investment,		
Case	life	\$	\$/kW	\$	\$/kW	\$\$	\$/kW	
Coal-Fired Power Unit								
1.2 1b SO ₂ /MBtu heat input								
allowable emission; onsite	:							
solids disposal (ponding)				26 226 222	100.0	20 700 000	100 /	
200 MW E 3.5% sulfur	20	25,057,000	125.3	26,006,000	130.0	38,788,000	193.9	
200 MW N 3.5% sulfur	30	25,461,000	127.3	25,477,000	127.4	38,075,000	190.9	
500 MW E 3.5% sulfur	25	50,120,000	100.2	53,675,000	107.4	72,605,000	145.2	
500 MW N 2.0% sulfur	30	39,641,000	79.3	42,110,000	84.2	58,098,000	116.2	
500 MW N 3.5% sulfur	30	48,728,000	97.5	50,551,000	101.1	71,639,000	143.3	
500 MW N 5.0% sulfur	30	54,621,000	109.2	57,579,000	115.2	82,572,000	165.1	
1,000 MW E 3.5% sulfur	25	74,830,000	74.8	85,487,000	85.5	109,024,000	109.0	
1,000 MW N 3.5% sulfur	30	71,423,000	71.4	79,016,000	79.0	106,589,000	106.6	
Solids disposal by trucking								
500 MW N 3.5% sulfur	30	42,307,000	84.6	41,335,000	82.7	-	-	
90% SO ₂ removal; onsite								
solids disposal (ponding)								
500 MW N 3.5% sulfur	30	50,437,000	100.9	52,404,000	104.8	74,624,000	149.2	
Oil-Fired Power Unit								
0.8 lb SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)								
500 MW E 2.5% sulfur	25	38,480,000	77.0	40,260,000	80.5	52,442,000	104.	

a. Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979. Minimum in-process storage; only pumps are spared. Disposal area located l mile from power plant. Investment requirements for fly ash removal and disposal excluded. Construction labor shortages with accompanying overtime pay incentive not considered.

b. These investment costs are characterized by the defined premises and assumptions. Modifying the project scope of the limestone process as shown in Table S-4 can increase system costs by \$96/kW or more depending on the assumptions made.

TABLE S-2. SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS

(INCLUDING BYPRODUCT CREDIT)

		Limestone	process	Generic do alkali pro		Citrate process		
Case	Years remaining life	Average annual revenue requirements,	Mills/kWh	Average annual revenue requirements,	Mills/kWh	Average annual revenue requirements,	Mills/kWh	
Coal-Fired Power Unit								
1.2 1b SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)								
200 MW E 3.5% sulfur	20	7,479,400	5.34	7,553,000	5.40	12,289,200	8.78	
200 MW N 3.5% sulfur	30	7,153,200	5.11	7,169,100	5.12	11,670,800	8.34	
500 MW E 3.5% sulfur	25	14,789,400	4.23	15,441,700	4.41	23,174,000	6.62	
500 MW N 2.0% sulfur	30	11,624,900	3.32	11,335,300	3.24	17,091,700	4.88	
500 MW N 3.5% sulfur	30	14,101,900	4.03	14,676,000	4.19	22,538,000	6.44	
500 MW N 5.0% sulfur	30	16,032,200	4.58	17,741,900	5.07	27,513,400	7.86	
1,000 MW E 3.5% sulfur	25	23,241,200	3.32	25,750,900	3.68	36,933,500	5.28	
1,000 MW N 3.5% sulfur Solids disposal by trucking	30	21,874,300	3.12	24,147,700	3.45	35,602,400	5.09	
500 MW N 3.5% sulfur 90% SO ₂ removal; onsite solids disposal (ponding)	30	15,172,400	4.33	14,293,900	4.08	-	-	
500 MW N 3.5% sulfur	30	14,651,300	4.19	15,438,800	4.41	23,812,400	6.80	
Oil-Fired Power Unit								
0.8 lb SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding) 500 MW E 2.5% sulfur	25	11,446,600	3.27	11,128,400	3.18	16,091,700	4.60	

a. Power unit on-stream time, 7,000 hr/yr. Midwest plant location, 1980 revenue requirements. Investment and revenue requirement for removal and disposal of fly ash excluded.

b. These revenue requirements are based on the defined premises and assumptions and the capital investments shown in Table S-1. They would vary as project scope changed; for example, with additions to the scope outlined in Table S-4, annual revenue requirements for limestone could increase to 9.37 mills/kWh for a new, 500-MW unit burning 3.5% sulfur.

TABLE S-3. SUMMARY OF LEVELIZED OPERATING COST OF FGD OVER POWER UNIT LIFETIME (INCLUDING BYPRODUCT CREDIT) $^{\mathbf{a}}$

		Limeston	e process	Generic double	-alkali process	Citrate	process
Case	Years remaining life	Cumulative present worth net increase (decrease) in cost of power, b \$	Levelized increase (decrease) in unit operating cost, mills/kWh ^c	Cumulative present worth net increase (decrease) in cost of power, b \$	Levelized increase (decrease) in unit operating cost, mills/kWh ^c	Cumulative present worth net increase (decrease) in cost of power, b \$	Levelized increas (decrease) in uni operating cost, mills/kWh ^c
Coal-Fired Power Unit							
1.2 lb SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)							
200 MW E 3.5% sulfur	20	52,811,700	9.28	53,388,600	9.39	84,862,500	14.92
200 MW N 3.5% sulfur	30	65,253,700	6.56	65,224,800	6.56	104,508,300	10.51
500 MW E 3.5% sulfur	25	122,034,600	5.82	127,562,500	6.09	187,099,800	8.93
500 MW N 2.0% sulfur	3 0	104,931,000	4.22	103,925,200	4.18	153,984,800	6.20
500 MW N 3.5% sulfur	30	127,709,200	5.14	132,472,900	5.33	200,363,000	8.06
500 MW N 5.0% sulfur	30	144,837,500	5.83	158,278,400	6.37	241,941,500	9.74
1,000 MW E 3.5% sulfur	25	188,891,100	4.51	209,774,100	5.00	293,113,800	6.99
1,000 MW N 3.5% sulfur solids disposal by trucking	30	195,672,000	3.94	215,525,300	4.34	312,517,300	6.29
500 MW N 3.5% sulfur 90% SO ₂ removal; onsite solids disposal (ponding)	30	132,750,600	5.34	125,275,900	5.04	-	-
500 MW N 3.5% sulfur	30	132,602,400	5.34	138,947,500	5.59	211,103,800	8.50
Dil-Fired Power Unit							
.8 1b SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)		a. a		02.002.602		121 /10 200	6 27
500 MW E 2.5% sulfur	25	94,271,900	4.50	93,023,600	4.44	131,410,200	6.27

a. Basis

Power unit operating profile for 30-year life = 7,000 hours - 10 years, 5,000 hours - 5 years, 3,500 hours - 5 years, 1,500 hours - 10 years. Midwest plant location, 1980 operating costs.

Investment and revenue requirements for removal and disposal of fly ash excluded.

Constant labor cost assumed over life of project.

b. Discounted at 10% to initial year.

c. Equivalent to discounted process revenue requirement over life of power unit.

TABLE S-4. LIMESTONE SLURRY PROCESS

ADDITIONAL INVESTMENT REQUIRED FOR MODIFIED PROJECT SCOPE

	Investment required, \$/kW
Base case - limestone slurry process: 500-MW new unit burning coal containing 3.5% sulfur, 16% ash, 10,500 Btu/lb neat value; 1.2 lb SO ₂ allowable emission per MBtu heat input; 0.1% liquid entrainment in cleaned stack gas; 30-yr life, 127,500-hr operation; no redundancy; 20% contingency; onsite solids disposal; mid-1979 cost basis	97.5
	Additional investment required, \$/kW
Modified case: 500-MW new unit burning coal containing 5% sulfur, 16% ash, 10,500 Btu/1b heat value; 90% S02 removal; 0.3% liquid entrainment in cleaned stack gas; 30-yr life, 127,500-hr operation; 50% redundancy; onsite solids disposal, mid-1979 cost basis	
Investment increases due to:	
Increased raw material handling	18.3
Larger waste disposal area and pond	46.9
50% redundancy of ball mills, scrubbers, and other equipment	30.8
Total increase in capital investment	96.0

Annual Revenue Requirements

For base case conditions the ranking of average annual revenue requirements for the processes is the same as the investment ranking: (1) limestone slurry, (2) generic double alkali, and (3) citrate.

Capital charges are the largest component of revenue requirements for all processes. Electrical demand is significantly greater for the limestone and citrate processes than for the double-alkali process. Raw materials cost is 19% and 22% of the total revenue requirements for base case citrate and double alkali, respectively, while raw material cost for limestone is only 8% of the total. For all case variations estimated in this study, projected 1980 FGD revenue requirements range from 3.25 to 8.78 mills/kWh.

Lifetime Revenue Requirements

The relative rankings in levelized lifetime revenue requirements are similar to those projected for annual requirements. Lifetime levelized revenue requirements are slightly higher than corresponding average annual revenue requirements because of the declining operating profile of the power unit. The average on-stream time over the life of the plant is 4,250 hr/yr, compared to the higher on-stream time of 7,000 hr/yr used for the annual revenue requirement estimates.

CONCLUSIONS

Because ponding costs for the limestone process offset the additional equipment needs of the double-alkali process, capital investment requirements are quite similar for the two processes. The capital investment for the citrate process is considerably higher; however, it should be recognized that citrate is a recovery process and should also be compared with other recovery processes.

The limestone or lime slurry process is the best known and most completely developed FGD system in the United States today. The evaluation of limestone FGD in this study, reflecting the broad experience of vendors and utilities in constructing and operating this system, is based on considerable available data. Limestone is still the simplest and cheapest FGD process available today for most applications, but it continues to require intensive maintenance effort, and it produces a waste sludge of questionable stability and environmental effect.

Although construction and operating experience is not as extensive for the double-alkali process as for limestone, unit areas in the double-alkali process can be compared either with limestone or with other chemical operations for an understanding of design and operation. Double-alkali FGD is a competitive alternative to limestone, especially when trucking is used to dispose of the waste filter cake. Even though double alkali is a waste-producing process, the system produces less waste solids than

limestone, requiring a smaller area for disposal, and it regenerates the process scrubbing liquor. Because of system design, it is expected to require less maintenance than limestone.

As a recovery system, the citrate process is inherently more expensive and should not be compared only with the waste-producing processes evaluated here but also with other recovery processes. For this study the citrate process is assumed proven, but less is known about the unit areas of the process as an integrated operating system than is known about the limestone or double-alkali processes, and the operation of many of these areas is more complex. Although the citrate process offers the advantage of producing a salable byproduct, the use of natural gas in the reduction step could limit its application. It is important that the citrate process be proven in the field in order to more fully answer the questions of real cost and operability.

INTRODUCTION

Coal-fired power plants are a major source of the sulfur dioxide (SO₂) emitted to the atmosphere in the United States. By the end of 1976, 54% of the electricity generated in the United States was being produced from coal-fired power plants according to <u>Electrical World</u> (1977c). The Federal Energy Administration (FEA) predicts that by 1985 this figure will increase to 70% of the total electrical energy produced (<u>Electrical World</u>, 1977b). Critical attention is focused on the electrical power utility industry as it searches for reliable emission control methods that will meet the air quality regulations.

Possible SO₂ control alternatives to flue gas desulfurization (FGD) do exist. However, recent court decisions have denied the use of tall stacks and reduced production during periods of weather stagnation as control methods. Projected shortages of natural gas and fuel oils force a growing dependence on coal, but low-sulfur coal is not found in sufficient quantity in regions of greatest electrical demand. While the concept of coal desulfurization prior to combustion is under study, its development has not yet reached the commercial status of FGD.

Although scattered attempts at power plant SO₂ control were pursued in Europe as early as the 1930's clean air legislation in the United States made SO₂ control a necessity in this country in the 1960's. At this time government-sponsored research and development (R&D) began to focus attention on FGD and it became increasingly important to be able to evaluate the systems technically and economically from a standard basis of comparison. In 1967 the National Center for Air Pollution Control (now part of the U.S. Environmental Protection Agency-EPA) contracted with the Tennessee Valley Authority (TVA) for a series of conceptual design and economic studies to be carried out by TVA on FGD processes. The first studies evaluated four processes

- Dry process limestone injection (TVA, 1968)
- Limestone wet scrubbing (TVA, 1969)
- Ammonia scrubbing (TVA, 1970)
- Magnesia scrubbing (McGlamery, et al., 1973)

The earliest SO_2 removal systems were limestone or lime processes and much of the R&D through the late 1960's and early 1970's focused on limestone and lime as absorbents. A previous TVA-EPA publication (McGlamery, et al., 1975) included evaluations of limestone slurry and lime slurry scrubbing. Most FGD systems operating today at power unit sites are limestone or lime, representing over 90% of the 13,000 MW of removal capacity (commercial and demonstration) currently employed at U.S. power plants by 1978 (Laseke, et al., 1978).

Although limestone and lime processes are considered the least expensive methods of FGD at this time, the processes have several disadvantages:
(1) they require intensive maintenance, (2) they are once-through processes, i.e., the scrubbing slurry is not regenerated for reuse, and (3) the SO₂ is removed in the form of a waste sludge. Continuing R&D has developed processes that minimize or eliminate one or more of these problems.

Two of the three processes selected for evaluation in this study offer possible solutions to the disadvantages mentioned. The generic double-alkali process, representing several of the double-alkali processes now available in the United States, reduces maintenance requirements by introducing lime as a second alkali outside the scrubbing loop, thereby reducing the potential for calcium scaling. Although the system produces a waste sludge that is principally calcium sulfite, it does regenerate the sodium scrubbing liquor for recycle. The citrate process, based on the U.S. Bureau of Mines FGD system, also regenerates and recycles its scrubbing liquor. In addition, the process reduces the removed SO₂ to elemental sulfur, an important chemical feedstock.

TVA-EPA studies now in preparation will evaluate processes producing salable sulfur compounds on a comparative basis.

PROCESS BACKGROUND AND DESCRIPTION

Full-scale scrubbing of power plant flue gas was first undertaken at the Battersea power station in London, England, in the early 1930's. This and the scrubbing systems at English power stations that followed in the decade of the 1930's posed many chemical and design questions. Investigators such as G. W. Hewson, et al. (1933), J. L. Pearson, et al. (1935), and R. L. Rees (1953) in England and H. F. Johnstone, et al. (1938) in the United States studied these and other factors pertaining to SO2; much of their research is still applicable today and forms the basis for current R&D. The most concentrated R&D effort in the United States toward improved FGD has occurred in the past 15 years, especially since the passage of the clean air legislation in 1967 and 1970. A useful summary of regulations proposed through mid-1976 has been prepared by Chaput (1976).

For a better understanding of the specific processes evaluated in this study, the development of each is given including present status, process characteristics, and chemistry.

LIMESTONE SLURRY PROCESS

Limestone and lime absorption systems are the most widely used technology in the United States today for SO₂ removal from fossil-fueled power plant flue gas. About 90% of the equivalent megawatts for which removal systems are in use, under construction, or planned is limestone or lime absorption (Kennedy and Tomlinson, 1978).

The chemistry of limestone slurry scrubbing can be described by the following series of reactions from McGlamery, et al. (1975). Equations 1, 2, and 3 are reactions of SO_2 absorption in an aqueous scrubbing liquor.

$$SO_2(g) \stackrel{?}{\leftarrow} SO_2(ag)$$
 (1)

$$so_{2(aq)} + H_2O \stackrel{?}{\leftarrow} H_2so_3 \stackrel{?}{\leftarrow} Hso_3^- + H^+$$
 (2)

$$HSO_3^- \stackrel{\rightarrow}{\leftarrow} H^+ + SO_3^=$$
 (3)

Simultaneously, limestone dissolves into the scrubbing liquor as shown in equations 4 and 5.

$$CaCO_{3(s)} \stackrel{?}{\leftarrow} CaCO_{3(aq)}$$
 (4)

$$CaCO_{3(aq)} \stackrel{?}{\leftarrow} Ca^{++} + CO_3^{=}$$
 (5)

Sulfite ion combines with calcium to yield the very insoluble calcium sulfite hemihydrate.

$$\text{Ca}^{++} + \text{SO}_3^{-} + 1/2\text{H}_2\text{O} \stackrel{\rightarrow}{\leftarrow} \text{CaSO}_3 \cdot 1/2\text{H}_2\text{O} \downarrow$$
 (6)

Carbon dioxide, either in the flue gas or from calcium carbonate interacts with water as shown in equations 7 and 8.

$$co_{2(g)} + H_2O \stackrel{?}{\leftarrow} H_2co_{3(aq)} \stackrel{?}{\leftarrow} H^+ + Hco_3^-$$
 (7)

$$HCO_3^{-} \stackrel{?}{\leftarrow} H^+ + CO_3^=$$
 (8)

In addition, sulfite ion may be ultimately converted to gypsum by the following reactions.

$$so_3^{=} + 1/2o_2 \rightarrow so_{\Delta}^{=}$$
 (9)

$$Ca^{++} + SO_4^{=} + 2H_2O \stackrel{?}{\leftarrow} CaSO_4 \cdot 2H_2O_{(s)}$$
 (10)

Because detailed discussions of process development may be found in many publications by TVA (TVA, 1970; McGlamery, et al., 1975; Kennedy and Tomlinson, 1978), only a brief historical description of the limestone slurry process and some codevelopment of lime slurry will be included here.

The scrubbing process developed by the London Power Company for its Battersea and Bankside power stations (Hewson, et al., 1933; Rees, 1953) used alkaline water from the Thames River to remove dust and SO₂ from boiler exhaust gases. The once-through system returned acidic effluent to the Thames and required very large quantities of water which cooled the gas to low temperatures creating plume problems. To overcome these difficulties, Howden and Company and Imperial Chemical Industries (Howden - ICI) developed a limescrubbing process which was a first attempt at closed-water-loop operation. A process pilot plant was constructed in Billingham in 1933 and the process was used commercially at the Tir John (Swansea) and Fulham (London) power stations. The Tir John scrubbing system was soon shut down because of operational difficulties from the high ash content of the coal. Fulham operated until World War II. The two Battersea scrubbers were closed permanently in 1969 and 1974 because of plume problems and Bankside is now England's only operational FGD system.

Although Canada and the USSR began SO_2 removal development in the 1930's and 1940's using sorbents other than limestone or lime, very little more was done with limestone and lime scrubbing during this time. In 1953 TVA began a brief series of pilot-plant studies of several FGD processes including a packed-tower scrubber using a 10% slurry of pulverized limestone (Slack, 1971). Reliance on atmospheric monitoring and tall stack dispersion during this period reduced TVA's interest in the expansion of these studies.

FGD development intensified in the 1960's. Wisconsin Electric Power and Universal Oil Products conducted a 1-MW joint program in 1965 (Pollack, et al., 1967) on a coal-fired 120-MW boiler. Combustion Engineering and Detroit Edison (Plumley, et al., 1967) collaborated on a 1966-1967 program to study limestone injection into a boiler. Other U.S. companies--Babcock and Wilcox Company, Chemical Construction Corporation (Chemico), Research-Cottrell, Inc., Zurn Industries, and Peabody Coal Company--also developed limestone scrubbing data during this decade.

A joint TVA-EPA-Bechtel program began in 1967 at TVA's Shawnee Steam Plant, Paducah, Kentucky (Bechtel Corporation, 1973). The EPA-funded test demonstration facility includes three 10-MW scrubbers of different types; the test program is directed by Bechtel and the facility is operated by TVA. All phases of limestone and lime scrubbing are being studied, from operating optimization to equipment reliability. At present two of the scrubbers, a venturi followed by a spray tower and a Turbulent Contact Absorber (TM) (TCA). are being operated in an advanced test program which began in June 1974 and is scheduled to run through December 1979 (Head, 1977; Head, et al., 1978). The program objectives include demonstrating process and equipment reliability under varying flue gas conditions, determining the effect of additives on SO2 removal, determining the effectiveness of forced oxidation to produce an improved waste sludge product, characterizing stack gas emissions, and evaluating methods of automatic control. In August 1978 a program sponsored by the Electric Power Research Institute (EPRI) was begun to study cocurrent limestone scrubbing on the third scrubber.

In conjunction with the EPA-sponsored Shawnee test program, Bechtel and TVA have jointly developed a computer program capable of projecting comparative investment and revenue requirements for limestone and lime scrubbing (Torstrick, et al., 1978). The computer program has been developed to permit the estimation of relative economics of limestone and lime scrubbing systems for variations in process design alternatives or variations in the values of independent design variables. Although the program is not intended to compute the economics of an individual system to a high degree of accuracy, it is based on sufficient detail to allow the rapid projection of preliminary conceptual design and costs for various limestone and lime case variations on a common design and cost basis.

Currently, 11 commercial-sized limestone units are in operation in the United States (Table 1). Kansas Power and Light Company's Lawrence installation was the initial system cited by EPA as evidence of demonstrated technology. The limestone injection - wet scrubber system has been replaced on unit 4 with limestone scrubbing in a spray tower. The new system went onstream in January 1977. The same type scrubber changes were made on unit 5 and this operation began in mid-1978. The boilers began burning Wyoming low-sulfur coal (0.5%) in the fall of 1974.

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TABLE 1. COMMERCIAL, OPERATIONAL LIMESTONE FGD

SYSTEMS AT U.S. ELECTRIC POWER STATIONS (DECEMBER 1977)

Power plant			FGD installation				
		Unit	FGD		New/		
Utility	Station	No.	MW	startup	retrofit	Vendor	
Kansas Power and Light	Lawrence	4	125	12/68 1/77	R	Combustion Engineering	
Kansas Power and Light	Lawrence	5	400	11/71 6/78	N	Combustion Engineering	
Kansas City Power and Light	La Cygne	1	820	2/73	N	Babcock and Wilcox	
Arizona Public Service	Cholla	1	115	10/73	R	Research-Cottrell	
Northern States Power	Sherburne	1	710	3/76	N	Combustion Engineering	
Northern States Power	Sherburne	2	680	4/77	N	Combustion Engineering	
Springfield City Utilities	Southwest	1	200	4/77	N	Universal Oil Products	
Tennessee Valley Authority	Widows Creek	8	550	5/77	R	Tennessee Valley Authorit	
South Carolina Public Service	Winyah	2	140	7/77	N	Babcock and Wilcox	
Texas Utilities Company	Martin Lake	1	793	8/77	N	Research-Cottrel1	
Indianapolis Power and Light Company	Petersburg	3	530	12/77	N	Universal Oil Products	

La Cygne unit l (Kansas City Power and Light) has eight identical venturi-sieve tray modules for fly ash and SO₂ removal. The unit burns highash (15% to 25%), high-sulfur (5.3% to 6%) coal which is mined locally. An intensive development program has been conducted at the site; however, operating and maintenance problems remain.

Flooded disc scrubbers and packed-tower absorbers were retrofitted to the 115-MW boiler of Arizona Public Service's Cholla unit 1. The unit burns 0.5% sulfur coal. High on-stream time has been achieved, but extensive maintenance and operation efforts are required.

Sherburne station boilers Nos. 1 and 2 burn low-sulfur (0.8%) coal. Each unit has 12 scrubbing modules. Each module operates with a ventri-rod scrubber followed by a marble-bed absorber. Erosion and spray nozzle plugging have caused problems in these units. Northern States Power Company is planning two additional power units of 860 MW each at Sherburne with limestone slurry FGD included for each unit.

During startup, the FGD system at Southwest No. 1 (Springfield City Utilities) experienced mist eliminator scaling and some control problems. It is anticipated that scrubber system modifications will be made during a scheduled outage. The unit burns 3.5% sulfur coal.

Coal with 3.7% sulfur content is burned in TVA's Widows Creek Unit 8. The TVA-designed scrubbing system has four trains, each of which includes a variable-throat venturi followed by a grid-type absorber. Commercial scrubber operation began in late 1977.

The scrubbing unit on Winyah No. 2, a part of the South Carolina Public Service system, began initial operation in July 1977. Fuel for the unit is a 1% sulfur Virginia coal. Plans are underway to increase the size of the scrubber which now cleans 50% of the flue gas from Unit 2.

Texas lignite with 1% sulfur and 8% ash content is burned in the new Martin Lake Unit 1 boiler of Texas Utilities Company. Six packed/spray tower absorbers scrub 75% of the total flue gas with the remainder bypassed for reheat. Compliance testing began in late 1977.

Indianapolis Power and Light Company has installed TCA limestone scrubbers at their new Petersburg No. 3 unit. The unit burns 3.5% sulfur with ash content of 10%. Operation of the four modules began in December 1977.

In addition to the 11 operating limestone units listed, another 17,500 equivalent megawatts of limestone FGD units are under construction or planned (Laseke, et al., 1978; Kennedy and Tomlinson, 1978).

The process design data and operating conditions used in this study for the limestone slurry process are based primarily on the latest design and operating conditions at the TVA Shawnee test facilities and Widows Creek Hait 8.

GENERIC DOUBLE-ALKALI PROCESS

As in the limestone slurry system, double-alkali processes dispose of removed SO_2 as throwaway calcium sludge. Unlike limestone, however, absorption of SO_2 and production of disposable waste are separated—the addition of limestone or lime occurring outside the scrubber loop. The scrubbing step utilizes an aqueous solution of soluble alkali. The absorption reaction depends on gas/liquid chemical equilibrium and mass transfer rates of sulfur oxides $(\mathrm{SO}_{\mathbf{X}})$ from flue gas to scrubbing liquid instead of limestone dissolution, the limiting factor in limestone scrubbing. Therefore, $\mathrm{SO}_{\mathbf{X}}$ absorption efficiency in a double-alkali system is potentially higher than in a limestone system with the same physical dimensions and liquid-to-gas (L/G) flow rates (Kaplan, 1974). Scaling and plugging in the absorption area are reduced because calcium slurry is confined to the regeneration and disposal loop and soluble calcium is minimized in the scrubber liquor. The process has been described by Kaplan (1976) and LaMantia, et al. (1976, 1977).

Technically, the use of any combination of alkaline compounds, organic or inorganic, for $\rm SO_2$ removal and disposal can be classified as a double-alkali process. The process chosen for evaluation in this report is a sodium sulfite absorbent - lime reactant system.

Sodium sulfite in solution absorbs SO_2 in the scrubbing step represented by equation 11.

$$SO_3^- + SO_2 + H_2O \rightarrow HSO_3^-$$
 (11)

Sodium hydroxide formed in the regeneration step and sodium carbonate added as sodium makeup react with SO_2 as shown below. The absorption reactions actually involve reaction of SO_2 with an aqueous base such as sulfite, hydroxide, or carbonate rather than sodium ion which is present only to maintain electrical neutrality.

$$20H^{-} + SO_{2} \rightarrow SO_{3}^{=} + H_{2}O$$
 (12)

$$co_3^{=} + so_2 + so_3^{=} + co_2$$
 (13)

The use of lime for regeneration allows the system to be operated over a wider pH range which in turn includes the complete range of active alkalihydroxide/sulfite/bisulfite. Limestone regeneration operates only in the sulfite/bisulfite range.

$$Ca(OH)_2 + 2HSO_3^- + SO_3^= + CaSO_3 \cdot 1/2H_2O + 3/2H_2O$$
 (14)

$$Ca(OH)_2 + SO_3^{=} + 1/2H_2O \rightarrow 2OH^{-} + CaSO_3 \cdot 1/2H_2O$$
 (15)

$$Ca(OH)_2 + SO_4^{=} + 2OH^{-} + CaSO_4$$
 (16)

$$Ca(OH)_2 + SO_4^{=} + 2H_2O + 2OH^{-} + CaSO_4 \cdot 2H_2O$$
 (17)

Total oxidizable sulfur (TOS) is the total concentration of sulfite and bisulfite in solution. Oxidation of TOS to sulfate may occur in any part of the system and is affected by composition of the scrubbing liquor, oxygen content of the flue gas, impurities in the lime, and design of the equipment.

$$so_3^{=} + 1/20_2 \rightarrow so_4^{=}$$
 (18)

$$HSO_3^- + 1/2O_2 \rightarrow SO_4^- + H^+$$
 (19)

The sum of the concentrations of NaOH, Na $_2$ CO $_3$, NaHCO $_3$, Na $_2$ SO $_3$, and NaHSO $_3$ in the scrubbing solution is termed active alkali. The active alkali concentration in a system can be dilute or concentrated; a concentrated mode (active sodium concentration greater than 0.15 M) was chosen for this study. In this mode high sulfite levels prevent the precipitation of calcium sulfate (CaSO $_4$) as gypsum (CaSO $_4$ ·2H $_2$ O), equation 17. However, CaSO $_4$ is precipitated along with calcium sulfite (CaSO $_3$ ·1/2H $_2$ O) as shown in equations 14-16. In this way the system can keep up with sulfite oxidation at the rate of 25% to 30% of the SO $_2$ absorbed without becoming saturated with CaSO $_4$. Usually, soluble calcium levels are less than 100 ppm in the regenerated liquor of a concentrated mode double-alkali process.

Several U.S. and Japanese companies have developed double-alkali FGD processes. Unlike the Japanese processes which generally result in the production of gypsum, U.S. processes are of the waste-producing type, producing a calcium sludge that is primarily CaSO₃·1/2H₂O.

The first U.S. patent for a double-alkali system was awarded to FMC Corporation in October 1975. FGD investigation was started at FMC in 1956 with limestone and lime scrubbing (FMC, 1976; Legatski, 1976), but by the 1960's FMC was testing a sodium-based scrubbing process on a pilot-plant scale

The process produce sodium sulfite (Na₂SO₃) and sodium sulfate (Na₂SO₄) and when efforts to sell these products failed, FMC began a search to find a method of recovering the sodium values from the system while producing an acceptable solid waste for disposal. The resulting concentrated double-alkali process was demonstrated as an equivalent 30-MW prototype installed on a reduction kiln at FMC's Modesto (California) Chemical Plant in 1971. Since 1971 several installations have been constructed or are planned for industrial boilers of up to 150 MW equivalent size. Removal of SO₂ and unit availability have been 90% or greater. An FMC system, scrubbing flue gas from coal of 3.75% sulfur, is planned for the 250-MW A. B. Brown Unit No. 1, Southern Indiana Gas and Electric Company (Table 2).

TABLE 2. COMMERCIAL, DOUBLE-ALKALI FGD

SYSTEMS UNDER CONSTRUCTION AT U.S.

ELECTRIC POWER STATIONS

Power plant			FGD installation				
Utility	Station	Unit No.	FGD MW	FGD startup	New/ retrofit	Vendor	
Louisville Gas and Electric	Cane Run	6	277	2/79	R	Combustion Equipment Associates/Arthur D. Little	
Southern Indiana Gas and Electric	A. B. Brown	1	250	4/79	N	FMC Corporation	
Central Illinois Public Service	Newton	1	575	11/79	N	Buell/Envirotech	

Envirotech Corporation developed its Buell double-alkali SO₂ control process for both dilute and concentrated mode operation (Bloss, et al., 1976). A joint R&D effort with Utah Power and Light Company was undertaken at Gadsby station in Salt Lake City. The 1-MW pilot plant began testing in January 1972. Envirotech research has also focused on high-chloride coals and the acceptable disposal of chlorides in a throwaway system. At present Envirotech is constructing a 575-MW FGD system at Newton station unit 1, Central Illinois Public Service (Table 2). Unit 1 will burn coal containing 4% sulfur and 0.2% chloride.

In 1972 Arthur D. Little, Inc., (ADL) was awarded a \$1.1M EPA contract to develop double-alkali technology. In the ADL laboratory program, tests were conducted to develop process chemistry, to study regeneration of sodium scrubbing solutions, and to characterize double-alkali waste products (LaMantia, et al., 1976, 1977). ADL, in conjunction with Combustion Equipment Associates, Inc., (CEA), conducted pilot-plant work involving both concentrated and dilute modes of operation. A 20-MW prototype double-alkali system using lime in a concentrated mode was designed and developed by CEA and ADL for installation at Gulf Power Company's Scholz Steam Plant at Sneads Florida. The test program, a part of the EPA contract, ran from May 1975 to July 1976. CEA and ADL have been awarded an EPA contract for a full-scale double-alkali demonstration unit now under construction at Cane Run Unit 6, Louisville Gas and Electric Company (Van Ness, 1978). Coal sulfur content at Unit 6 is 3.5% to 4%. Although the entire cost of the installation, \$16.3M, is being borne by Louisville Gas and Electric, EPA will provide additional funding of \$4.5M to cover performance testing and a 1-year operational study. SO₂ removal efficiencies greater than 95% have been guaranteed (Table 2)

Other U.S. companies have developed double-alkali processes or have conducted experimental programs to study process feasibility. A dilute mode, limestone regeneration double-alkali system, developed by General Motors Corporation and installed at its Parma, Ohio, steam plant, was put into operation March 1974 (Interess, 1977). Under contract to EPA, ADL conducted a 2-year test program at the Parma site to study operating characteristics and waste byproduct properties of the system. The Zurn double-alkali process (Zurn Industries, Inc.) is in use at the Caterpillar Tractor Company plant in Joliet, Illinois (Lewis, 1976). The process is dilute mode, lime regeneration, and scrubs gas from two industrial boilers burning 4% sulfur coal. The CALSOX system, a Monsanto Enviro-Chem Systems, Inc., development (Barnard, et al., 1974), absorbs SO₂ in an aqueous solution of ethanolamine and regenerates scrubbing liquor with lime. Chemico and Bechtel have also conducted pilot-plant tests of double-alkali systems.

Double-alkali process chemistry was studied in the laboratories of EPA at Research Triangle Park, North Carolina (Draemel, 1972), in the early 1970's as a part of an EPA program which included work contracted to Radian Corporation and ADL. Radian designed a mathematical model of the double-alkali system which included certain chemical species not already considered in the laboratory. A bench-scale study was undertaken by ADL to find optimum equipment arrangement, to develop mass transfer coefficients, and to use process knowledge to develop economic information about the system.

Also in the early 1970's laboratory— and bench—scale studies of sodium and ammonia sorbents were conducted by TVA (TVA, 1973, 1974) using limestone or lime as regenerants. A pilot—plant study at TVA's Colbert Steam Plant was developed under EPA contract using an ammonia system; the study concluded in 1976 (Williamson and Puschaver, 1977).

The design of the generic double-alkali process evaluated in this study follows the development of U.S. double-alkali throwaway systems, using a concentrated mode with sodium sulfite absorbent and lime regenerant.

CITRATE PROCESS

The U.S. Bureau of Mines Metallurgy Research Center at Salt Lake City began FGD research in 1968 to find ways to control $\rm SO_2$ emissions from the nonferrous smelting industry. After a year of testing many possible organic and inorganic sorbing combinations, an aqueous solution of sodium citrate and citric acid was chosen for its chemical stability, low vapor pressure, high $\rm SO_2$ absorption, completeness of regeneration, and purity of the resulting sulfur (Rosenbaum, et al., 1971; McKinney, et al., 1974a). The chemistry of the citrate process was investigated in laboratory studies by the Bureau of Mines and by Pfizer, Inc. (Korosy, 1974). In the absorption stage $\rm SO_2$ dissolves in water, but the absorption is self limiting.

$$so_2 + H_2O \stackrel{?}{\leftarrow} Hso_3^- + H^+$$
 (20)

Hydrogen ions are removed and solubility increases by the buffering action of the various citrate species.

$$\operatorname{Cit}^{=} + \operatorname{H}^{+} \stackrel{\rightarrow}{\leftarrow} \operatorname{HCit}^{=} \tag{21}$$

$$HCit^{=} + H^{+} \stackrel{\rightarrow}{\leftarrow} H_{2}Cit^{-}$$
 (22)

$$H_2Cit^- + H^+ \stackrel{?}{\leftarrow} H_3Cit$$
 (23)

Some thiosulfate, formed in the regeneration step, will recycle with the absorbing solution and can form a complex with SO_2 .

$$H^{+} + HSO_{3}^{-} + S_{2}O_{3}^{-} + SO_{2} \cdot S_{2}O_{3}^{-} + H_{2}O$$
 (24)

Reaction between bisulfite and thiosulfate can result in the formation of trithionate.

$$4HSO_3^- + S_2O_3^= + 2H^+ \rightarrow 2S_3O_6^= + 3H_2O$$
 (25)

Although the complexing of absorbed SO_2 (equation 24) inhibits oxidation to sulfate, some oxidation will occur during absorption.

$$HSO_3^- + 1/2O_2 \rightarrow HSO_4^- \stackrel{?}{\leftarrow} H^+ + SO_4^=$$
 (26)

The reaction of hydrogen sulfite ($\rm H_2S$) and $\rm SO_2$ in aqueous solution during regeneration is complex and thiosulfate and other intermediates are formed. Reduction of these and the intermediates of equations 24 and 25 result in the following general equations.

$$SO_3^{=} + 2H_2S + 2H^{+} \rightarrow 3S + 3H_2O$$
 (27)

$$s_2 o_3^{=} + 2H_2 S + 2H^+ \rightarrow 4S + 3H_2 O$$
 (28)

Some decomposition of thiosulfate occurs during the sulfur-melting step at temperatures above $257^{\circ}F$ ($125^{\circ}C$). The overall reaction is

$$3S_2O_3^{=} + 2H^{+} + 2SO_4^{=} + 4S + H_2O$$
 (29)

Sulfate formed by equations 26 and 29 is purged from the system by the addition of alkali to neutralize the hydrogen ions which have also formed.

$$H^{+} + SO_{4}^{-} + Na_{2}CO_{3} \rightarrow 2Na^{+} + SO_{4}^{-} + H_{2}O + CO_{2}$$
 (30)

Natural gas and steam are reacted with a portion of the product sulfur to produce ${\rm H}_2{\rm S}$ for the regeneration step (equations 26 and 27).

$$CH_4 + 4S + 2H_2O \rightarrow 4H_2S + CO_2$$
 (31)

The initial Bureau of Mines process was designed to include the following steps: (1) gas cooling and cleaning, (2) SO₂ absorption in citrate solution, (3) reaction of absorbed SO₂ with $\rm H_2S$, (4) washing of precipitated sulfur, and (5) formation of $\rm H_2S$. Laboratory-scale tests in 1970 processed up to 15 ft³/min of gas containing 0.3% to 2.0% SO₂. In these tests the precipitated sulfur was not washed but was filtered and melted to separate the occluded citrate. $\rm H_2S$ preparation was not a part of these tests.

In November 1970, a pilot plant treating a maximum $400 \, \mathrm{ft^3/min}$ of reverberatory furnace gas was placed into operation jointly by the Bureau of Mines and Magma Copper Company, a subsidiary of Newmont Mining Corporation, at the San Manuel smelter in Arizona (McKinney, et al., 1974b; Rosenbaum, et al., 1973). Liquid H₂S was purchased for the SO₂ reduction process step. The operation of the pilot plant was frequently interrupted by mechanical failures; however, the Bureau of Mines concluded that (1) the process could remove 90% to 99% of the SO₂ from the smelter gas, (2) regeneration of the scrubbing liquor was easily managed, and (3) high-quality sulfur could be recovered by a combination of thickening, centrifuging, and melting.

In 1971 Pfizer, Inc., a chemical plant operator and manufacturer of citric acid, working with the Bureau of Mines built and operated laboratory units to study citrate process chemistry. Arthur G. McKee and Company and Peabody Engineered Systems joined Pfizer in 1972 in plans to demonstrate the commercial feasibility of the citrate process (Korosy, 1974). A 2,000 sft³/min pilot plant was constructed at Pfizer's Vigo plant site in Terre Haute, Indiana. The gas stream, from a coal-fired industrial boiler, averaged 1,000 ppm SO₂ at the inlet to the FGD system. Two major design changes incorporated in

this pilot plant were the impingement plate tower which replaced the packed tower of the Bureau of Mines system and sulfur separation which was accomplished by air rather than hydrocarbon flotation. Peabody at one time offered this system under the trade name Citrex process.

Further investigation by the Bureau of Mines continued in February 1974 at the Bunker Hill Company lead smelter, Kellogg, Idaho. A pilot plant, using a packed tower with polypropylene Intalox saddles and sized to treat 1,000 sft 3 /min of 0.5% SO₂ gas, was designed to be operated in three phases (McKinney, et al., 1974). In Phase I, a smeltering furnace gas containing 4% to 5% SO_2 was diluted with air to 0.5% SO_2 . Purchased liquid H_2S was used for reducing the SO₂ to sulfur. Phase II operation was similar to Phase I with the exception that a 76% to 78% H₂S gas produced onsite from product sulfur, natural gas, and steam was used as the reducing gas. In Phase III tail gas from the lead smelter sinter plant, containing 0.3% to 0.9% SO2, was used as feed. A gas cooling and cleaning plant was designed to recover the dust in the tail gas in a baghouse, cool the gas in a packed wet scrubber, and remove sulfuric acid (H₂SO₄) mist and trace particles in a wet electrostatic precipitator (ESP). The Bunker Hill citrate pilot plant operated through November 1975 for a total of 4,500 hours and produced about 50 net tons of high-quality sulfur.

With EPA, the Bureau of Mines initiated plans for a full-scale citrate process demonstration plant and in mid-1976 entered into a cost-sharing cooperative agreement with the St. Joe Minerals Corporation to provide the host site (Madenburg and Kurey, 1978). A citrate process demonstration plant has been constructed at St. Joe's 60-MW coal-burning G. F. Weaton electric generating station at Monaca, Pennsylvania. Morrison-Knudsen Company of Boise, Idaho, has built the plant under a turnkey design/build/operate contract. The retrofitted system will treat 156,000 sft³/min of flue gas and is scheduled to begin operation in the summer of 1979. At that time Radian will begin a 1-year emission testing and performance evaluation of the demonstration system.

The citrate process design data and operating criteria used in this study are based primarily on the Bureau of Mines process. Design differences in the citrate process demonstration plant at Weaton Station are cited in the Systems Estimated. Citrate Process section below.

DESIGN AND ECONOMIC PREMISES

To make the comparison of process evaluations as equitable as possible, it is essential to carefully define the design and economic premises used as a basis for the study calculations. TVA has been involved in establishing study criteria and preparing technical and economic evaluations of alternate FGD processes for EPA and others since 1967. A report published by TVA and EPA (McGlamery, et al., 1975) outlined in detail a set of premises developed by TVA for use in its evaluation studies. Recently these premises have been modified through discussions with EPA and others to reflect prevailing fuel characteristics, current design practice, and projected economic conditions.

DESIGN PREMISES

The updated values used in this study are considered to be representative of modern boiler units less than 10 years old for which FGD would be considered. The base case is a new 500-MW power unit with a heat rate of 9,000 Btu/kWh, burning 3.5% sulfur coal (dry basis). Criteria that establish efficiencies, production rates, and other process design characteristics that are common to FGD systems are also included.

Power Plant

Both coal- and oil-fired power units are considered in the power plant design premises; because of decreasing emphasis on oil as a fuel source of electricity, however, only one oil-fired case--an existing 500-MW unit--is evaluated. A midwestern location (Illinois, Indiana, Kentucky area) is assumed for the power units because of the concentration of power stations in that area and their proximity to major coal fields.

Fuels--

Although coals of low sulfur and ash contents and high heating values are the most desirable, availability, location, and price often result in the use of coals of lesser quality. To represent the wide range of coals currently being burned, sulfur contents of 2.0%, 3.5%, and 5.0% (dry basis) were chosen. The coal composition was altered from previous studies to reflect a lower heating value (HHV) of 10,500 Btu/lb (as fired) and a higher ash content of 16%. The as-fired coal composition and flow rate for the three sulfur levels are given in Table 3.

A No. 6 fuel oil with 2.5% sulfur and an ash content of 0.1% is assumed for the oil case variation (Table 4). A heating value of 144,000 Btu/gal is assumed.

TABLE 3. COAL COMPOSITIONS AND FLOW RATES AT VARYING SULFUR LEVELS

(500-MW new unit, 9,000 Btu/kWh heat rate,
10,500 Btu/lb higher heating value of coal)

		case ry basis)	2.0% S (d	ry basis)	5.0% S (dry basis)	
Coal	Wt %,	Lb/hr,	Wt %,	Lb/hr,	Wt %,	Lb/hr,
components	as fired	as fired	as fired	as fired	as fired	as fired
С	57.56	246,800	58.03	248,700	56.89	244,000
Н	4.14	17,700	4.17	17,900	4.09	17,500
N	1.29	5,500	1.30	5,600	1.27	5,400
0	7.00	30,000	7.81	33,500	6.40	27,400
S	3.12	13,400	1.80	7,700	4.46	19,100
C1	0.15	600	0.15	600	0.15	600
Ash	16.00	68,600	16.00	68,600	16.00	68,600
H ₂ O	10.74	46,000	10.74	46,000	10.74	46,000
Total	100.00	428,600	100.00	428,600	100.00	428,600

TABLE 4. FUEL ALTERNATIVE CASE
OIL COMPOSITION AND FLOW RATE

(500-MW existing unit, 9,200 Btu/kWh heat rate, 2.5% S)

Oil components Wt %, as fired Lb/hr C 83.66 204,100 H 11.46 28,000 N 0.63 1,500 O 1.25 3,000 S 2.50 6,100 Ash 0.10 200 Sediment 0.40 1,000 Total 100.00 243,900
H 11.46 28,000 N 0.63 1,500 0 1.25 3,000 S 2.50 6,100 Ash 0.10 200 Sediment 0.40 1,000
H 11.46 28,000 N 0.63 1,500 0 1.25 3,000 S 2.50 6,100 Ash 0.10 200 Sediment 0.40 1,000
N 0.63 1,500 0 1.25 3,000 S 2.50 6,100 Ash 0.10 200 Sediment 0.40 1,000
0 1.25 3,000 S 2.50 6,100 Ash 0.10 200 Sediment 0.40 1,000
S 2.50 6,100 Ash 0.10 200 Sediment 0.40 1,000
Ash 0.10 200 Sediment 0.40 1,000
Sediment 0.40 1,000

Total 100.00 243,900

Design--

The size of operating fossil-fueled power plants in the United States today ranges to 1300 MW. Of the new units scheduled for commercial service in 1977 through 1980, sizes for coal-fired boilers range from 80-1300 MW (Electrical World, 1977a). Although a considerable portion of the future generating capacity will be from power units 500 MW or larger, many older and smaller units, 200 MW or less, will continue operation in the years to come. Therefore, to determine the effect of power unit size on the economics of SO₂ removal, three unit sizes—200, 500, and 1,000 MW—are chosen for study.

Balanced-draft boiler design is assumed for a horizontal, pulverized coal, frontal-fired unit. A tangential-fired boiler is assumed for the oil-fired unit. ESP units designed to remove 99.5% of the particulate matter are assumed to be located ahead of the FGD system for coal-burning units. Fly ash emission from oil-fired units does not exceed the EPA particulate emission standard; therefore, these power plants do not require fly ash collection facilities.

A balanced-draft power unit without an SO₂ removal unit normally requires one induced-draft (ID) fan per duct, capable of overcoming a pressure drop of approximately 15 inches downstream of the boiler. In the design of new power plants with SO₂ removal facilities, it is assumed that the balanced-draft system includes the same capacity ID fan which will feed flue gas into a common plenum. Downstream from the plenum one forced-draft (FD) fan (relative to the SO₂ absorber) is provided per scrubbing train to overcome the additional pressure drop attributed to SO₂ removal. Since existing power units are already equipped with a 15-inch ID fan, retrofitted SO₂ removal facilities will follow the same design by adding one FD fan per scrubbing train downstream of the plenum.

In this evaluation 200-MW power units are assumed to have two economizers, air heaters, and exhaust ducts, while 500- and 1,000-MW units are assumed to be equipped with four of each.

Operation --

Based on power plant evaluation guidelines suggested by the Federal Energy Regulatory Commission (FERC) (formerly the Federal Power Commission) (FERC, 1968), the expected operating life of a new fossil-fueled power unit is about 30 years. Reflecting past TVA experience (Slack, et al., 1971), Table 5 shows the power plant operating schedule assumed for this study. This schedule represents a total on-stream time of 127,500 hours over the life of the plant. Existing 200-MW units are assumed to be 10 years old with a remaining life of 20 years or 57,500 operating hours; existing 500-and 1,000-MW units are assumed to be 5 years old with a remaining life of 25 years or 92,500 operating hours.

TABLE 5. ASSUMED POWER PLANT CAPACITY SCHEDULE

Operating year	Capacity fact or, %	Annual operating time, hr
1-10	80	7,000
11-15	57	5,000
16-20	40	3,500
21-30	17	1,500
Average for 30-yr life	48.5	4,250

Power plant efficiencies vary with size and status. FERC data (1973) list heat rates for approximate 500-MW power units up to 5 years old, ranging from 8,800 to 12,800 Btu/kWh. Representative heat rates chosen for use in this study are given in Table 6.

TABLE 6. POWER UNIT INPUT HEAT REQUIREMENTS

Size, MW	Status	Heat rate, Btu/kWh
1,000	New	8,700
1,000	Existing	9,000
500	New	9,000
500	Existing	9,200
200	New	9,200
200	Existing	9,500

Flue gas compositions vary with power unit design, fuel, and a variety of operating conditions. The following combustion and emission parameters for determining gas composition are based on FERC (1976) and EPA (1973) data for balanced-draft boiler design and average values for the sulfur content of coal. Not taken into consideration are variations in coal—sulfur in actual coal deliveries—which can result in levels as much as 22% greater than average values.

Coal-fired units--Flue gas compositions are based on combustion of pulverized coal and a total air rate to the air preheater equivalent to 133% of stoichiometric requirement. This includes 20% excess air to the boiler and 13% air inleakage at the air preheater. These values reflect operating experience with typical horizontal, frontal-fired, coal-burning units. It is assumed that 80% of the ash present in coal is emitted as fly ash and 95% of the sulfur in coal is emitted as $SO_{\mathbf{x}}$. One percent of the $SO_{\mathbf{x}}$ emitted is assumed to be sulfur trioxide (SO3), the remainder is $SO_{\mathbf{x}}$. Nitrogen oxides (NO $_{\mathbf{x}}$) emission is reported as nitric oxide (NO).

Oil-fired unit--A tangential-fired boiler is considered for the oil-fired units with flue gas composition estimated assuming a total air rate to the air preheater equivalent to 115% of the stoichiometric requirement. This includes 5% excess air to the boiler with an estimated 10% air inleakage at the preheater. It is also assumed that all of the ash and sulfur in the fuel oil is emitted as fly ash and SO_{X} . One percent of the SO_{X} emitted is assumed to be SO_{3} .

The flue gas compositions and flow rates calculated from these parameters are shown in Table 7. Calculated flue gas and equivalent SO_2 emission rates are listed in Table 8.

TABLE 7. ESTIMATED FLUE GAS COMPOSITIONS

FOR POWER UNITS WITHOUT EMISSION CONTROL FACILITIES

		_Fue1	and boil	er_type				
	Coal-fired boiler							
		(horizonta	Oil-fired boiler					
	f	rontal fir	(tangential fired)					
Flue gas components	Sulfur	content of	fuel, %	by wt (dry basis)				
(% by vol)	2.0	3.5	5.0	2.5				
37	70. 60	70 76	70.00	70.40				
N_2	73.68	73.76	73.80	73.60				
02		4.83		2.54				
CO ₂	12.44	12.31	12.20	11.96				
SO ₂	0.14	0.24	0.34	0.13				
S03	0.0014	0.0024	0.0034	0.0013				
NO _x (as NO)	0.06	0.06	0.06	0.02				
нс1	0.01	0.01	0.01	_				
н ₂ 0	8.84	8.79	8.75	11.75				
Fly Ash Loading								
gr/sft ³ (dry)	6.67	6.65	6.66	0.036				
gr/sft ³ (wet)	6.08	6.06	6.08	0.032				

TABLE 8. POWER PLANT FLUE GAS AND SO2 RATES

Power plant size, MW	Type plant	Sulfur content of fuel, % (dry basis)	Gas flow to FGD systems, aft ³ /min (300°F)	Equivalent SO ₂ emission rate to FGD systems, 1b SO ₂ /hr
Coal-fired units				
200	Existing	3.5	652,000	10,610
200	New	3.5	631,000	10,270
500	Existing	3.5	1,577,000	25,690
500	New	2.0	1,539,000	14,500
500 (base case)	New	3.5	1,543,000	25,130
500	New	5.0	1,539,000	35,920
1,000	Existing	3.5	3,085,000	50,250
1,000	New	3.5	2,982,000	48,580
Oil-fired unit			· •	•
500	Existing	2.5	1,313,000	12,060

FGD System

Scrubber SO₂ removal requirements, design and redundancy, bypass, reheat, and other FGD design considerations are as follows:

Emission Standards--

Current EPA Federal Standards of Performance for New Stationary Sources (often called new source performance standards—NSPS) which define the maximum emission levels for new power plants in the United States are shown in Table 9 (Federal Register, 1971). The design assumed for this report is based on meeting the standard for particulate matter and SO2 emission, rather than designing for a higher degree of removal. NSPS revisions, proposed in the Federal Register (1978), include a requirement of 85% SO2 removal (24-hour average) with maximum emissions of 1.2 1b SO2/MBtu.

TABLE 9. CURRENT EPA EMISSION STANDARDS FOR

NEW STEAM	1 GENERATING FACI	LITIES
		ission, lb/MBtu
	Coal-fired unit	Oil-fired unit
Particulate matter SO ₂	0.1 1.2	0.1

Degree of Removal--

Because required SO_2 removal efficiencies vary depending on fuel type and sulfur content, case variations will show a range of 63% to 85% removal required to meet existing NSPS. The required removal efficiencies for fly ash and SO_2 are given in Table 10 for the fuels and sulfur levels considered. For all fuels evaluated, designs provide for limiting SO_2 emission to 1.2 lb SO_2 /MBtu input (current NSPS). An additional case based on a 500-MW new coal-fired unit with 3.5% sulfur level has been prepared to show the effect of designing for 90% SO_2 removal.

TABLE 10. REQUIRED REMOVAL EFFICIENCIES

Sulfur content	Degree of	Degree		
of fuel, %	particle removal, wt %	SO2 removal, %		
Coal-fired units				
2.0	99.5	62.7		
3.5	99.5	78.5		
5.0	99.5	85.0		
Oil-fired units				
2.5	-	69.8		

SO₂ Scrubber--

Scrubbing system design assumes that technology used in each process is proven, has been demonstrated, and is not first-of-a-kind. No special redundancy provisions are assumed necessary for utility boiler - SO₂ scrubber system reliability.

Several methods are available to provide turndown capabilities of the control systems resulting from changes in power supply requirements including:

- 1. Multiple-scrubbing trains
- 2. Variable-flow control to individual scrubbers
- 3. Compartmentalized scrubbers
- 4. Individual scrubber bypasses
- 5. Connecting plenum ducts between trains

For this study, ESP ducts are assumed to exhaust to a common plenum connecting the scrubbing trains. Separate ducts from the plenum to each scrubbing train are equipped with dampers for individual scrubber shutoff for maintenance or power plant turndown. Because of the reliability implied in the assumption that these processes are based on proven technology, other special design provisions for individual scrubber shutdown are not provided. Bypass ducts for maintaining full power generation capacity during shutdown of one or more scrubbing trains are not provided.

The scrubber type for each process is:

Process	Scrubber type				
Limestone	Mobile bed				
Double alkali	Perforated plate tower				
Citrate	Packed tower				

Each scrubber system is designed with a presaturator for cooling and humidifying the flue gas. Absorption of flue gas components in the presaturator is assumed as follows:

Component	% removal
so ₂	5
so ₂ so ₃	50
нcí	100
$NO_{\mathbf{x}}$	0

In the limestone and double-alkali processes these compounds are disposed of in the waste stream along with the additional SO_2 removed in the absorption tower. In the citrate process the excess liquor from the presaturator drains into the bottom of the SO_2 absorber and is recycled to the presaturator for humidification and cooling of the flue gas. A liquor purge stream is pumped to a neutralization tank to which lime is added to control chloride contamination of the system. An SO_2 stripper is placed upstream from the neutralization

tank to remove SO_2 from the purge stream and return it to the flue gas stream to allow as much sulfur as possible to be reclaimed from the system.

Each ${\rm SO}_2$ scrubber is equipped with a chevron-type entrainment separator at the scrubber outlet. The use of an entrainment separator or mist eliminator in the scrubber is desirable for the following purposes.

- 1. To reduce the heat load on the stack gas reheater.
- 2. To decrease the deposition of liquid and entrained solids in ducts and equipment located downstream from the scrubber.
- 3. To reduce the amount of entrained solids emitted to the atmosphere.

The exit gas from the SO_2 absorber is assumed to contain water entrainment equivalent to 0.1% by weight of the wet gas mass rate.

Specific design conditions for SO₂ removal will vary from installation to installation corresponding to expected fluctuations in the fuel analysis and to differences in operating requirements. The operating conditions chosen for each base case scrubbing system in this study are presented in Table 11.

TABLE 11. ASSUMED OPERATING CONDITIONS FOR SCRUBBING

SYSTEMS APPLIED TO NEW COAL-FIRED POWER UNITS

[500-MW units, 3.5% S in coal (dry basis), 1.2 1b SO₂/MBtu heat input allowable emission]

	Process				
		Generic			
Operating conditions	Limestone	double alkali	Citrate		
Stoichiometry	1.32	1.0	_		
Design gas velocity, ft/sec	12.5	7.0	10.0		
SO ₂ scrubber L/G, gal/kft ³	12.5	7.0	10.0		
Presaturator	4	4	4		
SO ₂ scrubber, recycle liquor	50	4	_		
SO ₂ scrubber, regenerated liquor	-	3	5		
Design pressure drop, inches H ₂ O	8	3	15		
Oxidation of removed SO ₂ to SO ₄ =, %	20	10	2		

Reheat --

The need for stack gas reheat for corrosion reduction and plume buoyancy after aqueous scrubbing is recognized in the contemporary designs. Indirect steam reheat of the cleaned gas to $175^{\circ}F$ is provided for all case variations except the oil-fired case. For the existing oil-fired power unit, direct stack gas reheat to $175^{\circ}F$ is provided by mixing the combustion byproducts of an oil-fired reheater directly with the scrubbed gas.

Raw Materials--

Listed below are the raw materials that are used in the three desulfurization processes, with typical characteristics given for each.

1. Limestone

Purchase size $-0 \times 1/2$ inch Analysis -90% CaCO₃, 0.15% MgO, 4.85% inerts, 5% H₂O Limestone ground as 60% solids slurry Ground size -70% minus 200 mesh Bulk density -95 1b/ft³

2. Lime

Analysis - 95% CaO, 1% SiO₂, 2% MgO, 2% H₂O Size - 3/4 to 1-1/4 inch Bulk density - 55 1b/ft³

3. Sodium carbonate

Analysis - 99.8% $\rm Na_2CO_3$ (58.36% $\rm Na_2O$), 0.15% $\rm NaC1$, 0.02% inerts, 0.03% $\rm H_2O$ Bulk density - 35.5 $\rm 1b/ft^3$

4. Citric acid

Analysis - 99.5% to 100% purity Bulk density - 55 $1b/ft^3$

Solids Disposal--

One important design consideration for the limestone and double-alkali processes is the method for waste solids disposal. Two alternatives are investigated in this study.

- 1. Onsite pond disposal—The base case for the disposal of untreated limestone sludge is direct ponding of spent slurry from the scrubber in a clay—lined pond. The slurry is pumped to the pond at a solid concentration of 15%. In the double—alkali base case, a filter cake of calcium waste solids is reslurried to 15% solids and pumped to a clay—lined pond. The following assumptions are made for the pond.
 - a. The pond is one mile from the scrubber system site and is located on flat land.
 - b. The pond life is the same as power plant remaining life defined earlier in the power plant design premises.

- c. The pond is sized and costed for the disposal of calcium wastes only. Fly ash disposal is not considered. Pond is designed to minimize total pond construction cost including cost of land by optimizing pond depth and excavation.
- d. Pond is lined with 12 inches of impervious clay.
- e. Settled sludge contains 40% by wt solids and 60% free water.
- f. Closed-loop water cycle is maintained by returning excess pond water to the scrubber system.
- g. Pond evaporation and seepage equals rainfall.
- 2. Trucking alternative—A special case is evaluated for the limestone and double—alkali processes in which the calcium solids are trucked to the disposal site. Each process is designed with a slurry dewatering system to produce a disposal cake containing 55% solids. Charges for land preparation by scraping are included. No stabilization is assumed; disposal cake is piled to a height of 30 feet. Further discussion of this alternative appears in the Systems Estimated section.

The disposal methods are those currently used. More stringent regulations for control of runoff pollution from solid wastes may be effected in the future and could affect some aspects of disposal area design and site maintenance. Although beyond the time frame projected in this report, such regulations could be an economic factor in waste disposal considerations.

ECONOMIC PREMISES

Economic evaluations of the three processes are divided into capital investment and revenue requirements. Criteria are assumed that define cost indexes; land, raw material, and utilities costs; capital charges; and other factors required for comparative estimates.

Capital Investment

Capital investment estimates represent projects beginning mid-1977 and ending mid-1980, with an average cost basis for scaling of mid-1979. Other project estimates may be scaled from mid-1979 to the midpoint of project expenditures. System design is assumed to require 6 to 12 months and construction 24 months. The overall project is assumed to be completed over a 30- to 36-month project schedule.

Estimates are based on cost information obtained from engineering-contracting, processing, and equipment companies; TVA equipment purchases and construction data; and authoritative publications on estimating and costs, such as Bauman (1964), Guthrie (1969), Peters and Timmerhaus (1968), Popper (1970), The Chemical Engineer's Handbook (Perry and Chilton, 1973), and The Richardson Rapid System (1978). Costs are projected (Table 12) for 1979 from historical annual Chemical Engineering (1974, 1975, 1976) cost indexes and published projections (Thorsen, 1972).

The battery limits of the SO₂ removal facility estimates began with the common plenum downstream of the ESP and include the stack gas reheaters downstream of the absorbers. The stack plenum is considered necessary to a power unit without SO₂ removal and is not included in the FGD cost. Costs for booster fans and ductwork required to circulate flue gas through the FGD system are included. Fly ash removal by ESP and fly ash disposal are considered power plant functions and are not included in investment or revenue requirement estimates. The ID fans located between the ESP and the first plenum are considered a part of the boiler unit and their cost is not included in the FGD evaluation. Neutralization of the chlorides purged from the flue gas in the citrate system presaturator is included in the FGD cost.

Other special provisions and assumptions used in the preparation of investment estimates are:

- Spare pumps are provided to prevent operational shutdowns due to pump failure. For the limestone slurry and generic double-alkali processes, a spare pipeline is included for transport of sludge to the disposal area. No other spare equipment is included.
- 2. Process water utilization is based on closed-loop operation.
- 3. Indirect steam reheat of stack gases is assumed in all cases except for the existing oil-fired unit which utilizes direct oil-fired reheat.
- 4. Costs for the supplemental generation facilities for electricity used by the FGD system are not included in the capital investment. Compensation for derating of the boiler caused by FGD system electrical usage is added to the cost of electricity in the revenue requirement estimates.
- 5. Equipment, material, and construction-labor shortages with accompanying overtime pay incentive are not considered.

