United States Environmental Protection Agency Motor Vehicle Emission (a), 2565 Plymouth Rd. Ann Arbor, Michigan 48105

Air



## Light Duty Vehicle Driveability Investigation

# LIGHT DUTY VEHICLE DRIVEABILITY INVESTIGATION

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#### ABSTRACT

This report describes the results of an automobile driveability, emission, fuel economy and performance testing program conducted for the U.S. Environmental Protection Agency. A total of twenty-two 1977 and 1978 model vehicles were subjected to a series of tests when adjusted to the manufacturers' recommended settings and when adjusted to simulate maladjustments found on in-use vehicles in an earlier EPA Restorative Maintenance Evaluation Project. The CRC driveability tests were performed on a weather controlled large roll chassis dynamometer at 16°C and the emissions and fuel economy tests were conducted according to the 1975 Federal Test Procedure, except that evaporative emissions tests were not conducted.

#### **FOREWORD**

This project was initiated by the Characterization and Applications Branch, Division of Emission Control Technology, Environmental Protection Agency, 2565 Plymouth Road, Ann Arbor, Michigan, 48105. The engineering effort on which this report is based was accomplished by the Automotive Laboratory of Suntech, Inc., P.O. Box 1135, Marcus Hook, Pennsylvania. The project was authorized by Contract 68-03-2607 and began on September 28, 1977 and was completed October 5, 1978.

The Suntech Project Leader was Dr. Robert E. Burtner, who supervised all of the work in the Marcus Hook Laboratory. Mr. Harry A. Toulmin, Jr. was Project Manager.

The Project Officer for this project was Mr. Andrew W. Kaupert, of the Characterization and Applications Branch, Environmental Protection Agency.

#### TABLE OF CONTENTS

				Page
ABSTR	RACT			iii
FOREW	IORD			iv
LIST	OF 1	FIGUR	ES	vii
LIST	OF ?	TABLE	S	viii
SUMMA	<b>LRY</b>			ix
	ı.	1	ntroduction	1
	II.	E	quipment, Instruments, Preparations and Procedures	2
		A B	•	2
		C	•	
		D	•	5
		-	. Driveability Test Procedure	5 5 6
			. Emission and Fuel Economy Tests	8
			. Acceleration Procedure	9
	III	. D	escription of Test Program	10
		А	. Sequence of Testing	10
			. Baseline Vehicle Tests	10
		С	. Maladjusted Vehicle Tests ·	17
			1. Effect of Disconnecting EGR	17
			<ol> <li>Effect of Rich Idle Mixture</li> </ol>	19
			<ol> <li>Effect of Richer Choke Settings</li> </ol>	21
			4. Effect of Advancing Spark	21
			5. Effect of Increased Idle RPM	24
			6. Turbocharged Buick Maladjustments	24
			7. Three-Way Catalysts Maladjustments	26
			8. Effect of Multiple Maladjustments	26
	IV.	R	ecommendations	30
List	of	Refer	ences	31
Apper	ndix	A		
	Eng	ine S	ettings Used in Baseline Tests a from Vehicles on Baseline and Maladjustment Tests	32 34
	+63	- val	d Tiom tonicates our massacratic and maradiasement issue	- '

## TABLE OF CONTENTS (Continued)

	Page
Appendix B	
Driveability Test Procedure Description of Emission Lab Instrumentation	57 65
Appendix C	
Repeatability Data on Emission and Fuel Economy Test Data for Individual Runs on Each Vehicle	66 68
Appendix D	
Plots of Driveability vs. Acceleration Time, FTP Fuel Consumption, HFET Fuel Consumption and HC, CO and NOx Emissions on an Absolute Basis	90
Plots of Driveability vs. Acceleration Time, FTP Fuel Consumption, HFET Fuel Consumption and HC, CO and NOx Emissions on a Normalized Basis	258

## LIST OF FIGURES

Figure		Page
1. Diagram	of Testing Sequences for Vehicle Tests	11
2. Distribu	tion of Driveability Demerits for all Cars Tested	13
_	on of Driveability Demerits with Results of ests on 1973, 1975 and 1977 Model Vehicles	14

## LIST OF TABLES

Table		Page
1	Driveability, Performance, Emission and Fuel Economy with Baseline Adjustments	12
2	Stalls During Driveability Runs	16
3	Effect of Disconnecting EGR on Vehicle Driveability, Emissions, Fuel Economy and Acceleration Time	18
4	Effect of Rich Idle on Vehicle Driveability, Emissions, Fuel Economy and Acceleration Time	20
5	Effect of Rich Choke Setting on Vehicle Driveability, Emissions, Fuel Economy and Acceleration Time	22
6	Effect of Advancing Spark on Vehicle Driveability, Emissions, Fuel Economy and Acceleration Time	23
7	Effect of Increased Idle RPM on Vehicle Driveability, Emissions, Fuel Economy and Acceleration Time	25
8	Effect of Multiple Maladjustments of Vehicle Driveability, Emissions, Fuel Economy and Acceleration Time	27
9	Summary of "Fleet Average" Effects of Maladjustments on Vehicle Driveability, Emissions, Fuel Economy and Acceleration Time	29

#### SUMMARY

Twenty-two 1977 and 1978 passenger cars selected on the basis of high sales volume and emission control technology were used to investigate and quantify the relationship between prevalent engine maladjustments found in in-use vehicles(1)\* and their effect on vehicle driveability, exhaust emissions, fuel economy and acceleration. Each vehicle was driveability tested in accordance with the CRC Driveability Procedure(2) at 16°C and exhaust emissions and fuel economy were determined by the 1975 Federal Test Procedure. Tests were conducted on a weather-controlled large roll chassis dynamometer. Each test vehicle was tested with all engine and emission control system settings according to the manufacturers' recommendations and also additional tests were run with four sets of maladjustments which were representative of maladjustments found on in-use vehicles in the EPA Restorative Maintenance Evaluation.

There was a large variation in the driveability ratings among vehicles when adjusted to standard settings. Driveability was improved by some of the maladjustments but made worse by others. The response to a given maladjustment varied widely among cars, probably because of the differences in the calibration compromises made in the standard settings among vehicles.

From an overall fleet standpoint, disconnecting EGR improved driveability by 31%, richer choke settings improved driveability by 27%, advancing spark timing improved driveability by 11%, increasing idle rpm by 9%. The richer idle settings decreased driveability by 4%.

These maladjustments frequently caused large changes in emissions with NOx increasing 190% when EGR was disconnected, 20% when the timing was advanced and 12% when the idle rpm was increased. The rich idle increased CO by 108% and the rich choke settings increased CO by 12%. The rich idle increased HC by 48% and increasing idle rpm decreased HC by 16%. All other maladjustments made less than 10% change in emissions.

Disconnecting EGR and advancing spark timing gave a slight improvement in fuel economy and increased idle rpm reduced fuel economy. Richer idle and richer choke settings changed fuel economy less than 1%.

Advancing the spark timing was the only modification that improved the vehicle acceleration performance to the point that the change might be perceptible to the driver (5%).

The overall average of the twenty cars with multiple maladjustments, similar to those found on many of the maladjusted cars in the Restorative Maintenance Evaluation Project, showed only a very slight improvement in driveability at the expense of 142% increase in CO, 53% increase in HC and a 13% increase in NOx. These maladjustments resulted in a 2% reduction in overall fuel economy and no change in acceleration performance.

A summary of the effects of the maladjustments is shown in Table 9.

<sup>\*</sup> A number in parenthesis ( ) denotes references listed at the end of the report.

#### I. INTRODUCTION

Surveillance studies of exhaust emissions from in-use vehicles have been conducted by the U.S. Environmental Protection Agency (EPA) for a number of years. Results of these programs have indicated that a large percentage of in-use automobiles of the newest model year did not meet their exhaust emission standards when tested in the as-received condition. Because of this, EPA conducted a Restorative Maintenance Evaluation Project on low-mileage 1975, 1976 and 1977 vehicles. This program concluded that maladjustments and disablements within the emission control system were primarily responsible for the poor emission performance. It appears that an important motivation for maladjustment is the owners' desire to improve the driveability characteristics of the vehicle.

The objective of this program was to investigate and quantify the relationship between prevalent engine maladjustments and their effect on driveability. Simultaneously, emissions, acceleration performance and fuel economy were also measured.

## II EQUIPMENT, INSTRUMENTS, PREPARATIONS AND PROCEDURES

This section describes the vehicles, facilities, instrumentation, procedures and fuels utilized in this project.

#### A. Vehicle Selection and Procurement

Twenty-two 1977 and 1978 passenger cars were selected for this program. The vehicles were selected on the basis of engine sales volume and emission control technology. Sixteen of the vehicles were certified to meet the Federal emission standards and six were California models. All cars were equipped with automatic transmissions. The following cars were used on the program:

	Code*	Cali- bra- tion	Dis- place- ment <u>Liters</u>	No.	Carb. Bbls.	Catalyst
GM						
1977 Chevrolet Chevette	A	Fed.	1.6	L-4	1	Oxidizing
1977 Chevrolet Chevelle	В	Fed.	5.0	V-8	2	*11
1977 Pontiac Sunbird	С	Cal.	2.5	L-4	2	3-Way
1978 Pontiac Grand Prix	D	Fed.	4.9	V-8	2	Oxidizing
1977 Buick Skylark	E	Fed.	3.8	<b>V</b> -6	2	If
1977 Buick Century	F	Fed.	5.7	<b>V-</b> 8	2	11
1978 Buick Regal	G	Fed.	3.8	<b>V-</b> 6	4 <sup>(1)</sup>	11
1977 Oldsmobile Cutlass	H	Fed.	5.7	V-8	4	11
1977 Oldsmobile 98	I	Fed.	6.6	V-8	4	11
FORD						
1977 Ford Pinto	J	Fed.	2.3	L-4	2	Oxidizing
1977 Ford Maverick	K	Fed.	4.1	L-6	1	**
1977 Ford Maverick	L	Cal.	4.1	L-6	1	11
1977 Granada	M	Fed.	5.0	<b>V-8</b>	2	11
1977 Ford Granada	N	Cal.	5.0	V-8	2 <sup>(2)</sup>	11
1977 Ford LTD II	0	Fed.	5.8	V-8	2	***
CHRYSLER						
1977 Plymouth Volare	P	Fed.	3.7	L-6	1	Oxidizing
1977 Plymouth Volare	Q	Fed.	5.2	<b>v-</b> 8	2	11
1977 Plymouth Volare	R	Cal.	5.2	V-8	2	11
1977 Chrysler Cordoba	S	Fed.	6.6	<b>V-</b> 8	4(3)	11

		Code*		Dis- place- ment Liters	No.	Carb. Bbls.	Catalyst
AMC							
1978	AMC Concord	T	Cal.	4.2	L-6	1	Oxidizing
IMPORTS							
1978	Toyota Corolla	U	Fed.	1.6	L-4		Oxodizing
1978	Volvo 245-DL	V	Cal.	2.1	L-4	FI <sup>(4)</sup>	3-Way

<sup>\*</sup> This letter code used to identify vehicles on tables in Appendix.

- (2) Two-barrel variable venturi carburetor
- (3) "Electronic Lean Burn" emission system
- (4) Port Fuel Injection System

Most of the vehicles were leased from rental or leasing agencies or automotive dealers and three of the vehicles were from the Suntech vehicle fleet. Because of problems obtaining some of the California vehicles, three were obtained from oil and additive companies and one was on loan from the manufacturer. An attempt was made to obtain all of the vehicles with between 4,000 and 15,000 accumulated miles, but in a few cases the only vehicles available had mileage outside this limit. The following vehicles were tested at mileages outside this limit:

Ford Maverick	4.1 liter	California calibration	27,800 miles
Plymouth Volare	5.2 liter	California calibration	25,748
AMC Concord	4.2 liter	California calibration	1,985 miles
Volvo 245-DL	2.1 liter	California calibration	2,020 miles
Pontiac Sunbird	2.5 liter	California calibration	33,470 miles
Chevrolet Chevette	1.6 liter	Federal calibration	20,577 miles
Toyota Corolla	1.6 liter	Federal Calibration	3,813 miles

In our opinion the difference in mileage on these vehicles would not influence the ratings for these tests since all of the vehicles were thoroughly checked prior to test and parts, i.e., spark plugs and filters were replaced on vehicles with over 10,000 miles. (See Section B)

The mileage on each vehicle at the start of this program is shown on Table A-1 in Appendix A.

<sup>(1)</sup> Turbocharged

#### B. Car Preparation

Each test vehicle was set to the manufacturers' recommended settings before test, using the following check list:

- 1. New spark plugs were installed in all vehicles with over 10,000 miles of mileage accumulation.
- 2. The basic ignition timing and dwell (if equipped with breaker points) were set to manufacturers' specification.
  - 3. The ignition system was scope tested to check for any malfunctions.
- 4. Carburetor air and fuel filters were replaced on vehicles with more than 10,000 miles.
- 5. The carburetor idle, and fast idle speed were set to manufacturers' specification.
- 6. The idle mixture was checked and reset if necessary by the procedure specified by the vehicle manufacturer. (Idle speed drop for GM, CO or propane enrichment for Ford and Chrysler, etc.)
- 7. The automatic choke mechanism and the choke vacuum break was set to specifications.
- 8. The EGR system was carefully checked to see that it was functioning properly.
- 9. All emission system linkages, hoses, heat valves, etc. were checked for proper connections and operation.
  - 10. The oil was drained and refilled with an SE quality 10W-40 grade.
  - 11. All fluid levels and tire pressures were checked.
- 12. A vacuum gauge and tachometer was installed for use in the driveability testing.

Recommended settings were obtained from the emission decal, engine shop manuals and from the engineering departments of the vehicle manufacturers. The settings used for the baseline tests are tabulated in Table A-1, Appendix A.

Most of the tune-up settings were obtained from the emission decal and the shop manuals without difficulty; however, in some cases the information was not available from these sources or from the local automobile dealers and had to be obtained directly from the manufacturers. Some of the information on models with running changes was obtained from service bulletins from the manufacturers.

#### C. Emission System Maladjustments

After each vehicle was run with the standard (baseline) settings, it was rerun at each of four maladjustment settings. These settings, which are detailed on the data summary tables, A-2 through A-23, of Appendix A, were obtained from EPA and represented settings and disablements found on similar vehicles in their Restorative Maintenance Evaluation Project (1). In most cases single maladjustments of one item were used on three of the tests and the fourth test was run with two or more maladjustments combined.

#### D. Test Fuels

All emissions tests, with the exception of one test run on the turbo-charged Buick, were run on Indolene O, as specified in the Federal Register. Acceleration tests, except on the turbocharged Buick, were run on this same fuel.

Indolene typically has a lower 90% evaporated point than the average commercial unleaded fuel in the marketplace and, therefore, the driveability of a vehicle will be different on Indolene than on a typical fuel. Inspections on recent batches of Indolene have indicated that the 90% point is about 158°C.

In order to make the program more meaningful, a test fuel meeting the following specifications was made up for the driveability testing:

	Specification	Max. ASTM D-439 Grade C	DOE	Fuel Used
10% Evaporated	51.7 <u>+</u> 3°C	60°C	49.4°C	50.6°C
50% Evaporated	104.4 <u>+</u> 3°C	116°C	105°C	107.2°C
90% Evaporated	173.9 <u>+</u> 5°C	185°C	167.2°	170°C
RVP, KPa	62 to 76		67.6	65.5
Driveability Index*		238.5	213.3	217.5

<sup>\*</sup> Driveability Index = 10% Pt/2 + 50% Pt + 90% Pt/2

This specification provides for a fuel that is slightly higher in driveability index than the average unleaded fuel from the Department of Energy Motor Gasoline Survey, BETC/PPS 78/1, but is well below the maximum limits of ASTM Standard D-439 Specifications for Automotive Gasoline. Inspection data for the fuel used in the program is shown in the table.

A third fuel was used in the program for one of the tests on the turbocharged Buick Regal. This fuel was specified by EPA as a high octane unleaded premium type fuel to determine the effect of the use of high octane fuel on the performance of this vehicle. A comparison of this fuel with the standard driveability fuel is shown in the following table:

	Special High Octane Fuel	Standard Driveability Fuel
Research Octane No.	101.0	93.4
Motor Octane No.	90.6	84.7
RVP, KPa	51.7	65.5
10% Evaporated, °C	67	51
50% Evaporated, °C	115	107
90% Evaporated, C	149	170
Driveability Index	223	217.5

## E. Driveability Test Procedure

The driveability quality of each car was evaluated by testing the vehicle using the Coordinating Research Council Cold Start Driveability Test Procedure on a controlled weather large roll chassis dynamometer. This cycle simulates a 5.8 kilometer (3.6 mile) trip after starting from a cold soak at 15.6°C (60°F). The cycle consists of a series of full and part throttle accelerations performed at measured distances. Any vehicle malfunction such as a stall, back fire, hesitation, stumble or surge is evaluated by the driver and rated as to severity. These ratings are then translated into demerit ratings and combined into total demerits for the run. A detailed description of the test procedure can be found in Appendix B.

Before each driveability run, each vehicle is placed on the chassis dynamometer and driven for ten minutes at 97 kph in order to obtain equilibrium engine temperatures. The vehicle is then allowed to soak at the control temperature for three hours with the hood up and the room temperature maintained at 15.6°C and the cooling air velocity at 22 kph. Details of the cool gown procedure can be found in Appendix B.

At the beginning of the program, each of the two test drivers made one of the driveability tests on each car. Since driveability rating is very subjective, there is always some difference in driveability rating, even among trained raters (2) This problem has been encountered on several CRC driveability programs.

After the first eight cars were tested, it was decided to conduct all of the driveability runs on a car with one driver, since this would improve the repeatability of ratings and the objective of the program was to compare the effect of vehicle adjustment on driveability rather than to compare driveability differences among cars. The last fourteen cars to be tested used this

procedure. The repeatability of the driveability test was improved from a standard deviation of 22.2 demerits for the first eight cars, using two drivers per car to 8.5 demerits for the second group of fourteen cars using the same driver for all of the runs on the car. The repeatability data was obtained, using the formula given below modified for duplicate tests for each car.

Std. Dev. 
$$=\sqrt{\frac{1}{N-1}\sum_{i+1}^{N} \left(\frac{\Delta}{2}\right)^2}$$

Where: 

= Range between duplicate determinations

N = Number of duplicate determinations

Detailed driveability data on each vehicle is shown in Table C-2 through C-23 in Appendix C.

Up to 1968 when the CRC driveability procedure was developed, most of the driveability or "warm-up" tests reported in the literature were conducted to compare fuels of different distillation characteristics and were conducted using a road load and acceleration cycle on a chassis dynamometer. The CRC procedure was developed to incorporate more vehicle maneuvers so that it could be used to evaluate both vehicles and fuels.

In 1968-1970 Ethyl Corporation used this procedure to run an extensive driveability program for the Air Pollution Research Advisory Committee of CRC. A fleet of twelve 1968, '69 and '70 model cars were driveability tested on the Ethyl large roll chassis dynamometer (which is very similar in all respects to the one used at Suntech) and then repeated some of the testing on the test track with an overnight soak before each run.

This correlation program, which seems to be the only one published in the literature, directly comparing driveability on the road and chassis dynamometers, compared the demerits obtained on two fuels in four test cars tested at 7°C on the dynamometer and at 4 to 10°C on the test track. The results were as follows:

## Average Demerits From Duplicate Runs

	Fue	el 1	Fue	e1 7
	Dyn.	Road	Dyn.	Road
'69 Ford	57	37	186	155
'69 Rambler	134	53	202	137
'69 01ds	47	35	141	74
'69 Valiant	42	25	95	48
AVERAGE	70	38	156	104

When the demerits from the individual malfunctions were compared, the correlation was good for stalls, idle roughness and backfire, but "seat of pants" feel of vehicle movement (surge, hesitation and stumble) are magnified by the dynamometer. This CRC project concluded that the chassis dynamometer is a satisfactory method of making driveability evaluations but is more severe than road testing. The relative fuel rankings correlated fairly well between the two tests. Details of this study can be found in the CRC report. (3)

#### F. Emission and Fuel Economy Tests

The emission and fuel economy tests were conducted in accordance with the 1975 FTP procedure as specified in the Federal Register, Vol. 41, No. 177, September 10, 1976, except that the tests were run on a large single roll (1280 mm diameter) dynamometer and the room temperature was controlled to 22°C+2 to promote repeatability of runs. Evaporative emission tests were not run but the evaporative emission control system was stabilized before each soak by running an LA-4 test on Indolene immediately before each soak period. Details of the CVS test equipment and instrumentation is given in Appendix B-2. Vehicle inertia weight and horsepower settings were the same as used in the official EPA vehicle certification tests for the engine family.

The repeatability of the emission and fuel economy tests was calculated from the duplicate tests on each car. The coefficient of variation (CV) was calculated by standard statistical procedures although our method of assessing the standard deviation (S) may be more severe than at some other laboratories. Since only duplicate emissions results are normally obtained for each car modification,

we calculated S equal to 
$$\frac{1}{N-1}$$
  $2\left(\frac{\Delta}{2}\right)^2$  five times for each car.

( $\triangle$  is simply the difference between duplicate tests, and  $\frac{\triangle}{2}$  is the difference from the mean.)

This S value reduces to 
$$\sqrt{\frac{\Delta}{2}}$$
 since N equals two and there are two  $\frac{\Delta}{2}$  values.

Thus the standard deviation for each car is 
$$S = \sqrt{\frac{S_1^2 + S_2^2 + S_3^2 + S_4^2 + S_5^2}{5}}$$
 for 10 testings.

The mean,  $\overline{X}$ , was simply obtained by averaging all the individual car runs and disregarding modification differences.

The following summary averages the coefficient of variation, (CV) (standard deviation, S, divided by the mean value, X) for the cars tested:

Emission Test Data	CV x 100%	Range, %
FTP Fuel Economy	1.9	0.5 to 5.3
Highway Fuel Economy	2.4	1.2 to 4.2
НС	9.5	4.0 to 20.6
со	12.7	2.4 to 25.3
NOx	6.5	2.5 to 11.4

Detailed repeatability data on each vehicle is shown in Table C-1 in Appendix C.

#### G. Acceleration Procedure

The performance of each car was measured by determining the time for a 16.1 to 96.6 kph (10 to 60 mph) acceleration on the chassis dynamometer. The 16.1 kph starting speed was used to prevent wheel spin on the dynamometer rolls. The acceleration time was the average of six runs at each test condition. The dynamometer load and inertia settings were the same as used for the driveability tests of the car.

#### III. DESCRIPTION OF TEST PROGRAM

#### A. Sequence of Testing

In order to make maximum use of the chassis dynamometer facilities, the program was laid out so that a block of four cars would be run during each test period of approximately five weeks. The program layout is shown in Figure 1 for a typical week's operation.

Since each vehicle was tested by running duplicate runs at each of five adjustment conditions, baseline plus four maladjustments, each block of four cars could be completed in five weeks if no breakdowns of cars or equipment were encountered.

#### B. Baseline Vehicle Tests

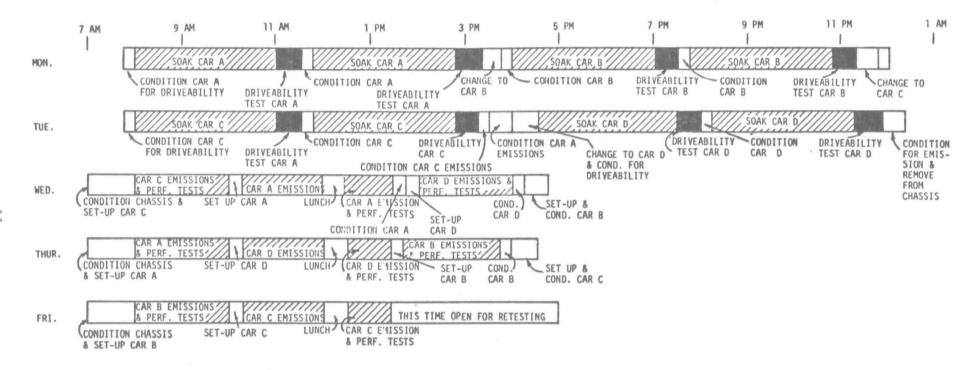
Table 1 shows the results of the baseline tests (tests with all adjustments to manufacturers recommended setting). Figure 2 shows the distribution of the driveability demerits. The driveability varied considerably from a low of 12 demerits to a high of 269 demerits. (The lower the number of demerits the better the driveability.) Such variability is not unusual and similar results have been found in tests conducted on the road by CRC.

Figure 3 is taken from a recent CRC report (5) and shows a comparison of the average demeritalevel of three fleets of cars tested by CRC in three recent programs (4)(5)(6) plotted against the fuel volatility as expressed as the driveability index (in Fahrenheit units). The fuel used for this EPA program had a driveability index of 456 (217.5 in Celsius units) and the average demerit rating of the 22 cars is plotted against this driveability index. The plot indicates that the average car from this program has better driveability than the average 1973 and 1975 models tested by CRC but were poorer than the CRC 1977 models.

The difference between the 1977 models tested by CRC and those run on this program could have been due to differences in driver ratings, differences in the severity of ratings on the chassis dynamometer and the road, and the selection of the cars tested. It is well known that there are differences between expert driver ratings and CRC makes a statistical analysis of ratings from each driver used on each program and corrects the driver bias out.

As discussed in the previous section, the program conducted by Ethyl Corporation comparing driveability ratings on the chassis dynamometer and test track has indicated that the chassis ratings are slightly more severe than on the road although both cars and fuels were lined up in the same order. Since the purpose of this program was to determine differences in driveability due to changes in the car adjustment, the fact that the chassis dynamometer procedure may have been slightly more severe should make little difference in the relative ratings.

#### DRIVEABILITY AND EMISSIONS TESTING



I

TABLE 1

DRIVEABILITY, PERFORMANCE, EMISSION AND FUEL ECONOMY

WITH BASELINE ADJUSTMENTS

Drive- Accel.	Emissions		
-1-414+ m4 NO	00 170-	Urban	Highway
ability Time HC <u>Demerits Sec. gm/km</u>	CO NOx gm/km gm/km	Liter/ 100 km	Liter/ 100 km
Benefits dec. gm/km	gm/ Km gm/ Km	100 KIII	100 Km
Volare 318-C 269 11.8 0.29	2.06 1.17	22.25	15.19
Volare 318-F 244 10.1 0.63	7.23 0.89	18.62	13.24
Volare 225-F 238 14.4 0.83	6.76 1.12	14.40	11.10
LTD II 351W-F 211 10.4 0.79	6.42 1.50	17.07	12.25
Cordoba 400-F 185 9.7 0.42	3.63 1.07	20.70	13.63
Maverick 250-F 160 12.9 1.09	8.02 0.90	13.90	10.60
Pinto 140-F 154 14.0 0.54	9.48 0.90	12.70	9.60
Granada 302-C 150 11.4 0.46	3.04 0.70	19.30	13.50
Cutlass 350-F 127 10.1 0.47	4.73 1.25	16.12	11.87
Concord 258-C 121 17.4 0.19	3.46 0.69	17.83	15.00
Sunbird 151-C 117 14.9 0.50	5.44 1.21	10.88	8.32
Chevelle 305-F 117 10.6 0.63	8.16 1.69	16.08	12.60
Maverick 250-C 115 15.5 0.55	7.37 0.80	16.18	12.94
Chevette 98-F 109 14.2 0.63	9.77 1.12	9.89	7.26
Skylark 231-F 105 14.7 0.46	11.36 1.03	15.17	10.36
Century 350-F 105 11.9 0.51	6.55 1.04	16.33	11.88
Buick 231T-F* 91 10.1 0.50	6.15 0.78	14.51	11.21
Oldsmobile 403-F 84 9.7 0.51	4.65 1.59	16.49	12.06
Granada 302-F 83 11.1 1.14	4.62 1.27	16.05	12.35
Grand Prix 301-F 55 9.8 0.72	5.72 1.03	14.30	10.19
Volvo 130-C 17 14.0 0.20	2.04 0.42	12.58	9.27
Toyota 97-F 12 13.0 0.45	6.19 1.15	10.65	8.52

<sup>\*</sup> Turbocharged

FIGURE 2

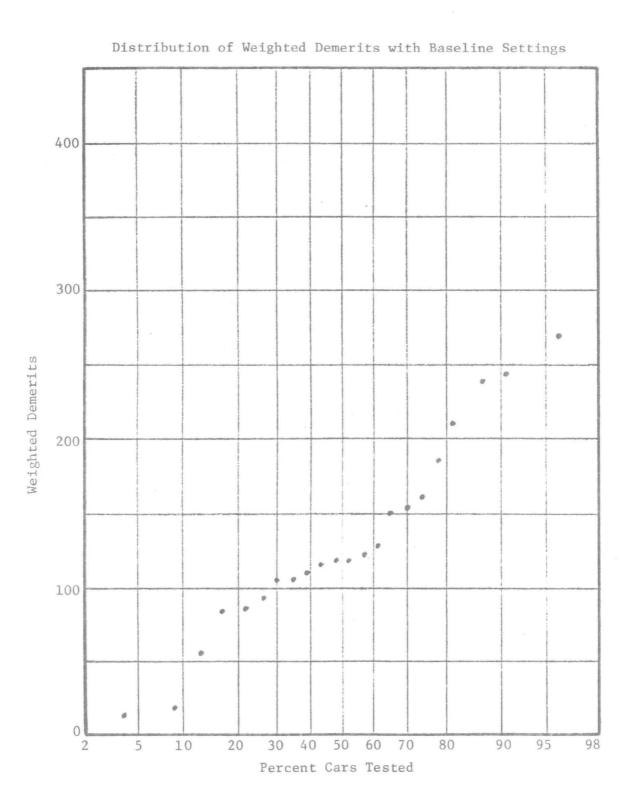


FIGURE 3

Driveability Comparison of Average of 1973, 1975 and 1977 Model Cars From CRC Tests (6) and 1977-78 EPA Test -1973 Models 1975 Models ⇒1977 Models Average Demerits X Δ 

Driveability Index = 0.5  $T_{10} + T_{50} + 0.5 T_{90}$ 

There has never been any good agreement within the industry on the level of demerits which gives acceptable driveability. This is probably due to the fact that demerits are assigned for many types of malfunctions and different people have different sensitivity to different types of malfunctions. For instance, a car that stalls twice every time that it is tested may be very annoyable, yet it could finish a driveability test with an excellent rating if the driveability was good in other respects. (Two stalls after start-up only contribute 16 demerits.) A car with moderate surge, however, on each maneuver of the driveability test would accumulate 192 demerits, yet it might not be objectionable to some drivers because the car was always dependable during cold driveaway.

In the CRC 1977 test program, <sup>(5)</sup> a subprogram was conducted to compare driveability as evaluated by people not familiar with driveability testing ("customer" drivers) with the driveability performance as determined by trained raters. The "customer" evaluated driveability in his every-day use of the vehicle while the trained rater used the CRC driveability procedure. The ratings were determined by the five "customers" driving nineteen of the test cars on three different fuels of low, intermediate and high volatility. The trained rater demerits for these three fuels on the average of the 18 cars was 114.1, 59.1 and 32.6 respectively.

The CRC report concludes - "Five 'customer' drivers were able to distinguish among the three main program test fuels on the basis of volatility-related driveability problems. Their performance ratings indicated a high degree of annoyance with the least volatile fuel, but few problems with either of the other fuels."

This does not mean that there was a high degree of annoyance with carfuel combinations that gave 114 demerits on the CRC procedure since only some of the cars on this fuel were rated low.

Although the program did not result in a go-nogo answer to the level of demerits that are acceptable, it did indicate that the "customer" drivers ranked the fuels much the same as trained drivers did under controlled conditions and also concluded that the "customer" is critical only if major malfunctions are observed.

It is apparent that much more work needs to be done on evaluating the relationship between the customers tolerance to driveability and the ratings obtained on a repetitive test procedure.

Table 2 summarizes the number of stalls obtained during all of the drive-ability tests. The idle stalls usually occur immediately after the cold start or when the transmission is shifted from park to drive. The moving stalls occur during attempted acceleration maneuvers. The idle stalls can be very annoying and the moving stalls can be dangerous if they occur in traffic. Since the cars are listed in the order of decreasing driveability demerits, it is obvious that there is only a slight correlation between the driveability demerits and the number of stalls.

TABLE 2
STALLS DURING DRIVEABILITY RUNS

	Runs	Idle Stalls	Idle Stalls/ Run	Moving Stalls	Moving Stalls/ Run	Total Stalls/ Run
Volare 318-C	10	9	0.9	10	1.0	1.9
Volare 318-F	12	18	1.5	7	0.6	2.1
Volare 225-F	14	13	0.9	34	2.4	3.3
LTD 351W-F	10	14	1.4	15	1.5	2.9
Cordoba 400-F	10	8	0.8	0	0	0.8
Maverick 250-F	10	0	0	5	0.5	0.5
Pinto 140-F	10	2	0.2	7	0.7	0.9
Granada 302-C	14	4	0.3	6	0.4	0.7
Cutlass 350-F	13	0	0	0	0	0
Concord 258-C	10	0	0	1	0.1	0.1
Sunbird 151-C	14	0	0	18	1.3	1.3
Chevelle 305-F	11	4	0.4	11	1.0	1.4
Maverick 250-C	8	0	0	0	0	0
Chevette 98-F	10	5	0.5	8	0.8	1.3
Skylark 231-F	10	0	0	0	0	0
Century 350-F	10	0	0	4	0.4	0.4
Buick 231T-F	10	0	0	10	1.0	1.0
01ds 98 403-F	10	0	0	1	0.1	0.1
Granada 302-F	10	7	0.7	4	0.4	1.1
Grand Prix 301-F	10	0	0	0	0	0
Volvo 130-C	10	0	0	0	0	0
Toyota 97-F	10	0	0	0	0	0

Most of the Federal calibration cars met the 1977 Federal emission standards and those that did not were very close to the limits. The fleet average was 31% below the standards for HC, 27% for CO and 33% for NOx.

Only two of the California cars met the emission standards on all pollutants. California cars were difficult to obtain on the East coast and the four cars that did not meet the limits were all laboratory test cars that had previously been used in other emission programs. After running a number of tests on the Maverick 250 vehicle, thoroughly checking the components of the emission system and rebuilding the carburetor, we found that the emissions were still high and CO was unstable from run to run, so this vehicle has not been included in the data analysis.

#### C. Maladjusted Vehicle Tests

The maladjustments used in this program were obtained from EPA and represented settings and disablements found to be prevalent in their "Restorative Maintenance Evaluation Project". Since the maladjustments differed from vehicle to vehicle, the effect of a class of maladjustment can best be evaluated by comparing the results on all of the vehicles upon which the maladjustment was used.

#### 1. Effect of Disconnecting the Exhaust Gas Recirculation Valve

This maladjustment was performed on all of the vehicles which used EGR valves. The results are shown in Table 3, divided into three categories of emission systems; i.e., Federal systems with oxidizing catalyst, California systems with oxidizing catalyst, and one car with a three-way catalyst system. Disconnecting the EGR valve improved driveability an average of 21%\* on the Federal emission control vehicles. Generally disconnecting the EGR valve reduced or eliminated surge when it was present on baseline tests and reduced hesitation on acceleration tip-in.

Although individual cars showed both higher and lower HC and CO emissions, the average emissions of the fleet were the same. Disconnecting the EGR gave the expected large increase in NOx emissions with the average of the fleet increasing by 210%. The average fuel economy was improved slightly and the acceleration rate was also improved slightly. The change in acceleration rate was probably due to the fact that the accelerations were made from road load 16.1 kph where the EGR would be functioning on the baseline runs.

<sup>\*</sup> Fleet average percent change in Tables 3 through 8 is calculated by comparing the average demerits, emissions, or acceleration time from all of the vehicles with the particular maladjustment with the average from the baseline tests. The fuel economy percent change is calculated by comparing the reciprocal of the average of the fuel consumption measurements from the vehicles with maladjustments with the reciprocal of the average from the baseline.

TABLE 3

EFFECT OF DISCONNECTING EGR ON VEHICLE DRIVEABILITY,
EMISSIONS, FUEL ECONOMY AND ACCELERATION TIME

## PERCENT CHANGE FROM BASELINE

	Drive-				n 1	A 1	
	ability Demerits	HC En	co CO	NOx	Urban	Economy Highway	Accel. Time
	Demei its	110	<u>50</u>	HOX	Orban	nii giiwa j	11
Volare 318-F	-20	-13	+ 7	+ 85	+ 6.6	+ 5.3	- 2.2
Volare 225-F	-35	+ 8	+ 6	+252	+10.7	+12.1	- 3.5
LTD II 351W-F	-40	- 6	+ 3	+248	- 1.6	- 2.7	+ 0.5
Maverick 250-F	-20	-26	+ 2	+430	+ 1.2	- 2.2	- 2.3
Pinto 140-F	- 1	+ 2	+ 6	+186	+ 6.1	+ 8.8	- 5.7
Cutlass 350-F	-34	- 1	-13	+280	+ 0.7	+ 2.7	- 1.4
Chevelle 305-F	+ 1	+14	+12	+ 36	+ 2.3	+ 6.3	- 0.8
Chevette 98-F	-18	-21	-21	+173	+ 0.5	- 2.6	- 3.5
Skylark 231-F	<b>-2</b> 5	+39	+10	+198	+10.0	+ 5.2	- 3.3
Century 350-F	-47	- 1	-10	+206	+ 3.7	+ 4.3	- 0.8
Regal 231-TF	-10	+ 6	+ 6	+227	- 6.7	- 9.6	- 2.4
01ds 403-F	+11	+13	- 3	+224	- 0.4	+ 0.4	- 0.5
Granada 302-F	-42	-11	+ 3	+252	- 0.1	- 4.6	- 1.4
Grand Prix 301-F	<u>+40</u>	+11	<u>- 1</u>	+214	<u>- 3.2</u>	<u>- 5.0</u>	<u>- 0.5</u>
FLEET AVERAGE	-21.2	- 1.4	+ 0.9	+210	+ 2.0	+ 1.1	- 2.2
Volare 318-C	-49	-23	-21	+ 60	+10.3	+16.2	0
Granada 302-C	<b>-</b> 97	+26	-23	+206	+ 7.1	+ 4.7	+ 1.8
Concord 258-C	<del>-72</del>	<u>-26</u>	<u>-45</u>	+281	+15.7	+28.4	<del>-26.7</del>
FLEET AVERAGE	-67.8	0	-31.0	+159	+10.8	+16.0	-11.0
Sunbird 151-C	-10	-32	-11	- 3.1	- 0.3	- 5.1	- 2.0
							_
TOTAL FLEET AVERAGE	GE -30.6	- 2.7	- 2.1	+190	+ 3.7	+ 3.7	- 3.8

The three California cars with oxidizing catalysts showed a much larger improvement in driveability when the EGR was disconnected. CO was reduced by 31% but NOx was increased by 159%. Fuel economy was improved considerably more on these California calibration cars than on the Federal cars both on a fleet average basis and on the two individual cars, Granada 302 and Volare 318, where a comparison can be made with their counterparts in the Federal fleet. The large change in acceleration time on the Concord 258 was due to the EGR valve opening at full throttle high engine speed. This is inherent in the calibration used on this engine.

Disconnecting the EGR on the one vehicle with a three-way catalyst made much less difference in driveability, economy and emissions than on the vehicles with oxidizing catalysts.

There are two side effects of disconnecting EGR that were not investigated as part of this program. The recycled exhaust gas lowers the part throttle octane requirement of the vehicle so disconnecting the EGR can increase the part throttle octane requirement of the vehicle and cause knock problems in vehicles with no part throttle knock with the normal calibration. Although knock observations were not specifically investigated in this program, knock was detected during the driveability test on the Pinto 140-F, Maverick 250-F and Granada 302-F during the runs with the EGR disconnected.

Also, disconnecting EGR can lead to a reduction in the service life of the clutches in automatic transmissions. The part throttle clutch pressure in automatic transmissions is calibrated to match the engine torque output in order to give smooth shifts. The transmission pressure is controlled by either a mechanical linkage from the carburetor throttle linkage or by a pressure modulator connected to manifold vacuum, depending on the make and model of the transmission. Disconnecting EGR changes the manifold vacuum or throttle position to engine torque relationship and results in lower clutch pressure during part throttle shifts. This can result in clutch slippage and shorten clutch life.

#### 2. Effect of Rich Idle Mixture

The idle mixture was adjusted richer than specification on 15 of the vehicles, as shown on Table 4. The amount of enrichment used (see the last column of Table 4) was dependent upon the settings found on the EPA Restorative Maintenance Evaluation Program and was described by the CO at idle with the air pump, on those cars so equipped, bypassed. In most cases these settings were only slightly richer than the standard setting and all settings could be obtained within the limits of adjustment of the idle screws.

The fleet average driveability was not affected by the richer idle settings. Some vehicles improved considerably and some were made worse. The two vehicles with the largest percentage increase in driveability demerits with the richer mixture were the Volare 225-F and the Volvo 130-C. When the mixture on the Volare was enrichened it stumbled very badly on the part throttle accelerations even when approaching the end of the test. In order to be sure that this was due to the adjustment and not some other engine malfunction, the baseline and the rich idle runs were rerun twice with the same

TABLE 4

EFFECT OF RICH IDLE ON VEHICLE DRIVEABILITY,
EMISSIONS, FUEL ECONOMY AND ACCELERATION TIME

## PERCENT CHANGE FROM BASELINE

	Drive- ability	Emissions			Fuel Economy		Idle Accel.Setting	
	Demerits	HC	<u>co</u>	NOx	Urban	Highway	<u>Time</u>	% CO
Volare 318-C	-22	+ 17	+ 7	-11	+3.5	+0.7	0	2%
Volare 318-F	+ 3	+ 46	+ 97	+ 8	-4.2	-1.8	-0.3	1%
Volare 225-F	+53	+ 51	+ 85	- 8	+4.4	+5.1	-2.8	4%
Cordoba 400-F	+15	+131	+397	- 1	-3.8	+2.5	+1.5	0.7%
Maverick 250-F	- 9	+ 42	+ 67	+ 3	+2.2	+3.2	-6.2	1%
Pinto 140-F	-40	+ 70	+ 91	- 1	+3.9	+7.2	-6.4	2%
Granada 302-C	-58	- 1	- 11	- 7	+2.1	+3.0	-1.8	2%
Concord 258-C	+ 5	- 3	+ 0	-13	+0.2	+3.5	-3.2	2%
Chevelle 305-F	+ 3	+126	+155	+ 2	+0.3	+4.9	-0.7	3%
Century 350-F	<b>-17</b>	+248	+379	-25	-7.1	-2.5	-2.0	3%
Regal 231T-F	-18	- 9	+ 76	-23	-7.5	+4.0	+1.9	2%
Granada 302-F	+48	- 32	+ 14	-22	-2.7	-3.0	+2.2	2%
Grand Prix 301-F	+22	+112	+151	+ 5	+0.6	+3.6	+0.4	1.5%
Volvo 130-C	+53	<u>- 3</u>	<u>+ 19</u>	<u>+42</u>	<u>-2.1</u>	<u>-5.3</u>	+2.1	4%
FLEET AVERAGE	+ 4.1	+ 48	+108	- 7.9	-0.9	+1.4	-1.2	

result. The Volvo 130-C had such low demerits on baseline that the increase in nine driveability demerits with the rich idle mixture was within the repeatability of the driveability procedure even though the percentage change was large.