Direct Investment--

A detailed equipment list is prepared for the base case estimate which itemizes cost for materials and installation labor for each equipment item. In addition the cost of piping, insulation, ductwork, concrete foundations, excavation, structures, electrical, instrumentation, painting, and buildings required for each unit area are itemized.

TABLE 12. COST INDEXES AND PROJECTIONS

Year	1972	1973	1974	1975	1976 ^a	1977 ^a	1978 ^a	1979 ^a	1980 ^a	1981 ^a
Plant ,	137.2	144.1	165.4	182.4	197.9	214.7	232.9	251.5	271.6	293.3
Plant Material ^b	135.4	141.9	171.2	194.7	210.3	227.1	245.3	264.9	286.1	309.0
Labor ^C	152.2	157.9	163.3	168.6	183.8	200.3	218.3	237.9	259.3	282.6

a. Projections. Although actual cost indexes are available for 1976-1978, TVA continues to use its projections for these years so that consistency with past estimates is maintained.

b. Same as index in Chemical Engineering for "equipment, machinery, supports."

c. Same as index in Chemical Engineering for "construction labor."

Services, utilities, and miscellaneous costs are calculated as 6% of direct investment minus pond construction costs. This is assumed to include such items as maintenance shops, stores, communications, security, and offices. Also included are costs for parking lots, walkways, landscaping, fencing, vehicles, and I mile of paved roads. Necessary electrical, fuel oil, steam, process water, fire and service water, and compressed air distribution facilities and instrument air generation facilities are also a part of this cost.

Indirect Investment--

In addition to direct costs which include equipment, installation, services and utilities, and pond construction, the indirect costs covering engineering design and supervision, architect and engineering contractor expenses, construction expense, contractor fees, and contingency are estimated for each project. The engineering design and supervision and contingency factors are based on proven design, not first-of-a-kind installation.

Engineering design and supervision (ED&S)—A technique that correlates the number of major equipment items with drafting room man-hour and engineering design costs is used to estimate this indirect investment factor. Battery-limit areas are included as a varying percentage of area cost. The percentage used is determined by commercial status and design reliability of the purchased unit. The formula used is:

Engineering design and supervision = (8900) (1.294) (number of major equipment pieces) + (5-25%) (battery-limit investment)

A separate procedure, based on pond construction expense, was developed to determine ED&S cost for the pond area.

Pond engineering design and supervision = (0.076) (a) $^{0.67}$ where (a) = direct pond investment in M\$

The sum of these costs appears in the indirect investment display as ED&S for each process case variation.

Architect and engineering contractor expenses (A&E)--This factor is derived from the costs of engineering design and supervision. Twenty-five percent of the portion of ED&S associated with major equipment and battery-limit units is assumed for A&E. For cases involving disposal ponds, 10% of the ED&S associated with pond construction is estimated as additional A&E expense.

<u>Construction expense</u>—Construction expense is estimated based on direct investment by the following equation:

Construction expense = $0.25 (b)^{0.83} + 0.13 (c)^{0.83}$

where b = direct investment in M\$ excluding pond investment costs

c = direct pond cost in M\$

Contractor fees--A correlation between contractor fees and direct investment is used to estimate the cost of contractor fees.

Contractor fees = 0.096 (d)^{0.76}

where d = total direct investment in M\$

Contingency--Contingency is assumed to be 20% of the sum of direct investment, engineering design and supervision costs, architect and engineering contractor expenses, construction expense, and contractor fees.

Other Capital Charges--

Total fixed investment is defined as the sum of the investment costs by area--services, utilities, and miscellaneous; pond construction; indirect investments; and contingency. Allowance for startup and modification is estimated to be 10% of the total fixed investment excluding pond construction.

Interest during construction is estimated to be 12% of the total fixed investment. This percentage is calculated as the simple interest which would be accumulated at a 10% per year rate assuming an incremental capital structure of 60% debt to 40% equity and a 3-year project expenditure schedule as shown in Table 13.

TABLE 13. PROJECT EXPENDITURE SCHEDULE

		Year		
	1	2	3	Total
Fraction of total expenditure as borrowed funds Simple interest as 10%/yr as % of total expenditure	0.15	0.30	0.15	0.60
Year 1 debt Year 2 debt Year 3 debt	1.5 - -	1.5 3.0 —	1.5 3.0 1.5	4.5 6.0 1.5
Accumulated interest as % of total expenditure	1.5	4.5	6.0	12.0

Land--

Total land requirements including disposal pond area are assumed purchased at the beginning of the project. Cost of land is estimated at \$3,500 per acre.

Working Capital --

Working capital consists of (1) money invested in raw materials, supplies and finished products carried in stock, and semifinished products in the process of being manufactured, (2) accounts receivable, (3) cash retained for payment of operating expenses, such as salaries, wages, and

raw material puschases, (4) accounts payable, and (5) taxes payable. For these premises, working capital is defined as the equivalent of 3 weeks of raw material costs, 7 weeks of direct costs, and 7 weeks of overhead costs.

Case Variations--

Each area of the base case direct investment is analyzed and adjusted as necessary to reflect required modifications in process design for the case variations. For example, indirect steam reheat investment costs are replaced with direct oil-fired reheat investment costs for the existing oil-fired unit. In the citrate process, the chloride purge is eliminated for the existing oil-fired case. Modifications are made in the amount of ductwork provided for all existing units.

The adjusted area investment subtotal is scaled exponentially according to the relative throughput, using a weighted average scaling exponent calculated from the base case investment breakdown. Flue gas processing areas are scaled on the basis of relative gas throughput; byproduct processing areas are scaled on the basis of relative sulfur throughput. Table 14 shows the relative quantities of gas and sulfur which must be processed for each of the case variations in comparison with the base case quantities. The direct, indirect, fixed, and total capital investments are then determined by the same procedure described for the base case investment.

-Revenue Requirements

Annual Revenue Requirements--

Average annual revenue requirements for each case variation are calculated under regulated economics assuming 7,000 hours of operation per year. Process operation schedules are assumed to be the same as the power plant operating profiles and remaining life assumptions given in the power plant design premises. Operating costs for removal and disposal of fly ash are not included.

Direct Costs--

Raw materials, operating labor and supervision, utilities, maintenance costs, and analyses have been projected to 1980 dollars to reflect a mid-1980 scrubbing unit startup. The projected unit costs for raw materials, labor, and utilities are shown in Table 15. All tonnages are expressed in short tons. Raw material costs are the delivered costs to a Chicago power plant location; labor costs are rates for the midwestern area (Illinois, Indiana, Kentucky). Unit costs for steam and electricity generated by the power plant are based on acutal production cost including labor, fuel, depreciation, rate base return on investment, and taxes.

TABLE 14. RELATIVE QUANTITIES OF GAS AND SULFUR TO BE PROCESSED IN COMPARISON WITH THE BASE CASE QUANTITIES

	Relative	throughput rate, %
	Gas	
Coal-Fired Power Unit		
1.2 lb SO2/MBtu heat input		
allowable emission		
200 MW E 3.5% sulfur	42.22	42.22
200 MW N 3.5% sulfur	40.89	40.89
500 MW E 3.5% sulfur	102.22	102.22
500 MW N 2.0% sulfur	100.00	46.01
500 MW N 3.5% sulfur	100.00	100.00
500 MW N 5.0% sulfur	100.00	153.81
1,000 MW E 3.5% sulfur	200.00	200.00
1,000 MW N 3.5% sulfur	193.33	193.33
Solids disposal by trucking		
500 MW N 3.5% sulfur	100.00	100.00
90% SO ₂ removal		
500 MW N 3.5% sulfur	100.00	113.92
Oil-Fired Power Unit		
0.8 lb SO ₂ /MBtu heat input		
allowable emission		
500 MW E 2.5% sulfur	84.70	44.08

TABLE 15. PROJECTED 1980 UNIT COSTS
FOR RAW MATERIALS, LABOR, AND UTILITIES

			\$/unit
Raw Materials			
Limestone Lime Soda ash Citric acid Natural gas Catalyst			7.00/ton 42.00/ton 90.00/ton 1,340.00/ton 3.50/kft ³
Labor			
Operating labor Analyses Trucking landfill			12.50/man-hr 17.00/man-hr 17.00/man-hr
Utilities			
Fuel oil (No. 6) Steam (500 psig) Process water (citrate) Process water ^b			0.40/gal 2.00/MBtu 0.06/kgal 0.12/kgal
	200 MW	500 MW	1,000 MW
Electricity	0.031/kWh	0.029/kWh	0.028/kWh

a. Unit costs supplied by C&I Girdler.

Quantities of raw materials and utilities required by each process, except for electricity, are derived from the base case material balance. Electricity requirements are compiled from motor horsepower and equivalent kilowatt usage as defined in the base case equipment description. The amount of equipment in each process area and the difficulty of operation are considered in estimating the hours of operating labor and supervision for each process. Labor estimates for laboratory analysis are based on the quantities of materials which must be analyzed to maintain quality control.

b. Varies according to water volume requirements which are process dependent.

Maintenance costs are estimated on the basis of direct investment and are varied for each process as a function of unit size to reflect economy of scale. Maintenance percentages are also varied for each process according to projected relative process complexity and historical experience, when available. Table 16 shows the estimated overall annual maintenance factors which are applied to the total direct investment, minus pond construction costs, for each process, corresponding to an annual operating schedule of 7,000 hours. Pond maintenance for the limestone and double-alkali processes is estimated as 3% of the pond construction cost.

TABLE 16. ESTIMATED OVERALL ANNUAL MAINTENANCE COSTS

		direct inv	vestment astruction
Process	200 MW	500 MW	1,000 MW
Limestone	9	8	7
Double alkali	5	4	3
Citrate	7	6	5

a. Pond maintenance is estimated as 3% of pond construction cost.

Indirect Costs--

In estimating revenue requirements for FGD systems, the method chosen for financing the system--regulated power industry practice, nonregulated chemical industry practice, or a combination of the two--has a major effect on capital charge items such as depreciation and taxes. This study is based on regulated utility economics. The capital charges included in the indirect revenue requirement costs are applied as average charges which include depreciation, interim replacements, insurance, cost of capital, and taxes. These charges vary with remaining life of the power plant. A breakdown of the capital charges is given in Table 17. The depreciation rate is straight line, based on the remaining life of the power plant after the FGD system is installed.

In estimating the regulated capital charges associated with stack gas scrubbing, the conventional method of considering the overall life of the power plant is used. FERC (1968, 1969) recognized the conclusion of the National Power Survey that a 30-year service life is reasonable for steam-electric plants. Because some equipment items have life spans less than 30 years, however, an allowance factor, designated interim replacements, is included. Use of this allowance, following FERC recommended practice, provides for financing the cost of replacing short-lived units. Although an average allowance of about 0.35% of the total investment is normally provided, a somewhat larger allowance factor is used for new units in this study to account for the unknown life span of FGD facilities. An insurance allowance is also included in the capital charges. Property taxes, the fourth item of the capital charge rate applied to the original investment, are estimated at 1.5% of the total depreciable capital investment.

TABLE 17. ANNUAL CAPITAL CHARGES FOR POWER INDUSTRY FINANCING

	Percentage of		
	<u>capital</u>	inves	tment
Years remaining life	30	25	20
Depreciation (straight line, based on			
years remaining life of power unit)	3.3	4.0	5.0
Interim replacements (equipment having			
less than 30-year life)	0.7	0.4	_
Insurance	0.5	0.5	0.5
Property taxes		1.5	
11000000			
Total rate applied to original			
investment	6.0	6.4	7.0
	Percentage capital		
	capical	THVCS	<u> </u>
Cost of capital (capital structure assume to be 60% debt and 40% equity)	d		
Bonds at 10% interest		6.0	
Equity ^b at 14% return to stockholder		5.6	
Income taxes (Federal and State) ^C		5.6	
		-	
Total rate applied to depreciation b		17.2 ^d	

a. Original investment yet to be recovered or "written off."

Debt to equity ratio is another component of capital charges for which variations of ratios may be expected. FERC data (1972, 1974) indicate that the long-term debt for privately owned electric utilities varied only slightly from 51.5% to 54.8% of total capitalization during the period 1965-1973. Recent economic trends have affected the incremental debt to equity ratio, however, as utilities are forced to depend more and more on bonds and bank loans for project funding. The capital structure for this study is assumed to be 60% debt and 40% equity, with the interest rate for bonds assumed to be 10% and the return to stockholders 14%. Federal and State income taxes are assumed to have the same effect on capital cost as return on equity (5.6%).

b. Contains retained earnings and dividends.

c. Federal and State income taxes are assumed to have the same impact on capital cost as return on equity.

d. Applied on an average basis, the total annual percentage of original fixed investment for new (30-yr) plants would be 6.0% + 1/2(17.2%) = 14.6%.

The procedure for calculating plant, administrative, and marketing overheads can vary from company to company. Based on several cost estimating sources used in this study, the following methods are used to estimate overheads.

- 1. Plant overhead is estimated as 50% of the total conversion costs less utilities. This method has been selected to avoid overcharging processes which are energy intensive.
- 2. Administrative overhead is estimated as 10% of the operating labor and supervision cost.
- 3. Marketing of FGD byproducts is defined as sales to a distributor, shipping costs excluded, and marketing overheads are estimated on the basis of the relative difficulty in marketing the various products of the processes studied. For the citrate process, marketing overhead is estimated as 10% of the revenue collected from the sale of sulfur.

The citrate process is the only system evaluated in this study that produces a salable byproduct. In the calculation of citrate annual and lifetime economics, credit from the sale of sulfur (\$40 per short ton) is deducted from the yearly projection of revenue requirement to give the net effect of the FGD process on the cost of power.

Case Variations--

Raw materials and utilities for the case variations are scaled from the requirements indicated on the detailed base case revenue requirement summary. Utilities such as reheat energy and fan electricity are scaled proportionatel to the relative gas rate for each case variation; raw materials and utilities such as absorbent and electricity for the sulfur processing areas are scaled proportionately to the relative sulfur rate for the various cases. Annual costs for raw materials and utilities are then calculated by applying the unit costs to the scaled annual usage rates.

Lifetime Revenue Requirements--

Because of the typical declining load of most power units over their life, lifetime revenue requirements are better measures of the overall procest costs than are annual revenue requirements. Since annual revenue requirement vary each year as the rate base declines because of depreciation writeoff and with any changes in on-stream time of the power unit, it is desirable to have a year-to-year tabulation of annual and cumulative lifetime revenue requirements for any given case. For a comparison that recognizes the time value of money, the declining annual revenue requirements for each process over the life of the plant should be discounted at the cost of money (11.6% for this study) to the initial year of operation. The total of these costs can be compared directly or can be converted to equivalent unit costs for comparison with the premium expected for low-sulfur fuels.

For each of the case variations of the three processes, lifetime costs are projected corresponding to the declining operating profile established (Table 5). Year-by-year revenue requirements included in the lifetime projections are calculated by computer in the same manner as annual revenue requirements, with the exception that capital charges are based on the declining undepreciated investment. Since the regulated return on investment profitability is included in the year-by-year projections of revenue requirements, any revenue received from sale of byproducts can be applied toward reducing these yearly costs.

SYSTEMS ESTIMATED

Process description, material balance, flow diagram, layout drawings, and equipment requirements have been prepared for each of the three processe evaluated. Each process is divided into major functional areas to facilitat comparisons of investment and revenue requirements for similar processing steps. Equipment lists follow the area-by-area pattern with material costs presented in 1979 dollars for each item. The additional items of cost in each area are piping and transport lines, ductwork, concrete foundations, excavation and site preparation, structure, electrical wiring, instrumentation, buildings, and pond construction.

LIMESTONE SLURRY PROCESS

The limestone slurry process for desulfurization of flue gas (Figure 1) assumes fly ash removal by ESP. A common plenum is placed downstream from the ESP and the power plant ID fans to distribute the gas to the absorbers. Booster fans are placed between the plenum and the absorber to overcome the pressure drop created by the FGD system (Figure 2).

Incoming 0 x 1-1/2 inches limestone is received either by truck or rail and conveyed to a 30-day storage pile located about 150 feet from the grinding facilities (Figure 3). The limestone is reduced to about 0 x 3/4 inches using gyratory crushers, wet-ground to 70% minus 200 mesh in two parallel ball mills, and stored as a 60% solids slurry in a feed tank with 8-hour storage capacity. The slurry feed tank is located near the absorber system (Figure 4) about 1500 ft from the limestone preparation area.

Makeup limestone slurry is combined with scrubber effluent slurry and recycle pond water in the absorber hold tank to control the concentration of the recirculating slurry at approximately 15% solids. Flue gas is cooled in a presaturator with recycle slurry and fed to the mobile-bed absorbers. Limestone slurry circulates through the absorbers where it reacts with the SO₂ in the cooled flue gas. The absorbers are equipped with chevron-type entrainment separators with provisions for upstream and downstream wash with fresh makeup water to control entrainment carryover in the gas stream. Scrubber outlet gas is reheated to 175°F by indirect steam heat before entering the stack.

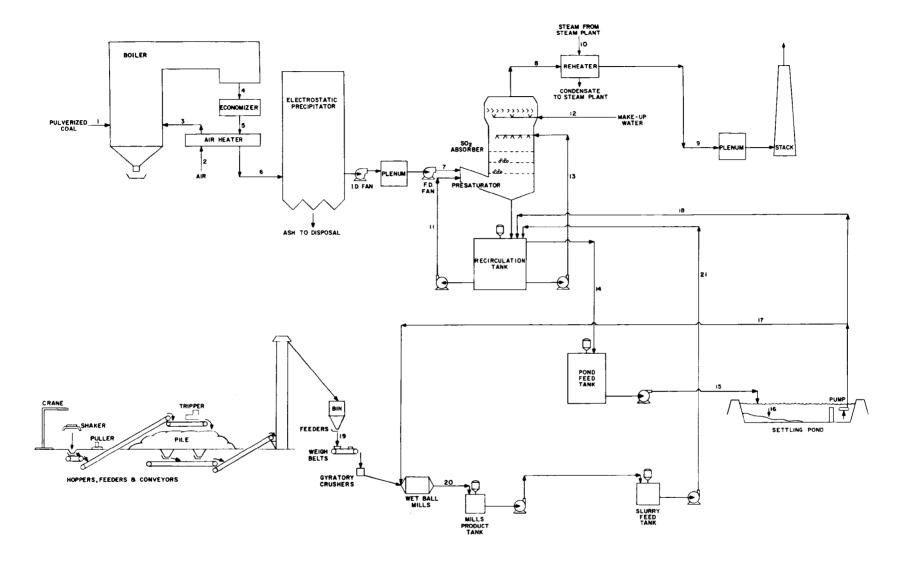


Figure 1. Limestone slurry process. Base case flow diagram.

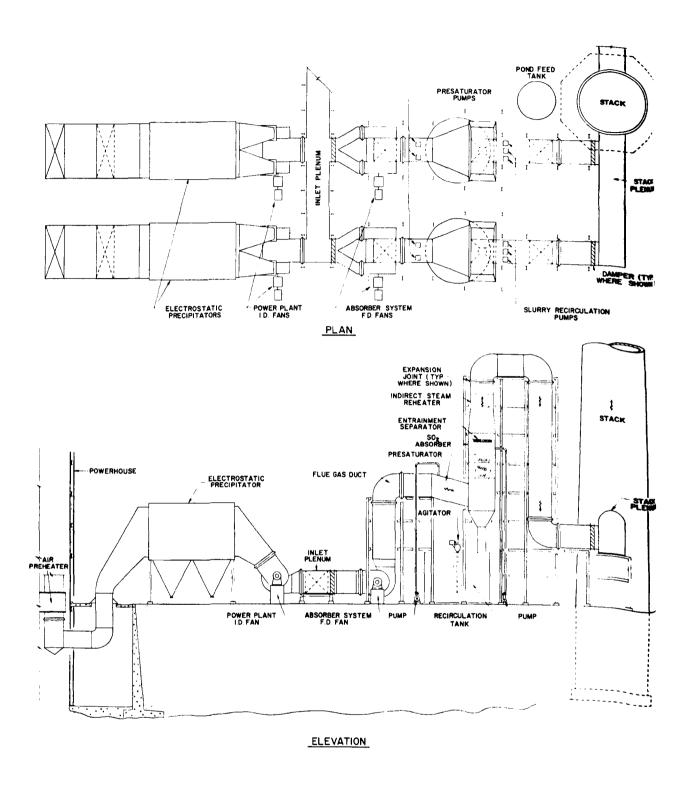


Figure 2. Limestone slurry process. Mobile-bed scrubber system base case plan and elevation.

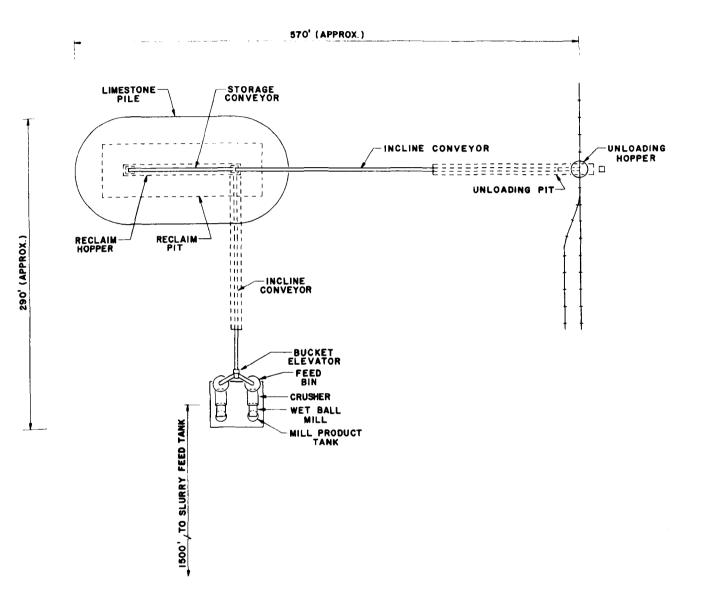


Figure 3. Limestone slurry process. Base case materials handling and feed preparation system layout.

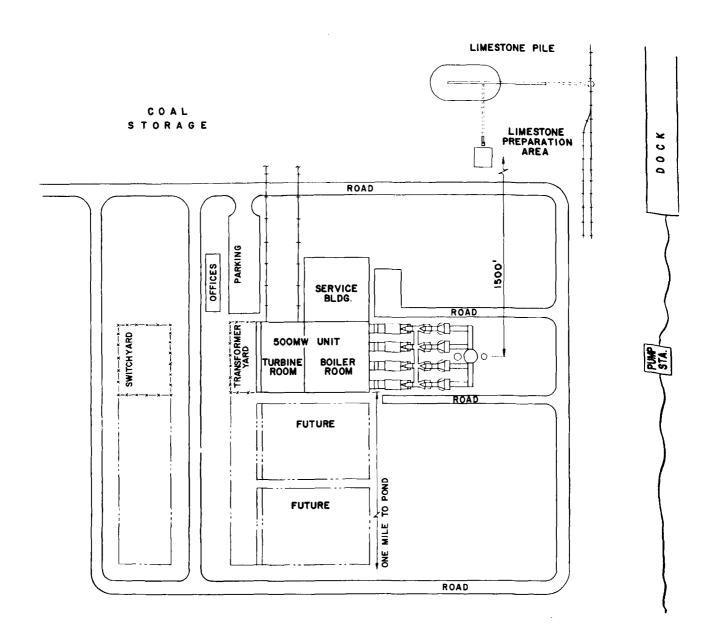


Figure 4. Limestone slurry process. Base case overall plot plan.

A bleedstream from the recirculation tank is fed to the pond feed tank and the spent slurry is pumped to the onsite pond where the solids in the slurry settle to form a sludge containing approximately 40% solids. Pond supernate is recycled to the wet ball mills and the absorber effluent hold tank to maintain closed-loop operation. A special case is evaluated in which the spent slurry is pumped to a slurry dewatering system to produce a disposal cake containing 60% solids; the cake is trucked to a disposal site located 1 mile from the scrubbing facilities. Slurry dewatering includes thickener and rotary drum filters. Overflow from the thickener is recycled to the wet ball mills and to the absorber recirculation tanks.

A material balance for the base case limestone slurry scrubbing process is shown in Table 18 and a detailed equipment list by area for the system is presented in Table 19.

Major Process Areas

The limestone slurry process is divided into the following operating areas.

- 1. <u>Materials handling</u>. Facilities for receiving raw limestone, a storage stockpile, and in-process limestone storage are included in this area.
- 2. Feed preparation. This area includes the equipment for converting raw limestone to a 70% minus 200 mesh, 60% solids slurry for feed to the scrubbers.
- 3. Gas handling. Included in this area is one inlet flue gas plenum interconnecting each of the four flue gas ducts which feed the absorbers and four FD fans which overcome the pressure drop in the FGD systems.
- 4. $\underline{\text{SO}_2}$ absorption. Four mobile-bed absorbers with presaturators, recirculation tanks, and pumps are included.
- 5. Stack gas reheat. Equipment in this area includes indirect steam reheaters and soot blowers for the coal variations. The oil-fired unit is designed with one direct oil-fired reheater per duct which discharges hot combustion gases directly into the duct.
- 6. <u>Solids disposal</u>. Equipment in this area consists of one pond feed tank with agitator and pond feed and pond return pumps.

Storage Capacity

Storage requirements for raw materials and allowances for in-process streams are listed below.

Raw materials:

Limestone storage - 30 days stockpile

In-process storage:

Crusher feed bin - 8 hours
Mills product tank - 20 minutes
Slurry feed tank - 8 hours
Pond feed tank - 15 minutes
Recirculation tanks - 10 minutes each (includes sufficient surge capacity for shutdown of scrubbers)

Solids Disposal

In the case variations which dispose of FGD waste solids by ponding, spent slurry containing 15% solids is pumped from an agitated pond feed tank to a disposal pond located 1 mile from the scrubbing facilities where the calcium salts settle to a sludge containing 40% solids. For the base case (500-MW, new, 3.5% sulfur, coal-fired unit), the field line transporting slurry to the pond is a 12-inch rubber-lined, carbon steel pipe. A spare field line to the pond is included and both lines are trenched. The recycle pond waterline for the base case is 10 inches, unlined, carbon steel pipe; no spare is included.

Pond Construction--

Optimum pond dimensions and costs for each case are calculated by computer based on a square configuration with a diverter dike three-fourths the length of a side. A pond construction diagram is shown in Figure 5. Assuming level land for the pond site, total pond depth for base case is 19.6 feet with an excavation depth of 3.0 feet. The pond is lined with 12 inches of impervious clay assumed to be excavated at the site. Pond areas for each case variation are listed in Table 20.

Trucking Alternative--

A case variation has been prepared on base case conditions which produces a filter cake disposed of by piling. A thickener and rotary drum filters which dewater the slurry to a 55% solids cake are added to the system after the pond feed tank (now the thickener feed tank). The cake is moved by conveyor to an in-process waste pile where wheeled loaders transfer the solids to dump trucks for transport to a disposal area 1 mile from the scrubbing facilities. Assuming level land, the disposal site is scraped to clay base and a ditch 10 feet wide and 10 feet long is dug around the perimeter of the site runoff to the ash pond. Waste solids are piled 30 feet high using a grader, a dozer, and a towed roller.

A detailed description of the economics of lime-limestone waste disposal has been published (Barrier, et al., 1978).

TABLE 18. LIMESTONE SLURRY PROCESS

MATERIAL BALANCE - BASE CASE

Stream No.	1	2	3	4	5
Description	Coal to boiler	Combustion air to air heater	Combustion air to boiler	Gas to economizer	Gas to air heater
Total stream, lb/hr	428,600	4,546,200	4,101,800	4,516,100	4,516,100
2 sft ³ /min (60°F)		1,005,000	906,700	958,000	958,000
} Temperature, ^O F		80	535	890	705
4 Pressure, psig	<u> </u>				
5 gpm					
6 Specific gravity					
7 pH					
8 Undissolved solids, %					
9	<u> </u>				
10					

	Stream No.	6	7	8	9	10
	Description	Gas to electrostatic precipitator	Gas to presaturator	Gas to reheater	Gas to stack	Steam to reheater
	Total stream, 1b/hr	4,960,400	4,905,800	5,108,100	5,108,100	93,070
2	sft ³ /min (60°F)	1,056,000	1,056,000	1,127,200	1,129,000	
3	Temperature, OF	300	300	127	175	470
4	Pressure, psig					500
5	gpm					
6	Specific gravity					
7	pH					
8	Undissolved solids, %					
9						
10						

Stream No.	11	12	13	14	15
Description	Recycle slurry for saturation	Makeup water to absorber	Recycle slurry to absorber	Overflow to pond feed tank	Slurry to pond
Total stream, 1b/hr	2,803,900	292,100	35,023,500	360,000	360,000
2 sft3/min (60°F)					1
j Temperature, ^O F					
4 Pressure, psig			1		
5 gpm	5,094	584	63,628	654	654
6 Specific gravity	1.1		1.1	1.1	1.1
7 pH	5.3		5.3		
8 Undissolved solids, %	15		15	15	15
9					I
10			1		Ι

Stream No.	16	17	18	19	20
Description	Settled sludge	Pond water to wet ball mill	Pond water to recirculation tank	Limestone to weigh feeder	Slurry to mills product tank
Total stream, lb/hr	135,000	26,400	198,600	45,200	71,600
2 sft3/min (60°F)					
3 Temperature, OF					
4 Pressure, psig					
5 gpm	205	53	397		89
6 Specific gravity	1.32				1.61
7 pH					
8 Undissolved solids, %	40				60
9					
10	1i				

(continued)

TABLE 18 (continued)

					 -
Stream No.	21				
	Limestone				
ļ	slurry to recirculation				
Description	tank		i		
1 Total stream, 1b/hr 2 sft ³ /min (60°F)	71,600				
2 sft ³ /min (60°F) 3 Temperature, °F					
4 Pressure, psig					
5 gpm	1.61				
6 Specific gravity 7 pH	1.01				
8 Undissolved solids, %	60				
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TABLE 19. LIMESTONE SLURRY PROCESS

BASE CASE EQUIPMENT LIST DESCRIPTION AND COST

Area	1Materials Handl	ing		
	Item	No.	Description	Total material cost, 1979 \$
1.	Car shaker	1	Top mounting with crane	9,000
2.	Car puller	1	25 hp with 5 hp return	50,000
3.	Hopper, limestone unloading	1	12 ft x 20 ft x 2 ft bottom, 20 ft deep, $4,800 \text{ ft}^3$, carbon steel	9,300
4.	Feeder, limestone unloading	1	Vibrating pan 42 in. wide x 60 in. long, 3 hp, 250 tons/hr	4,800
5.	Conveyor, limestone unloading	1	Belt 36 in. wide x 10 ft long, 5 hp, 250 tons/hr, 130 ft/min	2,200
6.	Conveyor, limestone stocking (incline)	1	Belt 36 in. wide x 320 ft long, 30 hp, 15° slope, 250 tons/hr, 130 ft/min	48,000
7.	Conveyor, limestone stocking	1	Belt 36 in. wide x 200 ft long, 7-1/2 hp, 250 tons/hr, 130 ft/mi	30,000 n
8.	Tripper	1	5 hp, 30 ft/min	14,800
9.	Mobile equipment	1	Scraper tractor, 22 to 24 yd ³ capacity	181,000
10.	Hopper, reclaim	2	7 ft x 7 ft, 4 ft deep, 60° slope, carbon steel	11,200
11.	Feeder, live limestone storage	2	Vibrating pan 24 in. wide x 40 in. long, l hp, 12 tons/hr	7,000
12.	Pump, tunnel sump	1	Vertical, 60 gpm, 70 ft head, 5 hp, carbon steel, neoprene lined	3,400
13.	Conveyor, live limestone feed	1	Belt 30 in. wide x 100 ft long, 2 hp, 100 tons/hr, 60 ft/min	14,400
14.	Conveyor, live limestone feed (incline)	1	Belt 30 in. wide x 190 ft long, 5 hp, 35 ft lift, 100 tons/hr, 60 ft/min	26,600

(continued)

TABLE 19 (continued)

	Item	No.	Description	Total material cost, 1979 \$
15.	Elevator, live limestone feed	1	Continuous, bucket, 12 in. x 8 in. x 11-3/4 in., 20 hp, 75 ft lift, 100 tons/hr, 160 ft/min	30 ,800
16.	Bin, crusher feed	1	17 ft dia x 17 ft high, w/cover, 3/8 in. carbon steel	13,800
17.	Dust collecting system	1	Cyclone, 2,100 aft^3/min , motor driven fan	5,900
18.	Dust collecting system	1	Cyclone, $6,200 \text{ aft}^3/\text{min, motor}$ driven fan	14,200
19.	Dust collecting system	1	Bag filter, polypropylene bag, 14,400 aft ³ /min, automatic shake system (1/2 cost in feed preparation area)	
	Subtotal			486,400

Area 2-	-Feed	Prepara	ition
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	Item	No.	Description	Total material cost, 1979 \$
1.	Feeder, limestone bin discharge	2	Vibrating, 12 tons/hr, w/cover, carbon steel	1,900
2.	Feeder, crusher	2	Weigh belt, 18 in. wide x 14 ft long, $1-1/2$ hp, 12 tons/hr	15,80 0
3.	Crusher	2	Gyratory, $0 \times 1-1/2$ to $3/4$ in., 50 hp, 12 tons/hr	⁵⁴ ,000
4.	Ball mill	2	Wet, open system, 8 ft dia x 13 ft long, 350 hp, 300 tons/day	393 ,100
	Ball charge			31,100
5.	Hoist	1	Electric, 5 ton	8,300
6.	Tank, mills product	1	9 ft dia x 5 ft high, 2,350 gal, open top, four 9 in. baffles, agitator supports, carbon steel	1,300
	Lining		<pre>1/4 in. neoprene lining (continued)</pre>	1,100

TABLE 19 (continued)

	Item	No.	Description	Total material cost, 1979 \$
7.	Agitator, mills product tank	1	36 in. dia, 10 hp, neoprene coated	12,000
8.	Pump, mills product tank	2	Centrifugal, 89 gpm, 60 ft head, 7-1/2 hp, carbon steel, neoprene lined	5,400
9.	Tank, slurry feed	1	18 ft dia x 22 ft high, 42,800 gal open top, four 18 in. baffles, agitator supports, carbon steel	, 10,500
	Lining		1/4 in. neoprene lining	9,800
10.	Agitator, slurry feed tank	1	3 turbines, 72 in. dia, 75 hp, neoprene coated	58,000
11.	Pump, slurry feed tank	2	Centrifugal, 89 gpm, 60 ft head, 7-1/2 hp, carbon steel, neoprene lined	5,400
12.	Dust collecting system	1	Cyclone, $8,200 \text{ aft}^3/\text{min, motor-driven fan}$	16,300
13.	Dust collecting system	1	Bag filter, polypropylene bag, 14,400 aft ³ /min, automatic shaker system (1/2 cost in materials handling area)	_10,000
	Subtotal			634,000

Area 3--Gas Handling

	Item	No.	Description	Total material cost, 1979 \$
1.	Fans	4	Forced draft, 13 in. static head, 890 rpm, 1,250 hp, fluid drive, double width, double inlet	812,000
	Subtotal			812,000

TABLE 19 (continued)

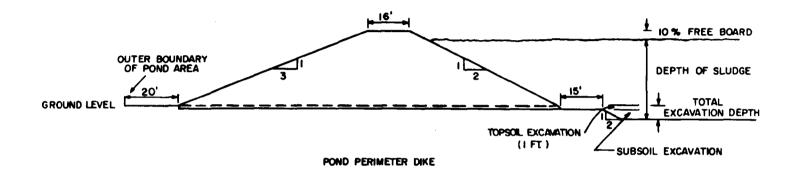
Area	4SO ₂ Absorption			
	Item	No.	Description	Total material cost, 1979 \$
1.	SO ₂ absorber	4	Mobile-bed scrubber, 31 ft long x 14 ft wide x 40 ft high, 1/4 in. carbon steel, neoprene lining; 316 SS grids, nitrile foam spheres, FRP spray headers, 316SS chevron vane entrainment separator	2,813,700
2.	Tank, recir- culation	4	34 ft dia x 26 ft high, 173,500 gal open top, four 34 in. baffles, agitator supports, carbon steel	, 85 ,600
	Lining		1/4 in. neoprene lined	⁷⁹ ,800
3.	Agitator, recir- culation tank	4	100 in. dia, 50 hp, neoprene coated	185,600
4.	Pump, presatu- rator	6	Centrifugal, 1,274 gpm, 105 ft head 75 hp, carbon steel, neoprene lined	
5.	Pump, makeup water	2	Centrifugal, 1,168 gpm, 150 ft head 75 hp, carbon steel	, 15,300
6.	Pump, slurry recirculation	10	Centrifugal, 7,954 gpm, 105 ft head 500 hp, carbon steel, neoprene lined	, 294,000
7.	Soot blowers	40	Air, retractable	260,000
	Subtotal			3,792,000

Area	5F	Reheat
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	Item	No.	Description	Total material cost, 1979 \$
1.	Reheater	4	Steam, tube type, 3,600 ft ² , one-half tubes made of Inconel 625 and one-half made of Cor-Ten	856,000
2.	Soot blowers	20	Air, retractable	130,000
	Subtotal			986,000

TABLE 19 (continued)

Area	6Solids Disposal			
	Item	No.	Description	Total material cost, 1979 \$
1.	Tank, pond feed	1	12 ft dia x 15 ft high, 12,700 gal, open top, four 12 in. baffles, agitator supports, carbon steel	•
	Lining		1/4 in. neoprene lining	3,700
2.	Agitator, pond feed tank	1	2 turbines, 66 in. dia, 15 hp, neoprene coated	19,500
3.	Pumps, pond feed	2	Centrifugal, 654 gpm, 100 ft head, 50 hp, carbon steel, neoprene lined	12,800
4.	Pumps, pond return	2	Centrifugal, 450 gpm, 100 ft head, 30 hp, carbon steel	6,900
	Subtotal			47,000



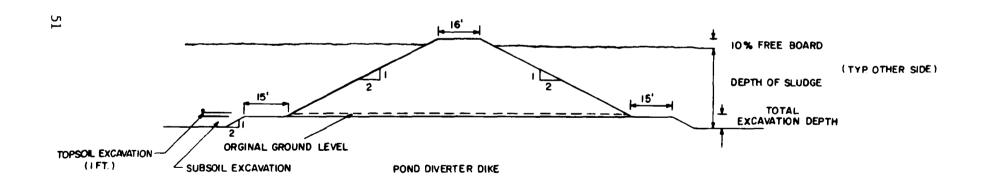


Figure 5. Pond construction diagram.

TABLE 20. LIMESTONE SLURRY PROCESS

ACREAGE REQUIRED FOR WASTE SOLIDS DISPOSAL

_	Years remaining	
Case	life	Acres
Coal-Fired Power Unit		
1.2 lb SO ₂ /MBtu heat input		
allowable emission; onsite		
solids disposal (ponding)		
200 MW E 3.5% sulfur	20	79
200 MW N 3.5% sulfur	30	142
500 MW E 3.5% sulfur	25	227
500 MW N 2.0% sulfur	30	155
500 MW N 3.5% sulfur	30	287
500 MW N 5.0% sulfur	30	424
1,000 MW E 3.5% sulfur	25	383
1,000 MW N 3.5% sulfur	30	480
Solids disposal by trucking		
500 MW N 3.5% sulfur	30	96
90% SO ₂ removal; onsite solids		
disposal (ponding)		
500 MW N 3.5% sulfur	30	329
Oil-Fired Power Unit		
0.8 lb SO ₂ /MBtu heat input		
allowable emission; onsite		
solids disposal (ponding)		
500 MW E 2.5% sulfur	25	110

GENERIC DOUBLE-ALKALI PROCESS

The double-alkali process included in this study (Figure 6) has been generalized from the several processes currently available in the United States. In this design, an ESP is used for removal of fly ash and a common plenum and booster fans are included downstream from the ESP and the power plant ID fans for distribution of the gas (Figure 7).

Flue gas is cooled and saturated in a presaturator with a recycle stream of scrubber effluent. In the absorber tower SO₂ is removed using a mixture of a regenerated sodium sulfite solution and recycle scrubber effluent (pH about 6.0). The outlet gas from the scrubber passes through a chevrontype entrainment separator with provisions for upstream wash with fresh makeup water. The cleaned flue gas is reheated to 175°F by indirect steam heat before entering the stack.

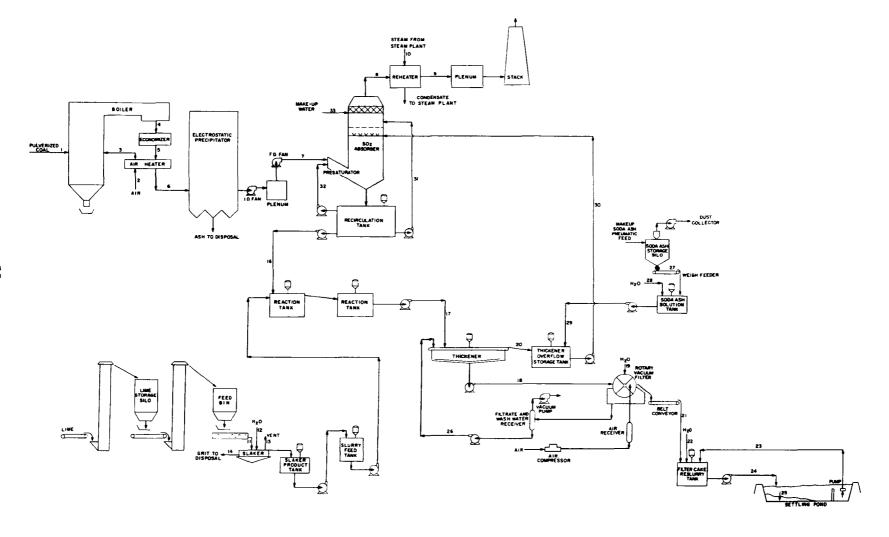


Figure 6. Generic double-alkali process. Base case flow diagram.

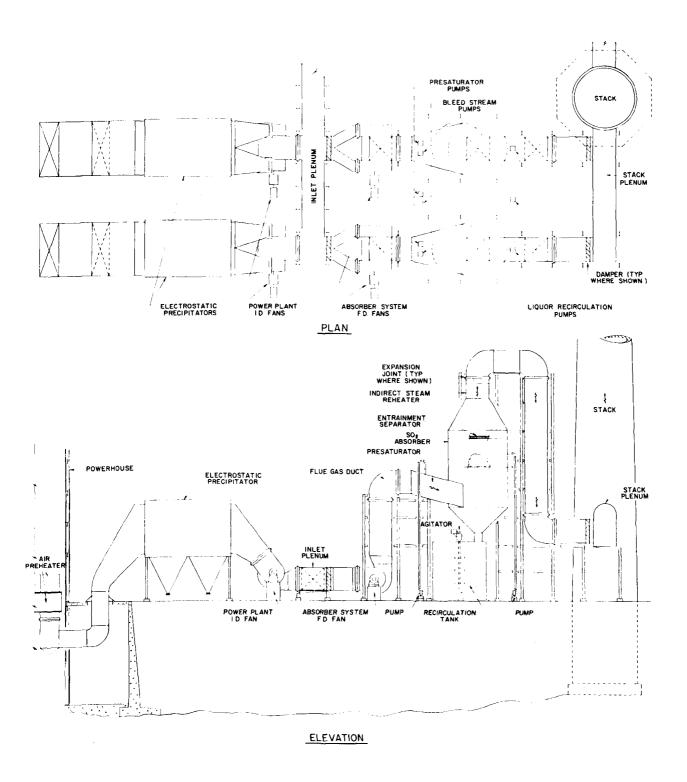


Figure 7. Generic double-alkali process. Perforated-tray scrubber system base case plan and elevation.

Incoming pebble lime, from an across-the-fence limestone calcination plant, is received in a silo with a 10-day capacity and conveyed to two 4-how feed bins that supply the slakers (Figures 8 and 9). The lime is processed in two parallel slakers to a slurry concentration of 15% solids. A slurry feed tank with a residence time of 8 hours is provided for in-process storage

Lime slurry is reacted with a bleedstream of absorber effluent in agitated tanks. The reaction product, predominately calcium sulfite, is pumped to a thickener where the slurry is concentrated to 25% solids. This stream is further dewatered using drum filters to produce a cake of about 55% solids. The filter is designed with two wash sections to minimize sodium loss. The filter cake is reslurried to 15% solids with supernate from the pond and fres makeup water for pumping to disposal. The solids settle to a concentration of approximately 40% in the pond. A special case is evaluated in which the spent slurry, after thickening and filtering, is trucked to a disposal site located 1 mile from the scrubbing facilities.

Makeup soda ash is pneumatically conveyed from a rail hopper car to the storage silo and fed to an agitated tank where it is slurried in fresh makeu water. The slurry is added to the regenerated scrubber liquor at the thick-ener overflow storage tank.

The material balance for the base case double-alkali system is shown in Table 21 and a detailed equipment list by area for the system is presented in Table 22.

Major Process Areas

The generic double-alkali process has been divided into the following operating areas.

- Materials handling. This area includes facilities for receiving pebble lime from an across-the-fence limestone calcination plant, lime storage silo, and in-process storage for supply to the slakers.
 Soda ash storage is also provided.
- Feed preparation. Included in this area are two parallel slaking systems and the facilities for dissolving makeup soda ash in water before feeding to the absorption system.
- 3. Gas handling. Fan location and duct configuration is the same as the limestone slurry process.
- 4. SO₂ absorption. Four tray tower absorbers with presaturators, recirculation tanks, and pumps are included.
- 5. Stack gas reheat. Equipment in this area includes indirect steam reheaters and soot blowers for the coal variations. The oil-fired unit is designed with one direct oil-fired reheater per duct which discharges hot combustion gases directly into the duct.

- 6. Reaction. Reaction tanks with agitators and pumps are provided in this area.
- 7. Solids separation. Separation of calcium salts is accomplished by thickener and filters.
- 8. Solids disposal. Filter cake is reslurried in this area and purged to the disposal pond. A pond return pump is included.

Storage Capacity

Storage requirements for raw materials and allowances for in-process streams are listed below.

Raw materials:

Lime storage silo - 10 days (from across-the-fence calcination plant) Soda ash storage silo - 4 months (purchased in bulk quantity by rail)

In-process storage:

Lime feed bins - 4 hours each

Slaker product tank - 5 minutes

Slurry feed tank - 8 hours

Soda ash solution tank - 8 hours

Recirculation tanks - 10 minutes each (includes sufficient surge capacity for shutdown of scrubbers)

Thickener - 4 hours

Thickener overflow storage tank - 20 minutes

Filter cake reslurry tank - 5 minutes

Solids Disposal

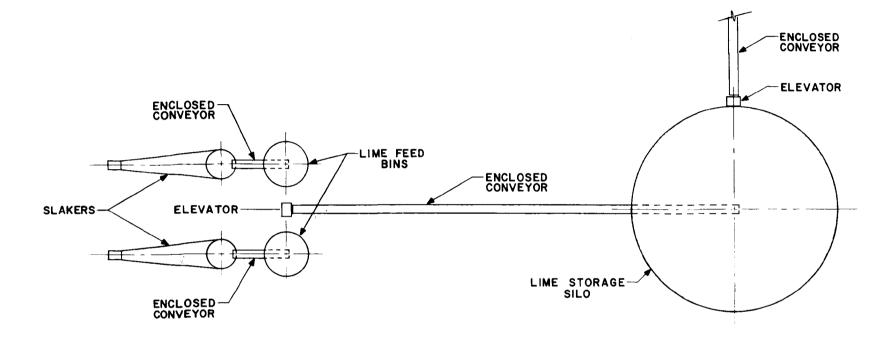
Waste solids in the generic double-alkali process are handled in the same manner as the limestone slurry process.

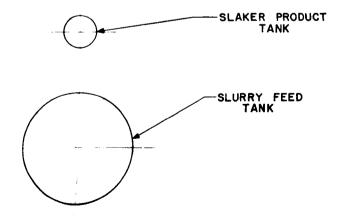
Pond Construction--

Pond designs are similar to the design for the limestone slurry process. Total pond depth for the base case is 18.9 feet and excavation depth is 3.1 feet. Pond areas for each case variation are listed in Table 23.

Trucking Alternative--

Transport of waste solids by truck to a disposal area is similar to the method used for the limestone process.





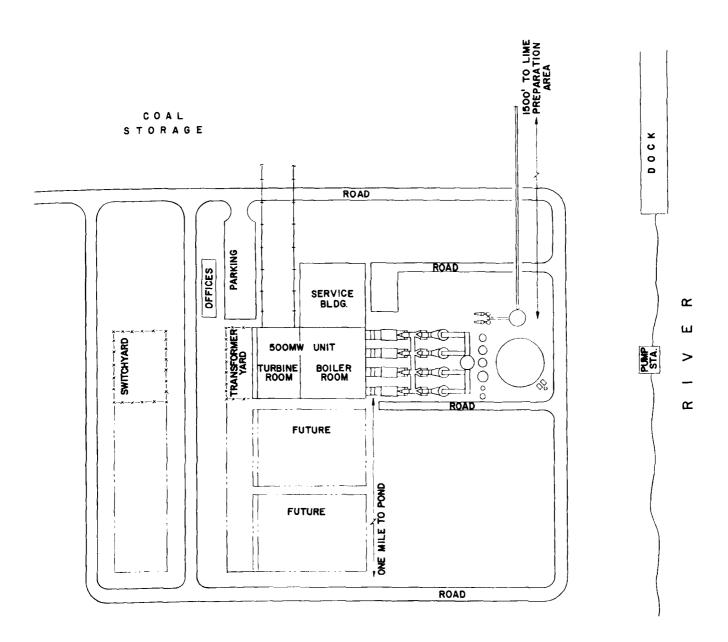


Figure 9. Generic double-alkali process. Base case overall plot plan.

TABLE 21. GENERIC DOUBLE-ALKALI PROCESS

MATERIAL BALANCE - BASE CASE

Stream No.	1	2	3	4	. 5
Description	Coal to boiler	Combustion air to air heater	Combustion air to boiler	Gas to economizer	Gas to air heater
Total stream, lb/hr	428,600	4,546,200	4,101,800	4,516,100	4,516,100
2 sft ³ /min (60°F)	<u> </u>	1,005,000	906,700	958,000	958,000
J Temperature, OF		80	535	890	705
4 Pressure, psig					
5 gpm					
6 Specific gravity	L		L		
7 pH	<u> </u>	L	I		
8 Undissolved solids, %	<u> 1</u>				1
9					
10 I					T

Stream No.	6	7	8	9	10
Description	Gas to electrostatic precipitator	Gas to presaturator	Gas to reheater	Gas to stack	Steam to reheater
Total stream, lb/hr	4,960,400	4,905,800	5,094,000	5,094,000	92,810
2 sft ³ /min (60°F)	1,056,000	1,056,000	1,125,000	1,126,700	
Temperature, OF	300	300	127	175	470
4 Pressure, psig					500
5 gpm			L		
6 Specific gravity					
7 pH					
8 Undissolved solids, %					
9					
10					

Stream No.	11	12	13	14	15
Description	Lime to slaker	Water to slaker	Vent from slaker	Grit to disposal	Lime slurry to reaction tank
Total stream, lb/hr	18,170	135,150	1,056	182	152,080
2 sft ³ /min (60°F)					1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1
3 Temperature, OF					
4 Pressure, psig					
5 gpm		270	2		279
6 Specific gravity					1.09
7 pH					
8 Undissolved solids, %					15
9					
10					T

Stream No.	16	17	18	19	20
Description	Bleedstream to reaction tank	Slurry to thickener	Thickener underflow to filter	Filter wash water	Thickener overflow to storage tank
Total stream, 1b/hr	1.898.900	2.051.000	167.800	59.700	2.034.400
2 sft ³ /min (60°F) 3 Temperature, °F	 				
4 Pressure, psig					
5 gpm	3,547	3.726	271	120	3,800
6 Specific gravity	1.07	1.1 T	1.24		1.07
7 pH	6.0	11.0			1
8 Undissolved solids, %		2	25		
9					†
10	7				

TABLE 21 (continued)

Stream No.	21	22	23	24	25
Description	Filter cake to reslurry tank	Water to reslurry tank	Recycle pond water	Slurry to pond	Settled sludge
l Total stream, lb/hr	76,270	28,600	174,780	279,650	104,870
2 sft3/min (60°F)					
3 Temperature, OF					
4 Pressure, psig					
5 gpm	J	57	349	508	161
6 Specific gravity				1.1	1.3
7 pH		1			
8 Undissolved solids, %	55			15	40
9	↓				
10	11				_1

Stream No.	26	27	28		30	
Description	Filtrate to thickener	Soda ash to solution tank	Water to solution tank	Makeup soda ash stream	Scrubbing liquor to absorber	
Total stream. lb/hr	151,230	1,730	9,800	11,530	2,045,900	
2 sft3/min (60°F)						
Temperature, OF						
Pressure, psig	283		20	20	3,821	
6 Specific gravity	1.07			1.14	1.07	
7 pH						
8 Undissolved solids. %						
0					- 	

Stream No.	31	32	33		
Description	Recycle liquor to absorber	Recycle liquor to presaturator	Makeup water to absorber		
Total stream, lb/hr	2,727,500	2,727,500	41,100		
2 sft ³ /min (60°F)					
J Temperature. OF					
4 Pressure, psig		4		<u> </u>	
5 gpm	5,094	5,094	82		
6 Specific gravity	1.07	1.07			
7 pH	5,8	J			
8 Undissolved solids, %					
9					
10					

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TABLE 22. GENERIC DOUBLE-ALKALI PROCESS

BASE CASE EQUIPMENT LIST DESCRIPTION AND COST

<u>Area</u>	lMaterials Hand	ling		Total material
	Item	No.	Description	cost, 1979 \$
1.	Conveyor, lime storage (enclosed)	1	Belt, 24 in. wide x 1,500 ft long, 30 hp, 100 tons/hr, 150 ft/min	169,900
2.	Elevator, lime storage	1	Continuous, bucket 16 in. x 8 in. x 11-3/4 in., 75 hp, 120 ft lif ^t , 100 tons/hr, 160 ft/min	102,900
3.	Silo, lime storage	1	46 ft dia x 69 ft high, $109,000$ ft ³ , cone bottom, $3/8$ in. carbon steel	75 ,900
4.	Feeder, reclaim	1	Vibrating pan, 3-1/2 hp, 40 tons/h	r 12,200
5.	Conveyor, live lime feed	1	Belt, 18 in. wide x 100 ft long, 2 hp, 40 tons/hr, 100 ft/min	9,300
6.	Elevator, live lime feed	1	Continuous, bucket 11 in. x 6 in. x 8-3/4 in., 50 hp, 50 ft lift, 40 tons/hr, 160 ft/min, with diverter gate	56,00 0
7.	Bin, lime feed	2	10 ft dia x 15 ft high, 1,180 ft ³ , w/cover, carbon steel	5,400
8.	Conveyor, soda ash storage	1	Pneumatic, vacuum, 40 hp	65 , 000
9.	Silo, soda ash storage	1	15 ft dia x 30 ft high, 5,850 ft 3 , cone bottom, carbon steel	9,200
	Vibrators	4		6,100
10.	Dust collecting system	1	Bag filter, polypropylene bag, 8,800 aft ³ /min, automatic shaker system	21,400
	Subtotal			533,300

Area	2Feed Preparation			Total material
	Item	No.	Description	cost, 1979 \$
1.	Feeder, lime bin discharge	2	Vibrating, 3-1/2 hp, carbon steel	9,200
2.	Feeder, slaker	2	Screw, 12 in. dia x 12 ft long, 1 hp, 5 tons/hr	12,000
3.	Slaker	2	6 ft wide x 28 ft long, 10 hp slaker, 2 hp classifier, 5 tons/hr	108,000
4.	Tank, slaker product	2	7 ft dia x 6 ft high, 1,730 gal, open top, four 7 in. baffles, agitator supports, carbon steel	2,100
	Lining		1/4 in. neoprene lining	1,700
5.	Agitator, slaker product tank	2	30 in. dia, 5 hp, neoprene coated	17,500
6.	Pump, slaker product tank	3	Centrifugal, 140 gpm, 100 ft head, 7-1/2 hp, carbon steel, neoprene lined	8,700
7.	Tank, slurry feed	1	24 ft dia x 36 ft high, 122,000 gal open top, four 24 in. baffles, agitator supports, carbon steel	
	Lining		1/4 in. neoprene lining	17,500
8.	Agitator, slurry feed tank	1	2 turbines, 96 in. dia, 50 hp, neo- prene coated	46,600
9.	Pump, slurry feed tank	2	Centrifugal, 279 gpm, 100 ft head, 15 hp, carbon steel, neoprene lines	6,700
10.	Feeder, soda ash silo discharge	1	Rotary air lock, carbon steel	2,500
11.	Feeder, soda ash solution tank	1	Weigh	5,400
12.	Tank, soda ash solution	1	12 ft dia x 14 ft high, 11,850 gal open top, four 12 in. baffles, agitator supports, carbon steel	
	Lining		1/4 in. neoprene lining	3,500
			(continued)	

TABLE 22 (continued)

	Item	No.	Description	Total material cost, 1979 \$
13.	Agitator, soda ash solution tank	1	48 in. dia, 15 hp, neoprene coated	19,500
14.	Pump, soda ash solution tank	2	20 gpm, 60 ft head, 1 hp, carbon steel, neoprene lined	4,700
	Subtotal			288,000

Area	3Gas	nanditin	K	

	Item	No.	Description	Total material cost, 1979 \$
1.	Fans	4	Forced draft, 8 in. static head, 700 rpm, 850 hp, fluid drive, double width, double inlet	752,000
	Subtotal			752,000

4-0-	450-	Absorption
area	4500	ADSOLPLION

	Item .	No.	Description	Total materis
1.	SO ₂ absorber	4	Tray tower, 31 ft dia x 40 ft high, 3/8 in. carbon steel, flake-lined; 1-316 SS sieve tray, 316 SS nozzles, polypropylene chevron vane entrainment separator	The second secon
2.	Tank, recircu- lation	4	28 ft dia x 30 ft high, 137,350 gal, open top, four 28 in. baffles, agitator supports, carbon steel	76 ,000
	Lining		1/4 in. neoprene lining	71,200
3.	Agitator, recir- culation tank	4	108 in. dia, 25 hp, neoprene coated	113,800
4.	Pump, presat- urator	6	Centrifugal, 1,274 gpm, 105 ft head 75 hp, carbon steel, neoprene lines	,
5.	Pump, liquor recirculation	6	75 hp, carbon steel, neoprene lineo	
			(continued)	

TABLE 22 (continued)

	Item	No.	Description	Total material cost, 1979 \$
6.	Pump, bleed to reaction	6	Centrifugal, 887 gpm, 100 ft head, 60 hp, carbon steel, neoprene lined	40,200
7.	Pump, makeup water	2	Centrifugal, 1,000 gpm, 150 ft head, 60 hp, carbon steel	12,000
8.	Soot blowers	40	Air, retractable	260,000
	Subtotal			4,006,000

Area 5--Reheat

<u>Arcu</u>	Item	No.	Description	Total material cost, 1979 \$
1.	Reheater	4	Steam, tube type, 3,600 ft ² , one-half tubes made of Inconel 625, and one-half made of Cor-Ten	856,000
2.	Soot blowers	20	Air, retractable	130,000
	Subtotal			986,000

Area 6--Reaction Tanks

Area	6Reaction lanks			M 1
	Item	No.	Description	Total material cost, 1979 \$
1.	Tank, reaction	2	26 ft dia x 15 ft high, 59,570 gal, open top, four 26 in. baffles, agitator supports, carbon steel	20,600
	Lining		1/4 in. neoprene lining	18,800
2.	Agitator, reaction tank	2	100 in. dia, 25 hp, neoprene coated	56,600
3.	Pump, reaction tank	2	Centrifugal, 3,726 gpm, 50 ft head, 100 hp, carbon steel, neoprene lined	31,200
	Subtotal			127,200

Area	7Soli	lds	Sep	arat	cion

	Item	No.	Description	Total materia cost, 1979 \$
1.	Thickener	1	Stainless steel tank, 140 ft dia x 8 ft high; concrete basin, 4 ft high	112,900
	Rake motor and mechanism		7-1/2 hp	422,000
2.	Pump, underflow slurry	2	Centrifugal, 271 gpm, 100 ft head, 20 hp, carbon steel, neoprene lined	9,300
3.	Tank, thickener overflow storage	1	33 ft dia x 15 ft high, 96,000 gal open top, four 33 in. baffles, agitator supports, carbon steel	
	Lining		1/4 in. neoprene lining	12,800
4.	Agitator, thick- ener overflow storage tank	1	132 in. dia, 25 hp, neoprene coated	²⁸ ,500
5.	Pump, scrubbing liquor return	6	Centrifugal, 955 gpm, 125 ft head, 60 hp, carbon steel, neoprene lined	41,600
6.	Filter	2	Rotary vacuum, 12 ft dia x 14 ft face, 20 total hp	²⁵¹ ,300
7.	Pump, filter wash water	2	240 gpm, 80 ft head, 15 hp, carbon steel	4,800
8.	Conveyor, filter cake	1	Belt, 18 in. wide x 100 ft long, 5 hp, 40 tons/hr, 100 ft/min	9,800
	Subtotal			907,000

TABLE 22 (continued)

Area	8Solids Disposal			
Area	Item	No.	Description	Total material cost, 1979 \$
1.	Tank, filter cake reslurry	1	7 ft dia x 10 ft high, 2,700 gal, open top, four 7 in. baffles, agitator supports, carbon steel	1,600
	Lining		1/4 in. neoprene lining	1,400
2.	Agitator, filter cake reslurry tank		30 in. dia, 7-1/2 hp, neoprene coated	11,700
3.	Pump, pond feed	2	Centrifugal, 508 gpm, 110 ft head, 50 hp, carbon steel, neoprene lined	12,400
4.	Pump, pond return	2	Centrifugal, 349 gpm, 110 ft head, 25 hp, carbon steel, neoprene linin	<u>9,900</u>
	Subtotal			37,000

TABLE 23. GENERIC DOUBLE-ALKALI PROCESS

ACREAGE REQUIRED FOR WASTE SOLIDS DISPOSAL

	Years remaining	
Case	life	Acres
Coal-Fired Power Unit		
1.2 lb SO ₂ /MBtu heat input		
allowable emission; onsite		
solids disposal (ponding)		
200 MW E 3.5% sulfur	20	64
200 MW N 3.5% sulfur	30	116
500 MW E 3.5% sulfur	25	187
500 MW N 2.0% sulfur	30	127
500 MW N 3.5% sulfur	30	233
500 MW N 5.0% sulfur	30	329
1,000 MW E 3.5% sulfur	25	315
1,000 MW N 3.5% sulfur	30	393
Solids disposal by trucking		
500 MW N 3.5% sulfur	30	87
90% SO ₂ removal; onsite		
solids disposal (ponding)		
500 MW N 3.5% sulfur	30	260
Oil-Fired Power Unit		
0.8 lb SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)		
500 MW E 2.5% sulfur	25	97

CITRATE PROCESS

The citrate process design developed for this study (Figure 10) is adapted from a U.S. Bureau of Mines process and represents the state of technology in 1977. The demonstration program for the Bureau of Mines citrate process has been in active development during the time for preparation of this report. Certain features of the demonstration design which are significantly different from the process design represented here have been identified under Major Process Areas.