The increase in HC and CO with idle enrichment varied widely among cars indicating that the effective mixture was being changed considerably more on some cars than on others. In future programs it would probably give more consistent results if the idle CO measurements were made ahead of the catalyst instead of downstream as used on this program and the Restorative Maintenance Program.

The total fleet average HC emissions were increased by almost 50% and the CO was more than doubled. The richer mixtures resulted in a slight reduction in NOx.

Urban and highway fuel economy and acceleration time showed very little change due to the change in idle mixtures.

#### 3. Effect of Richer Choke Settings

The effect of richer choke settings was investigated on seven vehicles as shown in Table 5. The two Chrysler vehicles used electric choke heaters in the choke housing to increase the rate of choke heat. On these vehicles the electric heater was disconnected. The four GM cars and the Granada all used chokes with adjustable housings. These were set one notch richer on the Chevette, two notches richer on the Oldsmobile 98 and three notches richer on the other vehicles.

The richer chokes improved driveability by 27% on the fleet average and showed the largest effect on the cars where the choke housing was adjusted. The richer choke settings reduced the demerits due to a reduction in stumble. In cases where vehicles encountered idle and moving stalls on the baseline runs the richer choke settings reduced the number of stalls on the Volare and the Granada but did not eliminate them. It must be remembered that these driveability runs were only run at one temperature,  $16^{\circ}\text{C}$  (60F), and other temperatures would probably show different influences of the richer choke settings. As can be seen from the table, the choke settings had little effect on emissions, fuel economy and acceleration time of the vehicles.

#### 4. Effect of Advancing Spark Timing

Spark timing was advanced on six of the vehicles, as shown in Table 6. Driveability was improved 11% on the fleet average. The Volvo had only 17 demerits on baseline, so the increase in percentage demerits was within the repeatability of the test even though the percentage is high. On an average the NOx was increased by 20% with little change in HC and CO emissions. Slight improvements were obtained on fuel economy. Advancing the spark was the only modification that improved the vehicle acceleration time to the point that it might be perceptible to the driver.

EFFECT OF RICH CHOKE SETTING ON VEHICLE DRIVEABILITY,
EMISSIONS, FUEL ECONOMY AND ACCELERATION TIME

TABLE 5

## PERCENT CHANGE FROM BASELINE

	Drive- ability Demerits HC		Emissions CO NOx		Fuel Economy Urban Highway		Accel.	Change in Choke Setting
	Demeries	110	<u>-00</u>		<del>OI Dan</del>			3333338
Volare 318-C	- 4	-21	- 6	-13	+3.5	+0.6	-1.7	(1)
Cordoba 400-F	-11	- 4	+44	+11	-5.1	-1.8	+1.6	(1)
Cutlass 350-F	-39	- 3	+25	- 5	-1.6	+0.4	-2.4	3-R
Chevette 98-F	-43	- 3	-13	- 3	+4.4	+3.7	-2.0	1-R
Skylark 231-F	-68	+35	+22	- 8	+4.3	+0.4	-0.5	3-R
Olds 98 403-F	-27	+ 4	+14	-12	+1.3	+4.1	+1.0	2-R
Granada 302-F	<u>-43</u>	+ 2	+ 6	<u>+10</u>	<u>-1.8</u>	<u>-1.4</u>	<u>-1.0</u>	<u>3-R</u>
FLEET AVERAGE	-27	+ 2.6	+12.3	- 3.3	+0.3	+0.6	-0.5	

<sup>(1)</sup> Disconnected electric choke heater

TABLE 6

# EFFECT OF ADVANCING SPARK ON VEHICLE DRIVEABILITY EMISSIONS, FUEL ECONOMY AND ACCELERATION TIME

## PERCENT CHANGE FROM BASELINE

	Drive-							
	ability	Emissions			Fuel Economy		Accel.	Spark
	Demerits	HC	<u>co</u>	NOx	Urban	Highway	Time	Advanced
Volare 225-F	-11	-10	-15	+ 8	+6.9	+5.9	-2.1	6°
LTD-II 351W-F	+12	- 5	- 1	+16	-2.2	-4.4	-3.1	4°
Cordoba 400-F	- 4	+ 6	+ 7	+18	-2.4	+2.4	-6.0	4°
Maverick 250-1	F -39	0	- 4	+32	+4.7	+2.5	-4.7	6°
Pinto 140-F	-25	- 1	-19	+32	+8.7	+7.4	-10.7	6°
Volvo 130-C	+35	<u>- 6</u>	+17	<u>+13</u>	<u>-0.6</u>	<u>-5.8</u>	1.4	<u>5°</u>
FLEET AVERAGE	-10.9	- 2.9	7.0	+19,6	+1.8	+1.1	-4.6	

It is well known that advancing the timing increases the knocking tendency of cars. Although knock was not monitored as part of this program, knock was observed on the Pinto 140-F and Maverick 250-F during the driveability tests with the advanced spark settings.

#### 5. Effect of Increased Idle RPM

The idle rpm was increased on four of the cars as shown in Table 7.

The increased idle speed improved the driveability on three of the cars and was detrimental on the fourth. Generally, the increased rpm reduced the stumble demerits except for the Skylark and on this car the stumble demerits were greatly increased. HC and CO emissions were reduced with a slight increase in NOx.

Fuel economy, particularly on the urban cycle, was reduced and there was a slight improvement in acceleration time.

#### 6. Turbocharged Buick Maladjustments

The turbocharged Buick Regal was treated as a special case. This vehicle uses a knock sensor to determine when the engine knocks and electronically retards the spark. Since the operating ignition timing would be different under knocking conditions when the vehicle is operating with a high octane fuel than on a normal regular unleaded fuel, the acceleration performance, and possibly the driveability, fuel economy and the emissions might be different.

The complete data on the performance of this car is shown on Table A-7 in Appendix A. The baseline acceleration runs were made on Sunlite unleaded gasoline of a nominal 91.5 Research octane number. When the accelerations were made on the special high octane fuel, described in Section II-D, the acceleration time was reduced by 9.5%. Driveability on this high octane fuel was 13% poorer than on the 93 octane driveability fuel but the driveability index of the high octane fuel was 223 (466 in °F units) compared to 217.5 (456) on the driveability fuel. Previous driveability/fuel volatility correlation programs would indicate that this change in driveability index should give about this change in driveability so it is believed that the high octane number of the test fuel had no effect on driveability.

This vehicle has an external connection to the control of carburetor power enrichment from the turbocharger boost pressure. If this hose is disconnected, the power enrichment valve will be open at all times. This modification improved driveability by 50% but the richer mixture at light loads reduced fuel economy by 13 to 14% and increased HC by 183% and CO by 745%. There was only a small improvement in acceleration time.

The idle CO and EGR disconnect modifications have been discussed in previous sections.

EFFECT OF INCREASED IDLE RPM ON VEHICLE DRIVEABILITY

EMISSIONS, FUEL ECONOMY AND ACCELERATION TIME

PERCENT CHANGE FROM BASELINE

	Drive- ability		Emissions			Conomy	Accel.	Inc. Idle
	<u>Demerits</u>	HC	<u>CO</u>	NOx	Urban	Highway	Time	Speed
Volare 318-F	- 7	-10	+25	+ 4	-5.7	-2.2	0	250
Cutlass 350-F	-44	- 9	- 1	+17	-6.4	-2.5	-1.3	125
Chevette 98-F	-11	-36	-15	+13	-5.8	-3.0	-3.5	125
Skylark 231-F	+32	- 4	<u>-21</u>	<u>+11</u>	+3.9	<u>+1.0</u>	<u>-2.3</u>	125
FLEET AVERAGE	- 9	-16.1	- 6.4	+11.9	-4.1	-1.6	-1.9	

#### 7. Three-way Catalyst Vehicle Maladjustment

Two of the vehicles used on the program were equipped with California calibration emission systems using oxygen sensors in the exhaust for feedback control of the fuel-air ratio. When the oxygen sensors were disconnected the Volvo, which had excellent driveability in baseline condition, showed no change in driveability and the Sunbird showed a 15 to 24% improvement. On the Volvo, the richer fuel metering with the sensor disconnected reduced the fuel economy on the urban cycle by 2% and 5% on the highway cycle and resulted in increases of HC, CO and NOx emissions of 59%, 193% and 145%. When a combination of 5° advanced spark and a slightly richer idle were combined with the O<sub>2</sub> sensor disconnect, the HC was increased by 430% and the CO by 1200%.

The  $0_2$  sensor disconnect on the Sunbird resulted in a 14% reduction in urban economy and a 13% reduction in highway economy. HC emissions were increased by 220% and CO by 1000%. NOx was reduced by 65%.

Complete data on these two cars is shown on Tables A-22 and A-23 in Appendix A.

#### 8. Effect of Multiple Maladjustments

One of the modifications tested on all but one car in the fleet was the maladjustment of two and sometimes three items at one time. These combinations of maladjustments were similar to those found on many of the maladjusted cars in the Restorative Maintenance Evaluation Project. Since the type of maladjustment varied from car to car, it would not be expected that these maladjustments would have the same effect on driveability, emissions or fuel economy, but a fleet average of all of the tests may be representative of the portion of in-use cars with multiple maladjustments.

Table 8 shows the results of these tests divided into groups according to the type of emission control system. Details of the maladjustments to each car are given in Tables A-2 to A-23 in Appendix A.

The multiple maladjustments improved the driveability on nine of the Federal calibration cars and made it worse on six for a fleet average of 3% improvement. Emissions of HC, CO and NOx were increased considerably and urban fuel economy was reduced slightly. Highway fuel economy and acceleration performance were improved very slightly.

The California fleet with oxidizing catalysts, although of very limited sample size, showed a larger improvement in driveability and a smaller increase in HC and CO and a reduction in NOx. The modifications resulted in a slight reduction in fuel economy and acceleration performance.

The two California cars with three-way catalyst both showed large increases in HC and CO since one of the maladjustments on each car was the disconnect of the  $\rm O_2$  sensor, as discussed in the previous section.

TABLE 8

# EFFECT OF MULTIPLE MALADJUSTMENTS OF VEHICLE DRIVEABILITY, EMISSIONS, FUEL ECONOMY AND ACCELERATION TIME

## PERCENT CHANGE FROM BASELINE

	Drive-	_				_	. 1	W 1 1
	ability		mission			Economy		
	Demerits	HC	co	NOx	<u>Urban</u>	Highway	Time	justments
Volare 318-F	- 4	+ 37	+111	+ 13	-8.1	-2.8	-0.8	IRPM, ICO
Volare 225-F	+48	+ 55	+130	- 13	-0.2	+2.7	+0.7	IRPM, ICO
LTD 351W-F	+ 6	+ 15	+ 31	+ 19	-2.5	-7.1	-2.5	+ Spark, RRPM
Cordoba 400-F	+ 4	+140	+488	+ 12	-6.8	-4.3	-0.3	ICO, IRPM
Maverick 250-F	- 5	+ 63	+ 69	+ 19	-0.2	-0.5	-4.7	+ Spark, ICO
Pinto 140-F	-11	+ 49	+ 77	- 4	+1.4	+2.5	-5.7	IRPM, ICO
Cutlass 350-F	-33	+ 8	+ 55	+ 34	-6.1	-2.8	-3.2	Choke, IRPM
Chevelle 305-F	+16	+125	+190	- 8	-1.2	+4.8	+5.3	- Spark, ICO
Chevette 98-F	-35	- 30	- 18	+ 13	-8.0	-10.1	+0.7	Choke, IRPM
Skylark 231-F	-40	+ 81	+ 31	+187	+10.6	+5.1	-3.9	EGR, Choke
Century 350-F	-13	+162	+149	+163	+3.7	+4.5	-3.9	EGR, ICO
01ds 98 403-F	-54	- 13	+ 4	- 24	+1.1	+4.4	+1.6	Choke, IFI
Granada 302-F	+ 4	- 33	+ 44	- 28	-8.0	-8.2	+6.6	- Spark, ICO
Grand Prix 301-F	+ 9	+ 78	+185	+172	+1.3		-3.7	EGR, ICO
Toyota 97-F	-100+	+ 10	+ 31	- 13	+1.1	-0.8	0.0	ICO, RFI
•								
FLEET AVERAGE	- 3.4	+ 40.1	+ 80.9	+ 22.5	-2.1	+0.3	-0.9	
Volare 318-C	+15	+ 23	+133	- 13	-6.9	-6.3	+9.3	- Spark, ICO
Granada 302-C	-77	- 3	- 13	- 10	+3.7	-1.5	0	RRPM, ICO
Concord 258-C	-12	+ 39	+ 83	- 22	+4.9	+4.8	+3.2	Choke, ICO
FLEET AVERAGE	-16.9	+13.8	+ 61.1	- 14.4	-0.3	-1.2	+4.1	
Sunbird 151-C	-12		+1024	- 64	-15.2	<b>-</b> 13.9	-4.7	0 <sub>2</sub> , EGR
Volvo 130-C	+ 6	+431	+1210	+ 5	-3.2	-6.2	-2.1	$0_2^2$ , + Spark, ICO
								-
FLEET AVERAGE	<b>-</b> 9.7	+277	+1074	<b>-</b> 46.2	-9.2	-10.0	-3.5	
OVERALL AVERAGE	- 6.4	+ 52.5	+141.7	+ 13.0	-2.3	-0.8	-0.4	
TDD1/ T T11	7714	a1 1					_ D.4	
IRPM = Increase Idl		Chok			ke riche			sconnect 0 <sub>2</sub> sensor
RRPM = Reduce Idle		+ Sp		Advance				crease fast idle
EGR = Disconnect E	GR	– Sp	ark =	Retard	spark	R	FI = Re	duce fast idle

The overall fleet with multiple maladjustments showed a slight improvement in driveability at the expense of higher emissions and a slight reduction in fuel economy and acceleration time.

Table 9 is a summary of the "fleet average" effects of maladjustments on vehicle driveability, emissions, fuel economy and acceleration time.

Appendix D contains plots of vehicle driveability vs. emissions, fuel economy and acceleration time for each vehicle on an absolute basis and on a normalized basis. It also contains plots of vehicle driveability vs. emissions, fuel economy and acceleration time on an absolute basis and on a normalized basis for each maladjustment.

TABLE 9

# SUMMARY OF "FLEET AVERAGE" EFFECTS OF MALADJUSTMENTS ON VEHICLE DRIVEABILITY, EMISSIONS, FUEL ECONOMY AND ACCELERATION TIME

## PERCENT CHANGE FROM BASELINE

	Drive- ability	Emissions	Fuel Economy	Accel.
	Demerits HC	CO NOx	Urban Highway	Time
Disconnect EGR	-31 - 3	- 2 +190	+4 +4	-4
Richer Idle	+ 4 +48	+108 - 8	-1 +1	<b></b> 1
Richer Choke	-27 + 3	+ 12 - 3	0 +1	-1
Advanced Spark	-11 - 3	- 7 + 20	+2 +1	<b>~</b> 5
Increased Idle RP	M - 9 -16	- 6 + 12	<b>-</b> 4 <b>-</b> 2	-2
Multiple Maladjus ment	t 6 +53	+142 + 13	-2 -1	0

<sup>-</sup> Means improved driveability, reduced emissions, better acceleration performance, but poorer fuel economy.

#### IV. RECOMMENDATIONS

The results of this project has indicated that there is a wide variation in the driveability of various makes of 1977 and 1978 passenger cars when tested at 16°C and that the driveability can be improved by modifications in the engine adjustment. These modified adjustments usually cause large increases in vehicle emissions. This program was only conducted at a mild temperature (16°C) and a lower temperature more representative of normal winter operation should be investigated to see if the lower temperature would give different and probably more critical driveability. Also, some of the maladjustments such as richer choke settings would probably show different effects on vehicle emissions if the emission tests were run at lower temperature to simulate winter operation.

The CRC driveability procedure was developed in 1968 when engine calibrations were much different than at present. In general both carburetor and choke calibrations were much richer and exhaust gas recirculation or catalyst were not used. Since the procedure is over ten years old and engines have changed drastically, it might be advisable to re-evaluate the procedure as it applies to modern vehicles.

The demerit rating weighting system used in the CRC procedure (see Appendix B, Driveability Test Procedure) assigns weightings to malfunctions by the degree of severity. A trace hesitation, stumble or backfire is counted 6 demerits, moderate 12 and heavy 24 demerits. An engine stall when the vehicle is idling only counts 8 demerits and a stall while maneuvering 32. Since stalls are more serious from a safety standpoint and more irritating to the driver, it seems that the relative weighting of stalls should be increased in future programs.

Also, more work needs to be done on evaluating the relationship between the tolerance to driveability of the average customer in normal vehicle operation and ratings obtained by trained raters on a repetitive test procedure.

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- 5. Coordinating Research Council Driveability Performance of 1975 Passenger Cars at Intermediate Ambient Temperatures Paso Robles, No. CM-102-74, May, 1976.
- 6. Coordinating Research Council Driveability Performance of 1977 Passenger Cars at Intermediate Ambient Temperatures Paso Robles, Report No. 499, September, 1978.

TABLE A-1 - APPENDIX A

## BASELINE TUNE-UP SETTINGS

	Model_		Cu. In. Disp.	Carb.	Odom.	Idle Setting Method	Speed Change	Idle Speed	Fast Idle Speed	Choke Setting	Basic Timing BTC
	Volare	177	225-F	1-Bb1.	11555	Propane	130 rpm	700-N	1700 (2nd)	.080 CI .110 Vac. Kick	2°
	Granada	177	302-C	2 <b>-</b> VV	10202	Propane	40 rpm <sup>(1)</sup>	600-D	1900 (H1)	Index	12°
	Maverick	177	250-F	1-Bb1.	11509	Propane	80 rpm	600-D	1700 (2nd)	1-R	6°
	Pinto	177	140-F	2-Bb1.	10241	Propane	70 rpm	800-D	2000 (2nd)	Index	20°
נג	Chevelle	177	305-F	2-Bb1.	15937	Idle Speed Drop	50 rpm	500-D	Pre-set	Index	8°
3	Skylark	177	231-F	2-Bb1.	5914	Idle Speed Drop	40 rpm	600-D	Pre-set	1-R	12°
	Century	177	350-F	2-Bb1.	8822	Idle Speed Drop	60 rpm	600-D	1600 (Hi)	1-R	12°
	Cutlass	177	350-F	4-Bb1.	8097	Idle Speed Drop	30 rpm	550-D	900	2-R	20°
	Cordoba	177	400-F	4-Bb1.	6996	Propane	130 rpm	830-N	1400	.100"	20°
	LTD II	177	351-F	2-Bb1.	14457	Propane	120 rpm	625-D	2100 (H1)	1-R	4°
	Granada	177	302-F	2-Bb1.	5379	Propane	80 rpm	650-D	2100	Index	2°
	Volare	<b>"</b> 77	318-F	2-Bb1.	8164	Propane	80 rpm	700-N	1400	.070 CI .110 Vac. Kick	8°

<sup>(1)</sup> Could not reach Specs.

TABLE A-1 - APPENDIX A

BASELINE TUNE-UP SETTINGS

		Cu. In. Disp.	Carb.	Odom.	Idle Setting Method	Speed Change	Idle Speed	Fast Idle Speed	Choke Setting	Basic Timing BTC
Corolla	<b>'</b> 78	97-F	2-Bb1.	3813	Idle Speed Drop	70 rpm	850-N	3200	Index	10°
Chevette	<b>'</b> 77	98-F	1-Bb1.	20577	Idle Speed Drop	50 rpm	800-D	2400 (Hi)	3-R	8°
Volare	<b>'</b> 77	318-C	2-Bb1.	25748	Idle CO (%)	0.5% CO	850-N	1500	Elect.	TDC
Maverick	<b>'</b> 77	250-C	1-Bb1.	27800	Optimum Idle	"0" Increase	600-D	2100 (2nd)	2-R	8°
Grand Pri	х <b>'</b> 78	301-F	2-Bb1.	12524	Propane	30 rpm	550 <b>-</b> D	2200 (Hi)	2-R	12°
$^{\omega}_{\omega}$ Olds 98	<b>'</b> 77	403-F	4-Bb1.	12079	Idle Speed Drop	30 rpm	550-D	900 (Lo)	2-R	20°
Concord	<b>'</b> 78	258-C	2-Bb1.	1985	Idle Speed Drop	25 rpm	700-D	1600 (2nd)	Index	8°
Regal <sup>(2)</sup>	<b>'</b> 78	231-F	4-Bb1.	8636	Lean Best Idle	20 rpm	650 <b>-</b> D	2500 (Hi)	Index	15°
Sunbird	<b>'</b> 78	151 <b>-</b> C	2-Bb1.	33470	Propane	1% CO	650 <b>-</b> D	2200	1-R	14°
Volvo 245-DL	<b>'</b> 78	130-C	F.I.	2020	Idle CO	2.0% CO	900-N	900	None	12°

<sup>(2)</sup> Turbocharged

TABLE A-2

PERFORMANCE OF 1977 CHEVROLET CHEVETTE

1.6 LITER (98 CU. IN.) 1-BBL. FEDERAL CALIBRATION

	Base		connect Edification	GR 1 7 2	Choke 1 Notch Rich  Modification 2  2 2	Incr. Idle 12  Modification	•	Incr. Id	Notch Ric le 125 rp fication 4	m
CRC Driveability Demerits	109	89	-20	-18.3		97 -12	-11.0	71	-38	-34.9
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	14.2	13.7	-0.5	-3.5		13.7 -0.5	-3.5	14.3	+0.1	+0.7
Fuel Economy FTP 1/100 km (mpg)	9.89 (23.79)	9.84 (23.91)	-0.05 (+0.12)	-0.5 (+0.5)		10.50 +0.61 (22.4) (-1.39	+6.2 ) (-5.8)	10.75 (21.88)	+0.86 (-1.91)	+8.7 (-8.0)
Highway 1/100 km (mpg)	7.26 (32.39)	7.46 (31.55)	+0.2 (-0.84)	+2.8 (-2.6)		7.49 +0.23 (31.42) (-0.97)	+3,2 (-3.0)	8.08 (29.11)	+0.82 (-3.28)	+11.3 (-10.1)
Emissions, HC, gm/km (gm/mi)	0.63 (1.02)	0.50 (0.81)	-0.13 (-0.21)	-20.6 (-20.6)		0.40 -0.23 (0.65) (-0.37)	-36.3 (-36.3)	0.44 (0.71)	-0.19 (-0.31)	-30.4 (-30.4)
CO, gm/km (gm/mi)	9.77 (15.72)	7.70 (12.4)	-2.07 (-3.32)	-21.1 (-21.1)		8.28 -1.49 (13.33) (-2.39)	-15.2 (-15.2)	7.97 (12.82)	-1.8 (-2.9)	-18.4 (-18.4)
NOx, gm/km (gm/mi)	1.12 (1.80)	3.06 (4.92)	+1.94 (+3.12)	+173 (+173)		1.27 +0.15 (2.04) (+0.24)	+13.3 (+13.3)	1.27 (2.04)	+0.15 (+0.24)	+13.3 (+13.3)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-2-A

PERFORMANCE OF 1977 CHEVROLET CHEVETTE\*

1.6 LITER (98 CU. IN.) 1-BBL. FEDERAL CALIBRATION

	Base*	Modification 1	Choke 1 Notch Ri Modification 2		Modification 3	Modification 4
CRC Driveability Demerits	109		62 -47	-43.1		
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	15.2		14.9 -0.3	-2.0		
Fuel Economy FTP 1/100 km (mpg)	10.64 (22.11)		10.19 -0.45 (23.08) (+0.97)	-4.2 (+4.4)		
Highway 1/100 km (mpg)	7.69 (30.60)		7.42 -0.27 (31.72) (+1.12)	-3.5 (+3.7)		
Emissions, HC, gm/km (gm/mi)	0.48 (0.78)		0.47 -0.01 (0.76) (-0.02)	-2.6 (-2.6)		
CO, gm/km (gm/mi)	9.14 (14.69)		7.99 -1.15 (12.86) (-1.83)	-12.5 (-12.5)		
NOx, gm/km (gm/mi)	1.22 (1.97)		1.19 -0.03 (1.92) (-0.05)	-2.5 (-2.5)		

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

Rebuilt trans. with old governor reinstalled.

TABLE A-3

PERFORMANCE OF 1977 CHEVROLET CHEVELLE

5.0 LITER (305 CU. IN.), 2-BBL. FEDERAL CALIBRATION

Base			Disconnect EGR Modification 1		Idle CO @ 3% Modification 2			Retard Spark 4° Modification 3			Retard Spark 4° Idle CO @ 3% Modification 4		
CRC Driveability Demerits	117	118	+1	+0.8	121	+4	+3.4	110	-7	-6.0	136	+19	+16.2
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	10.57	10.49	-0.08	-0.8	10.50	-0.07	-0.7	11.60	+1.03	+9.7	11.13	+0.56	+5.3
Fuel Economy FTP 1/100 km (mpg)	16.08 (14.64)	15.71 (14.98)	-0.37 (+0.34)	-2.3 (+2.3)	16.03 (14.68)	-0.05 (+0.04)	-0.3 (+0.3)	16.80 (14.00)	+0.72 (-0.64)	+4.5 (-4.4)	16.26 (14.47)	+0.18 (-0.17)	+1.1 (-1.2)
Highway 1/100 km (mpg)	12.6 (18.68)	11.85 (19.85)	-0.75 (+1.17)	-6.0 (+6.3)	12.0 (19.6)	-0.60 (+0.92)	-5.0 (+4.9)	13.22 (17.79)	+0.62 (-0.89)	+4.9 (-4.8)	12.02 (19.57)	-0.58 (+0.89)	-4.6 (+4.8)
Emissions, HC, gm/km (gm/mi)	0.63 (1.01)	0.71 (1.15)	+0.08 (+0.14)	+13.9 (+13.9)	1.42 (2.28)	+0.79 (+1.27)	+126 (+126)	0.70 (1.13)	+0.07 (+0.12)	+11.9 (+11.9)	1.41 (2.27)	+0.78 (+1.26)	+125 (+125)
CO, gm/km (gm/mi)	8.16 (13.14)	9.13 (14.69)	+0.97 (+1.55)	+11.8 (+11.8)	20.84 (33.53	+12.68 (+20.39)	+155 (+155)	11.76 (18.93)	+3.60 (+5.79)	+44.1 (+44.1)	23.95 (38.55)	+15.78 (+25.4)	+190 (+190)
NOx, gm/km (gm/mi)	1.69 (2.72)	2.31 (3.71)	+0.62 (+0.99)	+36.4 (+36.4)	1.73 (2.78)	+0.04 (+0.06)	+2.2 (+2.2)	1.24 (2.0)	-0.45 (-0.72)	-26.5 (-26.5)	1.56 (2.51)	-9.13 (-0.21)	-7.7 (-7.7)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-4
PERFORMANCE OF 1978 PONTIAC SUNBIRD

## 2.5 LITER (151 CU. IN.), 2-BBL., CALIFORNIA CALIBRATION

	Base	Disconnect $0_2$ Sensor Modification 1 $\Delta$ 1 $\chi$ 2		Disconnect Mix Control Vac.Hose From Solenoid Modification 2			Disconnect EGR Modification 3			Combine 2 & 3 Modification 4		
CRC Driveability Demerits	117	9 <b>9</b>	-18	-15.4	89	-28	-23.9	105	-12	-10.3	103	-14 -12.0
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	14.9	14.5	-0.4	-2.7	14.5	-0.4	-2.7	14.6	-0.3	-2.0	14.2 -	).7 -4.7
Fuel Economy FTP 1/100 km (mpg)	10.88 (21.61)	12.71 (18.51)	+1.83 (-3.1)	+16.8 (-14.3)	12.60 (18.67)	+1.72 (-2.94)	+15.8 (-13.6)	10.92 (21.54)	+0.04 (-0.07)	+0.4 (-0.3)	12.84 +1 (18.32) (-3	
Highway 1/100 km (mpg)	8.32 (28.28)	9.59 (24.52)	+1.27 (-3.76)	+15.3 (-13.3)	9.66 (24.35)	+1.34 (-3.93)	+16.1 (-13.9)	8.76 (26.85)	+0.44 (-1.43)	+5.3 (-5.1)	9.66 +1 (24.36) (-3	
Emissions, HC, gm/km (gm/mi)	0.50 (0.81)	1.62 (2.61)	+1.12 (+1.8)	+222 (+222)	1.62 (2.61)	+1.12 (+1.8)	+222 (+222)	0.34 (0.55)	-0.16 (-0.26)	-32.1 (-32.1)	1.59 +1 (2.56) (+1	
CO, gm/km (gm/mi)	5.44 (8.75)	60.37 (97.15)	+54.93 (+88.4)	+1010 (+1010)	57.83 (93.07)	+52.39 (+84.32)	+964 (+964)	4.84 (7.79)	-0.6 (-0.96)	-11.0 (-11.0)	61.09 +55 (98.31)(+89	
NOx, gm/km (gm/mi)	1.21 (1.95)	0.41 (0.66)	-0.8 (-1.29)	-66.2 (-66.2)	0.39 (0.63)	-0.82 (-1.32)	-67.7 (-67.7)	1.17 (1.89)	-0.04 (-0.06)	-3.1 (-3.1)	0.44 -0 (0.71) (-1	.77 -63.6 (24) (-63.6)

 $<sup>^{1}</sup>$  Difference between value for respective modification and base (- decrease, + increase)

 $<sup>^{2}</sup>$  Percent change between respective modification and base (- decrease, + increase)

TABLE A-5

PERFORMANCE OF 1978 PONTIAC GRAND PRIX

4.9 LITER (301 CU. IN.) 2-BBL. FEDERAL CALIBRATION

			onnect EGI Lfication	1		le CO @ 1. ification		Disc	le CO @ 1.5 connect EGR ification	3	+(	cuum Breal 0.025" fication	
	Base_		$\Delta^1$	<u>7 2</u>		$\Delta 1$	<u></u>		$\Delta^1$	<u>, 2</u>		$\Delta^1$	<u> , 2</u>
CRC Driveability Demerits	55	77	+22	+40	67	+12	+22	60	+5	+9.1	59	+4	+7.3
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	9.84	9.79	-0.05	-0.5	9.88	+0.04	-0.4	9.48	-0.36	-3.7	9.76	-0.08	-0.8
Fuel Economy FTP 1/100 km (mpg)	14.30 (16.45)	14.47 (15.93)	+0.47 (-0.52)	+3.3 (-3.2)	14.21 (16.55)	-0.09 (+0.1)	-0.6 (+0.6)	14.12 (16.66)	-0.18 (+0.21)	-1.3 (+1.3)	14.48 (16.24)	+0.18 (-0.21)	+1.3 (-1.3)
Highway 1/100 km (mpg)	10.19 (23.09)	10.72 (21.94)	+0.53 (-1.15)	+5.2 (-5.0)	9.83 (23.93)	-0.36 (+0.84)	-3.5 (+3.6)	9.72 (24.24)	-0.47 (+1.12)	-4.6 (+4.9)	9.97 (23.59)	-0.22 (+0.5)	+2.2 (+2.2)
Emissions, HC, gm/km (gm/mi)	0.72 (1.16)	0.80 (1.29)	+0.08 (+0.13)	+11.2 (+11.2)	1.53 (2.46)	+0.81 (+1.3)	+112 (+112)	1.29 (2.27)	+0.57 (+0.91)	+78.4 (+78.4)	0.89 (1.43)	+0.17 (+0.27)	+23.3 (+23.3)
CO, gm/km (gm/mi)	5.72 (9.21)	5.69 (9.15)	-0.03 (-0.06)	-0.6 (-0.6)	14.37 (23.12)	+8.65 (+13.91)	+151 (+151)	16.34 (26.29)	+10.62 (+17.08)	+185 (+185)	5.95 (9.58)	+0.23 (+0.37)	+4.0 (+4.0)
NOx, gm/km (gm/mi)	1.03 (1.66)	3.24 (5.21)	+2.21 (+3.55)	+214 (+214)	1.08 (1.74)	+0.05 (+0.08)	+4.8 (+4.8)	2.81 (4.52)	+1.78 (+2.86)	+172 (+172)	1.28 (2.06)	+0.25 (+0.4)	+24.1 (+24.1)

<sup>1</sup> Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-6
PERFORMANCE OF 1977 BUICK SKYLARK

## 3.8 LITER (231 CU. IN.), 2-BBL., FEDERAL CALIBRATION

	Disconnect EGR  Modification 1 $_2$		Choke	3 Notche Rich	es		sconnect I 3 Notche		Incr. Idle 125 rpm		rpm		
	Base	Modi Base		1 2	Modi	fication :	2 2		dification <b>\Delta</b>		Мо	lodification 4	
CRC Driveability Demerits	105	79	-26	-24.8	34	-71	-67.6	63	-42	-40	139	+34	+32.4
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	14.72	14.23	-0.49	-3.3	14.65	-0.07	-0.5	14.14	-0.58	-3.9	14.38	-0.34	-2.3
Fuel Economy FTP 1/100 km (mpg)	15.17 (15.51)	13.8 (17.06)	-1.37 (+1.55)	-9.0 (+10.0)	14.55 (16.17)	-0.62 (+0.66)	-4.1 (+4.3)	13.72 (17.15)	-1.45 (+1.64)	-9.6 (+10.6)	14.92 (15.77)	0.25 (+0.60)	-1.6 (+3.9)
Highway 1/100 km (mpg)	10.36 (22.70)	9.85 (23.88)	-0.51 (+1.18)	-4.9 (+5.2)	10.32 (22.78)	-0.04 (+0.08)	-0.4 (+0.4)	9.86 (23.86)	-0.5 (+1.16)	-4.8 (+5.1)	10.26 (22.92)	-0.1 (+0.22)	-1.0 +1.0
Emissions, HC, gm/km (gm/mi)	0.46 (0.74)	0.64 (1.03)	+0.18 (+0.29)	+39.2 (+39.2)	0.62 (1.0)	+0.16 (+0.26)	+35.1 (+35.1)	0.83 (1.34)	+0.37 (+0.60	+81.1 (+81.1)	0.44 (0.71)	-0.02 (-0.03)	-4.0 (-4.0)
CO, gm/km (gm/mi)	11.36 (18.27)	12.5 (20.11)	+1.14 (+1.84)	+10.1 (+10.1)	13.84 (22.26)	+2.48 (+3.99)	+21.8 (+21.8)	14.8 (23.9)	+3.50 (+5.63)	+30.8 (+30.8)	8.95 (14.40)	-2.40 (-3.87)	-21.2 (-21.2)
NOx gm/km (gm/mi)	1.03 (1.66)	3.07 (4.94)	+2.04 (+3.28)	+198 (+198)	0.95 (1.53)	-0.08 (-0.13)	-7.8 (-7.8)	2.96 (4.76)	+1.9 (+3.1)	+187 (+187)	1.15 (1.85)	+0.12 +0.19	+11.4 (+11.4)

 $<sup>^{</sup>m 1}$  Difference between value for respective modification and base (- decrease, + increase)

 $<sup>^{2}</sup>$  Percent change between respective modification and base (- decrease, + increase)

TABLE A-7

PERFORMANCE OF 1978 BUICK REGAL

3.8 LITER (231 CU. IN.) TURBOCHARGED, 4-BBL., FEDERAL CALIBRATION

		Disconnect Modificatio	n 1		e CO @ 2% ficațion 2	<b>!</b> _	Powe	nnect Exter er Enrichme dification	nt 3	0ct	cial High ane Fuel ication	4
	Base	Δ	<u> </u>		$\Delta 1$	<u> </u>		<u> </u>	<u> </u>		<u> </u>	<u> </u>
CRC Driveability Demerits	91	82 -9	-9.9	75	-16	-17.6	46	-45	-49.5	103	+12	+13.2
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	10.07*	9.83* -0.24	-2.4	10.26*	+0.19	+1.9	9.93*	-0.14	-1.4	9.11	-0.96	-9.5
Fuel Economy FTP 1/100 km (mpg)	14.51 (16.21)	15.56 +1.05 (15.12) (-1.09)	+7.2 (-6.7)	15.69 (14.99)	+1.18 (-1.22)	+8.1 (-7.5)	16.73 (14.06)	+2.22 (-2.15)	+15.3 (-13.3)	14.44 (16.29)	-0.07 (+0.08)	-0.05 (+0.05)
Highway 1/100 km (mpg)	11.21 (20.98)	12.41 +1.02 (18.96) (-2.02)	+10.7 (-9.6)	10.78 (21.81)	-0.43 (+0.83)	-3.8 (+4.0)	13.07 (17.99)	+1.86 (-2.99)	+16.6 (-14.3)	10.73 (21.92)	-0.48 (+0.94)	-4.3 (+4.4)
Emissions, HC, gm/km (gm/mi)	0.50 (0.81)	0.53 +0.03 (0.86) (+0.05)	+6.2 (+6.2)	0.46 (0.74)	-0.04 (0.07)	-8.6 (-8.6)	1.41 (2.29)	+0.92 (+1.48)	+183 (+183)	0.62 (1.0)	+0.12 (+0.19)	+23.5 (+23.5)
CO, gm/km (gm/mi)	6.15 (9.90)	6.52 +0.37 (10.49) (+0.59)	+6.0 (+6.0)	10.81 (17.4)	+1.66 (+7.5)	+75.8 (+75.8)	52.0 (83.7)	+45.85 (+73.78)	+745 (+745)	5.16 (8.3)	-0.99 (-1.6)	-16.2 (-16.2)
NOx, gm/km (gm/mi)	0.78 (1.26)	2.56 +1.78 (4.12) (+2.86)	+227 (+227)	0.60 (0.97)	-0.18 (-0.29)	-23.0 (-23.0)	0.22 (0.35)	-0.56 (-0.91)	-72.2 (-72.2)	0.88 (1.41)	+0.1 (+0.15)	+11.9 (+11.9)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

<sup>\*</sup> All accel. tests run on 91 RON nominal Sunlite Fuel

TABLE A-8

PERFORMANCE OF 1977 BUICK CENTURY

5.7 LITER (350 CU. IN.), 2-BBL., FEDERAL CALIBRATION

	Base		sconnect E lification \( \Delta \) 1	-		ile CO @ 3: ification			Drop 20 r dification		Idle	Drop 20 rulfication	om
CRC Driveability Demerits	105	56	-49	-46.7	87	-18	-17.1	90	-15	-14.3	91	-14	-13.3
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	11.91	11.81	-0.1	-0.8	11.67	-0.24	-2.0	11.78	-0.13	-1.1	11.45	-0.46	-3.9
Fuel Economy FTP 1/100 km (mpg)	16.33 (14.41)	15.76 (14.94)	-0.57 (+0.53)	-3.5 (+3.7)	17.58 (13.38)	+1.25 (-1.03)	+7.7 (-7.1)	16.35 (14.39)	+0.02 (-0.02)	+0.1 (-0.1)	15.74 (14.95)	-0.59 (+0.54)	-3.6 (+3.7)
Highway 1/100 km	11.88	11.39	-0.49	-4.1	12.18	+0.3	+2.3	11.53	-0.35	-2.9	11.35	-0.53	-4.5
(mpg)	(19.82)	(20.67)	(+0.85)	(+4.3)	(19.32)	(-0.50)	(-2.5)	(20.40)	(+0.58)	(+2.9)	(20.72)	(+0.9)	(+4.5)
Emissions, HC, gm/km (gm/mi)	0.51	0.50	-0.01	-1.2	1.75	+1.25	+248	1.19	+0.68	+13.6	1.32	+0.81	+162
	(0.81)	(0.80)	(-0.01)	(-1.2)	(2.82)	(+2.01)	(+248)	(1.91)	(+1.1)	(+136)	(2.12)	(+1.31)	(+162)
CO, gm/km	6.55	5.87	-0.68	-10.4	31.36	+24.79	+379	17.29	+10.75	+164	16.31	+9.76	+149
(gm/mi)	(10.53)	(9.44)	(-1.09)	(-10.4)	(50.46)	(+39.9)	(+379)	(27.83)	(+17.3)	(+164)	(26.25)	(+15.7)	(+149)
NOx, gm/km	1.04	3.18	+2.14	+206	0.78	-0.25	-24.6	0.78	-0.26	-2.5	2. <b>7</b> 3	+1.70'	+163
(gm/mi)	(1.67)	(5.11)	(+3.44)	(+206)	(1.26)	(-0.41)	(-24.6)	(1.25)	(-0.42)	(-2.5)	(4.4)	(+2.73)	(+163)

 $<sup>^{1}</sup>$  Difference between value for respective modification and base (- decrease, + increase)

 $<sup>^{2}</sup>$  Percent change between respective modification and base (- decrease, + increase)

TABLE A-9
PERFORMANCE OF 1977 OLDSMOBILE CUTLASS

## 5.7 LITER (350 CU. IN.), 4-BBL., FEDERAL CALIBRATION

		Di	sconnect	EGR	Chol	te 3 Notch Rich	nes		ke 3 Notch	•	Inci	r. Idle 12	25 rpm
	Base	Mc	dification	on 1	Modi	fication	2 %2		odification A	•	Mo	odification	on 4
CRC Driveability Demerits	127	84	-43	-33.9	77	-50	-39.4	85	-42	-33.1	71	-56	-44.1
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	10.14	10.00	-0.14	-1.4	9.90	-0.24	-2.4	9.82	-0.32	-3.2	10.01	-0.13	-1.3
Fuel Economy FTP 1/100 km (mpg)	16.12 (14.6)	16.0 (14.7)	-0.12 (+0.1)	-0.7 (+0.7)	16.38 (14.37)	+0.26 (-0.23)	+1.6 (-1.6)	17.16 (13.71)	+1.04 (-0.89)	+6.5 (-6.1)	17.20 (13.67)	+1.08 (-0.93)	+6.7 (-6.4)
Highway 1/100 km (mpg)	11.87 (19.83)	11.6 (20.36)	-0.27 (+0.53)	-2.3 (+2.7)	11.81 (19.91)	-0.06 (+0.08)	-0.5 (+0.4)	12.21 (19.27)	+0.34 (-0.56)	-2.9 (-2.8)	12.16 (19.34)	+0.29 (-0.49)	+2.4 (-2.5)
Emissions, HC, gm/km (gm/m1)	0.47 (0.75)	0.46 (0.74)	-0.01 (-0.01)	-1.3 (-1.3)	0.45 (0.73)	-0.02 (-0.02)	-2.7 (-2.7)	0.50 (0.81)	+0.04 (+0.06)	+8.0 (+8.0)	0.42 (0.68)	~0.04 (~0.07)	-9.3 (-9.3)
CO, gm/km (gm/mi)	4.73 (7.6)	4.12 (6.64)	-0.61 (-0.96)	-12.6 (-12.6)	5.92 (9.52)	+1.19 (+1.92)	+25.3 (+25.3)	7.31 (11.77)	+2.59 (+4.17)	+54.8 (+54.8)	4.68 (7.53)	-0.04 (-0.07)	-0.9 (-0.9)
NOx, gm/km (gm/m1)	1.25 (2.0)	4.7 (7.6)	+3.45 (+5.6)	+280 (+280)	1.19 (1.91)	-0.06 (-0.04)	-4.5 (-4.5)	1.66 (2.67)	+0.42 (+0.67)	+33.5 (+33.5)	1.45 (2.33)	+0.21 (+0.33)	+16.5 (+16.5)

 $<sup>^{1}</sup>$  Difference between value for respective modification and base (- decrease, + increase)

 $<sup>^{2}</sup>$  Percent change between respective modification and base (- decrease, +increase)

TABLE A-10

PERFORMANCE OF 1977 OLDSMOBILE 98

6.6 LITER (403 CU. IN.), 4-BBL. FEDERAL CALIBRATION

	Base		connect Edification			e 2 Notche Rich fication		P1u	t Idle s 150 rpm ification 	3 % 2	Fast Idl	Notches File + 150 r	c pm
CRC Driveability Demerits	84	93	+9	+10.7	61	-23	-27.4	88	+4	+4.8	39	-45	-53.6
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	9.72	9.67	-0.05	-0.5	9.82	+0.1	+1.0	9.72	0	0	9.88	+0.16	+1.6
Fuel Economy FTP 1/100 km (mpg)	16.49	16.55	+0.06	+0.4	16.29	-0.2	-1.2	16.06	-0.43	-2.6	16.32	-0.17	-1.0
	(14.26)	(14.21)	(-0.05)	(-0.4)	(14.44)	(+0.18)	(+1.3)	(14.65)	(+0.39)	(+2.7)	(14.41)	(+0.15)	(+1.1)
Highway 1/100 km (mpg)	12.06	12.01	-0.05	-0.4	11.59	-0.47	-3.9	11.13	-0.93	-7.7	11.56	-0.5	-4.1
	(19.50)	(19.58)	(+0.08)	(+0.4)	(20.29)	(+0.79)	(+4.1)	(21.13)	(+1.63)	(+8.4)	(20.35)	(÷0.85)	(+4.4)
Emissions, HC, gm/km (gm/mi)	0.51 (0.82)	0.58 (0.93)	+0.07 (+0.11)	+13.4 (+13.4)	0.53 (0.85)	+0.02 (+0.03)	+3.7 (+3.7)	0.47 (0.75)	-0.04 (-0.07)	<del>-</del> 8.5 (-8.5)	0.44 (0.71)	-0.07 (-0.11)	-13.4 (-13.4)
CO, gm/km	4.65	4.51	-0.14	-2.9	5.31	+0.66	+14.2	3.80	-0.85	-18.2	4.84	+0.19	+4.1
(gm/mi)	(7.48)	(7.26)	(-0.22)	(-2.9)	(8.54)	(+1.06)	(+14.2)	(6.12)	(-1.36)	(-18.2)	(7.79)	(+0.31)	(+4.1)
NOx, gm/km (gm/mi)	1.59	5.16	+3.57	+224	1.40	-0.19	-12.1	1.28	-0.31	-19.5	1.21	-0.38	-24.2
	(2.56)	(8.30)	(+5.74)	(+224)	(2.25)	(-0.31)	(-12.1)	(2.06)	(-0.5)	(-19.5)	(1.94)	(-0.62)	(-24.2)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-11

PERFORMANCE OF 1977 FORD PINTO

2.3 LITER (140 CU. IN.) 2-BBL, FEDERAL CALIBRATION

	Base		sconnect E lification \( \rightarrow 1			e Timing fication			le CO @ 2% ification	3 2 2	Incr.	Idle 120 fication	
CRC Driveability Demerits	154	152	-2	-1.3	115	-39	-25.3	93	-61	-39.6	137	-17	-11.0
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	14.0	13.2	-0.8	-5.7	12.5	-1.5	-10.7	13.1	-0.9	-6.4	13.2	-0.8	-5.7
Fuel Economy FTP 1/100 km (mpg)	12.7	12.0	-0.7	-5.7	11.67	-1.03	-8.1	12.21	-0.49	-3.9	12.51	-0,19	-1.5
	(18.54)	(19.67)	(+1.13)	(+6.1)	(20.15)	(+1.61)	(+8.7)	(19.27)	(+0.72)	(+3.9)	(18.80)	(+0,26)	(+1.4)
Highway 1/100 km (mpg)	9.6	8.8	-0.8	-8.0	8.95	-0.65	-6.8	8.97	-0.63	-6.6	9.39	-0.21	-2.2
	(24.46)	(26.60)	(+2.14)	(+8.8)	(26.27)	(+1.81)	(+7.4)	(26.22)	(+1.76)	(+7.2)	(25.06)	(+0.60)	(+2.5)
Emissions, HC, gm/km (gm/mi)	0.54	0.55	+0.01	+2.3	0.53	-0.01	-1.1	0.92	+0.38	+70.1	0.81	+0.27	+49.4
	(0.87)	(0.89)	(+0.02)	(+2.3)	(0.86)	(-0.01)	(-1.1)	(1.48)	(+0.61)	(+70.1)	(1.30)	(+0.43)	(+49.4)
CO, gm/km	9.48	10.04	+0.56	+5.8	7.70	-1.78	-18.8	18.08	+8.60	+90.7	16.77	+7.29	+76.9
(gm/mi)	(15.26)	(16.15)	(+0.89)	(+5.8)	(12.39)	(-2.87)	(-18.8)	(29.10)	(+13.84)	(+90.7)	(26.99)	(+11.13)	(+76.9)
NOx, gm/km	0.90	2.57	+1.67	+185.5	1.19	+0.29	+31.7	0.89	-0.01	-1.4	0.86	-0.04	-4.3
(gm/mi)	(1.45)	(4.14)	(+2.69)	(+185.5)	(1.91)	(+0.46)	(+31.7)	(1.43)	(-0.02)	(-1.4)	(1.39)	(-0.06)	(-4.3)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-12
PERFORMANCE OF 1977 FORD MAVERICK

## 4.1 LITER (250 CU. IN.), 1-BBL - FEDERAL CALIBRATION

	Base		sconnect E ification			Timing 6 ication 2	。 <sub>%</sub> 2		lle CO @ 1% iification		Advan	e CO @ 1% ce Timing .fication	
CRC Driveability Demerits	160	128	-32	~20	97	-63	-39.4	145	-15	-9.4	152	-8	-5.0
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	12.9	12.6	-0.3	-2.3	12.3	-0.6	-4.7	12.1	-0.8	-6.2	12.3	-0.6	-4.7
Fuel Economy FTP 1/100 km (mpg)	13.9 (16.91)	13.7 (17.12)	-0.2 (+0.21)	-1.0 (+1.24)	13.29 (17.70)	-0.61 (+0.79)	-4.4 (+4.7)	13.60 (17.29)	-0.30 (+0.38)	-2.2 (+2.2)	13.93 (16.88)	+0.03 (-0.03)	+0.2 (-0.2)
Highway 1/100 km (mpg)	10.6 (22.20)	10.8 (21.72)	+0.2 (-0.48)	+2.2 (-2.16)	10.33 (22.76)	-0.27 (+0.56)	-2.5 (+2.5)	10.27 (22.90)	-0.33 (+0.70)	-3.1 (+3.2)	10.64 (22.10)	+0.04 (-0.10)	+0.4 (-0.5)
Emissions, HC, gm/km (gm/mi)	1.09 (1.75)	0.82 (1.32)	-0.27 (0.43)	-25.6 (-25.6)	1.09 (1.75)	0 (0)	0 (0)	1.54 (2.48)	+0.46 (+4.73)	+41.7 (+41.7)	1.78 (2.86)	+0.69 (+1.11)	+63.4 (+63.4)
CO, gm/km (gm/mi)	8.02 (12.91)	8.15 (13.11)		+1.55 )(+1.55)	7.71 (12.40)	-0.31 (-0.51)	-4.0 (-4.0)	13.41 (21.57)	+5.39 (+8.66)	+67.2 (+67.1)	13.54 (21.79)	+5.52 (+8.88)	+68.8 (+68.8)
NOx, gm/km (gm/mi)	0.90 (1.45)	4.77 (7.68)	+3.87 (+6.23	+430 ) (+430)	1.19 (1.91)	+0.29 (+0.46)	31.7 (+31.7)	0.93 (1.50)	+0.03 (+0.05)	+3.4 (+3.4)	1.07 (1.73)	+0.17· (+0.28)	+19.3 (+19.3)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-13

PERFORMANCE OF 1977 FORD MAVERICK

4.1 LITER (250 CU. IN.), 1-BBL. CALIFORNIA CALIBRATION

	* Base		sconnect E lification \$\triangle 1			Notches Leafication 2		Choke 2	Notches Lification	ean		e CO @ 0. ification 	
CRC Driveability Demerits	115	51	-64	-55.7	53	-62	-53.9	47	-68	-59.1	-	-	-
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	15.5	15.0	-0.5	-3.2	15.6	+0.1	+0.6	15.4	-0.1	-0.6	15.45	-0.05	-0.3
Fuel Economy FTP 1/100 km (mpg)	16.18 (14.54)	15.03 (15.65)	-1.15 (+1.11)	-7.1 (+7.6)	16.12 (14.59)	-0.06 (+0.05)	-0.4 (+0.3)	15.22 (15.45)	-0.96 (+0.91)	-5.9 (+6.3)	16.12 (14.59)	-0.06 (+0.05)	-0.4 (+0.3)
Highway 1/100 km (mpg)	12.94 (18.17)	11.97 (19.65)	-0.97 (+1.48)	-7.5 (+8.1)	12.85 (18.30)	-0.09 (+0.13)	-0.7 (+0.7)	11.81 (19.91)	-1.13 (+1.74)	-8.7 (+9.6)	13.05 (18.02)	+0.11 (-0.15)	+0.01 (-0.01)
Emissions, HC, gm/km (gm/mi)	0.55 (0.89)	0.46 (0.74)	-0.09 (-0.15)	-16.9 (-16.9)	0.49 (0.79)	-0.06 (-0.1)	-11.2 (-11.2)	0.43 (0.70)	-0.12 (-0.19)	-21.3 (-21.3)	0.55 (0.88)	0 (-0.01)	0 (-0.01)
CO, gm/km (gm/mi)	7.37 (11.86)	5.29 (8.52)	-2.08 (-3.34)	-28.2 (-28.2)	5.64 (9.07)	-1.73 (-2.79)	-23.5 (-23.5)	7.57 (12.18)	+0.20 (+0.32)	+2.7 (+2.7)	11.43 (18.40)	+4.06 (+6.54)	+55.1 (+55.1)
NOx, gm/km (gm/mi)	0.80 (1.28)	4.09 (6.58)	+3.29 (+5.3)	+414 (+414)	0.78 (1.25)	-0.02 (-0.03)	-2.3 (-2.3)	2.38 (3.83)	+1.58 (+2.55)	+199 (+199)	(0.62) (1.00)		(-22.5) (-22.0)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

<sup>\*</sup> Idle CO @ 3.2% w/o exhaust manifold air injection.

<sup>\*\*</sup> Single run.

TABLE A-14
PERFORMANCE OF 1977 FORD CRANADA

## 4.9 LITER (302 CU. IN.) 2-BBL. FEDERAL CALIBRATION

		Disconne	et EGR	Choke	3 Notches	Rich	Idle	CO @ 2%			0 0 2%	•
	Base	Modifica	tion 1	2 Modi	fication, 2	- <u>•/6</u> 2	Mod1f:	ication <sub>1</sub> 3	% <sup>2</sup>		Timing 4°	- 1/0 2
CRC Driveability Demerits	83	48	-35 -42.	2 47	-36	-43.4	123	+40	+48.2	86	+3	+3.6
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	11.07	10.91 -	).16 <b>-1.</b>		-0.11	-1.0	11.31	+0.24	+2.2	11.80	+0.73	+6.6
Fuel Economy FTP 1/100 km (mpg)	16.54 (14.22)		).18 +0. ).15) (-0.		+0.31	+1,9 (-1.8)	16,99 (13.84)	+0,45 (-0.38)	+2.7 (-2.7)	17.98 (13.08)	+1.44	÷8.7 (-8.0)
Highway 1/100 km (mpg)	12.26 (19.19)		).59 +4. ).88) (-4.		+0.17 (-0.27)	+1.4 (-1.4)	12.64 (18.61)	+0.38 (0.58)	÷3.1 (-3.0)	13.36 (17.61)	+1.10 (-1.58)	+9.0 (-8.2)
Emissions,  HC, gm/km  (gm/mi)	1.14 (1.84)	1.01 -0. (1.63) (-0.		1.17	+0.03 (+0.04)	+2.2 (+2.2)	0.78 (1.26)	-0.36 (-0.58)	-31.5 (-31.5)	0.77 (1.24)	-0.37 (-0.60)	-32.6 (-32.6)
CO, gm/km (gm/mi)	4.62 (7.43)	4.76 +0. (7.65) (+0.		4.89 (7.87)	+0.27 (+0.44)	+5.9 (+5.9)	5.26 (8.47)	+0.64 (+1.04)	+14.0 (+14.0)	6.65 (10.7)	+2.03 (+3.27)	+44.0 (÷44.0)
NOx, gm/km (gm/mi)	1.27 (2.03)	4.45 +3. (7.15) (+5.		1.39 (2.23)	+0.12 (+0.20)	+9.9 (+9.9)	0.98 (1.58)	-0.29 (-0.45)	-22.2 (-22.2)	0.91 (1.47)	-0.36 (-0.56)	-27.6 (-27.6)

<sup>1</sup> Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (~ decrease, + increase)

TABLE A-15

PERFORMANCE OF 1977 FORD GRANADA

4.9 LITER (302 CU. IN.), 2-BBL., VARIABLE VENTURI - CALIFORNIA CALIBRATION

			connect E			Fiming 4° ication 2	, <sub>w</sub> 2		CO @ 2%	3 % 2	Decreas	e CO @ 2% e Idle 50 fication 4	
	Base	<del></del>			<del></del>		<u></u>						
CRC Driveability Demerits	150	4	-146	-97.3	45	-105	-70.0	63	-87	~58	35	-115	-76.7
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	11.4	11.6	+0.2	+1.8	13.0	+1.6	+14.0	11.2	-0.2	-1.8	11.4	0	0
Fuel Economy FTP 1/100 km (mpg)	19.3 (12.18)	18.0 (13.05)	-1.3 (+0.87)	-6.7 (+7.1)	20.52 (11.46)	+1.22 (-0.72)	+6.3 (-5.9)	18.92 (12.43)	-0.38 (+0.25)	-2.0 (+2.1)	18.62 (12.63)	-0.68 (+0.45)	-3.5 (+3.7)
Highway 1/100 km (mpg)	13.5 (17.46)	12.9 (18.28)	-0.6 (+0.82)	-4.4 (+4.7)	14.25 (16.51)	+0.75 (-0.95)	+5.6 (-5.4)	13.08 (17.98)	-0.42 (+0.52)	-3.1 (+3.0)	13.68 (17.19)	+0.18 (-0.27)	+1.3 (-1.5)
Emissions, HC, gm/km	0.46	0.58	+0.12	+25.7	0.43	-0.03	-5.4	0.45	-0.01	-1.4	0.45	-0.01	~2.7
(gm/mi)	(0.74)	(0.93)	(+0.19)	(+25.7)	(0.70)	(-0.04)	(-5.4)	(0.73)	(-0.01)	(-1.4)	(0.72)	(-0.02)	(~2.7)
CO, gm/km (gm/mi)	3.04 (4.90)	2.35 (3.79)	-0.69 (-1.11)	-22.7 (-22.7)	2.85 (4.58)	-0.19 (-0.32)	-6.5 (-6.5)	2.72 (4.38)	-0.32 (-0.52)	-10.6 (-10.6)	2.65 (4.26)	-0.30 (-0.64)	-13.1 (-13.1)
NOx, gm/km (gm/mi)	0.70 (1.12)	2.13 (3.43)	+1.43 (+2.31)	+206.3 (+206.3)	0.69 (1.10)	-0.01 (-0.02)	-1.8 (-1.8)	0.65 (1.04)	-0.05 (-0.08)	-7.1 (-7.1)	0.63 (1.02)	-0.07 (-0.10)	-10.0 (-10.0)

<sup>1</sup> Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-16

PERFORMANCE OF 1977 FORD LTD II

5.8 LITER (351 CU. IN.) 2-BBL., FEDERAL CALIBRATION

	_		sconnect E			ice Timi	. 2		Idle 10 $\Delta^{1}$		Adva Dec Modi	ince Timi Idle 75 ification	ng 4° (3)
	Base		<u> </u>	0/0		Δ	<b>%</b> <sup>2</sup>						
CRC Driveability Demerits	211	126	-85	-40.3	237	+26	+12.3	243	+32	+15.2	223	+12	+5.7
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	10.4	10.45	+0.05	+0.5	10.08	-0.32	-3.1	10.42	+0.02	+0.2	10.14	-0.26	-2.5
Fuel Economy FTP 1/100 km (mpg)	17.07 (13.79)	17.34 (13.57)	+0.27 (-0.22)	+1.6 (-1.6)	· · ·	+0.37 -0.30)	+2.2 (-2.2)	17.53 (13.42)	+0.46 (-0.37)	+2.7 (-2.7)	17.50 (13.44)	+0.43 (-0.35)	+2.5 (-2.5)
Highway 1/100 km (mpg)	12.25 (19.21)	12.6 (18.7)	+0.35 (-0.51)	+2.9 (-2.7)		+0.56 -0.85)	+4.6 (-4.4)	13.30 (17.68)	+1.05 (-1.53)	+8.6 (-8.0)	13.18 (17.85)	+0.93 (-1.36)	+7.6 (-7.1)
Emissions,  HC, gm/km (gm/mi)	0.79 (1.27)	0.75 (1.20)	-0.04 (-0.07)	-5.5 (-5.5)	0.75 - (1.21) (-	-0.04 -0.06)	-4.7 (-4.7)	0.87 (1.40)	+0.08 (+0.13)	+10.2 (+10.2)	0.91 (1.46)	+0.12 (-0.19)	+15.0 (+15.0)
CO, gm/km (gm/mi)	6.42 (10.32)	6.64 (10.67)	+0.22 (+0.35)	+3.4 (+3.4)		-0.04 -0.05)	-0.5 (-0.5)	8.87 (14.27)	+2.45 (+3.95)	+38.3 (+38.3)	8.43 (13.56)	+2.01 (+3.24)	+31.4 (+31.4)
NOx, gm/km (gm/mi)	1.5 (2.42)	5.24 (8.42)	+3.74 (+6.0)	+248 (+248)	1.75 - (2.81) (-	+0.25 +0.39)	+16.1 (+16.1)	1.22 (1.97)	-0.28 (-0.45)	-18.6 (-18.6)	1.78 (2.87)	+0.28 (+0.45)	+18.6 (+18.6)

<sup>1</sup> Difference between value for respective modification and base (-decrease, + increase)

 $<sup>^{2}</sup>$  Percent change between respective modification and base (- decrease, + increase)

<sup>&</sup>lt;sup>3</sup> EPa originally specified a 100 to 150 rpm reduction in idle speed; however, a 75 rpm reduction was the largest reduction possible to maintain a stall-free idle.

TABLE A-17
PERFORMANCE OF 1977 PLYMOUTH VOLARE

## 3.7 LITER (225 CU. IN.), 1-BBL., FEDERAL CALIBRATION

	Base		onnect EG			e Timing 6 fication 2	· 7. 2		CO @ 4% fication 3	% 2	Idle	dle 120 r co @ 4% fication 4	•
CRC Driveability Demerits	238	156	-82	~34.5	211	-27	-11.3	363	+125	+52.5	353	+115	+48.3
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	14.4	13.9	-0.5	-3.5	14.1	-0.3	-2.1	14.0	-0.4	-2.8	14.5	+0.1	+0.7
Fuel Economy FTP 1/100 km (mpg)	14.4 (16.32)	13.0 (18.07)	-1.4 (+1.75)	-9.7 (+10.7)	13.48 (17.45)	-0.92 (+1.13)	-6.4 (+6.9)	13.80 (17.04)	-0.6 (+0.72)	-4.2 (+4.4)	14.45 (16.28)	+0.05 (-0.04)	+0.3 (-0.2)
Highway 1/100 km (mpg)	11.1 (21.21)	9.9 (23.78)	-1.2 (+2.57)	~10.8 (+12.1)	10.47 (22.47)	-0.63 (+1.26	-5.7 (+5.9)	10.55 (22.29)	-0.55 (+1.08)	-5.0 (+5.1)	10.79 (21.79)	-0.31 (+0.58)	-2.8 (+2.7)
Emissions, HC, gm/km (gm/mi)	0.83 (1.34)	0.90 (1.45)	+0.07 (+0.11)	+3.2 (+8.2)	0.75 (1.21)	-0.08 (-0.13)	-9.7 (-9.7)	1.26 (2.02)	+0.43 (+0.68)	+50.7 (+50.7)	1.29 (2.07)	+0.46 (+0.73)	+54.5 (+54.5)
CO, gm/km (gm/mi)	6.76 (10.88)	7.18 (11.56)	+0.42 (+0.68)	+6.3 (+6.3)	5.76 (9.27)	-1.0 (-1.61)	-14.8 (-14.8)	12.53 (20.17)	+5.77 (+9.29)	+85.4 (+85.4)	15.52 (24.98)	+8.76 (+14.1)	+129.6 (+129.6)
NOx, gm/km (gm/mi)	1.12 (1.80)	3.94 (6.34)	+2.82 (4.54)	+252.2 (+252.2)	1.21 (1.95)	+0.9 (+0.15)	+8.3 (+8.3)	1.03 (1.66)	-0.09 (-0.14)	-7.8 (-7.8)	0.98 (1.57)	-0.14 (-0.23)	-12.8 (-12.8)

<sup>1</sup> Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-18

PERFORMANCE OF 1977 PLYMOUTH VOLARE

5.2 LITER (318 CU.IN.,) 2-BBL., FEDERAL CALIBRATION

	Base		sconnect E0			dle 250 ry ication 2			e CO @ 1 ification		Incr.	le CO € 1% Idle 250 Ification Δ 1	rpm
CRC Driveability Demerits	244	195	-49	-20.1	226	-18	<b>-7.4</b>	251	+7	+2.9	234	-10	-4
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	10.05	9.83	-0.22	-2.2	10.05	0	0	10.02	-0.03	-0.3	9.97	-0.03	<b>-</b> C
Fuel Economy FTP 1/100 km (mpg)	18.62	17.44	-1.18	-6.3	19.72	+1.1	+5.9	19.41	+0.79	+4.2	20.22	+1.6	3 <b>+</b>
	(12.65)	(13.49)	(+0.84)	(+6.6)	(11.93)	(-0.72)	(-5.7)	(12.12)	(-0.53)	(-4.2)	(11.63)	(-1.02)	8-)
Highway 1/100 km (mpg)	13.24	12.56	-0.68	~5.1	13.52	+0.28	+2.1	13.46	+0.22	+1.7	13.60	+0.36	+2
	(17.79)	(18.73)	(+0.94)	(+5.3)	(17.4)	(-0.39)	(-2.2)	(17.47)	(-0.32)	-1.8	(17.3)	(-0.49)	(-2
Emissions, HC, gm/km (gm/mi)	0.63 (1.02)	0.55 (0.89)	-0.08 (-0.13)	12.7 (-12.7)	0.57 (0.92)	-0.06 (-0.1)	-9.8 (-9.8)	0.93 (1.49)	+0,3 (+0.47)	+46.1 (+46.1)	0.87 (1.4)	+0.24 (+0.38)	+37 (+37
CO, gm/km (gm/mi)	7.23	7.73	+0.5	+6.9	9.03	+1.8	+24.9	14.25	+7.02	+97.2	15.25	+8.02	+]
	(11.63)	(12.43)	(+0.8)	(+6.9)	(14.53)	(+2.9)	(+24.9)	(22.74)	(+11.31)	(+97.2)	(24.54)	(12.91)	(+)
NOx, gm/km	0.89	1.65	+0.77	+85	0.93	+0.04	+4.2		+0.07	+8.4	1.00	+0.11	+1;
(gm/mi)	(1.43)	(2.65)	(+1.22)	(+85)	(1.49)	(+0.06)	(+4.2)		(+0.12)	(+8.4)	(1.61)	(+0.18)	(+1;

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

(gm/mi)

TABLE A-19
PERFORMANCE OF 1977 PLYMOUTH VOLARE

5.2 LITER (318 CU. IN.) 2-BBL. - CALIFORNIA CALIBRATION Idle CO @ 2% Retard timing 5° Modification 4 Idle CO @ 2% Disconnect EGR Disconnect Choke Heater Modification 3 Modification 1 Modification 2 <sub>76</sub> 2 <sub>7</sub> 2 <sub>%</sub> 2 <sub>72</sub> 2  $\Delta$  1  $\Delta 1$  $\Delta^{1}$  $\Delta$  1 Base CRC Driveability 136 Demerits 269 -133-49.4 259 -10 -3.7211 -58 -21.6308 +39 +14.5 Acceleration, sec. 11.8 11.8 0 0 16.1 to 96.6 km/h 11.6 -0.2 -1.7 11.8 0 0 12.9 +1.1 +9.3 (10 to 60 mph) Fuel Economy FTP 1/100 km 22.25 20.17 -2.08 -93 -3.421.50 -0.75-3.423.90 +1.65 +7.4 21.50 -0.75(10.57)(11.66)(+1.09)(+10.3)(+0.37)(+3.5)(9.84)(-0.73)(-6.9)(mpg) (10.94)(+0.37)(+3.5)(10.94)15.19 13.07 -2.12-14.0 -0.6 -0.7 16.22 +1.03 +6.8 Highway 1/100 km 15.10 -0.09 -0.10 15.09 (15.48)(17.99)(+2.51)(+16.2)(-0.95)(-6.3)(mpg) (15.58)(+0.10)(+0.6)(+0.11)(+0.7)(14.5)(15.59)Emissions. +0.05 0.34 0.29 0.22 -0.07 -23.4 0.23 -0.06 -21.3+17.0 0.36 +0.07 +23.4 HC, gm/km (+0.08)(0.47)(0.36)(0.55)(-0.11)(-23.4)(0.37)(-0.1)(-21,3)(+17.0)(0.58)(+0.11)(+23.4)(gm/mi) 2.06 1.63 -0.43-20.81.93 -0.13-6.32.21 CO, gm/km +0.15 +6.9 (+6.9) 4.82 +2.76 +133 (3.32)(2.63)(-0.69)(-20.8)(3.11)(-0.21)(-6.3)(3.55)(gm/mi) (+0.23)(7.75)(+4.43)(+133)NOx, gm/km 1.17 1.86 +0.69 +59.6 -0.16 -13.3-0.13-0.16 -13.3 1.01 1.04 -11.21.01

(-0.25)

(1.63)

(-13.3)

(-0.21)

(-11.2)

(1.63)

(1.67)

(-13.3)

(0.25)

(+1.12)

(+59.6)

(3.0)

(1.88)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-20
PERFORMANCE OF 1977 CHRYSLER CORDOBA

6.6 LITER (400 CU. IN.) 4-BBL. CARB., LEAN BURN, FEDERAL CALIBRATION

	Base	Disconnect El Choke Modificatio	n 1	Advance Timing Modification		Idle CO @ .75% Modification		Idle CO @ .75% Incr. Idle 125 rpm Modification 4	<sub>%</sub> 2
CRC Driveability Demerits	185	165 –20	-10.8	177 -8	-4.3	213 +28	+15.1	193 8	+4.3
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	9.7	9.86 +0.16	+1.6	9.12 -0.58	-6.0	9.85 +0.15	+1.5	9.67 -0.03	-0.3
Fuel Economy FTP 1/100 km (mpg)	20.7	21.83 +1.13	+5.5	21.21 +0.51	+2.5	21.52 +0.82	+4.0	22.21 +1.51	+7.3
	(11.36)	(10.78) (-0.58)	(-5.1)	(11.09) (-0.27)	(-2.4)	(10.93) (-0.43)	(-3.8)	(10.59) (-0.77)	(-6.8)
Highway 1/100 km (mpg)	13.63	13.88 +0.25	+1.8	13.30 -0.33	-2.4	13.29 -0.34	-2.5	14.24 +0.61	+4.5
	(17.26)	(16.95) (-0.31)	(-1.8)	(17.68) (+0.42)	(+2.4)	(17.7) (+0.44)	(+2.5)	(16.52) (-0.74)	(-4.3)
Emissions, HC, gm/km (gm/mi)	0.42 (0.68)	0.40 -0.02 (0.65) (-0.03)	-4.4 (-4.4)	0.45 +0.03 (0.72) (+0.04)	+5.9 (+5.9)	0.98 +0.56 (1.57) (+0.89)	+131 (+131)	1.01 +0.59 (1.63) (+0.95)	+140 (+140)
CO, gm/km	3.63	5.23 +1.6	+44.4	3.88 +0.25	+7.0	18.00 +14.37	+397	21.31 +17.68	+488
(gm/mi)	(5.83)	(8.42) (+2.59)	(+44.4)	(6.24) (-0.41)	(+7.0)	(28.97) (+23.14)	(+397)	(34.3) (+28.47)	(+488)
NOx, gm/km	1.07	1.18 +0.11	+10.5	1.26 +0.19	+18.0	1.06 -0.01	-1.2	1.20 +0.13 (1.93) (+0.21)	+12.2
(gm/mi)	(1.72)	(1.90) (+0.18)	(+10.5)	(2.03) (+0.31)	(+18.0)	(1.70) (-0.02)	(-1.2)		(+12.2)

 $<sup>^{</sup>m 1}$  Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-21
PERFORMANCE OF 1978 AMC CONCORD

4.2 LITER (258 CU. IN.), 1-BBL., CALIFORNIA CALIBRATION

	Page		connect EG ification		Reta Modi	rd Spark 3 fication 2	3° 2 % 2	Id1 Mod	e CO @ 2% ification	3 % 2	Choke	e CO @ 2% 2 Notches ification 	
CRC Driveability	Base						+36.4	127	+6	+5.0	106	-15	-12.4
Demerits	121	34	-87	-71.9	165	+44	+30.4	147	10	1310			
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	17.43	12.78	-4.65	-26.7	18.4	+0.97	+5.6	16.88	-0.55	-3.2	17.98	+0.55	+3.2
Fuel Economy FTP 1/100 km (mpg)	17.83 (13.19)	15.41 (15.26)	-2.42 (2.07)	-13.6 (+15.7)	19.65 (11.97)	+1.82 (-1.22)	+10.2 (-9.2)	17.79 (13.22)	-0.04 (+0.03)	-0.2 (+0.2)	17.01 (13.83)	-0.82 (+0.64)	-4.6 (+4.9)
Highway 1/100 km (mpg)	15.00 (15.68)	11.68 (20.14)	-3.32 (+4.46)	-22.1 (+28.4)	15.94 (14.76)	+0.94 (-0.92)	+6.3 (-5.9)	14.49 (16.23)	-0.51 (+0.55)	-3.4 (+3.5)	14.32 (16.43)	-0.68 (+0.75)	-4.5 (+4.8)
Emissions, HC, gm/km (gm/mi)	0.19 (0.31)	0.14 (0.23)	-0.05 (-0.08)	-25.8 (-25.8)	0.21 (0.33)	+0.02 (+0.02)	+6.5 (+6.5)	0.19 (0.30)	0 (-0.01)	-3.2 (-3.2)	0.27 (0.43)	+0.08 (+0.12)	+38.7 (+38.7)
CO, gm/km (gm/mi)	3.46 (5.57)	1.92 (3.09)	-1.54 (-2.48)	-44.5 (-44.5)	5.59 (9.00)	+2.13 (+3.43)	+61.6 (+61.6)	3.47 (5.59)	+0.01 (+0.02)	+0.4 (+0.4)	6.34 (10.21)	+2.88 (+4.64)	+83.3 (+83.3)
NOx, gm/km (gm/mi)	0.69 (1.11)	2.63 (4.23)	+1.94 (+3.12)	+281 (+281)	0.60 (0.96)	-0.09 (-0.15)	-13.5 (-13,5)	0.60 (0.97)	-0.09 (-0.14)	-12.6 (-12.6)	0.54 (0.87)	-0.15 (-0.24)	-21.6 (-21.6)

Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-22

PERFORMANCE OF 1978 TOYOTA COROLLA

1.6 LITER (97 CU. IN.), 2-BBL. FEDERAL CALIBRATION

	Base	Retard Spark 4° Modification 1  1 2 2		Dec. Fast Idle 200 rpm Modification 2			Idle CO @ 1% Modification 3			Dec. Fast Idle 200 rpm Idle CO @ 1% Modification 4  1			
CRC Driveability Demerits	12	12	0	0	6	-6	<b>~</b> 50	14	+2	+16.7	0	-12	-100
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	13.0	13.4	+0.4	+3.1	12.8	-0.2	-1.5	13.1	+0.1	+0.8	13.0	0	0
Fuel Economy FTP 1/100 km (mpg)	10.65 (22.09)	10.31 (22.81)	-0.34 (+0.72)	-3.2 (+3.3)	9.96 (23.61)	-0.69 (+1.52)	-6.5 (+6.9)	10.83 (21.71)	+0.18 (-0.38)	+1.7 (-1.7)	10.53 (22.33)	-0.12 (+0.24)	-1.1 (+1.1)
Highway 1/100 km (mpg)	8.52 (27.62)	8.49 (27.72)	-0.03 (+0.1)	-0.4 (+0.4)	8.48 (27.75)	-0.04 (+0.13)	-0.5 (+0.5)	8.95 (26.29)	+0.43 (-1.33)	+5.0 (-4.8)	8.58 (27.41)	+0.06 (-0.21)	+0.7 (-0.8)
Emissions, HC, gm/km (gm/mi)	0.45 (0.72)	0.42 (0.67)	-0.03 (-0.05)	-6.9 (-6.9)	0.42 (0.67)	-0.03 (-0.05)	-6.9 (-6.9)	0.46 (0.74)	+0.01 (+0.02)	+2.8 (+2.8)	0.49 (0.79)	+0.04 (+0.07)	+9.7 (+9.7)
CO, gm/km (gm/m1)	6.19 (9.96)	6.04 (9.72)	-0.15 (-0.24)	-2.4 (-2.4)	4.98 (8.02)	-1.21 (-1.94)	-19.5 (-19.5)	8.25 (13.28)	+2.06 (+3.32)	+33.3 (+33.3)	8.12 (13.06)	+1.93 (+3.1)	+31.1 (+31.1)
NOx, gm/km (gm/mi)	1.15 (1.85)	0.99 (1.59)	-0.16 (-0.26)	-14.1 (-14.1)	1.30 (2.10)	+0.15 (+0.25)	+13.5 (+13.5)	1.09 (1.76)	-0.06 (-0.09)	-4.9 (-4.9)	1.00 (1.61)	-0.15 (-0.24)	-13.0 (-13.0)

<sup>1</sup> Difference between value for respective modification and base (- decrease, + increase)

Percent change between respective modification and base (- decrease, + increase)

TABLE A-23

PERFORMANCE OF 1978 VOLVO 245-DL

2.1 LITER (130 CU. IN.) FUEL INJECTION - CALIFORNIA CALIBRATION

	Base	Disconnect O <sub>2</sub> Sensor Modification 1 \[ \Delta \ 1 \ \ \ \ \ \ \ 7 \ 2			Adv. Ignition Timing 5° Modification 2 \times 1 \times 2			Idle CO @ 4% Modification 3  \$\triangle \frac{1}{2} \frac{\pi}{\pi} \frac{2}{2}			Combine 1, 2, 3 Modification 4 $\Delta$ 1 $\chi$ 2		
CRC Driveability Demerits	17	16	-1	-5.9	23	+6	+35.3	26	+9	+52.9	18 +1	+5.9	
Acceleration, sec. 16.1 to 96.6 km/h (10 to 60 mph)	14.0	14.2	+0.2	+1.4	13.8	-0.2	-1.4	14.3	+0.3	+2.1	13.7 -0.3	-2.1	
Fuel Economy FTP 1/100 km (mpg)	12.58 (18.70)	12.85 (18.31)	+0.27 (-0.39)	+2.1 (-2.1)	12.65 (18.59)	+0.07 (-0.11)	+0.6 (-0.6)	12.85 (18.31)	+0.27 (-0.39)	+2.1 (-2.1)	12.99 +0.41 (18.10) (-0.6)	+3.3 (-3.2)	
Highway 1/100 km (mpg)	9.27 (25.36)	9.75 (24.12)	+0.48 (-1.24)	+5.2 (-4.9)	9.85 (23.89)	+0.58 (-1.47)	+6.3 (-5.8)	9.79 (24.02)	+0.52 (-1.34)	+5.6 (-5.3)	9.89 +0.62 (23.79) (-1.57)	+6.7 (-6.2)	
Emissions, HC, gm/km (gm/mi)	0.20 (0.32)	0.32 (0.51)	+0.12 (+0.19)	+59.4 (+59.4)	0.19 (0.30)	-0.01 (-0.02)	-6.3 (-6.3)	0.19 (0.31)	-0.01 (-0.01)	-3.1 (-3.1)	1.06 +0.86 (1.70) (+1.38)	+431 (+431)	
CO, gm/km (gm/mi)	2.04 (3.28)	5.97 (9.60)	+3.93 (+6.32)	+193 (+193)	2.39 (3.84)	+0.35 (+0.56)	+17.1 (+17.1)	2.42 (3.90)	+0.38 (+0.62)	+18.9 (+18.9)	26.70 +24.66 (42.97) (+39.69)	+1210 (+1210)	
NOx, gm/km (gm/mi)	0.42 (0.67)	1.02 (1.64)	+0.6 (+0.97)	+145 (+145)	0.47 (0.76)	+0.05 (+0.09)	+13.4 (+13.4)	0.59 (0.95)	+0.17 (+0.28)	+41.8 (+41.8)	0.43 +0.01 (0.70) (+0.03)	+4.5 (+4.5)	

Difference between value for respective modification and base (- decrease, + increase)

 $<sup>^{2}</sup>$  Percent change between respective modification and base (- decrease, + increase)

## APPENDIX B-1

### Driveability Procedure

The driveability procedure used in this test was developed by CRC in 1968 and updated in 1971, 1973, 1975 and 1977.

The drive-away phase of this procedure involves two different driving modes. The first, is a driving cycle consisting of five maneuvers followed by a 30 second idle period. Each maneuver is performed at 0.1 mile increments. At the termination of each maneuver, the driver's evaluation of the car's performance, categorizing the type of malfunction and its severity, is recorded by the observer. The five maneuvers are performed in the following order:

- 1. 0-25 mph light throttle acceleration
- 2. 25 mph cruise
- 3. 25-35 mph light throttle (detent) acceleration
- 4. 0-35 wide open throttle acceleration
- 5. 10-25 light throttle acceleration
- 6. 30 second engine idle

The attached log sheet shows the details of the procedure. This cycle is repeated two more times.

This is followed by a second mode of three cycles in duration. Each of these cycles consist of four maneuvers each followed by 30 second engine idle period. Three of the maneuvers are performed at 0.1 mile increments, while the fourth is a 0-45 mph crowd acceleration (at constant manifold vacuum) of 0.4 mile duration. The four maneuvers are performed in the order shown below:

- 1. 0-45 crowd acceleration (constant vacuum)
- 2. 25-35 light throttle (detent) acceleration
- 3. 0-35 wide open throttle acceleration
- 4. 10-25 light throttle acceleration
- 5. 30 second engine idle

This cycle is then repeated two more times.

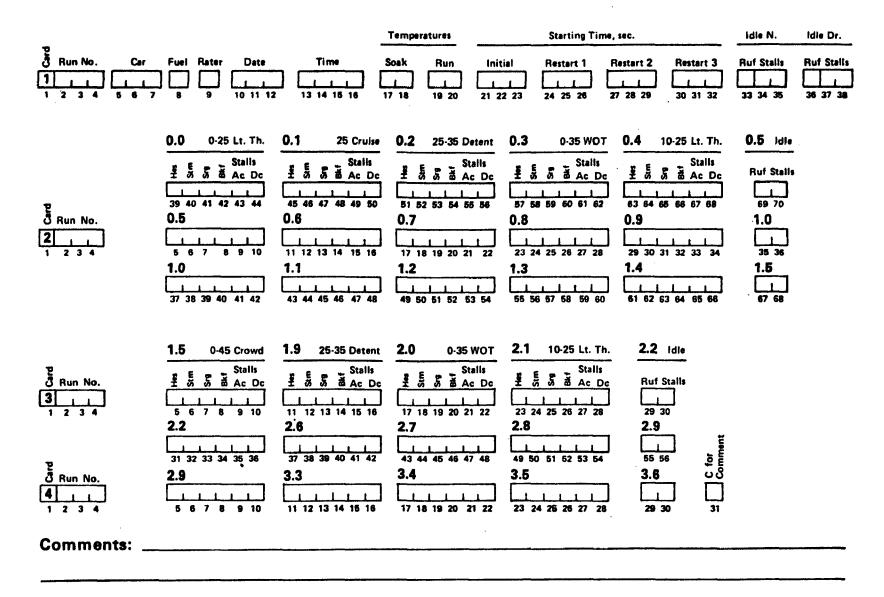
The various accelerations described in the above maneuvers are performed at predetermined manifold vacuum conditions, with the aide of a vacuum gauge.

These accelerations are defined below:

#### Test Run

Operation of a car throughout the prescribed sequence of operating conditions and/or maneuvers for a single test fuel.

## **CRC** driveability data sheet



## Maneuver

A specified single vehicle operation or change of operating condition (such as idle, acceleration or cruise) that constitutes one segment of the driveability driving schedule.

## Road Load

Operation at a prescribed constant vehicle speed with a fixed throttle position on a level road. Cruise conditions are intended to be road load operation.

## Wide Open Throttle (WOT) Acceleration

"Floorboard" acceleration through the gears from prescribed starting speed. Rate at which throttle is depressed is to be as fast as possible without producing tire squeal or appreciable slippage.

## Part Throttle (PT) Acceleration

An acceleration made at any defined throttle position, or consistent change in throttle position, less than WOT. Several PT accelerations are used. They are:

Light Throttle (LT th) - All light throttle accelerations are begun by opening the throttle to an initial manifold vacuum and maintaining constant throttle position throughout the remainder of the acceleration. The vacuum selected is that which just precedes carburetor power enrichment as indicated by carburetor flow curves. These vacuum settings will be obtained from the car manufacturers for each test car.