The scheme evaluated assumes fly ash removal by ESP. Power plant ID fans feeding a common plenum and booster FD fans are included in the design (Figure 11). Flue gas is cooled and saturated in a presaturator with recycle liquor from the bottom of the scrubber. SO_2 is removed from the flue gas by countercurrent scrubbing in a packed tower using a regenerated solution containing sodium citrate as a buffer. A purge stream to control chlorides is pumped from the bottom of the absorber through an SO_2 stripper to a neutralization tank where it is reacted with lime before being pumped to the ash disposal pond. Stripped SO_2 is returned to the absorption tower at the presaturator. Cleaned flue gas is passed through a chevron-type entrainment separator with provisions for upstream wash with fresh makeup water and reheated to $175^{\circ}F$ by indirect steam heat before entering the stack.

Elemental sulfur is precipitated from the SO_2 -laden sorbent in reduction tanks by countercurrent contact with H_2S gas containing 80% to 97% H_2S . The sulfur is separated by air flotation, then melted and settled from the slurry liquor in a decanter operating at a pressure of about 35 psig (Figure 12). Storage is provided for the molten sulfur before marketing.

Hydrogen from natural gas or other sources and a portion of the molten product sulfur from the decanter are feedstocks for $\rm H_2S$ generation. The system guards against $\rm H_2S$ escape in the reduction step by returning unreacted $\rm H_2S$ to the boiler for incineration and by neutralizing dissolved $\rm H_2S$ downstream from the reducing tanks with a small stream of $\rm SO_2$ -rich liquor from the absorber (5% of the absorber effluent).

About 2% of the absorbed SO_2 is oxidized in the system to sodium sulfate. This sulfate, along with the sulfate formed from absorption of SO_3 in the flue gas and thiosulfate decomposition during the sulfur melting step, is removed from the recirculated sorbent by crystallization as Glauber's salt $(Na_2SO_4 \cdot 10H_2O)$, which is disposed of in the fly ash pond. Liquor from the flotation tank is filtered to remove remaining sulfur particles before cooling and crystallizing. The sulfate crystals are separated by centrifuge and the liquor is returned to the system. Sodium and citrate losses are replaced by adding a mixture of sodium hydroxide or sodium carbonate and citric acid to the recycling sorbent.

The general layout (plot plan) for the citrate system is shown in Figure 13. A material balance for the base case citrate scrubbing process is shown in Table 24 and a detailed equipment list by area for the system is presented in Table 25.

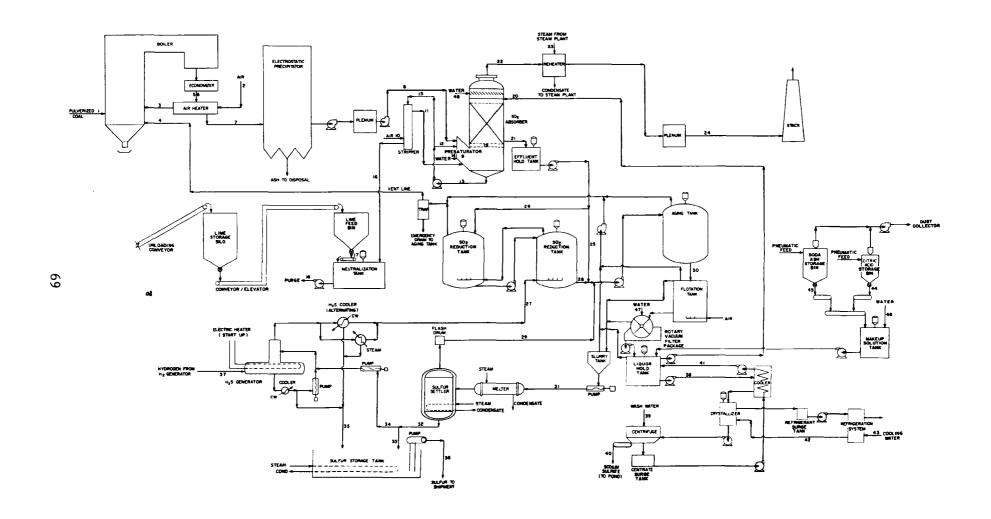


Figure 10. Citrate process. Base case flow diagram.

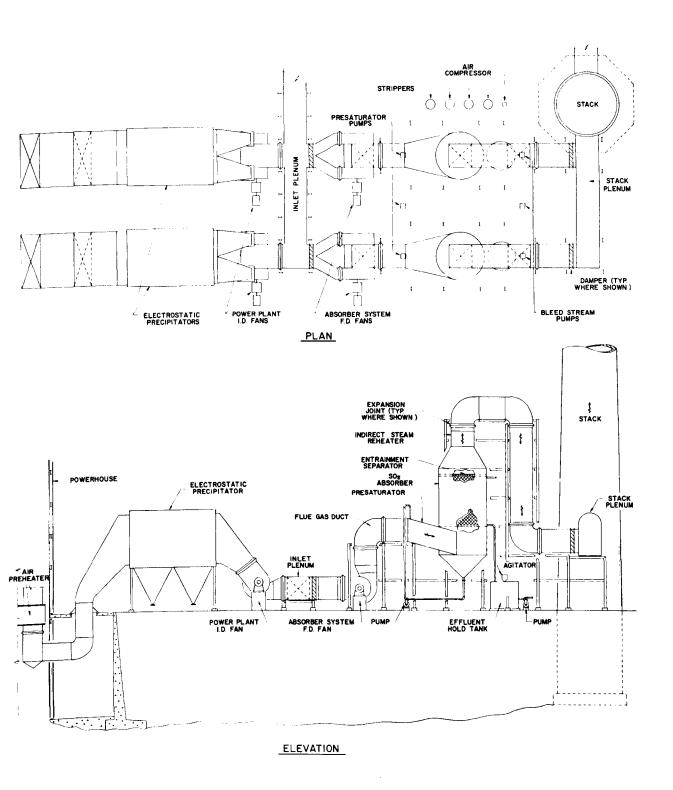


Figure 11. Citrate process. Packed-tower scrubber system base case plan and elevation.

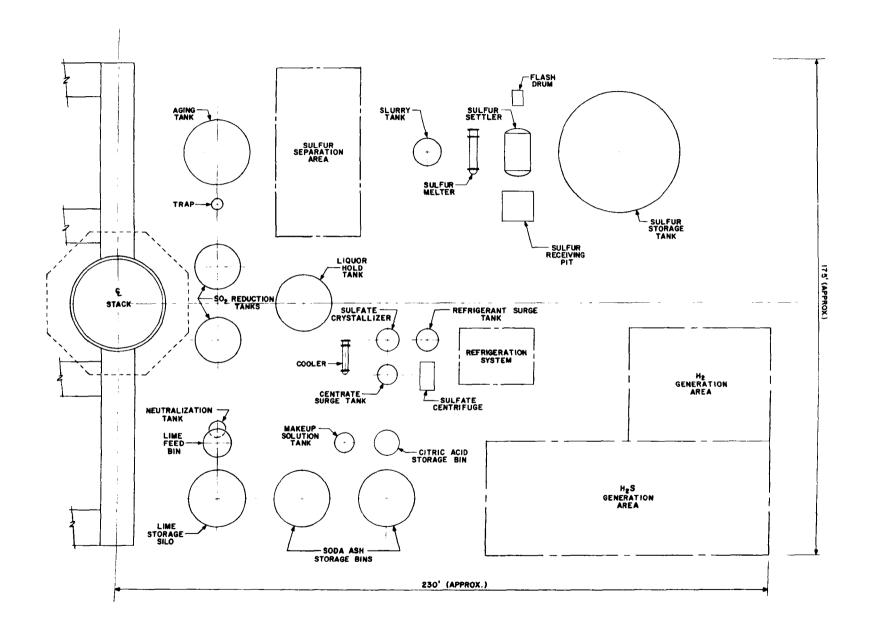


Figure 12. Citrate process. Base case sulfur processing area layout.

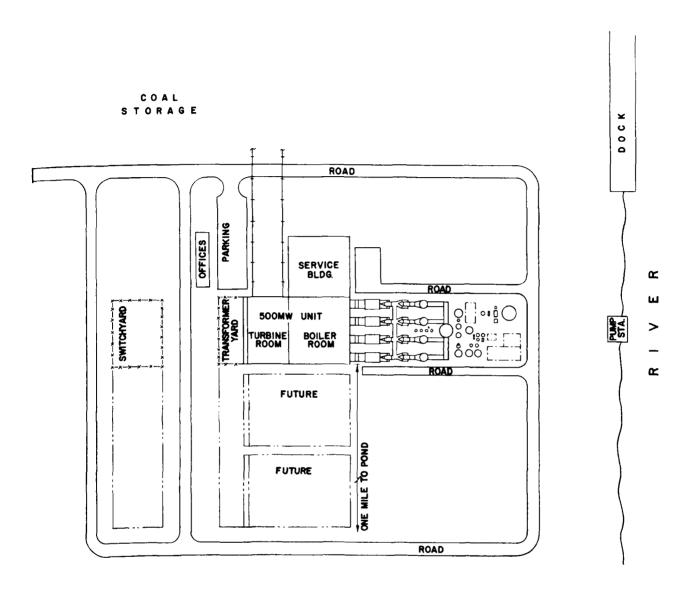


Figure 13. Citrate process. Base case overall plot plan.

TABLE 24. CITRATE PROCESS

MATERIAL BALANCE - BASE CASE

Stream No.	1	2	3	4	5
Description	Coal to boiler	Combustion air to air heater	Combustion air to boiler	Vented H ₂ S gas to boiler	Coal flue gas to air heater
Total stream, lb/hr	428,600	4,546,200	4,101,800	660	4.515.000
2	·	 			
4 sft3/min (60°F)		1,005,000	906,700	190	957.800
5 Temperature, OF		80	535	128	705
6 Pressure, psig		<u> </u>	<u> </u>		
7 gpm				1	
8 Specific gravity		ļ	L	<u> </u>	
9 pH		<u> </u>		<u> </u>	
10 Undissolved solids, %	.1	<u></u>	L	<u>. </u>	

Stream No.	6	7	8	9	10
Description	H ₂ S flue gas to air heater	Gas to electrostatic precipitator	Gas to presaturator	Cooled gas to absorber base	Air to stripper
Total stream, 1b/hr	1,750	4,961,100	4,906,500	5,087,000	4,200
2		 			1:00
4 sft ³ /min (60°F)	300	1,056,300	1,056,300	1,102,400	930
5 Temperature, oF	705	300	300	128	730
6 Pressure, psig					10
7 gpm					
8 Specific gravity		 		L	
9 pH O Undissolved solids, %		 		 	

Stream No.	11	12	13	14	15
Description	Recycle gas to presaturator	Recycle liquor to presaturator	Liquor from presaturator	Makeup water to presaturator	Liquor to stripper
Total stream, lb/hr	4,770	2,614,100	2,640,500	181,700	26,410
2					
3	ļ			 	
4 sft ³ /min (60°F)	1,060				
5 Temperature, OF	120	1			
6 Pressure, psig					
7 gpm		4,997	_5,048	363	50
8 Specific gravity		1.04			
9 pH					
O Undissolved solids, %	1	1		T	

Stream No.	16	17	18	19	20
Description	Liquor to neutralization	Lime to neutralization	Slurry to pond	Flue gas to absorber	Scrubbing liquor to absorber
l Total stream, lb/hr	25,840	655	26,500	5,091,500	3,500,800
2			 		
4 sft ³ /min (60°F)	+	 	<u> </u>	1,121,000	
5 Temperature, or				128	
6 Pressure, psig			ļ		
7 gpm	49	<u> </u>	48		6,360
8 Specific gravity	<u></u>	<u> </u>	1.1		1.1
9 pH			<u> </u>		4.5
O Undissolved solids, %		<u> </u>	2	I	

TABLE 24 (continued)

Stream No.	21	22	23	24	25
Description	Absorber effluent to hold tank	Gas to reheater	Steam to reheater	Gas to stack	Bypass liquor
Total stream, 1b/hr	3,545,000	5,097,200	92,870	5,097,200	177,300
2					
3	 				L
4 sft ³ /min (60°F)		1,126,500		1,128,300	<u> </u>
5 Temperature, OF		127	470	175	l
6 Pressure, psig	7 1		500	1	
7 gpm	6,440				322
8 Specific gravity				<u> </u>	ļ
9 pH					
10 Undissolved solids, %	<u> </u>			L	l

Stream No.	26	27	28	29	30
Description	Liquor to SO ₂	H ₂ S gas to SO ₂ reduction	Slurry from SO ₂ reduction	Return from sulfur settler	Slurry to flotation tank
Total stream, lb/hr	3,368,800	22,115	3,390,300	41,760	3,609,300
2	T	ļ			
3 4 sft ³ /min (60°F)		3,990	 	 	
5 Temperature, OF		130			
6 Pressure, psig	I				
7 gpm	6,120	L	6,159	<u> </u>	6,558
8 Specific gravity			ļ		
9 pH		L	<u> </u>	<u> </u>	
10 Undissolved solids, %		<u> </u>	0 9	1	l

Stream No.	31	32	33	34	35
Description	Slurry to melter	Sulfur from melter	Sulfur to storage	Sulfur to H ₂ S generators	Sulfur from H ₂ S generators
l Total stream, lb/hr	72,200	30,440	6,090	24,355	3,650
2					
4 sft ³ /min (60°F)					
5 Temperature, °F	<u> </u>	307		<u> </u>	
6 Pressure, psig		35		<u> </u>	ļ
7 gpm		<u> </u>		L	L
8 Specific gravity		1,78		l	<u> </u>
9 nH					
10 Undissolved solids, %	1	i l		1	

Stream No.	36	37	38	39	40
Description	Sulfur to shipment	Hydrogen to H ₂ S generator	Liquor to cooler	Centrifuge wash water	Glauber salts to disposal
Total stream, lb/hr	9,735	1,350	35,450	600	2,990
2					
3 4 sft ³ /min (60°F)		4,150			
5 Temperature, of					
6 Pressure, psig		ļI			
7 gpm		↓ ↓	65	11	<u> </u>
8 Specific gravity		 		 	L
9 pH		 		 	
10 Undissolved solids, %	<u>-</u>	<u> </u>			80

TABLE 24 (continued)

Stream No.	41	42	43	44	45
1					
		ì	Ì	Citric acid to	Sodo> .
1	Liquor recycle	Refrigerant to	Cooling H ₂ O to	makeup	Soda ash to makeup
Description	to hold tank	crystallizer	refrigeration	solution tank	solution tank
	33,060	221,520	123,420		
1 Total stream, 1b/hr 2	33,000	221,320	123,420	75	855
131	 				
4 sft ³ /min (60°F)					
4 sft ³ /min (60°F) 5 Temperature, °F		38			
6 Pressure, psig					
7 gpm	60	414	247		
8 Specific gravity		1.07			
9 pH	!				
10 Undissolved solids, %	<u> </u>		<u> </u>	<u> </u>	
Stream No.	46	47	48		
53,000.0	7		78		
5	1			}	
1	1				
I	Water to makeup		Water to		ĺ
Description	solution tank	Water to filter	absorber		
Total stream, lb/hr	4,635	1,600	50,000		
2	L	<u> </u>	<u> </u>		
3 4 sft3/min (60°F)	ļ		<u> </u>		
5 Temperature, OF				L	
6 Pressure, psig					
7 gpm	10	4	100	 	
8 Specific gravity					
9 рн	<u> </u>				
10 Undissolved solids, %					
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TABLE 25. CITRATE PROCESS

BASE CASE EQUIPMENT LIST DESCRIPTION AND COST

	1Materials Handl	No.	Description	Total material cost, 1979 \$
1.	Conveyor, lime unloading	1	Belt, 12 in. wide x 200 ft long, 3 hp, 10 tons/hr, 100 ft/min	28,300
2.	Silo, lime storage	1	20 ft dia x 35 ft high, 10,750 ft ³ , cone bottom, carbon steel	, 16,500
3.	Feeder, lime storage silo discharge	1	Rotary stargate, 1 hp, 5 tons/hr	1,800
4.	Conveyor/elevator, live lime feed	1	Redler Z type, 100 ft long, 3 hp, 5 tons/hr	13,300
5.	Bin, lime feed	1	10 ft dia x 10 ft high, 785 ft ³ , cone bottom, carbon steel	3,000
	Vibrators	2		3,000
6.	Conveyor, soda ash and citric acid	1	Pneumatic, vacuum, 50 hp, 20 tons/hr	102,500
7.	Bin, soda ash storage	2	20 ft dia x 24 ft high, 7,540 ft 3 , cone bottom, carbon steel	25,700
	Vibrators	2		3,000
8.	Bin, citric acid storage	1	9 ft dia x 8 ft high, 510 ft ³ , cone bottom, carbon steel	2,200
	Vibrators	2		3,000
	Subtotal			202,300

TABLE 25 (continued)

Arca	2Feed Preparation			Total material
	Item	No.	Description	cost, 1979 \$
1.	Feeder, soda ash bin discharge	2	Rotary stargate, 1/2 hp, 855 lb/hr	1,600
2.	Feeder, soda ash makeup con- veyor	2	Weigh belt, 14 in. wide x 5 ft long, 1/2 hp, 855 lb/hr, variable speed	7,200
3.	Feeder, citric acid bin discharge	1	Rotary stargate, 1/2 hp, 75 lb/hr	800
4.	Feeder, citric acid makeup conveyor	1	Weigh belt, 14 in. wide x 5 ft long, 1/2 hp, 75 lb/hr, variable speed	3,500
5.	Conveyor, makeup solution tank	1	Belt, 12 in. wide x 40 ft long, 1/2 hp, 1,000 lb/hr, 100 ft/min	4,200
6.	Tank, makeup solution	1	7 ft dia x 8 ft high, 2,300 gal, open top, four 7 in. baffles, agitator supports, carbon steel	1,200
	Lining		1/4 in. neoprene lining	1,200
7.	Agitator, makeup solution tank	1	30 in. dia, 7-1/2 hp, neoprene coated	11,700
8.	Pump, makeup solution tank	2	Centrifugal, 10 gpm, 50 ft head, 1 hp, carbon steel, neoprene lined	2,300
	Subtotal			33,700

	Item	No.	Description	Total material cost, 1979 \$
1.	Fans	4	Forced draft, 20 in. static head, 875 rpm, 2,000 hp, fluid drive, double width, double inlet	888,000
	Subtotal			888,000

TABLE 25 (continued)

Arca	4SO ₂ Absorption Item	No.	Description	Total material cost, 1979 \$
1.	SO ₂ absorber	4	Packed tower, 25 ft dia x 45 ft high, 5/8 in. carbon steel, FRP lining, 316 SS distributor plate, Inconel 625 spray header, 316 SS chevron vane entrainment separator; polypropylene cascade mini-ring packing	6,048,400
2.	Pump, absorber makeup water	2	Centrifugal, 100 gpm, 150 ft head, 10 hp, carbon steel	4,000
3.	Pump, presatu- rator liquor	6	Centrifugal, 1,262 gpm, 75 ft head, 50 hp, carbon steel, neoprene lined	
4.	Pump, presatu- rator makeup water	6	Centrifugal, 91 gpm, 150 ft head, 10 hp, carbon steel	12,000
5.	Stripper, chloride purge	4	Packed column, 4 ft dia x 30 ft high, carbon steel	64,800
6.	Compressor, stripper air	1	$1,000 \text{ ft}^3/\text{min}, 10 \text{ psig}, 300 \text{ hp}$	71,400
7.	Tank, effluent hold	4	14-1/2 ft dia x 14 ft high, 19,750 gal, open top, four 15 in. baffles, agitator supports, carbon steel	18,100
	Lining		1/4 in. neoprene lining	17,500
8.	Agitator, effluent hold tank	4	58 in. dia, 15 hp, neoprene coated	76,200
9.	Pump, effluent hold tank	6	Centrifugal, 1,610 gpm, 120 ft head, 100 hp, carbon steel, neopren lined	<u>59,700</u>
	Subtotal			6,410,500

TABLE 25 (continued)

Area	15Reheat	No.	Description	Total material
1.	Reheater	4	Steam, tube type, 3,600 ft ² , one-half tubes made of Inconel 625 and one-half made of Cor-Ten	856,000
2.	Soot blowers	20	Air, retractable	130,000
	Subtotal			986,000

Area	6	Ch1	orid	е	Purge
------	---	-----	------	---	-------

Area	6chioride Purge			
	Item	No.	Description	Total material cost, 1979 \$
1.	Feeder, lime feed bin discharge	1	Rotary stargate, 1/2 hp, 655 1b/hr	800
2.	Feeder, neutrali- zation tank	1	Weigh belt, 14 in. wide x 5 ft long, 1/2 hp, 655 lb/hr, variable speed	7,100
3.	Tank, neutraliza- tion	1	6 ft dia x 7-1/2 ft high, 1,530 gal, open top, four 6 in. baffles, agitator supports, carbon steel	1,000
	Lining		1/4 in. neoprene lining	900
4.	Agitator, neutral- ization tank	1	24 in. dia, 7-1/2 hp, neoprene coated	6,300
5.	Pump, neutrali- zation tank	2	Centrifugal, 48 gpm, 150 ft head, 7-1/2 hp, carbon steel, neoprene lined	5,400
	Subtotal			21,500

	Item			Total materia
_		No.	Description	cost, 1979 \$
1.	Tank, SO ₂ reduction (first)	1	16 ft dia x 24 ft high, 36,100 gal, convex dish head top and bottom, four 16 in. baffles, agitator supports, carbon steel, 30 psig operating pressure	12,400
	Lining		1/4 in. neoprene lining	10,000
2.	Agitator, SO ₂ reduction tank	1	2 turbines, 66 in. dia, 50 hp, neoprene coated	48,000
3.	Sparger, SO ₂ reduction tank	1	5 ft dia ring of 10 in. schedule 40, 316 stainless steel	5,900
4.	Pump, transfer	2	Centrifugal, 6,120 gpm, 60 ft head, 200 hp, carbon steel, neoprene lined	46,200
5.	Tank, SO ₂ reduction (second)	1	16 ft dia x 24 ft high, 36,100 gal, convex dish head top and bottom, four 16 in. baffles, agitator supports, carbon steel, 30 psig operating pressure	12,400
	Lining		1/4 in. neoprene lining	10,000
6.	Agitator, SO ₂ reduction tank	1	2 turbines, 66 in. dia, 50 hp, neoprene coated	48,000
7.	Sparger, SO ₂ reduction	1	5 ft dia ring of 12 in. schedule 40, 316 stainless steel	7,300
8.	Pump, sulfur slurry	2	Centrifugal, 6,540 gpm, 75 ft head, 250 hp, carbon steel, neoprene lined	52,200
9.	Trap, reduction tank offgas	1	4 ft dia x 10 ft high, carbon steel neoprene lined	1, 1,500
.0.	Tank, aging	1	23 ft dia x 24 ft high, 74,600 gal convex dish head top and bottom, four 23 in. baffles, agitator supports, carbon steel, 30 psig operating pressure	, 17,300

TABLE 25 (continued)

	Item	No.	Description	Total material cost, 1979 \$
10.	(continued)			
	Lining		1/4 in. neoprene lining	16,300
11.	Agitator, aging tank	1	92 in. dia, 30 hp, neoprene coated	31,300
	Subtotal			318,800

Area 8--Sulfur Separation and Removal

	Item	No.	Description	Total materia cost, 1979 \$
1.	Tank, flotation	5	5 ft wide x 20 ft long x 5 ft deep, carbon steel, neoprene lined; skimmer with 2 hp motor	55,500
2.	Compressor, flotation tank air	1	1,000 ft 3 /min, 10 psig, 300 hp	71,400
3.	Filter, flotation tank underflow	10	Rotary vacuum, 12 ft dia x 14 ft face, 20 total hp	1,256,600
4.	Pump, filtrate	6	Centrifugal, 1,500 gpm, 40 ft head, 50 hp, carbon steel, neoprene lined	³⁸ ,400
5.	Tank, liquor hold	1	20 ft dia x 30 ft high, 70,500 gal, closed top, four 20 in. baffles, agitator supports, carbon steel	14,200
	Lining		1/4 in. neoprene lining	13,600
6.	Agitator, liquor hold tank	1	2 turbines, 84 in. dia, 40 hp, neoprene coated	41,500
7.	Pump, scrubbing liquor return	6	Centrifugal, 1,590 gpm, 100 ft head, 75 hp, carbon steel, neoprene lined	⁵⁸ ,000
8.	Pump, cooler feed	2	Centrifugal, 60 gpm, 50 ft head, 2 hp, carbon steel, neoprene lined (continued)	4,100

TABLE 25 (continued)

	Item	No.	Description	Total material cost, 1979 \$
9.	Tank, sulfur slurry	1	10 ft dia x 10 ft high, 5,900 gal, closed top, cone bottom, carbon steel	2,900
	Lining		1/4 in. neoprene lining	2,600
10.	Pump, sulfur melter feed	2	Screw type, 100 gpm, 160 ft head, 10 hp, 316 stainless steel	7,900
11.	Melter, sulfur	1	Shell and tube, 1,140 ft ² , 316 stainless steel, insulated	59,900
12.	Tank, sulfur settler	1	9 ft dia x $13-1/2$ ft long, convex dish head top and bottom, 316 stainless steel	10,900
	Insulation		Fiberglass	2,100
	Heater	1	Steam, 100 ft ² , 316 stainless steel	2,600
13.	Flash drum, sulfur settler	1	4 ft dia x 5-1/2 ft long, 316 stainless steel	1,700
14.	Fan, vent line exhaust	1	$1,000 \text{ ft}^3/\text{min}, 5 \text{ hp}$	700
	Subtotal			1,644,600

	0Sulfur	Storage	and	Shipping
4	0Sill Till	SLOTARE	anu	DIITALTIIE

Area	9Sulfur Storage and Shipping					
				Total material		
	Item	No.	Description	cost, 1979 \$		
1.	Pit, sulfur receiving	1	10 ft wide x 10 ft long x 10 ft deep, w/cover, 304 stainless steel	10,400		
	Insulation		Fiberglass	2,500		
	Heater	1	Steam, 100 ft ² , 400 ft of 1 in. schedule 40, 304 stainless steel	2,500		
2.	Pump, sulfur transfer	2	Submerged, high temperature, 15 gpm, 100 ft head, 1-1/2 hp, 316 stainless steel, steam traced, insulated	5,500		

TABLE 25 (continued)

	Item	No.	Description	Total material cost, 1979 \$
3.	Tank, sulfur storage	1	43 ft dia x 41 ft high, 467,100 gal, closed top, 304 stainless steel	147,000
	Insulation		Fiberglass	²⁹ ,500
4.	Heater	1	Steam, 300 ft^2 , 1,200 ft of 1 in. schedule 40, 304 stainless steel	6,400
5.	Pump, sulfur shipping	2	Submerged, high temperature, 60 gpm, 100 ft head, 5 hp, 316 stain-less steel, steam traced, insulate	
	Subtotal			210,900

Area	10	Sulfate	Purge
------	----	---------	-------

ALEa	10==Sufface Purge			
	Item	No.	Description	Total materia cost, 1979
1.	Cooler, sulfate purge stream	1	700 ft ² , 316 stainless steel	³⁵ ,800
2.	Pump, liquor return	2	Centrifugal, 60 gpm, 60 ft head, 2 hp, carbon steel, neoprene lined	4,100
3.	Crystallizer, sulfate	1	3 ft dia x 12 ft high, 4,500 gal, closed top, four 8 in. baffles, agitator supports, 200 ft ² cooling coil	11,200
	Insulation		Polyurethane foam	1,400
4.	Agitator, sulfate crystal- lizer	1	32 in. dia, 10 hp, neoprene coated	12,000
5.	Pump, centrifuge feed	2	Centrifugal, 60 gpm, 60 ft head, 2 hp, carbon steel, neoprene lined	4,100
6.	Centrifuge, sul- fate purge	1	Solid bowl, 36 in. dia x 84 in. long, 200 hp, insulated	176,100

TABLE 25 (continued)

	Item	No.	Description	Total material cost, 1979 \$
7.	Conveyor, sulfate removal	1	Belt, 12 in. wide x 20 ft long, 1 hp, 2,990 lb/hr	3,900
8.	Tank, centrate surge	1	7 ft dia x 7 ft high, 2,000 gal, closed top, carbon steel	1,200
	Lining		Neoprene lining	800
9.	Pump, centrate return	2	Centrifugal, 60 gpm, 60 ft head, 2 hp, carbon steel, neoprene lines	4,100 d
10.	Tank, refrigerant surge	1	8 ft dia x 6 ft high, 2,250 gal, closed top, carbon steel	1,300
	Insulation		Polyurethane foam	800
11.	Pump, cooling water	2	Centrifugal, 247 gpm, 150 ft head 20 hp, carbon steel	, 5,800
12.	Refrigeration system	1	200 tons	47,000
	Subtotal			309,600

	•	•	11 (2 /	າດກ	ora	tion
A	1	1	-и~:	•	-en	era	LIOH

Item	No.	Description	Total material cost, 1979 \$
1. H ₂ S generator	1	300 tons/day, battery limit, installed cost	5,850,000
Subtotal			5,850,000

Area 12--H₂ Generation

Alon	Item	No.	Description	Total material cost, 1979 \$
1.	H ₂ generator	1	20 tons/day, battery limit, installed cost	4,680,000
	Subtotal			4,680,000

Major Process Areas

The citrate process has been divided into the following operating areas:

- 1. Materials handling. Facilities for receiving and storing lime, soda ash, and citric acid are included in this area. The solids handling and storage equipment for crystalline citric acid is eliminated at the demonstration plant by purchasing citric acid as a 50 weight percent liquid. Makeup citric acid solution is added in truckload batched directly to a liquor hold tank.
- 2. Feed preparation. This area includes facilities for producing a solution of makeup soda ash and citric acid.
- 3. <u>Gas handling</u>. Fan location and duct configuration are the same as the limestone slurry process.
- 4. SO₂ absorption. Four packed-tower absorbers with presaturators, effluent hold tanks and pumps are provided. Also included are SO₂ strippers and air compressor. For this study a carbon steel absorber with an FRP liner has been specified. Field applied flakeglass linim of the absorber is specified at the demonstration plant.
- 5. Stack gas reheat. Equipment in this area includes indirect steam reheaters and soot blowers for the coal-fired cases. The oil-fired unit is designed with one direct oil-fired reheater per duct which discharges hot combustion gases directly into the duct.
- 6. Chloride purge. This area includes facilities for neutralizing with lime a purge stream of presaturator liquor for the control of chloride buildup in the system.
- 7. SO₂ reduction. In this area, H₂S gas contacts the SO₂-rich sorbent in reduction (reactor) tanks to produce elemental sulfur. Both the transfer pump for circulating citrate solution between reactors and the sulfur slurry pump to feed solution containing sulfur crystals to the flotation tank have been eliminated in the demonstration-plant design by using gravity flow in a cascading elevation sequence.
- Sulfur separation and removal. Facilities are provided to separate sulfur particles from the slurry liquor and heat the sulfur to the molten state. Based on pilot plant operation data, filtration of regenerated solution has been discontinued. Filtration of the regenerated solution was used in development work on the process but was not considered necessary in scaleup to demonstration plant magnitude. The absorber packing is considered sufficiently washed by solution so that sulfur and ash particles will not foul the system. The regenerated solution underflow from the flotation tank flows by gravity directly to the liquor hold tank.

A flash system for letdown of pressure on the citrate solution leaving the sulfur settler tank has not performed reliably in pilot plant operation. When the citrate solution flashes to a reduced pressure, sufficient water is vaporized to cause citrate sulfate crystals to form in the flash system and cause plugging. The vapors leaving the flash drum are corrosive and must be condensed in order to return to the liquor hold tank. The Bureau of Mines system quenches the hot solution before pressure letdown.

- 9. Sulfur storage and shipping. A receiving pit and sulfur storage tank are provided in this area. A below-ground concrete pit or an insulated carbon steel tank can be used for molten sulfur storage.
- 10. Sulfate purge. A purge stream of scrubbing liquor is routed to the purge treatment area for removal of sodium sulfate from the system. Equipment for the crystallization, separation, and removal of sodium sulfate is included in this area. The Bureau of Mines demonstration unit does not include filtration of the slipstream to the sulfate purge area.

The unit uses an evaporative-cooled crystallizer system to chill the purge stream to about 39°F which produces sodium sulfate decahydrate crystals. The sulfate crystals are screened from the citrate solution. The residual solution removed with the crystals provides an additional purge from the system of accumulated chlorides and entrained solids.

- 11. H₂S generation. This area includes one complete H₂S generation unit with a capacity of 300 tons H₂S per day. The Bureau of Mines system uses an H₂S generator developed and licensed by the Home Oil Company, Ltd., of Canada. The generator design was adapted for use with the Bureau of Mines citrate system in the pilot stage of process development. The generator consumes natural gas, steam and molten sulfur to produce a product gas containing about 78% H₂S on a dry basis. Reductant gas feedstocks other than natural gas can be used. Propane, carbon monoxide, hydrogen, and methanol have been demonstrated. The molten sulfur source is provided by inventory from the citrate process. The generator is provided as a package plant.
- 12. $\underline{\text{H}_2 \ \text{generation}}$. A 20-ton-per-day $\underline{\text{H}_2}$ generation unit using natural gas as feedstock produces the required reducing gas for $\underline{\text{H}_2S}$ production. This area is combined with area 11 at the Bureau of Mines demonstration site.

Storage Capacity

Storage requirements for raw materials and allowances for in-process streams are listed below.

Raw materials:

Lime storage silo - 30 days Soda ash storage bin - 10 days Citric acid storage bin - 15 days

In-process storage:

Makeup solution tank - 4 hours Effluent hold tank - 5 minutes Neutralization tank - 30 minutes SO₂ reduction tanks - 5 minutes each Aging tank - 10 minutes Liquor hold tank - 10 minutes

Product storage:
Sulfur storage tank - 30 days

Chloride Purge

Unlike the waste-producing processes which trap enough chloride in the interstitial water of the settled sludge to maintain a steady-state chloride concentration in the recycle liquor, chlorides in a recovery process can build up over a period of time and thereby cause problems of product quality and equipment corrosion. A purge is added to the citrate process to control chloride buildup in the system. For this study it is assumed that the line neutralized purge stream for chloride control is pumped to the fly ash pond for disposal. However, this method may be environmentally unacceptable if seepage of calcium chloride from the ash pond contaminates underground or nearby water sources. Although several methods of control such as special pond liners and reverse osmosis are available, the scope of this study does not include the evaluation of water treatment systems.

ECONOMIC EVALUATION AND COMPARISON

Based on the design and economic conditions described in Design and Economic Premises section and the material balance and equipment requirements of each process detailed in Systems Estimated, capital investment and annual and lifetime revenue requirements have been projected for the economic evaluation and comparison of the three processes. All the possible design and economic configurations, variations, and combinations encountered in site-specific applications of these processes cannot be covered in this study. However, it is expected that the procedures used in preparing this evaluation are sufficiently discussed to allow adjustment of results to fit the many possible applications.

CAPITAL INVESTMENT

Results

The projected capital investment estimates are calculated in 1979 dollars. Three methods are used for displaying the results.

- 1. Total capital investment requirements tabular investment results for all case variations. For each of the three processes, a summary table is presented listing the projected total capital investment requirements for the case variations, expressed as total dollars and dollars per kW (Tables 26-28).
- Summary of estimated capital investment summarized area costs for all case variations studies. A summary of estimated capital investment is presented in the appendix for each of the projected case variations.
- 3. Total capital investment requirements base case process equipment and installation analysis. Tables 29-31 show summarized area-by-area equipment costs along with installation expense. For all three process displays, these costs are itemized separately and displayed according to the material and labor component of each. The area analysis tables show the distribution of total investment as a percent of direct investment.

TABLE 26. LIMESTONE SLURRY PROCESS

TOTAL CAPITAL INVESTMENT SUMMARY^a

Case	Years remaining life	Total capital investment, \$	\$/kW
			17 2000
Coal-Fired Power Unit			
1.2 lb SO ₂ /MBtu heat input			
allowable emission; onsite			
solids disposal (ponding)			
200 MW E 3.5% sulfur	20	25,057,000	125.3
200 MW N 3.5% sulfur	30	25,461,000	127.3
500 MW E 3.5% sulfur	25	50,120,000	100.2
500 MW N 2.0% sulfur	30	39,641,000	79.3
500 MW N 3.5% sulfur	30	48,728,000	97.5
500 MW N 5.0% sulfur	30	54,621,000	109.2
1,000 MW E 3.5% sulfur	25	74,830,000	74.8
1,000 MW N 3.5% sulfur	30	71,423,000	71.4
Solids disposal by trucking			
500 MW N 3.5% sulfur	30	42,307,000	84.6
90% SO ₂ removal; onsite			
solids disposal (ponding)			
500 MW N 3.5% sulfur	30	50,437,000	100.9
Oil-Fired Power Unit			
0.8 lb SO ₂ /MBtu heat input			
allowable emission; onsite			
solids disposal (ponding)			
500 MW E 2.5% sulfur	25	38,400,000	77.0

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mile from power plant.

Investment requirements for fly ash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE 27. GENERIC DOUBLE-ALKALI PROCESS

TOTAL CAPITAL INVESTMENT SUMMARY^a

Case	Years remaining life	Total capital investment, \$	\$/kW
Case	1116	Investment, 5	Ş/KW
Coal-Fired Power Unit			
1.2 lb SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)			
200 MW E 3.5% sulfur	20	26,006,000	130.0
200 MW N 3.5% sulfur	30	25,477,000	127.4
500 MW E 3.5% sulfur	25	53,675,000	107.4
500 MW N 2.0% sulfur	30	42,110,000	84.2
500 MW N 3.5% sulfur	30	50,551,000	101.1
500 MW N 5.0% sulfur	30	57,579,000	115.2
1,000 MW E 3.5% sulfur	25	85,487,000	85.5
1,000 MW N 3.5% sulfur Solids disposal by trucking	30	79,016,000	79.0
500 MW N 3.5% sulfur 90% SO ₂ removal; onsite solids disposal (ponding)	30	41,335,000	82.7
500 MW N 3.5% sulfur	30	52,404,000	104.8
Oil-Fired Power Unit			
0.8 lb SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)			
500 MW E 2.5% sulfur	25	40,260,000	80.5

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mile from power plant.

Investment requirements for fly ash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE 28. CITRATE PROCESS

TOTAL CAPITAL INVESTMENT SUMMARY^a

Case	Years remaining life	Total capital investment, \$	\$/kW
Coal-Fired Power Unit			
1.2 1b SO ₂ /MBtu heat input allowable emission 200 MW E 3.5% sulfur 200 MW N 3.5% sulfur 500 MW E 3.5% sulfur 500 MW N 2.0% sulfur	20 30 25 30	38,788,000 38,075,000 72,605,000 58,098,000	193.9 190.9 145.2 116.2
500 MW N 3.5% sulfur	30	71,639,000	143.3
500 MW N 5.0% sulfur 1,000 MW E 3.5% sulfur 1,000 MW N 3.5% sulfur 90% SO ₂ removal 500 MW N 3.5% sulfur	30 25 30	82,572,000 109,024,000 106,589,000 74,624,000	165.1 109.0 106.6
Oil-Fired Power Unit 0.8 1b SO ₂ /MBtu heat input allowable emission 500 MW E 2.5% sulfur	25	52,442,000	104.9

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F.

Minimum in-process storage; only pumps are spared.

Investment requirements for fly ash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE 29. LIMESTONE SLURRY PROCESS BASE CASE - DIRECT INVESTMENT PROCESS EQUIPMENT AND INSTALLATION COSTS (k\$)

	Materials handling	Feed preparation	Gas handling	SO ₂ absorption	Stack gas reheat	Solids disposal	Total	% of total direct investment	% of total capital investment
Direct Investment									
Equipment									
Material	486	634	812	3,792	986	47	6,757	26.0	13.9
Labor	106	104	78	773	122	17	1,200	4.6	2.5
Piping and insulation							- •		
Material	13	181	-	1,905	57	885	3,041	11.7	6.2
Labor	3	88	-	599	38	367	1,095	4.2	2.2
Ductwork, chutes, and supports							-,		
Material	-	-	1,562	-	_	-	1,562	6.0	3.2
Labor	-	_	1,187	-	_	_	1,187	4.6	2.4
Concrete foundations			-,				-,10,	7.0	-••
Material	112	55	12	74	_	12	265	1.0	0.5
Labor	452	212	51	207	-	35	957	3.7	2.0
Excavation, site preparation	432	212	J 1	201	-	33	931	3.7	2.0
Railroads, roads, and pond	-	_	_	_	_	8	٥		_
Structural	-	-	-	-	-	0	8	-	-
	25/			161			410		0.0
Material	254	-	-	164	-	1	419	1.6	0.9
Labor	91	-	19	399	-	12	521	2.0	1.1
Electrical									
Material	62	92	1 9 5	148	1	62	560	2.2	1.2
Labor	158	176	347	251	2	183	1,117	4.3	2.3
Instruments									
Material	11	66	46	490	63	6	682	2.6	1.4
Labor	3	16	8	91	12	2	132	0.5	0.3
Paint and miscellaneous									
Material	1	1	-	4	-	3	9	-	-
Labor	7	8	1	21	1	18	56	0.2	0.1
Buildings									
Material	-	39	-	-	-	-	39	0.2	0.1
Labor		68					68	0.3	<u>0.1</u>
Subtotal	1,759	1,740	4,318	8,918	1,282	1,658	19,675	75.7	40.4
ervices, utilities, and miscellaneous							1,180	4.5	2.4
Total excluding pond construction	1,759	1,740	4,318	8,918	1,282	1,658	20,855	80.2	42,8
ond construction							5,145	19.8	10.6
Total direct investment	1,759	1,740	4,318	8,918	1,282	1,658	26,000	100.0	53.4
Percent of total direct investment	6.8	6.7	16.6	34.3	4.9	6.4			

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TABLE 30. GENERIC DOUBLE-ALKALI PROCESS BASE CASE - DIRECT INVESTMENT PROCESS EQUIPMENT AND INSTALLATION COSTS (k\$)

	Materials handling	Feed preparation	Gas handling	SO ₂ absorption	Stack gas reheat	Reaction	Solids separation	Solids disposal	Total	% of total direct investment	% of total capital investment
Direct Investment											
Equipment											
Material	533	288	752	4,006	986	127	907	37	7,636	28.4	15.1
Labor	378	94	68	1,473	122	75	530	16	2,756	10.3	5.5
Piping and insulation											
Material	-	23	-	1,298	57	22	206	481	2,087	7.8	4.1
Labor	-	24	-	620	38	19	179	367	1,247	4.7	2.5
Ductwork, chutes, and supports											
Material	-	-	1,562	-	_	•	-	-	1,562	5.8	3.1
Labor	-	•	1,187	-	-	-	-	-	1,187	4.4	2.3
Concrete foundations											
Material	36	9	12	62	-	8	19	12	158	0.6	0.3
Labor	94	25	51	172	-	22	51	33	448	1.7	0.9
Excavation, site preparation											
Railroads, roads, and pond	-	-	-	-	-	-	27	8	35	0.1	0.1
Structural											
Material	129	-	-	160	-	14	10	2	315	1.2	0.6
Labor	46	-	19	388	_	6	4	6	469	1.8	0.9
Electrical									-		
Material	183	69	195	206	1	13	95	62	824	3.1	1.6
Labor	208	80	347	232	2	38	152	191	1,250	4.7	2.5
Instruments									-,		
Material	58	142	46	462	63	7	101	7	886	3.3	1.8
Labor	28	70	8	86	12	3	46	4	257	1.0	0.5
Paint and miscellaneous											
Material	2	1	-	5	_	2	4	3	17	0.1	-
Labor	15	8	1	36	1	1	17	18	97	0.4	0.2
Buildings					_					-	
Material	-	-	-	_	-	-	4	-	4	-	•
Labor		<u>-</u>		-	 _						<u>-</u>
Subtotal	1,710	833	4,248	9,206	1,282	357	2,352	1,247	21,235	79.4	42.0
Services, utilities, and miscellaneous		<u>-</u>				<u>-</u>			1,274	4.8	2.5
Total excluding pond construction	1,710	833	4,248	9,206	1,282	357	2,352	1,247	22,509	84.2	44.5
Pond construction		<u></u>	<u>.</u>			<u>-</u>			4,241	15.8	8.4
Total direct investment	1,710	833	4,248	9,206	1,282	357	2,352	1,247	26,750	100.0	52.9
Percent of total direct investment	6.4	3.1	15.9	34.4	4.8	1.3	8.8	4.7			

TABLE 31. CITRATE PROCESS BASE CASE - DIRECT INVESTMENT PROCESS EQUIPMENT AND INSTALLATION COSTS (k\$)

	Materials handling	Feed preparation	Gas handling	SO ₂	Stack gas reheat	Chloride purge	SO ₂ reduction	Sulfur separation and removal	Sulfur storage and shipping	Sulfate purge	H ₂ S generation	H ₂ generation	Total	% of total direct investment	% of tota capital investmen
Direct Investment															
quipment					***								11 007	20.0	
Material	202	34 9	888	6,410	986 122	22 4	319 183	1,645 266	211 280	310 83	-	-	11,027 3,260	29.9 8.8	15.4 4.6
Labor	116	,	92	2,105	122	4	103	200	280	83	-	-	3,200	0.0	4.6
iping and insulation		3	_	1,040	57	9	24	88	42	97	-		1,360	3.7	1.9
Material Labor	-	7		960	38	3	56	82	78	73	-	_	1,297	3.5	1.8
	-	,	•	900	30	,	30	02	70	/3	-	-	1,277	3.7	1.0
uctwork, chutes, and supports Material		_	1,406	-	-	_	200	86	_	-	_	_	1,692	4.6	2.4
Labor			1,068		_		150	64			_	-	1,282	3.5	1.8
oncrete foundations	=	=	1,000	_	_	_	130	•	_	=	_	_	1,101	3.5	1.0
Material	24	2	6	78	_	1	14	12	10	4	_	_	151	0.4	0.2
Labor	64	4	15	212	_	3	36	31	26	11	-	_	402	1.1	0.6
xcavation, site preparation	0-4	•	1,5			•	30	31		**			402	***	0.0
Railroads, roads, and pond	_	_	_	-	_	1	-	-	17	_	_	_	18	-	_
tructural						•			• *				10		
Material	52	2	12	380	_	1	13	2	-	-	-	_	462	1.3	0.6
Labor	32	ī	7	170	_	ī	7	2		1	-	-	221	0.6	0.3
lectrical		•	•	2,0		-	•	-		•				•••	0.5
Material	61	11	276	91	1	13	45	162	31	91	_	_	782	2.1	1.1
Labor	114	19	268	259	ž	19	30	176	44	259	-	_	1,190	3.2	1.7
nstruments	114	.,	200	237	-	• • •		1,0		-55			1,170	7.2	1.,
Material	57	19	37	369	63	10	13	40	20	40	-	-	668	1.8	0.9
Labor	31	ii	17	181	12	5	7	20	10	20	-	-	314	0.9	0.4
sint and miscellaneous			••			-								••,	0.4
Material	4	1	_	5	-	1	1	1	1	1	-	-	15		_
Labor	13	Š	1	25	1	ă.	2	4	2	4	-	-	61	0.2	0.1
ildings		-	•		-	-		-		•					
Material	_	3	-		_	-	-	20	-	-	_	-	23	0.1	-
Labor	-	i	_	_	-	_	_	5	-	-	-	-	6	-	_
attery limits		•						-			5,850	4,680	10,530	28.6	14.7
,	_	_				_									
Subtotal	770	132	4,093	12,285	1,282	97	1,100	2,706	772	994	5,850	4,680	34,761	94.3	48,5
rvices, utilities, and miscellaneous	-	<u>-</u>	<u> </u>			<u>-</u>	<u> </u>		<u></u>	<u>-</u>		<u></u>	2,086	_ 5.7	2,9
Total direct investment	770	132	4,093	12,285	1,282	97	1,100	2,706	772	994	5,850	4,680	36,847	100.0	51.4
Percent of total direct investment	2.1	0.4	11.1	33.2	3.5	0.3	3.0	7.3	2.1	2.7	15.9	12.7			

Discussion of Results

The capital investment costs for limestone and double alkali are quite close; the relative simplicity of limestone scrubbing offset by smaller pond requirements in double alkali. The projected total investments for the limestone slurry process range from \$25,057,000 (\$125.3/kW) for an existing 200-MW 3.5% sulfur coal-fired unit to \$74,830,000 (\$74.8/kW) for an existing 1,000-MW 3.5% sulfur coal-fired unit. Investments for the generic double-alkali process range from \$25,477,000 (\$127.4/kW) for a new 200-MW 3.5% sulfur coal-fired unit to \$85,487,000 (\$85.5/kW) for an existing 1,000-MW 3.5% sulfur coal-fired unit.

Understandably, the product-producing citrate process has greater capital investment requirements than the waste-producing processes. The projected capital investments for citrate range from \$38,075,000 (\$190.9/kW) for a new 200-MW 3.5% sulfur coal-fired unit to \$109,024,000 (\$109.0/kW) for an existing 1,000-MW 3.5% sulfur coal-fired unit.

The summarized capital investment results for the three processes are shown in Figures 14-16 which indicate the effect of power unit size and sulfur content of coal on the total fixed investment for units of different status (new or existing). The effects of similar variations on capital investment in dollars per kW are given in Figures 17-19.

A variation of the base case was prepared for the waste-producing processes in which the waste solids are disposed of by trucking to the disposal area. This is the single case variation comparison between limestone and double alkali in which double alkali has a lower investment requirement (\$41,353,000 for double alkali and \$42,307,000 for limestone). While the double-alkali process includes thickening and filtration as a normal process step, it must be added to the limestone system to produce a truckable filter cake. In addition, limestone FGD produces more waste solids because of a higher stoichiometric ratio of calcium to \$02 removed and it includes a more expensive feed preparation area. These factors combine to produce a limestone investment that is 2.4% higher than the double-alkali case. When the double-alkali disposal-by-trucking case is compared with the limestone base case (slurry disposal by ponding) the limestone capital investment requirement is 18% higher. Table 32 is a comparison of capital investment costs for the disposal alternatives.

TABLE 32. COMPARISON OF INVESTMENT

REQUIREMENTS FOR SOLIDS DISPOSAL ALTERNATIVES^a

	Slurry ponding, \$	Filter cake	Investment de	erease ernative
Process	(base case)	trucking, \$	\$	%
Limestone	48,728,000	42,307,000		13.2
Double alkali	50,551,000	41,335,000	9,216,000	18.2

a. Base case conditions: Pond and cake disposal are both 1 mile from scrubbing facilities.
95

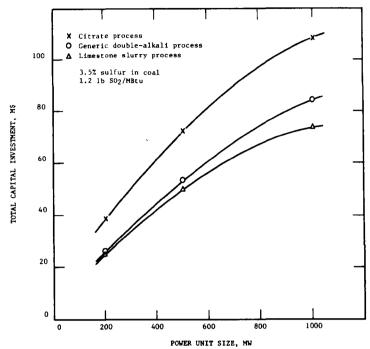


Figure 14. All processes. Effect of power unit size on total capital investment for new coal-fired units.

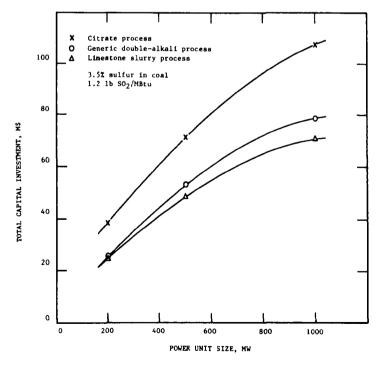


Figure 15. All processes. Effect of power unit size on total capital investment for existing coal-fired units.

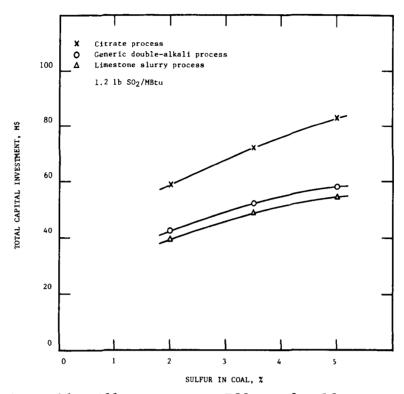


Figure 16. All processes. Effect of sulfur content of coal on total capital investment for new 500-MW units.

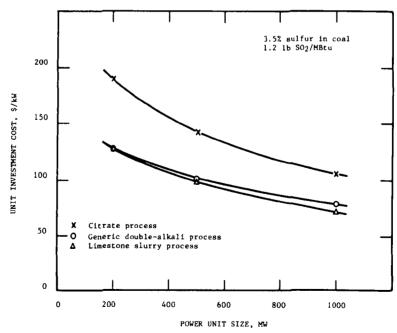


Figure 17. All processes. Effect of power unit size on unit investment cost for new coal-fired units.

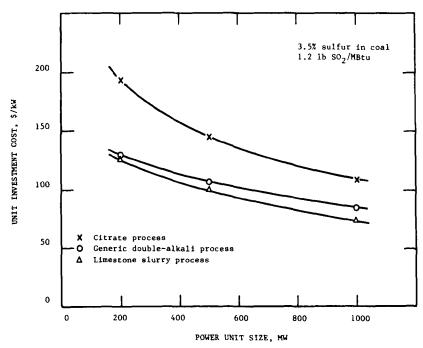


Figure 18. All processes. Effect of power unit size on unit investment cost for existing coal-fired units.

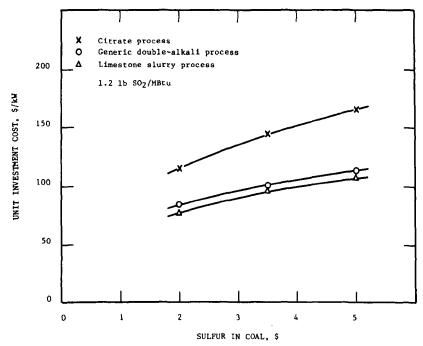


Figure 19. All processes. Effect of sulfur content of coal on unit investment cost for new 500-MW units.

The difference in investment requirements for SO₂ removal at base case conditions (1.2 lb SO₂/MBtu heat input allowable emissions) versus 90% SO₂ removal for each process is displayed in Table 33. Capital investment increases range from 3.5% to 4.2% or from an increase of \$1,709,000 add1-tional capital required for limestone to \$2,985,000 additional capital required for citrate.

TABLE 33. COMPARISON OF INVESTMENT REQUIREMENTS FOR DIFFERENT SO_2 REMOVAL LEVELS

	Projected total ca investment requirement 500-MW new 3.5% sulfur coa	Investment increase resulting from increased SO		
	1.2 1b SO ₂ /MBtu heat	90%	removal to	90%
Process	input allowable emission	SO ₂ removal	\$	7
Limestone	48,728,000	50,437,000	1,709,000	3.5
Double alkali	50,551,000	52,404,000	1,853,000	3.7
Citrate	71,639,000	74,624,000	2,985,000	4.2

Differences in capital investment requirements between processes, between new and existing units, or between sulfur content of fuels can best be analyzed by studying the specific unit areas within the processes. Base case summarized area equipment-and-installation breakdowns which give component costs for the three processes are shown in Tables 29-31. In each process the greatest fraction of the investment cost is attributed to the SO₂ absorption area, approximately 33% to 34% of the direct investment for base case conditions. Gas handling (contributing from 11% to 17% for the base case) and pond construction (contributing from 16% in double alkali to 20% in the limestone base case) also are significant portions of the direct investment. In the citrate process, the H₂ and H₂S generation plants represent approximately 29% of the direct investment. Special purging of chlorides in systems producing salable abatement products such as the citrate process accounts for only 0.3% of the direct investment in the citrate base case.

In a comprehensive area-by-area comparison of capital investment requirements for all case variations (see tables in appendix) the SO₂ absorption area cost ranges from 29% to 43% of the direct investment. The effect of plant age on investment costs becomes important in waste-producing processes where pond size and construction costs depend on remaining plant life. For example, the cost of pond construction for the double-alkali 200-MW new coal-fired unit (30-year remaining life) is \$2,141,000 while the pond construction cost for a 200-MW existing coal-fired unit (20-year remaining life) is \$1,197,000. The H₂ and H₂S generation plants represent 22% to 33% of the citrate direct investment. Chloride purge facilities account for less than 1% of citrate direct investment for all case variations.

Capital investment and revenue requirements are now available for a number of limestone FGD units. A citrate system and several double-alkali units are under construction. As costs for these become available, comparisons with the results of this study are to be expected. Care must be taken in these comparisons to understand the scope of the work and to determine the areas that may not be directly comparable. The base case (500-MW 3.5% sulfur new coal-fired unit) capital investment for limestone slurry scrubbing derived in this study is \$97.5/kW. As an example of how changes in scope affect the capital investment, Table 34 defines area-cost increases which total \$96/kW or a new capital investment for limestone of \$193.5/kW. Contractor bid competition, construction experience, and changes and refinements in process design will affect the actual costs of installing and operating a large-scale system. Ultimately, demonstrated performance of any FGD system will produce the necessary data for full understanding of process costs.

REVENUE REQUIREMENTS

Results

Annual and lifetime revenue requirements for the three processes are calculated on a regulated economics basis. The projected annual revenue requirements are calculated in 1980 dollars.

Annual Revenue Requirements--

Three methods for displaying results are presented.

- 1. Summary of average annual revenue requirements tabular revenue requirement results for all case variations. For each of the three processes, a summary table is presented listing the projected total average annual revenue requirements for the case variations, expressed as total dollars and equivalent unit costs (Tables 35-37).
- 2. Projected average annual revenue requirements all case variations for three processes. Summary tables showing changes in process costs and the corresponding equivalent unit revenue requirements are presented in the appendix for the case variations studied for each process. The distribution of revenue requirement components is expressed as a percent of the total average annual revenue requirements.
- 3. Average annual revenue requirements base case operating breakdown analysis. Summarized by operating area, revenue requirements are projected according to direct cost components (Tables 38-40).

Lifetime Revenue Requirements--

Results of the lifetime economic projections are presented.

- 1. Tables 41-43 summarizing the lifetime economics results for each case variation.
- 2. Computer printouts of the detailed year-by-year cash flow analyses, displayed in the appendix, for each case variation of each process.

TABLE 34. LIMESTONE SLURRY PROCESS

ADDITIONAL INVESTMENT REQUIRED FOR MODIFIED PROJECT SCOPE

	Investment required, \$/kW
Base case - limestone slurry process: 500-MW new unit burning coal containing 3.5% sulfur, 16% ash, 10,500 Btu/lb heat value; 1.2 lb SO ₂ allowable emission per MBtu heat input; 0.1% liquid entrainment in cleaned stack gas; 30-year life, 127,500-hr operation; no redundancy; 20% contingency; onsite solids disposal; mid-1979 cost basis	97.5
	Additional investment required, \$/kW
Modified case: 500-MW new unit burning coal containing 6% sulfur, 16% ash, 10,500 Btu/lb heat value; 90% SO ₂ removal; 0.3% liquid entrainment in cleaned stack gas; 30-year life, 127,500-hr operation; 50% redundancy; onsite solids disposal; mid-1979 cost basis	
Investment increases due to:	
Increased raw material handling Larger waste disposal area and pond 50% redundancy of ball mills, scrubbers, and	18.3 46.9
other equipment	30.8
Total increase in capital investment	96.0

TABLE 35. LIMESTONE SLURRY PROCESS

ANNUAL REVENUE REQUIREMENTS SUMMARY^a

Case	Years remaining life	Total annual revenue requirements	Mills/kWh	\$/ton (bbl) of coal (oil) burned	\$/MBtu heat input	\$/ton sulfur removed
Coal-Fired Power Unit						
1.2 lb SO ₂ /MBtu heat input						
allowable emission; onsite						
solids disposal (ponding)						
200 MW E 3.5% sulfur	20	7,479,400	5.34	11.81	0.56	506.05
200 MW N 3.5% sulfur	30	7,153,200	5.11	11.67	0.56	499.87
500 MW E 3.5% sulfur	25	14,789,400	4.23	9.65	0.46	413.34
500 MW N 2.0% sulfur	30	11,624,900	3.32	7.75	0.37	717.59
500 MW N 3.5% sulfur	30	14,101,900	4.03	9.40	0.45	402.91
500 MW N 5.0% sulfur	30	16,032,200	4.58	10.69	0.51	295.91
1,000 MW E 3.5% sulfur	25	23,241,200	3.32	7.75	0.37	332.02
1,000 MW N 3.5% sulfur	30	21,874,300	3.12	7.54	0.36	323.25
Solids disposal by trucking		, , ,			-	
500 MW N 3.5% sulfur	30	15,172,400	4.33	10.11	0.48	433.50
90% SO ₂ removal; onsite solids disposal (ponding)						
500 MW N 3.5% sulfur	30	14,651,300	4.19	9.77	0.47	358.22
Oil-Fired Power Unit						
0.8 lb SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)						
500 MW E 2.5% sulfur	25	11,446,600	3.27	2.15	0.35	770.81

a. Basis

Midwest plant location, 1980 revenue requirements.

Power unit on-stream time, 7,000 hr/yr.

Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of fly ash excluded.