<u>Crowd</u> - An acceleration made at a constant intake manifold vacuum throughout the acceleration. Throttle opening continually increasing with increasing engine speed. Crowd acceleration vacuums to be used in each car are the same as the detent vacuums.

Detent - All detent accelerations are begun by opening the throttle to the downshift position as indicated by transmission shift characteristic curves. Manifold vacuum corresponding to this point at 25 mph is determined for each car prior to the first driveability test. Maintain constant throttle position to 35 mph terminal speed.

At the end of each maneuver, the car's performance is evaluated by the driver using the categories indicated below:

## Stall

Any occasion during a test that the engine stops with the ignition on. Two types of stall, indicated by location on the data sheet, are:

Stall; idle - Any stall experienced when the vehicle is not in motion, or when a maneuver is not being attempted.

## Driveability Procedure

## Stall; driving

Any stall experienced during motion, or coincidental to initiation or elimination of motion of the vehicle.

## Idle Roughness

An evaluation of the idle quality or degree of smoothness while the engine is idling.

## Backfire

An explosion in the induction or exhaust system.

## Hesitation

A temporary lack of initial response to changes of throttle position to increase acceleration rate.

## Stumble

A short, sharp reduction in acceleration rate experienced under acceleration or road conditions.

#### Surge

A continued or transient condition of fluctuations in power, experienced as changes in acceleration rate, which are short or long, cyclic, and occurring at any speed and/or load.

The severity level of the malfunctions shown above are defined below with the obvious exception of stalls.

## Trace (T)

A level of malfunction severity that is just discernible to a test driver but not to most laymen. A severity level of one (1) demerit.

## Moderate (M)

A level of malfunction severity that is probably noticeable to the average layman. A severity level of two (2) demerits.

## Heavy

A level of malfunction severity that is pronounced and obvious to both test driver and layman. A severity level of four (4) demerits.

## Driveability Procedure

A T, M, H, is entered in the appropriate block on the data sheet to indicate both the occurrence of the malfunction and its severity. More than one type of malfunction may be recorded for each maneuver. If no malfunction occurs, enter a dash (-) to indicate that the maneuver was performed and the car performance was satisfactory during that maneuver.

A data rating system provides for the vehicle malfunctions and severity level experienced by the driver to be translated into a demerit scale, which allows for a numerical ranking of driveability quality. As shown above, the severity levels have been summarized by applying demerits to the three levels: Trace = 1, Moderate = 2, and Heavy = 4. These demerits are then multiplied by the following weighting factors:

Malfunction	Weighting	Factor
Starting time (sec $-2.0$ )	· I	
Idle roughness	1	
Hesitation	6	
Stumble	6	
Backfire	6	
Surge	4	
Stall, idle	8	
Stall, driving	32	

Demerits on each data sheet are totaled, counting only the maximum weighted demerit on each line (maneuver), to obtain the total weighted demerits (TWD) for each run. Thus, if two malfunctions occurred in one maneuver, such as a heavy hesitation (24 demerits and a trace stumble (6) demerits), only the heavy hesitation would contribute to the TWD for the run.

#### Cool Down Procedure

The CRC Intermediate Temperature Driveability Procedure has been adapted to the chassis dynamometer using a three-hour forced soak to bring the vehicle temperatures down to the test temperature. For a test temperature of 16°C (60°F) the forced soak procedure consists of opening the hood and allowing temperature controlled room air (16°C) to be circulated at 24 kph over the frontal area of the vehicle. For a lower test temperature, e.g. 4°C, the above procedure plus the use of an auxiliary pump and external radiator placed in the path of the 24 kph room air temperature is required. The pump is connected to the inlet-outlet radiator hoses to the engine block, which allows circulation of engine coolant through the external radiator and the block. At 16°C either of the above procedures are adequate to bring the engine temperature, carburetor air, engine oil, engine coolant and transmission fluid down to the test temperature within a three-hour soak period.

At the  $60^{\circ}F$  test temperature specified in the contract, the driveability test work conducted in this program was done without an auxiliary pump. The data in Tables B-1 and B-2 compares the cool-down rates with

## Cool Down Procedure

and without auxiliary cooling for two test cars, Plymouth Volare 225-F and Ford Granada 302-C, used in this program. Temperatures were measured using thermocouples placed (1) in the air horn for carburetor air, (2) in the oil sump through the drain plug for engine oil, (3) at the coolant temperature sensor for coolant temperature and (4) through the transmission pan for transmission fluid. This data shows the transmission fluid to be the most difficult to cool down. However, transmission fluid temperatures reached test temperatures ± 4°F before the end of the three hour soak period. Also shown on Tables B-1 and B-2 are the driveability test results (single determinations) using the two soak procedures. Within the test accuracy there is no difference in driveability demerits between the two methods.

TABLE B-1

FORD GRANADA 302-C FORCED COOL DOWN DATA

TEMPERATURE, °F WITH NO AUXILIARY COOLING

Soak- time Hrs.	Carbure- tor Air	Engine 0il	Coolant	Trans.	Room Air	Drive- ability Demerits
0.0	100	134	196	180	69	
0.5	66	74	176	111		
1.0	61	61	130	88	57	
1.5	62	62	100	78		
2.0	62	62	83	73	60	
2.5	64	64	73	70		
3.0	64	64	64	64	61	16
	TEMPERA	TURE, °F	WITH AUXILI	ARY COOLIN	G	
0.0	126	155	190	188	61	
0.5	62	63	63	106		
1.0	61	61	61	78	59	
1.5	63	63	63	68		
2.0	63	63	63	63	61	
2.5	65	65	65	65		
3.0	61	61	61	61	59	30

TABLE B-2

PLYMOUTH VOLARE 225-F FORCED COOL DOWN DATA

TEMPERATURE, °F WITH NO AUXILIARY COOLING

Soak- time Hrs.	Carbure- tor Air	Engine 0il	Coolant	Trans.	Room Air	Drive- ability Demerits
0.0	72	170	189	163	64	
0.5	67	92	141	109		
1.0	64	69	100	90	61	
1.5	64	64	81	79		
2.0	64	64	69	69	61	
2.5	63	61	63	63		
3.0	62	62	62	62	60	435
	TEMPER	ATURE, °F	WITH AUXILI	ARY COOLIN	<u>IG</u>	
0.0	73	167	190	153	67	
0.5	65	97	65	98		
1.0	62	73	62	79	61	
1.5	64	64	64	69		
2.0	64	64	64	64	62	
2.5	63	63	63	63		
3.0	62	62	62	62	61	416

## APPENDIX B-2

## EMISSION LAB INSTRUMENTATION

Measurement	Analyzer
Carbon Monoxide (CO)	Mine Safety Appliances Co. Model 200 FR Lira & Model 202 Lira Infrared Analyzer (NDIR) Maximum sensitivity = 0 to 50 ppm range
Carbon Dioxide (CO <sub>2</sub> )	Mine Safety Appliances Co. Model 303 Lira Infrared Analyzer Calibrated for Maximum sensitivity = 0 to 1% scale
Unburned Hydrocarbons (UNHC	) Mine Safety Appliances Co. Flame Ionization Detector Model 800
Nitrogen Oxides (NOx)	Thermo Electron Corp.  Model 10A Self Contained Chemiluminescent NO - NOx Gas Analyzer

## Sampler |

Constant Volume Sampler (CVS) - Scott Research Laboratories Inc. Model 301 Mass Sampling System with Water heater-cooler control unit.

CAR	<u>K</u>	J	<u> </u>		<u>B</u>	<u>E</u>	F	H	<u>s</u>	0	<u>M</u>	<u>Q</u>	U
FTP Fuel Economy													
s <sup>2</sup> <u>s</u> <del>x</del> %cv	.02 .16 17.18 .91	.04 .20 19.33 1.02	.03 .17 12.34 1.42	.05 .22 17.03 1.29	.04 .19 14.55 1.34	.11 .33 16.18 2.05	.08 .29 14.41 2.01	.08 .29 14.24 2.04	.01 .10 10.95 0.94	.02 .14 13.54 1.00	.004 .06 13.83 .45	.13 .36 12.31 2.89	.27 .52 22.46 2.31
HFE Fuel Economy													
s <sup>2</sup> <u>s</u> x %cv	.07 .26 22.34 1.18	.14 .37 25.70 1.44	.16 .40 17.48 2.29	.25 .50 22.28 2.22	.28 .53 19.10 2.76	.32 .57 23.24 2.44	.16 .39 20.18 1.95	.66 .82 19.86 4.11	.10 .31 17.23 1.81	.09 .30 18.35 1.64	.15 .38 18.49 2.08	.54 .74 17.85 4.12	.57 .75 27.31 2.75
HC Emissions													
s <sup>2</sup> <u>s</u> <del>X</del> %cv	.02 .14 2.03 6.83	.004 .07 1.10 6.13	.01 .12 0.76 15.23	.07 .26 1.62 15.85	.01 .11 1.57 7.05	.01 .10 .96 10.34	.04 .19 1.74 10.93	.001 .03 .74 3.98	.003 .05 1.05 4.78	.004 .07 1.31 5.08	.005 .07 1.57 4.40	.02 .15 1.13 12.93	.002 .05 .72 6.40
CO Em	issions												
s <sup>2</sup> S X %CV	.96 .98 16.36 5.99	.23 .48 20.10 2.40	.49 .70 4.38 15.98	7.46 2.73 15.37 17.76	1.40 1.18 23.77 4.98	6.10 2.47 20.49 12.06	4.54 2.13 25.62 8.32	1.43 1.19 7.85 15.21	1.60 1.27 16.75 7.55	1.30 1.14 11.82 9.63	1.01 1.01 8.37 12.02	13.30 3.65 16.79 21.73	1.58 1.26 10.71 11.74
NOx E	missions	_											
s <sup>2</sup> <u>\$</u> <del>X</del> %CV	.01 .10 2.85 3.66	.01 .10 2.04 4.79	.01 .08 1.54 4.95	.02 .14 2.66 5.40	.01 .09 2.74 3.43	.02 .13 2.95 4.36	.04 .21 2.71 7.80	.10 .31 3.13 9.96	.01 .10 1.85 5.60	.04 .21 3.70 5.64	.02 .15 2.89 5.17	.03 .17 1.76 9.34	.04 .20 1.77 11.15

TABLE C-1

REPEATABILITY OF EMISSION AND FUEL ECONOMY DATA

											RA	NGE
CAR	A	R	L	G	D	<u> </u>	T	C	<u>V</u>	AVG.	LOW	HIGH
FTP Fuel Economy												
s <sup>2</sup> s <u>x</u>	.70	.06	.02	.03	.30	.09	.51	.13	.07			
S	.84	.25	.13	.17	.54	.29	.72	.35	.27			
ა ⊽	22.84	10.79	14.97	15.34	16.37	14.43	13.49	19.73	18.40			
					3.33	2.04	5.31	1.79	1.46	1.89	0.45	5.31
%CV	3.67	2.29	.90	1.13	3.33	2.04	7.51	1.77	1.40	1.07	0.43	3.32
HFE Fuel Economy												
$s^2$		0.7	0.5	20	.37	.21	.48	.16	.17			
S	.69	.27	.05	.28	.61	.46	.70	.41	.41			
S X	.83	.52	.23	.53	23.36	20.18	16.65	25.67	24.23			
	31.06	15.87	18.79	20.34	2.61	20.16	4.18	1.58	1.70	2.40	1.18	4.18
%CV	2.68	3.26	1.22	2.60	2.01	2.20	4,10	1.50	1.70	2.40	1.10	4.10
HC Emissions												
s <sup>2</sup> <u>s</u> <u>x</u>	.01	.002	.01	.02	.10	.001	.004	.01	.001			
ა ი	.09	.002	.11	.15	.32	.03	.07	.08	.04			
2	.76	.46	.89	1.14	1.68	.79	.32	1.83	.63			
a %CV	11.21	9.09	12.28	12.92	18.95	4.09	20.63	4.31	5.97	9.52	3.98	20.63
%C V	11.21	9.09	12.20	12.72	10.75	4.07	20.03	7.31	3.7.	J.J.	3.70	
CO Emiss	sions											
$\frac{s^2}{\frac{s}{x}}$	6.69	.16	7.51	5.13	1.00	.69	2.84	8.16	.52			
s e	2.59	.40	2.74	2.27	1.00	.83	1.68	2.86	.72			
2	13.32	4.07	12.84	25.95	15.47	7.49	6.65	61.01	12.72			
x %CV	19.42	9.81	21.35	8.73	6.47	11.10	25.34	4.68	5.68	12.71	2.40	25.34
%CV	19.42	9.01	21.33	0.75	0.47	TT • TO	23.34	4.00	3.00	12.71	2140	23.3
NOx Emi	lssions											
<sub>c</sub> 2	00	01	0.2	.002	10	.02	.03	.02	.004			
$\frac{s^2}{\frac{s}{x}}$	.02	.01	.02		.12	.13	.17	.12	.004			
2	.13	.12	.14	.04	.35			1.17	.07			
	2.56	1.96	3.28	1.62	3.04	3.41	1.63		6.95	6.45	2.46	11.41
%CV	4.99	6.13	4.40	2.46	11.41	3.90	10.27	10.54	0.95	0.43	4.40	TT•4T

TABLE C-2

PERFORMANCE OF 1977 CHEVROLET CHEVETTE - CAR NO. W-53
98F CID - 1 BBL. CARB.

		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	23.46 24.12 *(22.35) *(21.87)	24.06 23.76	*( <sup>22.32</sup> )	21.74 23.06	21.72 22.04
	Highway Fuel Economy (Mi./Gal.)	32.00 32.77 *(30.05) *(31.16)	31.73 31.37	*(31.51)	30.51 32.32	28.88 29.33
	Emissions					
68	HC, (Gms./Mi.)	1.07 0.96 *(0.70)	0.82 0.80	*( <sup>0.79</sup> )	0.69 0.60	0.75 0.66
	CO, (Gms./Mi.)	16.67 14.77 *(12.26) *(17.13)	12.94 11.86	*(14.20)	17.07 9.59	13.43 12.21
	NOx, (Gms./MI.)	1.78 1.82 *(1.92)	4.76 5.08	*( <sup>1.97</sup> )	1.97 2.10	2.00 2.07
	Driveability Demerits	118 101	78 100	62 62	75 118	65 76

 $<sup>\</sup>star($  ) Data with Rebuilt Transmission, Retaining Original Governor.

PERFORMANCE OF 1977 CHEVROLET CHEVELLE - CAR NO. W-41
305F CID - 2 BBL. CARB.

		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	14.63 14.64	14.88 15.08	14.84 14.52	14.20 13.81	14.61 14.32
	Highway Fuel Economy (Mi./Gal.)	18.48 18.88	19.96 19.74	19.96 19.24	17.18 18.39	19.18 19.95
	Emissions					
60	HC, (Gms./Mi.)	0.99 1.02	1.16 1.14	2.37 2.18	1.12 1.14	2.12 2.41
	CO, (Gms./Mi.)	12.78 13.49	15.43 13.95	34.26 32.79	18.98 18.88	37.04 40.06
	NO×, (Gms./Mi.)	2.69 2.74	3.76 3.65	2.70 2.86	1.92 2.08	2.43 2.58
	Driveability Demerits	105 129	124 112	136 105	105 114	124 156 128

PERFORMANCE OF 1978 PONTIAC SUNBIRD - CAR NO. X-02
151C CID - 2 BBL CARB. (CALIF.)

		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	21.47 21.74	18.15 18.87	18.54 18.80	21.88 21.19	18.49 18.15
	Highway Fuel Economy (Mi./Gal.)	28.08 28.47	24.64 24.39	24.56 24.13	27.34 26.36	24.63 24.10
	Emissions					
70	HC, (Gms./MI.)	0.76 0.86	2.67 2.54	2.52 2.70	0.56 0.53	2.58 2.54
	CO, (Gms./Mi.)	9.25 8.25	97.81 96.49	95.25 90.88	7.80 7.78	94.44 102.17
	NO×, (Gms./Mi.)	1.95 1.95	0.60 0.72	0.76 0.49	1.82 1.96	0.60 0.81
	Driveability Demerits	130 111 136 8	9 86 4 111	77 116 85 78	112 97	94 111

PERFORMANCE OF 1977 PONTIAC GRAND PRIX - CAR NO. W-56
301F CID - 2 BBL. CARB.

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	16.44	16.07	16.36	17.05	15.51
	16.47	15.79	16.74	16.27	16.97
Highway Fuel Economy (Mi./Gal.)	21.93 23.13 24.58 22.84	22.45 21.43	23.86 24.00	24.23 24.20	23.24 23.94
Emissions					
HC, (Gms./Mi.)	1.11 1.21	1.41	2.50 2.42	1.58 2.55	1.45 1.42
CO, (Gms./Mi.)	8.85	9.70	24.48	26.49	9.16
	9.57	8.59	21.76	26.09	10.00
NO×, (Gms./Mi.)	1.88	4.88	1.74	4.22	2.29
	1.45	5.54	1.74	4.82	1.82
Driveability Demerits	51	65	67	56	52
	<b>56</b>	88	67	64	66

TABLE C-6

PERFORMANCE OF 1977 BUICK SKYLARK - CAR NO. W-42

231F CID - 2 BBL. CARB.

		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	15.73 15.29	16.98 17.11	16.12 16.21	16.87 17.43	15.89 15.64
	Highway Fuel Economy (Mi./Gal.)	22.08 23.04	23.49 24.27	23.09 22.48	23.66 24.06	23.21 22.63
	Emissions					
72	HC, (Gms./Mi.)	0.66 0.82	0.97 1.09	1.12 0.89	1.34 1.33	0.67 0.75
	CO, (Gms./M1.)	20.38 16.16	19.87 20.34	24.34 20.18	25.24 22.55	13.09 15.71
	NOx, (Gms./MI.)	1.60 1.71	5.09 4.78	1.48 1.57	4.87 4.65	1.84 1.86
	Driveability Demerits	115 95	97 60	45 22	52 73	127 150

PERFORMANCE OF 1978 BUICK REGAL - CAR NO. A-245
231F CID - 4 BBL. CARB. - (TURBOCHARGE)

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	16.13	15.02	14.78	14.18	16.30
	16.30	15.22	15.19	13.93	16.34
Highway Fuel Economy (Mi./Gal.)	20.48	19.39	21.38	18.25	21.89
	21.49	18.53	22.24	17.73	22.02
Emissions					
73 HC, (Gms./Mi.)	0.82	0.88	0.91	2.33	1.14
	0.80	0.83	<b>0.</b> 56	2.25	0.85
CO, (Gms./Mi.)	10.19	10.90	17.16	80.25	9.17
	9.61	10.08	17.63	87.11	7.43
NOx, (Gms./Mi.)	1.28	4.07	0.98	0.38	1.40
	1.24	4.16	0.95	0.31	1.42
Driveability Demerits	92	78	76	36	106
	90	86	73	56	100

PERFORMANCE OF 1977 BUICK CENTURY - CAR NO. W-43
350F CID - 2 BBL. CARB.

		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	14.41 14.41	14.53 15.35	13.21 13.54	14.27 14.50	14.95 14.98 14.92
	Highway Fuel Economy (Mi./Gal.)	19.49 20.14	20.25 21.08	19.28 19.34	20.07 20.73	20.73 20.71 20.71
74	Emissions					
	HC, (Gms./Mi.)	0.95 0.67	0.84 0.75	2.81 2.83	2.14 1.68	1.64 2.23 2.48
	CO, (Gms./Mi.)	11.15 9.91	10.86 8.02	51.23 49.68	30.72 24.94	19.05 29.85 29.86
	NOx, (Gms./Mi.)	1.76 1.57	5.41 4.81	1.34 1.17	1.26 1.23	4.71 4.18 4.32
	Driveability Demerits	105 104	42 69	87 87	79 100	99 <b>83</b>

PERFORMANCE OF 1977 OLDSMOBILE CUTLASS - CAR NO. W-44
350F CID - 4 BBL. CARB.

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	14.67 14.53	14.17 15.43 14.57	14.27 14.46	13.81 13.61	13.76 13.57
Highway Fuel Economy (Mi./Gal.)	19.94 19.72	18.94 22.33 19.80	19.74 20.09	19.11 19.54 19.17	19.47 19.20
Emissions 75					
HC, (Gms./Mi.)	0.77 0.73	0.73 0.72 0.78	0.74 0.71	0.78 0.83	0.67 0.68
CO, (Gms./Mi.)	7.36 7.83	6.33 6.03 7.56	9.83. 9.21	14.08 9.45	7.09 7.96
NOx, (Gms./Mi.)	1.87	8.60 6.65 <b>7</b> .57	1.90 1.92	2.33 3.01	2.44 2.21
Driveability Demerits	180 7 123*	108 146 18 90*	76 78	104 66	79 62
*Average for an individual rater	131	78	•		

PERFORMANCE OF 1977 OLDSMOBILE "98" - CAR NO. W-57
403F CID - 4 BBL. CARB.

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	14.23 14.30	14.30 14.11	14.34 14.54	14.70 14.61	14.07 15.00 14.17
Highway Fuel Economy (Mi./Gal.)	19.30 19.71	19.65 19.51	20.31 20.28	21.69 20.56	20.15 20.87 20.04
Emissions					
HC, (Gms./Mi.)	0.80 0.84	0.88 0.79	0.85 0.85	0.74 0.76	0.71 0.72 0.70
CO, (Gms./Mi.)	7.03 7.92	7.09 7.43	8.68 8.39	5.28 6.95	7.59 8.97 6.81
NO×, (Gms./Mi.)	2.67 2.44	8.23 8.38	2.21 2.28	2.06 2.07	2.02 1.73 2.06
Driveability Demerits	84 84	84 102	66 56	90 86	30 48

PERFORMANCE OF 1977 FORD PINTO - CAR NO. W-38
140F CID - 2 BBL. CARB.

		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	18.67 18.41	19.48 19.86	20.09 20.2	18.86 19.66	18.94 18.66
	Highway Fuel Economy (Mi./Gal.)	24.53 24.39	26.22 26.97	25.81 26.73	25.58 26.86	24.65 25.47
!	Emissions					
77	HC, (Gms./Mi.)	0.85 0.89	0.90 0.88	0.80 0.91	1.29 1.67	1.36 1.24
	CO, (Gms./Mi.)	15.35 15.17	16.52 15.78	11.91 12.86	28.03 30.16	27.62 26.35
	NOx, (Gms./Mi.)	1.33	4.06 4.21	1.84 1.98	1.52 1.33	1.37 1.41
1	Driveability Demerits	155 152	138 168	122 107	77 108	143 132

TABLE C-12

PERFORMANCE OF 1977 FORD MAVERICK - CAR NO. W-37
250F CLD - 1 BBL. CARB.

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	16.84	17.22	17.76	17.10	16.80
	16.98	17.02	17.64	17.48	16.96
Highway Fuel Economy (Mi./Gal.)	22.04	21.51	22.53	22.67	22.01
	22.36	21.92	22.98	23.12	22.19
Emissions					
HC, (Gms./Mi.)	1.57 1.93	1.27	1.81 1.68	2.41 2.55	2.79 2.92
CO, (Gms./Mi.)	11.56	13.63	12.95	21.61	21.74
	14.26	12.59	11.85	21.53	21.84
NOx, (Gms./MI.)	1.48	7.81	1.85	1.48	1.80
	1.42	7.55	1.97	1.51	1.65
Driveability Demerits	147	118	108	126	140
	173	138	86	164	164

PERFORMANCE OF 1977 FORD MAVERICK - CAR NO. W-55
250C CID - 1 BBL. CARB. (CALIF.)

		***************************************	Base	Modification 1	Modification 2	Modification 3
	FTP Fuel Economy (Mi./Gal.)	14.54 14.54	*14.63 **14.59	15.64 15.65	14.47 14.71	15.63 15.28
	Highway Fuel Economy (Mi./Gal.)	18.19 18.15	*18.43 **18.02	19.61 19.68	18.29 18.31	19.91 19.32
79	Emissions					
	HC, (Gms./Mi.)	1.00 0.77	*0.96 **0.88	0.78 0.69	0.79 0.79	1.25 1.02
	CO, (Gms./Mi.)	12.75 10.96	*11.87 **18.40	10.03 7.01	9.19 8.95	21.84 17.36
	NOx, (Gms./Mi.)	1.36 1.20	*1.27 **1.00	6.56 6.59	1.21 1.29	6.00 6.32
	Driveability Demerits		104 126	44 56	43 62	54 40

<sup>\*</sup> Idle CO @ 0.3%

<sup>\*\*</sup> Rebuild Carb. Idle CO @ 0.3%

TABLE C-14

PERFORMANCE OF 1977 FORD GRANADA - CAR NO. W-50
302F CID - 2 BBL. CARB.

		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	14.24 14.32 14.11	14.05 14.09	13.93 13.99	13.81 13.86	13.10 13.05
	Highway Fuel Economy (Mi./Gal.)	19.58 18.51 19.49	18.31 18.32	19.04 18.79	18.83 18.38	17.39 17.78
80	Emissions					
	HC, (Gms./Mi.)	1.75 1.91 1.85	1.63 1.64	1.96 1.80	1.26 1.26	1.27
	CO, (Gms./Mi.)	7.90 6.39 8.01	7.37 7.93	7.45 8.29	8.53 8.41	11.99 9.41
	NOx, (Gms./Mi.)	2.05 2.06 1.99	7.37 6.93	2.26 2.19	1.65 1.51	1.45 1.49
	Driveability Demerits	79 86	53 43	48 49	116 130	90 82

PERFORMANCE OF 1977 FORD GRANADA - CAR NO. A-243
302C CID - 2 BBL. V.V. CARB. (CALIF.)

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	12.27 12.08	13.24 12.86	11.39	12.56 12.29	12.52 12.70
Highway Fuel Economy (Mi./Gal.)	17.33	17.98	16.55	18.52	17.17
	17.58	18.57	16.47	17.43	17.21
Emissions					
HC, (Gms./Mi.)	0.78	1.04	0.70	0.85	0.78
	0.69	0.81	0.69	0.61	0.66
CO, (Gms./Mi.)	4.92	3.60	4.47	5.46	4.22
	4.88	3.97	4.68	3.29	4.29
NOx, (Gms./Mi.)	1.13	3.33 3.53	1.11 1.09	1.00	0.97 1.07
Driveability Demerits	129 154	4	41 26	72	39
	156 162	3	68 45	54	30

TABLE C-16

PERFORMANCE OF 1977 FORD LTD11 - CAR NO. W-49
351F CID - 2 BBL. CARB.

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	13.92	13.44	13.46	13.41	13.54
	13.65	13.70	13.51	13.43	13.34
Highway Fuel Economy (Mi./Gal.)	19.23	18.27	18.49	17.62	18.04
	19.19	19.09	18.22	17.73	17.66
Emissions					
HC, (Gms./Mi.)	1.21	1.18 1.22	1.13 1.29	1.37 1.42	1.46 1.46
CO, (Gms./Mi.)	9.17	10.05	11.48	14.44	13.36
	11.47	11.29	9.06	14.10	13.76
NOx, (Gms./MI.)	2.52	8.68	2.65	1.98	2.80
	2.30	8.16	2.96	1.97	2.94
Driveability Demerits	222	129	234	250	216
	199	123	240	<b>236</b>	231

TABLE C-17

PERFORMANCE OF 1977 PLYMOUTH VOLARE - CAR NO. A-241
225F CID - 1 BBL. CARB.

	_Base_	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	16.27 16.37	18.10 18.04	17.40 17.49	16.99 17.09	16.61 15.94
Highway Fuel Economy (Mi./Gal.)	21.12 21.29	23.13 24.43	22.67 21.98 22.76	22.09 22.49	21.63 21.94
Emissions					
HC, (Gms./Mi.)	1.31 1.37	1.28 1.62	1.33	2.10 1.94	2.40 1.73
CO, (Gms./Mi.)	10.29 11.47	11.55 11.56	10.70 7.84	23.75 16.59	26.83 23.12
NO×, (Gms./Mi.)	1.93 1.66	6.39 6.28	1.84	1.75 1.56	1.47 1.67
Driveability Demerits	268 <b>2</b> 69* 207	116 196	224 198	379 <b>&gt;</b> 366* 360	328 377 329 372

<sup>\*</sup>Average for an individual rater

PERFORMANCE OF 1977 PLYMOUTH VOLARE - CAR NO. W-51
318F CID - 2 BBL CARB.

		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	13.12 12.64 11.96	13.66 13.32	11.96 11.90	12.31 11.84 12.21	11.73 11.52
	Highway Fuel Economy (Mi./Gal.)	18.71 17.27 17.46	18.83 18.62	17.57 17.23	18.69 16.46 17.25	17.39 17.21
0	Emissions					
	HC, (Gms./Mi.)	1.01 1.00 1.06	0.87 0.91	1.00	1.65 1.22 1.60	1.33
	CO, (Gms./Mi.)	9.35 13.64 11.95	11.61 13.25	16.96 12.09	25.27 16.66 26.87	23.29 25.79
	NOx, (Gms./Mi.)	1.34 1.37 1.58	2.65 2.64	1.34 1.64	1.37 1.76 1.51	1.53 1.69
	Driveability Demerits	242 246	197 192 183 206	220 231	257 244	226 241

TABLE C-19

PERFORMANCE OF 1977 PLYMOUTH VOLARE - CAR NO. W-54

318C CID - 2 BBL. CARB. - (CALIF.)

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	10.53	11.53	10.75	11.25	9.78
	10.61	11.78	11.13	10.63	9.89
Highway Fuel Economy (Mi./Gal.)	16.22 15.34 14.87	17.75 18.22	15.98 15.18	15.87 15.31	14.26 14.76
Emissions					
HC, (Gms./MI.)	0.50 0.43	0.41	0.37 0.37	0.52 0.57	0.59 0.57
CO, (Gms./Mi.)	3.57	2.99	3.31	3.91	7.57
	3.08	2.26	2.91	3.18	7.93
NOx, (Gms./Mi.)	1.79	3.06	1.72	1.57	1.55
	1.97	2.93	1.53	1.76	1.70
Driveability Demerits	274	126	240	197	305
	263	145	278	<b>224</b>	310

PERFORMANCE OF 1977 CHRYSLER CORDOBA - CAR NO. W-48
400F CID - 4 BBL. CARB. (LEAN BURN)

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	11.34	10.70	11.19	11.03	10.59
	11.38	10.84	10.99	10.82	10.59
Highway Fuel Economy (Mi./Gal.)	17.23 17.29	16.51 17.39	17.61 17.75	17.54 17.86	16.46 16.41 16.70
Emissions					
HC, (Gms./Mi.)	0.68	0.63	0.64	1.58	1.63
	0.69	0.67	0.79	1.55	1.64
CO, (Gms./Mi.)	6.11	9.03	5.13	30.42	33.84
	5.55	7.80	7.35	27.52	34.76
NOx, (Gms./Mi.)	1.84	1.90	1.96	1.74	1.86
	1.59	1.88	2.10	1.65	1.99
Driveability Demerits	183	156	187	207	198
	187	170	167	218	187

PERFORMANCE OF 1978 AMC CONCORD - CAR NO. W-59
258C CID - 1 BBL CARB. (CALIF.)

	Base	Modification 1	Modification 2	Modification 3	Modification 4
FTP Fuel Economy (Mi./Gal.)	13.45	14.37	11.82	13.13	13.20
	12.93	16.15	12.11	13.30	14.46
Highway Fuel Economy (Mi./Gal.)	15.88	19.08	14.80	16.12	16.22
	15.48	21.19	14.73	16.34	16.64
Emissions					
<sup>∞</sup> HC, (Gms./Mi.)	0.34	0.22	0.35	0.24	0.51
	0.28	0.24	0.31	0.35	0.35
CO, (Gms./Mi.)	6.27	4.81	10.26	4.26	9.47
	4.86	1.36	7.74	6.91	10.52
NOx, (Gms./Mi.)	1.16	4.48	0.96	1.01	0.86
	1.05	3.97	0.96	0.93	0.88
Driveability Demerits	121	33	150	120	94
	121	35	179	134	118

TABLE C-22

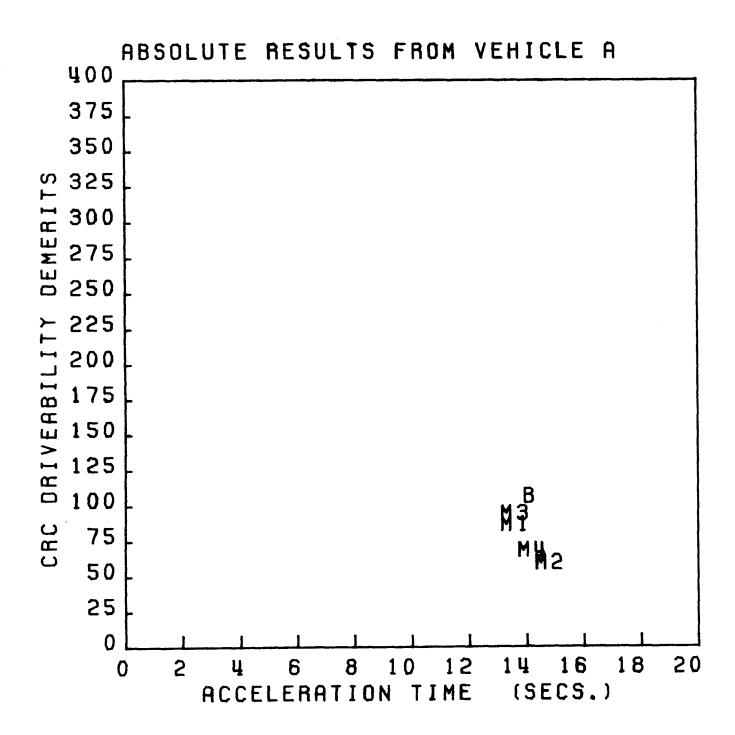
PERFORMANCE OF 1977 TOYOTA COROLLA - CAR NO. W-52
97F CID - 2 BBL. CARB.

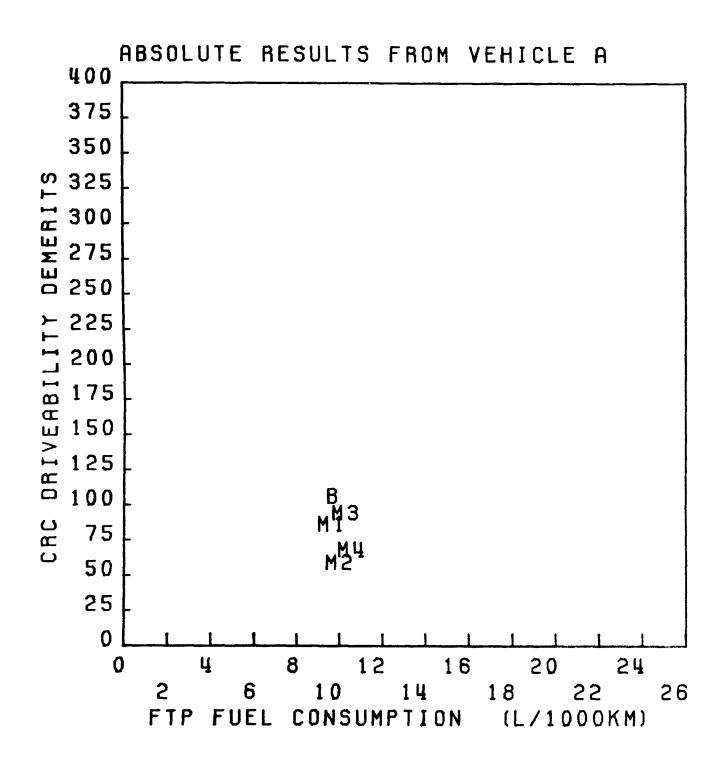
	Base	Modification 1	Modification 2	Modification 3	Modification 4		
FTP Fuel Economy (Mi./Gal.)	22.07 22.10	22.62 22.99	23.94 23.27	20.83 22.48 21.82	22.02 22.63		
Highway Fuel Economy (Mi./Gal.)	26.94 28.29	27.86 27.57	28.36 27.13	25.36 26.99 26.53	27.15 27.67		
Emissions							
HC, (Gms./Mi.)	0.73 0.71	0.66 0.68	0.69 0.64	0.82 0.67 0.73	0.82 0.76		
CO, (Gms./Mi.)	9.84 10.07	10.19 9.25	8.28 7.76	14.54 11.34 13.96	14.27 11.84		
NOx, (Gms./MI.)	1.90 1.80	1.52 1.66	1.98 2.22	1.91 1.96 1.42	1.51 1.71		
Driveability Demerits	12 12	12 12	6 6	18 9	0		

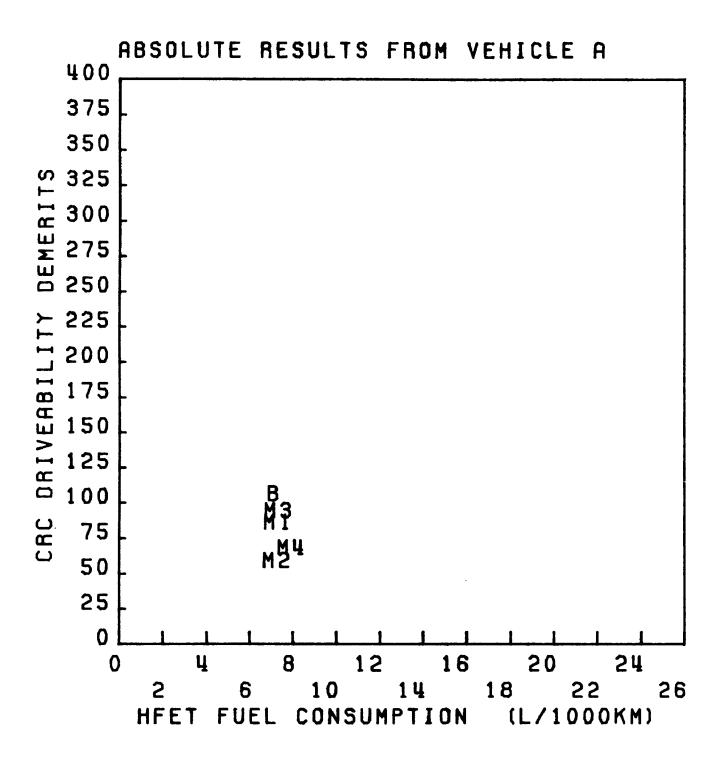
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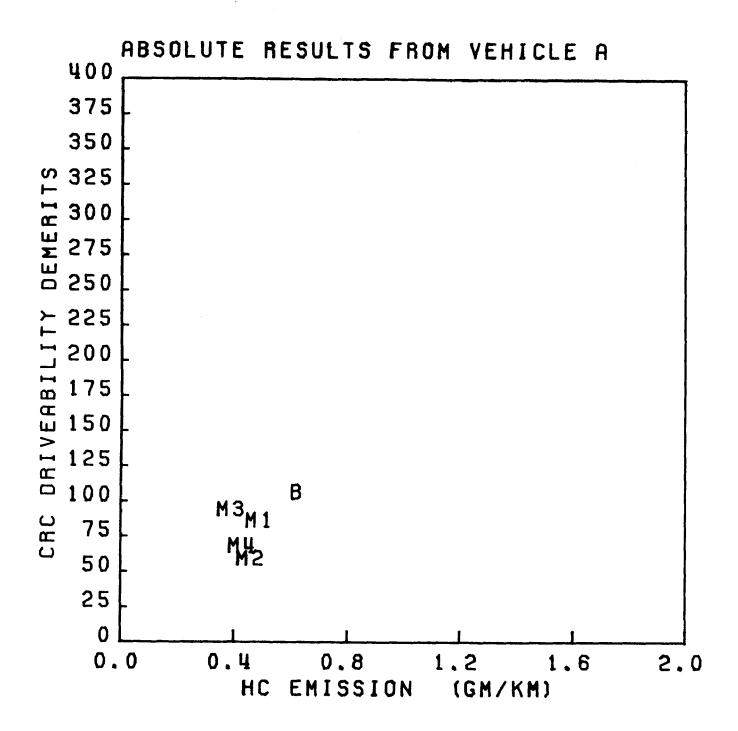
TABLE C-23 PERFORMANCE OF 1978 VOLVO 245 DL - CAR NO. X-03 130C CID - FUEL INJECTION (CALIF.)

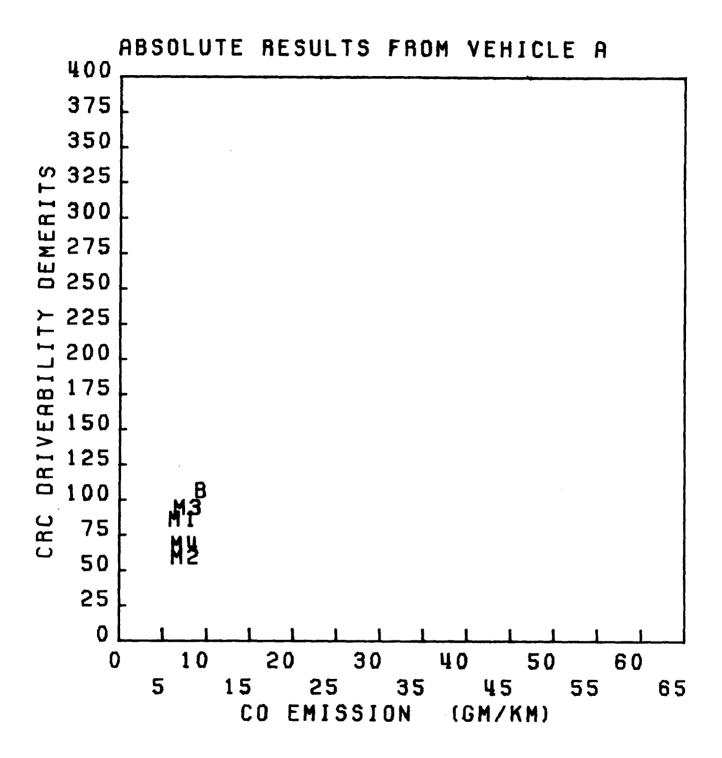
		Base	Modification 1	Modification 2	Modification 3	Modification 4
	FTP Fuel Economy (Mi./Gal.)	18.63 18.76	18.44 18.17	18.28 18.89	18.55 18.06	18.16 18.03
89	Highway Fuel Economy (Mi./Gal.)	25.94 24.78	24.35 23.89	23.92 23.86	24.03 24.00	23.97 23.60
	Emissions					
	HC, (Gms./Mi.)	0.31 0.32	0.48 0.53	0.31 0.28	0.32 0.30	1.65 1.75
	CO, (Gms./Mi.)	3.25 3.31	8.83 10.37	4.31 3.36	3.99 3.80	43.66 42.28
	NOx, (Gms./Mi.)	0.70 0.64	1.73 1.56	0.73 0.78	0.93 0.97	0.66 0.74
	Driveability Demerits	14 19	13 19	23 23	29 23	15 21