TABLE 36. GENERIC DOUBLE-ALKALI PROCESS

ANNUAL REVENUE REQUIREMENTS SUMMARY^a

Case	Years remaining life	Total annual revenue requirements	Mills/kWh	<pre>\$/ton (bb1) of coal (oil) burned</pre>	\$/MBtu heat input	\$/ton sulfur removed
Coal-Fired Power Unit						
1.2 lb SO ₂ /MBtu heat input						
allowable emission; onsite						
solids disposal (ponding)						
200 MW E 3.5% sulfur	20	7,553,000	5.40	11.92	0.57	511.03
200 MW N 3.5% sulfur	30	7,169,100	5.12	11.69	0.56	500.99
500 MW E 3.5% sulfur	25	15,441,700	4.41	10.07	0.48	431.57
500 MW N 2.0% sulfur	30	11,335,300	3.24	7.56	0.36	699.71
500 MW N 3.5% sulfur	30	14,676,000	4.19	9.78	0.47	419.31
500 MW N 5.0% sulfur	30	17,741,900	5.07	11.83	0.56	327.46
1,000 MW E 3.5% sulfur	25	25,750,900	3.68	8.58	0.41	367.87
1,000 MW N 3.5% sulfur	30	24,147,700	3.45	8.33	0.40	356.84
Solids disposal by trucking						
500 MW N 3.5% sulfur	30	14,293,900	4.08	9.53	0.45	408.40
90% SO ₂ removal; onsite						
solids disposal (ponding)						
500 MW N 3.5% sulfur	30	15,438,800	4.41	10.29	0.49	387.90
Dil-Fired Power Unit						
0.8 lb SO ₂ /MBtu heat input allowable emission; onsite solids disposal (ponding)						
500 MW E 2.5% sulfur	25	11,128,400	3.18	2.09	0.34	749.39

a. Basis

Midwest plant location, 1980 revenue requirements.

Power unit on-stream time, 7,000 hr/yr.

Meach san releas to 1750.

involvent and revenue requirement for removal and disposal of fly ash excluded.

TABLE 37. CITRATE PROCESS

ANNUAL REVENUE REQUIREMENTS SUMMARY^a

Case	Years remaining life	Total annual revenue requirements	Mills/kWh	\$/ton (bb1) of coal (oi1) burned	\$/MBtu heat input	\$/ton sulfur removed	\$/ton sulfur recovered
Coal-Fired Power Unit							
1.2 lb SO ₂ /MBtu heat input							
allowable emission							
200 MW E 3.5% sulfur	20	12,289,200	8.78	19,40	0.92	831.47	859.99
200 MW N 3.5% sulfur	30	11,670,800	8.34	19.03	0.91	815.56	843.26
500 MW E 3.5% sulfur	25	23,174,000	6.62	15.11	0.72	647.68	669.96
500 MW N 2.0% sulfur	30	17,091,700	4.88	11.39	0.54	1,055.04	1,097.73
500 MW N 3.5% sulfur	30	22,538,000	6.44	15.02	0.72	643.94	654.98
500 MW N 5.0% sulfur	30	27,513,400	7.86	18.34	0.87	507.81	528.60
1,000 MW E 3.5% sulfur	25	36,933,500	5.28	12.31	0.59	527.62	545.71
1,000 MW N 3.5% sulfur	30	35,602,400	5.09	12.28	0.58	526.12	544.21
90% SO2 removal							• • • • • • • • • • • • • • • • • • • •
500 MW N 3.5% sulfur	30	23,812,400	6.80	15.87	0.76	598.30	617.70
Oil-Fired Power Unit							
0.8 lb SO ₂ /MBtu heat input							
500 MW E 2.5% sulfur	25	16,091,700	4.60	3.02	0.50	1,042.88	1,060.76

a. Basis

Midwest plant location, 1980 revenue requirements.

Power unit on-stream time, 7,000 hr/yr.

Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of fly ash excluded.

TABLE 38. LIMESTONE SLURRY PROCESS BASE CASE
ANNUAL REVENUE REQUIREMENTS DIRECT COSTS

	Total	- 10 .	Materials handling	Feed preparation	Gas _handling	SO ₂	Stack gas reheat	Solids disposal	Services, utilities, and miscellaneous	Pond construction	Total annual quantities	Total annual dollars	<pre>1 of average annual revenuent:</pre>
Total direct investment, \$ Total depreciable investment, \$ Total capital investment, \$	26,000,000 46,677,000 48,728,000)	1,759,000	1,740,000	4,318,000	8,918,000	1,282,000	1,658,000	1,180,000	5,145,000		26,000,000	
Direct Costs	Unit cost, \$	Raw material											
Delivered rsw materials Limestone Annual quantity, tons Annual cost, \$	7.00/ton	158,300 1,108,100									158,300	1,108,100	<u>7.86</u>
Subtotal raw materials cost		1,108,100										1,108,100	7.86
Conversion costs Operating labor and supervision Annual quantity, man-hr Annual cost, \$ Utilities	12.50/man-hr		4,200 52,500	6,600 82,500	1,690 21,100	8,500 106,200	1,500 18,800	3,500 43,800	:	Ī	25,990	324,900	2.30
Stem Annual quantity, MBtu Annual cost, \$	2.00/MBtu		:	-	:	:	489,800 979,600	-	-	-	489,800	979,600	6.95
Process water Annual quantity, kgal Annual cost, \$	0.12/kgal		-	-	-	247,400 29,700	•	:	:	:	247,400	29,700	0.21
Electricity Annual quantity, kWh Annual cost, \$ Haintenance (labor and material)	0.029/kWh		770,000 22,300	4,458,000 129,300	26,179,000 759,200	24,171,000 700,900	-	637,000 18,500	455,000 13,200	-	56,670,000	1,643,400	11.65
Annual cost, \$	17.00/man-hr		140,700	139,200	345,500	713,400	102,600	132,600	94,400	154,400		1,822,800	12.93
Analyses Annual quantity, man-hr Annual cost, \$	17.00/man-nr	1,500 25,500		<u>:</u>	<u> </u>	1,880 32,000	<u>:</u>	380 6,400			3,760	63,900	0.45
Subtotal conversion costs		25,500	215,500	351,000	1,125,800	1,582,200	1,101,000	201,300	107,600	154,400		4,864,300	34.49
Total direct costs		1,133,600	215,500	351,000	1,125,800	1,582,200	1,101,000	201,300	107,600	154,400		5,972,400	42.35
Percent of total direct		18.98	3,61	5.88	18.85	26.49	18.43	3.37	1.80	2.59			

TABLE 39. GENERIC DOUBLE-ALKALI PROCESS BASE CASE
ANNUAL REVENUE REQUIREMENTS DIRECT COSTS

	Total		Materials handling	Feed preparation	Gas handling	SO ₂	Stack gas reheat	Reaction	Solids separation	Solids disposal	Services, utilities, and miscellaneous	Pond construction	Total annual quantities	Total annual dollars	% of average annual revenu requirements
Total direct investment, \$ Total depreciable investment, \$ Total capital investment, \$	26,750,000 48,530,000 50,551,000	•	1,710,000	833,000	4,248,000	9,206,000	1,282,000	357,000	2,352,000	1,247,000	1,274,000	4,241,000		26,750,000	
Direct Costs	Unit cost, \$	Rav material													
Delivered raw materials Lime Annual quantity, tons Annual cost, \$	42.00/tox	63,600 2,671,200											63,600	. 2,671,200	18.20
Sode ash Annual quantity, tons Annual cost, \$	90.00/ton	6,060 545,400											6,060	545,400	3.72
Subtotal raw materials cost		3,216,600												3,216,600	21.92
Conversion costs: Operating labor and supervision Annual quantity, man-hr Annual cost, \$ Utilities	12.50/mam-hr		4,200 52,500	6,600 82,500	1,700 21,200	7,000 87,500	1,500 18,800	1,750 21,900	8,250 103,100	3,500 43,800	:	Ë	34,500	431,300	2.94
Steam Ammual quantity, MBtu Ammual cost, \$	2.00/MBtu		:	•	-	•	489,800 979,600	:	-	:	:	•	489,800	979,600	6.67
Process water Annual quantity, kgal Annual cost, \$	0.12/kga1		121,800 14,600	-	:	46,620 5,600	:	:	44,100 5,300	28,980 3,500	-	:	241,500	29,000	0.20
Electricity Annual quantity, kWh Annual cost, \$	0,029/kWh		1,078,000 31,300	903,000 26,200	17,872,000 518,300	5,369,000 155,700	:	819,000 23,700	2,100,000 60,900	504,000 14,600	455,000 13,200	:	29,100,000	843,900	5.75
Maintenance (labor and material) Annual cost, \$ Analyses	17.00/man-hr		68,400	33,300	169,900	368,200	51,300	14,300	94,100	49,900	51,000	127,200		1,027,600	7.00
Amnual quantity, hr Annual cost, \$		1,500 25,500	<u> </u>	<u>:</u>	<u>.</u>	1,700 28,900		700 11,900	280 4,700	380 6,500	<u>-</u>	<u> </u>	4,560	77,500	0.53
Subtotal conversion costs		25,500	166,800	142,000	709,400	645,900	1,049,700	71,800	268,100	118,300	64,200	127,200		3,388,900	23.09
Total direct costs		3,242,100	166,800	142,000	709,400	645,900	1,049,700	71,800	268,100	118,300	64,200	127,200		6,605,500	45.01
Percent of total direct		49,08	2.52	2.15	10.74	9.78	15.89	1.09	4.06	1.79	0.97	1.93			

TABLE 40. CITRATE PROCESS BASE CASE

ANNUAL REVENUE REQUIREMENTS DIRECT COSTS

	Total		Materials handling	Feed preparation	Gas handling	SO ₂	Stack gas reheat	Chloride purge	SO ₂ reduction	Sulfur separation and removal	Sulfur storage and shipping
Total direct investment, \$ Total depreciable investment, \$ Total capital investment, \$	36,847,000 69,520,000 71,639,000		770,000	132,000	4,093,000	12,285,000	1,282,000	97,000	1,100,000	2,706,000	772,000
Direct Costs	Unit cost, \$	Raw material									
Délivered raw materials											
Lime	42.00/ton										
Annual quantity, tons		2,870									
Annual cost, \$		120,500									
Soda ash	90.00/ton										
Annual quantity, tons		2,630									
Annual cost, \$		236,700									
Citrate	1,340.00/ton	230									
Annual quantity, tons		308,200									
Annual cost, \$ Natural gas	3.50/kft ³	300,200									
Annual quantity, kft ³	3.30/ KIL	1,050,000									
Annual cost, \$		3,675,000									
Catalyst		-,,									
Annual quantity, tons		-									
Annual cost, \$		21,000									
Subtotal raw materials cost		4,361,400									
Conversion costs											
Operating labor and supervision Annual quantity, man-hr Annual cost, \$	12.50/man-hr		2,000 25,000	1,750 21,900	1,700 21,200	7,000 87,500	1,500 18,700	1,750 21,900	9,240 115,500	9,240 115,500	3,500 43,800
Utilities			•	•	•	•	•	•	•	•	•
Steam	2.00/MBtu										
Annual quantity, MBtu			-	•	-	•	489,800	-	•	180,700	68,600
Annual cost, \$			-	· -	-	-	979,600	-	-	361,400	137,200
Process water	0.06/kgal										
Annual quantity, kgal			-	-		197,400	-	•	-	400	-
Annual cost, \$ Electricity	0,029/kWh		•	•	-	11,900	-	-	-	-	-
Annual quantity, kWh	0,0237 KWII		367,600	127,400	41,846,000	5,553,100	_	118,500	3,063,700	5,641,800	139,400
Annual cost, \$			10,700	3,700	1,213,600	161,000	-	3,400	88,900	163,600	4,000
Maintenance (labor and material)				,,,,,	-,,	,		•	•	•	•
Annual cost, \$			46,200	7,900	245,600	737,100	76,900	5,800	66,000	162,400	46,300
Analyses	17.00/man-hr					•					
Annual quantity, man-hr		400	-	400	-	1,750	-	500	2,750	1,400	400
Annual cost, \$		6,800		6,800		29,700		<u>8,500</u>	46,800	23,800	6,800
Subtotal conversion costs		6,800	81,900	40,300	1,480,400	1,027,200	1,075,200	39,600	317,200	826,700	238,100
Total direct costs		4,368,200	81,900	40,300	1,480,400	1,027,200	1,075,200	39,600	317,200	826,700	238,100
Percent of total direct											
costs		37.21	0.70	0.34	12.61	8.75	9.16	0,34	2.70	7.04	2.03

TABLE 40 (continued)

	Sulfate purge	H ₂ S generation	H ₂ generation	Services, utilities, and miscellaneous	Byproduct sales revenue	Total annual quantities	Total annual dollars	% of average annual revenue requirements
Total direct investment, \$ Total depreciable investment, \$ Total capital investment, \$	994,000	5,850,000	4,680,000	2,086,000			36,847,000	
Direct Costs								
Delivered raw materials								
Lime Annual quantity, tons Annual cost, \$						2,870	120,500	0.53
Soda ash Annual quantity, tons Annual cost, \$ Citrate						2,630	236,700	1.05
Annual quantity, tons Annual cost, \$ Natural gas						230	308,200	1.37
Annual quantity, kft ³ Annual cost, \$ Catalyst						1,050,000	3,675,000	16.31
Annual quantity, tons Annual cost, \$						-	21,000	0.09
Subtotal raw materials cost							4,361,400	19.35
Conversion costs								
Operating labor and supervision Annual quantity, man-hr Annual cost, \$ Utilities	9,240 115,500	14,000 175,000	7,000 87,500	Ī	:	67,920	849,000	3.77
Steam Annual quantity, MBtu Annual cost, \$	-	121,000 242,000	175,800 351,600	<u>-</u> -	:	1,035,900	2,071,800	9.19
Process water Annual quantity, kgal Annual cost, \$	107,200 6,400	507,500 30,500	1,680,000 100,800	-	-	2,492,500	149,600	0.66
Electricity Annual quantity, kWh Annual cost, \$	6,090,500 176,600	1,535,000 44,500	1,085,000 31,500	532,000 15,400	-	66,100,000	1,916,900	8.51
Maintenance (labor and material) Annual cost, \$ Analyses	59,600	351,000	280,800	125,200	-		2,210,800	9.81
Annual quantity, man-hr Annual cost, \$	500 8,500	2,000 34,000	500 8,500	<u>-</u>	-	10,600	180,200	0,80
Subtotal conversion costs	366,600	877,000	860,700	140,600			7,378,300	32.74
Total direct costs	366,600	877,000	860,700	140,600			11,739,700	52.09
Percent of total direct costs	3.12	7.47	7.33	1.20				

TABLE 41. LIMESTONE SLURRY PROCESS

ACTUAL AND DISCOUNTED CUMULATIVE TOTAL AND UNIT INCREASE (DECREASE)

IN COST OF POWER OVER THE LIFE OF THE POWER UNITa

					increase (dec nue requireme:			L		rease (decrea e requirement	
Case	Years remaining life	Cumulative actual net increase (decrease) in cost of power, \$	\$/ton (bbl) of coal (oil) burned	Mills/kWh	\$/MBtu heat input	\$/ton of S removed	Cumulative present worth net increase (decrease) in cost of power, b \$	\$/ton (bbl) of coal (oil) burned	Mills/kWh	\$/MBtu heat input	\$/ton of S remove
Coal-Fired Power Unit											
1.2 lb SO2/MBtu heat input											
allowable emission; onsite											
solids disposal (ponding)											
200 MW E 3.5% S	20	115,734,600	22.25	10.06	105.94	948.64	52,811,700	20.52	9.28	0.98	875.8
200 MW N 3.5% S	30	183,304,700	16.41	7.19	78.13	702.32	65,253,700	14.99	6.56	0.71	642.20
500 MW E 3.5% S	25	300,128,600	14.81	6.49	70.54	633.85	122,034,600	13.29	5.82	0.63	569.19
500 MW N 2.0% S	30	293,271,500	10.73	4.60	51.11	992.46	104,931,000	9.85	4.22	0.47	911.6
500 MW N 3.5% S	30	357,374,000	13.08	5.61	62.29	560.59	127,709,200	11.99	5.14	0.57	513.92
500 MW N 5.0% S	30	405,112,800	14.83	6.35	70.61	410.45	144,837,500	13.60	5.83	0.65	376.40
1,000 MW E 3.5% S	25	462,118,100	11.66	5.00	55.51	499.59	188,891,100	10.52	4.51	0.50	450.71
1,000 MW N 3.5% S	30	544,862,300	10.32	4.27	49.12	441.72	195,672,000	9.50	3.94	0.45	407.06
Solids disposal by trucking											
500 MW N 3.5% S	30	372,822,400	13.65	5.85	64.98	591.78	132,750,600	12,47	5.34	0.59	540.52
90% SO ₂ removal; onsite solids disposal (ponding) 500 MW N 3.5% S	30	371,004,000	13.58	5.82	64.66	497.66	132,602,400	12,45	5.34	0.59	456.62
Oil-Fired Power Unit	30	371,004,000	13.30	3.02	04.00	437.00	132,002,400		3.34	•••	430.00
0.8 lb SO ₂ /MBtu heat input allowable emission; onsite											
solids disposal (ponding) 500 MW E 2.5% S	25	231,792,200	3.29	5.01	54.48	1,182.61	94,271,900	2.96	4.50	0.49	1,062.82

a. Basis

Midwest plant location, 1980 revenue requirements.

Over previously defined unit operating profile. 30-yr life; 7,000 hr - 10 yr, 5,000 hr - 5 yr, 3,500 hr - 5 yr, 1,500 hr - 10 yr.

Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of fly ash excluded.

Limestone raw material cost, \$7/ton.

Constant labor cost assumed over life of project.

b. Discounted at 10% to initial year.

c. Equivalent to discounted process cost over life of power units.

TABLE 42. GENERIC DOUBLE-ALKALI PROCESS

ACTUAL AND DISCOUNTED CUMULATIVE TOTAL AND UNIT INCREASE (DECREASE)

IN COST OF POWER OVER THE LIFE OF THE POWER UNITa

					increase (dec nue requireme					ase (decrease e requirement	
Case	Years remaining life	Cumulative actual net increase (decrease) in cost of power, \$	\$/ton (bbl) of coal (oil) burned	Mills/k\h	\$/MBtu heat input	\$/ton of S removed	Cumulative present worth net increase (decrease) in cost of power, b \$	\$/ton (bbl) of coal (oil) burned	Mills/kWh	\$/MBtu heat input	\$/ton of S_remove
Coal-Fired Power Unit											
1.2 lb SO ₂ /MStu heat input allowable emission; onsite solids disposal (ponding)											
200 MH E 3.57 S	20	116,680,000	22,43	10.15	106.80	956.39	53,388,600	20.75	9.39	0.99	885.38
200 MS N 3.5% S	30	182,336,300	16.32	7.15	77.72	698.61	65,224,800	14,98	6.56	0.71	641.9
500 MW E 3.5% S	25	312,313,600	15.41	6,75	73.40	659.59	127,562,500	13.89	6.09	6.66	594.9
500 MW N 2.0% S	30	290,205,200	10.62	4.55	50.58	982.08	103,925,200	9.76	4.18	0.46	902.9
500 MW N 3.5% S	30	368,601,500	13.49	5.78	64.24	578.20	132,472,900	12,44	5,33	0.59	533.0
500 MW N 5.0% S	30	439,183,100	16.07	6.89	76.55	444.97	158,278,400	14,86	6.37	0,71	411.3
1,000 MW E 3.5% S	25	511,039,500	12.89	5.52	61.39	552.48	209,774,100	11,68	5.00	0.56	500.5
1,000 MW N 3.5% S	30	596,859,100	11,30	4.68	53.81	484.27	215,525,300	10.47	4.34	0.50	448.5
Solids disposal by trucking 500 MW N 3.5% S	30	348,993,900	12.77	5.47	60.83	547.44	125,275,900	11.76	5.04	0.56	504.13
90% SO2 removal; onsite solids disposel (ponding) 500 MW N 3.5% S	30	386,333,300	14.14	6,06	67.33	533.24	138,947,500	13.05	5,59	0,62	491.85
Oil-Fired Power Unit											
0.8 1b SO2/MBtu heat input allowable emission; onsite solids disposal (ponding)											
500 MW E 2.5% S	25	228,580,000	3.25	4.94	53.72	1,166,22	93,023,600	2.92	4.44	0.48	1,048.7

a. Basis

Midwest plant location, 1980 revenue requirements.

Over previously defined unit operating profile. 30-yr life; 7,000 hr - 10 yr, 5,000 hr - 5 yr, 3,500 hr - 5 yr, 1,500 hr - 10 yr.

Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of fly ash excluded. Constant labor cost assumed over life of project.

b. Discounted at 10% to initial year.

c. Equivalent to discounted process cost over life of power units.

TABLE 43. CITRATE PROCESS

ACTUAL AND DISCOUNTED CUMULATIVE TOTAL AND UNIT INCREASE (DECREASE)

IN COST OF POWER OVER THE LIFE OF THE POWER UNITa

					increase (de enue requirem		Cumulative present worth net increase (decrease) in cost of power, b \$	Levelized increase (decrease) in unit revenue requirement ^c				
Case	Years remaining life	Cumulative actual net increase (decrease) in cost of power, \$	\$/ton (bbl) of coal (oil) burned	Mills/kWh	\$/MBtu heat input	\$/ton of S removed		\$/ton (bbl) of coal (oil) burned	Mills/kWh	\$/MBtu heat input	\$/ton of S remove	
Coal-Fired Power Unit												
1.2 lb SO ₂ /MBtu heat input allowable emission												
200 MW E 3.5% S	20	185,604,300	35.68	16.14	169.89	1,521.35	84,862,500	32.98	14.92	1.57	1,407.3	
200 MW N 3.5% S	30	292,291,500	26.17	11.46	124.59	1,119.89	104,508,300	24.00	10.51	1.14	1,028.6	
500 HW E 3.5% S	25	457,099,200	22.56	9.88	107.43	965.36	187,099,800	20.38	8.93	0.97	872.6	
500 HW N 2.0% S	30	429,700,300	15.73	6.74	74.89	1,454.15	153,984,800	14.46	6.20	0.69	1,337.8	
500 MW N 3.5% S	30	557,059,800	20.39	8.74	97.09	873.82	200,363,000	18.81	8.06	0.90	806.2	
500 MW N 5.0% S	30	670,722,600	24.55	10.52	116.90	679.56	241,941,500	22.72	9.74	1.08	628.7	
1,000 MW E 3,5% S	25	711,393,300	17.94	7.69	85.45	769.07	293,113,800	16.32	6.99	0.78	699.3	
1,000 MW N 3.5% S	30	863,634,100	16.35	6.77	77.86	700.72	312,517,300	15.18	6.29	0.72	650.4	
90% SO ₂ removal												
500 MW N 3.5% S	30	586,326,400	21.46	9.20	102.19	808.73	211,103,800	19.82	8.50	0.94	747.0	
Oil-Fired Power Unit												
0.8 lb SO ₂ /MBtu heat input allowable emission												
500 MW E 2.5% S	25	322,358,300	4.58	6.97	75.76	1,584,07	131,410,200	4.12	6.27	0.68	1,425.	

a. Basis

Midwest plant location, 1980 revenue requirements.

Over previously defined unit operating profile. 30-yr life; 7,000 hr - 10 yr, 5,000 hr - 5 yr, 3,500 hr - 5 yr, 1,500 hr - 10 yr. Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of fly ash excluded.

Revenue \$40/short ton S.

Constant labor cost assumed over life of project.

b. Discounted at 10% to initial year.

c. Equivalent to discounted process cost over life of power units.

Discussion of Results

Annual Revenue Requirements--

Summaries of the case variations for each process are shown in the appendix and tabulated totals are presented in Tables 35-37. In comparing results, it should be remembered that limestone and double alkali are waste-producing processes and citrate is a recovery process; however, credit for the sale of sulfur is included in the annual revenue requirements projected for citrate.

Generally, the ranking of annual revenue requirements for the processes is the same as the capital investment rankings. Projected revenue requirements for the limestone slurry process range from \$7,153,200 (5.11 mills/kWh) for a new 200-MW 3.5% sulfur coal-fired unit to \$23,241,200 (3.32 mills/kWh) for an existing 1,000-MW 3.5% sulfur coal-fired unit. Annual revenue requirements for the generic double-alkali process range from \$7,169,100 (5.12 mills/kWh) for a new 200-MW 3.5% sulfur coal-fired unit to \$25,750,900 (3.68 mills/kWh) for an existing 1,000-MW 3.5% sulfur coal-fired unit.

The sulfur-producing citrate process has greater annual revenue requirements than the waste-producing processes. The projected annual revenue requirements for citrate range from \$11,670,800 (8.34 mills/kWh) for a new 200-MW 3.5% sulfur coal-fired unit to \$36,933,500 (5.28 mills/kWh) for an existing 1,000-MW 3.5% sulfur coal-fired unit.

The sensitivity of revenue requirements to variations in the more important economic parameters has been evaluated and the effects of these variations on the projected annual revenue requirements are presented in Figures 20-36. Table 44 identifies the parameters that are varied and the range of values that is studied. Each range has been selected to correspond to differences in design or costs which might be encountered in more site-specific operation. As an illustration, limestone price variations represent the effect of plant location and the corresponding effect on overall process costs. Operating labor price fluctuations might also be the result of plant location.

Figures 20-22 show the effects of power unit size and status (new and existing) and sulfur content of coal on annual revenue requirements. As the projections show, sulfur in coal has a greater effect on the citrate process, while the differences in status of power units have a small effect on the annual revenue requirements of a specific unit size.

Special case variations are shown for the alternate disposal of waste solids by trucking and $90\%~\mathrm{SO}_2$ removal. Tables 45 and 46 display the results of these projections.

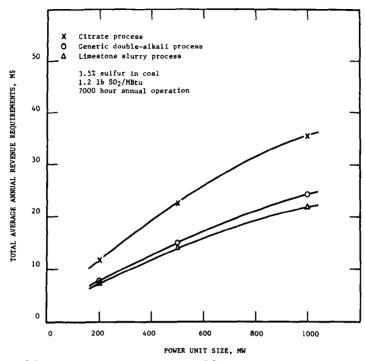


Figure 20. All processes. Effect of power unit size on annual revenue requirements for new coal-fired units.

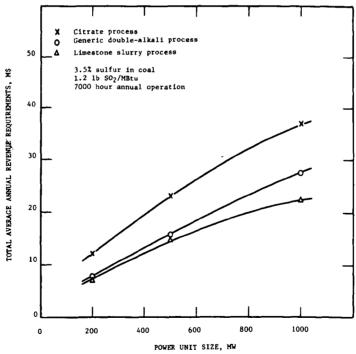


Figure 21. All processes. Effect of power unit size on annual revenue requirements for existing coal-fired units.

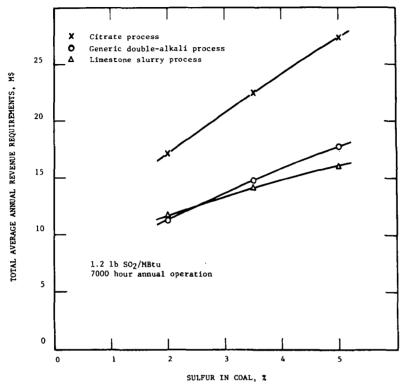


Figure 22. All processes. Effect of sulfur content of coal on annual revenue requirements for new 500-MW units.

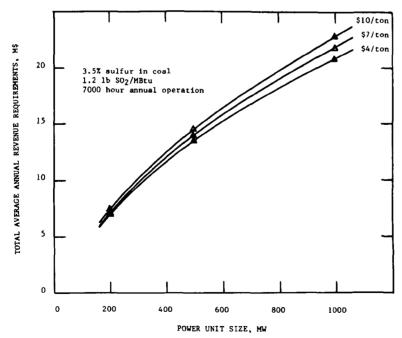


Figure 23. Limestone slurry process. Effect of power unit size and variations in limestone price on annual revenue requirements for new coal-fired units.

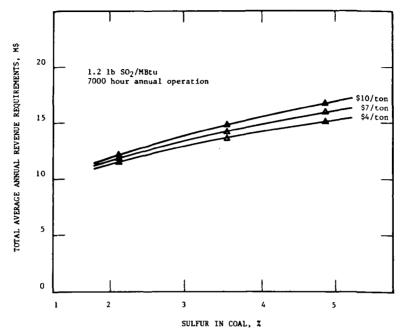


Figure 24. Limestone slurry process. Effect of sulfur in coal and variations in limestone price on annual revenue requirements for new 500-MW units.

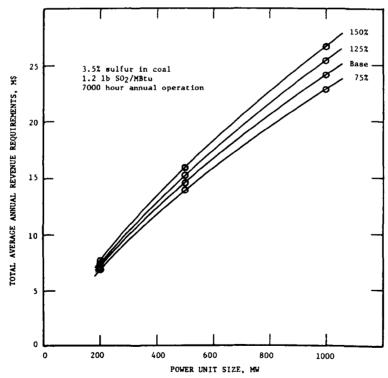


Figure 25. Generic double-alkali process. Effect of power unit size and variations in total raw materials cost on annual revenue requirements for new coal-fired units.

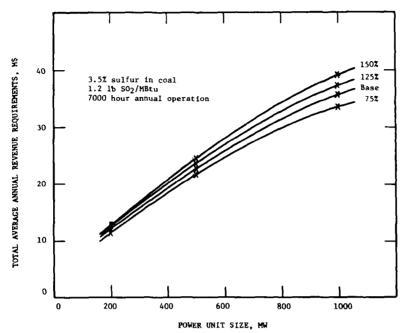


Figure 26. Citrate process. Effect of power unit size and variations in total raw materials cost on annual revenue requirements for new coal-fired units.

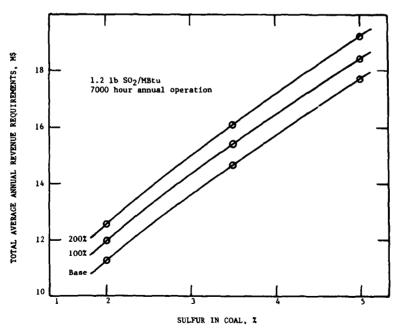


Figure 27. Generic double-alkali process. Effect of sulfur in coal and variations in operating labor cost on annual revenue requirements for new 500-MW units.

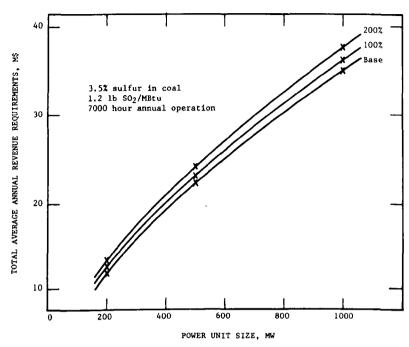


Figure 28. Citrate process. Effect of power unit size and variations in operating labor cost on annual revenue requirements for new coal-fired units.

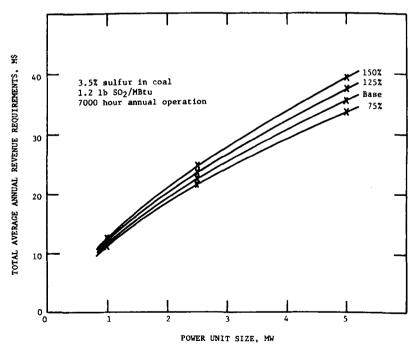


Figure 29. Citrate process. Effect of power unit size and variations in energy cost on annual revenue requirements for new coal-fired units.

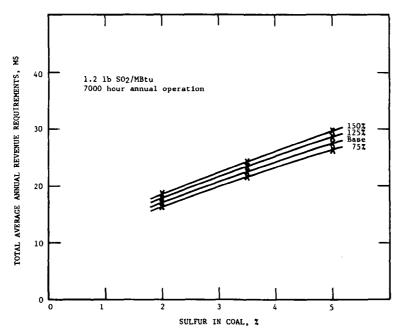


Figure 30. Citrate process. Effect of sulfur in coal and variations in energy cost on annual revenue requirements for new 500-MW units.

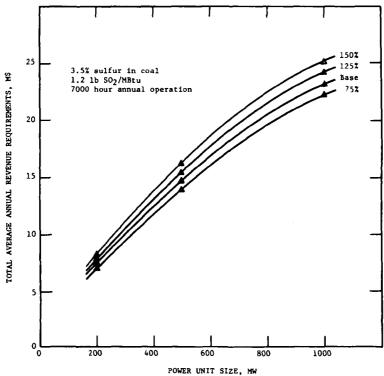


Figure 31. Limestone slurry process. Effect of power unit size and variations in maintenance cost on annual revenue requirements for new coal-fired units.

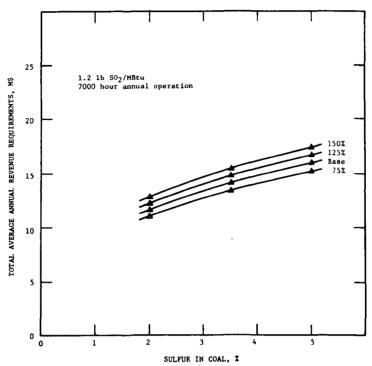


Figure 32. Limestone slurry process. Effect of sulfur in coal and variations in maintenance cost on annual revenue requirements for new 500-MW units.

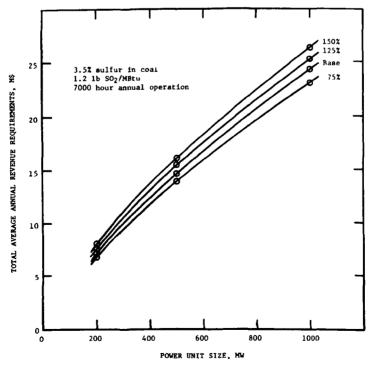


Figure 33. Generic double-alkali process. Effect of power unit size and variations in capital charges on annual revenue requirements for new coal-fired units.

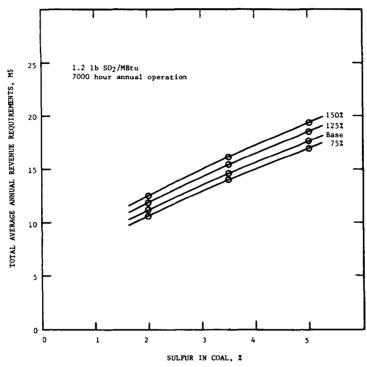


Figure 34. Generic double-alkali process. Effect of sulfur in coal and variations in capital charges on annual revenue requirements for new 500-MW units.

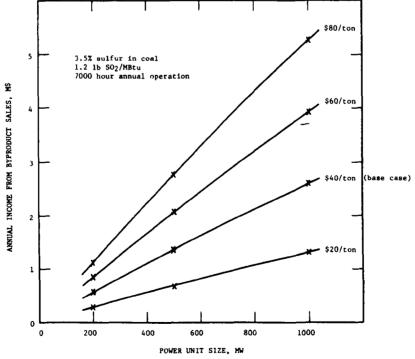


Figure 35. Citrate process. Effect of power unit size and variations in sulfur price on total annual income from byproduct sales for new coal-fired units.

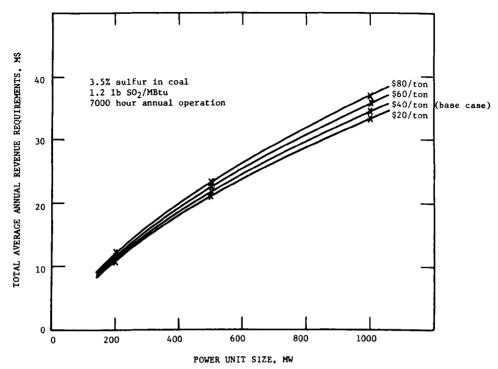


Figure 36. Citrate process. Effect of power unit size and variations in sulfur price on annual revenue requirements for new coal-fired units.

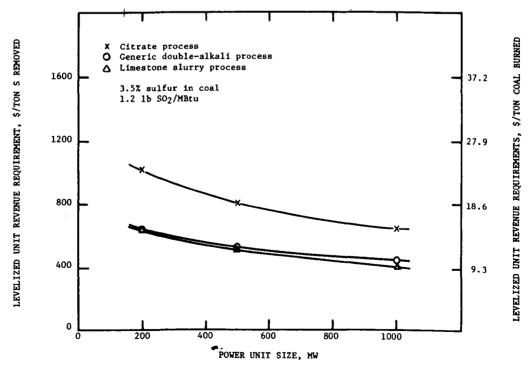


Figure 37. All processes. Effect of power unit size on levelized unit revenue requirements for new coalfired units.

TABLE 44. SENSITIVITY VARIATIONS STUDIED IN THE ECONOMIC COST PROJECTIONS

		Power unit	Annual revenue req		
Item	Process	description ^a	Base value	Range of variations	
Raw material price	Limestone	1 and 2	Limestone, \$7/ton	\$4-\$10/ton	
	Double alkali	1	Lime, \$42/ton Soda ash, \$90/ton	75-150% of total raw material cost	
	Citrate	1	Lime, \$42/ton Soda ash, \$90/ton Citric acid, \$0.67/ton Natural gas, \$3.50/kft ³	75-150% of total raw material cost	
Operating labor	Double alkali	2	Labor, \$12.50/man-hr	\$12.50-\$25.00/man-hr	
	Citrate	1	Labor, \$12.50/man-hr	\$12.50-\$25.00/man-hr	
Energy cost	Citrate process	1	Steam, \$2.00/MBtu Electricity, \$0.029/kWh		
Maintenance	Limestone	1 and 2	8% of direct investment excluding pond construction plus 3% of pond construction	50-150%	
Capital charges	Double alkali	1 and 2	Average capital charges, 6.0% of total depreciable investment plus 8.6% of total capital investment		
Product revenue	Citrate	1	Sulfur, \$40/ton	\$20-\$80/ton	

a. Power unit description

^{1.} New power units: 200, 500, and 1,000 MW; 3.5% sulfur in coal.

^{2.} New power unit, 500 MW: 2.0%, 3.5%, and 5.0% sulfur in coal.

TABLE 45. COMPARISON OF AVERAGE ANNUAL REVENUE
REQUIREMENTS FOR SOLIDS DISPOSAL ALTERNATIVES^a

Process	Slurry ponding (base case), \$	Filter cake trucking, \$	Revenue req increase (dec trucking alt	rease) in
Limestone	14,101,900	15,172,400	1,070,500	7.6
Double alkali	14,676,000	14,293,900	(382,100)	(2.6)

a. Base case conditions: Pond and cake disposal areas each 1 mile from scrubbing facilities.

TABLE 46. COMPARISON OF AVERAGE ANNUAL REVENUE REQUIREMENTS FOR DIFFERENT SO₂ REMOVAL LEVELS

	Projected too annual (7,000 revenue requirement (500-MW new 3.5% sulfur con 1.2 lb SO ₂ /MBtu heat	Annual revenue requirement increase resulting from increased SO ₂ removal		
Process	input allowable emission	90% SO ₂ removal	\$	z
Limestone Double alkali Citrate	14,101,900 14,676,000 22,538,000	14,651,300 15,438,800 23,812,400	549,400 762,800 1,274,400	3.9 5.2 5.7

The trucking alternative for limestone increases annual revenue requirements by 7.6% over the limestone base case, a result of additional operating labor, analyses, electricity, and fuel. While operating labor for trucking and fuel charges are added to the cost of double alkali, the original operating labor and electricity needs are decreased because the filter cake is not reslurried and pumped to disposal. In addition, the indirect cost decreases by \$957,000, resulting in an overall decrease in revenue requirements. The double-alkali trucking alternative revenue requirements are 6% less than limestone trucking but are still higher than the limestone slurry ponding case by approximately 1.4%.

Removal of 90% of the SO₂ compared with removal to meet emission standards results in revenue requirement increases of 4% to 6% for new 500-MW units. The credit for additional sulfur recovered and sold in the citrate process does not equal the increases in raw materials and utilities necessary for the additional removal.

From the detailed area-by-area base case annual revenue requirement breakdown analyses (shown in Tables 38-40) it can be seen that total capital charges are the largest components of revenue requirement for each process. Base case capital charges range from 46% of total annual revenue requirements in the citrate process to 50% in limestone and double-alkali processes. As would be expected because of the complexity of the process, citrate has the highest process operating labor cost. When disposal equipment operation is included (trucking alternative cases), however, labor costs for limestone are the highest. Excluding the trucking case variations, operating labor ranges from 2% to 6% of the total revenue requirements for all processes. Energy costs are significant for all processes. Steam for reheat is approximately the same for all processes, but citrate requires additional steam for product sulfur. Table 47 shows the four major operating cost components of each process and the corresponding percentage distribution of annual revenue requirements attributed to each component for the base case installation.

TABLE 47. MAJOR OPERATING COST COMPONENTS INCLUDED

IN THE BASE CASE ANNUAL REVENUE REQUIREMENTS

	Major operating cost components (percent of annual revenue requirements)						
Process	1	2	3	4			
Limestone	Capital charges (49.58)	Maintenance (12.93)	Electricity (11.65)	Limestone (7.86)			
Double alkali	Capital charges (49.47)	Raw materials (21.92)	Maintenance (7.00)	Steam (6.67)			
Citrate	Capital charges (45.84)	Raw materials (19.35)	Maintenance (9.81)	Steam (9.19)			

The sensitivity of the annual revenue requirements to variations in raw material price for the limestone process is shown in Figures 23-26. Figures 27 and 28 show the sensitivity of annual revenue requirements to variations in operating labor costs for the generic double-alkali process. Although similar variations in operating labor projections for limestone result in different ranges of costs, the general effect is similar.

The effect of energy cost variations for the citrate process is shown in Figures 29 and 30 for variations in power unit sizes and sulfur levels in coal. The effect of varying energy is similar for the other processes.

Maintenance is one of the major operating cost components of annual revenue requirements for all three processes. Figures 31 and 32 project the effect of varying maintenance requirements for the limestone slurry process.

Table 47 shows that capital charges have the greatest effect on annual revenue requirements. For the double-alkali process the effect of capital charge variations as a function of power unit size and sulfur level is shown in Figures 33 and 34.

Annual income from the sale of sulfur for the citrate process will vary according to Figure 35 as a function of power unit size and selling prices. The effect of variations in selling price on annual revenue requirements is presented in Figure 36.

Lifetime Revenue Requirements--

Along with the investment and annual revenue requirement summary tables given in the appendix, computer projections of the detailed year-to-year operating cost and sales revenue analyses for all case variations for each of the three processes are presented. These projections are prepared on a regulated economics basis as discussed in the procedure and correspond to the 30-year declining operating profile of the unit established in the power plant premises. Annual capital charges are based on the undepreciated investment. The overall net increase or decrease in cost of power is shown for each year, considering the declining annual operating cost and the net sales revenue resulting from sale of sulfur. Lifetime costs, both total and discounted (at the regulated cost of money - 11.6% for this study), are displayed and equivalent unit revenue requirements are shown. Summarized results of the lifetime revenue requirement projections for the three processes are presented in Tables 41-43. Table 48 shows the cumulative lifetime credits, both actual and discounted, for the citrate process which are included in the lifetime cost projections. Cumulative lifetime costs for the solids disposal alternatives and for different SO₂ removal levels are compared in Tables 49 and 50.

Graphic representations of the effect of power unit size on levelized unit revenue requirement in dollars per ton of sulfur removed for new and existing coal-fired power units are shown in Figures 37 and 38. These unit cost results show trends similar to the annual revenue requirement estimates; however, the magnitude of the costs is greater. The higher costs are the result of the declining operating profile of the power plant.

TABLE 48. CITRATE PROCESS

LIFETIME SULFUR PRODUCTION AND CREDIT

	Years remaining	Lifetime production	Net revenue,	Cumulati	ve revenue
Case	life	sulfur, short tons	\$/short ton sulfur	Actual, \$	Discounted,
Coal-Fired Power Unit					
1.2 lb SO ₂ /MBtu heat input					
allowable emission					
200 MW E 3.5% sulfur	20	117,500	40.00	4,700,000	2,320,50
200 MW N 3.5% sulfur	30	252,000	40.00	10,080,000	3,922,20
500 MW E 3.5% sulfur	25	457,000	40.00	18,280,000	8,285,30
500 MW N 2.0% sulfur	30	283,500	40.00	11,340,000	4,427,10
500 MW N 3.5% sulfur	30	627,000	40.00	25,080,000	9,771,30
500 MW N 5.0% sulfur	30	949,000	40.00	37,960,000	14,794,70
1,000 MW E 3.5% sulfur	25	894,000	40.00	35,760,000	16,207,40
1,000 MW N 3.5% sulfur	30	1,191,000	40.00	47,640,000	18,571,80
90% SO ₂ removal 500 MW N 3.5% sulfur	30	702,000	40.00	28,080,000	10,936,30
Oil-Fired Power Unit					
0.8 1b SO ₂ /MBtu heat input					
allowable emission					
500 MW E 2.5% sulfur	25	201,000	40.00	8,040,000	3,637,70

TABLE 49. COMPARISON OF CUMULATIVE LIFETIME DISCOUNTED PROCESS COST

FOR SOLIDS DISPOSAL ALTERNATIVES^a

	Cumulative d		Cumulative di lifetime in (decrease)	ncrease
Process	Slurry ponding (base case), \$	Filter cake	from trucking	
			5 043 400	/6
Limestone Double alkali	127,709,200 132,472,900	132,750,600 125,275,900	5,041,400 (7,197,000)	3.9 (5.4)

a. Base case conditions: Pond and cake disposal areas each 1 mile from scrubbing facilities.

TABLE ⁵⁰. COMPARISON OF CUMULATIVE LIFETIME DISCOUNTED PROCESS COSTS

FOR DIFFERENT SO₂ REMOVAL LEVELS

	Cumulative lifeti process cost, \$ (5 sulfur coal-f:	Cumulative lifetime discounted cost increase resulting		
Process	1.2 1b SO ₂ /MBtu heat input allowable emission	90% SO2 removal	from incr SO2 removal	eased
Limestone Double alkali Citrate	127,709,200 132,472,900 200,363,000	132,602,400 138,947,500 211,103,800	4,893,200 6,474,600 10,740,800	3.8 4.9 5.4

Figure 39 shows the effect of sulfur content of coal on levelized lifetime unit revenue requirements (\$/ton of sulfur removed) for a new 500-MW unit. In comparison with the annual revenue requirements given earlier, the relative ranking remains the same.

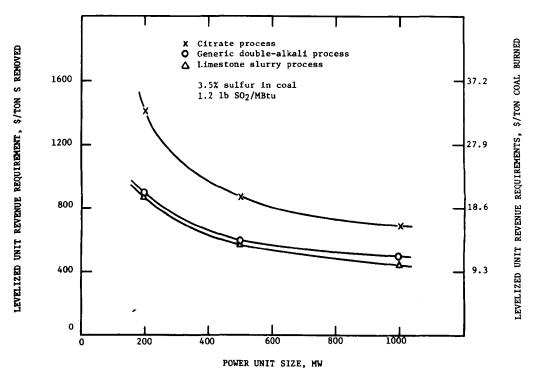


Figure 38. All processes. Effect of power unit size on levelized unit revenue requirements for existing coal-fired units.

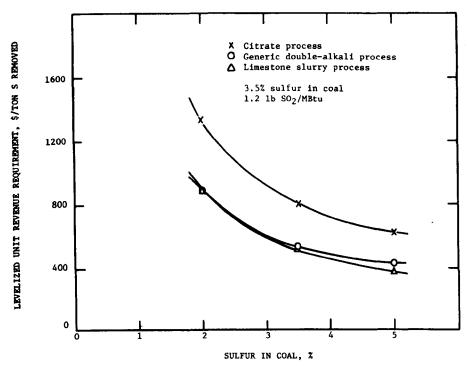


Figure 39. All processes. Effect of sulfur in coal on levelized unit revenue requirements for new 500-MW units.

CONCLUSIONS

The conclusions of this study have been summarized for capital investment requirements, revenue requirements, and processes. These are listed below.

CAPITAL INVESTMENT CONCLUSIONS

- 1. For base case conditions, the limestone process has the lowest investment requirements, followed by the double-alkali process, with the citrate process the highest. This ranking remains the same for each case variation except for the disposal-by-trucking alternative in which the limestone case variation investment is 2.4% higher than the double-alkali case. Limestone FGD requires more waste solids handling and a more expensive feed preparation area resulting in slightly higher capital investment needs. When the double-alkali disposal-by-trucking case is compared with the limestone base case (slurry disposal by ponding) limestone capital investment is 18% higher. It should be recognized that citrate is a recovery process and should also be compared with other recovery processes.
- 2. With one exception, the existing power unit case variations are greater than the new power unit case variations at each power plant size (200, 500, or 1,000 MW) in each process. In the limestone 200-MW cases, the decrease in costs because of the decrease in pond size based on a remaining life of 20 years is greater than the increase in labor charges required for retrofit situations so that the capital investment for the 200-MW existing unit is lower than the 200-MW new unit investment. Plant age is an important factor in the limestone and double-alkali waste-producing processes where pond size depends on remaining plant life.
- 3. Capital investment requirements are greater for systems that are designed for higher sulfur content. The existing oil-fired variation (2.5% sulfur in oil), however, requires less capital investment than the existing 500-MW unit burning 2.0% sulfur coal.
- 4. Removal of 90% of the SO₂ (instead of the removal to meet emission standards) increases investment by 3.5% to 4%.

- 5. Special purging of chlorides is unnecessary in waste-producing processes where enough neutralized chloride is trapped in the interstitial water in the settled sludge to maintain chloride control. Processes producing salable products, such as the citrate process, must control chloride buildup in the system. However, the addition of a chloride purge accounts for less than 1% of the direct investment.
- 6. In each process the SO_2 absorption area has greatest effect on the investment cost, from 29% to 43% of the direct investment. Gas handling and pond construction also contribute significantly to the direct investment. In the citrate process the H_2 and $\mathrm{H}_2\mathrm{S}$ generation plants represent 22% to 33% of the direct investment.

REVENUE REQUIREMENT CONCLUSIONS

- For base case conditions, the limestone process has the lowest annual revenue requirements, followed by the double-alkali process, with the citrate process the highest. This ranking remains the same for each case variation except for three instances: (1) 500-MW, 2% sulfur in coal, (2) 500-MW, 3.5% sulfur in coal with disposal-by-trucking, and (3) 500-MW, 2.5% sulfur in oil. For these variations, double-alkali annual revenue requirements are lower than limestone. In the limestone 500-MW, 2.0% sulfur in coal variation, electricity and maintenance costs are great enough to increase annual revenue requirements 3% over the comparable double-alkali requirements. (Base case limestone annual revenue requirements are 4% less than comparable doublealkali annual revenue requirements and 40% less than comparable citrate annual revenue requirements.) In the trucking and oil variations, electricity and maintenance charges increase limestone annual revenue requirements 6% and 3%, respectively, over those of double alkali. Also contributing to the increase in limestone annual revenue requirements over those of double alkali in the trucking variation are additional vehicle fuel costs and a plant overhead charge that is \$500,000 greater in limestone. Lifetime revenue requirements follow a similar pattern.
- 2. Annual revenue requirements for the existing power unit variations are greater than the new power unit costs at each power plant size in each process. The increases in annual revenue requirements range from 3% at the 500-MW size for citrate to 7% at the 1,000-MW size for double alkali.
- 3. Annual revenue requirements are greater for systems which are designed for higher sulfur content. As with capital investment requirements, the oil variation (existing 500-MW unit, 2.5% sulfur) requires less revenue than the existing 500-MW unit burning 2.0% sulfur coal, but there is no direct comparison between the two.

- 4. Removal of 90% of the SO_2 (instead of removal to meet 1.2 lb/MBtu emission standards) increases revenue requirement by 4% to 6%. The credit for additional sulfur removed and sold in the citrate process does not equal the increases in raw material and utility costs required for the additional removal.
- 5. Raw material costs are highest for the citrate process and lowest for the limestone process. Natural gas is the largest raw material cost in the citrate process, representing approximately 85% of the total raw material cost. The lime required for chloride neutralization in the citrate process adds from \$49,100 to \$240,700 to the raw material costs in the case variations evaluated.
- 6. As would be expected because of the complexity of the process, citrate has the highest total process operating labor cost. When disposal equipment operation is included (trucking alternative cases), however, labor costs for limestone are the highest. Excluding the trucking case variations, operating labor ranges from 2% to 6% of the annual revenue requirements for all processes.
- 7. Energy costs are significant for all processes. Double alkali has the lowest electricity requirement; citrate requires additional steam for product sulfur. Steam for reheat is essentially the same for all processes.
- 8. Maintenance ranges from 5% of the annual revenue requirements for the double-alkali 1,000-MW existing unit to 15% for the limestone 200-MW existing unit.
- 9. Capital charges are the largest component of revenue requirement for each process. Base case capital charges range from 50% of annual revenue requirements in limestone and double-alkali processes to 46% in the citrate process.
- 10. Revenue from the sale of sulfur produced in the citrate process amounts to 4% to 8% of the adjusted revenue requirement.

PROCESS CONCLUSIONS

The limestone-lime slurry process is the best known and most completely developed FGD system in the United States today. The evaluation of limestone FGD in this study reflects the broad experience of vendors and utilities in constructing and operating this system. Limestone is still the simplest and cheapest FGD process available today for most applications, but it continues to require intensive maintenance effort, it is a once-through process, and it produces a throwaway sludge of questionable stability and environmental effects.

While construction and operating experience is not as extensive for double alkali as for limestone, double-alkali FGD is a competitive alternative to limestone, especially when trucking is used to dispose of the waste. While double alkali is a waste-producing process, it requires less area for disposal and it regenerates the process scrubbing liquor. Because of system design, it should require less maintenance than limestone. As more experience is gained in constructing and operating the system, capital investment and revenue requirements could decrease because of changes in process design, but no significant changes are anticipated.

As a recovery system, the citrate process is inherently more expensive and cannot be compared directly with the throwaway processes evaluated here. For this study the citrate process is assumed proven. However, less is known about the integrated technology for this system than is known about limestone or double alkali, and the operation of many of the process areas is more complex. The citrate process is a more environmentally acceptable process than either the limestone or double-alkali processes because the disadvantage of producing waste solids is eliminated by the production of sulfur and sodium sulfate. Maintenance may also be relatively simple. More extensive engineering and operating experience could decrease costs in the areas of reduction and sulfur separation. However, the use of natural gas in the reduction step presents possible future problems of supply. The citrate process must be proven in the field in order to answer questions of real cost and operability.

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APPENDIX A

TOTAL CAPITAL INVESTMENT, AVERAGE ANNUAL REVENUE REQUIREMENT,

AND LIFETIME REVENUE REQUIREMENT TABLES - ALL PROCESSES AND CASE VARIATIONS

TABLE A-1. LIMESTONE SLURRY PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT^a

(200-MW existing coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller) Feed preparation (feeders, crushers, ball mills, hoist,	1,070,000	8.3
tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	1,208,000	9.4
dampers from absorber to reheater and stack) SO ₂ absorption (two TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators,	2,203,000	17.2
and pumps) Stack gas reheat (two indirect steam reheaters) Solids disposal (onsite disposal facilities including feed tank, agitator, slurry disposal pumps, and pond water return	4,310,000 584,000	33.6 4.5
pumps)	1,392,000	10.8
Subtotal	10,767,000	83.8
Services, utilities, and miscellaneous	646,000	5.0
Total process areas excluding pond construction	11,413,000	88.8
Pond construction	1,444,000	11.2
Total direct investment	12,857,000	100.0
Indirect Investment		
Engineering design and supervision Architect and engineering contractor Construction expense Contractor fees	869,000 203,000 2,062,000 669,000	6.8 1.6 16.0 5.2
Total indirect investment	3,803,000	29.6
Contingency	3,332,000	25.9
Total fixed investment	19,992,000	155.5
Other Capital Charges		
Allowance for startup and modifications Interest during construction	1,855,000 2,399,000	14.4 18.7
Total depreciable investment	24,246,000	188.6
Land Working capital	295,000 516,000	2.3 4.0
Total capital investment	25,057,000	194.9

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979. Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared. Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

TABLE A-2. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(200-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annua quant		Unit cost, S	Total annual cost,	ann	of average ual revenue quirements
Direct Costs						
Raw materials						
Limestone	67,700	tons	7.00/tor	473,9	000	6.34
Total raw materials cost				473,9	000	6.34
Conversion costs						
Operating labor and supervision Utilities	16,440	man-hr	12.50/mar	-hr 205,5	00	2.75
Steam	206,800		2.00/MBt	u 413,6	00	5.53
Process water	107,100	kgal	0.12/kga			0.17
Electricity	23,927,000	kWh	0.031/kWh			9.92
Maintenance	•			-, .		
Labor and material				1,070,5	00	14.31
Analyses	1,980	man-hr	17.00/mar			0.45
Total conversion costs				2,477,9	00	33.13
Total direct costs				2,951,8	00	39.47
Indirect Costs Capital charges						
Depreciation, interim replacement insurance at 7.0% of total depre investment				1 (07 0	•	
Average cost of capital and taxes	at 8.6%			1,697,2		22.69
of total capital investment				2,154,9	00	28.81
Overheads						
Plant, 50% of conversion costs le		3		654,9		8.76
Administrative, 10% of operating	labor			20,6	<u>00</u>	0.27
Total indirect costs				4,527,6	00	60.53
Total average annual revenue r	equirements			7,479,4	00	100.00
	Mills/		ton coal	\$/MBtu heat input	\$/short S remo	
Equivalent unit revenue requirement	s 5.3	14	11.81	0.56	506.6	\s

a. Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 20 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 633,500 tons/yr, 9,500 Btu/kWh. Stack gas reheat to 175°F.

S removed, 14,780 short tons/yr; solids disposal 77,790 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$12,857,000; total depreciable investment, \$24,246,000; and total capital investment, \$25,057,000.

				FIXED	INVESTMENT: \$	25057000				
AFTER	ANNUAL OPERA- TION+ KW-HR/ KW	POWER UNIT HEAT REQUIREMENT• MILLION BTU /YEAR	POWER UNIT FUEL CONSUMPTION. TONS COAL /YEAR	SULFUR REMOVED BY POLLUTION CONTROL PROCESS* TONS/YEAR	RY-PRODUCT HATE; EQUIVALENT TONS/YEAR DRY SOLIDS	NET REVENUE, \$/TON DRY SOLIDS	TOTAL OP. COST INCLUDING REGULATED ROI FOR POWER COMPANY, \$/YEAR	TOTAL NET SALES REVENUE + S/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER,	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER, \$
1 2 3 4 5 6 7 8										
.1 <u>0</u>	~~~~									
11	5000	9500000	452400	10600	55600	0.0	8773700	0	8773700	8773700
12 13	5000 5000	9500000	452400	10600	55600 55400	0.0	8565200	0	8565200	17338900 25695600
14	5000	9500000 9500000	452400 452400	10600 10600	55600 55600	0.0 0.0	8356700 8148200	0	8356700 8148200	33843800
-15	5000	9500000	452400 452400	10600	55600	0.0	7939600	0	7939600_	41783400
16	3500	6650000	316700	7400	38900	0.0	7052200	<u>v</u> -	7052200	48835600
17	3500	6650000	316700	7400	38900	0.0	6843700	ŏ	6843700	55679300
18	3500	6650000	316700	7400	38900	0.0	6635200	ŏ	6635200	62314500
19	3500	6650000	316700	7400	38900	0.0	6426700	Ŏ	6426700	68741200
-55	3500_	6650000	316700	7400	38900	0.0	6218200	o_	6218200	74959400
21	1500	2850000	135700	3200	16700	0.0	5015A00	0	5015800	79975200
22	1500	2850000	135700	3200	16700	0.0	4807300	0	4807300	84782500
23	1500	2850000	135700	3200	16700	0.0	4598800	0	4598800	89381300
24	150¢	2850000	135700	3200	16700	0.0	4390300	0	4390300	93771600
-25_	1500	2920030	135700	3200	16700	<u>-</u>	4181890	<u>Q</u> -	4181800_	97953400
26	1500	2850000	135700	3200	16700	0.0	3973300	0	3973300	101926700
27	1500	2850000	135700	3200	16700	0.0	3764800	0	3764800	105691500
59 28	1500 1500	2850000	135700	3200	16700	0.0	3556200 3347700	0	3556200 3347700	109247700 112595400
30	1500	2850000 2850000	135700 135700	3200 3200	16700 16700	0.0	3139200	ů	3139200	115734600
-45					T3TA6			X-		
TOT	57500	109250000	5202500	122000	639500		115734600	0	115734600	
LI	FETIME A		SE (DECREASE)		ING COST					
			S PER TON OF C				22.25	0.0	22.25	
			PER KILOWATT-H				10.06	0.0	10.06	
			PER MILLION BT				105.94	0.0	105.94	
80005			S PER TON OF S				948.64	0.0	948.64	
PRUCE	35 CUST	THOREAGE (DEC	11.6% TO INI	TIAL YEAR+ DOL	LARS	DICCOUNTED DOOR	52811700	0	52811700	
LE	ACTIVED		MEASE) IN UNIT S PER TON OF C		T EQUIVALENT TO	DISCOUNTED PROC	20.52	0.0	20.52	
			PER KILOWATT-H				9.28	0.0	9.28	
			PER MILLION BT				97.73	0.0	97.73	
			S PER TON OF S				875.82	0.0	875.82	
		OOLL 40.	2 7 277 10.4 (7) 3	OC. ON PEROVED			0.3.00	•••		

TABLE A-4. LIMESTONE SLURRY PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(200-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller)	960,000	7.4
Feed preparation (feeders, curshers, ball mills, hoist, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts	1,188,000	9.1
and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack) SO ₂ absorption (two TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators,	1,850,000	14.2
and pumps) Stack gas reheat (two indirect steam reheaters) Solids disposal (onsite disposal facilities including feed tank, agitator, slurry disposal pumps, and pond water return	4,034,000 569,000	30.8 4.4
pumps)	1,250,000	9.6
Subtotal	9,851,000	75.5
Services, utilities, and miscellaneous	591,000	4.6
Total process areas excluding pond construction	10,442,000	80.1
Pond construction	2,598,000	19.9
Total direct investment	13,040,000	100.0
Indirect Investment		
Engineering design and supervision Architect and engineering contractor Construction expense Contractor fees	916,000 207,000 2,039,000 676,000	7.0 1.6 15.6 5.2
Total indirect investment	3,838,000	29.4
Contingency	3,376,000	25.9
Total fixed investment	20,254,000	155.3
Other Capital Charges		
Allowance for startup and modifications Interest during construction	1,766,000 2,430,000	13.5 18.7
Total depreciable investment	24,450,000	187.5
Land Working capital	514,000 497,000	3.9 3.8
Total capital investment	25,461,000	195.2

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average Cost basis for scaling, mid-1979. Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared. Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-5. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(200-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs				
Raw materials				
Limestone	65,600 tons	7.00/ton	459,200	6.42
Total raw materials cost			459,200	6.42
Conversion costs				
Operating labor and supervision Utilities	16,440 man-hr	12.50/man-hi	205,500	2.87
Steam	200,300 MBtu	2,00/MBtu	400,600	5.60
Process water	103,700 kgal	0.12/kgal	12,400	0.17
Electricity	23,173,000 kWh	0.031/kWh	718,400	10.04
Maintenance	•	•	•	
Labor and material			1,017,700	14.24
Analyses	1,980 man-hr	17.00/man-hi	33,700	0.47
Total conversion costs			2,388,300	33.39
Total direct costs			2,847,500	39.81
Indirect Costs Capital charges Depreciation, interim replacement	s, and			
insurance at 6.0% of total depre	ciable		1,467,000	20.51
Average cost of capital and taxes	at 8.6%		1,407,000	20.52
of total capital investment			2,189,600	30,61
Overheads			• •	
plant, 50% of conversion costs le	ss utilities		628,500	8.78
Administrative, 10% of operating	labor		20,600	0.29
Total indirect costs			4,305,700	60.19
Total average annual revenue r	requirements		7,153,200	100.00
	\$ Mills/kWh	/ton coal \$, burned		short ton removed
Equivale nt unit revenue requirement	s 5.11	11.67	0.56	499.87

Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 613,200 tons/yr, 9,200 Btu/kWh. Stack gas reheat to 175°F.

s removed, 14,310 short tons/yr; solids disposal 75,310 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$13,040,000; total depreciable investment, \$24,450,000; and total capital investment, \$25,461,000.