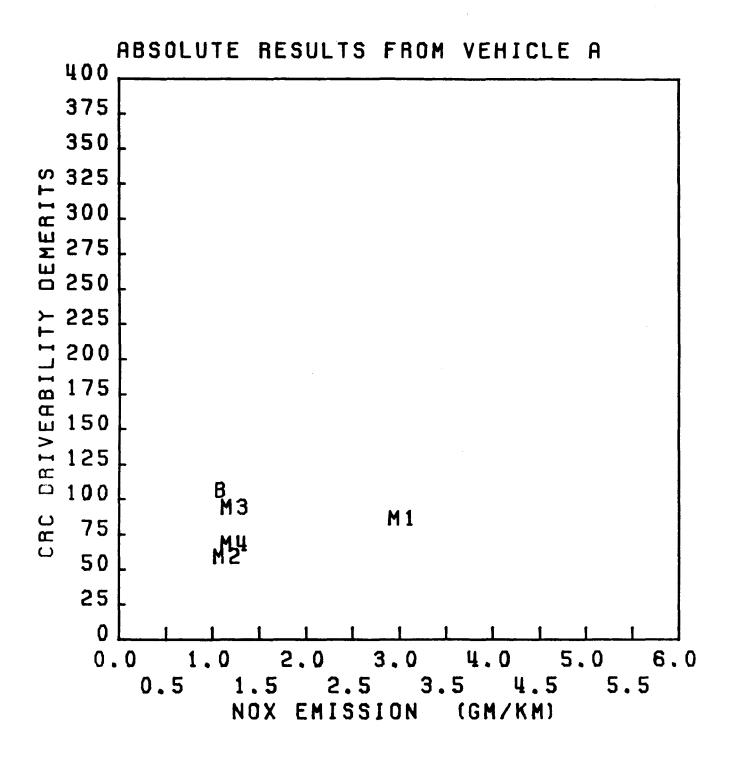


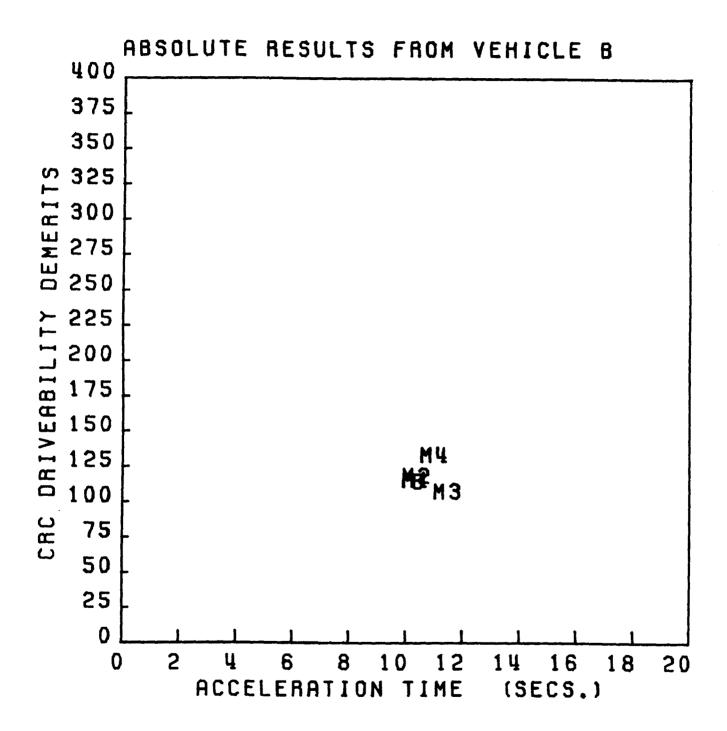


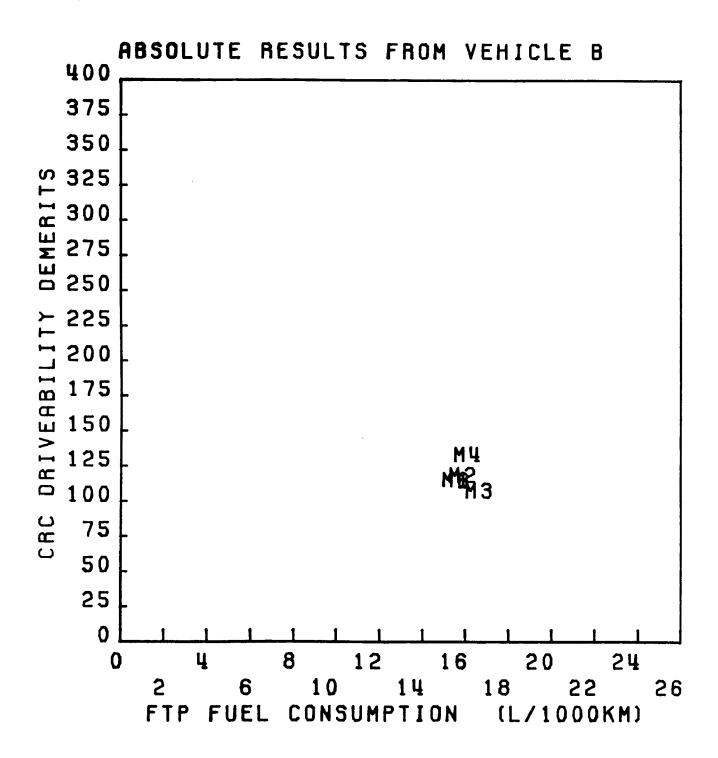


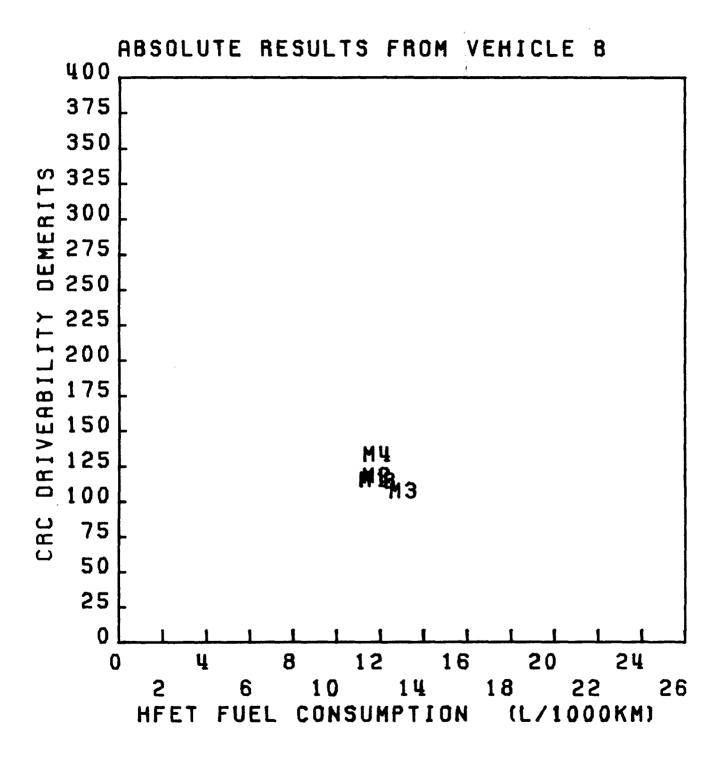


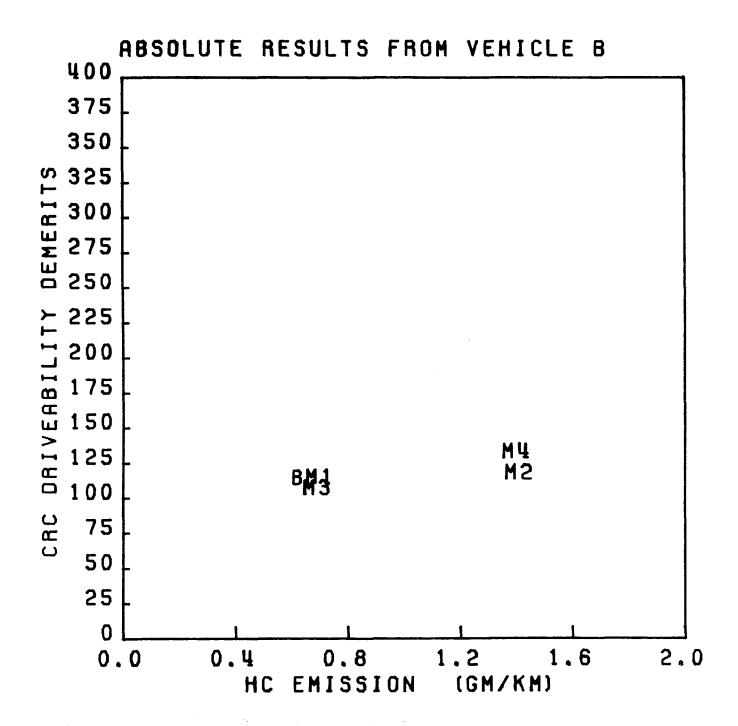


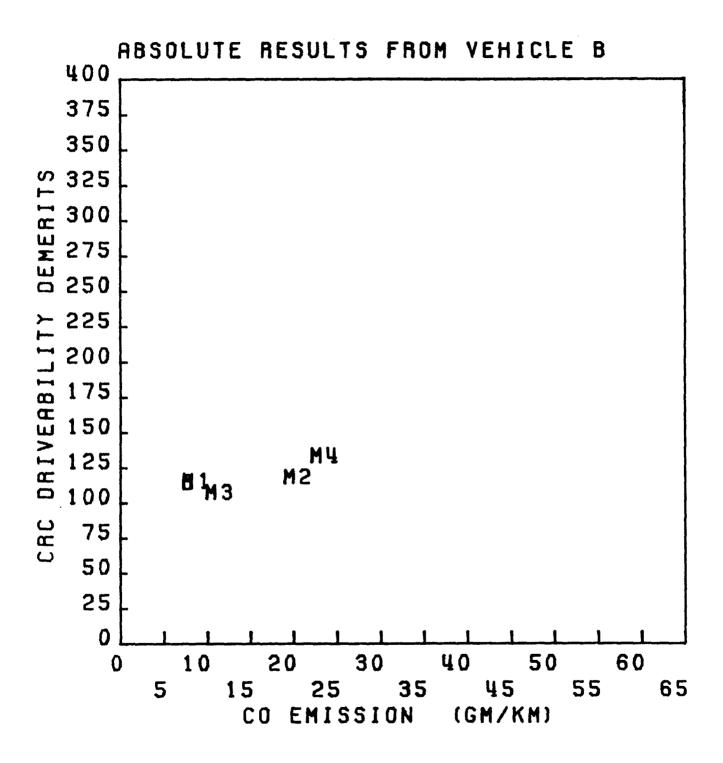


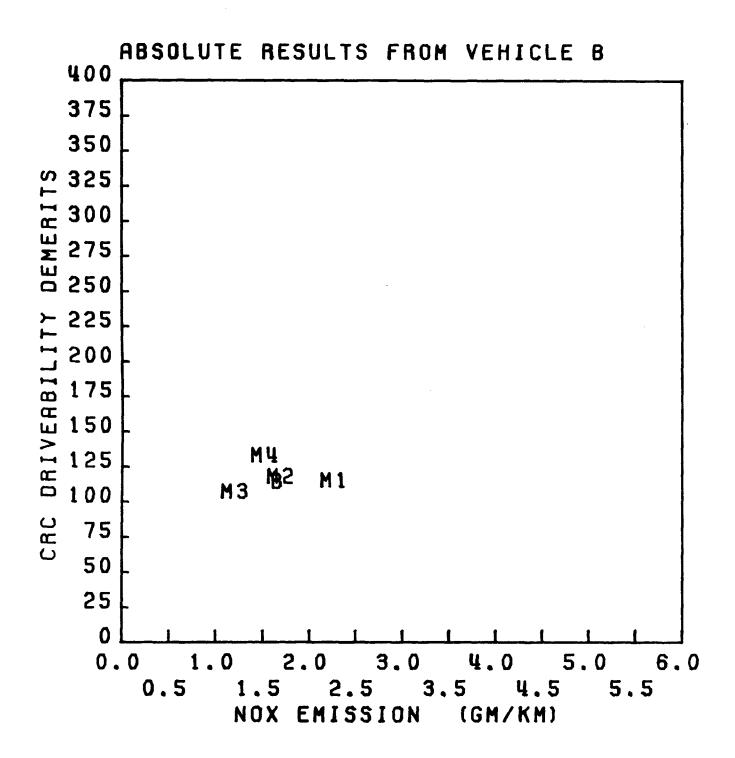


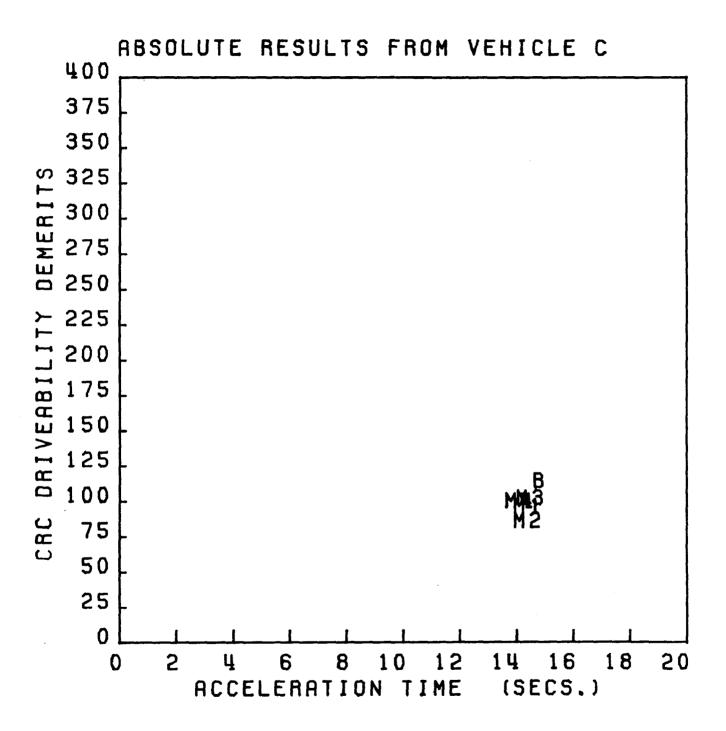


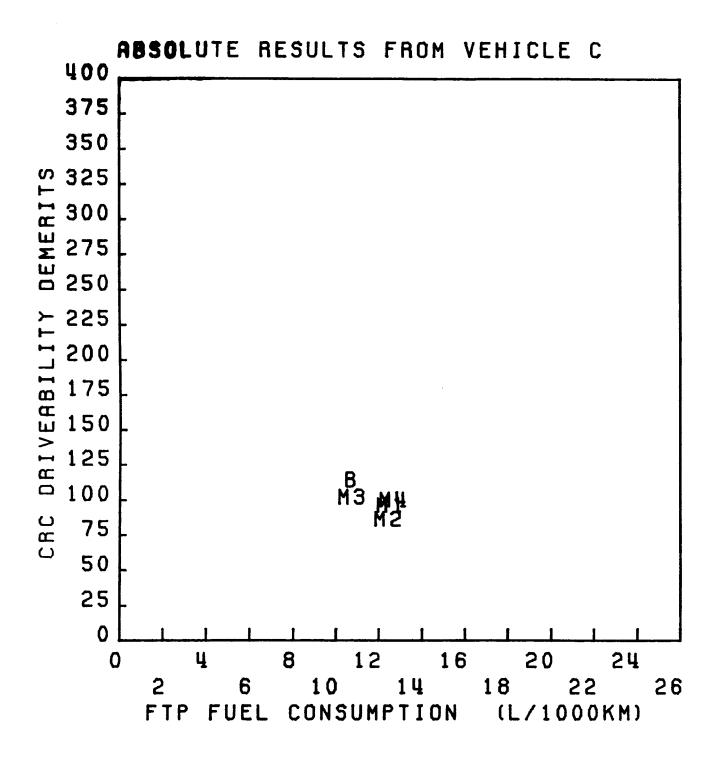


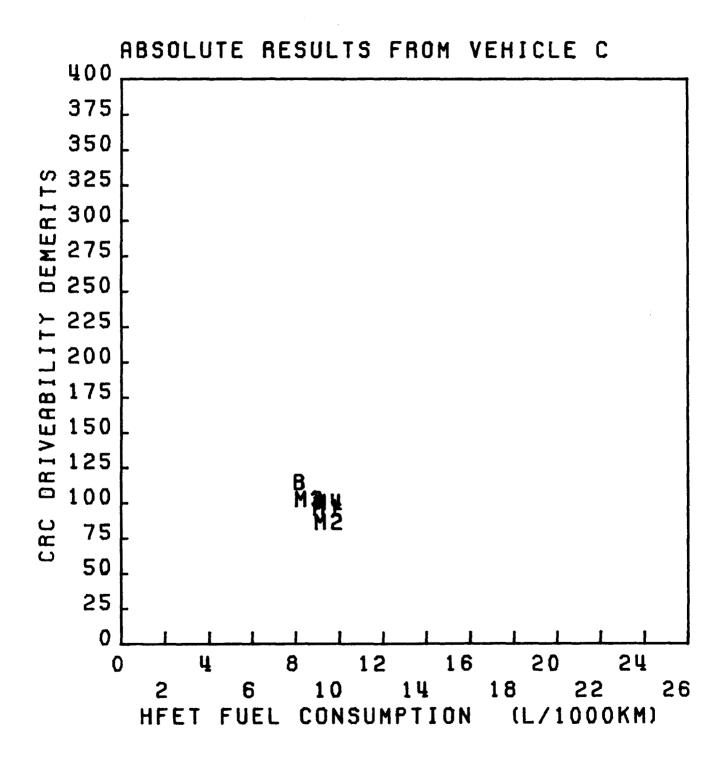


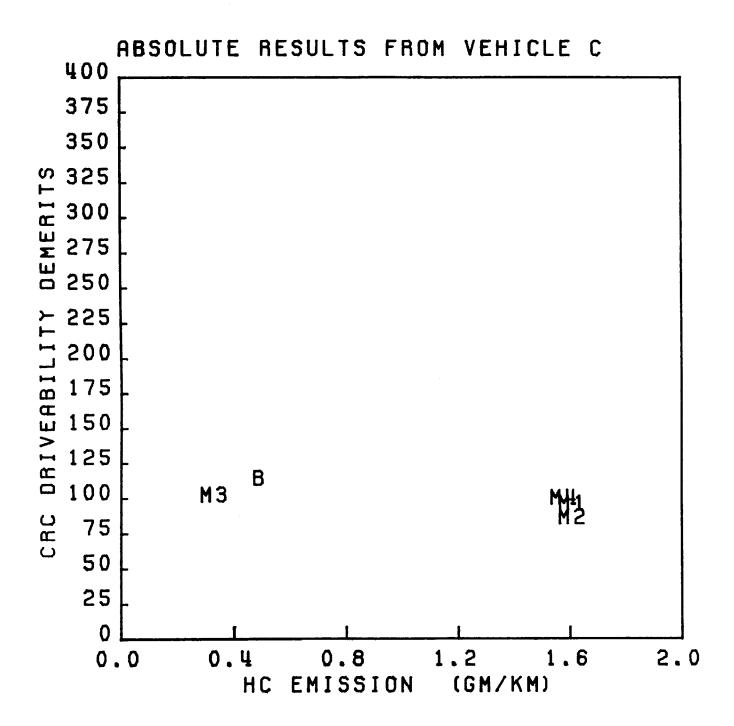


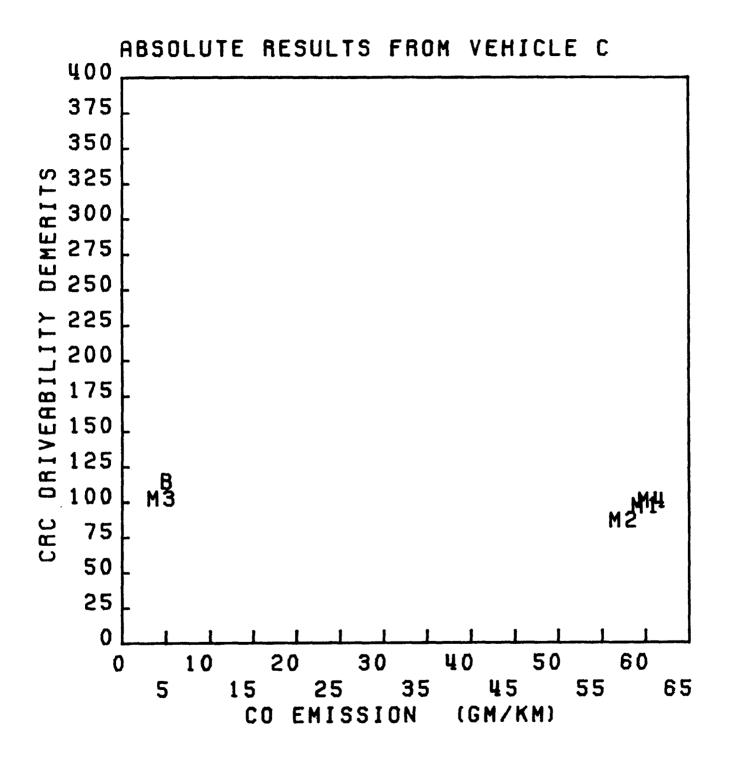


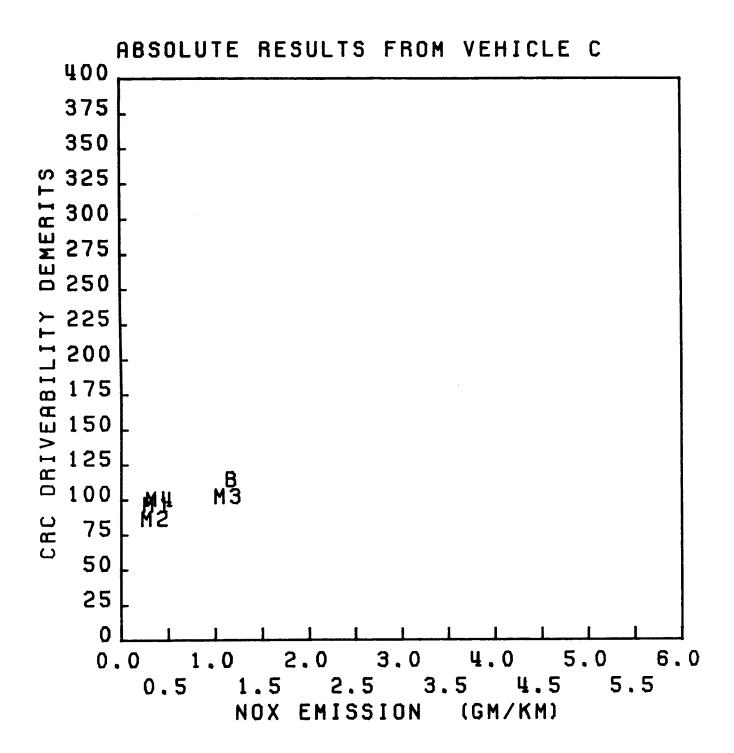


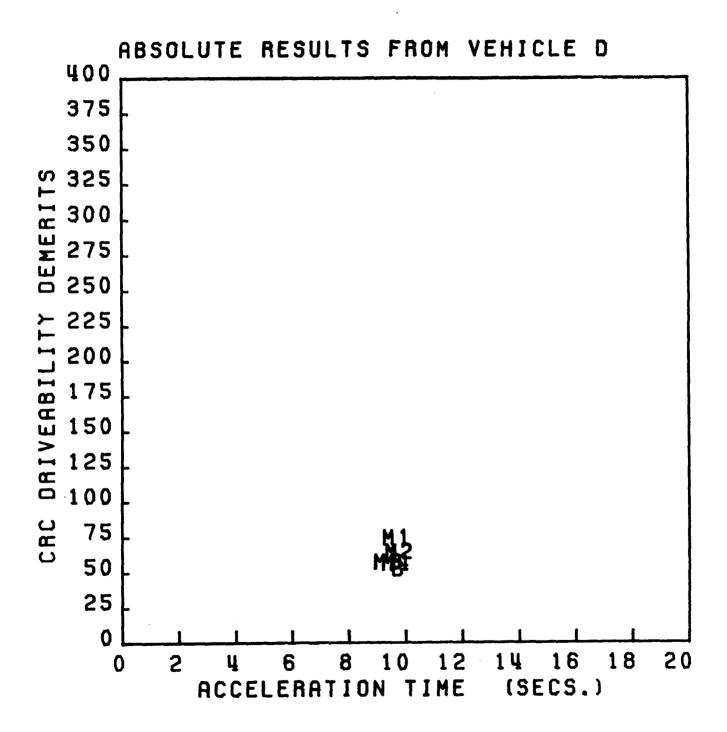


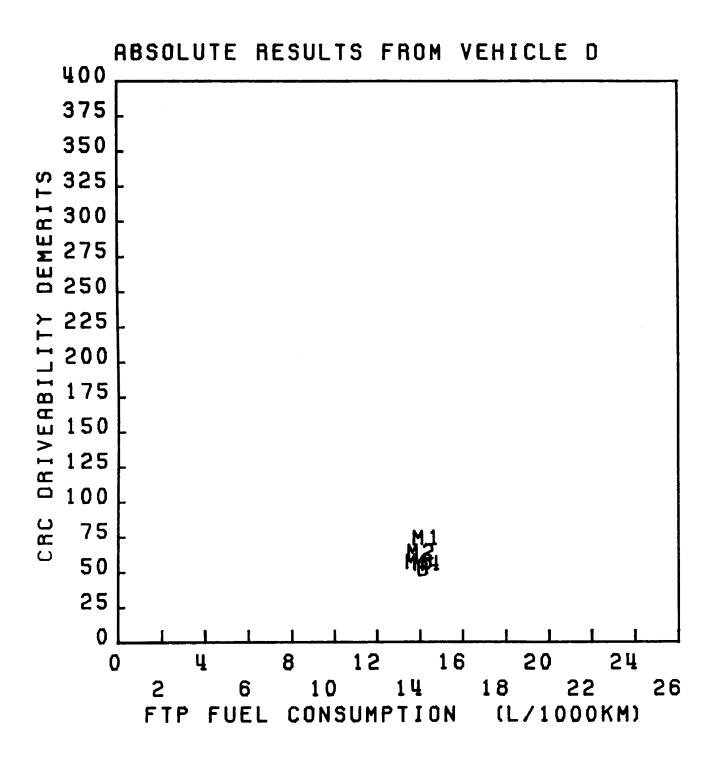


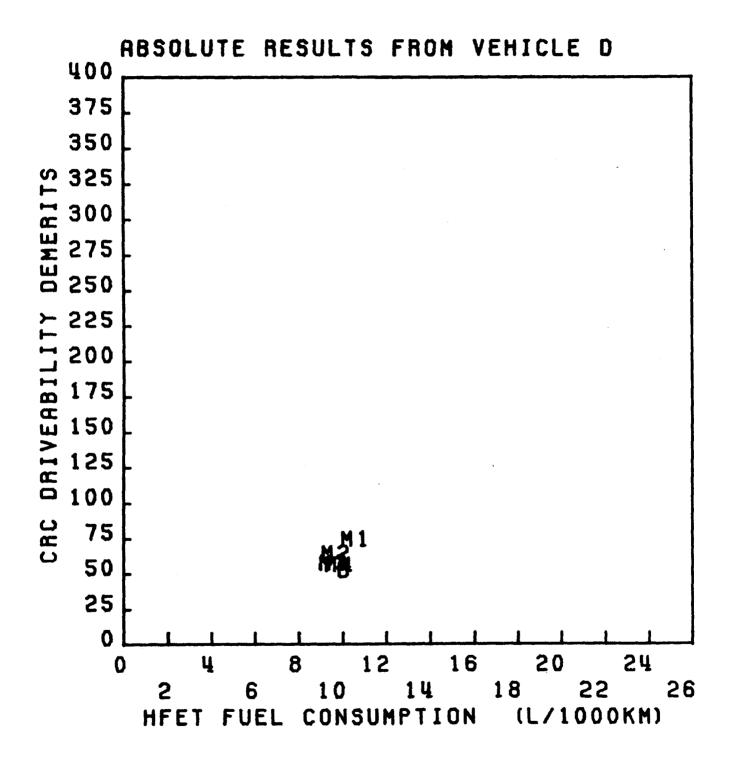


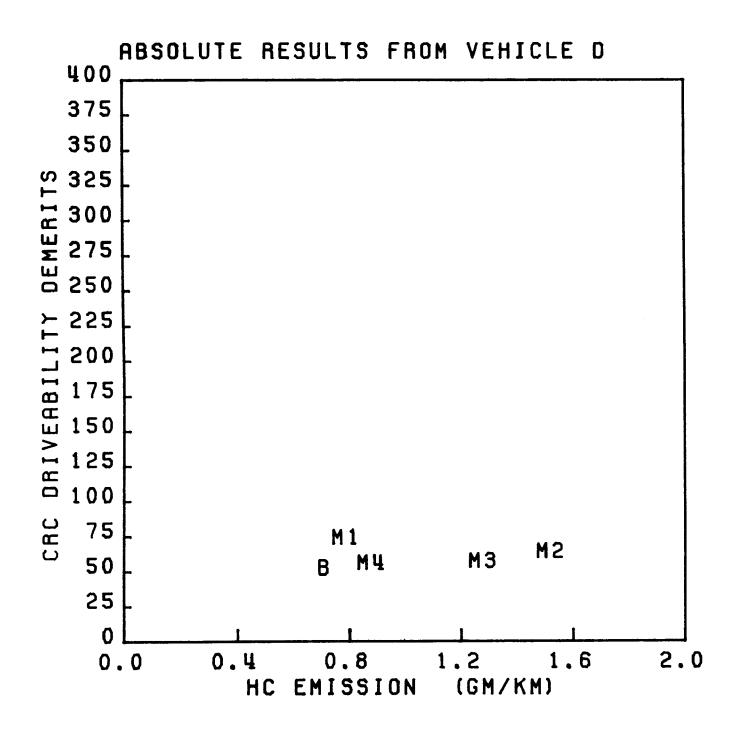


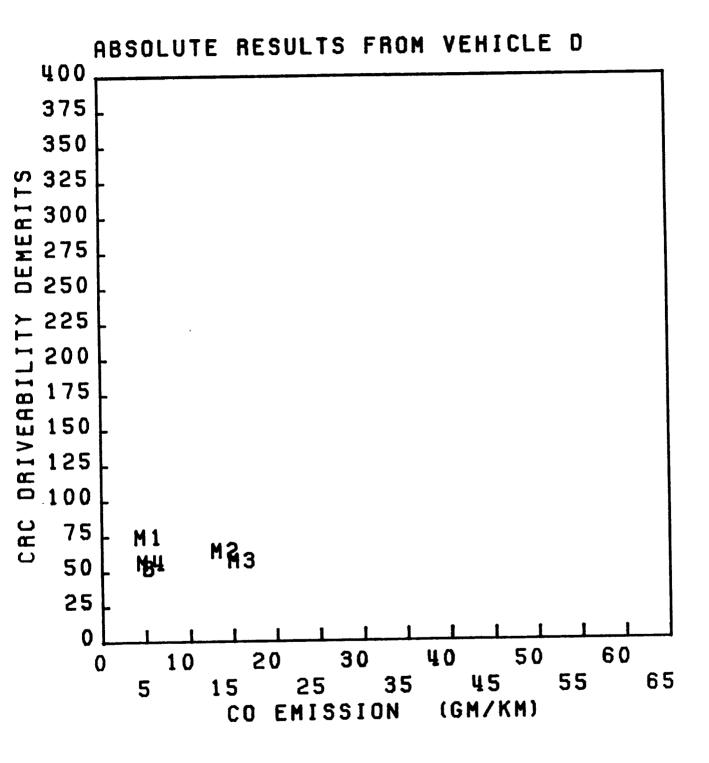


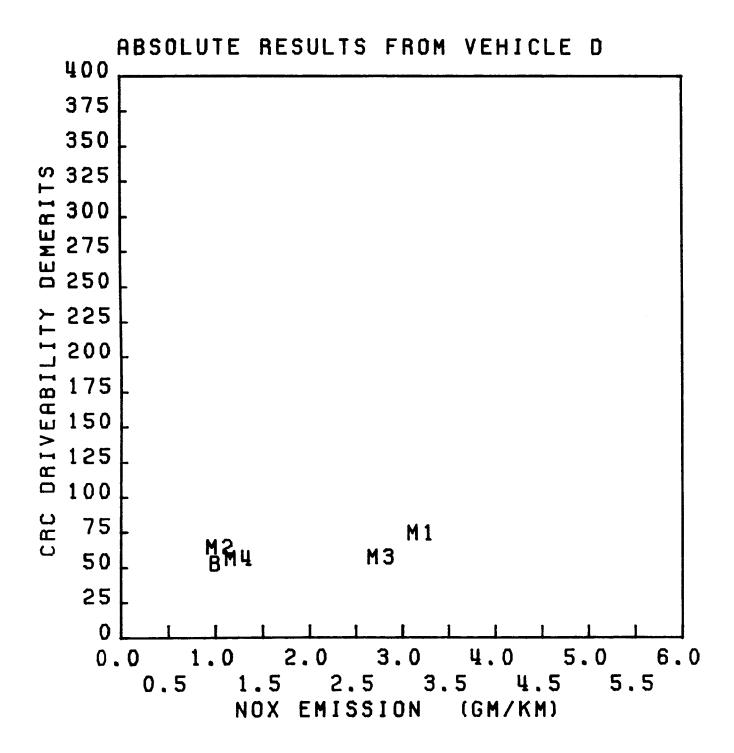


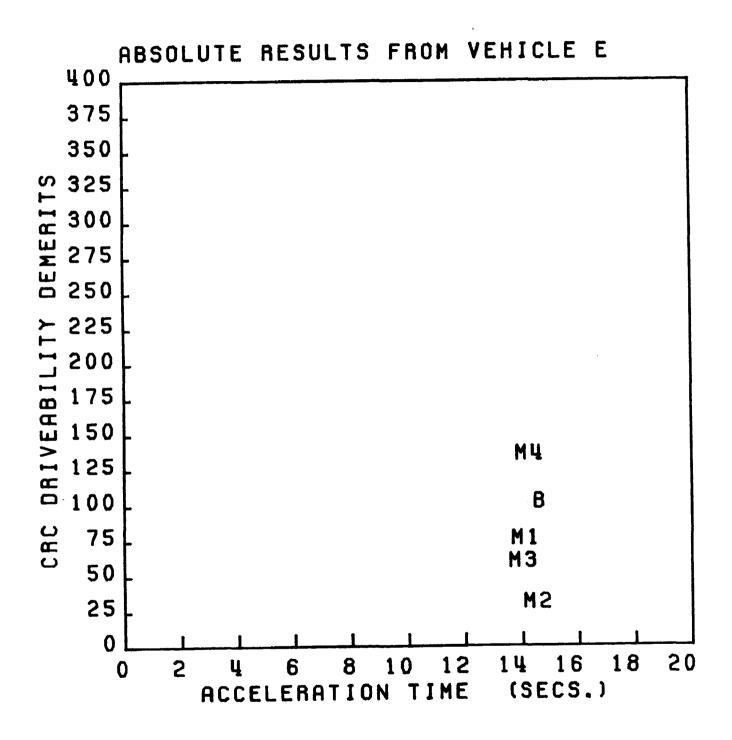


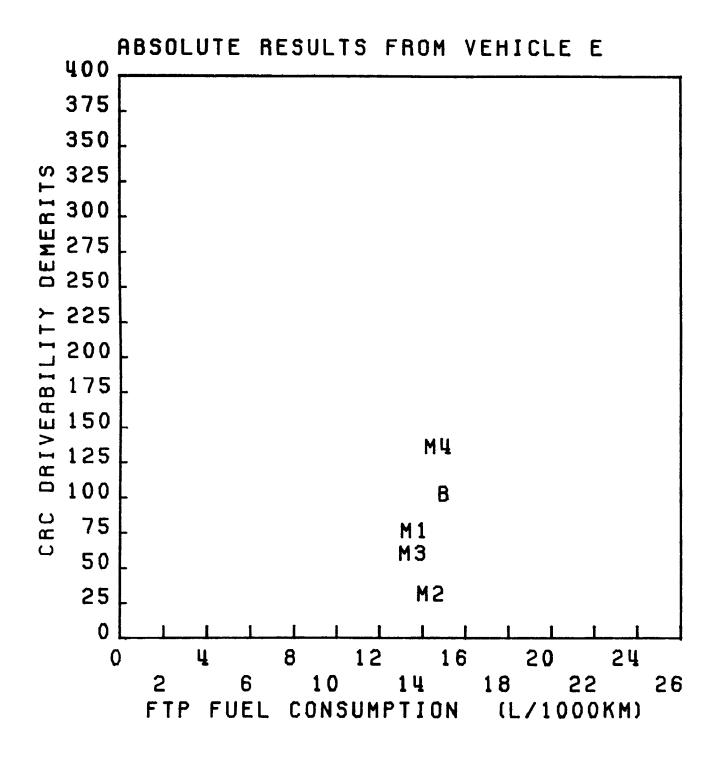


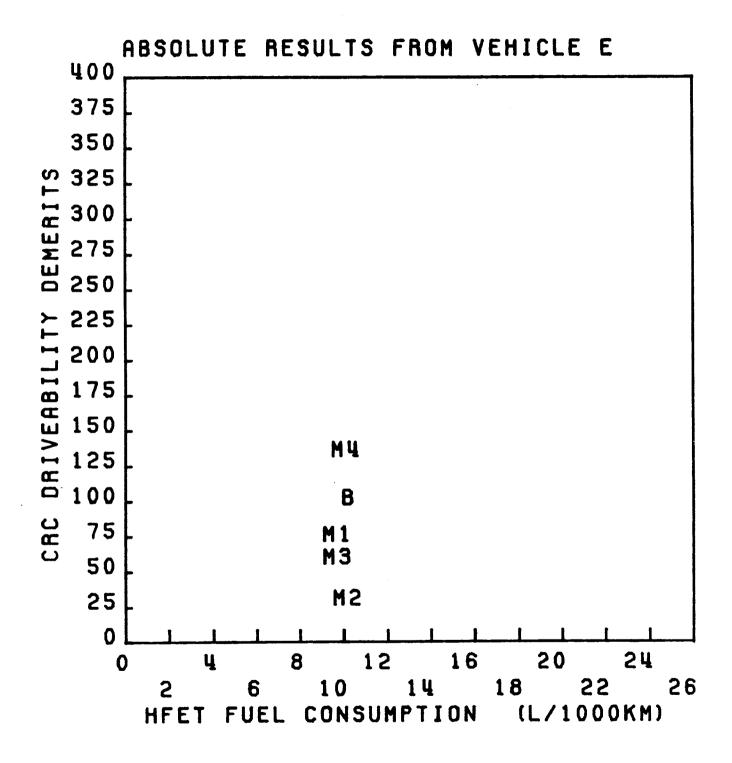


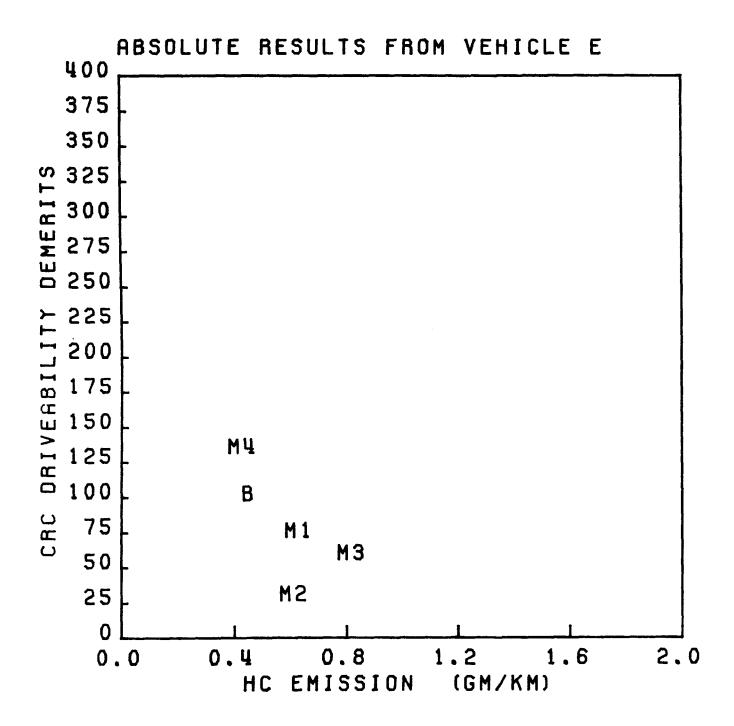


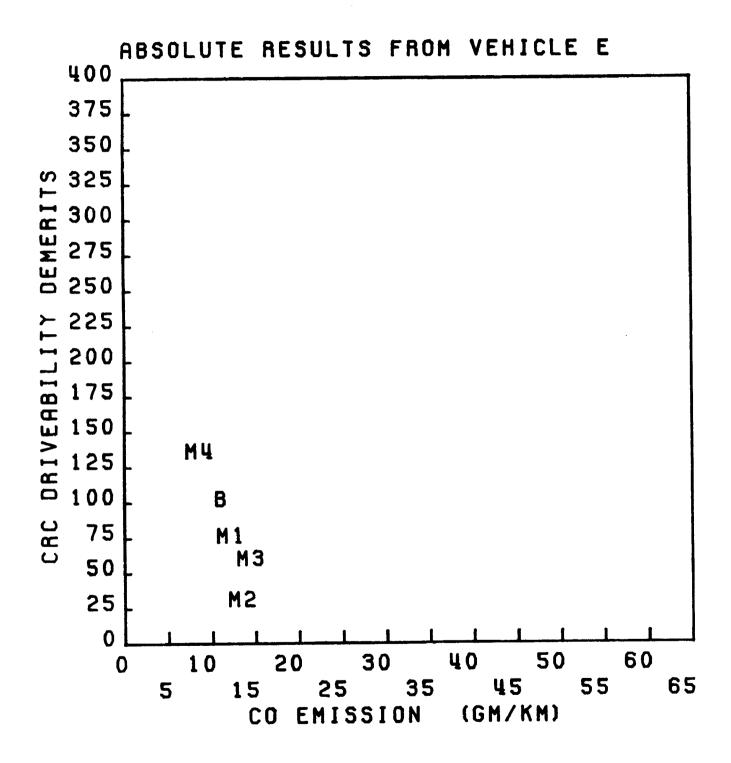


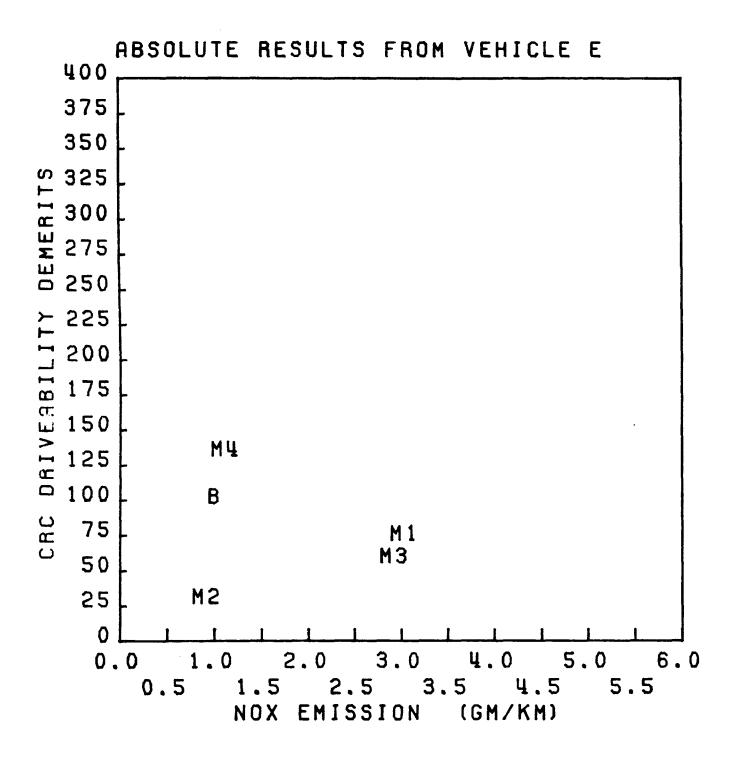


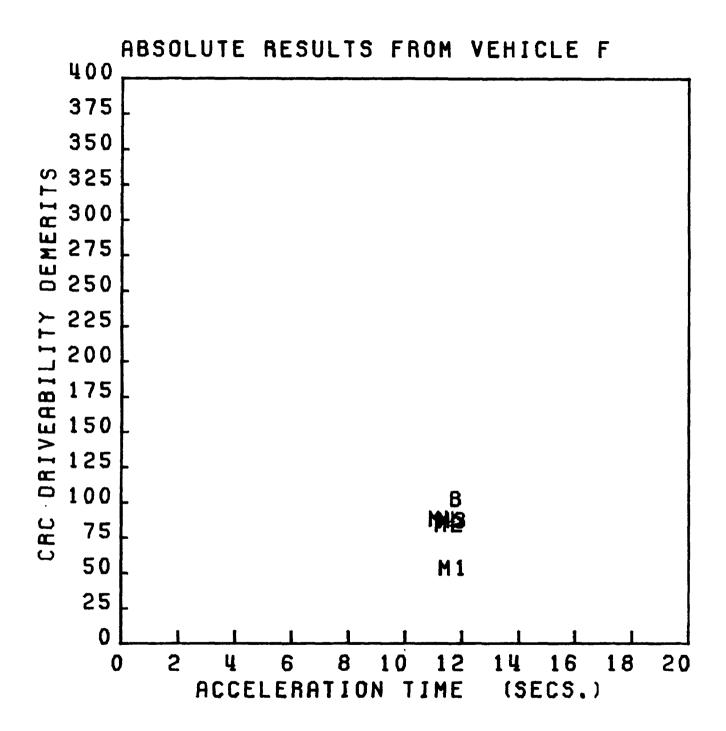


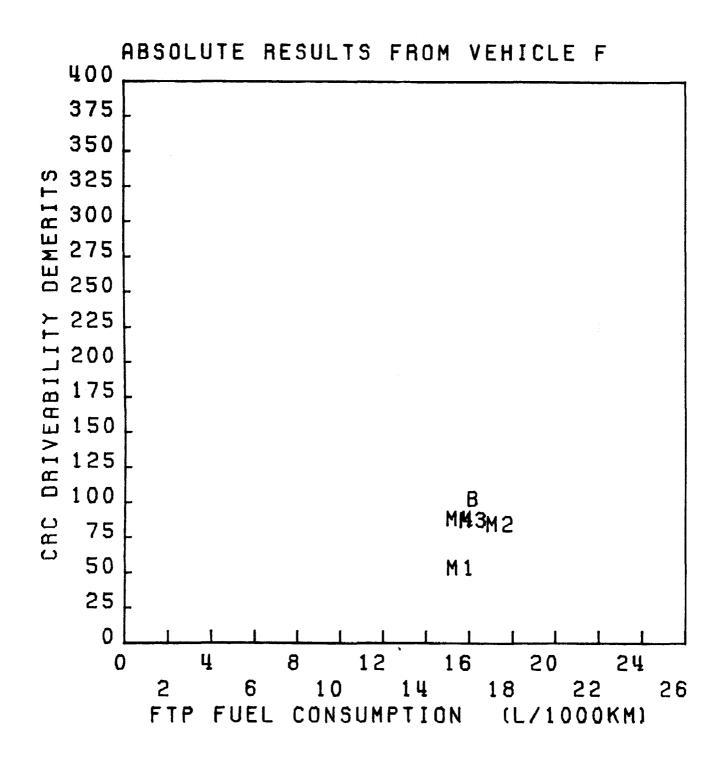


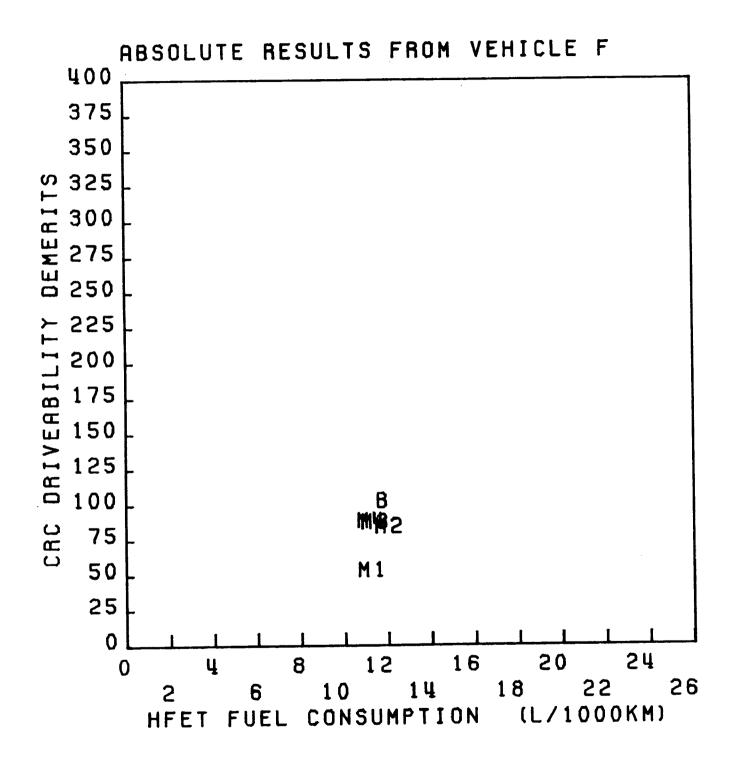


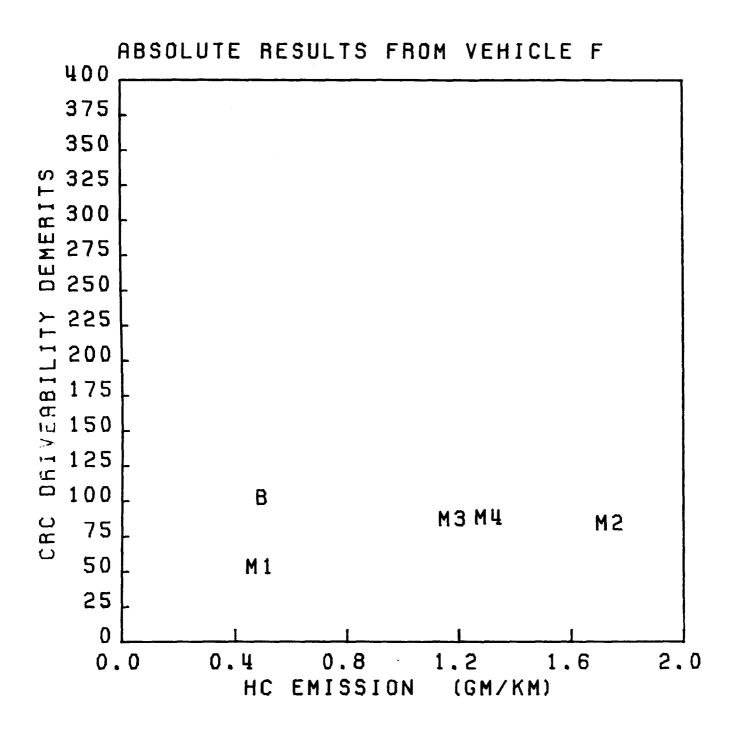


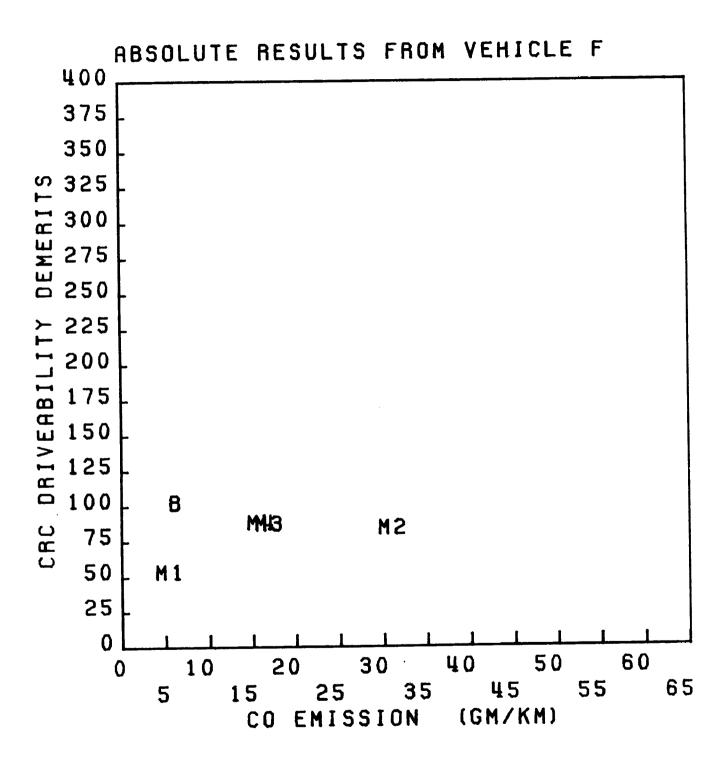


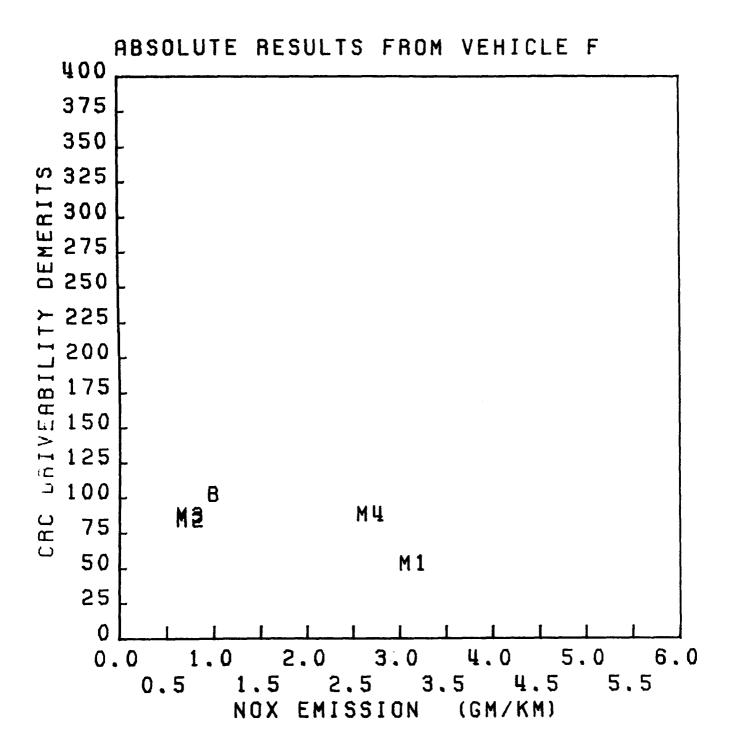


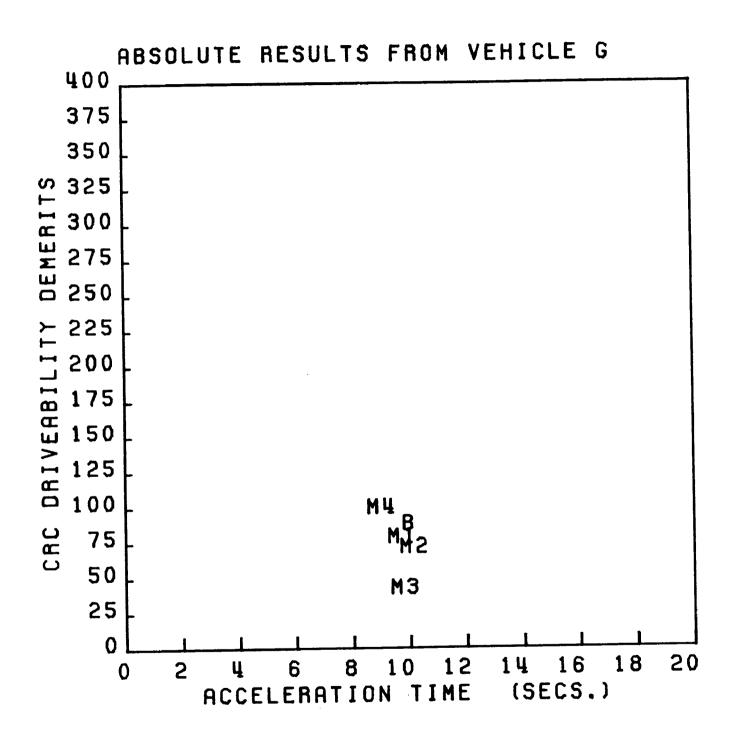