				FIXED	INVESTMENT: \$	25461000				
							TOTAL			
				SULFUR	BY-PRODUCT		OP. COST			
				HEMOVED	RATE		INCLUDING		NET ANNUAL	CUMULATIVE
	ANNUAL	POWER UNIT	POWER UNIT	BY	EQUIVALENT	NET REVENUE.	REGULATED	TOTAL	INCREASE	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	ROI FOR	NET	(DECREASE)	(DECREASE)
POWER	-		CONSUMPTION,	CONTROL			POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION ATU	TONS COAL	PROCESS.	DRY	DRY	COMPANY.	REVENUE .	POWER,	PUWER+
START	KW	/YEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	\$/YEAR	\$	
1	7000	12980000	613300	14300	75300	0.0	9343100	-	9343100	9343100
2	7000	12880000	613300	14300	75300	0.0	9202900	0	9202900	18546000
3	7000	12880000	613300	14300	75300	0.0	9062700	Ó	9062700	27608700
4	7000	12980000	613300	14300	75300	0.0	8922600	0	8922600	36531300
5	7000	12880000	613300	14300	75300	0.0	8782400	Q	8782400_	45313700
6	7000	12880000	613300	14300	75300	0.0	8642200		8642200	53955900
7	7000	12880000	613300	14300	75300	0.0	8502000	0	8502000	62457900
8	7000	12880100	613300	14300	75300	0.0	8361800	0	8361800	70819700
9	7000	12880000	613300	14300	75300	0.0	8221700	0	8221700	79041400
10	7000	12880000	613300	14300	Z5300	0.0	8081500	Q	8081500_	87122900
11	5000	9200000	438100	10200	53800	0.0	7111000	0	7111000	94233900
12	5000	9200000	438100	10200	53800°	0.0	6970800	0	6970800	101204700
13	5000	9200000	438100	10200	53800	0.0	6830600	0	6830600	108035300
14	5000	9200000	438100	10200	53800	0.0	6690500	. 0	6690500	114725800
15	5000	9200000	438100	10200	53800		6550300	Q	6550300_	121276100
16	3500	6440000	306700	7200	37700	0.0	5755300	0	5755300	127031400
17	3500	6440000	306700	7200	37700	0.0	5615100	0	5615100	132646500
18	3500	6440000	306700	7200	37700	0.0	5474900	0	5474900	138121400
19	3500	6440000	306700	7200	37700	0.0	5334800	0	5334800	143456200
-50	3500	6440000	306700		37700		5124600	0_	5194600_	148650800
21	1500	2760000	131400	3100	16100	0.0	4076200	0	4096200	152747000
22	1500	2760010	131400	3100	16100	0.0	3956000	0	3956000	156703000
23	1500	2760000	131400	3100	16100	0.0	3815800	0	3815800	160518800
24	1500	2760000	131400	3100	16100	0.0	3675700	0	3675700	164194500
25	1500	2760000	131400	3100	16100		3535500	0_	3535500_	<u>16773000</u> 0 171125300
26	1500	2760000	131400	3100	16100	0.0	3395300	0	3395300	174380400
27	1500	2760000	131400	3100	16100	0.0	3255100	0	3255100	177495300
28	1500	2760000	131400	3100	16100	0.0	3114900	0	3114900	180470100
29	1500	2760000	131400	3100	16100	0.0	2974800	0	2974800	183304700
_30	1500	2760000	131400	3100	16100				2834600	
TAT	127500	234600000	11171000	261000	1371500		183304700	0	183304700	
			SE (DECREASE)				103304700	v	10330410	
L 11	CITAC W		S PER TON OF C		11.40 COST		16.41	0.0	16.41	
			PER KILOWATT-H				7.19	0.0	7.19	
			PER MILLION BT				78.13	0.0	78.13	
			S PER TON OF S				702.32	0.0	702.32	
000055	C COST				LADC		65253700	0.0	65253700	
			11.6% TO INI		LARS ST EQUIVALENT TO	DICCOUNTED BOAC			POWER UNIT	
LEV	ELIZED I				SI EMOTAMERAL IO	DISCOUNIED PROC			14.99	
			PER TON OF CO				14.99	0.0	6.56	
		•	ER KILOWATT-HO				6.56	0.0	71.36	
			ER MILLION BTU				71.36	0.0	642.26	
		DOLLARS	PEH TON OF SU	LFUK KEMUYED			642.26	0.0	046.60	

TABLE A-7. LIMESTONE SLURRY PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(500-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb $SO_2/MBtu$ heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total directinvestment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators,		
bins, shaker, puller) Feed preparation (feeders, crushers, ball mills, hoist,	1,940,000	7.2
tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	1,870,000	7.0
dampers from absorber to reheater and stack) 50 absorption (four TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators,	5,111,000	19.0
and pumps)	9,424,000	35.1
Stack gas reheat (four indirect steam reheaters) Solids disposal (onsite disposal facilities including feed tank, agitator, slurry disposal pumps, and pond water return	1,312,000	4.9
pumps)	1,826,000	6.8
Subtotal	21,483,000	80.0
Services, utilities, and miscellaneous	1,289,000	4.8
Total process areas excluding pond construction	22,772,000	84.8
Pond construction	4,084,000	15.2
Total direct investment	26,856,000	100.0
Indirect Investment		
Engineering design and supervision	1,174,000	4.4
Architect and engineering contractor	265,000	1.0
Construction expense	3,764,000	13.9
Contractor fees	1,170,000	4.4
Total indirect investment	6,373,000	23.7
Contingency	6,646,000	24.8
Total fixed investment	39,875,000	148.5
Other Capital Charges		
Allowance for startup and modifications	3,579,000	13.3
Interest during construction	4,785,000	17.8
Total depreciable investment	48,239,000	179.6
Land	820,000	3.1
Working capital	1,061,000	3.9
Total capital investment	50,120,000	186.6

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175 F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-8. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS

(500-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annua quanti		Unit cost, \$	Total annual cost,	l ann	of averagual reven
Direct Costs						
Raw materials	•					
Limestone	163,900	tons	7.00/ton	1,147,3	100	7.76
Total raw materials cost				1,147,3	300	7.76
Conversion costs						
Operating labor and supervision Utilities	25,990	man-hr	12.50/man	-hr 324,9	000	2.20
Steam	500,700	MBtu	2.00/MBt	u 1,001,4	•00	6,77
Process water	257,900	kga1	0.12/kga			0.21
Electricity 5	7,930,000	kWh	0.029/kWh			11.36
Maintenance	-			.,,		11.30
Labor and material				1,944,3	300	13.14
Analyses	3,760	man-hr	17.00/man			0.43
Total conversion costs				5,045,4	00	34.11
Total direct costs				6,192,7	00	41.87
Indirect Costs Capital charges Depreciation, interim replacements,	and					
insurance at 6.4% of total deprecial investment				3,087,3	00	20.88
Average cost of capital and taxes at of total capital investment	8.6%			4,310,3	00	29.14
Overheads						
Plant, 50% of conversion costs less				1,166,6		7.89
Administrative, 10% of operating lab	oor			32,5	<u>00</u>	0.22
Total indirect costs				8,596,7	00	58.13
Total average annual revenue requ	irements			14,789,4	00	100.00
	Mills/		ton coal	\$/MBtu heat input	\$/short S remov	ton ved
Equivalent unit revenue requirements	4.2	3	9.65	0.46	413.3	

Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 25 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,533,350 tons/yr, 9,200 Btu/kWh. Stack gas reheat to 175 F.

S removed, 35,780 short tons/yr; solids disposal 188,300 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$26,856,000; total depreciable investment, \$48,239,000; and total capital investment, \$50,120,000.

LIMESTONE SLURRY PROCESS 500 MW EXISTING COAL-FIRED POWER UNIT 3.5% S IN COAL. REGULATED CO. ECONOMICS

VEADS ANNUAL POWER UNIT P					FIXED	INVESTMENT: S	50120000				
1	AFTER POWER UNIT	OPERA- TION+ KW-HR/	HEAT REQUIREMENT. MILLION ATU	FUFL CONSUMPTION. TONS COAL	REMOVED BY POLLUTION CONTROL PROCESS+	RATE. EQUIVALENT TONS/YEAR DWY	\$/TUN DRY	OP. COST INCLUDING REGULATED POI FOR POWER COMPANY.	NET SALES REVENUE,	INCREASE (DECREASE) IN COST OF POWER,	NET INCREASE (DECREASE) IN COST OF POWER;
5											
7 7000 32200000 1533300 35400 168300 0.0 18767700 0 18767700 37867300 9 7000 32200000 1533300 35400 188300 0.0 1843590 0 0 18435900 5630220 9 7000 32200000 1533300 35400 188300 0.0 1840400 0 18104000 74407200 10 7000 32200000 1593300 35400 188300 0.0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 17712100 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771210 0 1771	4										
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DOLLARS PER TON OF SULFUR REMOVED PROCESS COST DISCOUNTED AT 11.6% TO INITIAL YEAR+ DOLLARS LEVELIZED INCREASE (DECREASE) IN UNIT OPERATING COST EQUIVALENT TO DISCOUNTED PROCESS COST OVER LIFE OF POWER UNIT DOLLAPS PER TON UF COAL BURNED MILLS PER KILOWATT-HOUH 5.82 CENTS PER MILLION BY U HEAT INPUT 63.29 0.0 63.29											
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			DOLLARS	PER TON OF SI	JLFUR REMOVED					569.19	

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TABLE A-10. LIMESTONE SLURRY PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT^a

(500-MW new coal-fired power unit, 2.0% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators,	07/ 000	
bins, shaker, puller) Feed preparation (feeders, crushers, ball mills, hoist,	974,000	4.7
tanks, agitators, and pumps)	1,179,000	5.6
Gas handling (common feed plenum and booster fans, gas ducts		
and dampers from plenum to absorber, exhaust gas ducts and		
dampers from absorber to reheater and stack)	4,120,000	19.7
SO ₂ absorption (four TCA scrubbers including presaturators		
and entrainment separators, recirculation tanks, agitators,	9 202 000	
and pumps) Stack gas reheat (four indirect steam reheaters)	8,282,000	39.6
Solids disposal (onsite disposal facilities including feed	1,222,000	5.9
tank, agitator, slurry disposal pumps, and pond water return		
pumps)	1,290,000	6.2
Paris,		0.2
Subtotal	17,067,000	81.7
Services, utilites, and miscellaneous	1,024,000	4.9
Total process areas excluding pond construction	18,091,000	86.6
Pond construction	2,800,000	13.4
Total direct investment	20,891,000	100.0
Indirect Investment		
Engineering design and supervision	1,130,000	5.4
Architect and engineering contractor	260,000	1.2
Construction expense	3,071,000	14.8
Contractor fees	967,000	4.6
Total indirect investment	5,428,000	26.0
Contingency	5,264,000	25.2
Total fixed investment	31,583,000	151.2
Other Capital Charges		
Allowance for startup and modifications	2,878,000	12.0
Interest during construction	3,790,000	13.8 18.1
Total depreciable investment	38,251,000	
TOTAL SEPTEMBEL ANTONOMIC	50,251,000	183.1
Land	563,000	2.7
Working capital	827,000	3.9
Total capital investment	39,641,000	189.7

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979. Stack gas reheat to 175 F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

TABLE A-11. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW new coal-fired power unit, 2.0% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantity	Unit cost, \$	Total annual cost, \$	% of average annual revenu requirements
Direct Costs				
Raw materials				
Limestone	73,600 tons	7.00/ton	515,200	4.44
Total raw materials cost			515,200	4.44
Conversion costs				
Operating labor and supervision Utilities	23,280 man-hr	12.50/man-h	291,000	2.50
Steam	489,800 MBtu	2.00/MBtu	979,600	8.43
Process water	215,000 kgal	0.12/kga1	25,800	0.22
Electricity	53,505,000 kWh	0.029/kWh	1,551,600	13.35
Maintenance	• • • • • • • • • • • • • • • • • • • •		, , , , ,	
Labor and material			1,531,300	13.17
Analyses	3,370 man-hr	17.00/man-h		0.49
Total conversion costs			4,436,600	38.16
Total direct costs			4,951,800	42.60
Indirect Costs Capital charges Depreciation, interim replacement insurance at 6.0% of total depre	s, and ciable			
investment	. 0 (#		2,295,100	19.74
Average cost of capital and taxes of total capital investment	at 8.6%		3,409,100	29.33
Overheads			939,800	0.00
Plant, 50% of conversion costs le	ss utilities		,	8.08
Administrative, 10% of operating	labor		29,100	0.25
Total indirect costs			6,673,100	57.40
Total average annual revenue r	equirements		11,624,900	100.00
	Mills/kWh	/ton coal \$		short ton removed
			•	

Basis

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh. Stack gas reheat to 175°F.

S removed, 16,200 short tons/yr; solids disposal 85,260 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$20,891,000; total depreciable investment, \$38,251,000; and total capital investment, \$39,641,000.

Midwest plant location, 1980 revenue requirements.

				FIXED	INVESTMENT: \$	39641000				
							TOTAL			
				SULFUR	RY-PRODUCT		OP. COST			
				HEMOVED	RATE.		INCLUDING		NET ANNUAL	CUMULATIVE
	ANNUAL	POWER UNIT	POWER UNIT	BY	EQUIVALENT	NET REVENUE.	REGULATED	TOTAL	INCREASE	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	ROI FOR	NET	(DECREASE)	(DECREASE)
	TION.		CONSUMPTION.	CONTROL			POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	DHY	DRY	COMPANY,	REVENUE.	POWER,	POWER.
START	KW	/YEAR	/YEAR	TONS/YEAH	SOLIDS	SOLIDS	S/YEAR	\$/YEAR	s	\$
-	7000	31500000	1500000	16200	в 5300	0.0	15034400	<u>_</u>	15034400	15034400
ž	7000	31500000	1500000	16200	85300	0.0	14815100	0	14815100	29849500
3	7000	31500000	1500000	16200	85300	0.0	14595800	0	14595800	44445300
4	7000	31500000	1500000	16200	85300	0.0	14376500	0	14376500	58821800
5	7000	31500000	1500000	16200	85300	<u> </u>	14157200	0_	14157200_	12±79000
6	7000	31500000	1500000	16200	65300	0.0	13937900	0	13937900	86916900
7	7000	31500000	1500000	16200	85300	0.0	13718600	0	13718600	100635500
8	7000	31500000	1500000	16200	85300	0.0	13499300	0	13499300	114134800
9	7000	31500000	1500000	16200	H5300	0.0	13580000	0	13280000	127414800
10	7000	31500000	1500000	16200	85300	Q.Q	13060700	0_	13060700_	140475500
11	5000	22500000	1071400	11600	60900	0.0	11340500	0	11390500	151866000
12	5000	22500000	1071400	11600	60900	0.0	11171200	0	11171200	163037200
13	5000	22500000	1071400	11600	60900	0.0	10951900	0	10951900	173989100
14	5000	22500000	1071400	11600	60900	0.0	10732600	0	10732600	184721700
15	5000	22500000	1071400	11600	60900	Q.Q	10513300	Q	10513300_	195235000
16	3500	15750000	750000	A100	42600	0.0	9160000	0	9160000	204395000
17	3500	15750000	750000	#100	42600	0.0	8940700	0	8940700	213335700
18	3500	15750000	750000	8100	42600	0.0	8721400	0	8721400	222057100
19	3500	15750000	750000	8100	42600	0.0	8502100	0	8502100	230559200
_20	3500	15750000	750000	6100		Q_Q	82 <u>62</u> 600	0_	8282800_	236442000
21	1500	6750000	321400	3500	18300	0.0	6424800	0	6429800	245271800
22	1500	6750000	321400	3500	18300	0.0	6210500	0	6210500	251482300
23	1500	6750000	321400	3500	18300	0.0	5991200	0	5941200	257473500
24	1500	6750000	321400	3500	18300	0.0	5771900	0	5771900	263245400
25	1500	6750000	321400	3500	13300		5552600	Q	5552600_	268798000
26	1500	6750000	321400	3500	18300	0.0	5333300	0	5333300	274131300
27	1500	6750000	321400	3500	18300	0.0	5114000	0	5114000	279245300
28	1500	6750000	321400	3500	18300	0.0	4894700	0	4894700	284140000
29	1500	6750000	321400	3500	18300	0.0	4675400	0	4675400	288815400
30	1500	6750000	321400	3500	18320		4456100	Q	4456100	293271500
TOT	127500	573750000	27321000	295500	1553500		293271500	0	293271500	
101	ETIME AV		SE (DECREASE)				270211300	•	4,02,1200	
			PER TON OF CO				10.73	0.0	10.73	
			PER KILOWATT-HO				4.60	0.0	4.60	
			FR MILLION ATL				51.11	0.0	51.11	
			PER TON OF SU				992.46	0.0	992.46	
PROCES	S COST D		11.6% TO INIT		LARS		104931000	0	104931000	
IFU	FI TZED T	NCREASE (DECE	FACEL IN HAIT	OPERATING COS	T EQUIVALENT TO	DISCOUNTED PHOC		R LIFE OF		
			PER TON OF CO			0.0000 HED FROM	9.85	0.0	9.85	
			FR KILOWATT-HO				4.22	0.0	4.22	
			ER MILLION ATU				46.92	0.0	46.92	
			PER TON OF SU				911.65	0.0	911.65	
		MULLARS	PER ION OF 50	CLOM MEMORED			71100	V • V	41100	

TABLE A-13. LIMESTONE SLURRY PROCESS SUMMARY OF ESTIMATED CAPITAL INVESTMENT^a

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller) Feed preparation (feeders, crushers, ball mills, hoist,	1,759,000	6.8
tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack)	1,740,000	6.7
SO ₂ absorption (four TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators, and pumps)	8,918,000	34.3
Stack gas reheat (four indirect steam reheaters) Solids disposal (onsite disposal facilities including feed	1,282,000	4.9
tank, agitator, slurry disposal pumps, and pond water return pumps)	1,658,000	6.4
Subtotal	19,675,000	75.7
Services, utilities, and miscellaneous	1,180,000	4.5
Total process areas excluding pond construction	20,855,000	80.2
Pond construction	5,145,000	19.8
Total direct investment	26,000,000	100.0
Indirect Investment		
Engineering design and supervision Architect and engineering contractor Construction expense Contractor fees	1,207,000 268,000 3,617,000 1,142,000	4.6 1.0 13.9 4.4
Total indirect investment	6,234,000	23.9
Contingency	6,447,000	24.8
Total fixed investment	38,681,000	148.7
Other Capital Charges		
Allowance for startup and modifications Interest during construction	3,354,000 4,642,000	12.9 17.9
Total depreciable investment	46,677,000	179.5
Land Working capital	1,030,000 1,021,000	4.0 3.9
Total capital investment	48,728,000	187.4

a. Basis
 Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.
 Stack gas reheat to 175°F by indirect steam reheat.
 Minimum in-process storage; only pumps are spared.
 Disposal pond located 1 mi from power plant.
 Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.
 Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-14. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

_			<u> </u>	
	Annual quantity	Unit cost, \$	Total annual cost, \$	% of average annual revenu requirements
Direct Costs				
Raw materials				
Limestone	158,300 tons	7.00/ton	1,108,100	7.86
Total raw materials cost			1,108,100	7.86
Conversion costs				
Operating labor and supervision Utilities	25,990 man-h	12.50/man-1	nr 324,900	2.30
Steam	489,800 MBtu	2.00/MBtu	979,600	6.95
Process water	247,400 kgal	0.12/kgal		0.21
Electricity	56,670,000 kWh	0.029/kWh	1,643,400	11.65
Maintenance				
Labor and material			1,822,800	12.93
Analyses	3,760 man-hi	17.00/man-1	nr <u>63,900</u>	0.45
Total conversion costs			4,864,300	34.49
Total direct costs			5,972,400	42.35
Indirect Costs Capital charges				
Depreciation, interim replacement insurance at 6.0% of total depre investment			2,800,600	19.86
Average cost of capital and taxes	at 8.6%		-	
of total capital investment			4,190,600	29.72
Overheads			1 105 900	7 0/
Plant, 50% of conversion costs le Administrative, 10% of operating			1,105,800 32,500	
	14001		32,300	0.23
Total indirect costs			8,129,500	57.65
Total average annual revenue r	equirements		14,101,900	100.00
	Mills/kWh	\$/ton coal burned		/short ton S removed
	- -			

a. Basis

Midwest plant location, 1980 revenue requirements. Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh. Stack gas reheat to 175°F.

S removed, 35,000 short tons/yr; solids disposal 184,200 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$26,000,000; total depreciable investment, \$46,677,000; and total capital investment, \$48,728,000.

				FIXED	INVESTMENT: 5	48728000				
				SULFUR	BY-PRODUCT		TOTAL OP. COST		_	
		501/53 (1)/53	00.150 UNIT	REMOVED	RATE.		INCLUDING		NET ANNUAL	CUMULATIVE
	ANNUAL OPERA-	POWER UNIT HEAT	POWER UNIT	BY	EQUIVALENT	NET REVENUE,	REGULATED	TOTAL	INCREASE	NET INCREASE
	TION.	REQUIREMENT.	FUEL	POLLUTION CONTROL	TONS/YEAR	\$/TON	ROI FOR POWER	NET SALES	(DECREASE) IN COST OF	(DECREASE) In cost of
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	DRY	DRY	COMPANY.	REVENUE,	POWER.	POWER.
START		/YEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	S/YEAR	S	S
•					302.23					
1	7000	31500000	1500000	35000	184200	0.0	18292200	0	18292200	18292200
2	7000	31500000	1500000	35000	184200	0.0	18024600	0	18024600	36316800
3	7000	31500000	1500000	35000	184200	0.0	17757000	0	17757000	54073800
4	7000	31500000	1500000	35000	184200	0.0	17489400	0	17489400	71563200
5	7000	31500000	1500000	35000	184200	<u>&•</u> g	17221800	ğ-	17221800_	68765000
6 7	7000 7000	31500000	1500000	35000	184200	0.0 0.0	16954100	0	16954100	105739100
8	7000	31500000 31500000	1500000 1500000	35000 35000	184200 184200	0.0	16686500 16418900	ŏ	16686500 16418900	122425600 138844500
9	7000	31500000	1500000	35000	184200	0.0	16151300	0	16151300	154995800
_10 _	7000	31500000	1500000	35000	184200	0.0	15883700	0	15863700	170879500
11	5000	22500000	1071400	25000	131600	0.0	13871300	-	13871300	184750800
12	5000	22500000	1071400	25000	131600	0.0	13603700	Ŏ	13603700	198354500
13	5000	22500000	1071400	25000	131600	0.0	13336000	0	13336000	211690500
14	5000	22500000	1071400	25000	131600	0.0	13068400	0	13068400	224758900
_15	5000	22500000	1071400	25000	131600	Q_Q	12800800	Q_	12800800	237559700
16	3500	15750000	750000	17500	92100	0.0	11169400	0	11169400	248729100
17	3500	15750000	750000	17500	92100	0.0	10901800	0	10901800	259630900
18	3500	15750000	750000	17500	92100	0.0	10634200	0	10634200	270265100
19	3500	15750000	750000	17500	92100	0.0	10366500	0	10366500	280631600
-50	3500	15750000	750000	17500	92100	<u></u>	10098900	ğ	10028200_	290730500
21	1500	6750000	321400	7500 7500	39500	0.0	7868600	0	7868600	298599100 306200100
22 23	1500 1500	6750000 6750000	321400	7500 7500	39500 39500	0.0 0.0	7601000 7333400	Ů	7601000 7333400	313533500
24	1500	6750000	321400 321400	7500 7500	39500	0.0	7065800	Ŏ	7065800	320599300
_25	1500	6750000	321400	7500 7500	39500	9.0	6798200	0	6798200	327397500
26	1500	6750000	321400	7500	39500	0.0	6530500	0	6530500	333928000
27	1500	6750000	321400	7500	39500	0.0	6262900	ŏ	6262900	340190900
28	1500	6750000	321400	7500	39500	0.0	5995300	Ō	5995300	346186200
29	1500	6750000	321400	7500	39500	0.0	5727700	0	5727700	351913900
_30	1500	5750000	321400	7500	39500	Q.Q	5460100	Q	5460100	357374000
TOT I		573750000 VERAGE INCREAS	27321000	637500	3355500		357374000	o	357374000	
Lir	CIIME M		S PER TON OF C		ING COST		13.08	0.0	13.08	
			PER TOWATT-H				5.61	0.0	5.61	
			PEH MILLION HT				62.29	0.0	62.29	
			PER TON OF SI				560.59	0.0	560.59	
PROCES	S COST	DISCOUNTED AT	11.6% TO INI	TIAL YEAR+ DOL	LARS		127709200	0	127709200	
LEV	ELIZED	INCREASE (DECR	EASE) IN UNIT	OPERATING COS	T EQUIVALENT TO	DISCOUNTED PRO	CESS COST OVER	LIFE OF	POWER UNIT	
			PER TON OF CO				11.99	0.0	11.99	
		MILLS P	ER KILOWATT-HO	DUR			5.14	0.0	5.14	
			ER MILLION BTU				57.10	0.0	57.10	
		DOLLARS	PER TON OF SE	JLFUR REMOVED			513.92	0.0	513.92	

TABLE A-16. LIMESTONE SLURRY PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(500-MW new coal-fired power unit, 5.0% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller) Feed preparation (feeders, crushers, ball mills, hoist,	1,931,000	6.6
tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	2,028,000	6.9
dampers from absorber to reheater and stack) dampers from absorber to reheater and stack) SO ₂ absorption (four TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators,	4,327,000	14.8
and pumps) Stack gas reheat (four indirect steam reheaters) Solids disposal (onsite disposal facilities including feed	8,948,000 1,283,000	30.6 4.4
tank, agitator, slurry disposal pumps, and pond water return pumps)	1,957,000	6.7
Subtotal	20,474,000	70.0
Services, utilities, and miscellaneous	1,228,000	4.2
Total process areas excluding pond construction	21,702,000	74.2
Pond construction	7,553,000	25.8
Total direct investment	29,255,000	100.0
Indirect Investment		
Engineering design and supervision Architect and engineering contractor Construction expense Contractor fees	1,274,000 275,000 3,911,000 1,249,000	4.4 0.9 13.3 4.3
Total indirect investment	6,709,000	22.9
Contingency	7,193,000	24.6
Total fixed investment	43,157,000	147.5
Other Capital Charges		
Allowance for startup and modifications Interest during construction	3,560,000 5,179,000	12.2 17.7
Total depreciable investment	51,896,000	177.4
Land Working capital	1,511,000 1,214,000	5.2 4.1
Total capital investment	54,621,000	186.7

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979. Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared. Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP. Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-17. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW new coal-fired power unit, 5.0% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantity	Unit cost, \$	Total annual cost, \$	% of average annual revenu requirements
Direct Costs				
Raw materials				
Limestone	266,500 tons	7.00/ton	1,865,500	11.64
Total raw materials cost			1,865,500	11.64
Conversion costs				
Operating labor and supervision Utilities	27,910 man-hr	12.50/man-	hr 348,900	2.18
Steam	489,800 MBtu	2.00/MBtu	979,600	6.11
Process water	295,300 kgal	0.12/kgal	35,400	0.22
Electricity	59,828,000 kWh	0.029/kWh	1,735,000	10.82
Maintenance				
Labor and material			1,962,800	12.24
Analyses	4,040 man-hr	17.00/man-	h r 68,700	0.43
Total conversion costs			5,130,400	32.00
Total direct costs			6,995,900	43.64
Indirect Costs				
Capital charges				
Depreciation, interim replacement insurance at 6.0% of total depre				
investment	0 6%		3,113,800	19.42
Average cost of capital and taxes of total capital investment	3 at 0.0%		4,697,400	29.30
Overheads				
Plant, 50% of conversion costs 1			1,190,200	7.42
Administrative, 10% of operating	labor		34,900	0.22
Total indirect costs	-		9,036,300	56.36
Total average annual revenue	requirements		16,032,200	100.00
	Ş Mills/kWh	ton coal	,,, ,,	short ton removed
	LITTS / KAU	Darnea	Tubur 2	r emo Aeri
Equivalent unit revenue requiremen	ts 4.58	10.69	0.51	295.91

a. Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.
Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh.
Stack gas reheat to 175 F.

S removed, 54,180 short tons/yr; solids disposal 285,140 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$29,255,000; total depreciable investment, \$51,896,000; and total capital investment, \$54,621,000.

TABLE A-18

LIMFSTONE SLURRY PROCESS 500 MW NEW COAL-FIRED POWER UNIT 5% S IN COAL+ REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: 5	54621000				
				SULFUR	8Y-PRODUCT		TOTAL OP. COST			
				REMOVED	RATE		INCLUDING		NET ANNUAL	CUMULATIVE
YEARS	ANNUAL	POWER UNIT	POWER UNIT	BY	FRUIVALENT	NET REVENUE.	REGULATED	TOTAL	INCREASE	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	ROI FOR	NET	(DECREASE)	(DECREASE)
	TION.	REQUIREMENT.	CONSUMPTION.	CONTROL	7.7.757 (24	37 1 0.1	POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	gey	DRY	COMPANY.	REVENUE.	POWER.	POWER.
STAPT		TYEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	S/YEAR	S/YEAR	\$	\$
	7000	31500000	1500000	54200	285100		20730200		20730200	20730200
ż	7000	31500000	1500000	54200	265100	0.0	20432700	0	20432700	41162900
3	7000	31500000	1500000	54200	285100	0.0	20135100	0	20135100	61298000
Ă	7000	31500000	1500000	54200	285100	0.0	19837600	ŏ	19837600	81135600
5	7000	31500000	1500000	54200	245100	0.0	19540000	ő	19540000	100675600
6	7000	31500000	1500000	54200	285100	0.0	19242500		19242500	119918100
7	7000	31500000	1500000	54200	285100	0.0	18945000	ō	18945000	138863100
8	7000	31500000	1500000	54200	285100	0.0	18647400	Ō	18647400	157510500
9	7000	31500000	1500000	54200	285100	0.0	18349900	0	18349900	175860400
10	7000	31500000	1500000	54200	285100	0.0	18052300	Q	18052300_	193912700
11	5000	22500000	1071400	38700	203700	0.0	15715600	0	15715600	209628300
12	5000	22500000	1071400	38700	203700	0.0	15414000	0	15418000	225046300
13	5000	22500000	1071400	38700	203700	0.0	15120500	0	15120500	240166800
14	5000	22500000	1071400	38700	203700	0.0	14823000	0	14823000	254989800
.15	5000	22509090	1071400	3 <u>*</u> 700	203100		14525400	0_	14525400_	269515200
16	3500	15750000	750000	27100	142600	0.0	15634000	0	12634000	282154200
17	3500	15750000	750000	27100	142600	0.0	12341400	0	12341400	294495600
18	3500	15750000	750000	27100	142600	0.0	12043900	0	12043900	306539500
19	3500	15750000	750000	27100	142600	0.0	11746300	0	11746300	318285800
20	3500	15750000	750000	27100	142600	<u>0</u> - <u>0</u>	11448800	<u>0</u> -	11448800_	329734600
21 21	1500	6750000 6750000	321400	11600	61100	0.0	8876900 8579200	Ů,	8876800 8579200	338611400 347190600
23	1500 1500	6750000	321400 321400	11600 11600	61100 61100	0.0 0.0	8281700	0	8281700	355472300
24	1500	6750000	321400	11600	61100	0.0	7984100	0	7984100	363456400
24 _ 25	1500	6750000	321400	11600	61100	0.0	Z646500	0	7686600_	371143000
26	1500	6750000	321400	11600	61100	0.0	7389000		7389000	378532000
27	1500	6750000	321400	11600	61100	0.0	7091500	ŏ	7091500	385623500
28	1500	6750000	321400	11600	61100	0.0	6794000	ŏ	6794000	392417500
29	1500	6750000	321400	11600	61100	0.0	6476400	Ō	6496400	398913900
30	1500	6750000	321400	11600	61100	0.0	6178500	<u></u> 0-	6198900	405112800
	127500 FETIME A	573750000 VERAGE INCREA	27321000 SE (DECREASE)	987000 IN UNIT OPERAT	5193500		405112800	0	405112800	
LI			S PER TON OF C		1.10 0031		14.83	0.0	14.83	
			PER KILOWATT-H				6.35	0.0	6.35	
			PER MILLION BT				70.61	0.0	70.61	
			S PER TON OF S				410.45	0.0	410.45	
PROCES	S COST	DISCOUNTED AT	11.6% TO INI	TIAL YEAR+ DOL	LARS		144837500	0	144837500	
LFV	ELIZED	INCREASE (DECE	REASE) IN UNIT	OPERATING COS	T EQUIVALENT TO	DISCOUNTED PROC	ESS COST OVE	R LIFE OF		
			PER TON OF CO				13.60	0.0	13.60	
			PER KILOWATT-HO				5.83	0.0	5.83	
			ER MILLION BTU				64.76	0.0	64.76	
			PER TON OF SL				376.40	0.0	376.40	

TABLE A-19. LIMESTONE SLURRY PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(1000-MW existing coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller) Feed preparation (feeders, crushers, ball mills, hoist,	2,434,000	5.9
tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	2,412,000	5.9
dampers from absorber to reheater and stack) 50 absorption (four TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators,	8,690,000	21.2
<pre>and pumps) Stack gas reheat (four indirect steam reheaters) Solids disposal (onsite disposal facilities including feed tank, agitator, slurry disposal pumps, and pond water return</pre>	14,301,000 2,026,000	35.0 4.9
pumps)	2,316,000	5.7
Subtotal	32,179,000	78.6
Services, utilities, and miscellaneous	1,931,000	4.7
Total process areas excluding pond construction	34,110,000	83.3
Pond construction	6,856,000	16.7
Total direct investment	40,966,000	100.0
Indirect Investment		
Engineering design and supervision Architect and engineering contractor Construction expense Contractor fees	1,255,000 273,000 5,323,000 1,613,000	3.1 0.7 13.0 <u>3.9</u>
Total indirect investment	8,464,000	20.7
Contingency	9,886,000	24.1
Total fixed investment	59,316,000	144.8
Other Capital Charges		
Allowance for startup and modifications Interest during construction	5,246,000 7,118,000	12.8 17.4
Total depreciable investment	71,680,000	175.0
Land Working capital	1,376,000 1,774,000	3.4
Total capital investment	74,830,000	182.7

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.
Disposal pond located 1 mi from power plant.
Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

TABLE A-20. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

${\tt REGULATED~UTILITY~ECONOMICS}^{\bf a}$

(1000-MW existing coal-fired power unit. 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantity	Unit cost, \$	Total annual cost, \$	% of average annual revenu- requirements
Direct Costs				
Raw materials				
Limestone	320,600 tons	7.00/ton	2,244,200	9.65
Total raw materials cost			2,244,200	9.65
Conversion costs				
Operating labor and supervision Utilities	36,750 man-hr	12.50/man-H	r 459,400	1.98
Steam	979,700 MBtu	2.00/MBtu	1,959,400	8.43
Process water	503,400 kgal	0.12/kgal	60,400	0.26
Electricity	113,344,000 kWh	0.028/kWh	3,173,600	13.65
Maintenance			,	-3.03
Labor and material			2,593,400	11.16
Analyses	6,100 man-hr	17.00/man-h		0.45
Total conversion costs			8,349,900	35.93
Total direct costs			10,594,100	45.58
Indirect Costs Capital charges Depreciation, interim replacemen	ts, and			
insurance at 6.4% of total depr investment			4,587,500	19.74
Average cost of capital and taxe of total capital investment	s at 8.6%		6,435,400	27.69
Overheads			• •	
Plant, 50% of conversion costs 1	ess utilities		1,578,300	6.79
Administrative, 10% of operating	labor		45,900	0.20
Total indirect costs			12,647,100	54.42
Total average annual revenue	requirements		23,241,200	100.00
	Mills/kWh	ton coal burned		short ton removed
Equivalent unit revenue requiremer	its 3.32	7.75	0.37	332,02

a. Basis

Remaining life of power plant, 25 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 2,999,850 tons/yr, 9,000 Btu/kWh. Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded.

Midwest plant location, 1980 revenue requirements.

S removed, 70,000 short tons/yr; solids disposal 368,400 tons/yr Ca solids including only hydrate water.

Total direct investment, \$40,966,000; total depreciable investment, \$71,680,000; and total capital investment, \$74,830,000.

TABLE A-21

LIMESTONE SLURRY PROCESS 1000 MM EXISTING COAL-FIRED MOMER UNIT 3.5% S IN COAL REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: 5	74830000				
AFTFR	ANNUAL OPERA- TION: KW-HR/ KW	POWER UNIT HEAT REQUIREMENT. MILLION HTU YYEAR	POWER UNIT FUEL CONSUMPTION • TONS COAL /YEAK	SULFUR PEMOVED AY POLLUTION CONTROL PROCESS* TONS/YEAR	PRUDUCT HATE; EQUIVALENT TONS/YEAR DRY SOLIDS	NET REVENUE, \$/TON DHY SULINS	TOTAL OP. COST INCLUDING REGULATED ROI FOR POWER COMPANY. \$/YEAR	TOTAL NET SALES REVENUE, \$/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER,	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER, \$
1 2 3 4										
	7000	63000000	3000000	70000	368400	0.0	29676700		29676700	29676700
7	7000	63000000	300000	70000	368400	0.0	29143500	Ö	29183500	58860200
ė	7000	63000000	3000000	70000	368400	0.0	28690300	Ö	28690300	87550500
9	7000	63000000	3000000	70000	368400	0.0	28197200	ŏ	28197200	115747700
1 <u>0</u>	7000	63000020	3000000	70000	368400	0.0	27704000	_ 0	27704000	143451700
11	5000	45000000	2142900	50000	263100	0.0	24114800	-	24114800	167566500
12	5000	45000000	2142900	50000	263100	0.0	23621600	0	23621600	191188100
13	5000	45000000	2142900	50000	263100	0.0	23128500	0	23128500	214316600
14	5000	45000000	2142900	50000	263100	0.0	22635300	0	22635300	236951900
_15	5000	45000000	2142900	50000	263110	O_Q	22142100	0_	22142100_	259094000
16	3500	31500000	1500000	35000	184200	0.0	19251200	0	19251200	278345200
17	3500	31500000	1500000	35000	184200	0.0	18758000	0	18758000	297103200
18	3500	31500000	1500000	35000	184200	0.0	18264900	0	18264900	315368100
19	3500	31500000	1500000	35000	184200	0.0	17771700	0	17771700	333139800
_20	3500	31500000	1500000	35000	184200	Q_Q	17276200	0_	17278500_	3504183Q0
21	1500	13500000	642900	15000	7×400	0.0	13349200	0	13389200	363807500
55	1500	13500000	642400	15000	78900	0.0	12846000	0	12896000	376703500
23	1500	13500000	642400	15000	78900	0.0	12402900	0	12402900	389106400
24	1500	13500000	642900	15000	78400	0.0	11909700	0	11909700	401016100
-25	1500	13520000	645580	15000	<u>[</u> 2729		11416600	<u>Q</u> -	11416600_	412432700
26	1500	13500000	642900	15000	7HY00	0.0	10923400	0	10923400	423356100
27	1500	13500000	642900	15000	74900	0.0	10430200	U	10430200 9937100	433786300 443723400
28	1500	13500000	642900	15000	74900	0.0	9937100	Ü	9443900	453167300
29	1500	13500000	642900	15000	78900	0.0	9443900	Ü	8950800_	462118100
_30	1500	13500000	642900	15000	78900		8¥50900	¥	3X3KOAA-	INCLIMATE
TOT	92500	832500000 VERAGE TACREA	39643500 SE (DECHEASE)	925000 IN UNIT OPERAT	4867500		462118100	0	462118100	
			S PER TON OF C				11.66	0.0	11.66	
			PFR KILOWATT-H				5.00	0.0	5.00	
			PER MILLION HT				55.51	0.0	55.51	
			S PER TON OF S				499.59	0.0	499.59	
PROCES	S COST		11.6% TO INI		LARS		188891100	0	188891100	
I F	/ELIZED	INCREASE (DEC	REASE) IN UNIT	OPERATING COS	T EUIIIVALENT TO	DISCOUNTED PRO	CESS COST OVE	LIFE OF	POWER UNIT	
			S PER TON OF C				10.52	0.0	10.52	
			PER KILOWATT-H				4.51	0.0	4.51	
			PER MILLION BT				50.07	0.0	50.07	
		DOLLAR	S PEP TON OF S	ULFUR REMOVED			450.71	0.0	450.71	

TABLE A-22. LIMESTONE SLURRY PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(1000-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller) Feed preparation (feeders, crushers, ball mills, hoist,	2,199,000	5.7
tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	2,229,000	5.7
dampers from absorber to reheater and stack) SO ₂ absorption (four TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators,	7,135,000	18.3
and pumps) Stack gas reheat (four indirect steam reheaters) Solids disposal (onsite disposal facilities including feed tank, agitator, slurry disposal pumps, and pond water return	13,087,000 1,875,000	33.7 4.8
pumps)	2,104,000	5.4
Subtotal	28,629,000	73.6
Services, utilities, and miscellaneous	1,718,000	4.4
Total process areas excluding pond construction	30,347,000	78.0
Pond construction	8,547,000	22.0
Total direct investment	38,894,000	100.0
Indirect Investment		
Engineering design and supervision Architect and engineering contractor Construction expense Contractor fees	1,299,000 277,000 5,019,000 1,551,000	3.3 0.7 12.9 4.0
Total indirect investment	8,146,000	20.9
Contingency	9,408,000	24.2
Total fixed investment	56,448,000	145.1
Other Capital Charges		
Allowance for startup and modifications Interest during construction	4,790,000 6,774,000	12.3 17.5
Total depreciable investment	68,012,000	174.9
Land Working capital	1,717,000 1,694,000	4.4
Total capital investment	71,423,000	183.6

Minimum in-process storage; only pumps are spared. Disposal pond located $1\ \mathrm{mi}$ from power plant.

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979. Stack gas reheat to 175°F by indirect steam reheat.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-23. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS $^{\mathbf{a}}$

(1000-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantity	Un cos	it t, \$	Total annual cost, \$	annu	f average al revenu uirements
Direct Costs						
Raw materials						
Limestone	309,900 to	ns 7.00	/ton	2,169,300	<u>)</u>	9.92
Total raw materials cost				2,169,300)	9.92
Conversion costs						
Operating labor and supervision Utilities	36,750 ma	n-hr 12.50	/man-hr	459,400)	2.10
Steam	947,000 ME		/MBtu	1,894,000)	8.66
Process water	487,200 kg		/kgal	58,500		0.27
Electricity	109,566,000 kV	n 0.028	/kWh	3,067,800)	14.03
Maintenance						
Labor and material			, .	2,380,700		10.88
Analyses	6,100 ma	m-hr 17.00	/man-hr	103,700	<u>)</u>	0.47
Total conversion costs				7,964,100)	36.41
Total direct costs				10,133,400)	46.33
Indirect Costs Capital charges						
Depreciation, interim replacemen insurance at 6.0% of total depr						
investment Average cost of capital and taxe	s at 8.6%			4,080,70)	18.65
of total capital investment Overheads	3 44 37 3%			6,142,40)	28.08
Plant, 50% of conversion costs 1	ess utilities			1,471,90	١	6.73
Administrative, 10% of operating				45,90		0.21
Total indirect costs				11,740,90	-)	53,67
Total average annual revenue	requirements			21,874,30	o	100.00
	Mills/k	\$/ton co Vh burned		Stu heat nput	\$/short S remov	
Equivalent unit revenue requiremen	ts 3.12	7.54		0.36	323.2	25

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 2,900,100 tons/yr, 8,700 Btu/kWh. Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$38,894,000; total depreciable investment, \$68,012,000; and total capital investment, \$71,423,000.

Midwest plant location, 1980 revenue requirements.

S removed, 67,670 short tons/yr; solids disposal 356,140 tons/yr Ca solids including only hydrate water.

TABLE A-24

LIMESTONE SLURRY PROCESS 1000 MW NEW COAL-FIRED POWER UNIT 3.5% S IN COAL. REGULATED CO. ECUNOMICS

				FIXED	INVESTMENT: 5	71423000				
							TOTAL			
				SULFUR	HY-PRODUCT		OP. COST			
WE 400		BOUES 411 22	BOUED 111.77	PEMOVED	RATE.	NET OFFICE	INCLUDING	70744	NET ANNUAL	CUMULATIVE
	ANNUAL	POWER UNIT	POWER UNIT	RY	EQUIVALENT	NET REVENUE.	REGULATED ROI FOR	TOTAL NET	INCREASE (DECREASE)	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	POWER	SALES	IN COST OF	(DECREASE)
UNIT	KM-HB/	REQUIREMENT.	CONSUMPTION. TONS COAL	CONTROL PROCESS•	DRY	DRY	COMPANY.	REVENUE.	POWER+	IN COST OF
START	KA -44	MILLION HTU /YEAR	YEAR	TUNS/YFAR	SOLIUS	SOLIDS	\$/YEAR	S/YEAR	PUWER.	POWER.
31441	~₩	/ ICAR	/ TCMT	TONSTIFAN	30,2103	300103	37 IE4N	37 TCMN		•
1	7000	60900000	2900000	67700	356100	0.0	28016100		28016100	28016100
2	7000	60900000	2900000	67700	356100	0.0	27626100	0	27626100	55642200
3	7000	60400000	2900000	67700	356100	0.0	27236200	0	27236200	82878400
•	7000	60900000	2900000	67700	356100	0.0	26846200	0	26846200	109724600
\$	7000	60200100	2900000	67700	356100	Q&Q	26456300	<u>Q</u> -	26456300_	136186560
6	7000	60900000	2900000	67700	356100	0.0	26066400	0	26066400	162247300
7	7000	60900000	2900000	67700	356100	0.0	25676400	0	25676400	187923700
A	7000	60900000	2900000	67700	356100	0.0	25286500	0	25286500	213210200
9	7000	60400000	2900000	67700	356100	0.0	24896500	0	24896500	238106700
.10	7999	60900000		67799	356100	QeQ	24506600	<u>-</u> -	24506600_	
11	5000	43500000	2071400	48400	254400	0.0	21155300	0	21155300	283768600
12	5000	43500000	2071400	44400	254400	0.0	20765400	0	20765400	304534000
13	5000	43500000	2071400	48400	254400	0.0	20375500	0	20375500	324909500
14	5000	43500000	2071400	48400	254400	0.0	19945500	0	19985500	344895000
-15	5000	43500000	2071400		254400	Q&Q	19595600	ñ-	19595600_	364490600
16	3500	30450000	1450000	33400	178100	0.0	16914400	0	16914400	381405000
17	3500	30450000	1450000	33+00	178100	0.0	16524500	0	16524500	397929500
18	3500	30450000	1450000	33400	178190	0.0	16134600	0	16134600	414064100
19	3500	30450000	1450000	33900	178100	0.0	15744600	0	15744600	429808700
-50	3500	30450000	1450000	33200	1 <u>78100</u>	<u></u>	15354700	<u>k</u> -	15354700_	445163400
21	1500	13050000	621400	14500	76300	0.0	11724600	0	11724600	456868000
53 52	1500	13050000	621400	14500	76300 76300	0.0 0.0	11334700 10944700	0	11334700 10944700	468222700 479167400
	1500	13050000	621400	14500 14500	76300	0.0	10554900	0	10554800	489722200
24 - 25	1500	13050000	621400		76300 76300	9.0	10164900	v	10164900_	499887100
	1500	13050000	621400	14500 14500	76300	0.U	9774900	- -	9774900	509662000
26 27	1500 1500	13050000 13050000	621400 621400	14500	76300	0.0	9385000	ň	9385000	519047000
28	1500	13050000	621400	14500	76300	0.0	8945000	ñ	8995000	528042000
29	1500	13050000	621400	14500	76300	0.0	8605100	ŏ	8605100	536647100
_30	1500	13050000	621400	14500	76300	Q.Q	8215200	ň	8215200	544862300
5 F	****	*********								ETIERBEE.
TOT	127500	1109250000	52#21000	1233500	6486500		544862300	0	544862300	
LI	FETIME A			IN UNIT OPERAT	ING COST					
			PER TON OF C	· - · · -			10.32	0.0	10.32	
			PER KILUWATT-H				4.27	0.0	4.27	
			PER MILLION PT				49.12	0.0	49.12	
			PER TON OF SI				441.72	0.0	441.72	
PROCES	S COST	DISCOUNTED AT	11.6% TU INI	TIAL YEAR+ DOLI	LARS		195672000	0	195672000	
LEV	ELIZED I				T EQUIVALENT TO	DISCOUNTED PROC	ESS COST OVE	K LIFE OF	POWER UNIT	
			PER TON OF CO				9.50	0.0	9.50	
			ER KILOWATT-HO				3.94	0.0	3.94	
			ER MILLION HTL				45.26	0.0	45.26	
		DOLLARS	PER TON OF SU	JLFUR HEMOVED			407.06	0.0	407.06	

TABLE A-25. LIMESTONE SLURRY PROCESS SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; trucking alternative)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller)	1,759,000	8.1
Feed preparation (feeders, crushers, ball mills, hoist,	1,739,000	0.1
tanks, agitators, and pumps)	1,740,000	8.0
Gas handling (common feed plenum and booster fans, gas ducts		
and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack)	4 210 200	20.0
SO, absorption (four TCA scrubbers including presaturators	4,318,000	20.0
and entrainment separators, recirculation tanks, agitators,		
and pumps)	8,918,000	41.2
Stack gas reheat (four indirect steam reheaters)	1,282,000	5.9
Solids disposal (thickener, drum filters, tanks, agitators,	2 (00 000	11 1
pumps, and conveyors)	2,400,000	11.1
Subtotal	20,417,000	94.3
Services, utilities, and miscellaneous	1,225,000	5.7
Total direct investment	21,642,000	100.0
Indirect Investment		
Engineering design and supervision	1,255,000	5.8
Architect and engineering contractor	314,000	1.5
Construction expense	3,208,000	14.8
Contractor fees	993,000	4.6
Total indirect investment	5,770,000	26.7
Contingency	5,482,000	25.3
Total fixed investment	32,894,000	152.0
Other Capital Charges		
Allowance for startup and modifications	3,289,000	15.2
Interest during construction	3,947,000	18,2
Total depreciable investment	40,130,000	185.4
Lend	361,000	1.7
Working capital	1,282,000	5.9
Trucking charge (including indirect charges)	534,000	2.5
Total capital investment	42,307,000	195.5

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979. Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Disposal area located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-26. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; trucking alternative)

_	Annua quanti		Unit cost, \$	Total annual cost,	annight revell
Direct Costs					
Raw materials Limestone	158,300	tons	7.00/ton	1,108,1	00 7.20
Total raw materials cost	150,500	20.10	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	1,108,1	
				1,100,1	00 7.30
Conversion costs					
Operating labor and supervision		man-hr	12.50/man	343,0	
Operating labor disposal equipment Utilities	•	man-hr	17.00/man	, •	00 4.71
Steam	489,800		2.00/MBt	, .	
Process water	247,400		0.12/kga		
· •	8,119,000		0.029/kW	-,,-	
Fuel	245,930	gal	0.60/ga1	. 147,6	00 0.97
Maintenance					
Labor and material				2,100,4	
Analyses		man-hr	17.00/man		00 0.45
Disposal land preparation	5.3	acres	1600/acr	e 8,5	0.06
Total conversion costs				6,276,8	00 41.37
Total direct costs				7,384,9	00 48.67
Indirect Costs					
Capital charges Depreciation, interim replacements, insurance at 6.0% of total depreci					
investment Average cost of capital and taxes a	t 8.6%			2,487,2	00 16.39
of total capital investment Overheads				3,633,4	00 23.95
Plant, 50% of conversion costs less		3		1,171,5	
Administrative, 10% of operating la	bor			54,4	00 0.36
Trucking labor				441,0	00 2.91
Total indirect costs				7,787,5	00 51.33
Total average annual revenue req	uirements			15,172,4	00 100.00
		٥	/ton coal	\$/MBtu heat	\$/short ton
	Mills		burned	1nput	S removed

a. Basis

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh. Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded.

Midwest plant location, 1980 revenue requirements. Remaining life of power plant, 30 yr.

S removed, 35,000 short tons/yr; solids disposal 184,200 tons/yr Ca solids including only hydrate water.

Total direct investment, \$21,642,000; total depreciable investment, \$40,130,000; and total capital investment, \$42,307,000.

LIMESTONE SLURRY PROCESS 500 Mb NEW COAL-FIRED POWER UNIT 3.5%5 IN COAL, TRUCKING, REGULATED CO. ECONOMICS

CLLLARS PER TON EF SULFUR FEMOVED

FIXED INVESTMENT: \$ 42307000 TOTAL SULFUR BY-PRUDUCT DP. COST REMOVED RATE, INCLUDING NET ANNUAL CUMULATIVE YEARS ANNUAL POWER UNIT POWER UNIT BY EQUIVALENT NET REVENUE. REGULATED TOTAL INCREASE NET INCREASE AFTER OPERA-HEAT FUEL POLLUTION TONS/YEAR (DECREASE) \$/TON ROI FOR NET (DECREASE) POWER TION. REQUIREMENT. CONSUMPTION. CONTROL POWER SALES IN COST OF IN COST OF PILLION BIL TEAS CEAL DRY CRY POWER, UNIT KK-ER/ PRECESS, COMPANY. REVENUE. POWER. SOLIDS SULIUS START K.W /YEAR /YEAR TONS/YEAR S/YEAR S/YEAR \$ 0.0 1500 COO 0.0 70C0 0.0 3150000C 1500C00 0.0 1500.000 .184203 17895700_ __91779200 0.0 0.0 0.0 3150000C 1500C00 0.0 .000000دنــ _1200.000 QQA DE. .16345200. -10 .نــ م 0.0 0.0 0.0 2250000C 6.0 1011400. 157500CC 750LDG 0.0 0.0 35C0 1575C00C 750C0C 0.0 0.0 25,0000 _20 157500CC 0_0 G_0 67500CC 0.0 3 95 00 0.0 67500CG 0.0 _25 _1500 321400. 39500. 0_0 67500CC 0.0 32 1400 0 -0 67500CC 32140C 0.0 0.0 __6750000__ 5919800_ _30_. _1500___ _321400_ Z400. 35500. 5919800. TOT 127500 LIFETIME AVERAGE INCREASE (CECREASE) IN UNIT OPERATING COST DULLARS PER TON OF COAL BURNED 13.65 0.0 13.65 PILLS PER KILCHATT-HOUR 0.0 5.85 5.85 64.98 CENTS PER MILLION BY HEAT INPUT 64 -98 0.0 DOLLARS PER TON OF SULFUR REMOVED 591.78 591.78 0-0 PROCESS (CST DISCELNIED AT 11.6% TO INITIAL YEAR, DOLLARS Ω LEVELIZED INCREASE (DECREASE) IN UNIT OPERATING COST EQUIVALENT TO DISCOUNTED PROCESS COST OVER LIFE OF POWER UNIT DILLARS PER TON UF CHAL BURNED 12.47 0.0 12.47 MILLS PER KILDWATT-HOUR 5.34 0.0 5.34 59.36 59.36 CENTS PER PILLION BYU HEAT INPUT 0.0

540.52

0.0

540.52

TABLE A-28. LIMESTONE SLURRY PROCESS SUMMARY OF ESTIMATED CAPITAL INVESTMENT $^{\mathrm{a}}$

(500-MW new coal-fired power unit, 3.5% S in coal; 90% SO₂ removal; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller) Feed preparation (feeders, curshers, ball mills, hoist,	1,788,000	6.6
tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	1,804,000	6.7
dampers from absorber to reheater and stack) SO ₂ absorption (four TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators,	4,323,000	16.0
and pumps) Stack gas reheat (four indirect steam reheaters) Solids disposal (onsite disposal facilities including feed tank, agitator, slurry disposal pumps, and pond water return	8,930,000 1,283,000	33.2 4.8
pumps)	1,752,000	6.5
Subtotal	19,880,000	73.8
Services, utilities, and miscellaneous	1,193,000	4.4
Total process areas excluding pond construction	21,073,000	78,2
Pond construction	5,867,000	21.8
Total direct investment	26,940,000	100.0
Indirect Investment		
Engineering design and supervision Architect and engineering contractor Construction expense Contractor fees	1,228,000 270,000 3,703,000 1,173,000	4.6 1.0 13.7 4.4
Total indirect investment	6,374,000	23.7
Contingency	6,663,000	24.7
Total fixed investment	39,977,000	148.4
Other Capital Charges		
Allowance for startup and modifications Interest during construction	3,411,000 4,797,000	12.7 17.8
Total depreciable investment	48,185,000	178.9
Land Working capital	1,175,000 1,077,000	4.4 3.9
Total capital investment	50,437,000	187.2

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared. Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

TABLE A-29. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW new coal-fired power unit, 3.5% S in coal; 90% SO₂ removal; onsite solids disposal)

<u>-</u>	Annual quantity	Unit cost, \$	Total annual cost, \$	% of average annual revenu- requirements
Direct Costs				
Raw materials				
Limestone	192,000 tons	7.00/ton	1,344,000	9.17
Total raw materials cost			1,344,000	9.17
Conversion costs				
Operating labor and supervision Utilities	25,990 man-hr	12.50/man-h	r 324,900	2.22
Steam	489,800 MBtu	2.00/MBtu	979,600	6.68
Process water	264,200 kgal	0.12/kgal	31,700	0.22
Electricity	7,197,000 kWh	0.029/kWh	1,658,700	11.32
Maintenance			, ,	
Labor and material			1,861,900	12.71
Analyses	3,760 man-hr	17.00/man-h		0.44
Total conversion costs			4,920,700	33.59
Total direct costs			6,264,700	42.76
Indirect Costs Capital charges Depreciation, interim replacements,	and			
insurance at 6.0% of total depreci				
investment			2,891,100	19.73
Average cost of capital and taxes a	at 8.6%		-,,	
of total capital investment			4,337,600	29.61
Overheads			, ,	
Plant, 50% of conversion costs less	utilities		1,125,400	. 7.68
Administrative, 10% of operating 1s	ibor		32,500	0.22
Total indirect costs			8,386,600	57.24
Total average annual revenue red	quirements		14,651,300	100.00
	Mills/kWh	\$/ton coal \$ burned	,	short ton removed
				358.22

Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh. Stack gas reheat to 175°F.

S removed, 40,900 short tons/yr; solids disposal 215,250 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$26,940,000; total depreciable investment, \$48,185,000; and total capital investment, \$50,437,000.

TABLE A-30

LIMESTONE SLURRY PROCESS 500 MW NEW COAL-FIPED POWER UNIT 3.5% S 90% REMOVAL REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: \$	50437000	****			
				SULFUR	BY-PRODUCT		TOTAL OP. COST		NET ANNUAL	CUMULATIVE
VE 400	ANNUAL	DOMES HATT	DONCO UNIT	REMOVED	RATE.	NET SEVENUE	INCLUDING	TOTAL	INCREASE	NET INCREASE
	OPERA-	POWER UNIT HEAT	POWER UNIT FUEL	BY POLLUTION	EQUIVALENT TONS/YEAR	NET REVENUE.	REGULATED ROI FOR	TOTAL NET	(DECREASE)	(DECREASE)
	TION.		CONSUMPTION.	CONTROL	TONSZTEAR	37 TUN	POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION RTU	TONS COAL	PROCESS.	DRY	DRY	COMPANY,	REVENUE.	POWER.	POWER.
START	KW	/YEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	S/YEAR	S S	S
31841	N	/ IC#K	/ ICMH	TONSTIEMA	300103	300103	#/ /EAR	37 TEAR	•	•
1	7000	31500000	1500000	40900	215300	0.0	18989300	0	18989300	18989300
5	7000	31500000	1500000	40900	215300	0.0	18713000	Ŏ	18713000	37702300
3	7000	31500000	1500000	40900	215300	0.0	18436700	Ō	18436700	56139000
4	7000	31500000	1500000	40900	215300	0.0	18160500	0	18160500	74299500
5	7000	31500000	1500000	40200	215300	0.0	17884200	Q	17884200	92183700
6	7000	31500000	1500000	40900	215300	0.0	17607900	0	17607900	109791600
7	7000	31500000	1500000	40900	215300	0.0	17331700	0	17331700	127123300
8	7000	31500000	1500000	40900	215300	0.0	17055400	0	17055400	144178700
9	7000	31500000	1500000	40900	215300	0.0	16779100	0	16779100	160957800
10	7000	31500000	1500000	40200	215300		16502900	Q	16502900	177460700
11	5000	22500000	1071400	29200	153800	0.0	14397800	0	14397800	191858500
12	5000	22500000	1071400	24500	153800	0.0	14121500	0	14121500	205980000
13	5000	22500000	1071400	29200	153800	0.0	13845300	Ō	13845300	219825300
14	5000	22500000	1071400	29200	153800	0.0	13569000	0	13569000	233394300
-15	5000	22500000	1071400	29200	153600	<u>0</u> •0	13292700		13292700_	246687000
16	3500	15750000	750000	20500	107600	0.0	11589100	0	11589100	258276100
17	3500	15750000	750000	20500	107600	0.0	11312800	0	11312800	269588900
18 19	3500 3500	15750000	750000	20500	107600	0.0	11036500	0	11036500 10760300	280625400 291385700
_	3500	15750000	750000	00005	107600 107600	0.0	10760300	Ü	10780300	<u>30186970</u> 0
-50	1500	15750000 6750000		00 <u>202</u>	46100	0.0	<u>10444000</u>		8156600	310026300
22	1500	6750000	321400	8800	46100	0.0	7450400	0	7880400	317906700
23	1500	6750000	321400	0068	46100	0.0	7604100	0	7604100	325510800
24	1500	6750000	321400	8800	46100	0.0	7327800	ň	7327800	332838600
_25	1500	6750000	321400	8800	46100		7051600	ň	7051600	339890200
26	1500	6750000	321400	8800	46100	0.0	6775300		6775300	346665500
27	1500	6750000	321400	8600	46100	0.0	6499000	ŏ	6499000	353164500
28	1500	6750000	321400	8800	46100	0.0	6255800	Ō	6222800	359387300
29	1500	6750000	321400	8600	46100	0.0	5946500	Ó	5946500	365333800
30	1500	6750000	321+00	8400	46100	0.0	5670200	Q	5670200	371004000
TOT 1	27500	573750000	27321000	745500	3921000		371004000	0	371004000	
LIF	FETIME A	VERAGE INCREAS	SE (DECREASE)	IN UNIT OPERAT	ING COST					
			FER TON OF C				13.58	0.0	13.58	
		MILLS F	PER KILOWATT-HO	DUH			5.82	0.0	5.82	
			PER MILLION BT				64.56	0.0	64.66	
			PER TON OF SE				497.66	0.0	497.66	
PROCES	S COST	DISCOUNTED AT	11.6% TO INIT	TIAL YEAR+ DOL	LARS		132602400	0_	132602400	
LEV	EL1ZED				T EQUIVALENT TO	DISCOUNTED PROC	CESS COST OVER	LIFE OF	POWER UNIT	
		DOLLARS	PER TON OF CO	AL BURNED			12.45	0.0	12.45	
			ER KILOWATT-HO				5.34	0.0	5.34	
			ER MILLION BTU				59.29	0.0	59.29	
		DOLLARS	PER TON OF SU	ILFUR RFMOVED			456.62	0.0	456.62	

TABLE A-31. LIMESTONE SLURRY PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT^a

(500-MW existing oil-fired power unit, 2.5% S in oil; 0.8 1b $SO_2/MBtu$ heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (hoppers, feeders, conveyors, elevators, bins, shaker, puller)	1,077,000	5.3
Feed preparation (feeders, crushers, ball mills, hoist, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	1,196,000	5.9
dampers from absorber to reheater and stack) SO, absorption (four TCA scrubbers including presaturators and entrainment separators, recirculation tanks, agitators,	4,447,000	21.9
and pumps) Stack gas reheat (four direct oil reheaters) Solids disposal (onsite disposal facilities including feed tank, agitator, slurry disposal pumps, and pond water return	8,377,000 726,000	41.3 3.6
pumps)	1,399,000	6.9
Subtotal	17,222,000	84.9
Services, utilities, and miscellaneous	1,033,000	5.1
Total process areas excluding pond construction	18,255,000	90.0
Pond construction	2,020,000	10.0
Total direct investment	20,275,000	100.0
Indirect Investment		
Engineering design and supervision Architect and engineering contractor Construction expense Contractor fees	1,101,000 257,000 3,018,000 945,000	5.4 1.3 14.8 <u>4.7</u>
Total indirect investment	5,321,000	26.2
Contingency	5,119,000	25.3
Total fixed investment	30,715,000	151.5
Other Capital Charges		
Allowance for startup and modifications Interest during construction	2,870,000 3,686,000	14.2 18.1
Total depreciable investment	37,271,000	183.8
Land Working capital	409,000 800,000	2.0
Total capital investment	38,480,000	189.8

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by direct oil-fired reheat.