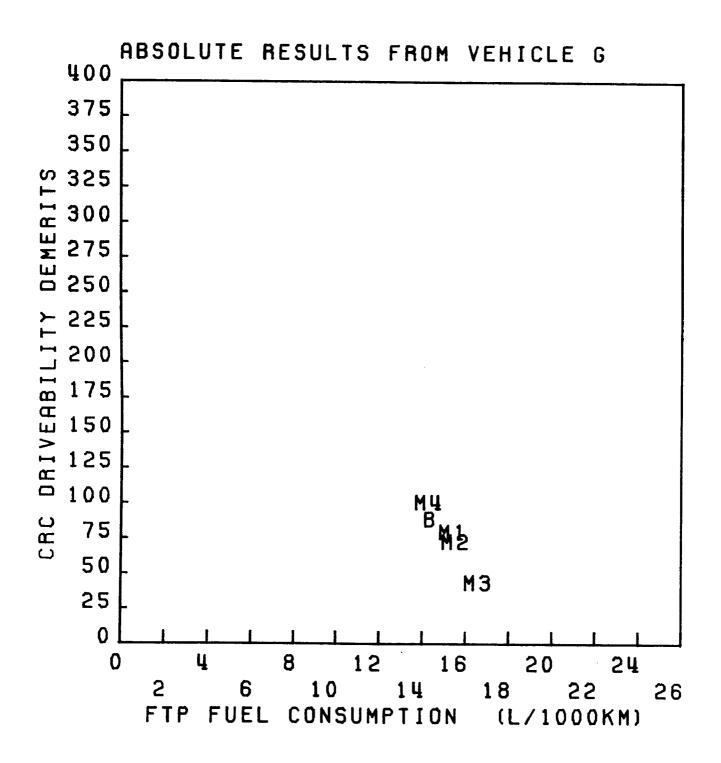


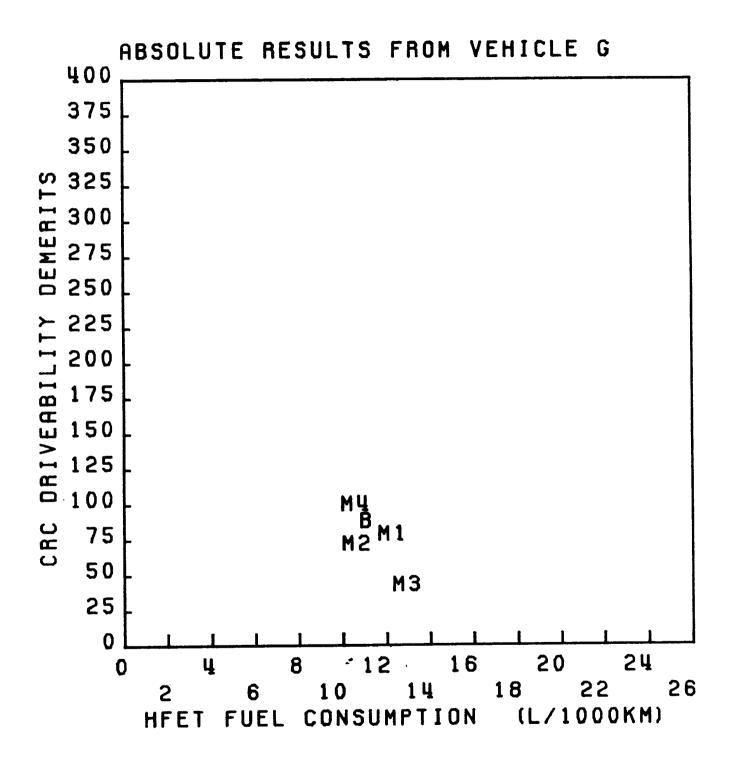


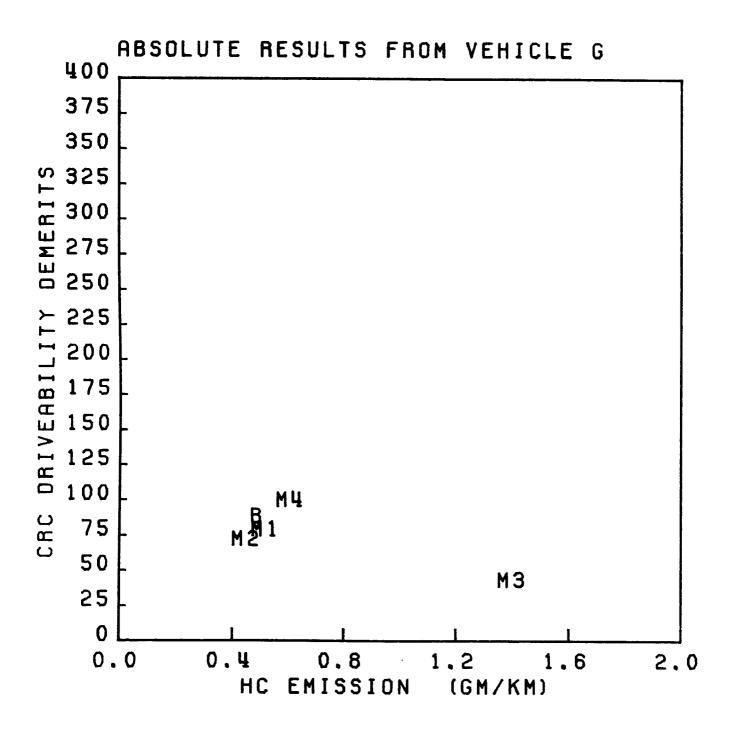


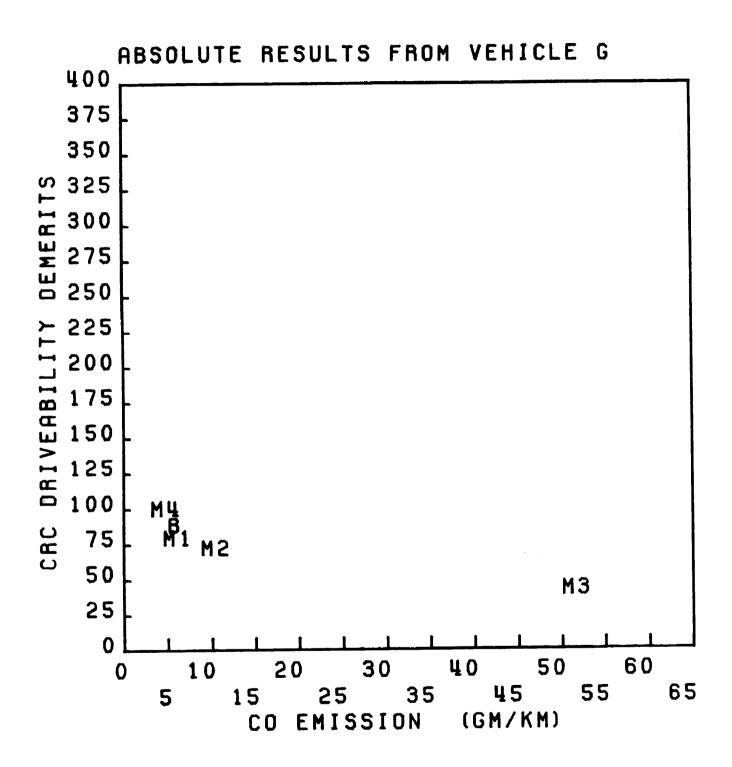


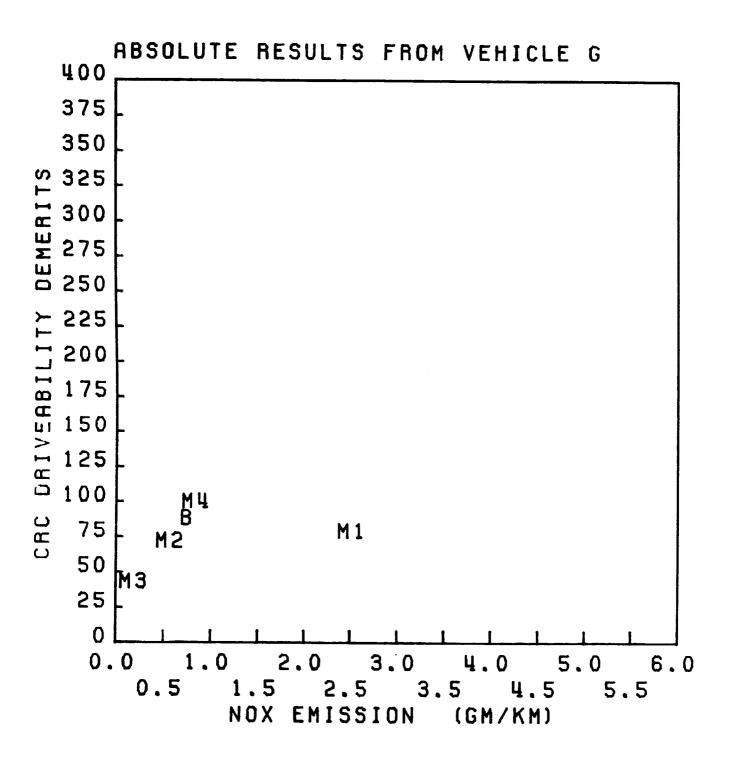


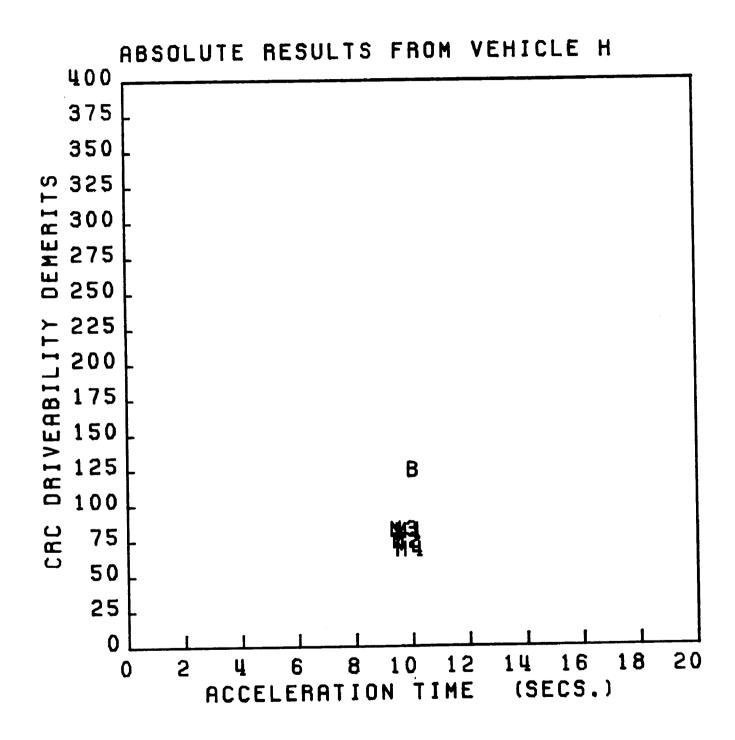


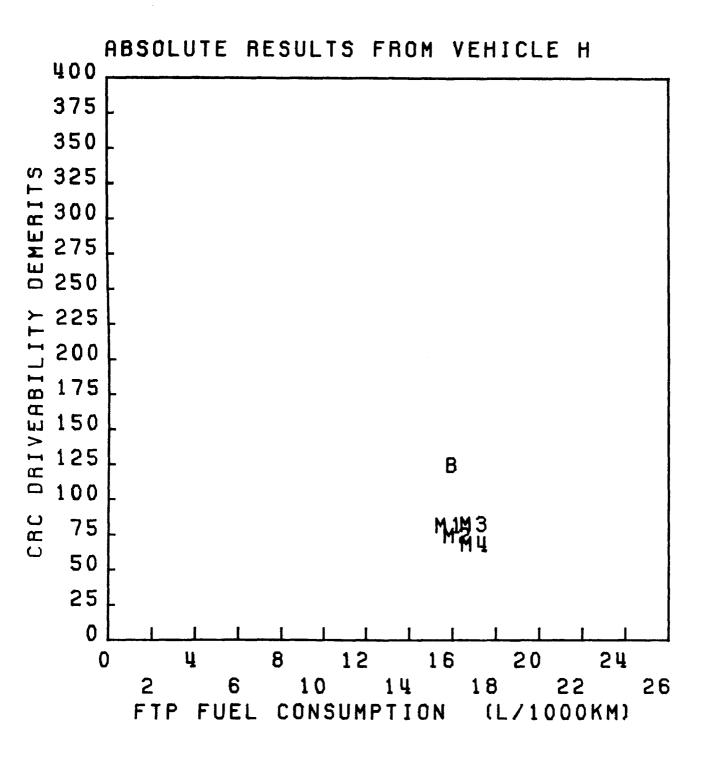


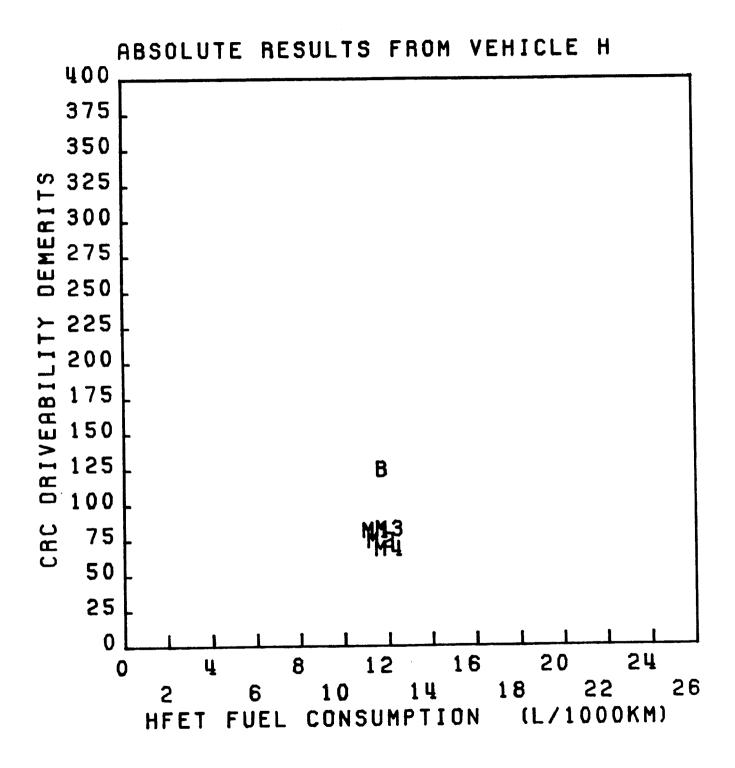


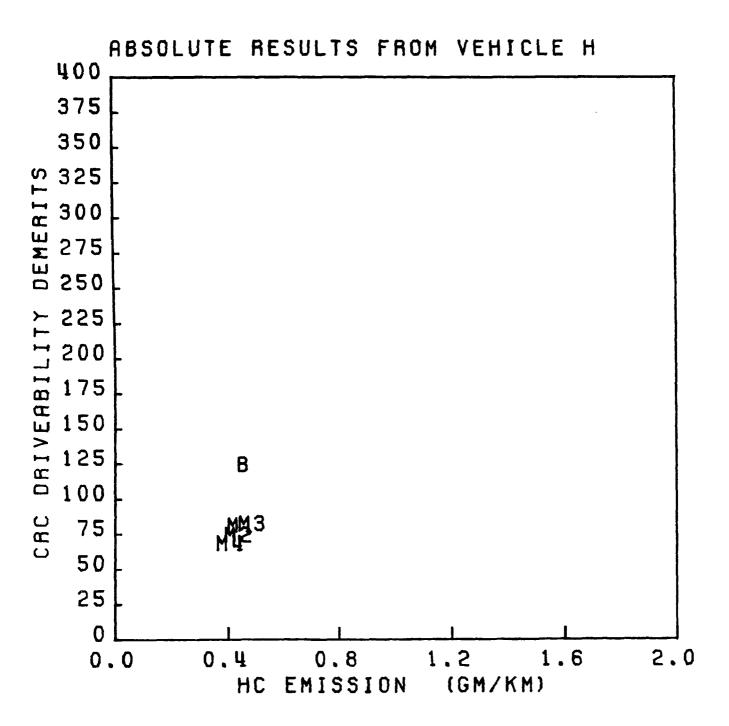


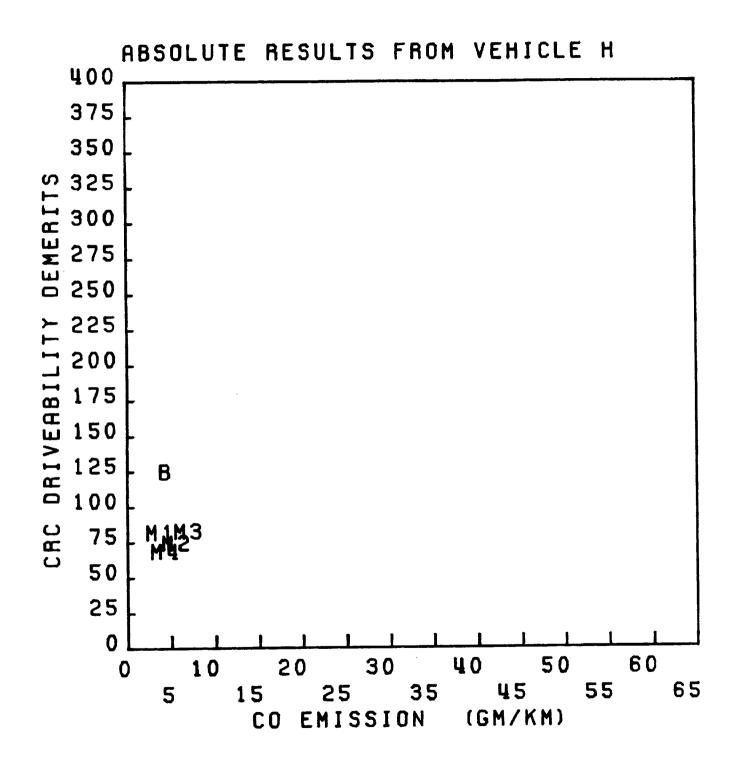


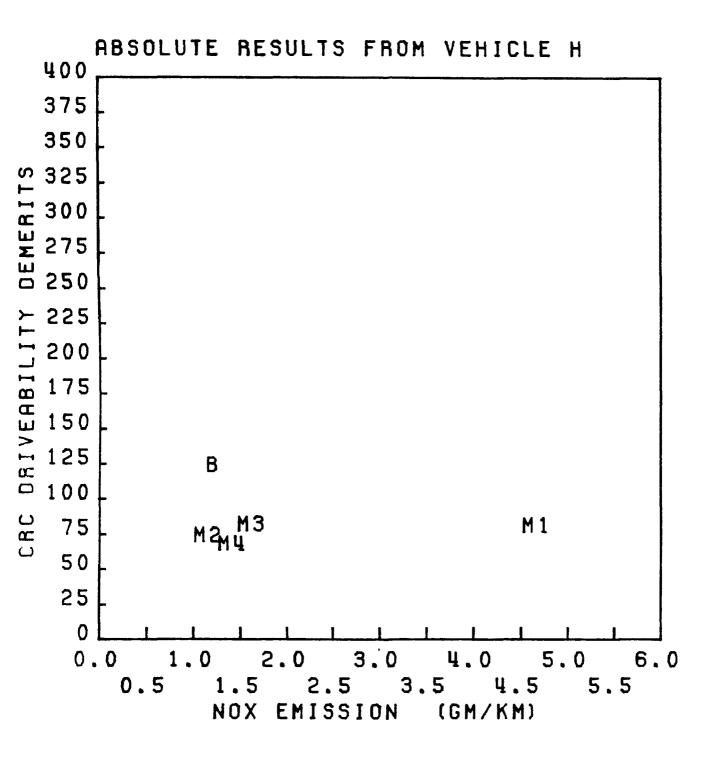


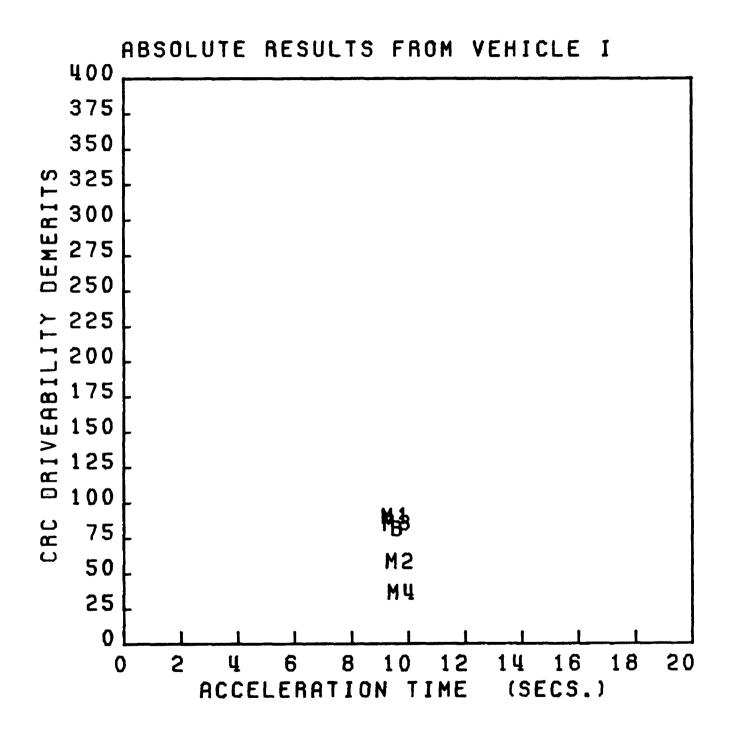


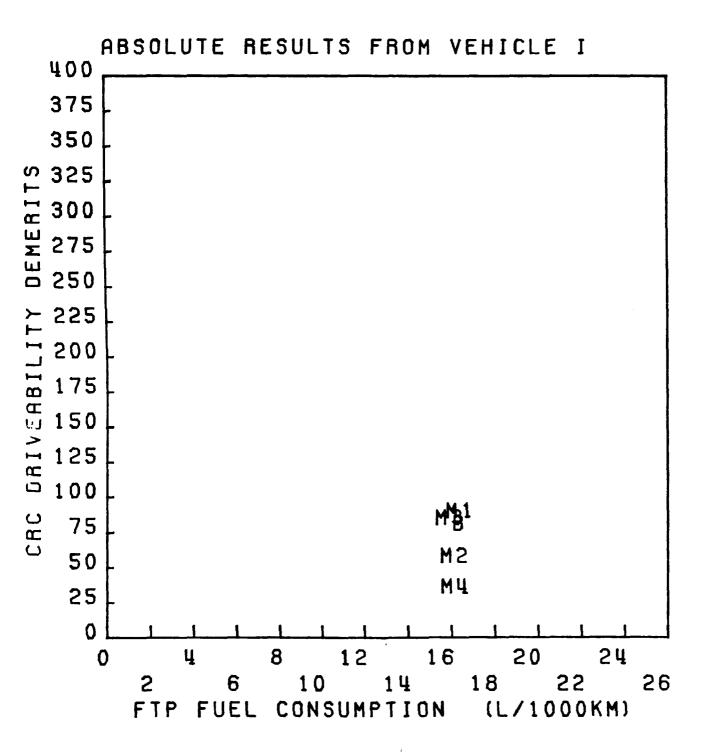


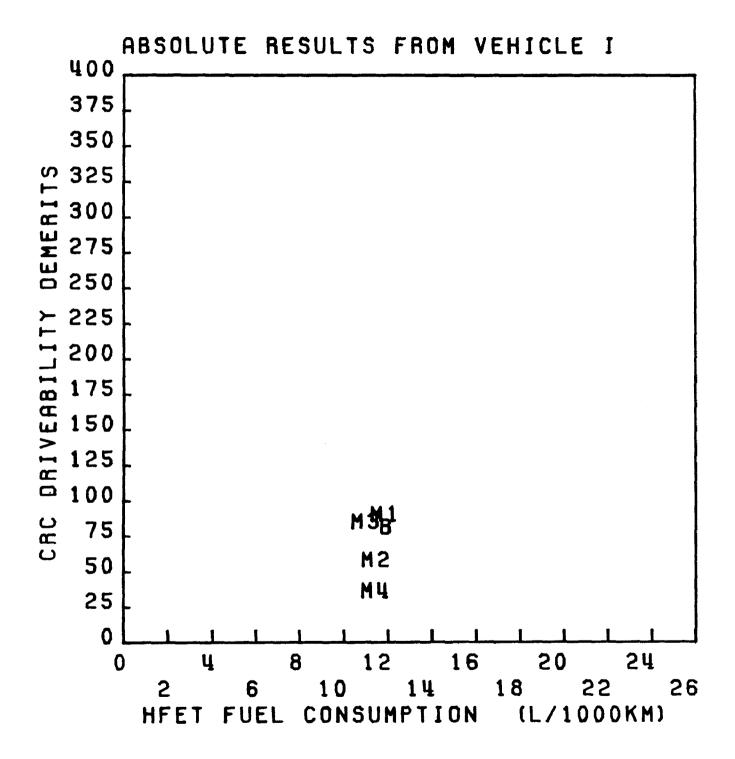


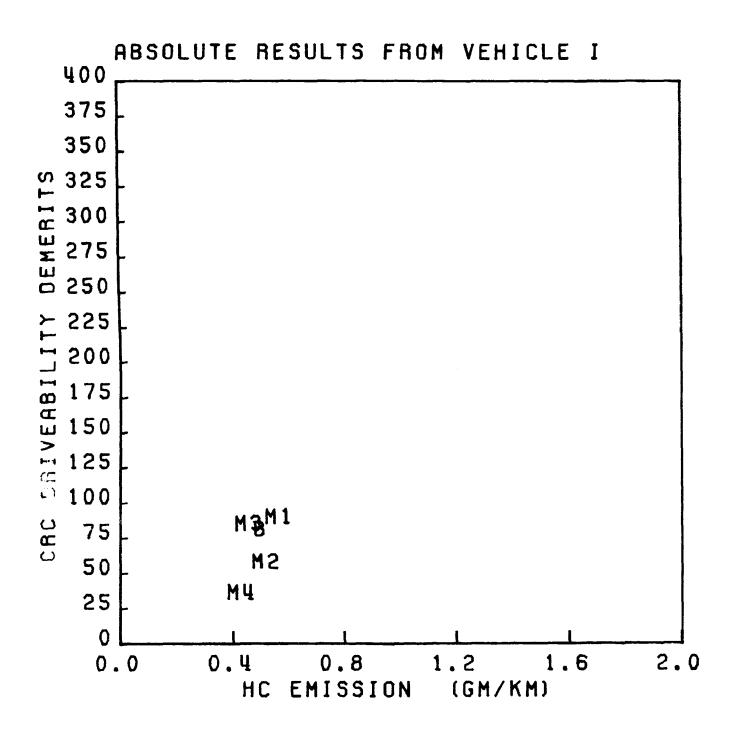


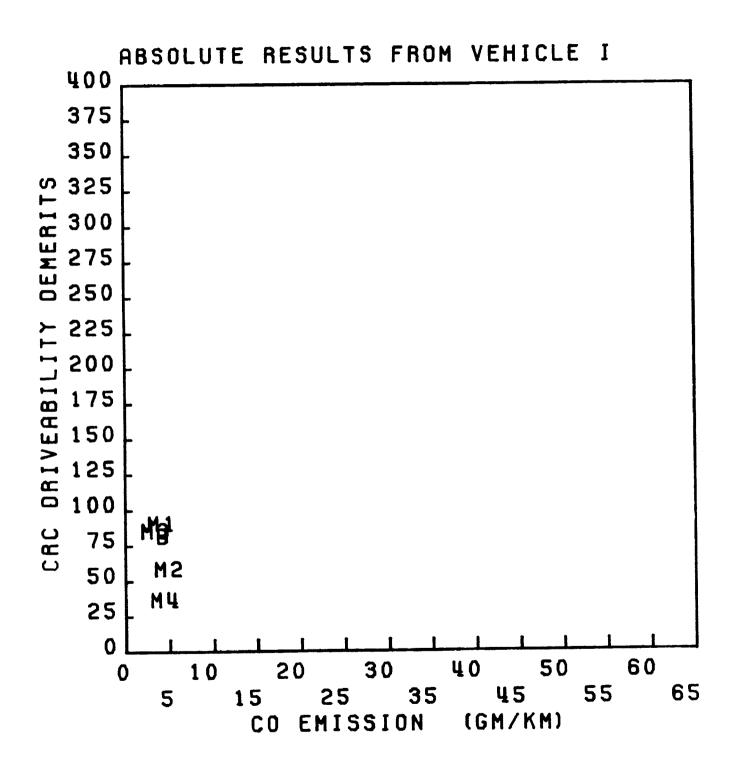


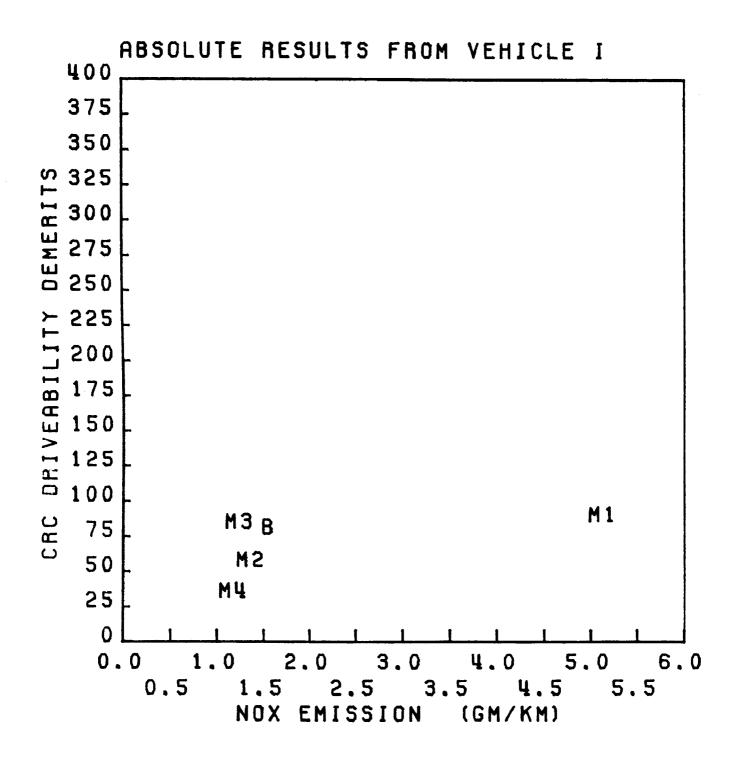


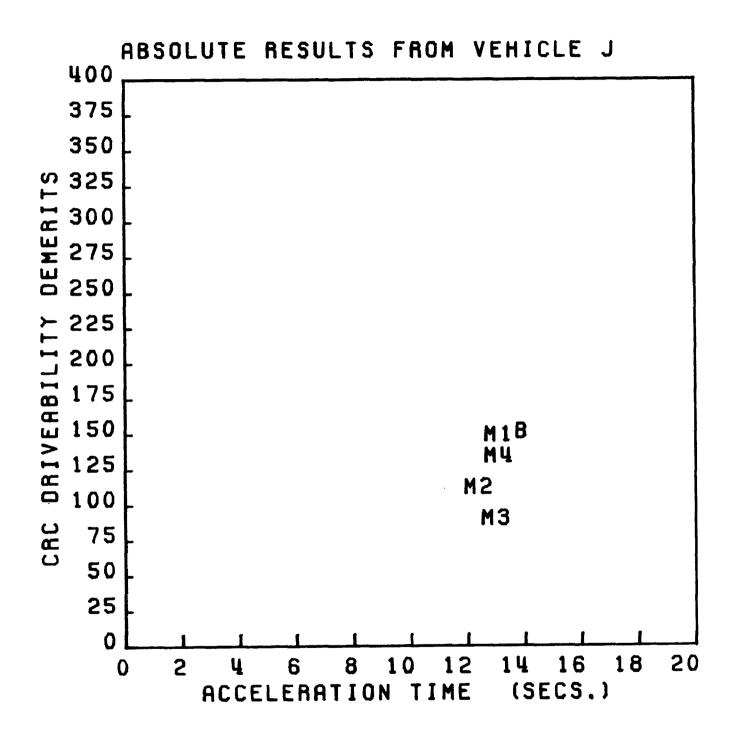


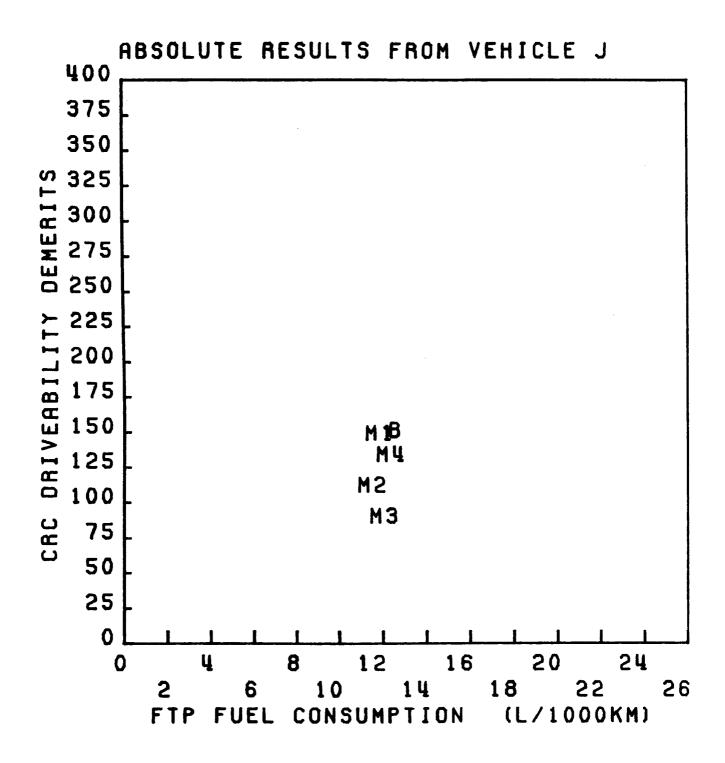


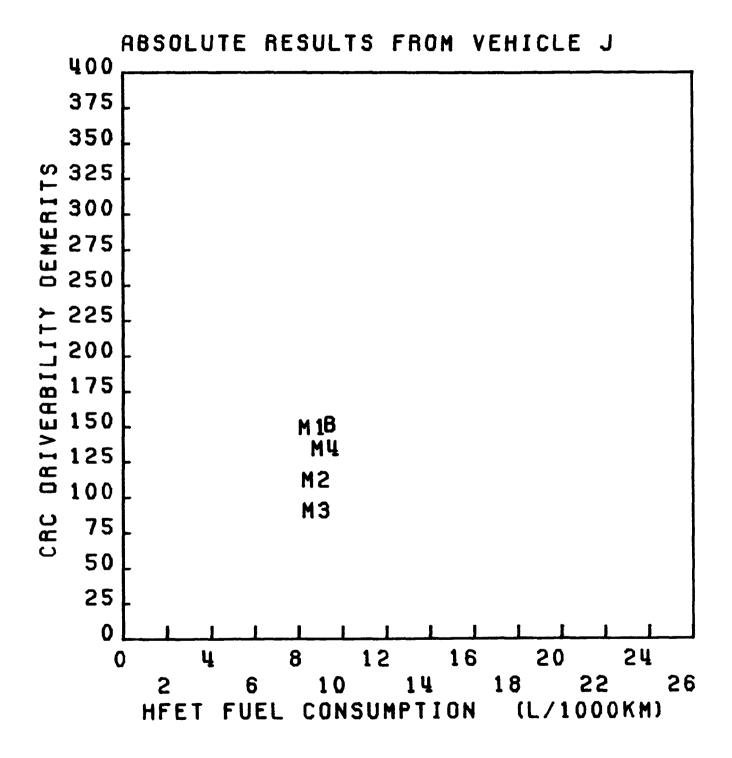


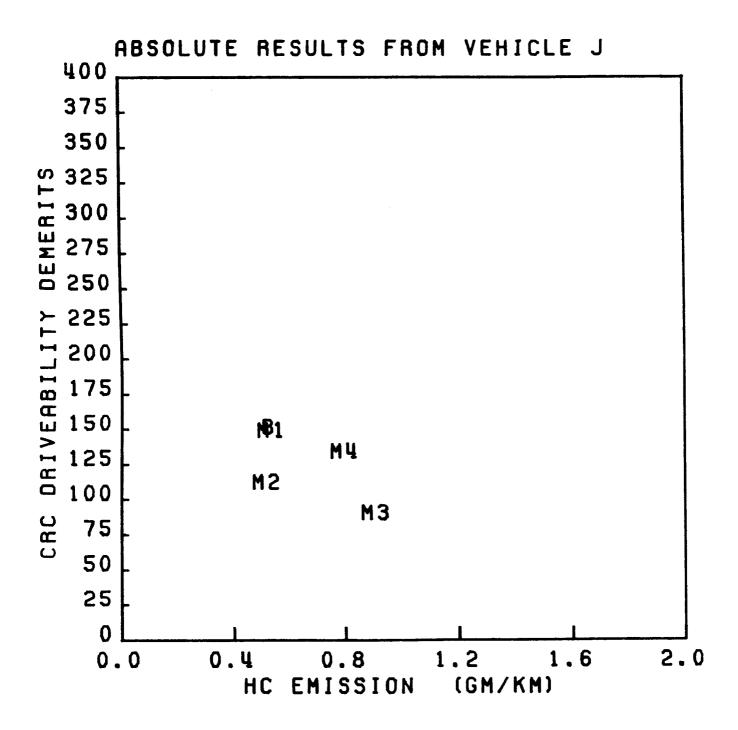


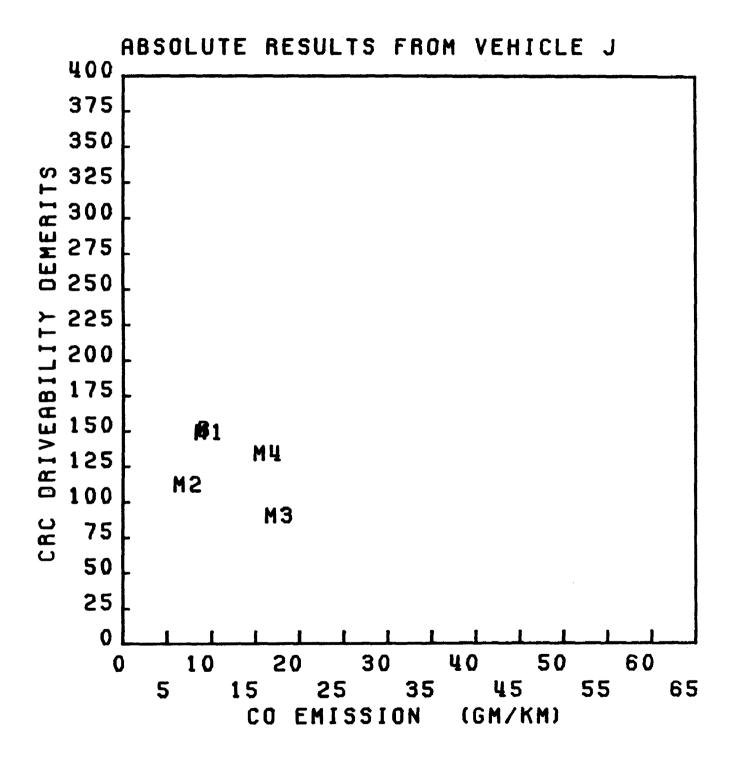


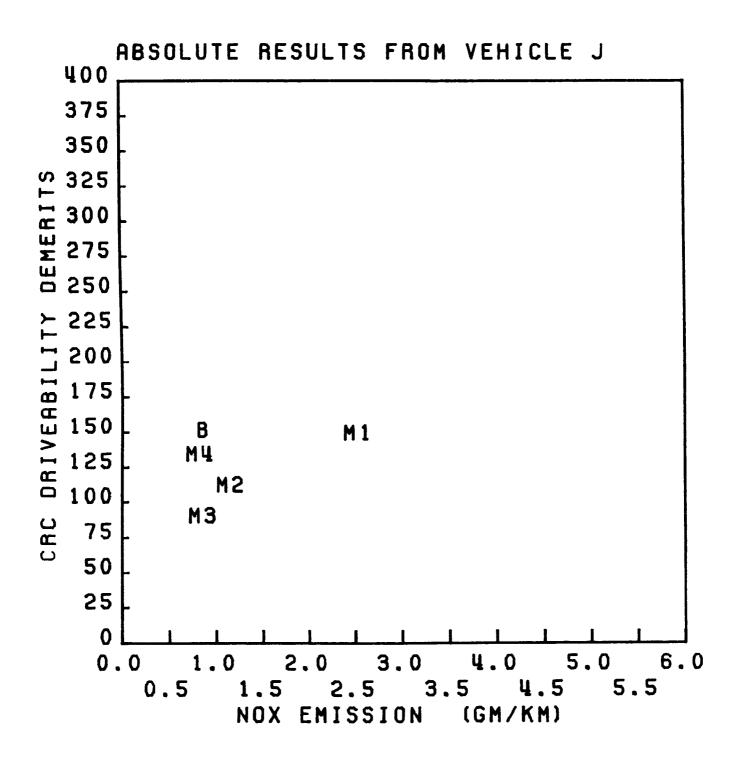


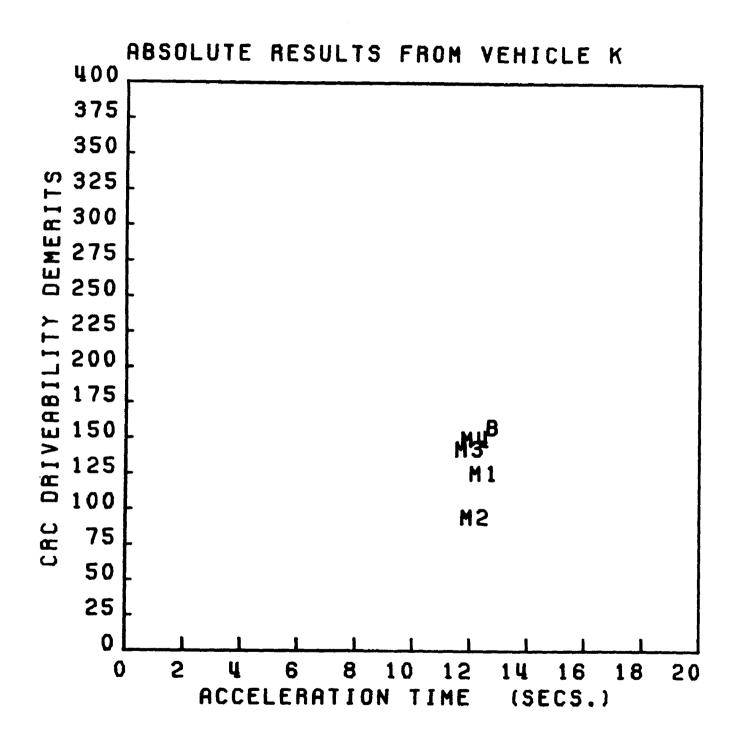


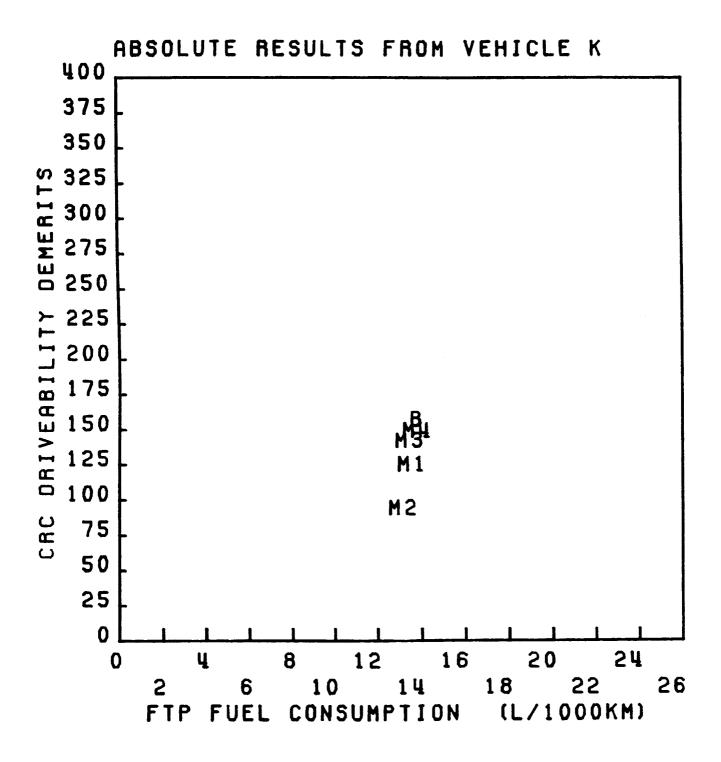


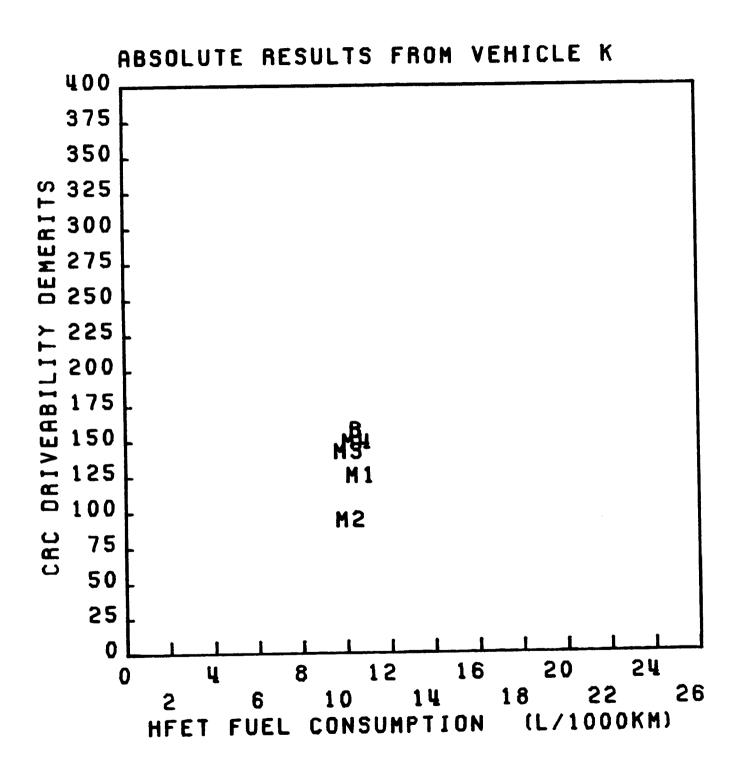


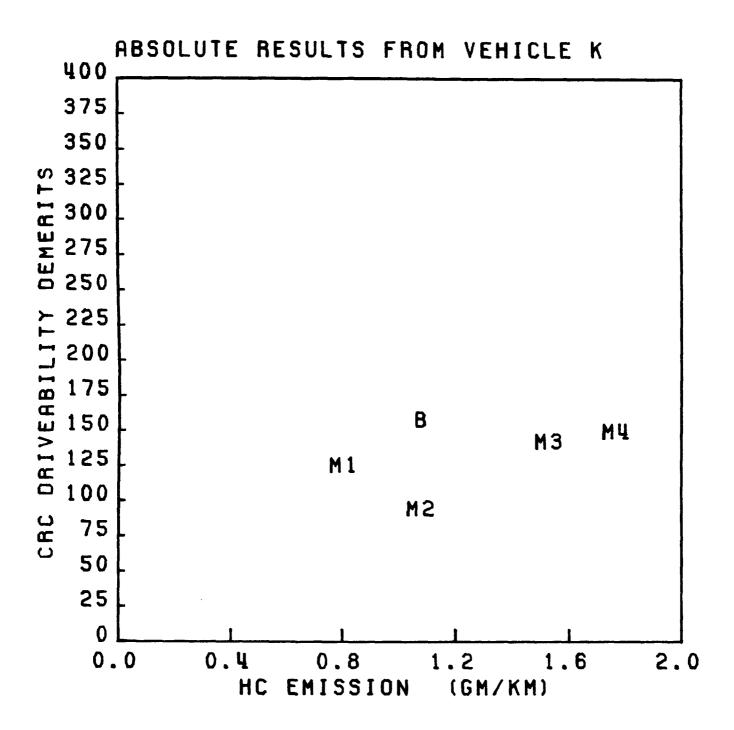


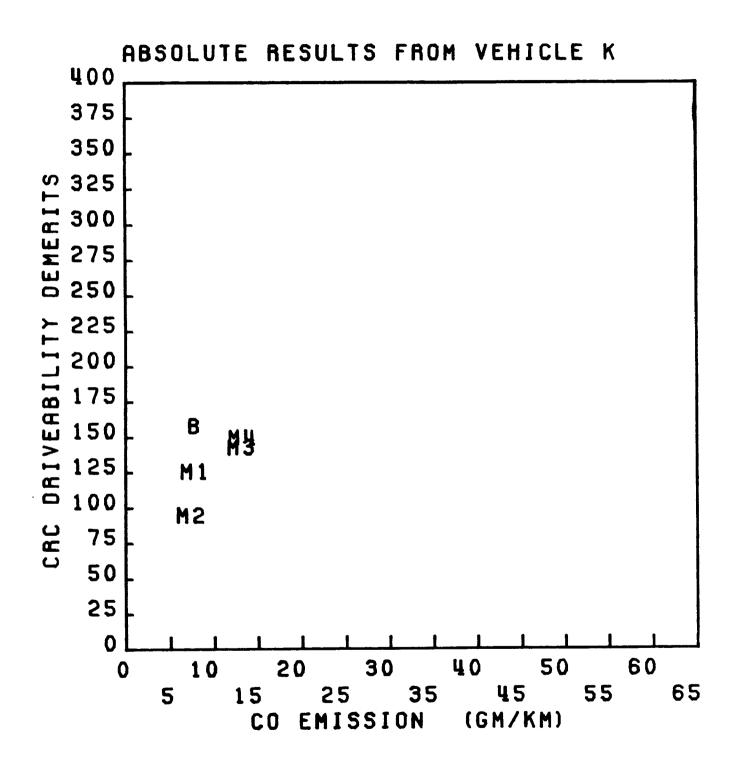


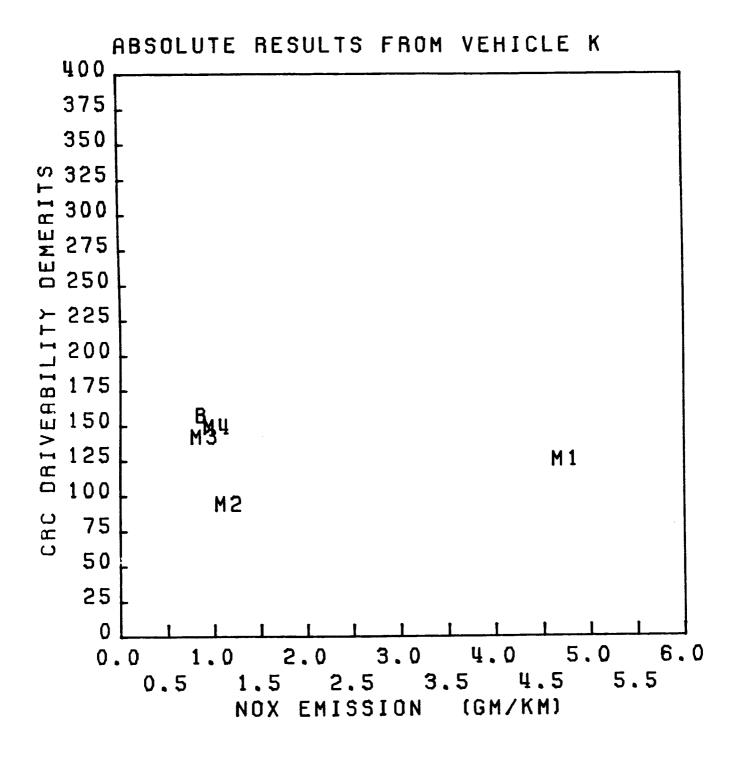


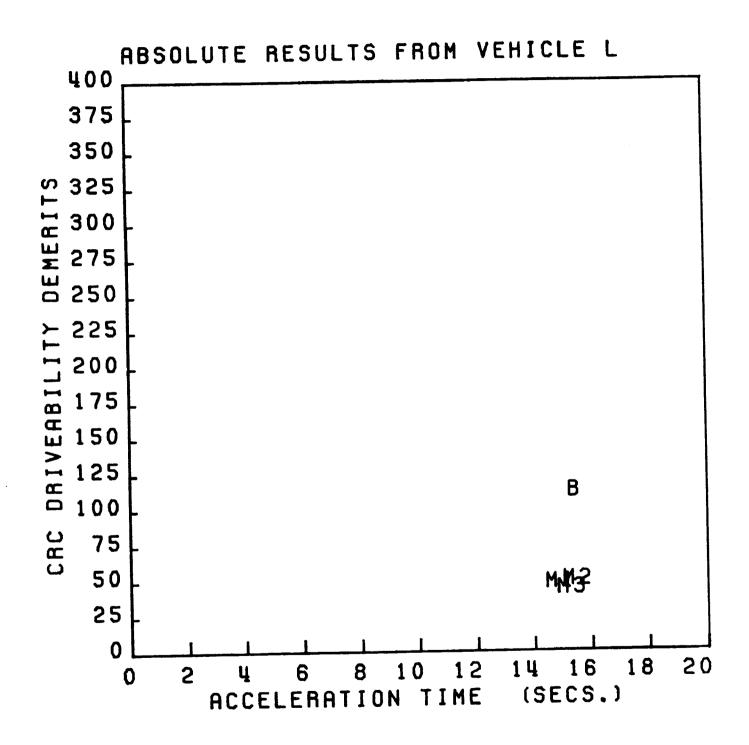


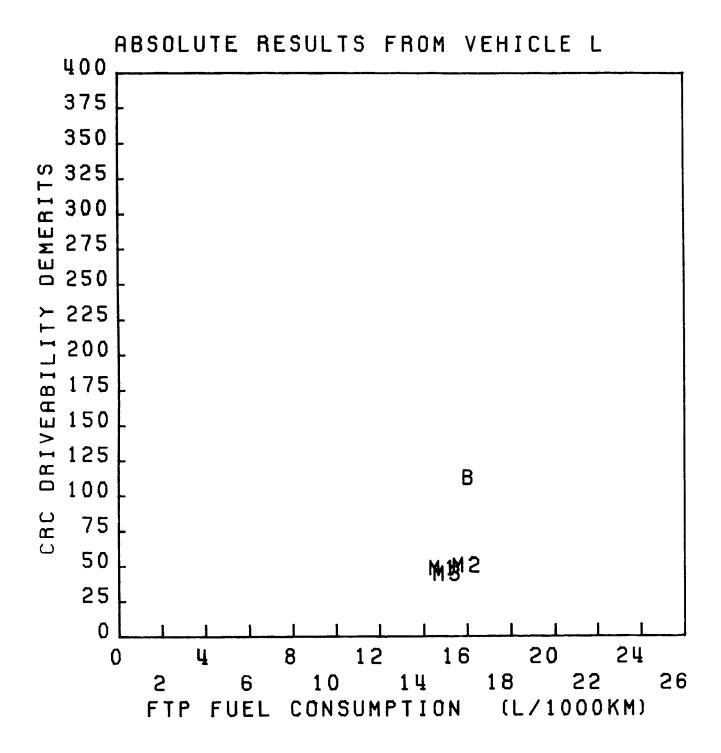


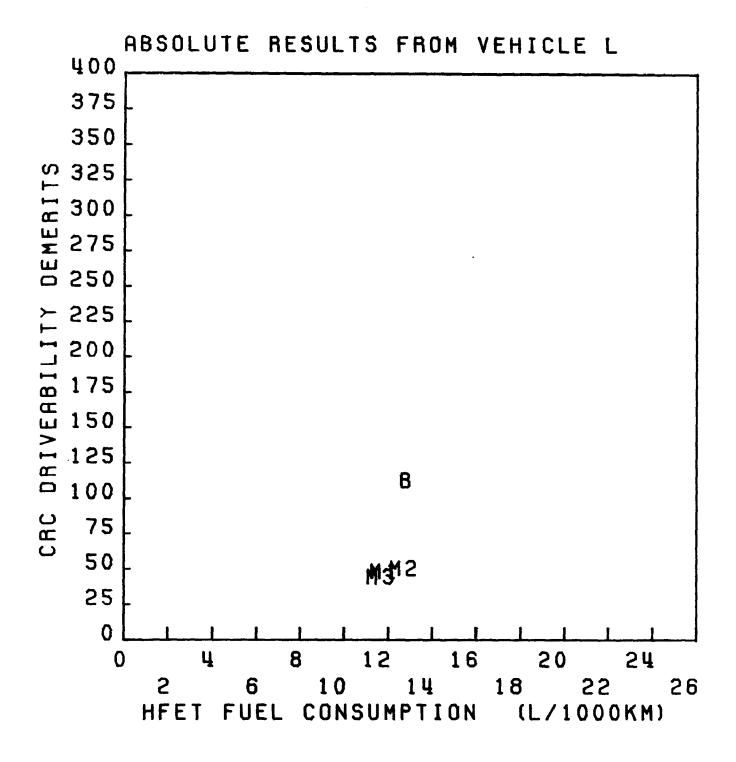