Minimum in-process storage; only pumps are spared. Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP. Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-32. LIMESTONE SLURRY PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW existing oil-fired power unit, 2.5% S in oil; 0.8 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

Total % of average Annual Unit annual annual revenue quantity cost, \$ cost, \$ requirements Direct Costs Raw materials 62,410 tons 7.00/ton 436,900 3.82 Limestone 436,900 Total raw materials cost 3.82 Conversion costs 24,860 man-hr 12.50/man-hr 310,800 2.72 Operating labor and supervision Utilities 2,676,600 gal 0.40/gal 1,070,600 9.35 Fuel oil (No. 6) 174,700 kgal 0.12/kgal 21,000 Process water 0.18 0.029/kWh 45,618,000 kWh 1,322,900 11.56 Electricity Maintenance 1,541,200 13.46 Labor and material 3,590 man-hr 17.00/man-hr 61,000 0.53 Analyses 4,327,500 37,80 Total conversion costs 4,764,400 41.62 Total direct costs Indirect Costs Capital charges Depreciation, interim replacements, and insurance at 6.4% of total depreciable 2,385,300 20.84 investment Average cost of capital and taxes at 8.6% of total capital investment 3,309,300 28.91 956,500 8.36 Plant, 50% of conversion costs less utilities Administrative, 10% of operating labor 31,100 0.27 6,682,200 58.38 Total indirect costs 11,446,600 Total average annual revenue requirements 100.00

	Mills/kWh	\$/bbl oil burned	\$/MBtu heat input	\$/short ton S removed
Equivalent unit revenue requirements	3.27	2.15	0.35	770.81

Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 25 yr.

Power unit on-stream time, 7,000 hr/yr.

Oil burned, 5,350,000 bb1/yr, 9,200 Btu/kWh. Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded.

S removed, 14,850 short tons/yr; solids disposal 63,030 tons/yr Ca solids including only hydrate water.

Total direct investment, \$20,275,000; total depreciable investment, \$37,271,000; and total capital investment, \$38,480,000.

				FIXED	INVESTMENT: \$	38480000				
AFTER		POWER UNIT HEAT REQUIREMENT. MILLION BTU /YEAR	POWER UNIT FUFL CONSUMPTION. RARRELS OIL /YEAR	SULFUR REMOVED BY POLLUTION CONTROL PROCESS+ TUNS/YEAR	HY-PRODUCT RATE: EQUIVALENT TONS/YEAR DHY SOLIDS	NET REVENUE; \$/TON Dry Solids	TOTAL OP. COST INCLUDING REGULATED HOI FOR POWER COMPANY, \$/YEAR	TOTAL NET SALES REVENUE• \$/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER:	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER;
1 2 3 4 5										
6	7000	32200000	5324100	14800	63000	0.0	14755500		14755500	14755500
7	7000	32200000	5324100	14800	63000	0.0	14499000	ŏ	14499000	29254500
8	7000	32200000	5324100	14800	63000	0.0	14242600	ŏ	14242600	43497100
9	7000	32200000	5324100	14800	63000	0.0	13946200	Ō	13986200	57483300
10	7000	32200000	5324100	14800	63000	0.0	13729800	Q	13729800_	71213100
11	5000	23000000	3802900	10600	45000	0.0	12077300	0	12077300	83290400
12	5000	23000000	3802900	10600	45000	0.0	11820900	0	11820900	95111300
13	5000	23000000	3402900	10600	45000	0.0	11564400	0	11564400	106675700
14	5000	23000000	3802900	10600	45000	0.0	11304000	0	11308000	117983700
15	5000	23000000	3802900	10600	45000	<u>Q+Q</u>	11051600	Q	11051600_	129035300
16	3500	16100000	2662000	7400	31500	0.0	9701000	0	9701000	138736300
17 18	3500 3500	16100000	2662000	7400 7400	31500	0.0	9444600	0	9444600	148180900
19	3500	16100000	2662000 2662000	7400	31500 31500	0.0	9188100	Ü	9188100	157369000
_20	3500	16100000 16100000	2662000	7400	31500	0.0	8931700	Ü	8931700 <u>8675300</u>	166300700 174976000
21	1500	6900000	1140900	3200	13500	0.0	<u>8675300</u>	<u>V</u>	6832200-	181811500
22	1500	6900000	1140900	3200	13500	0.0	6579100	0	6579100	188390600
23	1500	6900000	1140900	3200	13500	0.0	6322700	ň	6322700	194713300
24	1500	6900000	1140900	3200	13500	0.0	6066200	ŏ	6066200	200779500
25	1500	6900000	1140900	3200	13500	0.0	5809800	ō	5809800_	206589300
26	1500	6900000	1140900	3200	13500	0.0	5553400		5553400	212142700
27	1500	6900000	1140900	3200	13500	0.0	5297000	0	5297000	217439700
28	1500	6900000	1140900	3200	13500	0.0	5040600	0	5040600	222480300
29	1500	6900000	1140900	3200	13500	0.0	4784200	0	4784200	227264500
_30	_1500	6900000	1140900	3200	13500	Q_Q	4527700		\$527700_	231792200
TOT LIF	92500 ETIME A	425500000 VERAGE INCREAS	70354000 SE (DECREASE)	196000 IN UNIT OPERATI	A32500 Ing Cost		231792200	0	231792200	
		DOLL 4RS	PER BARREL O	F OIL BURNED			3.29	0.0	3,29	
			PER KILOWATT-H				5.01	0.0	5.01	
			PER MILLION BT				54.48	0.0	54.48	
			PER TON OF S				1182.61	0.0	1182.61	
				TIAL YEAR, DULL			94271900	0	94271900	
LEV	ELIZED :				F EQUIVALENT TO	DISCOUNTED PHOC				
			PER BARREL O				2.96	0.0	2.96	
			ER KILOWATT-H				4.50	0.0	4.50	
			ER MILLION BT				48.89	0.0	48.89	
		DOLLARS	PER TON OF S	OLIUK KEMUTEU			1062.82	0.0	1062.85	

TABLE A-34. GENERIC DOUBLE-ALKALI PROCESS SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(200-MW existing coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts, and	961,000 550,000	7.3 4.2
dampers from absorber to reheater and stack) SO ₂ absorption (two tray towers including presaturators and entrainment separators, recirculation tanks, agitators, and	2,141,000	16.3
pumps)	4,354,000	33.1
Stack gas reheat (two indirect steam reheaters)	584,000	4.4
Reaction (tanks, agitators, and pumps) Solids separation (thickener, drum filters, tanks, agitators,	238,000	1.8
pumps, and conveyors)	1,555,000	11.8
Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond	-,,	1110
water return pumps)	891,000	6.8
Subtotal	11,274,000	85.7
Services, utilities, and miscellaneous	676,000	5.2
Total process areas excluding pond construction	11,950,000	90.9
Pond construction	1,197,000	9.1
Total direct investment	13,147,000	100.0
Indirect Investment		
Engineering design and supervision	1,099,000	8.4
Architect and engineering contractor	262,000	2.0
Construction expense	2,111,000	16.1
Contractor fees	680,000	5.1
Total indirect investment	4,152,000	31.6
Contingency	3,460,000	26.3
Total fixed investment	20,759,000	157.9
Other Capital Charges		
Allowance for showing and middle strong	1,956,000	1/ 0
Allowance for startup and modifications		14.9
Interest during construction	2,491,000	18.9
Total depreciable investment	25,206,000	191.7
Land	243,000	1.8
Working capital	557,000	4.3
Total capital investment	26,006,000	197.8

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-35. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(200-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

		Annual Luantity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Raw materials		04.050	10.00/		14 02
Lime		26,850 tons	42.00/ton	1,127,700	14.83
Soda ash		2,560 tons	90.00/ton	230,400	<u>3.0</u> 5
Total raw materials cost				1,358,100	17.98
Conversion costs					
Operating labor and supervision		22,490 man-hr	12.50/man-h	r 281,100	3.72
Utilities					
Steam		206,800 MBtu	2.00/MBtu	413,600	5.48
Process water		102,100 kgal	0.12/kgal	12,300	0.16
Electricity	12,2	270,000 kWh	0.031/kWh	380,400	5.04
Maintenance					
Labor and material				580,600	7.69
Analyses		2,630 man-hr	17.00/man-h	44,700	0.59
Total conversion costs				1,712,700	22.68
Total direct costs				3,070,800	.40.66
Indirect Costs					
capital charges Depreciation, interim replacements, a	ind				
insurance at 7.0% of total deprecial investment				1,764,400	23.36
Average cost of capital and taxes at of total capital investment	0.0%			2,236,500	29.61
Overheads Plant, 50% of conversion costs less Administrative, 10% of operating labo	itilities or			453,200 28,100	
Total indirect costs				4,482,200	59.34
Total average annual revenue requ	irements			7,553,000	100.00
	Mills/kWh	\$/ton coal burned	\$/MBtu heat input	\$/short ton S removed	
Equivalent unit revenue requirements	5.40	11.92	0.57	511.03	

Basis Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 20 yr. Power unit on-stream time, 7,000 hr/yr.

Coal burned, 633,500 tons/yr, 9,500 Btu/kWh.

Stack gas reheat to 175°F.

S removed, 14,780 short tons/yr; solids disposal 60,280 tons/yr Ca solids including only hydrate water. Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$13,147,000; total depreciable investment, \$25,206,000; and total capital investment, \$26,006,000.

					*********	24004000				
				FIXED	INVESTMENT: \$	26006000	TOTAL			
AFTER POWER	ANNUAL OPERA- TION:		POWER UNIT FUEL CONSUMPTION.	SULFUR REMOVED BY POLLUTION CONTROL	BY-PRODUCT RATE, Equivalent Tons/Year	NET REVENUE, \$/TON	OP. COST INCLUDING REGULATED ROI FOR POWER	TOTAL NET SALES	NET ANNUAL INCREASE (DECREASE) IN COST OF	CUMULATIVE NET INCREASE (DECREASE) IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	DRY	DRY	COMPANY.	REVENUE .	POWER.	POWER,
START	KW	/YEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	S/YEAR	S	5
1 2 3 4 5										
7 8 9 -10										
11	5000	9500000	452400	10600	43100	0.0	8903100	0	8903100	8903100
12	5000	9500000	452400	10600	43100	0.0	8686400	0	8686400	17589500
13	5000	9500000	452400	10600	43100	0.0	8469600	0	8469600	26059100
14	5000	9500000	452400	10600	43100	0.0	8252800	0	8252800	34311900
-15	5000	9500000	452400	10600	43100	<u> </u>	8036000	<u>-</u> -	8036000	42347900
16	3500	6650000	316700	7400	30100	0.0	7128500	0	7128500	49476400
17 8	3500 3500	6650000 6650000	316700 316700	7400 7400	30100 30100	0.0	6911700 6694900	0	6911700	56388100
19	3500	6650000	316700	7400	30100	0.0 0.0	6478200	0	6694900 6478200	63083000 69561200
2 <u>0</u>	3500	6650000	316700	7400	30100	Q.Q	6261400	ŭ	6261400	<u>1582260</u> 0
21	1500	2850000	135700	3200	12900	0.0	5061200		5061200	80883800
55	1500	2850000	135700	3200	12900	0.0	4844400	ŏ	4844400	85728200
23	1500	2850000	135700	3200	12900	0.0	4627700	ŏ	4627700	90355900
24	1500	2850000	135700	3200	12900	0.0	4410900	Ŏ	4410900	94766800
25	1500	2850000	135700	3200	12900	0.0	4194100	0	4194100	98960900
26	1500	2850000	135700	3200	12900	0.0	3977400		3977400	102938300
27	1500	2850000	135700	3200	12900	0 • 0	3760600	0	3760600	106698900
28	1500	2850000	135700	3200	12900	0.0	3543800	0	3543800	110242700
29	1500	2850000	135700	3200	12900	0.0	3327000	0	3327000	113569700
30	1500	2850000	135700	3200	12900		3110300		3110300	11000000
TOT LII	57500 FETIME A	109250000 VERAGE INCREAS	5202500 SE (DECREASE)	122000 IN UNIT OPERAT	495000 ING COST		116680000	0	116680000	
-		DOLLARS	S PER TON OF C	OAL BURNED			22.43	0.0	22.43	
		MILLS I	PER KILOWATT-H	OUR			10.15	0.0	10.15	
		CENTS F	PER MILLION BT	U HEAT INPUT			106.80	0.0	106.80	
			S PER TON OF S				956.39	0.0	956.39	
PROCES	S COST	DISCOUNTED AT	11.6% TO INI	TIAL YEAR+ DOL	LARS		53388600	0	53388600	
LEV	/ELIZED				T EQUIVALENT TO	DISCOUNTED PRO				
			PER TON OF C				20.75	0.0	20.75	
			ER KILOWATT-H				9.39	0.0	9.39	
			ER MILLION BIL				98.80	0.0	98.80	
		DULLARS	PER TON OF SU	JEPUR REMOVED			885.38	0.0	885.38	

TABLE A-37. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT $^{\mathbf{a}}$

(200-MW new coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts, and	846,000 489,000	6.6 3.8
dampers from absorber to reheater and stack) SO, absorption (two tray towers including presaturators and efitrainment separators, recirculation tanks, agitators, and	1,853,000	14.5
pumps)	3,926,000	30.7
Stack gas reheat (two indirect steam reheaters)	569,000	4.5
Reaction (tanks, agitators, and pumps)	209,000	1.6
Solids separation (thickener, drum filters, tanks, agitators,	207,000	1.0
pumps, and conveyor)	1 275 000	10.0
pumps, and conveyor) Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond	1,375,000	10.8
water return pumps)	776,000	6.1
Subtotal	10,043,000	78.6
Services, utilities, and miscellaneous	603,000	4.7
Total process areas excluding pond construction	10,646,000	83.3
Pond construction	2,141,000	16.7
Total direct investment	12,787,000	100.0
Indirect Investment		
Engineering design and supervision	1,140,000	8.9
Architect and engineering contractor		2.1
Construction expense	266,000	
	2,025,000	15.8
Contractor fees	666,000	5,2
Total indirect investment	4,097,000	32.0
Contingency	3,377,000	26.4
Total fixed investment	20,261,000	158.4
Other Capital Charges		
Allowance for startup and modifications	1,812,000	14.2
Interest during construction	2,431,000	19.0
Total depreciable investment	24,504,000	191.6
Land	425,000	3.3
Working capital	548,000	4.3
- •		
		199.2

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175 F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-38. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(200-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Ann quan		Unit cost, \$	annual a	% of average nnual revenue requirements
Direct Costs					
Raw materials					
Lime	26,010	tons	42.00/ton	1,092,400	15.24
Soda ash	2,480	tons	90.00/ton	223,200	3.12
Total raw materials cost				1,315,600	18.36
Conversion costs					
Operating labor and supervision Utilities	22,490	man-hr	12.50/man-hr	281,100	3.92
Steam	200,300	MBtu	2.00/MBtu	400,600	5.59
Process water	98,700	kgal	0.12/kga1	11,800	0.16
Electricity	11,880,000	kWh	0.031/kWh	368,300	5.14
Maintenance					
Labor and material				596,500	8.32
Analyses	2,630	man-hr	17.00/man-hr	44,700	0.62
Total conversion costs				1,703,000	23.75
Total direct costs				3,018,600	42.11
Indirect Costs					
Capital charges Depreciation, interim replacements and	d				
insurance at 6.0% of total depreciab	le				
investment	0 69			1,470,200	20.51
Average cost of capital and taxes at of total capital investment Overheads	5.0%			2,191,000	30.56
Plant, 50% of conversion costs less w Administrative, 10% of operating lab				461,200 28,100	6.43 0.39
Total indirect costs				4,150,500	57.89
Total average revenue requirements				7,169,100	100.00
	Mills/kWh	\$/ton coal	\$/MBtu heat input	\$/short tor S removed	i
				o removed	

a. Basis

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 613,000 tons/yr, 9,200 Btu/kWh.

Stack gas reheat to 175°F.

Midwest plant location, 1980 revenue requirements.

S removed, 14,310 short tons/yr; solids disposal 58,360 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$12,787,000; total depreciable investment, \$24,504,000; and total capital investment, \$25,477,000.

GENERIC DOUBLE ALKALI PROCESS 200 MN NEW COAL-FIRED POWER UNIT 3.5% S IN CUAL, REGULATED CO ECONOMICS

FIXED INVESTMENT: \$ 25477000

						2311100	TOT AL			
				SULFUR	BY-PRODUCT		DP. (DST			
				REMOVED	RATE,		INCLUDING		NET ANNUAL	CUMULATIVE
YEARS	ANNUAL	POWER UNIT	PONER UNIT	BY	EQUIVALENT	NET REVENUE.	REGULATED	TOTAL	INCREASE	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	ROI FOR	NET	(DECREASE)	
	TION.		CONSUMPTION,	CONTROL	VONS/ VERN	47.00	POWER	SALES	IN COST OF	IN COST OF
UNIT		MILLION BTU	TONS COAL	PROCESS,	DRY	DRY	COMPANY.	REVENUE,	POWER.	POWER.
START		/YEAR	/YEAR	TONS/YEAR	\$0L 1D 5	SULIDS	\$/YEAR	\$/YEAR	\$	\$
JIANI	N.W	/ ILAn	/ ILAN	IUNS/ ICAN	306 103	306193	47 1 LAN	37 1 L AK	•	•
1	7000	12880000	613300	14300	5 84 0 0	0.0	9360000	0	9360000	9360000
2	7000	12880000	613300	14300	58400	0.0	9219600	0	9219600	18579600
3	7000	12880000	613300	14300	58400	0.0	9079100	0	9079100	27658700
4	7000	12880000	613300	14300	58400	0.0	89386))	0	8938600	36597300
5	7000	12880000	613300	14300	58400	0_0	6798100		8798100_	453£5400
6	7000	12880000	613300	14300	58400	0 -0	8657633	0	8657600	5405 3000
7	7000	12880000	613300	14300	58400	0.0	8517100	0	8517100	62570100
8	7000	12880000	613300	14300	58400	û.O	83766))	0	8376600	70946700
9	7000	12880000	613300	14300	58400	0.0	8236100	0	8236100	79182800
70	Z000	12880000	613300	14300	58400	0_0_	8095630		8095600	<u>8727840</u> 0
11	5000	9200000	438100	10200	41700	0.0	7081500	0	7081500	94359900
12	5000	9200000	438100	10200	41700	0 •0	6941100	0	6941100	101301000
13	5000	9200000	438100	10200	41700	0.0	6800600	0	6800 € 00	108101600
14	5000	9200000	438100	10200	41700	0.0	6660100	0	6660100	114761700
_15	5000	9200000	438100	10200	41200	0_0	6519600	a_	6519600_	121281300
16	3500	6440000	306 700	7200	2 92 00	0 -0	5699900	0	5699900	126981200
17	3500	6440000	306700	7200	29200	0.0	5559400	0	5559400	1 32 54 0 600
18	3500	6440000	306700	7200	29200	0.0	5418900	0	5418 900	137959500
19	3500	6440000	306 700	7200	29200	0.0	5278400	0	5278400	14 32 3 7 9 0 0
_20	3500	6640000	306700	7200	29200	0_0	5137920		5137900_	148375800
21	1500	2760000	131400	3100	12500	0 -0	4028333	0	4028300	152404100
22	1500	2760000	131400	3100	1 25 00	0.0	3887800	0	3887800	156291900
23	1500	2760000	131400	3100	12500	C -O	374 73))	0	3747300	16003 9200
24	1500	2760000	131400	3100	12500	0.0	3606800	0	3606800	163646000
_25	1500	2760000	131400	3100	12500	0 _0	3666300		3466300_	167112300
26	1500	2760000	131400	3100	1 2500	0.0	3325800	0	3325 800	170438100
27	1500	2760000	131400	3100	1 2500	0 -0	3185300	0	31#5300	173623400
28	1500	2760000	131400	3100	1 2500	0.0	3044800	0	3044 800	176668200
29	1500	2760000	131400	3100	12500	0.0	2904300	0	2904300	179572500
30	1500	2760000	131400	3100	12500		2763800		2763800	182336300
								•		
	127500	234600000	11171000	261000	1063500		182336300	0	182336300	
LI	LELIME A		SE (CECREASE)		LING COST				14 23	
			S PER TON CF C				16.32	0.0	16.32	
			PER KILOWATT-H				7.15	0.0	7.15	
			PER MILLION BT				77.72	0.0	77.72	
			S PER TON OF S				698-61	0.0	698.61	
PKUCE	33 CUST	DISCOUNIED AT	11.63 TO INI	TIAL YEAR, DUI	LAKS		65224800	0	65224800	
LE	AFFISED				I EQUIVALENT T	O DISCOUNTED PRO				
			S PER TON OF C				14.98	0.0	14 - 98	
			PER KILDWATT-H				6.56	0.0	6.56	
		-	PER MILLION BT				71.33	0.0	71 .33	
		DOLLAR	S PER TON OF S	ULFUR REMOVED			641.98	0-0	641.98	

à

TABLE A-40. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT^a

(500-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direc investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders)	1,927,000	6.7
Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts, and	932,000	3, 3
dampers from absorber to reheater and stack) SO ₂ absorption (four tray towers including presaturator s an d entrainment separators, reciruclation tanks, agitators, and	5,058,000	17.6
pumps)	10,126,000	35.4
Stack gas reheat (four indirect steam reheaters)	1,312,000	4.6
Reaction (tanks, agitators, and pumps) Solids separation (thickener, drum filters, tanks, agitators,	404,000	1.4
pumps, and conveyor)	2,643,000	9.2
Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond water return	2,043,000	7.2
pumps)	1,424,000	_5.0
Subtotal	23,826,000	83.2
Services, utilities, and miscellaneous	1,430,000	_5.0
Total process areas excluding pond construction	25,256,000	88.2
Pond construction	3,377,000	11.8
Total direct investment	28,633,000	100.0
Indirect Investment		
Engineering design and supervision	1,416,000	5.0
Architect and engineering contractor	328,000	1.1
Construction expense	4,004,000	14.0
Contractor fees	1,229,000	4.3
Total indirect investment	6,977,000	24.4
Contingency	7,122,000	24.8
Total fixed investment	42,732,000	149.2
Other Capital Charges		
Allowance for startup and modifications	3 034 002	
	3,936,000	13.8
Interest during construction	5,128,000	17.9
Total depreciable investment	51,796,000	180.9
Land	678,000	2.4
Working capital	1,201,000	4.2
Total capital investment	53,675,000	187.5

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°P by indirect steam reheat.

Minimum in-process storage; only pumps are spared. Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-41. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantit		Unit cost	-	annual a	% of average nnual revenu requirements
Direct Costs						
Raw materials						
Lime	65,010		42.00/		2,730,400	17.68
Soda ash	6,190	tons	90.00/	ton	557,100	3.61
Total raw materials cost					3,287,500	21.29
Conversion costs						
Operating labor and supervision Utilities	34,500	man-hr	12.50	man-hr	431,300	2.79
Steam	500,700	MBtu	2,00/	MBtu	1,001,400	6.49
Process water	247,000		0.12		29,600	0.19
Electricity	29,700,000		0.029		861,300	5.58
Maintenance	,,		,		,	
Labor and material					1,016,400	6.58
Analyses	4,560	man-hr	17.00	man-hr	77,500	0.50
Total conversion costs					3,417,500	22.13
Total direct costs					6,705,000	43.42
Indirect Costs						
Capital charges Depreciation, interim replacements, insurance at 6.4% of total deprecia	and ble					
investment Average cost of capital and taxes at					3,314,900	21.47
of total capital investment	. 0.0%				4,616,100	29.89
Overheads Plant, 50% of conversion costs less	utilities				762,600	4.94
Administrative, 10% of operating lab	or				43,100	0.28
Total indirect costs					8,736,700	56.58
Total average annual revenue requ	irements				15,441,700	100.00
	Mills/kWh	\$/ton buri		\$/MBtu hea input	t \$/short to S removed	
Equivalent unit revenue requirements	4.41	10.		0.48	431.57	_

a. Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 25 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,533,350 tons/yr, 9,200 Btu/kWh.

Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded.

S removed, 35,780 short tons/yr; solids disposal 145,931 tons/yr Ca solids including only hydrate water.

Total direct investment, \$28,633,000; total depreciable investment, \$51,796,000; and total capital investment, \$53,675,000.

TABLE A-42

GENERIC DOUBLE ALKALI PROCESS 500 MW EXISTING COAL-FIRED POWER UNIT 3.5% 5 IN COAL+ REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: \$	53675000				
AFTER		POWER UNIT HEAT REQUIREMENT, MILLION BTU /YEAR	POWER UNIT FUEL CONSUMPTION, TONS COAL /YEAR	SULFUR REMOVED BY POLLUTION CONTROL PROCESS+ TONS/YEAR	BY-PRODUCT PATE+ EQUIVALENT TONS/YEAR DRY SOLIDS	NET REVENUE, \$/TON DRY SOLIDS	TOTAL OP. COST INCLUDING REGULATED ROI FOR POWER COMPANY, \$/YEAR	TOTAL NET SALES REVENUE+ \$/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER, \$	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER, \$
1 2 3 4										
	7000	32200000	1533300	35800	145900	0.0	20058100		20058100	20058100
7	7000	32200000	1533300	35800	145900	0.0	19701800	Ō	19701800	39759900
8	7000	32200000	1533300	35800	145900	0.0	19345400	0	19345400	59105300
9	7000	32200000	1533300	35800	145900	0.0	18989100	Ō	18989100	78094400
10	7000	32200000	1533300	35800	145900	0.0	18632700	0	18632700_	96727100
11	5000	23000000	1095200	25600	104200	0.0	16333300	0	16333300	113060400
12	5000	23000000	1095200	25600	104200	0.0	15976900	0	15976900	129037300
13	5000	23000000	1095200	25600	104200	0.0	15620600	0	15620600	144657900
14	5000	23000000	1095200	25600	104200	0.0	15264200	0	15264200	159922100
15	5000	23000000	1095200	25600	104200	0.0	14907900		14907900	174830000
16	3500	16100000	766700	17900	73000	0.0	13056000	0	13056000	187886000
17	3500	16100000	766700	17900	73000	0.0	12699700	0	12699700	200585700
18	3500	16100000	766700	17900	73000	0.0	12343300	0	12343300	212929000
19	3500	16100000	766700	17900	73000	0.0	11987000	0	11987000	224916000
-20	3500	161000000	766700	17900	73000	0_0	11630600	<u>-</u>		236546600
21	1500	6900000	328600	7700	31300	0.0	9180300	0	9180300	245726900
22	1500	6900000	328600	7700	31300	0.0	8823900	0	8823900	254550800
23	1500	6900000	328600	7700	31300	0.0	8467600	0	8467600	263018400
24	1500	6900000	328600	7700	31300	0.0	8111200	Ů	8111200	271129600
_25	1500	6900000	328600	7700	31300] • <u>}</u>		-	7398500	<u>27888450</u> 0 286283000
26 27	1500	6900000	328600	7700 7700	31300	0.0	7348500 7042200	0	7042200	293325200
27 28	1500 1500	6900000 6900000	328600 328600	7700	31300 31300	0.0 0.0	6685800	ŏ	6685800	300011000
29	1500	6900000	328600	7700	31300	0.0	6329500	ŏ	6329500	306340500
30	_1500	6900000	328600	7700	31300	0.0	5973100	ŏ	5973100	312313600
-44	*=**									
TOT LIF	92500 ETIME A	425500000 VERAGE INCREAS	20262000 E (DECREASE)	473500 IN UNIT OPERATI	1928500 Ing cost		312313600	0	312313600	
		DOLLARS	PER TON OF CO	DAL BURNED			15.41	0.0	15.41	
		MILLS P	ER KILOWATT-H	OUR			6.75	0.0	6.75	
		CENTS P	ER MILLION BT	J HEAT INPUT			73.40	0.0	73.40	
		DOLLARS	PER TON OF SI	JLFUR REMOVED			659.59	0.0	659.59	
PROCES	S COST	DISCOUNTED AT	11.6% TO INI	TIAL YEAR, DOLL	.ARS		127562500	0	127562500	
LEV	ELIZED 1	INCREASE IDECR	EASE) IN UNIT	OPERATING COST	EQUIVALENT TO	DISCOUNTED PROC	ESS COST OVE	R LIFE OF	POWER UNIT	
			PER TON OF CO				13.89	0.0	13.89	
			ER KILOWATT-HO				6.09	0.0	6.09	
			ER MILLION BTU				66.16	0.0	66.16	
		DOLLARS	PER TON OF SU	ILFUR REMOVED			594.97	0.0	594.97	

TABLE A-43. GENERIC DOUBLE-ALKALI PROCESS SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(500-MW new coal-fired power unit, 2.0% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts	929,000 524,000	4.2
and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack) SO ₂ absorption (four tray towers including presaturators and	4,248,000	19.2
entrainment separators, recirculation tanks, agitators, and pumps)	0 204 000	/1 4
Stack gas reheat (four indirect steam reheaters) Reaction (tanks, agitators, and pumps) Solids separation (thickener, drum filters, tanks, agitators,	9,206,000 1,222,000 224,000	41.6 5.5 1.0
pumps, and conveyor) Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond water return	1,476,000	6.7
pumps)	826,000	3.7
Subtotal	18,655,000	84.3
Services, utilities, and miscellaneous	1,119,000	5.1
Total process areas excluding pond construction	19,774,000	89.4
Pond construction	2,339,000	10.6
Total direct investment	22,113,000	100.0
Indirect Investment		
Engineering design and supervision	1,378,000	6.2
Architect and engineering contractor	324,000	1.5
Construction expense	3,239,000	14.6
Contractor fees	1,010,000	4.6
Total indirect investment	5,951,000	26.9
Contingency	5,613,000	25.4
Total fixed investment	33,677,000	152.3
Other Capital Charges		
Allowance for startup and modifications	3,134,000	14.2
Interest during construction	4,041,000	18.2
Total depreciable investment	40,852,000	184.7
Land	464,000	2.1
Working capital	794,000	3.6
Total capital investment	42,110,000	190.4

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979. Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.
Disposal pond located 1 mi from power plant.
Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP. Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-44. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW new coal-fired power unit, 2.0% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantity	Unit cost,	an	tal nual st, \$	% of averag annual reven requirement
Direct Costs					
Raw materials	22.242	10.001			
Lime	29,260 tons	42.00/to	-,-	28,900	10.84
Soda ash	2,790 tons	90.00/to	n2	51,100	2.21
Total raw materials cost			1,4	80,000	13.05
Conversion costs					
Operating labor and supervision	31,070 man-h	ı r 12.50/ma	in-hr 3	88,400	3.43
Utilities			•		
Steam	489,800 MBtu	2.00/MI	Stu 9	79,600	8,64
Process water	226,000 kgal	0.12/kg	al	27,100	0.24
Electricity	26,130,000 kWh	0.029/kV	ль 7	57,800	6.68
Maintenance				•	*****
Labor and material			8	61,100	7.60
Analyses	4,125,man-h	r 17.00/ma		70,100	0.62
Total conversion costs			3,0	84,100	27.21
Total direct costs			4,5	64,100	40.26
Indirect Costs					
Capital charges Depreciation, interim replacements insurance at 6.0% of total deprec					
investment			2,4	51,100	21.63
Average cost of capital and taxes of total capital investment	at 8.6%		3,6	521,500	31.95
Overheads					
Plant, 50% of conversion costs les	s utilities		•	559,800	5.82
Administrative, 10% of operating 1	abor			38,800	0.34
Total indirect costs			6,7	771,200	59.74
Total average annual revenue re	quirements		11,3	335,300	100.00
	• • • • • • • • • • • • • • • • • • • •	ton coal	\$/MBtu heat input	\$/short S remo	
Paulualant water		7 56			
Equivalent unit revenue requirements	3.24	7.56	0.36	699.7	11

a. Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh.

Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded.

S removed, 16,200 short tons/yr; solids disposal 66,070 tons/yr Ca solids including only hydrate water.

Total direct investment, \$22,113,000; total depreciable investment, \$40,852,000; and total capital investment, \$42,110,000.

GENERIC DOUBLE ALKALI PROCESS 500 MW NEW COAL-FIRED POWER UNIT 2.0% S IN COAL, REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: \$	42110000				
				SULFUR	BY-PRODUCT		TOTAL OP. COST			
				REMOVED	RATE.		INCLUDING		NET ANNUAL	CUMULATIVE
	ANNUAL	POWER UNIT	POWER UNIT	BY	EQUIVALENT	NET REVENUE.	REGULATED	TOTAL	INCREASE	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	ROI FOR	NET	(DECREASE)	(DECREASE)
	TION.		CONSUMPTION,	CONTROL	804		POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	DRY	DRY	COMPANY.	REVENUE.	POWER.	POWER.
START	KW	/YEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	S/YEAR	\$	5
1	7000	31500000	1500000	16200	66100	0.0	14956600	0	14956600	14956600
2	7000	31500000	1500000	16200	66100	0.0	14722400	0	14722400	29679000
3	7000	31500000	1500000	16200	66100	0.0	14488200	0	14488200	44167200
4	7000	31500000	1500000	16200	66100	0.0	14254000	0	14254000	58421200
5	7000	31540000	1500000	16200	66100		140 <u>19800</u>		14019800	72441000
6	7000	31500000	1500000	16200	66100	0.0	13785600	0	13785600	86226600
7	7000	31500000	1500000	16200	66100	0.0	13551300	0	13551300	99777900
8	7000	31500000	1500000	16200	66100	0.0	13317100	Q	13317100	113095000
9	7000	31500000	1500000	16200	66100	0.0	13082900	0	13082900	126177900
-10	7000	31500000	1500000	16200	66100		12648700	<u>-</u>	12848700_	139026600
11	5000	22500000	1071400	11600	47200	0.0	11285300	0	11285300	150311900
12	5000	22500000	1071400	11600	47200	0.0	11051100	0	11051100	161363000
13	5000	22500000	1071400	11600	47200	0.0	10816900	0	10816900	172179900
14	5000	22500000	1071400	11600	47200	0.0	10582700	v	10582700	182762600 193111000
-15	5000	22500000	<u>1071400</u>	<u>11600</u>	<u>47200</u> 33000	<u>Q.Q.</u>	<u>10348400</u> 9085000		<u>10348400</u> _ 9085000	202196000
16 17	3500 3500	15750000 15750000	750000	8100	33000	0.0 0.0	8850800	0	8850800	211046800
18	3500	15750000	750000	8100	33000	0.0	8616600	ň	8616600	219663400
19	3500	15750000	750000	8100	33000	0.0	8382400	ň	8382400	228045800
-60	3500	15750000	750000	8100	33000	9.0	8148200	ă	8148200	234194000
21	1500	6750000	321400	3500	14200	0.0	6455100		6455100	242649100
55	1500	6750000	321400	3500	14200	0.0	6220900	ŏ	6220900	248870000
23	1500	6750000	321400	3500	14200	0.0	5986600	ŏ	5986600	254856600
24	1500	6750000	321400	3500	14200	0.0	5752400	ă	5752400	260609000
_25	_1500	6750000	321400	3500	14200	0.0	5518200	Ō	5518200	266127200
56	1500	6750000	321400	3500	14200	0.0	5284000		5284000	271411200
27	1500	6750000	321400	3500	14200	0.0	5049800	Ó	5049800	276461000
28	1500	6750000	321400	3500	14200	0.0	4815600	0	4815600	281276600
29	1500	6750000	321400	3500	14200	0.0	4581400	0	4581400	285858000
_30	_1500	6750000	321400	3500	14200		4347200	Q	4347200	<u> 29020520</u> 0
	27500	573750000	27321000	295500	1204000		290205200	0	290205200	
LII	CITME W		SE (UECKEASE) S PER TON OF C	IN UNIT OPERAT	THO COSI		10.62	0.0	10.62	
			PER KILOWATT-H				4.55	0.0	4.55	
			PER MILLION BT				50.5B	0.0	50.58	
			S PER TON OF S				982.08	0.0	982.08	
ppnrs	S COST			TIAL YEAR, DOL	LARS		103925200	٠.٠٥	103925200	
						DISCOUNTED PROC		-	POWER UNIT	
(21			S PER TON OF C				9.76	0.0	9.76	
			PER KILOWATT-H				4.18	0.0	4.18	
			PER MILLION BT				46.47	0.0	46.47	
			PER TON OF S				902.91	0.0	902.91	
				= = ==						

TABLE A-46. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	1,710,000 833,000	6.4 3.1
dampers from absorber to reheater and stack) SO ₂ absorption (four tray towers including presaturator and entrainment separators, recirculation tanks, agitators, and	4,248,000	15.9
pumps)	9,206,000	34.4
Stack gas reheat (four indirect steam reheaters)	1,282,000	4.8
Reaction (tanks, agitators, and pumps)	357,000	1.3
Solids separation (thickener, drum filters, tanks, agitators,	337,000	1.5
	2 252 000	0.0
pumps, and conveyor) Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond water return	2,352,000	8.8
pumps)	1,247,000	4.7
Subtotal	21,235,000	79.4
Services, utilities, and miscellaneous	1,274,000	4.8
Total process areas excluding pond construction	22,509,000	84.2
Pond construction	4,241,000	15.8
Total direct investment	26,750,000	100.0
Indirect Investment		
Engineering design and supervision	1,444,000	5.4
Architect and engineering contractor	331,000	1.2
Construction expense	3,746,000	14.0
Contractor fees		
Contractor rees	1,167,000	4.4
Total indirect investment	6,688,000	25.0
Contingency	6,688,000	25.0
Total fixed investment	40,126,000	150.0
Other Capital Charges		
Allowance for startup and modifications Interest during construction	3,589,000 4,815,000	13.4 18.0
Total depreciable investment	48,530,000	181.4
Tarit		
Land	837,000	3.1
Working capital	1,184,000	4.4
Total capital investment	50,551,000	188.9

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-47. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb $SO_2/MBtu$ heat input allowable emission; onsite solids disposal)

	Annual quantity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs				
Raw materials				
Lime	63,600 to	ons 42.00/ton	2,671,200	18.20
Soda ash	6,060 to	ons 90.00/ton	545,400	3.72
Total raw materials cost			3,216,600	21.92
Conversion costs				
Operating labor and supervision Utilities	34,500 ma	an-hr 12.50/man	-hr 431,300	2.94
Steam	489,800 M	Btu 2.00/MBt	u 979,600	6.67
Process water	241,500 kg		1 29,000	0.20
Electricity Maintenance	29,100,000 kV	√h 0.029/kWh	843,900	5.75
Labor and material			1,027,600	7.00
Analyses	4,560 ma	an-hr 17.00/man	-hr 77,500	0.53
Total conversion costs			3,388,900	23.09
Total direct costs			6,605,500	45.01
Indirect Costs				
Capital charges Depreciation, interim replacement insurance at 6.0% of total dep	•			
investment			2,911,800	19.84
Average cost of capital and tax of total capital investment Overheads	es at 6.0%		4,347,400	29.63
Plant, 50% of conversion costs	lece utilities		768,200	5.23
Administrative, 10% of operating			43,100	0.29
Total indirect costs			8,070,500	54.99
Total average annual revenue	requirements		14,676,000	100.00
	Mills/	\$/ton coal kWh burned	.,	/short ton 5 removed
	nts 4.1	9 9.78	0.47	

a. Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh.

Stack gas reheat to 1750F.

S removed, 35,000 short tons/yr; solids disposal 142,750 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$26,750,000; total depreciable investment, \$48,530,000; and total capital investment, \$50,551,000.

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				FIXED 1	INVESTMENT: \$	50551000				
,							TOTAL			
				SULFUR	BY-PRODUCT		OP. COST			
				REMOVED	RATE.		INCLUDING		NET ANNUAL	CUMULATIVE
	ANNUAL	POWER UNIT	POWER UNIT	BY	EQUIVALENT	NET REVENUE.	REGULATED	TOTAL	INCREASE	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	ROI FOR	NET	(DECREASE)	(DECREASE)
	TION.	REQUIREMENT.		CONTROL			POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	DRY	DRY	COMPANY,	REVENUE,	POWER.	POWER,
START	KW	/YEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	S/YEAR	s	5
1	7000	31500000	1500000	35000	142700	0.0	19023600	0	19023600	19023600
5	7000	31500000	1500000	35000	142700	0.0	18745300	0	18745300	37768900
3	7000	31500000	1500000	35000	142700	0.0	18467100	0	18467100	56236000
4	7000	31500000	1500000	35000	142700	0.0	18188800	0	18188800	74424800
5	7999	31500000	1500000	35000	142700		<u> </u>		17910600_	92335400
6	7000	31500000	1500000	35000	142700	0.0	17632400	0	17632400	109967800
7	7000	31500000	1500000	35000	142700	0.0	17354100	0	17354100	127321900
8	7000	31500000	1500000	35000	142700	0.0	17075900	0	1707590 0	144397800
9	7000	31500000	1500000	35000	142700	0.0	16797600	0	16797600	161195400
10	7000	31500000	1500000	<u> </u>	142700	<u>Qal</u>	16519400	<u>-</u> -	16519400	177714800
11	5000	22500000	1071400	25000	102000	0.0	14326600	0	14326600	192041400
12	5000	22500000	1071400	25000	102000	0.0	14048400	0	14048400	206089800
13	5000	22500000	1071400	25000	102000	0.0	13770100	0	13770100	219859900
14	5000	22500000	1071400	25000	102000	0.0	13491900	0	13491900	233351800
-15	5000	22500000	1071400	25000	105000	Q_Q	13213700	<u>_</u>	13213700_	246565500
16	3500	15750000	750000	17500	71400	0.0	11461300	0	11461300	258026800
17	3500	15750000	750000	17500	71400	0.0	11183100	0	11183100	269209900
18	3500	15750000	750000	17500	71400	0.0	10904800	0	10904800	280114700
19	3500	15750000	750000	17500	71400	0.0	10626600	0	10626600	290741300
-50	3500	15750000	750000	17500	<u>7140</u> 0	<u></u>	10348300	<u>Q</u> _	10348300_	301083600
21	1500	6750000	321400	7500	30600	0.0	8003300	0	8003300	309092900
22	1500	6750000	321400	7500	30600	0.0	7725000	0	7725000	316817900
23	1500	6750000	321400	7500	30600	0.0	7446800	0	7446800	324264700
24	1500	6750000	321400	7500	30600	0.0	7168600	0	7168600	331433300
25	1500	6750000	321400	7 <u>500</u>	30600	lag	6020300		6890300	338323600
26	1500	6750000	321400	7500	30600	0.0	6612100	0	6612100	344935700
27	1500	6750000	321400	7500	30600	0.0	6333800	0	6333800	351269500
28	1500	6750000	321400	7500	30600	0.0	6055600	0	6055600	357325100
29	1500	6750000	321400	7500	30600	0.0	5777300	0	5777300	363102400
-30	1500	6750000	321400	7500	30600		5429100	Q_	5499100_	368601500
TOT 1		573750000 VERAGE INCREAS	27321000 F (DECREASE)	637500 In unit operati	2600000 NG COST		368601500	0	368601500	
			PER TON OF C				13.49	0.0	13.49	
			ER KILOWATT-H				5.78	0.0	5.78	
			ER MILLION BT				64.24	0.0	64.24	
			PER TON OF SE				578.20	0.0	578.20	
PPACES	S COST I			TIAL YEAR, DOLL	ADC		132472900	0.0	132472900	
IFU	5 0031 E	NCBEASE (DECD	TAGES TO INIT	ODERATING COST	FALITUAL ENT TA	DISCOUNTED PROC		•	POWER UNIT	
LLV			PER TON OF CO		PROTABLEM! IA	DISCOUNIED PROC	12.44	0.0	12.44	
			ER KILOWATT-HO				5.33	0.0	5.33	
			ER MILLION BTU				59.23	0.0	59 . 23	
							533.09		533.09	
		DULLARS	PER TON OF SU	FLOW MEMORED			333607	0.0	233.47	

TABLE A-49. GENERIC DOUBLE-ALKALI PROCESS SUMMARY OF ESTIMATED CAPITAL INVESTMENT a

(500-MW new coal-fired power unit, 5.0% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direc investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	2,399,000 1,077,000	7.8 3.5
dampers from absorber to reheater and stack) SO ₂ absorption (four tray towers including presaturators and entrainment separators, recirculation tanks, agitators, and	4,248,000	13.9
pumps)	9,206,000	30.1
Stack gas reheat (four indirect steam reheaters)	1,283,000	4.2
Reaction (tanks, agitators, and pumps)	462,000	1.5
Solids separation (thickener, drum filters, tanks, agitators,	402,000	1.3
	2 2/5 202	10.0
pumps, and conveyor) Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond water return	3,045,000	10.0
pumps)	1,567,000	5.1
Subtotal	23,287,000	76.1
Services, utilities, and miscellaneous	1,397,000	4.6
Total process areas excluding pond construction	24,684,000	80.7
Pond construction	5,905,000	19.3
Total direct investment	30,589,000	100.0
Indirect Investment		
Engineering design and supervision	1,494,000	4.9
Architect and engineering contractor	336,000	1.1
Construction expense	4,146,000	13.6
Contractor fees	1,292,000	4.2
Total indirect investment	7,268,000	23.8
Contingency	7,571,000	24.7
Total fixed investment	45,428,000	148.5
Other Capital Charges		
A ALEX	3,952,000	10.0
Allowance for startup and modifications		12.9
Interest during construction	5,451,000	<u>17.9</u>
Total depreciable investment	54,831,000	179.3
Land	1,184,000	3.9
Working capital	1,564,000	_5.1
Total capital investment	57,579,000	188.3

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared. Disposal pond located l mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.
Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-50. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS $^{\mathbf{a}}$

(500-MW new coal-fired power unit, 5.0% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annua quanti	_	Unit cost,	\$	Total annual cost, \$	% of average annual revenu requirements
Direct Costs						
Raw materials						
Lime	97,820	tons	42.00/t		4,108,400	23.16
Soda ash	9,320	tons	90.00/t	on	838,800	_4.73
Total raw materials cost					4,947,200	27.89
Conversion costs						
Operating labor and supervision Utilities	37,150	man-hr	12.50/n	an-hr	464,400	2.62
Steam	489,800		2.00/N		979,600	5.52
Process water	257,000	kgal	0.12/1	cgal	30,800	0.17
Electricity	31,960,000	kWh	0.029/	cWh	926,800	5.22
Maintenance						
Labor and material					1,164,500	6.57
Analyses	4,940	man-hr	17.00/m	man-hr	84,000	0.47
Total conversion costs					3,650,100	20.57
Total direct costs					8,597,300	48.46
Indirect Costs						
Capital charges						
Depreciation, interim replacements as						
insurance at 6.0% of total deprecial	ole					
investment					3,289,900	18.54
Average cost of capital and taxes at	8.6%					
of total capital investment					4,951,800	27.91
Overheads					054	
Plant, 50% of conversion costs less of Administrative, 10% of operating laborations					856,500 46,400	4.83 _0.26
Total indirect ocsts					9,144,600	51.54
Total average annual revenue requ	irements				17,741,900	100.00
		64.	1	ć (Mp. 1	. 0/1	
	Mills/kWh	.,		\$/MBtu hea input	t \$/short S remov	

a. Basis

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,000 tons/yr, 9,000 Btu/kWh.

Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded.

Midwest plant location, 1980 revenue requirements.

S removed, 54,180 short tons/yr; solids disposal 221,000 tons/yr Ca solids including only hydrate water.

Total direct investment, \$30,589,000; total depreciable investment, \$54,831,000; and total capital investment, \$57,579,000.

TABLE A-51

GENERIC DOUBLE ALKALI PROCESS 500 MW NEW COAL-FIRED POWER UNIT 5.0% S IN COAL. REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: \$	57579000				
							TOTAL			
				SULFUR	RY-PRODUCT		OP. COST		NET ANNUIAL	CHAIN ATTME
VEADO	ANNUAL	POWER UNIT	POWER UNIT	REMOVED BY	RATE; Equivalent	NET REVENUE.	INCLUDING REGULATED	TOTAL	NET ANNUAL Increase	CUMULATIVE NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	ROI FOR	NET	(DECREASE)	(DECREASE)
	TION		CONSUMPTION.	CONTROL	TONSTIEAR	37 TON	POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	DRY	DRY	COMPANY.	REVENUE,	POWER.	POWER.
START	KW	/YEAR	YEAR	TONS/YEAR	SOLIOS	SOLIDS	S/YEAR	S/YEAR	\$	\$
3,12.1	.,,,,									
1	7000	31500000	1500000	54200	221000	0.0	22693200	0	22693200	22693200
2	7000	31500000	1500000	54200	221000	0.0	22378800	0	22378800	45072000
3	7000	31500000	1500000	54200	221000	0.0	22064500	0	22064500	67136500
4	7000	31500000	1500000	54200	221000	0.0	21750100	0	21750100	88886600
5	7000	31500000	1500000	54200	221000	QaQ	21435700	<u>Q</u> -	21435700_	110355300
6	7000	31500000	1500000	54200	221000	0.0	21121400	0	21121400	131443700
7	7000	31500000	1500000	54200	221000	0.0	20807000	0	20807000	152250700
8 9	7000	31500000	1500000	54200	221000	0.0	20492600	0	20492600	172743300
-	7000	31500000	1500000	54200	221000	0.0	20178300	U	20178300	192921600
-10	- <u>-7000</u>	31500000 22500000	1500000	<u>54200</u>	221000	<u>Q</u> <u>e</u> Q	<u>19863900</u> 17064300	<u>P</u>	<u>19863900</u> _ 17064300	<u>21278550</u> 0 229849800
12	5000	22500000	1071400 1071400	38700	157900	0.0 0.0	16750000	0	16750000	246599800
13	5000	22500000	1071400	38700	157900	0.0	16435600	0	16435600	263035400
14	5000	22500000	1071400	38700	157900	0.0	16121300	0	16121300	279156700
_15	_5000_	22500000	1071400	38700	157900	0.0	15806900	ň	15806900	294963600
16	3500	15750000	750000	27100	110500	0.0	13585700		13585700	308549300
17	3500	15750000	750000	27100	110500	0.0	13271400	ŏ	13271400	321820700
18	3500	15750000	750000	27100	110500	0.0	12957000	ŏ	12957000	334777700
19	3500	15750000	750000	27100	110500	0.0	12642600	Ö	12642600	347420300
-20	3500	15750000	750000	27100	110500	0.0	12329300	Ō	12328300	359748600
21	1500	6750000	321400	11600	47400	0.0	9358100	0	9358100	369106700
22	1500	6750000	321400	11600	47400	0.0	9043700	0	9043700	378150400
23	1500	6750000	321400	11600	47400	0.0	8729400	0	8729400	386879800
24	1500	6750000	321400	11600	47400	0.0	8415000	0	8415000	395294800
_25	_1500	6750000	321400	11600	47400		8100600		8100600	403395400
26	1500	6750000	321400	11600	47400	0.0	7786300	D	7786300	411181700
27	1500	6750000	321400	11600	47400	0.0	7471900	0	7471900	418653600
28	1500	6750000	321400	11600	47400	0.0	7157500	0	7157500	425811100
29	1500	6750000	321400	11600	47400	0.0	6843200	0	6843200	432654300
30	1500	6750000	321400	11600	47400	lel	6528800		6528800	439183100
TOT 1		573750000	27321000	987000	4026000		439183100	0	439183100	
LIF	ETIME A			IN UNIT OPERAT	ING COST				16.07	
			PER TON OF CO				16.07	0.0	6.89	
			ER KILOWATT-H				6.89	0.0	76.55	
			PER MILLION BTO				76.55	0.0	444.97	
DDACES	C COST		PER TON OF SE	JLFOR REMOVED TIAL YEAR, NOLI	436		444.97 158278400	0.0	158278400	
160	5 CU31	DISCOUNIED AT	EACE I THILLE	TARE TEARS TIVE!	T EQUIVALENT TO	DISCOUNTED BOAC	FEE CUST UAR			
(2)	FFIEL	1707EM3E 10EU4	PER TON OF CO	TAL BUDNED CUS	" "ANTANTEM! IO	PISCOUNIED PROC	14.86	0.0	14.86	
			FR KILOWATT-HO				6.37	0.0	6.37	
			ER MILLION ATI				70.77	0.0	70.77	
			PER TON OF SU				411.33	0.0	411.33	
		0022443		22. 3						

GENERIC DOUBLE-ALKALI PROCESS TABLE A-52.

SUMMARY OF ESTIMATED CAPITAL INVESTMENT^a

(1000-MW existing coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	3,269,000 1,390,000	7.0 3.0
dampers from absorber to reheater and stack) SO2 absorption (four tray towers encluding presaturators and entrainment separators, recirculation tanks, agitators, and	8,447,000	18.0
pumps)	17,207,000	36.7
Stack gas reheat (four indirect steam reheaters)	2,026,000	4.3
Reaction (tanks, agitators, and pumps)	603,000	1.3
Solids separation (thickener, drum filters, tanks, agitators,	000,000	1.5
pumps, and conveyor)	2 05/ 000	8.4
pumps, and conveyor; Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond water return	3,954,000	0.4
pumps)	2,032,000	<u>4.3</u>
Subtotal	38,928,000	83.0
Services, utilities, and miscellaneous	2,336,000	_5.0
Total process areas excluding pond construction	41,264,000	88.0
Pond construction	5,636,000	12.0
Total direct investment	46,900,000	100.0
Indirect Investment		
Engineering design and supervision	1,486,000	3.2
Architect and engineering contractor	335,000	0.7
Construction expense	6,027,000	12.8
Contractor fees	1,788,000	3.8
Total indirect investment	9,636,000	20.5
Contingency	11,307,000	24.1
Total fixed investment	67,843,000	144.6
Other Capital Charges		
Allowance for startup and modifications	6,221,000	13.3
Interest during construction	8,141,000	17.4
·		
Total depreciable investment	82,205,000	175.3
Land	1,142,000	2.4
Working capital	2,140,000	4.6
Total capital investment	85,487,000	182.3

Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°P by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-53. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS

(1000-MW existing coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantii	_	Uni cost	-	Total annual a cost, \$	% of average nnual revenu- requirements
Direct Costs .						
Raw materials						
Lime	127,200	tons	42.00/	ton	5,342,400	20.75
Soda ash	12,120	tons	90.00/	ton	1,090,800	4.24
Total raw materials cost					6,433,200	24.98
Conversion costs						
Operating labor and supervision Utilities	48,150	man-hr	12.50/	man-hr	601,900	2.34
Steam /	979,700	MBtu	2.00/	MBtu	1,959,400	7.61
Process water	483,000	kgal	0.12/	'kgal	58,000	0.23
Electricity	58,100,000	kŴh	0.028/	kWh	1,626,800	6.31
Maintenance						
Labor and material					1,277,900	4.96
Analyses	7,080 1	man-hr	17.00/	man-hr	120,400	0.47
Total conversion costs					5,644,400	21.92
Total direct costs					12,077,600	46.90
Indirect Costs						
Capital charges Depreciation, interim replacements, insurance at 6.4% of total deprecial investment Average cost of capital and taxes at	ble				5,261,100	20.43
of total capital investment Overheads	0.04				7,351,900	28.56
Plant, 50% of conversion costs less	utilities				1,000,100	3.88
Administrative, 10% of operating lab					60,200	0.23
Total indirect costs					13,673,300	53.10
Total average annual revenue requ	irements				25,750, 9 00	100.00
	Mills/kWh	\$/ton buri		\$/MBtu hea	s removed	
Equivalent unit revenue requirements	3.68	8.	58	0.41	367.87	

a. Basis

Midwest plant location, 1980 revenue requirements. Remaining life of power plant, 25 yr.

Power unit on-stream time, 7,000 hr/yr.
Coal burned, 2,999,850 tons/yr, 9,000 Btu/kWh.
Stack gas reheat to 175°F.

S removed, 70,000 short tons/yr; solids disposal 285,500 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$46,900,000; total depreciable investment, \$82,205,000; and total capital investment, \$85,487,000.

TABLE A-54

GENERIC DOUBLE ALKALI PROCESS 1000 MW EXISTING COAL-FIRED POWER UNIT 3.5% S IN COAL+ REGULATED CO. ECONOMICS

		٠		FIXED	INVESTMENT: \$	85487000	T 0. T 4.			
AFTER	ANNUAL OPERA-	POWER UNIT	POWER UNIT	SULFUR REMOVED BY POLLUTION	BY-PRODUCT RATE, EQUIVALENT TONS/YEAR	NET REVENUE, \$/TON	TOTAL OP. COST INCLUDING REGULATED ROI FOR	TOTAL NET	NET ANNUAL INCREASE (DECREASE)	CUMULATIVE NET INCREASE (DECREASE)
UNIT		MILLION BTU	CONSUMPTION. TONS COAL	CONTROL Process.	DRY	DRY	POWER COMPANY:	SALES REVENUE,	IN COST OF POWER.	IN COST OF POWER.
START	KM	/YEAR	/YE AR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	S/YEAR	\$	S
1 2 3 4										
6	7000	63000000	3000000	70000	285500	0.0	33104800	-	33104800	33104800
7	7000	63000000	3000000	70000	285500	0.0	32539200	Ŏ	32539200	65644000
8	7000	63000000	3000000	70000	285500	0.0	31973600	Ō	31973600	97617600
9	7000	63000000	3000000	70000	285500	0.0	31408100	Ō	31408100	129025700
-10	7000	63000000	3000000	70000	285500	0.0	30842500		30842500	159868200
11	5000	45000000	2142900	50000	203900	0.0	26778600	0	26778600	186646800
12	5000	45000000	2142900	50000	203900	0.0	26213000	0	26213000	212859800
13	5000	45000000	2142900	50000	203900	0.0	25647500	0	25647500	238507300
14	5000	45000000	2142900	50000	203900	0.0	25081900	0	25081900	263589200
15	5400	45000000	2142900	<u> </u>	002502	<u></u>	24516300	<u>-</u>	24516300	288105500
16	3500	31500000	1500000	35000	142700	0.0	21279700	0	21279700	309385200
17	3500	31500000	1500000	35000	142700	0.0	20714100	0	20714100	330099300
18	3500	31500000	1500000	35000	142700	0.0	20148500	0	20148500	350247800
19	3500	31500000	1500000	35000	142700	0.0	19582900	0	19582900	369830700
-20	3500	31500000	1500000	35000	142700	<u>QaQ</u>	19017400	<u>k</u> -	19017400-	<u>38484810</u> 0 403612300
21	1500	13500000	642900	15000 15000	61200	0.0 0.0	14764200 14198600	0	14764200 14198600	417810900
23 22	1500 1500	13500000 13500000	642900 642900	15000	61200 61200	0.0	13633100	Ö	13633100	431444000
24	1500	13500000	642900	15000	61500	0.0	13067500	0	13057500	444511500
-25	1500	1350000	642900	15000	61200		12501900	ň	12501900	457013400
56	1500	13500000	642900	15000	61200	0.0	11936400		11936400	468949800
27	1500	13500000	642900	15000	61200	0.0	11370800	ŏ	11370800	480320600
28	1500	13500000	642900	15000	61200	0.0	10805200	ŏ	10805200	491125800
29	1500	13500000	642900	15000	61200	0.0	10239600	ŏ	10239600	501365400
30	1500	13500000	642900	15000	61200		9674100	Q	9674100	511039500
TOT	92500	832500000	39643500	925000	3772500		511039500	0	511039500	
LI	CLIME A		SE (DECREASE) S PER TON OF C	IN UNIT OPERAT	1140 C021		12.89	0.0	12.89	
			PER KILOWATT-H				5.52	0.0	5.52	
			PER MILLION BT				61.39	0.0	61.39	
			S PER TON OF S				552.48	0.0	552.48	
PROCES	T200 22			TIAL YEAR+ DOL	1 405		209774100	0	209774100	
I FI	VEL TZED	INCREASE (DEC	REASE) IN LIMIT	OPERATING COS	T EQUIVALENT TO	DISCOUNTED PRO				
			S PER TON OF C		. 4401186511 10		11.68	0.0	11.68	
			PER KILOWATT-H				5.00	0.0	5.00	
			PER MILLION BT				55.61	0.0	55.61	
		DOLLARS	PER TON OF S	ULFUR REMOVED			500.53	0.0	500.53	

TABLE A-55. GENERIC DOUBLE-ALKALI PROCESS

SUITIARY OF ESTIMATED CAPITAL INVESTMENT

(1000-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direc investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	2,873,000 1,234,000	6.7 2.8
dampers from absorber to reheater and stack) SO2-absorption (four tray towers including presaturators and entrainment separators, recirculation tanks, agitators, and	6,651,000	15.5
pumps)	15,497,000	36.2
Stack gas reheat (four indirect steam reheaters)	1,875,000	4.4
Reaction (tanks, agitators, and pumps)	530,000	1.2
Solids separation (thickener, drum filters, tanks, agitators,		
pumps, and conveyor)	3,493,000	8.1
Solids disposal (onsite disposal facilities including reslurry	,,	
tank, agitator, slurry disposal pumps, and pond water return		
pumps)	1,769,000	4.1
F	1,703,000	
Subtotal	33,922,000	79.0
• • • • • • • • • • • • • • • • • • • •	33,922,000	77.0
Services, utilities, and miscellaneous	2 035 000	4.7
octivities, and magnetical control of	2,035,000	-4.7
Total process areas excluding pond construction	25 057 000	83.7
Total process areas excluding pond consciuction	35,957,000	03.7
Pond construction	7 005 000	1/ 1
rond construction	<u>7,025,000</u>	<u>16.3</u>
Total direct investment	42,982,000	100.0
Indirect Investment		
Tietasantas deaten and ausamutaten		2.5
Engineering design and supervision	1,525,000	3.5
Architect and engineering contractor	339,000	0.8
Construction expense	5,545,000	12.9
Contractor fees	_1,673,000	3.9
m - 1 1 11 1		
Total indirect investment	9,082,000	21.1
Contingency	10,413,000	24.3
Total fixed investment	62,477,000	145.4
Other Capital Charges		
Company of the second of the s		
Allowance for startup and modification	5,545,000	12.9
Interest during construction	7,497,000	17.4
Total depreciable investment	75,519,000	175.7
Land	1,412,000	3.3
		4.8
Working capital	2,085,000	
Total capital investment	79,016,000	183.8

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-56. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(1000-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Annual quantity	Uni cost	lt .		% of average nnual revenu requirements
Direct Costs					
Raw materials					
Lime	123,000 to			,166,000	21.39
Soda ash	11,720 to	ons 90.00)/ton <u>1</u>	,054,800	4.37
Total raw materials cost			6	,220,800	25.76
Conversion costs					
Operating labor and supervision Utilities	48,150 ma	in-hr 12.50)/man-hr	601,900	2.49
Steam	947,000 ME	3tu 2.00)/MBtu 1	,894,000	7.85
Process water	467,000 kg		2/kgal	56,000	0.23
Electricity	56,160,000 kk	Jh 0.028	3/kWh 1	,572,500	6.51
Maintenance				•	
Labor and material			1	,289,500	5.34
Analyses	7,080 ma	an-hr 17.00	O/man-hr _	120,400	0.50
Total conversion costs			5	5,534,300	22.92
Total direct costs			. 11	,755,100	48.68
Indirect Costs					
Capital charges					
Depreciation, interim replacement insurance at 6.0% of total depre					
investment	. 0 (%		4	,531,100	18.76
Average cost of capital and taxes of total capital investment	at 8.6%		6	5,795,400	28.14
Overheads					
Plant, 50% of conversion costs le	ss utilities]	1,005,900	4.17
Administrative, 10% of operating	labor			60,200	0.25
Total indirect costs			12	2,392,600	51.32
Total average annual revenue r	equirements		24	4,147,700	100.00
	Mills/kWh	\$/ton coal burned	\$/MBtu heat input	\$/short to S removed	

a. Basis

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 2,900,100 tons/yr, 8,700 Btu/kWh.

Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$42,982,000; total depreciable investment, \$75,519,000; and total capital investment, \$79,016,000.

Midwest plant location, 1980 revenue requirements.

S removed, 67,670 short tons/yr; solids disposal 276,000 tons/yr Ca solids including only hydrate water.

FIXED INVESTMENT: \$ 79016000

DOLLARS PER TON OF SULFUR REMOVED

				FIXED	INAEZIMENI: 2	1.401.000				
							TOTAL			
				SULFUR	BY-PRODUCT		OP. COST			
				REMOVED	RATE.		INCLUDING		NET ANNUAL	CUMULATIVE
	ANNUAL	POWER UNIT	POWER UNIT	BY	EQUIVALENT	NET REVENUE.		TOTAL	INCREASE	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	S/TON	ROI FOR	NET	(DECREASE)	(DECREASE)
POWER	TION.		CONSUMPTION.	CONTROL			POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	ORY	DRY	COMPANY,	REVENUE,	POWER.	POWER,
START	KW	/YEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	S/YEAR	\$	\$
<u>-</u>	7000	60900000	2400000	67700	276000	0.0	30943600	0	30943600	30943600
2	7000	60900000	2900000	67700	276000	0.0	30510600	0	30510600	61454200
3	7000	60900000	2900000	67700	276000	0.0	30077600	0	30077600	91531800
4	7000	60900000	2900000	67700	276000	0.0	29644600	0	29644600	121176400
5	7000	60900000	2900040	67700	276000	0_0	29211600	Q	29211600	150388000
6	7000	60900000	2900000	67700	276000	0.0	28778700	0	28778700	179166700
7	7000	50900000	2900000	67700	276000	0.0	28345700	٥	28345700	207512400
8	7000	60900000	2900000	67700	276000	0.0	27912700	Ó	27912700	235425100
9	7000	60900000	2900000	67700	276000	0.0	27479700	Õ	27479700	262904800
_10	7000	60900000	2900000	67700	276000	0.0	27046800	0	27046800	28 9 951600
11	5000	43500000	2071400	48300	197200	0.0	23208400	0	23208400	313160000
12	5000	43500000	2071400	48300	197200	0.0	22775400	0	22775400	335935400
13	5000	43500000	2071400	48300	197200	0.0	22342400	Ô	22342400	358277800
14	5000	43500000	2071400	48300	197200	0.0	21909500	ō	21909500	380187300
15	5000	43500000	2071400	48300	197200		21476500	ă	21476500	401663800
16	3500	30450000	1450000	33800	138000	0.0	18441500	0	18441500	420105300
17	3500	30450000	1450000	33800	138000	0.0	18008500	ă	18008500	438113800
18	3500	30450000	1450000	33800	138000	0.0	17575600	ŏ	17575600	455689400
19	3500	30450000	1450000	33800	138000	0.0	17142600	ŏ	17142600	472832000
20	3500	30450000	1450000	33800	138000		16709600	ō	16709600	489541600
21	1500	13050000	621400	14500	59100	0.0	12680100		12680100	502221700
55	1500	13050000	621400	14500	59100	0.0	12247200	Ŏ	12247200	514468900
23	1500	13050000	621400	14500	59100	0.0	11814200	ŏ	11814200	526283100
24	1500	13050000	621400	14500	59100	0.0	11381200	ă	11381200	537664300
25	1500	13050000	621400	14500	59100		10948200	ă	10948200	548612500
26	1500	13050000	621400	14500	59100	0.0	10515300		10515300	559127800
27	1500	13050000	621400	14500	59100	0.0	10082300	Ŏ	10082300	569210100
28	1500	13050000	621400	14500	59100	0.0	9649300	5	9649300	578859400
29	1500	13050000	621400	14500	59100	0.0	9216300	ŏ	9216300	588075700
30	1500	13050000	621400	14500	59100		8783400		8783400	596859100
-4x			¥#118E				ATAKIRA		#4 = = 4 = = -	
TOT 1	27500	1109250000	52821000	1232500	5027000		596859100	0	596859100	
			E (DECHEASE)				390037100	•	370037100	
L 41	C11.11C 4		PER TON OF CO		146 6031		11.30	0.0	11.30	
			PER KILOWATT-H				4.68	0.0	4.68	
			PER MILLION BT				53.81	0.0	53.81	
			PER TON OF SI				484.27	0.0	484.27	
DDACES	e cost (11.6% TO INI		I ADC		215525300	V. 0	215525300	
PRUCES	13 LU31 L	INCOEACE ICECO	INI UF GOOLL	DECATING COC	LATO T FOUTUALENT TO	DISCOUNTED PRO				
LEV	CL17ED				I EMOTAMENT TO	OTSCOONIED BEC	10.47	0.0	10.47	
			PER TON OF CO				4.34	0.0	4.34	
			ER KILOWATT-HO						49.85	
		CENTS P	ER MILLION BT	J MEAT INPUT			49.85	0.0	47.83	

448.54

0.0

448.54

TABLE A-53. GENERIC DOUBLE-ALKALI PROCESS

SULMARY OF ESTIMATED FIXED INVESTMENT

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; trucking alternative)

	Investment, \$	% of total direc investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts	1,710,000 833,000	8.1 3.9
and dampers from plenum to absorber, exhaust gas ducts, and dampers from absorber to reheater and stack) SO, absorption (four tray towers including presaturators and entrainment separators, recirculation tanks, agitators, and	4,248,000	20.0
•	0 206 000	
pumps) Stack gas reheat (four indirect steam reheaters)	9,206,000	43.4
	1,282,000	6.1
Reaction (tanks, agitators, and pumps) Solids disposal (thickener, drum filters, tanks, agitators,	357,000	1.7
pumps, and conveyor)	2,352,000	11.1
Subtotal	19,988,000	94.3
Services, utilities, and miscellaneous	1,199,000	5,7
Total direct investment	21,187,000	100.0
Indirect Investment		
Engineering design and supervision	1,175,000	5.5
Architect and engineering contractor	294,000	1.4
Construction expense	3,152,000	14.9
Contractor's fees	<u>977,000</u>	4.6
Total indirect investment	5,598,000	26.4
Contingency	5,357,000	25.3
Total fixed investment	32,142,000	151.7
Other Capital Charges		
Allowance for startup and modifications	3,214.000	15.2
Interest during construction	3,857,000	18.2
Total depreciable investment	39,213,000	185.1
Land	326,000	1.5
Working capital	1,305,000	6.3
Trucking charge (including indirect charges)	491,000	2.3
Total capital investment	41,335,000	195.2

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.
Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared. Disposal area located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-59. GENERIC DOUBLE-ALKALI PROCESS

TOTAL AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS

(500-11W new coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission; trucking alternative)

	Annual quantity	Unit cost, \$	Total annual cost, \$	% of average annual revenu requirements
Direct Costs	4500000	0000, 4	2032, 9	requirements
Raw materials				
Lime	63,600 tons	42.00/to	2,671,200	18.69
Soda ash	6,060 tons	90.00/to	. , ,	3.81
Total raw material cost			3,216,600	22.50
Conversion costs				
Operating labor and supervision	31,000 man-h	r 12.50/mar	n-hr 387,500	2.73
Operating labor disposal equipment Utilities	42,000 man-h			5.00
Steam	489,800 MBtu	2.00/MB	tu 979,600	6.85
Process water	217,600 kgal	0.12/kg		6.85
	7,000,000 kWh	0.029/kW		0.18
Fuel	196,000 gal	0.60/ga		0.82
Maintenance	,			5,48
Labor and material			876,900	6.13
Analyses	5 acres	1600/ac		0.06
Disposal land preparation	4,180 man-h	•	-,	0.50
Total conversion costs			3,963,800	27.73
Total direct costs			7,180,400	50.23
Indirect Costs				
Capital charges	1			
Depreciation, interim replacements, insurance at 6.0% of total deprecia				
investment Average cost of capital and taxes at			2,425,800	16.97
of total capital investment Overheads	. 0.0%		3,554,800	24.87
Plant, 50% of conversion costs less	utilities		653,100	4.57
Administrative, 10% of operating lab			38,800	0.27
Trucking labor			441,000	3.09
Total indirect costs			7,113,500	49.77
Total annual revenue requirements	:		14,293,900	100.00
		\$/ton coal		short ton
	Mills/kWh	burned	input !	S removed_
Equivalent unit revenue requirements	4.08	9.53	0.45	408.40

a. Basis

Remaining life of power plant, 30 yr. Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Bru/kWh. Stack gas reheat to 175°F.

Investment and revenue requirement for removal and disposal of flyash excluded. Total direct investment, \$21,187,000; total depreciable investment, \$39,213,000, and total capital investment, \$41,335,000.

Midwest plant location, 1980 revenue requirements.

S removed, 35,000 short ton/yr; solids disposal 142,750 tons/yr Ca solids including only hydrate water.

				FIXED	INVESTMENT: \$	41335000				
							TOTAL			
				SULFUR Removed	BY-PRODUCT		OP. COST Including		NET ANNUAL	CUMUS ATTUE
VEARS	ANNUAL	POWER UNIT	POWER UNIT	BY	RATE, EQUIVALENT	NET REVENUE.	REGULATED	TOTAL	INCREASE	CUMULATIVE NET INCREASE
	GPERA-	FEAT	FUEL	PELLUTION	TONS/YEAR	\$/TON	ROL FOR	NET	(DECREASE)	(DECREASE)
	TION.		CONSUMPTION,	CONTROL	TONS/ TEAM	77.84	POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	DRY	DRY	COMPANY,	REVENUE,	POWER,	POWER,
START		/YEAR	/YEAR	TONS/YEAR	201102	SOLIDS	\$/YEAR	\$/YEAR	\$	\$
1	7000	315000CC	1500C0C	35000	142700	0.0	17849000	0	17849000	17849000
į	7000	31500000	1500000	35000	142700	0 -0	17623600	Ö	17623600	35472600
3	7000	315000CC	1500C0C	35000	142700	0.0	17398200	ő	17398200	52870800
4	7000	31500000	1500000	35000	142700	0.0	17172900	ŏ	17172900	70043700
5	000	31500000	1500000	35000	142700	0_0	16947500		16947500_	86991200
6	7000	31500000	1500000	35000	142700	0.0	16722100	0	16722100	103713300
7	7000	315000CC	1500000	35000	142700	0.0	16496700	0	16496700	120210000
8	7000	31500000	1500000	35000	142700	0 - 0	16271300	0	16271300	136481300
9	7000	31500000	1500000	35000	142700	0.0	16045933	0	16045900	152527200
_10	2000	31500000	1500£00	35000	142700	0_0	15820500		15820500	168347700
11	5000	22500000	1071400	25000	102000	0 -0	13524100	0	13524100	181871800
12	5000	22500000	1071400	25000	102000	0.0	13298700	0	13298700	195170500
13	5000	22500000	1071400	25000	102000	0-0	13073400	0	13073400	208243900
14	5000	225000CC	107140C	25000	102000	C - O	12848000	0	12848000	221 091 900
15	5000	22500000	1071400	25000	102000		12622600		12622600_	<u>23371650</u> 0
16	3500	157500CC	750000	17500	71400	0.0	10785500	0	10789500	244504000
17	35CD	15750000	750000	17500	71400	0 -0	10564100	0	10564100	255068100
18	3500	157500CC	750000	17500	71400	0.0	10338700	O	10338700	265406800
19	3500	15750000	750000	17500	71400	0.0	10113300	0	10113300	275520100
_20	3500	152500CC	350000	17500	71400	<u></u>	9887900	<u>0</u> _	9887900_	28540.8000
51	1500	6750000	321400	7500	30600	0.0	7372800	0	73 72 800	292780800
22	1500	6750000	32140C	7500	30600	0.0	7147500	0	7147500	299928300
5.3	1500	6750000	321400	7500	30600	0 - 0	6922100	0	6922100	306850400
24 _25	1500	67500CC 6750000	321400	7500 7500	30600	0.0	6696700 6671300	Ü	6696700 6 <u>671300</u> _	31 3 54 7100 32001.8400
26	1500 1500	675COCC	<u>321400</u> 321400	7500	<u>30600</u> 30600	0.0	6245900	0	62459C0	326264300
27	1500	6750000	321400	7500 7500	30600	0.0	6020500	ŏ	6020500	332284800
28	1500	6750000	321400	7500 7500	30600	0.0	5795100	ő	5795100	338079900
29	1500	6750000	321400	7500	30600	0.0	5569700	ő	5569700	34 364 9600
30	1500	675UQQQ	321400	Z500	30600	0_0	5344333	ă_	5344300_	348993900
								_		
	127500	573750000 VERAGE INCREAS	27321000	637500	2600000		348993900	0	348993900	
L 1	. LIINE A		S PEP TON CF C		ותט נטטו		12.77	0.0	12.77	
			PER PILOBATT-H				5.47	0.0	5.47	
		_	PER FILLIAN BT	-			60.83	0.0	60.83	
			PER TON OF SI				547.44	0.0	547.44	
DD 0 C 5	Tana 22	DISCOUNTED AT			LABC		125275900	0.00	125275900	
1 6	VEL 17F0	IACREASE IFECT	1176 U1 6U+1 1 1141 Al 12242	OPERATING COS	T FCHIVALENT TO	D DISCOUNTED PRO	CESS COST OVE			
			PER TUN OF CE		. F4011WFF41 10	, ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	11.76	0.0	11.76	
			FR KILDWATT-HO				5.04	0.0	5.04	
			ER MILLION BTL				56.02	0.0	56.02	
			PER TON CF SI				504.13	0.0	504.13	

TABLE A-61. GENERIC DOUBLE-ALKALI PROCESS SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(500-MW new coal-fired power unit, 3.5% S in coal; 90% SO₂ removal; onsite solids disposal)

	Investment, \$	% of total direc investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders) Feed preparation (feeders, slakers, tanks, agitators, and pumps) Cas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	1,889,000 897,000	6.8 3.2
dampers from absorber to reheater and stack) SO ₂ absorption (four tray towers including presaturators and entrainment separators, recirculation tanks, agitators, and	4,248,000	15.3
pumps)	9,206,000	33.2
Stack gas reheat (four indirect steam reheaters)	1,283,000	4.6
Reaction (tanks, agitators, and pumps) Solids separation (thickener, drum filters, tanks, agitators,	385,000	1.4
pumps, and conveyor) Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond water return	2,536,000	9.1
pumps)	1,333,000	4.8
Subtotal	21,777,000	78.4
Services, utilities, and miscellaneous	1,307,000	4.7
Total process areas excluding pond construction	23,084,000	83.1
Pond construction	4,679,000	16.9
Total direct investment	27,763,000	100.0
Indirect Investment		
Engineering design and supervision	1,458,000	5.3
Architect and engineering contractor	332,000	1.2
Construction expense	3,852,000	13.9
Contractor fees	1,200,000	4.3
Total indirect investment	6,842,000	24.7
Contingency	6,921,000	24.9
Total fixed investment	41,526,000	149.6
Other Capital Charges		
Allowance for startup and modifications	3,685,000	13.3
Interest during construction	4,983,000	17.9
Total depreciable investment	50,194,000	180.8
Land	933 000	3.4
Working capital	932,000 1,278,000	4.6
Total capital investment	52,404,000	188.8

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979. Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.
Disposal pond located 1 mi from power plant.
Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

TABLE A-62. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW new coal-fired power unit, 3.5% S in coal; 90% SO₂ removal; onsite solids disposal)

	Annua quanti	_	Un: cost		Total annual cost, \$	% of average annual revenu requirements
Direct Costs						
Raw materials						
Lime	72,450	tons	42.00	/ton	3,042,900	19.71
Soda ash	6,900	tons	90.00	/ton	621,000	4.02
Total raw materials cost					3,663,900	23.73
Conversion costs						
Operating labor and supervision Utilities	34,500	man-hr	12.50	/man-hr	431,300	2.79
Steam	489,800		2.00)/MBtu	979,600	6.34
Process water	245,300		0.12	!/kgal	29,400	0.19
Electricity	29,161,000	kWh	0.029	/kWh	845,700	5.48
Maintenance Labor and material					1 0/2 700	
Analyses	4,560	man-hr	17.00	/man-hr	1,063,700 77,500	6.90 <u>0.50</u>
Total conversion costs					3,427,200	22.20
Total direct costs					7,091,100	45.93
Indirect Costs						
Capital charges						
Depreciation, interim replacements,						
insurance at 6.0% of total deprecia	able				2 011 (00	
investment Average cost of capital and taxes at	8.6%				3,011,600	19.51
of total capital investment Overheads					4,506,700	29.19
Plant, 50% of conversion costs less	utilities				786,300	5.09
Administrative, 10% of operating lab	oor				43,100	0.28
Total indirect costs					8,347,700	54.07
Total average annual revenue requ	uirements			1	5,438,800	100.00
		\$/ton	coal	\$/MBtu heat	\$/short t	on
	Mills/k	Wh bur	ned	input	S remove	
	4.41		. 29			

a. Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh.

Stack gas reheat to 175°F.

S removed, 40,900 short tons/yr; solids disposal 166,810 tons/yr Ca solids including only hydrate water.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$27,763,000; total depreciable investment, \$50,194,000; and total capital investment, \$52,404,000.

TABLE A-63

GENERIC DOUBLE ALKALI PROCESS 500 MW NEW COAL-FIRED POWER UNIT 3.5% S IN COAL. 90% REMOVAL REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: \$	52404000				
							TOTAL			
				SULFUR	BY-PRODUCT		OP. COST			A T
VEADE	ANNUAL	POWER UNIT	POWER UNIT	REMOVED By	RATE; Equivalent	NET REVENUE,	INCLUDING REGULATED	TOTAL	NET ANNUAL INCREASE	CUMULATIVE NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TON	ROI FOR	NET	(DECREASE)	(DECREASE)
	TION	REQUIREMENT.	CONSUMPTION.	CONTROL	TONS/ TEAR	. 37 1014	POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PROCESS.	DRY	DRY	COMPANY,	REVENUE.	POWER.	POWER.
START	KW	/YEAR	/YEAR	TONS/YEAR	SOLIDS	SOLIDS	\$/YEAR	S/YEAR	\$	\$
								- -		
1	7000	31500000	1500000	39800	166800	0.0	19945500	0	19945500	19945500
2 3	7000 7000	31500000	1500000	39800 39800	166800 166800	0.0 0.0	19657700 19369900	0	19657700 19369900	39603200 58973100
4	7000	31500000 31500000	1500000 1500000	39800	166800	0.0	19082200	0	19082200	78055300
5	7000	31500000	1500000	39800	166800	0.0	18794400	ŏ	18794400	96849700
	7000	31500000	1500000	39800	166800	0.0	18506600		18506600	115356300
7	7000	31500000	1500000	39800	166800	0.0	18218800	Ŏ	18218800	133575100
8	7000	31500000	1500000	39800	166800	0.0	17931100	ō	17931100	151506200
9	7000	31500000	1500000	39800	166800	0.0	17643300	0	17643300	169149500
_10	_7000_	31500000	1500000	39800	166800	0.0	17355500	Q	17355500	186505000
11	5000	22500000	1071400	28400	119200	0.0	15014400	0	15014400	201519400
12	5000	22500000	1071400	28400	119200	0.0	14726600	0	14726600	216246000
13	5000	22500000	1071400	28400	119200	0.0	14438800	0	14438800	230684800
14	5000	22500000	1071400	28400	119200	0.0	14151000	0	14151000	244835800
15	5000	22500000	1071 <u>4</u> 00	20400	119200	lal	13863300	<u>.</u>	13863300_	258699100
16	3500	15750000	750000	19900	83400	0.0	11996300	0	11996300	270695400
17	3500	15750000	750000	19900	83400	0.0	11708500	0	11708500	282403900
18	3500	15750000	750000	19900	83400	0.0	11420700	0	11420700	293824600 304957600
19 24	3500 3500	15750000	750000 750000	19900 19900	83400	0.0	11133000	U	11133000 10845200_	315892800
21 21	3348 1500	15750000	<u>750000</u> 321400	8500	83400 35700	0.0	<u>10845200</u> 8348000	<u>v</u>	8348000	324150800
55	1500	6750000	321400	8500	35700 35700	0.0	8060300	ŏ	8060300	332211100
23	1500	6750000	321400	8500	35700	0.0	7772500	Ŏ	7772500	339983600
24	1500	6750000	321400	8500	35700	0.0	7484700	ŏ	7484700	347468300
25	1500	6750000	321400	8500	35700	0.0	7196900	<u> </u>	7196900	354665200
26	1500	6750000	321400	8500	35700	0.0	6909200	0	6909200	361574400
27	1500	6750000	321400	8500	35700	0.0	6621400	0	6621400	368195800
28	1500	6750000	321400	8500	35700	0.0	6333600	0	6333600	374529400
29	1500	6750000	321400	8500	35700	0.0	6045800	0	6045800	380575200
30	1500	6750000	321400	8500	35700	lal	5758100		5758100	<u> </u>
TOT	127500	573750000	27321000	724500	3038000		386333300	0	386333300	
			SE (DECREASE)				00000000	_		
			PER TON OF C				14.14	0.0	14.14	
			PER KILOWATT-H				6.06	0.0	6.06	
			PER MILLION BT				67.33	0.0	67.33	
			PER TON OF S				533.24	0.0	533.24	
PROCES	SS COST	DISCOUNTED AT	11.6% TO INI	TIAL YEAR+ DOL	LARS		138947500	0	138947500	
LE	/ELIZED				T EQUIVALENT TO	DISCOUNTED PRO	CESS COST OVER	LIFE OF	POWER UNIT	
			PER TON OF C				13.05	0.0	13.05	
			ER KILOWATT-H				5.59	0.0	5.59	
			ER MILLION BT				62.13	0.0	62.13	
		DOLLARS	PER TON OF S	ULFUR REMOVED			491.85	0.0	491.85	

TABLE A-64. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT^a

(500-MW existing oil-fired power unit. 2.5% S in oil; 0.8 lb SO₂/MBtu heat input allowable emission; onsite solids disposal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (conveyors, elevators, bins, and feeders)	995,000	4.7
Feed preparation (feeders, slakers, tanks, agitators, and pumps) Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and	564,000	2.7
dampers from absorber to reheater and stack) SO: absorption (four tray towers including presaturators and	4,398,000	20.9
entrainment separators, recirculation tanks, agitators, and pumps)	8,728,000	41.4
Stack gas reheat (four direct oil reheaters)	726,000	3.4
Reaction (tanks, agitators, and pumps)	243,000	1.2
Solids separation (thickener, drum filters, tanks, agitators,	,	
pumps, and conveyor) Solids disposal (onsite disposal facilities including reslurry tank, agitator, slurry disposal pumps, and pond water return	1,596,000	7.6
pumps)	931,000	4.4
Subtotal	18,181,000	86.3
Services, utilities, and miscellaneous	1,091,000	5.2
Total process areas excluding pond construction	19,272,000	
Pond construction	•	91.5
rond construction	1,794,000	8.5
Total direct investment	21,066,000	100.0
Indirect Investment		
Engineering design and supervision	1,356,000	6.5
Architect and engineering contractor	322,000	1.5
Construction expense Contractor fees	3,125,000	14.8
	973,000	4.6
Total indirect investment	5,776,000	27.4
Contingency	5,368,000	25.5
Total fixed investment	32,210,000	152.9
Other Capital Charges		
Allowance for startup and modifications	3,042,000	14.4
Interest during construction	3,865,000	18.4
Total depreciable investment	39,117,000	185.7
Land	366,000	1.7
Working capital	777,000	3.7
Total capital investment	40,260,000	191.1

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175 of by direct oil-fired reheat.

Minimum in-process storage; only pumps are spared.

Disposal pond located 1 mi from power plant.

Investment requirements for flyash removal and disposal excluded FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-65. GENERIC DOUBLE-ALKALI PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW existing oil-fired power unit, 2.5% S in oil; 0.3 lb $SO_2/MBtu$ heat input allowable emission; onsite solids disposal)

	Annu quant		Unit cost, \$	Total annual cost, \$	% of average annual revenu requirements
Direct Costs					
Raw materials					
Lime	28,030	tons	42.00/ton	1,177,300	10.58
Soda ash	2,670	tons	90.00/ton	240,300	2.16
Total raw materials cost				1,417,600	12.74
Conversion costs					
Operating labor and supervision Utilities	32,800	man-hr	12.50/man-hr	410,000	3.68
Fuel oil (No. 6)	2,676,600	gal	0.40/gal	1,070,600	9.62
Process water	169,300		0.12/kgal	20,300	0.18
Electricity	22,410,000	kWh	0.029/kWh	649,900	5.84
Maintenance					
Labor and material				824,700	7.41
Analyses	4,350	man-hr	17.00/man-hr	74,000	0.67
Total conversion costs				3,049,500	27.40
Total direct costs				4,467,100	40.14
Indirect Costs					
Capital charges					
Depreciation, interim replacement					
insurance at 6.4% of total depre	•				
investment	Clable			2,503,500	22.5
Average cost of capital and taxes	at 9 6%			2,303,300	22.3
of total capital investment	at 0.0%			3,462,400	31.11
Overheads				3,402,400	31.11
Plant, 50% of conversion costs le	es utilities			654,400	5.88
Administrative, 10% of operating				41,000	0.37
Administrative, 10% of operating	1001			41,000	
Total indirect costs				6,661,300	59.86
Total average annual revenue r	equirements			11,128,400	100.00
		\$/bbl	oil \$/MBtu ho	eat \$/short	ton
				.,	
	Mills/kW	h bur	ned input	S remov	ed

a. Basis

Power unit on-stream time, 7,000 hr/yr.

011 burned, 5,324,100 bbl/yr, 9,200 Btu/kWh.

Investment and revenue requirement for removal and disposal of flyash excluded. Total direct investment, \$21,066,000; total depreciable investment, \$39,117,000; and total capital investment, \$40,260,000.

Midwest plant location, 1980 revenue requirements. Remaining life of power plant, 25 yr.

Stack gas reheat to 175°F.
S removed, 14,850 short tons/yr; sol'ds disposal 63,030 tons/yr Ca solids including only hydrate water.

TABLE A-66

GENERIC DOUBLE ALKALI PROCESS 500 MW EXISTING OIL-FIRED POWER UNIT 2.5% S IN OIL REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: \$	40260000				
	ANNUAL OPERA-	POWER UNIT HEAT	POWER UNIT FUEL CONSUMPTION	SULFUR REMOVED BY POLLUTION CONTROL	BY-PRODUCT RATE+ EQUIVALENT TONS/YEAR	NET REVENUE. \$/TON	TOTAL OP. COST INCLUDING REGULATED ROI FOR POWER	TOTAL NET Sales	NET ANNUAL INCREASE (DECREASE) IN COST OF	CUMULATIVE NET INCREASE (DECREASE) IN COST OF
UNIT	KW-HR/	MILLION BTU	BARRELS OIL	PROCESS.	ORY	DRY	COMPANY .	REVENUE.	POWER.	POWER,
START	KW	/YEAR	/YEAR	TUNS/YEAR	SOLIDS	SOLIDS	\$/YEAR	\$/YEAR	S	\$
<u>-</u>										
5										
3										
4										
5				1,440				<u>_</u> _		7.500.50
6 7	7000 7000	32200000	5324100	14800 14800	63000	0.0	14590600	0	14590600	14590600
8	7000	32200000 32200000	5324100 5324100	14800	63000 63000	0.0 0.0	14321500 14052400	0	14321500 14052400	28912100 42964500
9	7000	32200000	5324100	14500	63000	0.0	13783200	0	13783200	56747700
10	7000	32200000	5324100	14800	63000	0.0	13514100	0	13514100	70261800
11	5000	23000000	3802900	10600	45000	0.0	11943500	<u>v</u> -	11943500	82205300
12	5000	23000000	3802900	10600	45000	0.0	11674300	ŏ	11674300	93879600
13	5000	23000000	3802900	10600	45000	0.0	11405200	ŏ	11405200	105284800
14	5000	23000000	3802900	10600	45000	0.0	11136100	Ö	11136100	116420900
15	5000	23000000	3802900	10600	45000	0.0	10867000	0	10867000	127267900
16	3500	16100000	2662000	7400	31500	0.0	9589800	0	9589800	136877700
17	3500	16100000	2667000	7400	31500	0.0	9320700	0	9320700	146198400
18	3500	16100000	5465404	7400	31500	0.0	9051600	0	9051600	155250000
19	3500	16100000	2662000	7400	31500	0.0	8782500	0	8782500	164032500
-50	3500	16100000		7 <u>4</u> 00	31500		8513300	<u>-</u>	8513300_	172545800
21	1500	6900000	1140900	3200	13500	0.0	6814500	0	6814500	179360300
22	1500	6900000	1140900	3200	13500	0.0	6545400	0	6545400	185905700
23	1500	6900000	1140900	3200	13500	0.0	6276200 6007100	v	6276200 6007100	192181900 198189000
24 _ 25	1500	6900000	1140900	3200 3200	13500 13500	0.0	5738000	0	5738000_	203927000
_ E 2	1500 1500	<u>690000</u>		3200	13500	0.0	3138888 5468900		5468900	209395900
27	1500	6900000	1140900	3200	13500	0.0	5199700	ŏ	5199700	214595600
28	1500	6900000	1140900	3200	13500	0.0	4930600	ŏ	4930600	219526200
29	1500	6900000	1140900	3200	13500	0.0	4661500	ŏ	4661500	224187700
_30	_1500	6900000	1140900	3200	13500	0.0	4392300	0_	4392300	228580000
										_
TOT	92500	425500000	70354000	196000	832500		228580000	0	228580000	
LIF	FETIME A	VERAGE INCREAS		_	TING COST					
			S PER BARKEL O				3.25	0.0	3.25	
			PER KILOWATT-H				4.94	0.0	4.94	
			PER MILLION BT				53.72	0.0	53.72	
000050	C COST		PER TON OF S		+ ADC		1166.22	0.0	1166.22 93023600	
PROCES	15 6031	DISCOUNTED AT	INI UI MOELL	DEPATTAGE COS	LAKS	DISCOUNTED PROC	93023600	0 0		
LEV	C 1 E				I EMOTAMENT IO	DISCOONIED PROC		0.0	2.92	
			5 PER BARREL OF PER KILOWATT-HI				2.92 4.44	0.0	4.44	
			ER MILLION BT				48.25	0.0	48.25	
			PER TON OF SU				1048.74	0.0	1048.74	
		DUCLARY		ATT ON MEMOAED				•••	2040814	

TABLE A-67. CITRATE PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT $^{\mathbf{a}}$

(200-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (unloading conveyor, elevator conveyor, pneumatic conveyor, feed storage bins)	417,000	2.2
Feed preparation (feeders, conveyor, tanks, agitator, and		
pumps)	77,000	0.4
Gas handling (common feed plenum and booster fans, gas		
ducts and dampers from plenum to absorber, exhaust gas		
ducts and dampers from absorber to reheater and stack)	1,824,000	9.6
SO ₂ absorption (two packed tower absorbers including		
presaturators and entrainment separators, strippers, compressor, tanks, agitators, and pumps)	5 512 000	29.0
Stack gas reheat (two indirect steam reheaters)	5,512,000	3.1
Chloride purge (feeder, tank, agitator, and pumps)	584,000 60,000	0.3
SO ₂ reduction (reactor tanks, aging tank, agitators, and	00,000	0.5
centrifugal pumps)	661,000	3.5
S separation and removal (flotation tanks, rotary drum	001,000	3.3
filters, pumps, slurry tank, heat exchanger, settling		
tank, heaters, flash drum, and compressor)	1,599,000	8.4
S storage and shipping (S receiving pit, heaters, S pump,	,,	
and storage tank)	445,000	2.3
Sulfate purge (coolers, agitators, centrifuge, tanks,		
pumps, and refrigeration)	544,000	2.9
H ₂ S generation (battery limit plant)	3,641,000	19.2
H ₂ generation (battery limit plant)	2,537,000	13.4
Subtotal	17,901,000	94.3
Services, utilities, and miscellaneous	1,074,000	5.7
Total direct investment	18,975,000	100.0
Indirect Investment		
Engineering design and supervision	2,412,000	12,7
Architect and engineering contractor	603,000	3.2
Construction expense	2,876,000	15.2
Contractor fees	899,000	4.7
Total indirect investment	6,790,000	35.8
Contingency	5,153,000	27.1
Total fixed investment	30,918,000	162.9
Other Capital Charges		
Allowance for startup and modifications	3,092,000	16.3
Interest during construction	3,710,000	19.6
Total depreciable investment	37,720,000	198.8
Land	35,000	0.2
Working capital	1,033,000	5.4
Total capital investment	38,788,000	204.4

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-63. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS $^{\mathbf{a}}$

(200-MW existing coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission)

		Annual uantity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Raw materials					
Lime		,210 tons	42.00/ton	50,800	0.41
Soda ash	1	,110 tons	90.00/ton	99,900	0.81
Citric acid		96 tons	1,340.00/ton	128,600	1.05
Natural gas	443	,000 kft ³	3.50/kf t ³	1,550,500	12.62
Catalyst				8,900	0.07
Total raw materials cost				1,838,700	14.96
Conversion costs					
Operating labor and supervision	52	,700 man-hr	12.50/man-hr	658,800	5.36
Utilities					
Steam	436	,550 MBtu	2.00/MBtu	873,100	7.10
Process water		,000 kgal	0.06/kgal	63,100	0.51
Electricity	27,908	,000 kWh	0.031/kWh	865,100	7.04
Maintenance					
Labor and material				1,327,000	10.81
Analyses	5	,600 man-hr	17.00/man-hr	95,200	0.77
Total conversion costs				3,882,300	31.59
Total direct costs				5,721,000	46.55
Capital charges Depreciation, interim replacements, and insurance at 7.0% of total depreciable					
investment Average cost of capital and taxes at 8.	6%			2,640,400	21.48
of total capital investment Overheads				3,335,800	27.14
Plant, 50% of conversion costs less uti	lities			1,040,500	8.47
Administrative, 10% of operating labor				65,900	0.54
Marketing, 10% of sales revenue				57,200	0.47
Total indirect costs				7,139,800	58.10
Gross average annual revenue require	ments			12,860,800	104.65
Byproduct Sales Revenue					
Sulfur	1.6	,290 short t	ons 40.00/short ton	(571 600)	
	14	,=>o anott t	one words short ton		(4.65)
Subtotal byproduct sales revenue				(571,600)	(4.65)
Total average annual revenue require	ments			12,289,200	100.00
		\$/ton co	al \$/MBtu heat	\$/short ton	\$/short ton
	Mills/kWh	burned	input	S removed	S recovered

a. Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 20 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 633,500 tons/yr, 9,500 Btu/kWh.

Stack gas reheat to 175 F.

S removed, 14,780 short tons/yr.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$18.975.000: total depreciable investment, \$37,720,000;

Total direct investment, \$18,975,000; total depreciable investment, \$37,720,000; and total capital investment, \$38,788,000.

TABLE A-69

CITRATE PROCESS 200 MW EXISTING COAL-FIRED POWER UNIT 3.5% S IN COAL REGULATED CO. ECONOMICS

	AFTER POWER	ANNUAL OPERA- TION+ KW-HR/ KW	POWER UNIT HEAT REQUIREMENT, MILLION BTU /YEAR	POWER UNIT FUEL CONSUMPTION, TONS COAL /YEAR	FIXED SULFUR REMOVED RY POLLUTION CONTROL PROCESS+ TONS/YEAR	INVESTMENT: \$ BY-PRODUCT RATE, EQUIVALENT TONS/YEAR SULFUR	38788000 NET REVENUE. S/TON SULFUR	TOTAL OP. COST INCLUDING REGULATED ROI FOR POWER COMPANY, \$/YEAR	TOTAL NET SALES REVENUE, \$/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER, \$	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER,
208		5000 5000 5000 5000 3500 3500 3500 3500	DOLLARS	452400 452400 452400 452400 452400 316700 316700 316700 135700 135700 135700 135700 135700 135700 135700 135700 135700 135700 135700 135700 135700 135700 135700 135700 135700	DAL BURNED	10200 10200 10200 10200 10200 10200 7100 71	40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00 40.00	14523800 14199400 13875100 13550700 13526300 11593100 11268700 10619900 10295500 8080500 7756100 7431700 7107300 6782900 6458600 6134200 5809800 5485400 5161000 190304300 36.58	408000 408000 408000 408000 208000 208000 208000 208000 208000 208000 208000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 12400 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000 124000	14115800 13791400 13467100 13142700 12818300 11309100 10984700 10660300 10335900 10011500 7956500 7632100 7307700 6983300 6658900 5334600 6010200 5685800 5361400 5037000	14115800 27907200 41374300 54517000 67335300 78644400 89629100 1106289400 1106289400 120636800 120636800 136225400 143533100 150516400 157175300 163509900 169520100 175205900 180567300 188604300
	PROCES LEV	S COST	CENTS F DOLLARS DISCOUNTED AT INCREASE (DECF DOLLARS MILLS F CENTS F	PER MILLION BTO S PER TON OF SU 11.6% TO INIT	J HEAT INPUT JLFUR REMOVED FIAL YEAR+ DOL OPERATING COS DAL BURNED DUR J HEAT INPUT	LARS T EQUIVALENT TO	DISCOUNTED PROC	174.19 1559.87 87183000	4.30 38.52 2320500	169.89 1521.35 84862500	

TABLE A-70. CITRATE PROCESS

SUIDIARY OF ESTIMATED CAPITAL INVESTMENT

(200-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (unloading conveyor, elevator conveyor, .	٠	
pneumatic conveyor, feed storage bins) Feed preparation (feeders, conveyor, tanks, agitator, and	408,000	2.2
pumps)	75,000	0.4
Gas handling (common feed plenum and booster fans, gas	,	0.4
ducts and dampers from plenum to absorber, exhaust gas	1 705 000	
ducts and dampers from absorber to reheater and stack) SO, absorption (two packed tower absorbers including	1,785,000	9.6
presaturators and entrainment separators, strippers,		
compressor, tanks, agitators, and pumps)	5,400,000	29.1
Stack gas reheat (two indirect steam reheaters)	569,000	3.1
Chloride purge (feeder, tank, agitator, and pumps)	59,000	0.3
SO ₂ reduction (reactor tanks, aging tank, agitators, and		
centrifugal pumps)	649,000	3.5
S separation and removal (flotation tanks, rotary drum filters, pumps, slurry tank, heat exchanger, settling		
tank, heaters, flash drum, and compressor)	1,568 000	8.4
S storage and shipping (S receiving pit, heaters, S pump.	2,500,000	0.4
and storage tank)	436,000	2.3
Sulfate purge (coolers, agitators, centrifuge, tanks,		
pumps, and refrigeration)	531,000	2.8
H ₂ S generation (battery limit plant)	3,577,000	19.3
H ₂ generation (battery limit plant)	2,480,000	13.3
Subtotal	17,537,000	94.3
Services, utilities, and miscellaneous	1,052,000	5.7
Total direct investment	18,589,000	100.0
Indirect Investment		
Engineering design and supervision	2,394,000	. 12.9
Architect and engineering contractor	599,000	3.2
Construction expense	2,828,000	15.2
Contractor fees	885,000	4.8
Total indirect investment	6,706,000	36.1
Contingency	5,059,000	27.2
Total fixed investment	30,354,000	163.3
Other Capital Charges		
Allowance for startup and modifications	3,035,000	14.0
Interest during construction	3,643,000	16.3 19.6
Total depreciable investment	37,032,000	199.2
Land	35,000	0.2
Working capital	1,008,000	5.4
• • • • • •		
Total capital investment	38,075,000	204.8

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-71. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(200-MW new coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission)

		nnual intity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Raw materials					
Lime	1,	170 tons	42.00/ton	49,100	0.42
Soda ash	1,	070 tons	90.00/ton	96,300	0.83
Citric acid		93 tons	1,340.00/ton	124,600	1.07
Natural gas	429,	000 kft ³	3.50/kft ³	1,501,500	12.86
Catalyst				8,600	0.07
Total raw materials cost				1,780,100	15.25
Conversion costs					
Operating labor and supervision	52,	700 man-hr	12.50/man-hr	658,800	5.64
Utilities	(22	600 MRs	2.00/200	0/7 000	3.06
Steam Process water		600 MBtu	2.00/MBtu	847,200	7.26
rrocess water Electricity		200 kgal	0.06/kgal	61,200	0.52
Maintenance	20,947,	000 kWh	0.031/kWh	835,400	7.16
Labor and material				1 301 300	11.15
Analyses	5,	600 man-hr	17.00/man-hr	1,301,200 95,200	0.82
Total conversion costs				3,799,000	32.55
Total direct costs				5,579,100	47.80
Capital charges Depreciation, interim replacements, au insurance at 6.0% of total depreciab					
investment				2,221,900	19.04
Average cost of capital and taxes at of total capital investment Overheads	0.0%			3,274,500	28.07
Plant, 50% of conversion costs less u	riliriae			1,027,600	8.80
Administrative, 10% of operating labo				65,900	0.56
Marketing, 10% of sales revenue	-			55,400	0.47
Total indirect costs				6,645,300	56.94
Gross average annual revenue requi	rements			12,224,400	104.74
Byproduct Sales Revenue					
Sulfur	13,	,840 short to	ons 40.00/short ton	(553,600)	(4.74)
Subtotal byproduct sales revenue				(553,600)	(4.74)
Total average annual revenue requi	rements			11,670,800	100.00
		\$/ton coa	al \$/MBtu heat	\$/short ton	\$/short tor
	Mills/kWh	burned	input input	S removed	S recovered

a. Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 613,200 tons/yr, 9,200 Btu/kWh.

Stack gas reheat to 175°F.

S removed, 14,310 short tons/yr.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$18,589,000; total depreciable investment, \$37,032,000; and total capital investment, \$38,075,000.

TABLE A-72

CITRATE PROCESS 200 MM NEW COAL-FIRED POWER UNIT 3.5% S IN COAL, REGULATED CO. ECONOMICS

				FIXED	INVESTMENT:	\$ 38075000				
AFTER		POWER UNIT HEAT REQUIREMENT, MILLION BTU /YEAR	POWER UNIT FUEL CUNSUMPTION, TONS COAL /YEAR	SULFUR REMOVED BY POLLUTION CONTROL PROCESS. TONS/YEAR	BY-PRODUCT RATE, EQUIVALENT TONS/YEAR SULFUR	NET REVENU \$/TON SULFUR	ROI FOR POWER COMPANY,	TBTAL NET SALES REVENUE. \$/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER,	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER, \$
1	7000	12880000	613300	14300	13800	40.00	15498800	552000	14946800	14946800
ž	7000	12880000	613300	14300	13800	40.00	15286500	552000	14734500	29681300
3	7000	12880000	613300	14300	13800	40.00	15074200	552000	14522200	44203500
4	7000	12880000	613300	14300	13800	40.00	148618))	552000	14309800	5851 3300
5	7000	1288.0000	613300	16300	13800_	40-00	14649500	552000_	14097500_	72610800
6	7000	12880000	613300	14300	13800	40.00	144372))	552000	13885200	86496000
7	7000	12880000	613300	14300	13800	40.00	14224900	552000	13672900	100168900
8	7000	12880000	613300	14300	13800	40.00	14012600	552000	13460600	11362 9500
9	7000	12880000	61330C	14300	13800	40.00	13800300	552000	13248300	126877800
-T0	7000	12880000	613300	14300	13800.		13587900_	552000_	13035900_	139913700
11	5000	9200000	438100	10200	9900	40.00	11744700	396000	11348700	151262400
12	5000	9200000	438100	10200	9900	40 -00	11532430	396000	11136400	162398800
13	5000	9200000	438100	10200	9900	40.00	11320100	396000	10924100	173322900
14	5000	9200000	438100	10200	9900	40.00	11107800	396000	10711800	184034700
15 16	<u>5000</u> 3500	<u>920000</u>	<u>438100</u> 306700	10200 7200	9900	40-00	10895500	35 v 000_	10699500_	194534200
17	3500 3500	6440000	306700	7200 7200	6900 6900	40.00 40.00	9406400 9194100	276000 276000	9130400	203664600 212582700
18	3500	6440000	306700	7200	6900	40.00	8981830	276000	8918100 8705800	221288500
19	3500	6440000	306 700	7200	6900	40.00	8769500	276000	8493500	229782000
20	3500	6440000	306700	7200	0069	<u> </u>	8552200	276000	8281200_	2380&3200
21	1500	2760000	13140C	3100	3000	40.00	6498300	120000	6378300	244441500
22	1500	2760000	131400	3100	3000	40.00	6285900	120000	6165900	250607400
23	1500	2760000	131400	3100	3000	40.00	6073600	120000	5953600	256561000
24	1500	2760000	131400	3100	3000	40.00	5861300	120000	5741300	262302300
_25	1500	2760000	131400	3100	3000.	60_0	5669011	120000_	5529000_	267831300
26	1500	2760000	131400	3100	3000	40.00	5436700	120000	5316700	273148000
27	1500	2760000	131400	3100	3000	40.00	52244))	120000	5104400	278 25 2400
28	1500	276 00 0 0	131400	3100	3000	40.00	5012000	120000	4892000	283144400
29	1500	2760000	131400	3100	3000	40 -00	47997 30	120000	4679700	287824100
30	1500	2760000	131600	3100	3000	60.00_	4583400	120000_	4467400_	292291500
	127500 FETIME A	234600000 VERAGE INCREA	11171000 SE (CECREASE)	2610D0 IN UNIT OPERAT	252000 TING COST		302371500	10080000	292291500	
		DOLLAR	S PER TON OF C	DAL BURNED			27. 07	0.90	26.17	
		MILLS	PER KILOWATT-H	OUR			11.86	0-40	11.46	
			PER MILLION BT				128.89	4.30	124.59	
			S PER TON OF S				1158.51	38.62	1119.89	
PROCE	SS COST	DISCOUNTED AT	11.62 TO INI	TIAL YEAR, DOL	LARS		108430500	3922200	104508300	
LE	VELIZED				T EQUIVALENT	TO DISCOUNTED	PROCESS COST DVI			
			PER TON OF C				24.90	0.90	24.00	
			ER KILOWATT-HE	- • • •			10.91	0.40	10.51	
			ER MILLION BTO				118.57	4.28	114.29	
		DULLARS	PER TON OF SU	DELOK MEMMAED			1067.23	38.61	1028.63	

TABLE A-73. CITRATE PROCESS

SULLIARY OF ESTIMATED CAPITAL INVESTMENT $^{\mathbf{a}}$

(500-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total direc investment
Direct Investment		
Materials handling (unloading conveyor, elevator conveyor,		
pneumatic conveyor, feed storage bins)	782,000	2.1
Feed preparation (feeders, conveyor, tank, agitator, and pumps)	12/ 000	۸,
Gas handling (common feed plenum and booster fans, gas	134,000	0.4
ducts and dampers from plenum to absorber, exhaust gas		
ducts and dampers from absorber to reheater and stack)	4,154,000	11.1
SO, absorption (four packed tower absorbers including	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	
presaturators and entrainment separators, strippers,		
compressor, tanks, agitators, and pumps)	12,459,000	33.3
Stack gas reheat (four indirect steam reheaters)	1,312,000	3.5
Chloride purge (feeder, tank, agitator, and pumps)	98,000	0.3
SO reduction (reactor tanks, aging tank, agitators, and		
centrifugal pumps)	1,114,000	3.0
S separation and removal (flotation tanks, rotary drum filters, pumps, slurry tank, heat exchanger, settling		
tank, heaters, flash drum, and compressor)	2,743,000	7.3
S storage and shipping (S receiving pit, heaters, S pump,	2,743,000	7.3
and storage tank)	783,000	2.1
Sulfate purge (coolers, agitators, centrifuge, tanks,	703,000	2.1
pumps, and refrigeration)	1,009,000	2.7
H ₂ S generation (battery limit plant)	5,921,000	15.8
H ² generation (battery limit plant)	4,753,000	12.7
Subtotal	35,262,000	94.3
Services, utilities, and miscellaneous	2,116,000	_5.7
Total direct investment	37,378,000	100.0
Indirect Investment		
Engineering design and supervision	3,352,000	9.0
Architect and engineering contractor	838,000	2.2
Construction expense	5,049,000	13.5
Contractor fees	1,505,000	4.0
Total indirect investment	10,744,000	28.7
Contingency	9,624,000	25.8
Total fixed investment	57,746,000	154.5
Other Capital Charges		
Allowance for startup and modifications	5,775,000	15.5
Interest during construction	6,930,000	18.5
Total depreciable investment	70,451,000	188.5
Land	39,000	0.1
Working capital	2,115,000	5.7
Total capital investment	72,605,000	194.3
	72,003,000	194.3

midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyssh removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-74. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS^a

(500-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

		nnual antity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Raw materials					
Lime	2,9	30 tons	42.00/ton	123,100	0.53
Soda ash	2,6	80 tons	90.00/ton	241,200	1.04
Citric acid		233 tons	1,340.00/ton	312,200	1.35
Natural gas	1,070,0	000 kft ³	3.50/kft ³	3,745,000	16.16
Catalyst				21,600	0.09
Total raw materials cost				4,443,100	19.17
Conversion costs					
Operating labor and supervision	67,9	920 man-hr	12.50/man-hr	849,000	3.66
Utilities					
Steam		000 MBtu	2.00/MBtu	2,118,000	9.14
Process water		300 kgal	0.06/kgal	152,900	0.66
Electricity	67,568,0	000 kWh	0.029/kWh	1,959,500	8.46
Maintenance				•	
Labor and material				2,242,700	9.68
Analyses	10,6	000 man-hr	17.00/man-hr	180,200	0.78
Total conversion costs				7,502,300	32.38
Total direct costs				11,945,400	51.55
Capital charges Depreciation, interim replacements, an insurance at 6.4% of total depreciab					
investment				4,508,900	19.46
Average cost of capital and taxes at 8 of total capital investment Overheads	0.0%			6,244,000	26.93
Plant, 50% of conversion costs less up	flities			1,636,000	7.06
Administrative, 10% of operating labor				84.900	0.37
Marketing, 10% of sales revenue	•			138,400	0.60
Total indirect costs				12,612,200	54.42
Gross average annual revenue requi	rements			24,557,600	105.97
Byproduct Sales Revenue					
Sulfur	34,59	00 short tons	40.00/short ton	(1,383,600)	(5.97)
Subtotal byproduct sales revenue				(1,383,600)	(5.97)
Total average annual revenue require	rements			23,174,000	100.00
	M4.13 - /I-IP	\$/ton coal		\$/short ton	\$/short ton
	Mills/kWh	burned	input	S removed	S recovered
	6.62	15.11	0.72		

a. Basis

Midwest plant location, 1980 revenue requirements. Remaining life of power plant, 25 yr. Power unit on-stream time, 7,000 hr/yr. Coal burned, 1,533,350 tons/yr, 9,200 Btu/kWh. Stack gas reheat to 175°F.

Scannoid 35,780 short tons/yr.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$37,378,000; total depreciable investment, \$70,451,000; and total capital investment, \$72,605,000.

TOTAL PRICE PRIC					FIXED	INVESTMENT:	72605000				
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PROCESS COST DISCOUNTEC AT 11.62 TO INITIAL YEAR, OCLLARS LEVELIZED INCREASE (DECREASE) IN UNIT OPERATING COST EQUIVALENT TO DISCOUNTED PROCESS COST OVER LIFE OF POWER UNIT DOLLARS PER TON OF COAL BURNED MILLS PER KILOWATT-HOUR 7.32 CERTS PER PILLION BYL HEAT INPLT 101.34 4.30 97.04											
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DOLLARS PER TON OF COAL BURNED 21.28 0.90 20.38 MILLS PER KILOWATT-HOUR 9.32 0.39 8.93 CERTS PER PILLION BYL HEAT INPLY 101.34 4.30 97.04	LE	VELIZED	INCREASE (DECA	EASE) IN UNIT	OPERATING CO.	ST EQUIVALENT	TO DISCOUNTED PE				
MILLS PER KILOWATT-HOUR 9.32 0.39 8.93 CERTS PER PILLION BYL HEAT INPLT 101.34 4.30 97.04											
CERTS PER PILLION BYL HEAT INPLT 101.34 4.30 97.04								9.32	0.39	B.93	
			CERTS F	ER PILLION BT	L HEAT INPLT				4.30		
			DOLLARS	PER TON OF S	ULFUR REMOVED			911.31	38.64	872.67	

TABLE A-76. CITRATE PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(500-MW new coal-fired power unit, 2.0% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (unloading conveyor, elevator conveyor,		
pneumatic conveyor, feed storage bins) Feed preparation (feeders, conveyor, tank, agitator, and	444,000	1.5
pumps) Gas handling (common feed plenum and booster fans, gas	81,000	0.3
ducts and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack) SO ₂ absorption (four packed tower absorbers including	4,093,000	13.7
presaturators and entrainment separators, strippers,	10 000	
compressor, tanks, agitators, and pumps)	12,285,000	41.2
Stack gas reheat (four indirect steam reheaters)	1,222,000	4.1
Chloride purge (feeder, tank, agitator, and pumps) SO ₂ reduction (reactor tanks, aging tank, agitators, and	97,000	0.3
centrifugal pumps)	606 000	
filters, pumps, slurry tank, heat exchanger, settling	696,000	2.3
tank, heaters, flash drum, and compressor)	1,685,000	5.6
S storage and shipping (S receiving pit, heaters, S pump,	1,005,000	3.0
and storage tank) Sulfate purge (coolers, agitators, centrifuge, tanks,	470,000	1.6
pumps, and refrigeration)	577,000	1.9
H ₂ S generation (battery limit plant)	3,817,000	12.8
H ₂ generation (battery limit plant)	2,697,000	9.0
Subtotal	28,164,000	94.3
Services, utilities, and miscelianeous	1,690,000	5.7
Total direct investment	29,854,000	100.0
Indirect Investment		
Engineering design and supervision	2,728,000	9.1
Architect and engineering contractor	682,000	2.3
Construction expense	4,190,000	14.0
Contractor fees	1,268,000	4.2
Total indirect investment	8,868,000	29.6
Contingency	7,744,000	26.0
Total fixed investment	46,466,000	155.6
Other Capital Charges		
Allowance for example and modificanting		
Allowance for startup and modifications Interest during construction	4,647,000 5,576,000	15.6 18.7
Total depreciable investment	56,689,000	189.9
Land	20 000	
Working capital	39,000 1,370,000	0.1 4.6
Total capital investment	58,098,000	

a. Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyash removal and disposal excluded; FGD process investment

estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-77. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS a

(500-MW new coal-fired power unit, 2.0% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

Mills/kWh burned input S removed S recover			Annual uantity	Unit cost, \$	Total annual cost, \$	% of average annual revenu- requirements
Lime	Direct Costs					
1.210 tons	Raw materials					
Citricicid 105 tons 1,340.00/ton 140,700 0.82 Natural gas 483,000 kft 3.50/kft 1.690.500 9.89 Natural gas 483,000 kft 3.50/kft 1.690.500 9.89 9.700 0.06 Total raw materials cost 2.005,200 11.73 Conversion costs Operating labor and supervision 56,380 man-hr 12.50/man-hr 704,800 4.12 Utilities Steam 741,500 MBtu 2.00/MBtu 1,483,000 8.68 Process water 1.253,400 kgal 0.06/kgal 75,200 0.44 Electricity 56,355,000 kWh 0.029/kWh 1.634,300 9.56 Naintenance Labor and material 1,791,200 10.49 Analyses 9,500 man-hr 17.00/man-hr 161,500 0.94 Total conversion costs 9,500 man-hr 17.00/man-hr 161,500 0.94 Total conversion costs 7,855,200 45.96 Total direct costs 7,855,200 45.96 Total conversion costs 9,500 man-hr 17.00/man-hr 161,500 0.94 15.96 Total conversion costs 10,700 man-hr 17.00/man-hr 17.00/man-hr 17.00/man-hr 17.00/man-hr 18.00 0.94 15.96 Total conversion costs 10,700 man-hr 17.00/man-hr 18.04 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94 161,500 0.94						
Natural gas	Soda ash	1				
Total raw materials cost Total conversion costs Operating labor and supervision Total conversion costs Total direct costs Total direct costs Total direct costs Total direct costs Total capital investment Average cost of capital and taxes at 8.6% of total capital investment Average cost of capital and taxes at 8.6% of total capital investment Average cost of capital and taxes at 8.6% of total capital investment Total indirect costs						
Conversion costs Operating labor and supervision 56,380 man-hr 12.50/man-hr 704,800 4.12 Utilities Steam 741,500 MBtu 2.00/MBtu 1,483,000 8.68 Process water 1,253,400 kgal 0.06/kgal 75,200 0.44 Electricity 56,355,000 kWn 0.029/kWn 1,634,300 9.56 Maintenance Labor and material 1,791,200 10.49 Analyses 9,500 man-hr 17.00/man-hr 161,500 0.34.23 Total conversion costs 5,850,000 34.23 Total direct costs 7,855,200 45.96 Indirect Costs Capital charges Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment 4,496,400 29.24 Overheads Plant, 50% of conversion costs less utilities 1,1328,800 7.77 Administrative, 10% of operating labor 70,500 0.41 Marketing, 10% of sales revenue 62,300 0.36 Total indirect costs Cross average annual revenue requirements 40,00/short ton (622,800) (3.64) Subtotal byproduct sales revenue (622,800) (3.64) Subtotal byproduct sales revenue 17,091,700 100.00		483	3,000 ktt-	3.50/Kt E		
Operating labor and supervision 56,380 man-hr 12.50/man-hr 704,800 4.12 Utilities 741,500 MBtu 2.00/MBtu 1,483,000 8.68 Process water 1,233,400 kgal 0.06/kgal 75,200 0.44 Electricity 56,355,000 kWh 0.029/kWh 1,634,300 9.56 Maintenance Labor and material 1,791,200 10.49 Analyses 9,500 man-hr 17.00/man-hr 161,500 0.94 Total conversion costs 5,850,000 34.23 Total direct costs 7,855,200 45.96 Indirect Costs 5,850,000 34.23 Capital charges Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment 3,401,300 19.90 Average cost of capital and taxes at 8.6% of total capital investment 4,996,400 29.24 Overheads 71 1,7500 0.41 Marketing, 10% of sales revenue 70,500 0.41 Marketing, 10% of sales revenue 62,300 0.36 Gross average annual revenue requirements 17,714,500	Total raw materials cost				2,005,200	11.73
Operating labor and supervision 56,380 man-hr 12.500/mman-hr 704,800 4.12 Utilities 741,500 MBtu 2.00/MBtu 1,483,000 8.68 Process water 1,233,400 kgal 0.06/kgal 75,200 0.44 Electricity 56,355,000 kWh 0.029/kWh 1,634,300 9.56 Maintenance 1,791,200 10.49 10.49 Analyses 9,500 man-hr 17.00/man-hr 161,500 0.94 Total conversion costs 5,850,000 34.23 Total direct costs 7,855,200 45.96 Indirect Costs 20 45.96 Capital charges 20 45.96 Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment 3,401,300 19.90 Average cost of capital and taxes at 8.6% of total capital investment 4,996,400 29.24 Overheads 71 70,500 0.41 Marketing, 10% of sales revenue 70,500 0.41 Archeting, 10% of sales revenue 62,300 0.36 Gross average annual revenue requi	Conversion costs					
Utilities Steam		56	5.380 man-hr	12.50/man-hr	704.800	4.12
Steam			,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,			
Process water 1,253,400 kgal 0.06/kgal 75,200 0.44 Electricity 56,355,000 kWh 0.029/kWh 1,634,300 9.56 Maintenance Labor and material 1,791,200 10.49 Analyses 9,500 man-hr 17.00/man-hr 161,500 0.94 Total conversion costs 5,850,000 34.23 Total direct costs 7,855,200 45.96 Total direct costs 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200 7,855,200		741	1.500 MBtu	2.00/MBtu	1.483.000	8.68
Electricity 56,355,000 kWh 0.029/kWh 1,634,300 9.56 Maintenance Labor and material 1,791,200 10.49 Analyses 9,500 man-hr 17.00/man-hr 161,500 0.94 Total conversion costs 5,850,000 34.23 Total direct costs 7,855,200 45.96 Indirect Costs Capital charges Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment 3,401,300 19.90 Average cost of capital and taxes at 8.6% of total capital investment 4,996,400 29.2% Overheads Plant, 50% of conversion costs less utilities 1,328,800 7.77 Administrative, 10% of operating labor 70,500 0.41 Marketing, 10% of sales revenue 62,300 0.36 Total indirect costs 9,859,300 57.68 Gross average annual revenue requirements 10,570 short tons 40.00/short ton (622,800) (3.64) Byproduct Sales Revenue Sulfur 15,570 short tons 40.00/short ton (622,800) (3.64) Total average annual revenue requirements 17,091,700 100.00						
Maintenance Labor and material Analyses 9,500 man-hr 17.00/man-hr 161,500 0.94 Total conversion costs 5,850,000 34.23 Total direct costs 7,855,200 45.96 Indirect Costs Capital charges Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment 4,996,400 29.24 Average cost of capital and taxes at 8.6% of total capital investment 4,996,400 29.24 Decrheads Plant, 50% of conversion costs less utilities 1,328,800 7.77 Administrative, 10% of operating labor 70,500 0.41 Marketing, 10% of sales revenue 62,300 0.36 Total indirect costs 9,859,300 57.68 Cross average annual revenue requirements 15,570 short tons 40.00/short ton (622,800) (3.64) Total average annual revenue requirements 17,091,700 100.00 Sylton coal S/MBtu heat S/short ton S/short ton Mills/kWh burned input S removed S recover					•	
1,791,200 10.49		30,03.	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	0.000,000	2,03.,000	
Analyses 9,500 man-hr 17.00/man-hr 161,500 0.94 Total conversion costs 5,850,000 34.23 Total direct costs 7,855,200 45.96 Indirect Costs Capital charges Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment 3,401,300 19.90 Average cost of capital and taxes at 8.6% of total capital investment 4,996,40C 29.24 Overheads Plant, 50% of conversion costs less utilities 1,328,800 7.77 Administrative, 10% of operating labor 70,500 0.41 Marketing, 10% of sales revenue 62,300 0.36 Total indirect costs 9,859,300 57.68 Gross average annual revenue requirements 17,714,500 103.64 Byproduct Sales Revenue Sulfur 15,570 short tons 40.00/short ton (622,800) (3.64) Total average annual revenue requirements 17,091,700 100.00					1.791.200	10.49
Total direct costs Indirect Costs Capital charges Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment Average cost of capital and taxes at 8.6% of total capital investment Voerheads Plant, 50% of conversion costs less utilities Administrative, 10% of operating labor Marketing, 10% of sales revenue Total indirect costs Gross average annual revenue requirements Sulfur 15,570 short tons 45.96 45.96 45.96 45.96 19.90 45.96 19.90 49.96,400 29.24 70,500 0.41 62,300 0.36 62,300 0.36 70,500 0.41 70,500 0.41 70,500 0.41 70,500 0.45 622,800) 103.64 8yproduct Sales Revenue Total average annual revenue requirements 17,714,500 103.64 Total average annual revenue requirements 17,091,700 100.00 Mills/kWh burned input S removed S recover		ģ	9,500 man-hr	17.00/man-hr		
Indirect Costs Capital charges Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment Average cost of capital and taxes at 8.6% of total capital investment Verleads Plant, 50% of conversion costs less utilities Plant, 50% of conversion costs less utilities Administrative, 10% of operating labor Total indirect costs Gross average annual revenue requirements Total indirect sales Revenue Sulfur 15,570 short tons 40.00/short ton (622,800) (3.64) Total average annual revenue requirements \$ // NBtu heat \$ // short ton \$	Total conversion costs				5,850,000	34.23
Depreciation, interim replacements, and insurance at 6.4% of total depreciable investment	Total direct costs				7,855,200	45.96
investment Average cost of capital and taxes at 8.6% of total capital investment Overheads Plant, 50% of conversion costs less utilities Administrative, 10% of operating labor Marketing, 10% of sales revenue Total indirect costs Gross average annual revenue requirements 15,570 short tons Total average annual revenue requirements 17,091,700 100.00 Mills/kWh burned Syton coal SymBtu heat Syshort ton	Depreciation, interim replacements, and					
of total capital investment Overheads Plant, 50% of conversion costs less utilities Plant, 50% of conversion costs Plant, 50% o	investment	· •/			3,401,300	19.90
Plant, 50% of conversion costs less utilities	of total capital investment	J /6			4,996,400	29.24
Administrative, 10% of operating labor 70,500 0.41 Marketing, 10% of sales revenue 62,300 0.36 Total indirect costs 9,859,300 57.68 Gross average annual revenue requirements 17,714,500 103.64 Byproduct Sales Revenue 15,570 short tons 40.00/short ton (622,800) (3.64) Subtotal byproduct sales revenue (622,800) (3.64) Total average annual revenue requirements 17,091,700 100.00 Mills/kWh burned input S removed S recover		lition			1.328.800	7.77
Marketing, 10% of sales revenue 62,300 0.36 Total indirect costs 9,859,300 57.68 Gross average annual revenue requirements 17,714,500 103.64 Byproduct Sales Revenue 5,570 short tons 40.00/short ton (622,800) (3.64) Subtotal byproduct sales revenue (622,800) (3.64) Total average annual revenue requirements 17,091,700 100.00 Mills/kWh burned 1put \$/short ton		illes				0.41
Gross average annual revenue requirements 17,714,500 103.64 Byproduct Sales Revenue Sulfur 15,570 short tons 40.00/short ton (622,800) Subtotal byproduct sales revenue (622,800) Total average annual revenue requirements 17,091,700 100.00 Mills/kWh burned input S removed S recover						
Byproduct Sales Revenue Sulfur 15,570 short tons 40.00/short ton (622,800) (3.64) Subtotal byproduct sales revenue (622,800) (3.64) Total average annual revenue requirements 17,091,700 100.00 **Ston coal S/MBtu heat S/short ton S/short ton Mills/kWh burned input S removed S recover	Total indirect costs				9,859,300	57.68
Sulfur 15,570 short tons 40.00/short ton (622,800) (3.64) Subtotal byproduct sales revenue (622,800) (3.64) Total average annual revenue requirements 17,091,700 100.00 Mills/kWh Ston coal S/MBtu heat S/short ton S/short ton S/secover	Gross average annual revenue requirem	ments			17,714,500	103.64
Subtotal byproduct sales revenue (622,800) (3.64) Total average annual revenue requirements 17,091,700 100.00 **Ston coal \$/MBtu heat \$/short ton \$/	Byproduct Sales Revenue					
Total average annual revenue requirements 17,091,700 100.00 \$/ton coal \$/MBtu heat \$/short ton \$/short t Mills/kWh burned input \$ removed \$ recover	Sulfur	1	5,570 short to	ns 40.00/short ton	(622,800)	(3.64)
\$/ton coal \$/MBtu heat \$/short ton \$/short t Mills/kWh burned input 5 removed 5 recover	Subtotal byproduct sales revenue				(622,800)	(3.64)
Mills/kWh burned input S removed S recover	Total average annual revenue requires	ments			17,091,700	100.00
	,	4431a/ktn				\$/short ton
	Equivalent unit revenue requirements	4.88	11.39	1nput 0.54	1,055.04	1,097.73

Midwest plant location, 1980 revenue requirements. Remaining life of power plant, 30 yr. Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh.
Stack gas reheat to 175 F.
S removed, 16,200 short tons/yr.
Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$29,854,000; total depreciable investment, \$56,689,000; and total capital investment, \$58,098,000.

FIXED INVESTMENT: \$ 58098000

					FIXED	IMAESIMEMI: 2	58058000				
	AFTER	ANNUAL OPERA- TION , KW-HR/ KW	POWER UNST HEAT REQUIREMENT, HILLION BTU /YEAR	PDWER UNIT FUEL CONSUMPTION, TOAS CCAL /YEAR	SULFUR REMOVED BY POLLUTION CONTROL PROCESS. TONS/YEAR	BY-PRODUCT RATE, EQUIVALENT TONS/YEAR SULFUR	NET REVENUE \$/TON SULFUR	TOTAL OP. COST INCLUDING REGULATED ROI FOR POWER COMPANY, \$/YEAR	TOTAL NET SALFS REVENUE, \$/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER,	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER, \$
	1	7000	31500000	1500000	16200	15600	40.00	22711000	624000	22087000	22087000
	ž	7000	31500000	1500000	16200	15600	40.00	22385900	624006	21761900	43848900
	3	7000	31500000	1500000	16200	15600	40.00	220609))	624000	21436900	65285800
	4	7000	31500000	1500000	16200	15600	40.00	21735900	624000	21111900	86397700
	5	7000	31500000	1500000	16200	15600		21410920_	624000_	20786900	107184600
	6	7000	31500000	1500000	16200	15600	40.00	21085900	624000	20461900	127646500
	7	7000	31500000	1500000	16200	15600	40.00	20760900	624000	20136900	147783460
	8	7000	31500000	1500000	16200	15600	40.00	20435900	624000	19811900	167595300
	ğ	7000	31500000	1500000	16200	15600	40.00	20110900	624000	19486900	18708 2200
	<u>_i</u>	7000_	31500000	1500000	16200	15600	40-00	19785900_	624000_	19161900_	206264100
	11	5000	22500000	1071400	11600	11100	40.00	17150400	444000	16706400	222950500
	12	5000	22500000	1071400	11600	11100	40.00	16825400	444000	16381400	239331900
,	13	5000	22500000	1071400	11600	11100	40.00	16500400	444000	16056400	255388300
	14	5000	22500000	1071400	11600	11100	46.00	161754))	444000	15731400	271119700
J	15	5000	22500000	1071400	11600	11100	40-00	15850430	444000	15406400	286526100
	16	3500	15750000	750000	8100	7800	40.00	13726933	312000	13414900	299941000
	17	3500	15750000	750 COO	8100	7800	40.00	13401930	312000	13089900	313030900
	18	3500	15750000	750000	8100	7800	40.00	13076900	312000	12764900	325795800
	19	3500	15750000	750000	8100	7800	40.00	12751900	31 2000	12439900	338235700
	_20	3500	15750000	750000	8100	7800	60_00_	12426830_	312000_	12114800_	350350500
	21	1500	6750000	321400	3500	3300	40.00	9529500	132000	9397500	359748000
	22	1500	6750000	321400	3500	3300	40 .DO	9204500	132000	9072500	368820500
	23	1500	6750000	321400	3500	3300	40.00	8879500	132000	8747500	377568000
	24	1500	6750000	321400	3500	3300	40.00	8554500	132000	8422500	385990500
	_25	1500	6750000	321400	3500	3300	40_00	8229500_	132000_	80.97500_	344088000
	26	1500	6750000	321400	3500	3300	40.00	79045 00	132000	7772500	401860500
	27	1500	6750000	321400	3500	3300	40.00	7579500	132000	7447500	409308000
	28	1500	6750000	321400	3500	3300	40.00	7254500	132000	71 22 500	416430500
	29	1500	6750000	321400	3500	3300	40.00	69294))	132000	6797400	423227900
	_30	1500	6750000	321400	3500	3300	60_00		132000_	6472400_	<u>62970030</u> 0
	LI PROCE:	SS C0 S T	DOLLAR MILLS CENTS DOLLAR DISCOUNTED AT INCREASE FDECI DOLLAR MILLS F	S PER TON OF C PER KILOWATT-H PER MILLION BT S PER TON CF S 11.62 TO INI	OUR U HEAT IMPUT ULFUR REMOVED TIAL YEAR, DOL OPERATING COS OAL BURNED OUR		DISCOUNTED P	441040333 16.14 6.92 76.87 1492.52 158411900 RUCESS COST DV 14.88 6.37 70.83	0.41 0.18 1.98 38.37 4427100 ER LIFF OF 0.42 0.17	429700300 15.73 6.74 74.89 1454.15 153984800 POWER UNIT 14.46 6.20 68.85	
				S PER TON OF S				1376.30	38.47	1337.83	

TABLE A-79. CITRATE PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT $^{\mathbf{a}}$

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total directions investment
Direct Investment		
Materials handling (unloading conveyor, elevator conveyor, pneumatic conveyor, feed storage bins)	770,000	2.1
Feed preparation (feeders, conveyor, tank, agitator, and pumps)	132,000	0.4
Gas handling (common feed plenum and booster fans, gas ducts and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack)	4,093,000	11.1
SO ₂ absorption (four packed tower absorbers including presaturators and entrainment separators, strippers,		
compressor, tanks, agitators, and pumps)	12,285,000	33.2
Stack gas reheat (four indirect steam reheaters)	1,282,000	3.5
Chloride purge (feeder, tank, agitator, and pumps) reduction (reactor tanks, aging tank, agitators, and	97,000 1,100,000	0.3
cëntrifugal pumps) S separation and removal (flotation tanks, rotary drum filters, pumps, slurry tank, heat exchanger, settling	1,100,000	3.0
tank, heaters, flash drum, and compressor) S storage and shipping (S receiving pit, heaters, S pump,	2,706,000	7.3
and storage tank) Sulfate purge (coolers, agitators, centrifuge, tanks,	772,000	2.1
pumps, and refrigeration)	994,000	2.7
${ m H_2^2}$ generation (battery limit plant) ${ m H_2^2}$ generation (battery limit plant)	5,850,000 4,680,000	15.9 12.7
Subtotal	34,761,000	94.3
Services, utilities, and miscellaneous	2,086,000	5.7
Total direct investment	36,847,000	100.0
Indirect Investment		
Engineering design and supervision	3,330,000	9.0
Architect and engineering contractor	833,000	2.3
Construction expense	4,989,000	13.5
Contractor fees	1,488,000	4.0
Total indirect investment	10,640,000	28.8
Contingency	9,497,000	25.8
Total fixed investment	56,984,000	154.6
Other Capital Charges		
Allowance for startup and modifications Interest during construction	5,698,000 6,838,000	15.5 18.6
Total depreciable investment	69,520,000	188.7
Land Working capital	39,000 2,080,000	0.1 5.6
Total capital investment	71,639,000	194.4

asis
Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost
basis for scaling, mid-1979.
Stack gas reheat to 175°F by indirect steam reheat.
Minimum in-process storage; only pumps are spared.
Investment requirements for flyash removal and disposal excluded; FGD process investment
estimate begins with common feed plenum downstream of the ESP.
Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-80. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS $^{\mathbf{a}}$

(500-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

	Ann quan		Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Raw materials					
Lime		0 tons	42.00/ton	120,500	0.53
Soda ash		0 tons	90.00/ton	236,700	1.05
Citric acid			1,340.00/ton	308,200	1.37
Natural gas	1,050,00	00 kft ³	3.50/kft ³	3,675,000	16.31
Catalyst				21,000	0.09
Total raw materials cost				4,361,400	19.35
Conversion costs					
Operating labor and supervision	67,92	20 man-hr	12.50/man~hr	849,000	3.77
Utilities					
Steam	1,035,90		2.00/MBtu	2,071,800	9.19
Process water	2,492,50		0.06/kgal	149,600	0.66
Electricity	66,100,00	00 kWh	0.029/kWh	1,916,900	8.51
Maintenance					
Labor and material				2,210,800	9.81
Analyses	10,60	00 man-hr	17.00/man-hr	180,200	0.80
Total conversion costs				7,378,300	32.74
Total direct costs				11,739,700	52.09
Capital charges Depreciation, interim replacements, an insurance at 6.0% of total depreciabl					
investment Average cost of capital and taxes at 8				4,171,200	18.51
of total capital investment Overheads	• • • •			6,161,000	27.33
Plant, 50% of conversion costs less ut	ilities			1,620,000	7.19
Administrative, 10% of operating labor				84,900	0.38
Marketing, 10% of sales revenue				137,600	0.61
Total indirect costs				12,174,700	54.02
Gross average annual revenue requir	ements			23,914,400	106.11
Byproduct Sales Revenue					
Sulfur	34,410	short tons	40.00/short ton	(1,376,400)	(6.11)
	,		,		
Subtotal byproduct sales revenue				(1,376,400)	(6.11)
Total average annual revenue requir	ements			22,538,000	100.00
		\$/ton coal	\$/MBtu heat	\$/short ton	\$/short tor
	Mills/kWh	burned	input	S removed	S recovered

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh.

Stack gas reheat to 175°F.

S removed, 35,000 short tons/yr.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$36,847,000; total depreciable investment, \$69,520,000; and total capital investment, \$71,639,000.

FIXED INVESTMENT: \$ TOTAL SULFUR BY-PRODUCT OP. COST REMOVED RATE. INCLUDING RET ANNUAL CUMULATIVE YEARS ANNUAL POWER UNIT POWER UNIT EQUIVALENT TUTAL INCREASE BY NET REVENUE. REGULATED NET INCREASE AFTER OPERA-HEAT FUEL **POLLUTION** ROI FOR NET (DECREASE) TONS/YEAR \$/TON (DECREASE) POWER TION. REQUIREMENT, CONSUMPTION. CONTROL POWER SALES IN COST OF IN COST OF UNIT KW-HR/ MILLION BTU TONS COAL PROCESS. COMPANY. REVENUE. POWER. POWER. START K M /YEAR /YEAR TONS/YEAR SULFUR SULFUR \$/YEAR \$/YEAR \$ 1500C0C 40.CO 40.00 5700 0000 40.00 40.00 28481011 __1376000 27105000_ _139510800 40-00-40.00 40.00 276839)) 40.00 40 -00 _10 40.00 _00188205_ 40.00 40.00 40.00 40.00 40.00 21044900. 984000. 75000C 40.00 40.00 40.00 750 000 40.00 45581 3800 _20. 40_00 40.00 40 -00 118156)) 40.00 40 .00 40.00 1061 9900. _25 2500. **34.00** 40.00 40.00 40.00 40.00 54 072 8800 _8331000____557059800 40-00 B623000_ 7500. **74 00** TOT 127500 27321COC 582139800 25080000 LIFETIME AVERAGE INCREASE (DECREASE) IN UNIT OPERATING COST 20.39 DULLARS PER TON OF COAL BURNED 21.31 0.92 0.39 8.74 MILLS PER KILDWATT-HOUR 9.13 101.46 4.37 97.09 CENTS PER PILLION BTU HEAT INPUT 913.16 39.34 873.82 DOLLARS PER TON OF SULFUR REMOVED PROCESS COST DISCOUNTED AT 11.6% TO INITIAL YEAR. DOLLARS LEVELIZED INCREASE (DECREASE) IN UNIT OPERATING COST EQUIVALENT TO DISCOUNTED PROCESS COST OVER LIFE UF POWER UNIT DOLLARS PER TON OF COAL BURNED 19.73 0.92 18.81 8.46 0.40 MILLS PER KILOWATT-HOUR 8.06 93.96 4.37 89.59 CENTS PER MILLION BTU HEAT INPUT 39.32 845.61 806.29 DOLLARS PER TON OF SULFUR REMOVED

TABLE A-32. CITRATE PROCESS

Summary of estimated capital investment $^{\mathrm{a}}$

(500-MW new coal-fired power unit, 5.0% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (unloading conveyor, elevator conveyor,		
pneumatic conveyor, feed storage bins) Feed preparation (feeders, conveyor, tank, agitator, and	1,045,000	2.5
pumps) Gas handling (common feed plenum and booster fans, gas	173,000	0.4
ducts and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack) SO ₂ absorption (four packed tower absorbers including	4,093,000	9.6
presaturators and entrainment separators, strippers,	12 205 202	
compressor, tanks, agitators, and pumps)	12,285,000	28.9
Stack gas reheat (four indirect steam reheaters)	1,283,000	3.0
Chloride purge (feeder, tank, agitator, and pumps) SO ₂ reduction (reactor tanks, aging tank, agitators, and	97,000	0.2
centrifugal pumps) S separation and removal (flotation tanks, rotary drum filters, pumps, slurry tank, heat exchanger, settling	1,418,000	3.3
tank, heaters, flash drum, and compressor)	3,519,000	8.3
S storage and shipping (S receiving pit, heaters, S pump,		0.5
and storage tank) Sulfate purge (coolers, agitators, centrifuge, tanks,	1,017,000	2.4
pumps, and refrigeration)	1,344,000	3.2
H ₂ S generation (battery limit plant)	7,413,000	17.5
H ₂ generation (battery limit plant)	6,354,000	15.0
Subtotal	40,041,000	94.3
Services, utilities, and miscellaneous	2,402,000	5.7
Total direct investment	42,443,000	100.0
Indirect Investment		
Engineering design and supervision	3,816,000	9.0
Architect and engineering contractor	954,000	2.2
Construction expense	5,611,000	13.2
Contractor fees	1,657,000	3.9
Total indirect investment	12,038,000	28.3
Contingency	10,896,000	25.7
Total fixed investment	65,377,000	154.0
Other Capital Charges		
A11		
Allowance for startup and modifications Interest during construction	6,538,000 7,846,000	15.4 _18.5
Total depreciable investment	79,761,000	187.9
Land	20.000	
Working capital	39,000 2,772,000	0.1 <u>6.5</u>
Total capital investment	82,572,000	194.5

Midwest plant location represents project beginnin; mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyash removal and disposal excluded; FGD process investment

estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-33. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS $^{\mathbf{a}}$

(500-MW new coal-fired power unit, 5.0% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

		nual ntity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Raw materials					
Lime		10 tons	42.00/ton	185,200	0.67
Soda ash	4,0	40 tons	90.00/ton	363,600	1.32
Citric acid	3	50 tons	1,340.00/ton	469,000	1.70
Natural gas	1,620,0	00 kft ³	3.50/kf t 3	5,670,000	20.61
Catalyst				32,300	0.12
Total raw materials cost				6,720,100	24.42
Conversion costs					
Operating labor and supervision	79,4	50 man-hr	12.50/man-hr	993,100	3.61
Utilities					
Steam	1,329,8	300 MBtu	2.00/MBtu	2,659,600	9.67
Process water		00 kgal	0.06/kgal	223,600	0.81
Electricity	75,814,0		0.029/kWh	2,198,600	7.99
Maintenance	. ,, ,, ,			-,,	
Labor and material				2,546,600	9.26
Analyses	11,	350 man-hr	17.00/man-hr	193,000	0.70
Total conversion costs				8,814,500	32.04
Total direct costs				15,534,600	56.46
Capital charges Depreciation, interim replacements, an insurance at 6.0% of total depreciabl					
investment				4,785,700	17.39
Average cost of capital and taxes at 8 of total capital investment Overheads	1.6%			7,101,200	25.82
Plant, 50% of conversion costs less ut	414+4			1,866,400	6.78
				99,300	0.36
Administrative, 10% of operating labor Marketing, 10% of sales revenue				208,200	0.76
Total indirect costs				14,060,800	51.11
Gross average annual revenue requir	remeilt e			29,595,400	107.57
oross average annual revenue requir	emetres				
Byproduct Sales Revenue					
Sulfur	52,	050 short to	ns 40.00/short ton	(2,082,000)	(7.57)
Subtotal byproduct sales revenue				(2,082,000)	(7.57)
Total average annual revenue requir	ements			27,513,400	100.00
	Mills/kWh	\$/ton coal	l \$/MBtu heat input	\$/short ton \$ removed	\$/short tor
.		· · · · · · · · · · · · · · · · · · ·			S recovered
Equivalent unit revenue requirements	7.86	18.34	0.87	507.81	528.60

a, Basis

Midwest plant location, 1980 revenue requirements.

Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh.

Stack gas reheat to 175°F.

S removed, 54,180 short tons/yr.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$42,443,000; total depreciable investment, \$79,761,000; and total capital investment, \$82,572,000.

CENTS PER WILLION BTU HEAT INPUT

DOLLARS PER TON OF SULFUR REMOVED

FIXED INVESTMENT: \$ TOTAL SULFUR BY-PROCUCT BP. COST REMOVED RATE. INCLUDING NET ANNUAL CUMULATIVE YEARS ANNUAL POWER UNIT POWER UNIT BY EQUIVALENT NET REVENUE. REGULATED TOTAL INCREASE NET INCREASE AFTER OPERA-POLLUTION HEAT FUEL TONS/YEAR \$/TDN ROI FOR NET (DECREASE) (DECREASE) POWER TION. REQUIREMENT, CONSUMPTION. CONTR OL POWER SALES IN COST OF IN COST OF UNIT KW-HR/ MILLION BTU TONS COAL PROCESS. COMPANY. REVENUE, POWER . POWER. START KW /YEAR /YEAR TONS/YEAR **SULFUR** SULFUR \$/YEAR \$/YEAK \$ \$ 40.00 3461 2900 40.00 20841 00 40.00 3 36 98 3 0 0 40.00 54.200 40-00 40 -00 20081 7900 40.00 40.00 40.00 29505 3300 _10 40-00 20840.00 40.00 40.00 37724 0000 40.00 266468)) 40.00 **_15**. 60.00 75000C 40.00 40.00 5 6000 40.00 40.00 40-00 _20 40.00 14092 ROD 40.00 40.00 40.00 _25 77 PDD ومـمه 40.00 40.00 40.00 40.00 _30_ 40.00 10425100. 6.70.72.2600 TOT 127500 27321C00 LIFETIME AVERAGE INCREASE (DECREASE) IN UNIT OPERATING COST DOLLARS PER TON OF COAL BURNED 25.94 1.39 24.55 MILLS PER KILOWATT-HOUR 11.12 0.60 10.52 CENTS PER MILLION BTU HEAT INPUT 123.52 6.62 116.90 DOLLARS PER TON OF SULFUR REMOVED 718.02 679.56 38.46 PROCESS COST DISCOUNTED AT 11.6% TO INITIAL YEAR. DOLLARS LEVELIZED INCREASE (DECREASE) IN UNIT OPERATING COST EQUIVALENT TO DISCOUNTED PROCESS COST OVER LIFE OF POWER UNIT 22.72 DOLLARS PER TON CF COAL BURNED 24.11 1.39 10.33 9.74 MILLS PER KILDWATT-HOUR 0.59

114.80

667.19

108.18

628.75

6.62

38.44

TABLE A-85. CITRATE PROCESS

Suimary of estimated capital investment $^{\mathrm{a}}$

(1000-MW existing coal-fired power unit, 3.5% S in coal; 1.2 1b SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total direct investment
Direct Investment		
daterials handling (unloading conveyor, elevator conveyor,		
pneumatic conveyor, feed storage bins) Feed preparation (feeders, conveyor, tank, agitator, and	1,260,000	2.2
pumps) Gas handling (common feed plenum and booster fans, gas	204,000	0.4
ducts and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack) SO ₂ absorption (four packed tower absorbers including	6,557,000	11.4
presaturators and entrainment separators, strippers, compressor, tanks, agitators, and pumps)	19,144,000	33.4
Stack gas reheat (four indirect steam reheaters)	2,026,000	3.5
Chloride purge (feeder, tank, agitator, and pumps)	143,000	0.2
SO, reduction (reactor tanks, aging tank, agitators, and	143,000	0.2
centrifugal pumps) Separation and removal (flotation tanks, rotary drum	1,656,000	2.9
filters, pumps, slurry tank, heat exchanger, settling tank, heaters, flash drum, and compressor)	4,130,000	7,2
S storage and shipping (S receiving pit, heaters, S pump,	4,130,000	/ • •
and storage tank) Sulfate purge (coolers, agitators, centrifuge, tanks,	1,203,000	2.1
pumps, and refrigeration)	1,615,000	2.8
H ₂ S generation (battery limit plant)	8,565,000	14.9
H ² generation (battery limit plant)	7,656,000	13.3
Subtotal	54,159,000	94.3
Services, utilities, and miscellaneous	3,250,000	5.7
Total direct investment	57,409,000	100.0
Indirect Investment		
Engineering design and supervision	4,184,000	7.3
Architect and engineering contractor	1,046,000	1.8
Construction expense	7,209,000	12.6
Contractor fees	2,085,000	3.6
Total indirect investment	14,524,000	25.3
Contingency	14,386,000	25.1
Total fixed investment	86,319,000	150.4
Other Capital Charges		
Allowance for startup and modifications	8,632,000	15.0
Interest during construction	10,358,000	18.0
Total depreciable investment	105,309,000	183.4
Land	45,000	0.1
Working capital	3,670,000	6.4
Total capital investment	109,024,000	189.9

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost

basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.
Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-36. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS $^{\mathbf{a}}$

(1000-MW existing coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

	Annu quant		Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Naw materials	£ 720		42.00/ton	240,700	0.65
Lime		tons	90.00/ton	472,500	1.28
Soda ash		tons	1,340.00/ton	609,700	1.65
Citric acid		tons	3.50/kft ⁹	7,350,000	19.91
Natural gas	2,100,000	KIL	3.30/ KIL		_0.11
Catalyst				42,000	_0.11
Total raw materials cost				8,714,900	23.60
Conversion costs			10 50/	1 020 000	2.81
Operating labor and supervision	83,100) man-hr	12.50/man-hr	1,038,800	2.01
Utilities					
Steam	2,062,800		2.00/MBtu	4,125,600	11.17
Process water	4,984,900		0.06/kgal	299,100	0.81
Electricity	132,201,000) kWh	0.028/kWh	3,701,600	10.03
Maintenance					
Labor and material				2,870,500	7.77
Analyses	17,450) man-hr	17.00/man-hr	296,700	_0.80
Total conversion costs				12,332,300	33.39
Total direct costs				21,047,200	56.99
Capital charges Depreciation, interim replacements, and					
insurance at 6.4% of total depreciable investment				6,739,800	18.25
Average cost of capital and taxes at 8. of total capital investment	6%			9,376,100	25.39
Overheads				2,103,000	5.69
Plant, 50% of conversion costs less uti	lities			103,900	0.28
Administrative, 10% of operating labor				2/3,700	0.73
Marketing, 10% of sales revenue				2.3,700	0.73
Total indirect costs				18,593,500	50.34
Gross average annual revenue require	ments			39,640,700	107.33
Byproduct Sales Revenue					
Sulfur	67 . 680) short ton	s 40.00/short ton	(2,707,200)	(7.33)
Sulfur	07,000	, short con	, , , , , , , , , , , , , , , , , , , ,		
Subtotal byproduct sales revenue				(2,707,200)	(7.33)
Total average annual revenue require	ments			36,933,500	100.00
	Mills/kWh	\$/ton coa	1 \$/MBtu heat input	\$/short ton S removed	\$/short to: S recovered
Equivalent unit revenue requirements	5.28	12.31	0.59	527.62	545.71
					J4J./1

a. Basis

Midwest plant location, 1980 revenue requirements. Remaining life of power plant, 25 yr. Power unit on-stream time, 7,000 hr/yr. Coal burned, 2,999,850 tons/yr, 9,000 Btu/kWh. Stack gas reheat to 175°F.

S removed, 70,000 short tons/yr.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$57,409,000; total depreciable investment, \$105,309,000; and total capital investment, \$109,024,000.

FIXED INVESTMENT: \$ 109024000

				FIVED	TMAESIWEMI: 3	109024000				
AFTER	ANNUAL OPERA- TION: KW-HR/ KW	POWER UNIT HEAT REQUIREMENT. MILLION BTU /YEAR	POWER UNIT FUEL CONSUMPTION. TONS COAL /YEAR	SULFUR HEMOVED BY POLLUTION CONTROL PROCESS+ TONS/YEAR	AY-PRODUCT RATE, EQUIVALENT TONS/YEAR	NET REVENUE. \$/TON SULFUR	TOTAL OP. COST INCLUDING REGULATED ROI FOR POWER COMPANY, \$/YEAR	TOTAL NET SALES REVENUE+ \$/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER+ \$	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER+ S
1 ? 3 4										
5	=									
6	7000	63000000	3000000	70000	67700	40.00	49016900	2708000	46308900	46308900
7	7000	63000000	3000000	70000	67700	40.00	48292400	2708000	45584400	91893300
8	7000	63000000	3000000	70000 70000	67700 67700	40.00	47567900	2708000	44859900	136753200
9	7000	63000000	3000000 3000000	70000	67700	40.00 40.00	46843300 46118800	2708000	44135300	180888500
-10	7000 5000	<u>6300000</u>	<u></u>	50000	48300	40.00	39200600	2708000_ 1932000	<u>43410800</u> _ 37268600	2242 <u>930</u> 0 261567900
12	5000	45000000	2142900	50000	48300	40.00	38476000	1932000	36544000	298111900
13	5000	45000000	2142900	50000	48300	40.00	37751500	1932000	35819500	333931400
14	5000	45000000	2142900	50000	48300	40.00	37027000	1932000	35095000	369026400
15	5000	45000000	2142900	50000	48300	40.00	36302400	1932000	34370400_	408396800
16	3500	31500000	1500000	35000	33800	40.00	30833900	1352000	29481900	432878700
17	3500	31500000	1500000	35000	33800	40.00	30109400	1352000	28757400	461636100
18	3500	31500000	1500000	35000	33800	40.00	29384800	1352000	28032800	489668900
19	3500	31500000	1500000	35000	33800	40.00	28660300	1352000	27308300	516977200
20	3500	31500000	1500000	35000	33800	40.00	27935800	1352000	26583800_	543561000
21	1500	13500000	642900	15000	14500	40.00	20623600	580000	20043600	563604600
22	1500	13500000	642900	15000	14500	40.00	19899100	580000	19319100	582923700
23	1500	13500000	642900	15000	14500	40.00	19174600	580000	18594600	601518300
24	1500	13500000	642900	15000	14500	40.00	18450000	580000	17870000	619388300
25	1500	13500000	642900	15000	14500	40.00	17725500	580000	17145500_	636533800
26	1500	13500000	642900	15000	14500	40.00	17001000	580000	16421000	652954800
27	1500	13500000	642900	15000	14500	40.00	16276400	580000	15696400	668651200
28	1500	13500000	642900	15000	14500	40.00	15551900	580000	14971900	683623100
29	1500	13500000	642900	15000	14500	40.00	14827400	580000	14247400	697870500
30	1500	13500000	642900	15000	14500		14102800	580000_	13522800_	711393300
TOT L I F	92500 FETIME A	832500000 Verage increas	39643500 SE (DECREASE)	925000 IN UNIT OPERAT	894000 ING COST		747153300	35760000	711393300	
		DOLLARS	PER TON OF C	OAL BURNED			18.85	0.91	17.94	
		MILLS F	PER KILOWATT-H	OUR			8.08	0.39	7.69	
		CENTS F	PER MILLION BT	U HEAT INPUT			89.75	4.30	85.45	
		DOLLARS	PER TON OF S	ULFUR REMOVED			807.73	38.66	769.07	
				TIAL YEAR+ DOL			309321200	16207400	293113800	
LEV	/ELIZED				T EQUIVALENT TO	DISCOUNTED PRO				
			PER TON OF C				17.22	0.90	16.32	
			PER KILOWATT-H				7.38	0.39	6.99	
			ER MILLION BT				82.00	4.30	77.70	
		DOLLARS	PER TON OF S	ULFUR REMOVED			738.06	38.67	699.39	

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TABLE A-38. CITRATE PROCESS

Summary of estimated capital investment $^{\mathrm{a}}$

(1000-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (unloading conveyor, elevator conveyor,		
pneumatic conveyor, feed storage bins) Feed preparation (feeders, conveyor, tank, agitator, and	1,230,000	2.2
pumps)	200,000	0.4
Gas handling (common feed plenum and booster fans, gas		
ducts and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack)	6,408,000	11.4
SO, absorption (four packed tower absorbers including	0,400,000	11.4
presaturators and entrainment separators, strippers,		
compressor, tanks, agitators, and pumps) Stack gas reheat (four indirect steam reheaters)	18,733,000	33.5
Chloride purge (feeder, tank, agitator, and pumps)	1,875,000 140,000	3.3
SO ₂ reduction (reactor tanks, aging tank, agitators, and	140,000	0.2
.centrifugal pumps)	1,623,000	2.9
S separation and removal (flotation tanks, rotary drum		
filters, pumps, slurry tank, heat exchanger, settling tank, heaters, flash drum, and compressor)	/ O/E 000	
S storage and shipping (S receiving pit, heaters, S pump,	4,045,000	7.2
and storage tank)	1,177,000	2.1
Sulfate purge (coolers, agitators, centrifuge, tanks,	, ,	
pumps, and refrigeration)	1,577,000	2.8
H ₂ S generation (battery limit plant) H ₂ generation (battery limit plant)	8,406,000	15.0
2 generation (bactery times pront)	7,473,000	13.3
Subtotal	52,887,000	94.3
Services, utilities, and miscellaneous	3,173,000	_5.7
Total direct investment	56,060,000	100.0
Indirect Investment		
Engineering design and supervision	4,132,000	7.4
Architect and engineering contractor	1,033,000	1.8
Construction expense	7,068,000	12.6
Contractor fees	2,048,000	_3.7
Total indirect investment	14,281,000	25.5
Contingency	14,068,000	25.1
Total fixed investment	84,409,000	150.6
Other Capital Charges		
Allowance for startup and modifications	9 (/) 000	
Interest during construction	8,441,000 10,129,000	15.1 18.0
Total depreciable investment	102,979,000	183,7
Land	45,000	0.1
Working capital	3,565,000	6.4
Total capital investment		
Total capital investment	106,589,000	190.2

Basis

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-39. CITRATE PROCESS

SUICIARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS $^{\mathbf{a}}$

(1000-MW new coal-fired power unit, 3.5% S in coal; 1.2 lb SO₂/MBtu heat input allowable emission)

		nual ntity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Raw materials					
Line	5.5	40 tons	42.00/ton	232,700	0.65
Soda ash		70 tons	90.00/ton	456,300	1.28
Citric acid		40 tons	1,340.00/ton	589,600	1.66
Natural gas	2,030,0		3.50/kf t 3	7,105,000	19.96
Catalyst	-,030,0	oo ki c	31307 112	40,600	0.11
Total raw materials cost				8,424,200	23.66
Conversion costs					
Operating labor and supervision	83,1	00 man-hr	12.50/man-hr	1,038,800	2.92
Utilities	•				
Steam	2,002,7	00 MBtu	2.00/MBtu	4,005,400	11.26
Process water	4,818,6		0.06/kgal	289,100	0.81
Electricity	127,919,0		0.028/kWh	3,581,700	10.06
	127,717,0	OO KWII	0.020/ K#II	3,301,700	
Maintenance				2,803,000	7.87
Labor and material	17 /	50 b	17.00/man-hr	, ,	0.83
Analyses	17,4	50 man-hr	1/.00/man-nr	296,700	0.83
Total conversion costs				12,014,700	33.75
Total direct costs				20,438,900	57.41
<u>Indirect Costs</u> Capital charges Depreciation, interim replacements, and					
insurance at 6.0% of total depreciable investment				6,178,700	17.35
Average cost of capital and taxes at 8. of total capital investment	. 6%			9,166,700	25.75
Overheads				2 2/2 102	5.81
Plant, 50% of conversion costs less uti	lities			2,069,300	
Administrative, 10% of operating labor				103,900	0.29
Marketing, 10% of sales revenue				261,700	0.74
Total indirect costs				17,780,300	49.94
Gross average annual revenue require	ements			38,219,200	107.35
Byproduct Sales Revenue					
Sulfur	65 43	0 short ton	as 40.00/short ton	(2.616.800)	(7.35)
Satiat	03,44	.o anort ton	is 40.00/short ton		
Subtotal byproduct sales revenue				(2,616,800)	(7.35)
Total average annual revenue require	ements			35,602,400	100.00
	Mills/kWh	\$/ton coa burned	1 \$/MBtu heat input	\$/short ton S removed	\$/short ton S recovered
Equivalent unit revenue requirements	5.09	12.28	0.58	526.12	544.21

a. Basis

Midwest plant location, 1980 revenue requirements. Remaining life of power plant, 30 yr.

Power unit on-stream time, 7,000 hr/yr.

Coal burned, 2,900,100 tons/yr, 8,700 Btu/kWh.

Stack gas reheat to 175 F.

Stack gas relied to 175 r.

S removed, 67,670 short tons/yr.

Investment and revenue requirement for removal and disposal of flyash excluded.

Total direct investment, \$56,060,000; total depreciable investment, \$102,979,000; and total capital investment, \$106,589,000.

TABLE A-90

CITRATE PROCESS 1000 MW NEW COAL-FIRED POWER UNIT 3.5% S IN COAL, REGULATED CO. ECONOMICS

FIXED INVESTMENT: \$ 106589000

				FIXED	TWAF2 LMEM1: >	100264000				
							TOTAL			
				SULFUR	BY-PRODUCT		DP. COST			
				REMOVED	RATE,		INCLUDING		NET ANNUAL	CUMULATIVE
	ANNUAL	POWER UNIT	POWER UNIT	BY	EQUIVALENT	NET REVENUE.	REGULATED	TOTAL	INCREASE	NET INCREASE
	OPERA-	HEAT	FUEL	POLLUTION	TONS/YEAR	\$/TUN	RDI FOR	NET	(DECREASE)	(DECREASE)
	TION.		CONSUMPTION.	CONTROL			POWER	SALES	IN COST OF	IN COST OF
UNIT	KW-HR/	MILLION BTU	TONS COAL	PRUCESS,			COMPANY.	REVENUE,	POWER,	POWER,
START	KW	/YE AR	/YEAR	TONS/YEAR	SULFUR	SULFUR	\$/YEAR	\$/YEAR	\$	\$
1	7000	6090000C	2900COC	67700	65400	40.00	47385600	2616000	44769600	4476 5600
Ž	7000	60900000	2900000	67700	65400	40.00	46795200	2616000	44179200	88948800
3	7000	60900000	2900000	67700	65400	40.00	46204800	2616000	43588800	132537600
4	7000	60900000	2900000	67700	65400	40.00	45614400	2616000	42998400	175536000
5	7000	60900000	2900000	67700	65400	40-00	45024011	_2616000_	42408000_	
6	7000	60900000	2900000	67700	65400	40.00	44433600	2616000	41817600	259761600
7	7000	60900000	2900000	67700	65400	40.00	438432))	2616000	41227200	300988800
8	7000	60900000	2900000	67700	65400	40.00	43252800	2616000	4063680C	341625600
9	7000	60900000	2900000	67700	65400	40 -00	42662400	2616000	40046400	381672000
10	_7000	0000000	2900000	67700	65400	40-00	42071900_	2616000_	39455900	421127900
11	5000	43500000	2071400	48300	46700	40.00	35466300	1868000	33598300	454726200
12	5000	43500000	2071400	48300	46700	40.00	34875900	1868000	33007900	487734100
13	5000	43500000	2071400	48300	46700	40 -00	34285500	1868000	32417500	520151600
14	5000	43500000	2071400	48300	46700	40.00	33695100	1868000	31827100	551 97 8700
15	5000	43500000	2071400	48300	46700	40-00	33104700	1868000	31236700	583215600
16	3500	30450000	145000C	33800	32700	40.00	27905700	1308000	26597700	609813100
17	3500	30450000	1450000	33800	32700	40.00	27315300	1308000	26007300	635820400
18	3500	30450000	1450000	33800	32700	40.00	26724900	1308000	25416900	661237300
19	3500	30450000	1450000	33800	32700	40.00	26134500	1308000	24826500	686063800
_20	3500	30450000	1450000	33800	32700	60_00	25544122_	1338000_	24236100_	710299900
21	1500	13050000	621400	14500	14000	40.00	18550300	560000	17990300	728290200
22	1500	13050000	621400	14500	14000	40.00	179599))	560000	17399900	745690100
23	1500	13050000	621400	14500	14000	40.00	17369400	5600C0	16809400	762499500
24	1500	13050000	621400	14500	14000	40.00	16779000	560000	16219000	778718500
_25	1500	13050000	621600	14500	14000	60_00	16188600_	560000_	15628600	794347100
26	1500	13050000	621400	14500	14000	40.00	15598200	560000	15038200	809385300
27	1500	13050000	621400	14500	14000	40.00	15007800	560000	14447800	823833100
28	1500	13050000	621400	14500	14000	40.00	14417400	560000	13857400	837690500
29	1500	13050000	621400	14500	14000	40-00	13827000	560000	13267000	850 95 7500
30	1500	13050000	<u>621400</u>	14500	14000	40.00	13236600	260000_	15676600_	863634100
							44.4974444	.=	********	
	27500	1109250000	5282100C	1232500	1191000		511274100	476400C0	863634100	
611	Elluc W			IN UNIT OPERAT	INC COZI		17.35	0.00	14 25	
			S PER TON OF C				17.25	0.90	16.35	
			PER KILDWATT-H				7-15	0.38	6.77	
			PER MILLION BT				82 .15 739 .37	4.29	77.86	
0000	e cost		PER TON OF S		1 405		739.37 331089100	38.65 18571800	700.72	
				TIAL YEAR, DOL		. D. F.C. CILIN TEA			312517300	
LEV	EFITED				I EMOTATEME IS	DISCOUNTED PRO				
			PER TON CF C				16.08	0.90	15.18	
			ER FILOWATT-H				6.66	0.37	6.29	
		• • • • • •	ER MILLION BT				76.57	4.29	72.28	
		DOLLARS	PER TON OF S	ULPUK KEMUYED			689.05	38.65	650.40	

TABLE A-91. CITRATE PROCESS

SUITARY OF ESTIMATED CAPITAL INVESTMENT

(500-NW new coal-fired power unit, 3.5% S in coal; 90% SO₂ removal)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (unloading conveyor, elevator conveyor,		
pneumatic conveyor, feed storage bins)	845,000	2.2
Feed preparation (feeders, conveyor, tank, agitator, and pumps)	143,000	0.4
Gas handling (common feed plenum and booster fans, gas		
ducts and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack)	4,093,000	10.7
odeta and dampets from absorber to treated and state, So ₂ absorption (four packed tower absorbers including presaturators and entrainment separators, strippers,	4,033,000	1017
compressor, tanks, agitators, and pumps)	12,285,000	31.9
Stack gas reheat (four indirect steam reheaters)	1,283,000	3.3
Chloride purge (feeder, tank, agitator, and pumps)	97,000	0.3
SO ₂ reduction (reactor tanks, aging tank, agitators, and	1,188,000	3.1
centrifugal pumps) s separation and removal (flotation tanks, rotary drum	1,100,000	3.1
filters, pumps, slurry tank, heat exchanger, settling		
tank, heaters, flash drum, and compressor)	2,930,000	7.6
S storage and shipping (S receiving pit, heaters, S pump,		
and storage tank)	839,000	2.2
Sulfate purge (coolers, agitators, centrifuge, tanks, pumps, and refrigeration)	1 000 000	
In Sign generation (battery limit plant)	1,089,000 6,285,000	2.8 16.4
2 generation (battery limit plant)	5,133,000	13.4
2	3,133,000	
Subtotal	36,210,000	94.3
Services, utilities, and miscellaneous	2,173,000	5.7
Total direct investment	38,383,000	100.0
Indirect Investment		
Engineering design and supervision	3,463,000	9.0
Architect and engineering contractor	866,000	2.3
Construction expense	5,161,000	13.4
Contractor fees	1,535,000	_4.0
Total indirect investment	11,025,000	28.7
Contingency	9,881,000	25.7
Total fixed investment	59,289,000	154.4
Other Capital Charges		
111		
Allowance for startup and modifications Interest during construction	5,929,000 7,115,000	15.4 18.6
Total depreciable investment	72,333,000	188.4
Land	39,000	0.1
Working capital	2,252,000	5.9
Total capital investment	74,624,000	194.4

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by indirect steam reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyash removal and disposal excluded; FGD process investment

estimate begins with common feed plenum downstream of the ESP. Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-92. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS $^{\mathbf{a}}$

(500-MW new coal-fired power unit, 3.5% S in coal; 90% SO₂ removal)

		nual ntity	Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Naw materials					
Lime	3,	260 tons	42.00/ton	136,900	0.57
Soda ash	2,	990 tons	90.00/ton	269,100	1.13
Citric acid		259 tons	1,340.00/con	347,100	1.46
Natural gas	1,200,	000 kft*	3.50/kft ³	4,200,000	17.64
Catalyst				23,900	0.10
Total raw materials cost				4,977,000	20.90
Conversion costs					
Operating labor and supervision	67,	920 man-hr	12.50/man-hr	849,000	3.57
Utilities					
Steam	1,111.	900 MBtu	2.00/MBtu	2,223,800	9.33
Process water		000 kgal	0.06/kga1	168,700	0.71
		000 kWh	0.029/kWh	1,989,800	8.36
Electricity	00,013,		3	_,,,,,,,,	J.50
Maintenance				2,303,000	9.67
Labor and material Analyses	10,	600 man-hr	17.00/man-hr	180,200	0.76
Total conversion costs				7,714,500	32.40
Total direct costs				12,691,500	53.30
Indirect Costs					
Capital charges Depreciation, interim replacements, and insurance at 6.0% of total depreciable				/ 2/0 000	10.00
investment Average cost of capital and taxes at 8.	6%			4,340,000	18.23
of total capital investment Overheads				6,417,700	26.94
Plant, 50% of conversion costs less uti	lities			1,666,100	7.00
Administrative, 10% of operating labor				84,900	0.36
Marketing, 10% of sales revenue				154,200	0.65
Total indirect costs				12,662,900	53.18
Gross average annual revenue require	ements			25,354,400	106.48
Byproduct Sales Revenue					
	20.51		/0.00/shaws 5:-	(1.5/2.000)	// /^
Sulfur	38,55	50 short tons	40.00/short ton	(1,542,000)	(6.48)
Subtotal byproduct sales revenue				(1,542,000)	(6.48)
Total average annual revenue require	ements			23,812,400	100.00
	Mills/kWh	\$/ton coa: burned	l \$/MBtu heat input	\$/short ton S removed	\$/short to S recovere
Equivalent unit revenue requirements					
EUULVAIENT unit revenue reguirements	6.80	15.87	0.76	598.30	617.70

a. Basis

asis
Midwest plant location, 1980 revenue requirements.
Remaining life of power plant, 30 yr.
Power unit on-stream time, 7,000 hr/yr.
Coal burned, 1,500,100 tons/yr, 9,000 Btu/kWh.
Stack gas reheat to 175°F.
S removed, 39,800 short tons/yr.
Investment and revenue requirement for removal and disposal of flyash excluded.
Total direct investment, \$38,383,000; total depreciable investment, \$72,333,000; and total capital investment, \$74,624,000.

FIXED INVESTMENT: \$

TABLE A-94. CITRATE PROCESS

SUMMARY OF ESTIMATED CAPITAL INVESTMENT

(500-MW existing oil-fired power unit, 2.5% S in oil; 0.8 lb SO₂/MBtu heat input allowable emission)

	Investment, \$	% of total direct investment
Direct Investment		
Materials handling (pneumatic conveyor, feed storage bins)	230,000	0.9
Feed preparation (feeders, conveyor, tank, agitator, and pumps)	76,000	0.3
Gas handling (common feed plenum and booster fans, gas		
ducts and dampers from plenum to absorber, exhaust gas ducts and dampers from absorber to reheater and stack)	3,656,000	13.7
SO ₂ absorption (four packed tower absorbers including		•
presaturators and entrainment separators, tanks, agitators, and pumps)	10,865,000	40.6
Stack gas reheat (four direct oil reheaters)	726,000	2.7
SO, reduction (reactor tanks, aging tank, agitators, and		
centrifugal pumps)	678,000	2.5
S separation and removal (flotation tanks, rotary drum filters, pumps, slurry tank, heat exchanger, settling		
tank, heaters, flash drum, and compressor)	1,642,000	6.1
S storage and shipping (S receiving pit, heaters, S pump,		
and storage tank)	456,000	1.7
Sulfate purge (coolers, agitators, centrifuge, tanks, pumps, and refrigeration)	561,000	2.1
H ₂ S generation (battery limit plant)	3,728,000	13.9
H ₂ generation (battery limit plant)	2,616,000	9.8
Subtotal	25,234,000	94.3
Services, utilities, and miscellaneous	1,514,000	5.7
Total direct investment	26,748,000	100.0
Indirect Investment		
Engineering design and supervision	2,529,000	9.5
Architect and engineering contractor	632,000	2.4
Construction expense	3,825,000	14.3
Contractor fees	1,167,000	4.4
Total indirect investment	8,153,000	30.6
Contingency	6,980,000	26.0
Total fixed investment	41,881,000	156.6
Other Capital Charges		
Allowance for startup and modifications Interest during construction	4,188,000 5,026,000	15.6 18.8
Total depreciable investment	51,095,000	191.0
Land	39,000	0.1
Working capital	1,308,000	_ <u>5.8</u>

Midwest plant location represents project beginning mid-1977, ending mid-1980. Average cost basis for scaling, mid-1979.

Stack gas reheat to 175°F by direct oil reheat.

Minimum in-process storage; only pumps are spared.

Investment requirements for flyash removal and disposal excluded; FGD process investment estimate begins with common feed plenum downstream of the ESP.

Construction labor shortages with accompanying overtime pay incentive not considered.

TABLE A-95. CITRATE PROCESS

SUMMARY OF AVERAGE ANNUAL REVENUE REQUIREMENTS -

REGULATED UTILITY ECONOMICS

(500-MW existing oil-fired power unit, 2.5% S in oil; 0.8 lb SO₂/MBtu heat input allowable emission)

	Annu quant		Unit cost, \$	Total annual cost, \$	% of average annual revenue requirements
Direct Costs					
Raw materials			00.00/	104,400	0.65
Soda ash) tons	90.00/ton	134,000	0.83
Citric acid) tons	1,340.00/ton 3.50/kft ³	1,619,800	10.07
Natural gas	462,80) kft ⁻	3.30/ KI C	9,300	0.06
Catalyst					
Total raw materials cost				1,867,500	11.61
Conversion costs					F 01
Operating labor and supervision	64,52	5 man-hr	12.50/man-hr	806,600	5.01
Utilities					6.65
Fuel oil (No. 6)	2,676,60	0 gal	0.40/gal	1,070,600	2.99
Steam	240,71		2.00/MBtu	481,400	
Process water	1,178,90	0 kgal	0.06/kgal	70,700	0.44
Electricity	48,688,00	0 kWh	0.029/kWh	1,412,000	8.78
Maintenance					0.07
Labor and material			_	1,604,900	9.97
Analyses	10,10	0 man-hr	17.00/man-hr	171,700	1.07
Total conversion costs				5,617,900	34.92
Total direct costs				7,485,400	46.52
Capital charges Depreciation, interim replacements, an insurance at 6.4% of total depreciabl				2 270 100	20. 22
investment				3,270,100	20.32
Average cost of capital and taxes at 8 of total capital investment	.6%			4,510,000	28.02
Overheads				1,291,600	8.03
Plant, 50% of conversion costs less ut				80,700	0.50
Administrative, 10% of operating labor				60,700	0.38
Marketing, 10% of sales revenue					
Total indirect costs				9,213,100	57,25
Gross average annual revenue requir	ements			16,698,500	103.77
Pursuaduat Calon Payanua					
Byproduct Sales Revenue			10.0011	((0(000)	15 771
Sulfur	15,170) short to	s 40.00/short ton	(606,800)	(3.77)
Subtotal byproduct sales revenue				16,091,700	100.00
Total average annual revenue requir	rements				
	Mills/kWh	\$/bbl oi burned	1 \$/MBtu heat input	\$/short ton S removed	\$/short to S recoveie
Equivalent unit revenue requirements	4.60	3.02	0.50	1,042.88	1,060.76
	/ 6A		0.50	1.047.88	1.060.76

Investment and revenue requirement for removal and disposal of flyash excluded. Total direct investment, \$26,748,000; total depreciable investment, \$51,095,000; and total capital investment, \$52,442,000.

Asis
Midwest plant location, 1980 revenue requirements.
Remaining life of power plant, 25 yr.
Power unit on-stream time, 7,000 hr/yr.
Oil burned, 5,324,100 bbl/yr, 9,200 Btu/kWh.
Stack gas reheat to 175°F.
S removed, 15,430 short tons/yr.
Investment and revenue requirement for removed and

TABLE A-96

CITRATE PROCESS 500 MW EXISTING OIL-FIRED POWER UNIT 2.5% S IN OIL REGULATED CO. ECONOMICS

				FIXED	INVESTMENT: \$	52442000				
AFTER	ANNUAL OPERA- TION: KW-HR/ KW	POWER UNIT HEAT REQUIREMENT, MILLION BTU /YEAR	POWER UNIT FUEL CONSUMPTION. BARRELS OIL /YEAR	SULFUR REMOVED BY POLLUTION CONTROL PROCESS. TONS/YEAR	BY-PRODUCT RATE, EQUIVALENT TONS/YEAR SULFUR	NET REVENUE: \$/TON SULFUR	TOTAL OP. COST INCLUDING REGULATED ROI FOR POWER COMPANY+ \$/YEAR	TOTAL NET SALES REVENUE, \$/YEAR	NET ANNUAL INCREASE (DECREASE) IN COST OF POWER, \$	CUMULATIVE NET INCREASE (DECREASE) IN COST OF POWER+ \$
1 2 3 4					***************************************					
2	7000	32200000	5324100	15400	15200	40.00	21207900	608000	20599900	20599900
7	7000	32200000	5324100	15400	15200	40.00	20856400	608000	20248400	40848300
8	7000	32200000	5324100	15400	15200	40.00	20504900	608000	19896900	60745200
9	7000	32200000	5324100	15400	15200	40.00	20153300	608000	19545300	80290500
_10	7000	32200000	5324100	15400	15200	40.00	19801800	608000	19193800	99484300
11	5000	23000000	3802900	11000	10800	40.00	17248700	432000	16816700	116301000
12	5000	23000000	3802900	11000	10800	40.00	16897100	432000	16465100	132766100
13	5000	23000000	3802900	11000	10800	40.00	16545600	432000	16113600	148879700
14	5000	23000000	3802900	11000	10800	40.00	16194100	432000	15762100	164641800
15	5000	23000000	3802900	11000	10800	40.00	15842500	432000	15410500_	180052300
16	3500	16100000	2662000	7700	7600	40.00	13775600	304000	13471600	193523900
17	3500	16100000	2662000	7700	7600	40.00	13424100	304000	13120100	206644000
18	3500	16100000	2662000	7700	7600	40.00	13072500	304000	12768500	219412500
19	3500	16100000	2662000	7700	7600	40.00	12721000	304000	12417000	231829500
-50	3500	16198988	2662000	7700		49.00	12369500_	304000_	12065500_	243895000
21	1500	6900000	1140900	3300	3300	40.00	9560200	132000	9428200	253323200
55	1500	6900000	1140900	3300	3300	40.00	9208700	132000	9076700	262399900
23	1500	6900000	1140900	3300	3300	40.00	8857200	132000	8725200	271125100
24	1500	6900000	1140900	3300	3300	40.00	8505600	132000	8373600	279498700 287520800
-25 26	1500 1500	6900000	<u>1140900</u>	<u>3300</u> 3300	<u>3300</u> _	<u>-\$8.00</u>	8154100 7802600	<u>132000</u> 132000	<u>8022100</u> 7670600	295191400
27	1500	6900000	1140900	3300	3300	40.00	7451000	132000	7319000	302510400
28	1500	6900000	1140900	3300	3300	40.00	7099500	132000	6967500	30947790C
29	1500	6900000	1140900	3300	3300	40.00	6748000	132000	6616000	316093900
_30	1500	6900000	1140900	3300	3300	40.00	6396400	132000	6264400	322358300
TOT	92500	425500000	70354000 SE (DECREASE)	203500	201000		330398300	8040000	322358300	
		DOLLAR	S PER BARREL O	F OIL BURNED			4.70	0.12	4.58	
		MILLS	PER KILOWATT-H	IOUR			7.14	0.17	6.97	
		CENTS	PER MILLION BT	U HEAT INPUT			77.65	1.89	75.76	
		DOLLAR	S PER TON OF S	ULFUR REMOVED			1623.58	39.51	1584.07	
PROCE	SS COST	DISCOUNTED AT	11.6% TO INI	TIAL YEAR, DOL	LARS		135047900	3637700	131410200	
LE	VELIZED				T EQUIVALENT TO	DISCOUNTED PRO				
			S_PER_BARREL_O				4.24	0.12	4.12	
			PER KILOWATT-H				6.44	0.17	6.27	
			PER MILLION BT				70.04	1.88	68.16	
		DOLLAR	S PER TON OF S	ULPUR REMOVED			1464.73	39.46	1425.27	

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15. SUPPLEMENTARY NOTES IERL-RTP project officer is Charles J. Chatlynne, Mail Drop 61, 919/541-2915.

16. ABSTRACT The report gives results of a detailed comparative technical and economic evaluation of limestone slurry, generic double alkali, and citrate flue gas desulfurization (FGD) processes, assuming proven technology and using representative power plant, process design, and economic premises. For each process, economic projections were made for a base case (500 MW, 3.5% sulfur coal, new unit) and case varjations in power unit size, fuel type, sulfur in fuel, new and existing power units, waste slurry ponding and filter cake trucking, and SO2 removal (1.2 lb SO2 allowable emission per million Btu heat input vs 90%). Depending on unit size and status, fuel type and sulfur content, solids disposal method, and overall project scope, ranges in estimated capital costs in 1979 dollars are \$71 to \$127/kW for limestone slurry. \$80 to \$130/kW for generic double alkali, and \$105 to \$194/kW for citrate (recovery process). Results can be scaled or altered to reflect other site-specific conditions. Capital investment, annual revenue requirements (7000 hr/yr), and lifetime revenue requirements over a 30-year declining operating profile were estimated for the base case and each variation. Investment costs were projected to mid-1979; annual revenue requirements were calculated in projected mid-1980 dollars. Effects of variations in various cost parameters were studied.

ı7	KEY WORDS AND	D DOCUMENT ANALYSIS			
a. DES	SCRIPTORS	b. IDENTIFIERS/OPEN ENDED TERMS	c. COSATI Field/Group		
Pollution	ion Sulfur Oxides Pollution Control		13B	07B	
Evaluation	Limestone	Stationary Sources	14B	08G	
Coal	Slurries	Double Alkali Process	21D	11G	
Combustion	Citrates	Trucking	21B	07C	
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