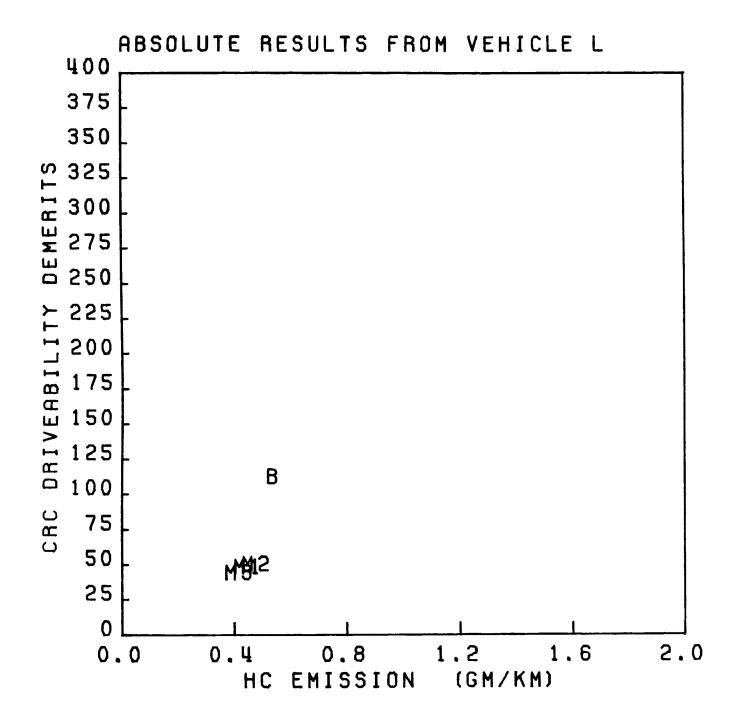


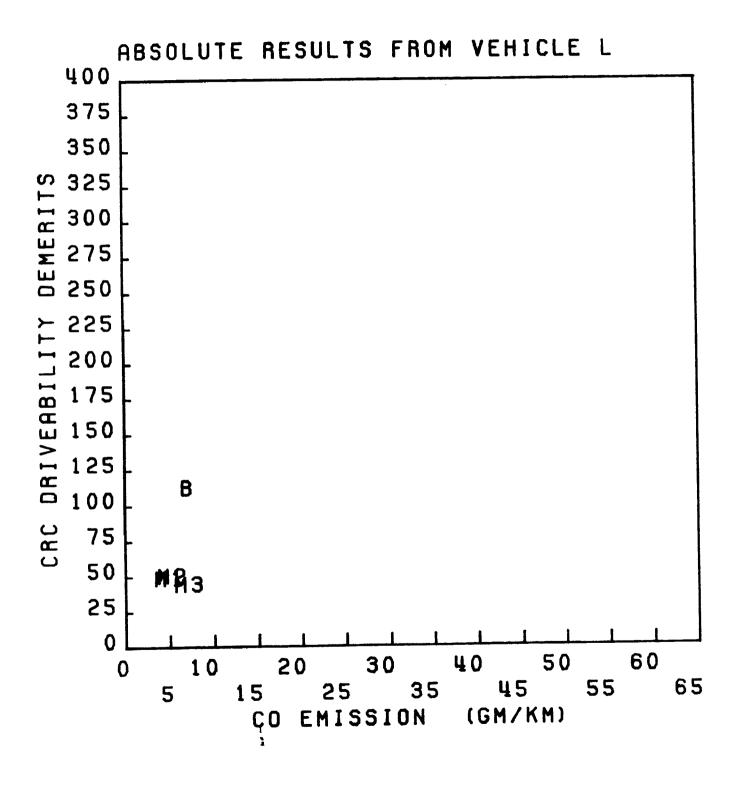


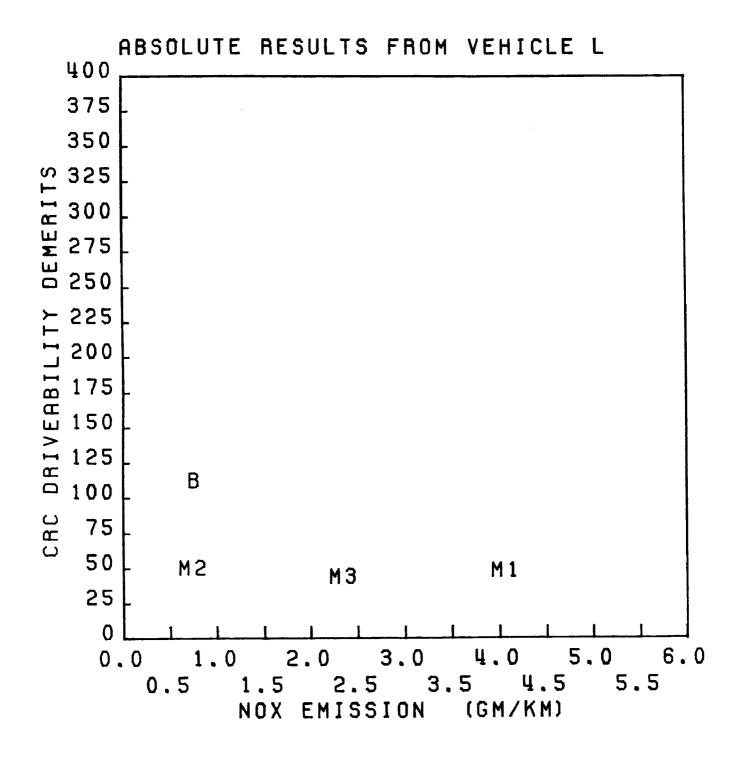


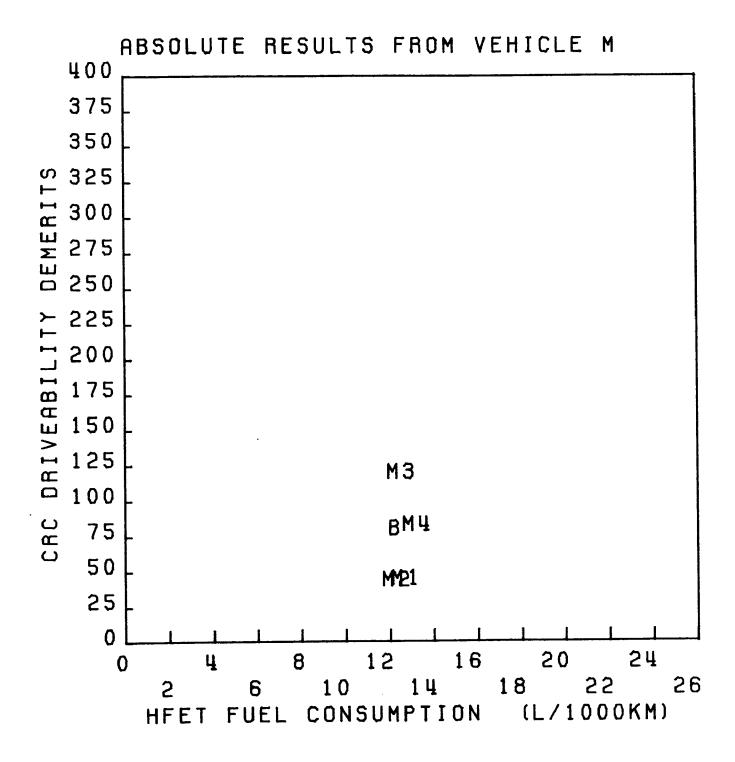


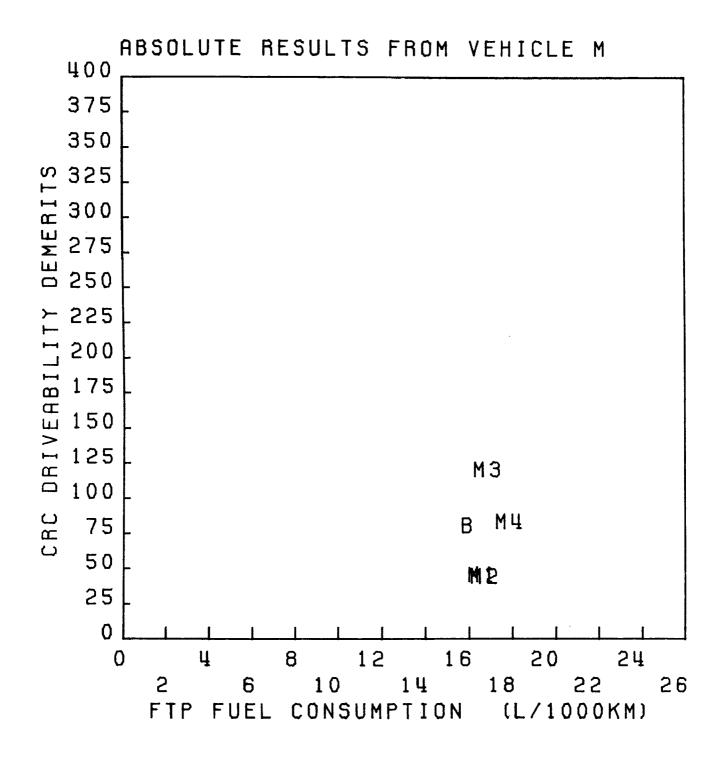


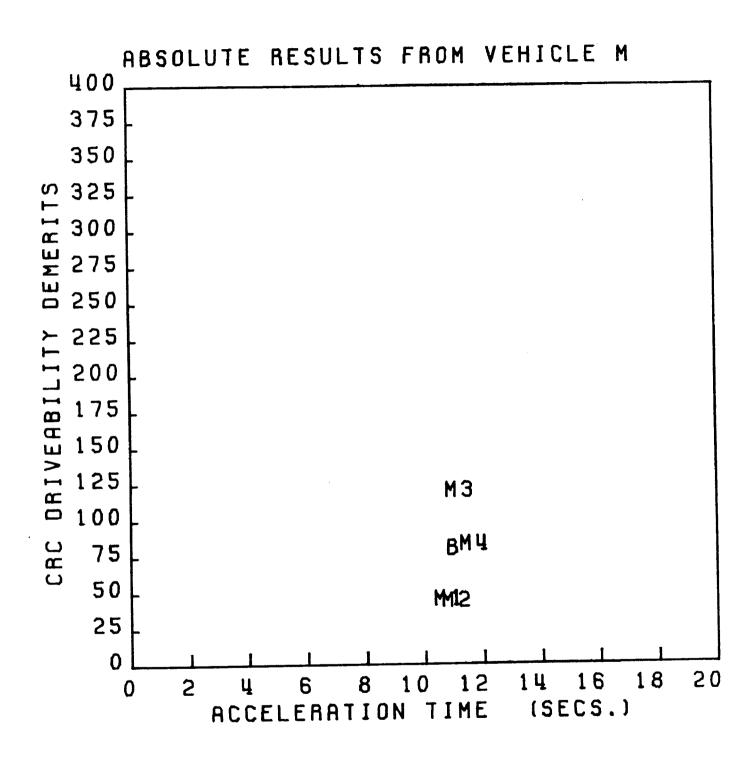


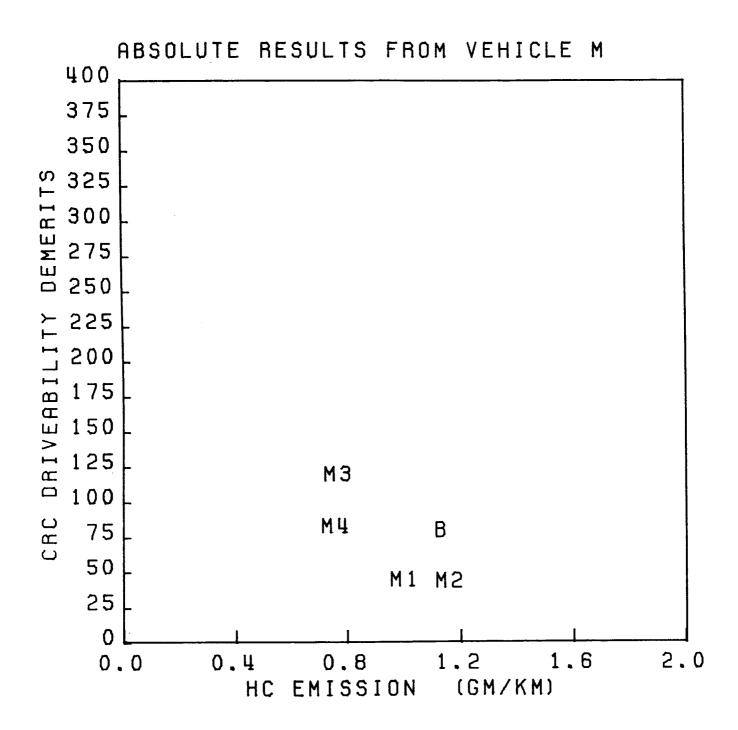


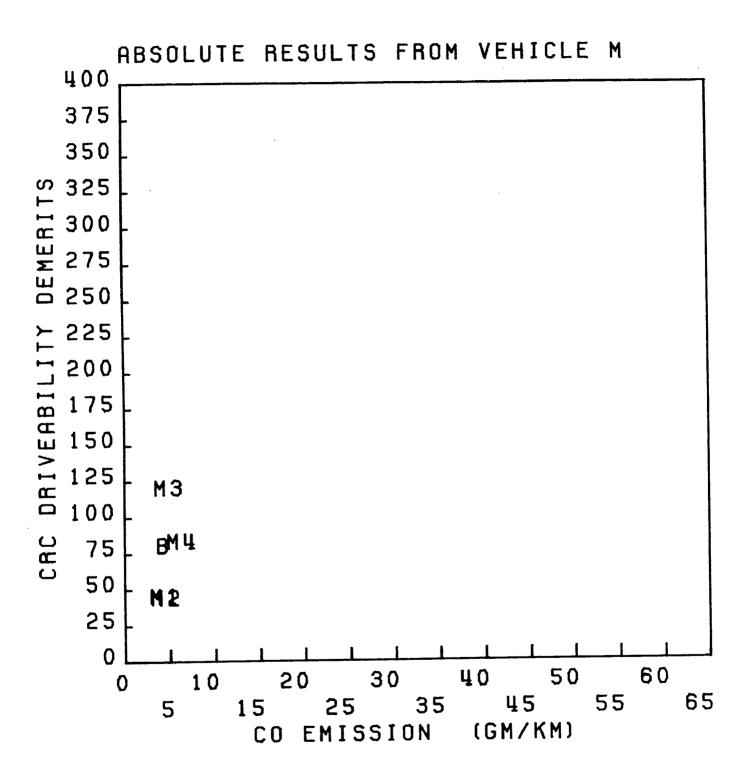


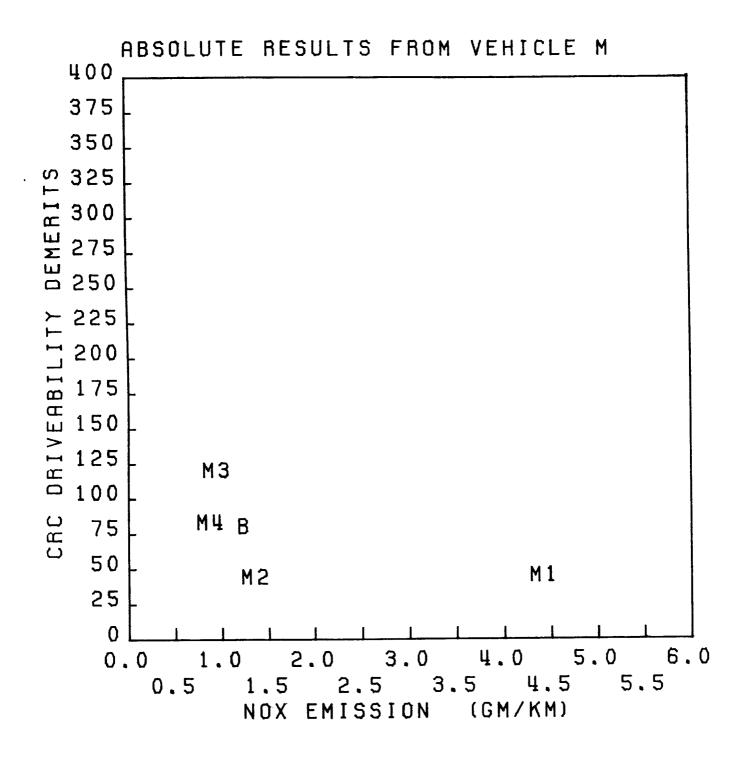


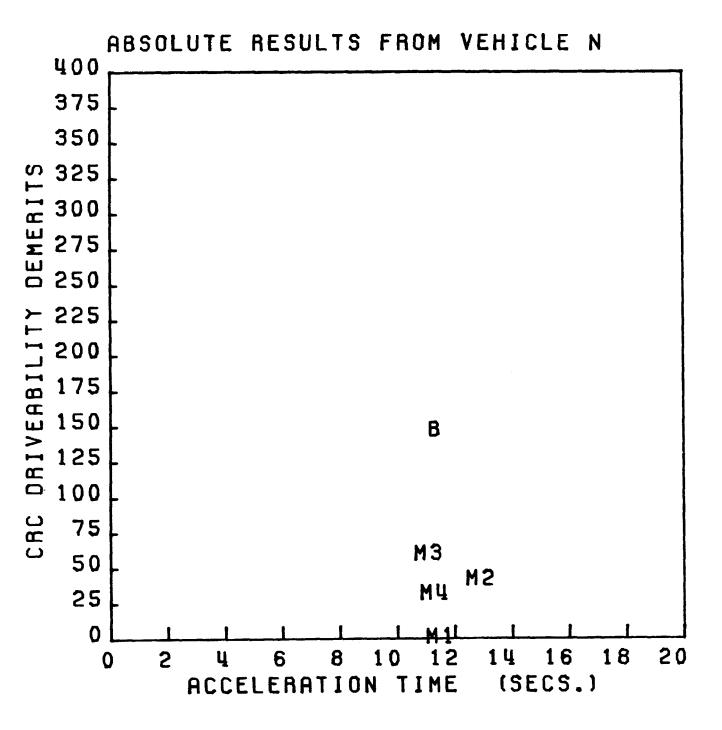


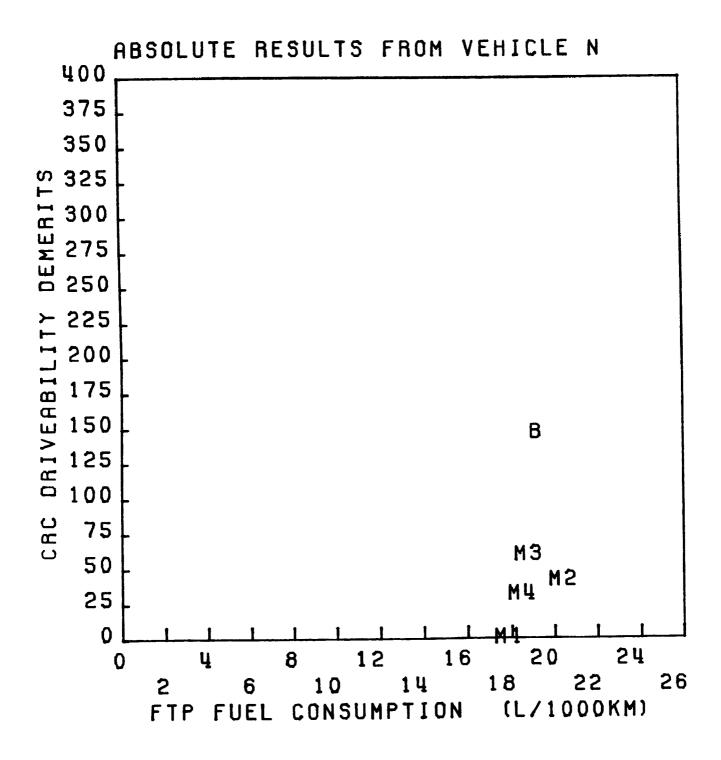


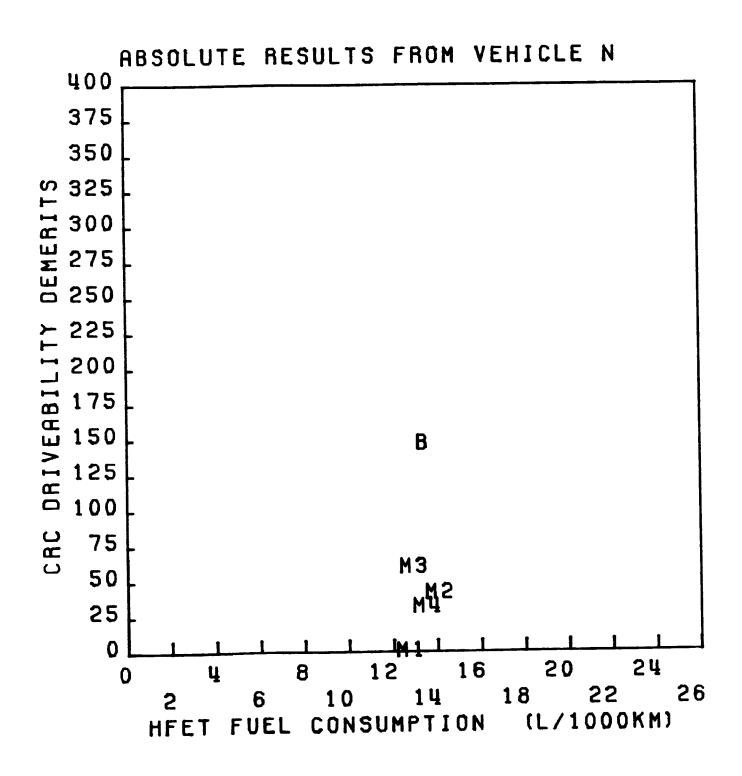


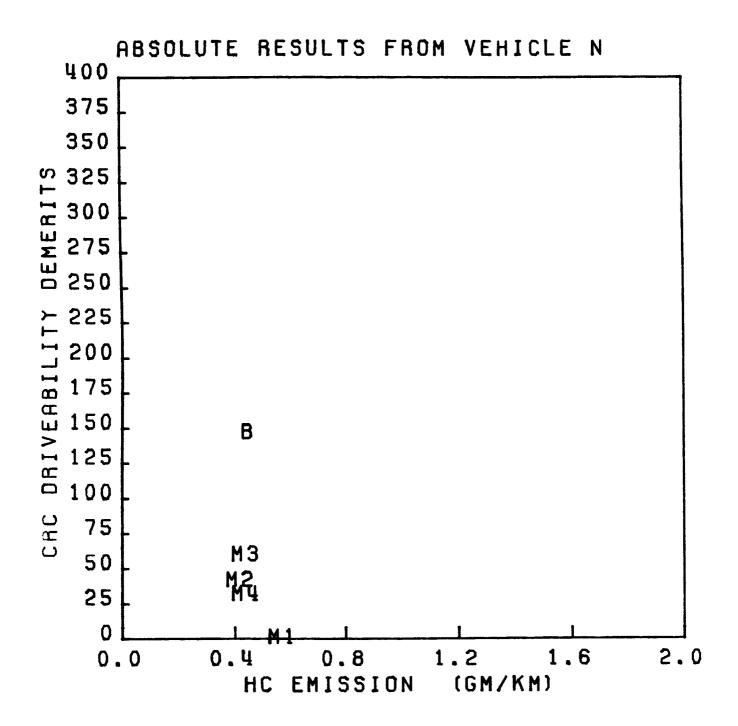


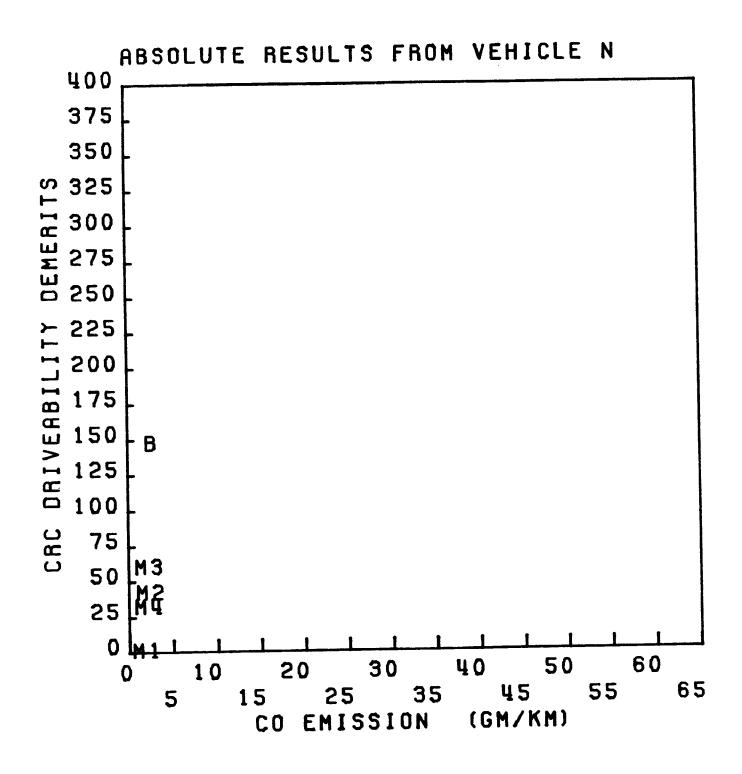


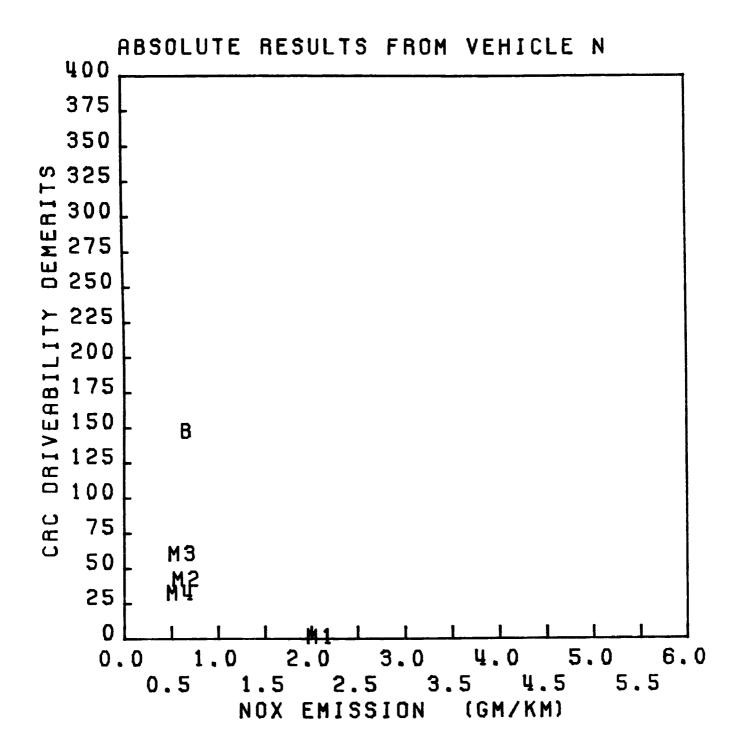


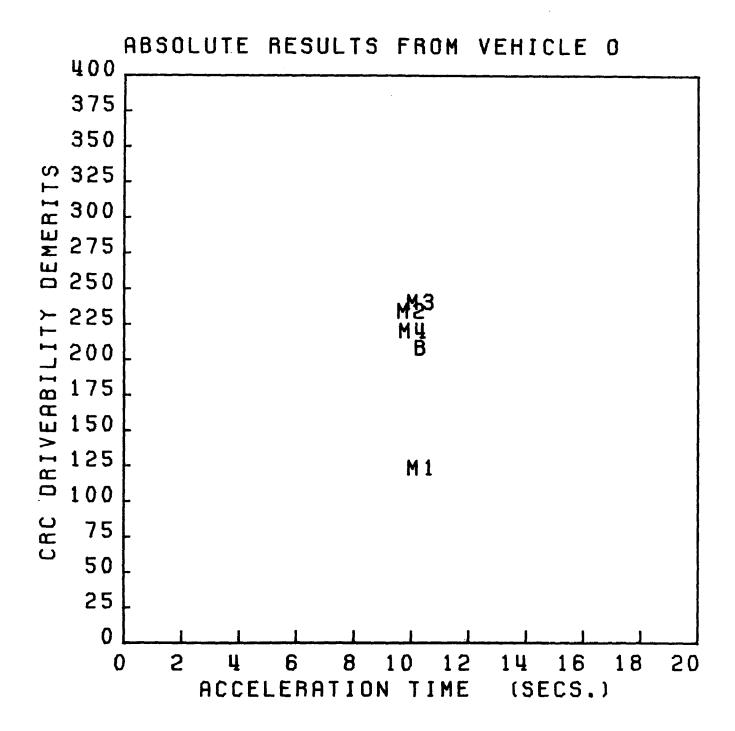


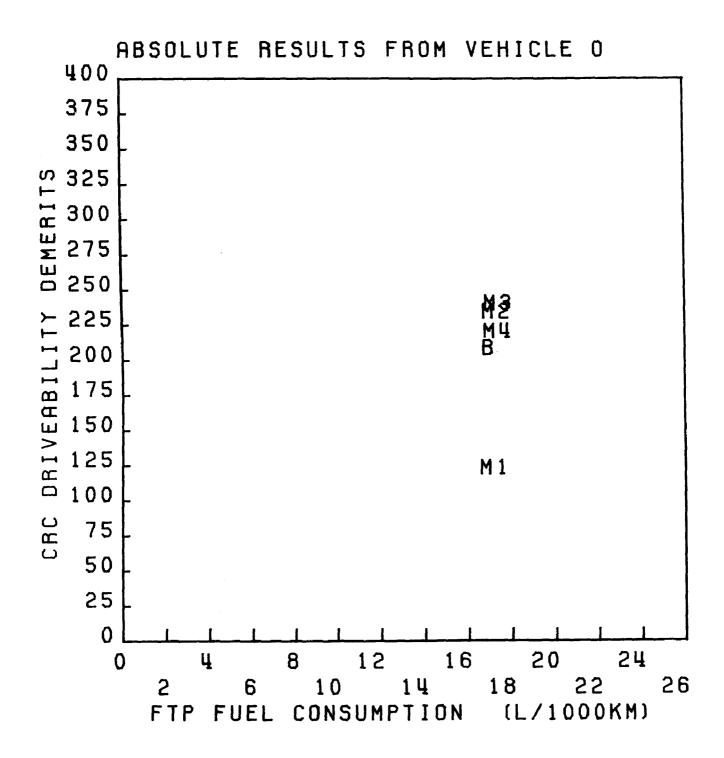


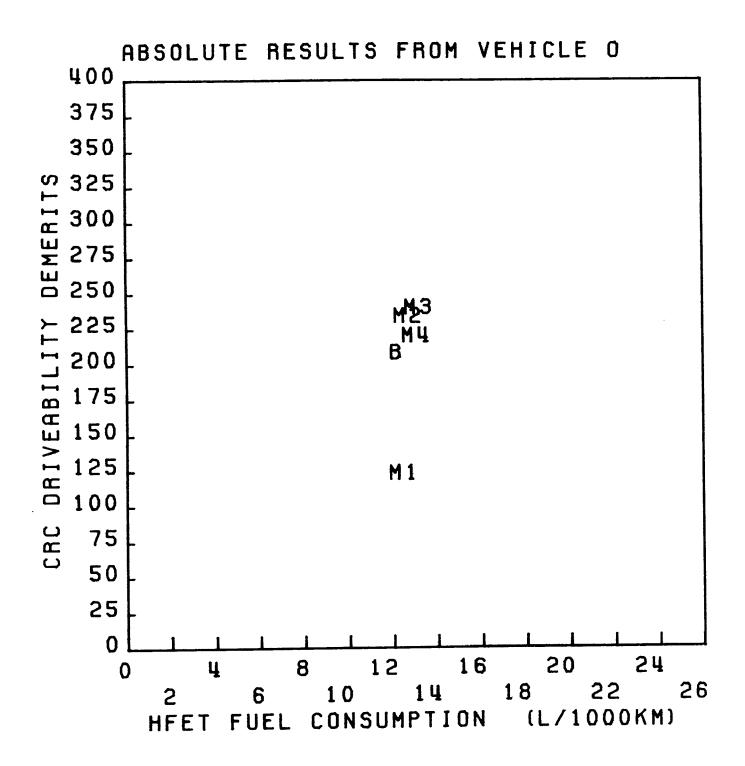


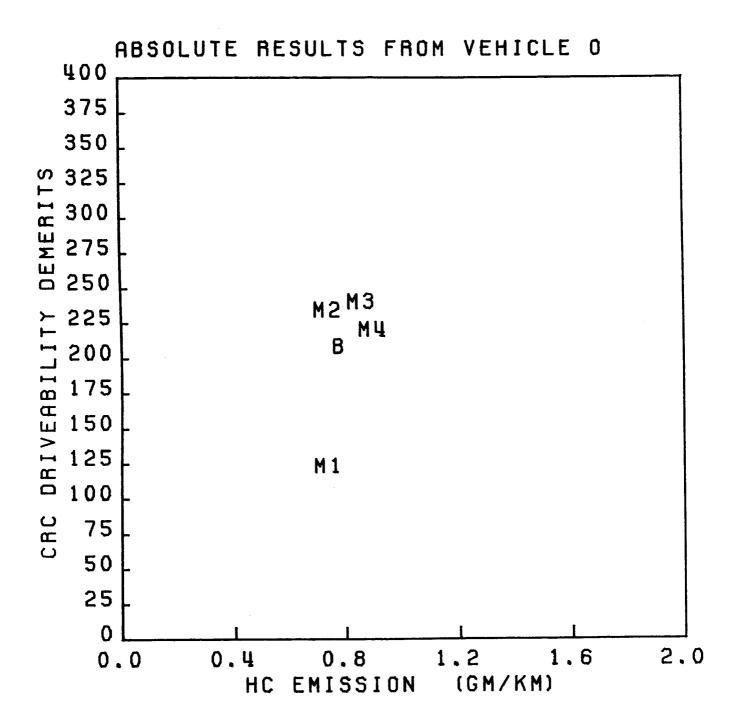


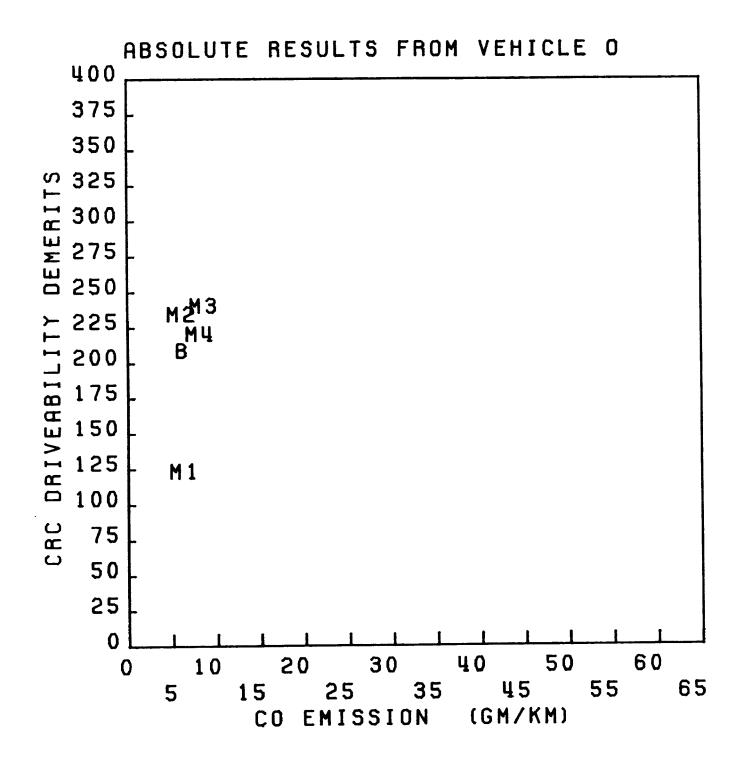


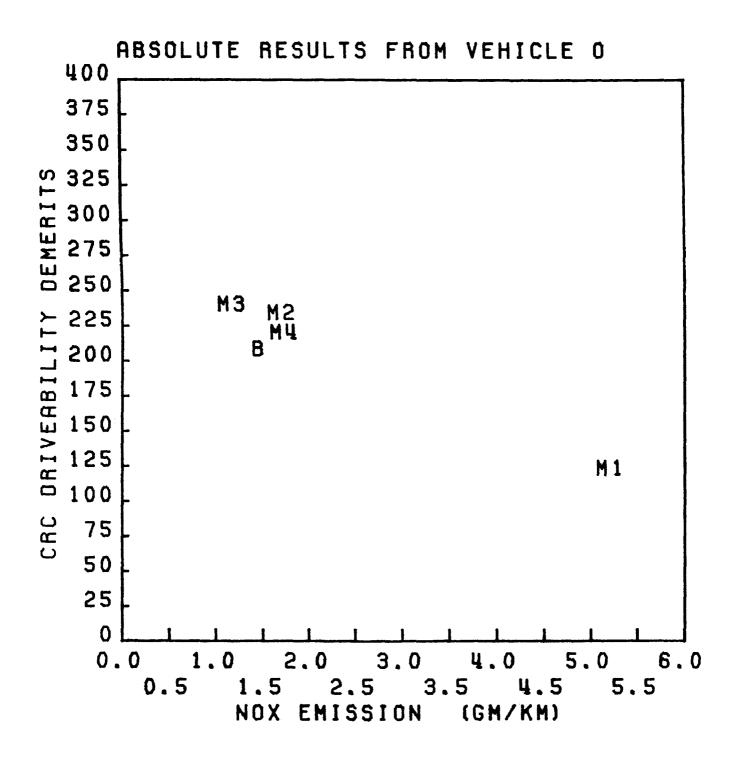


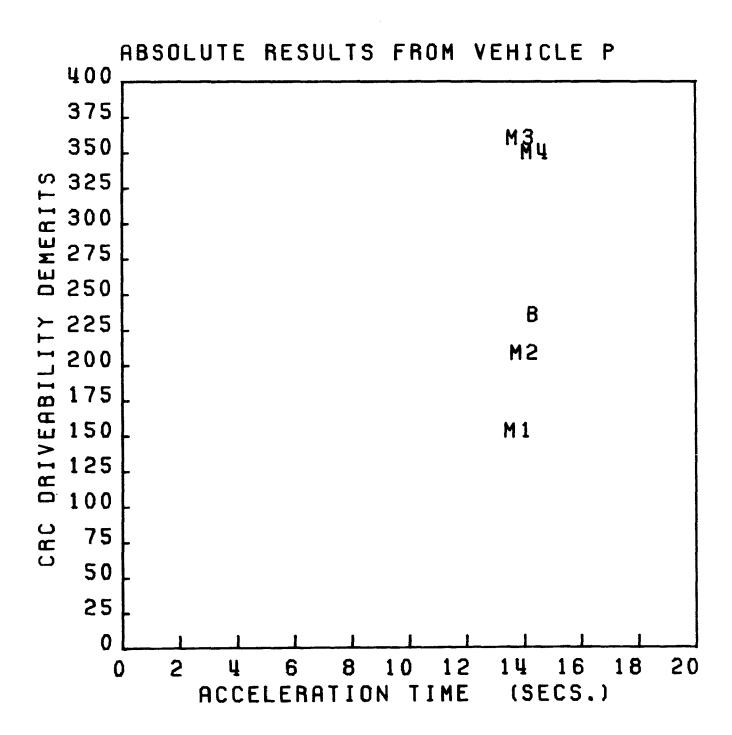


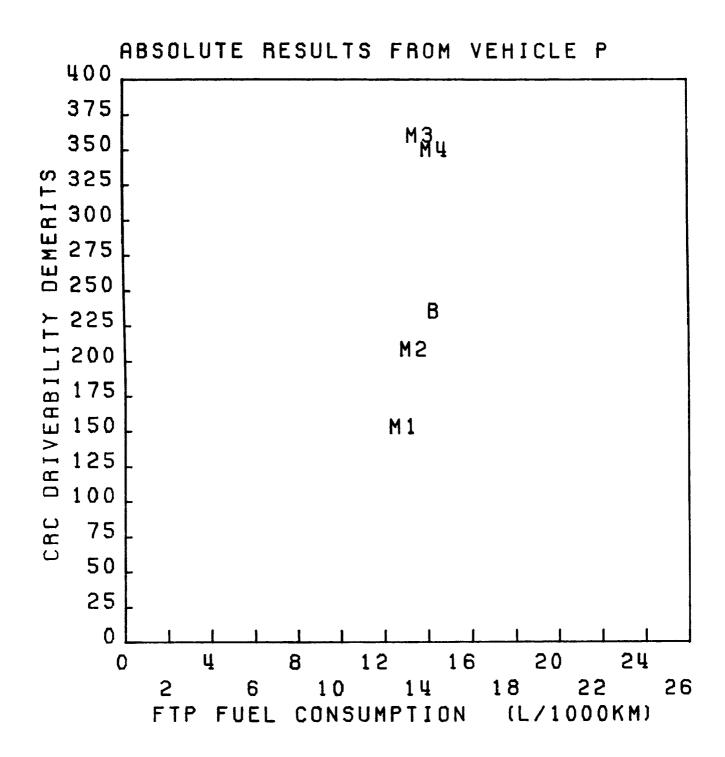


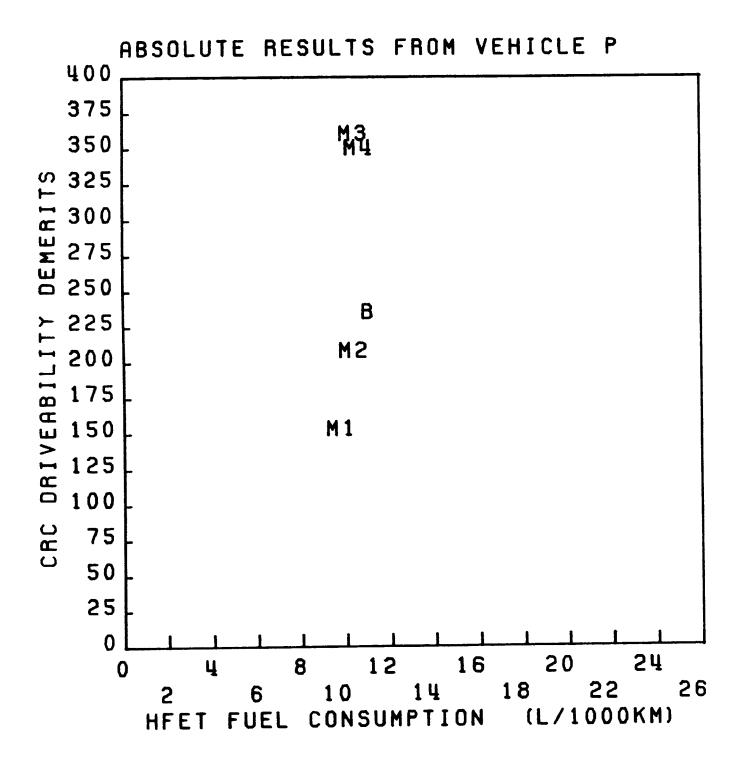


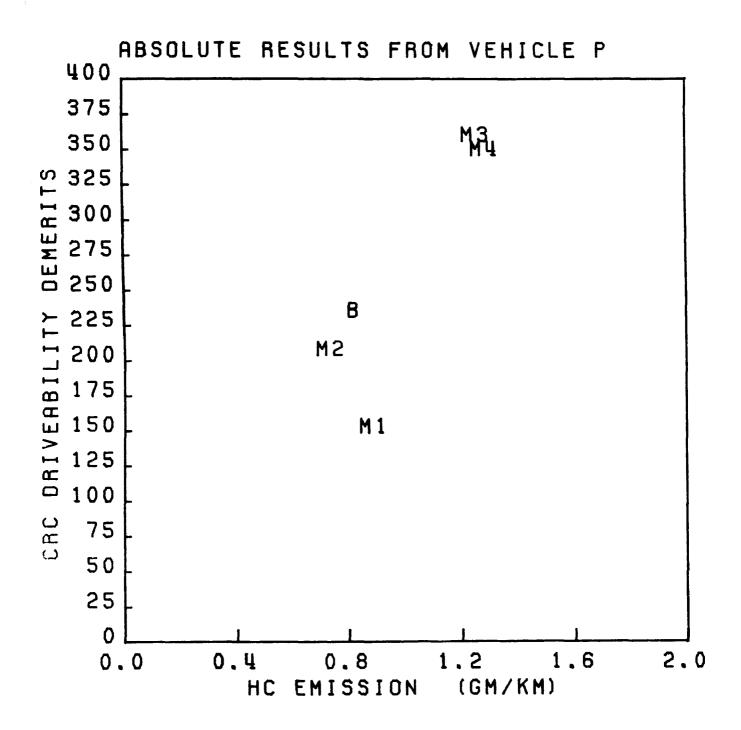


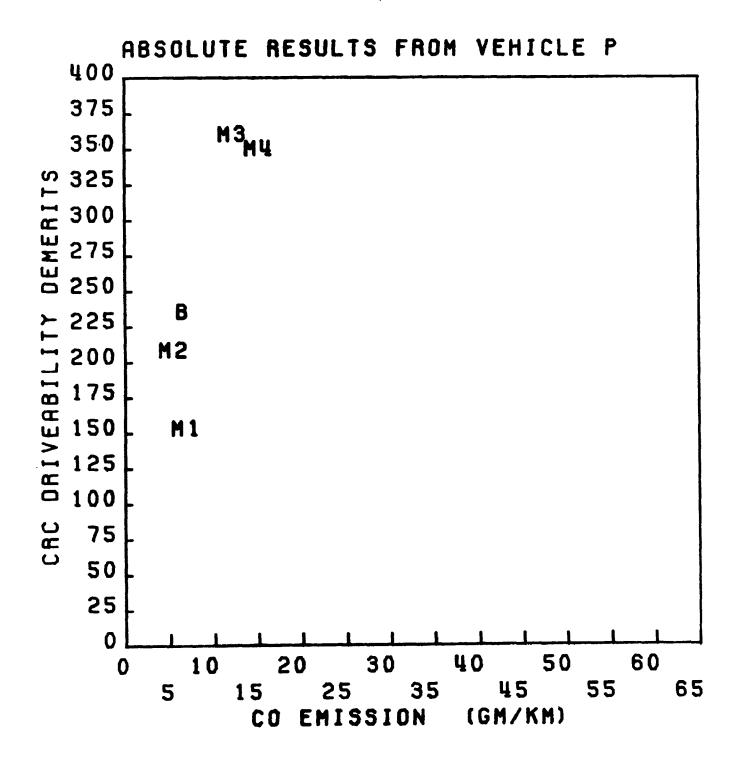


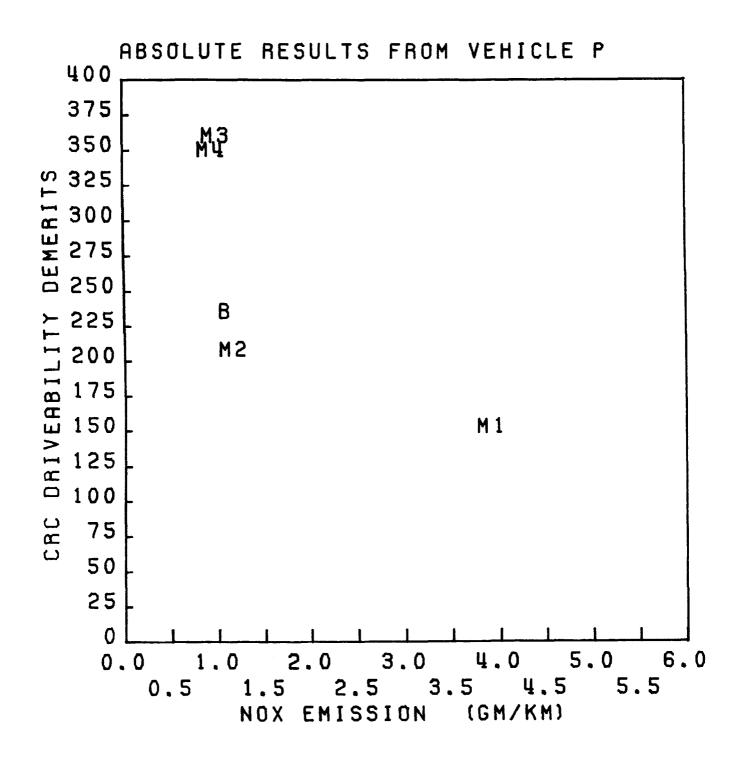


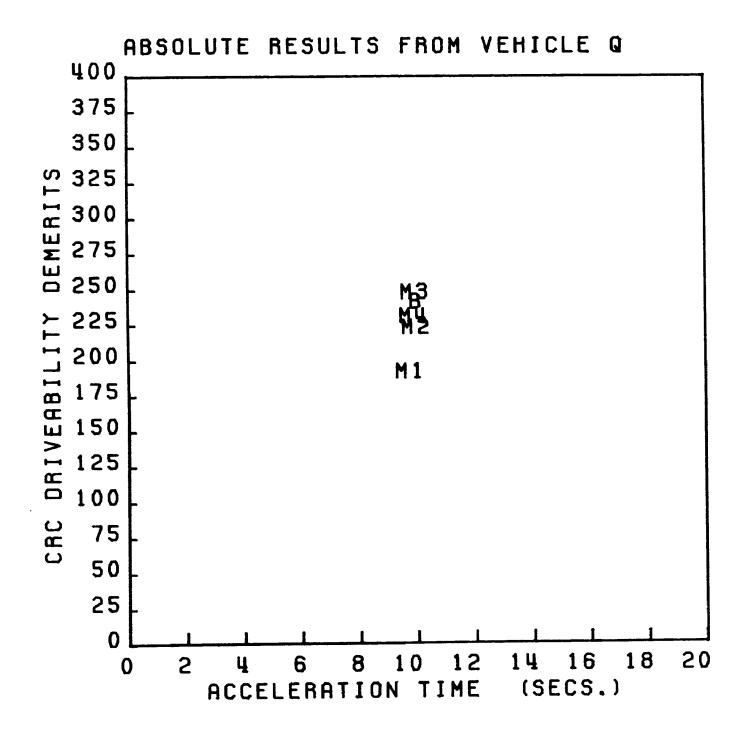


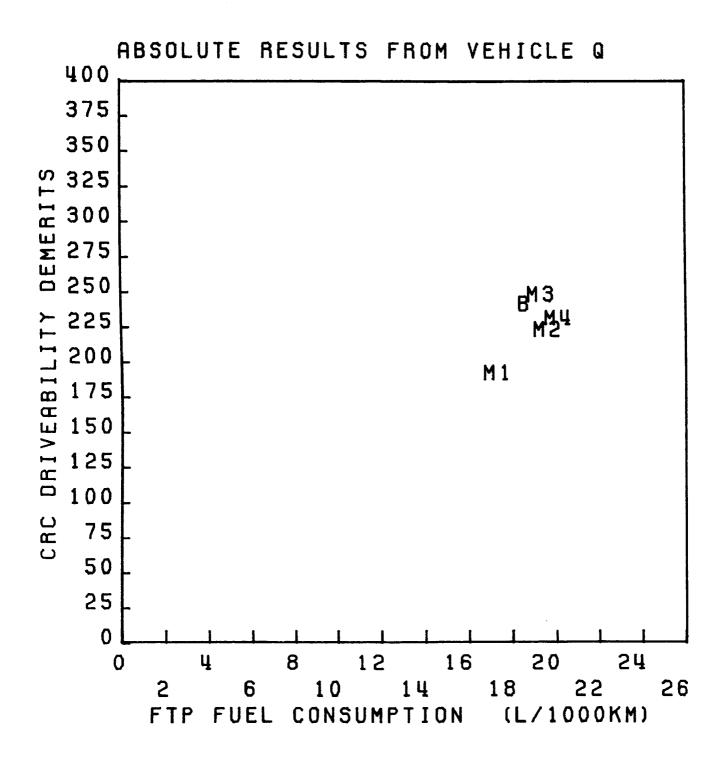


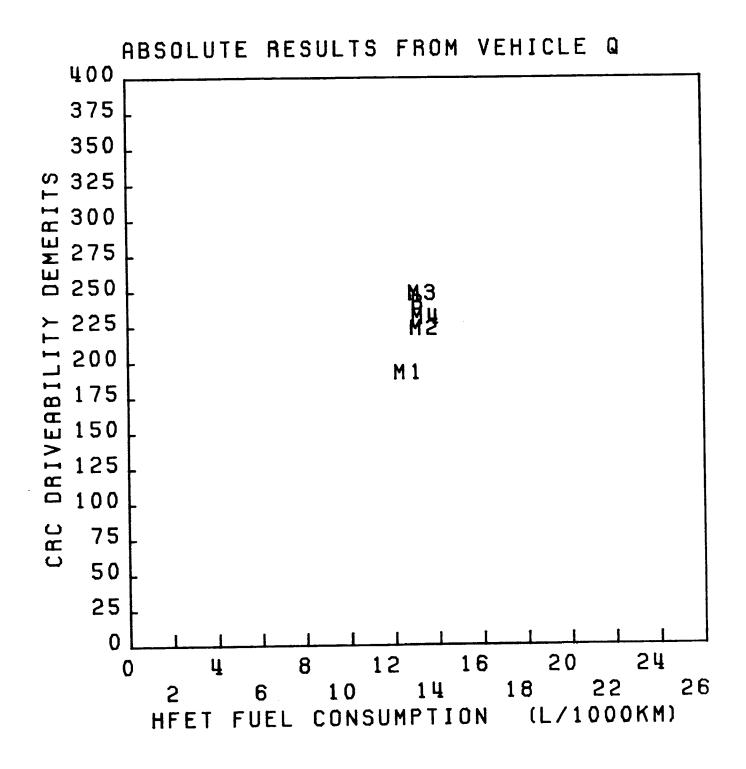


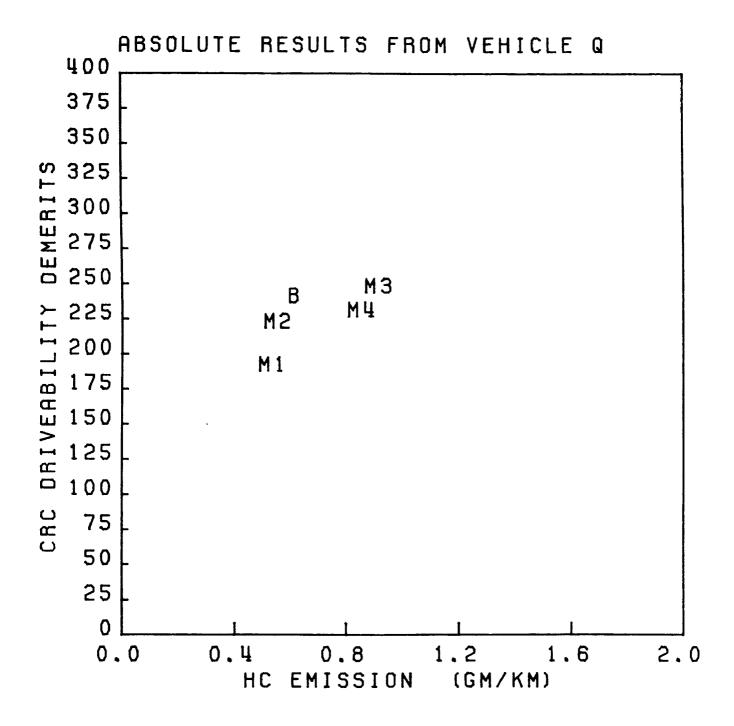


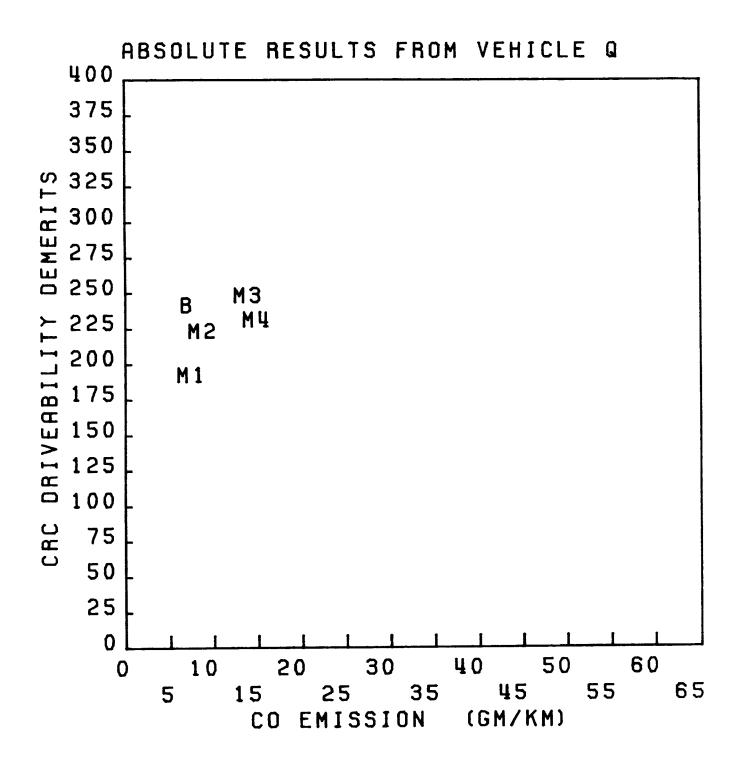


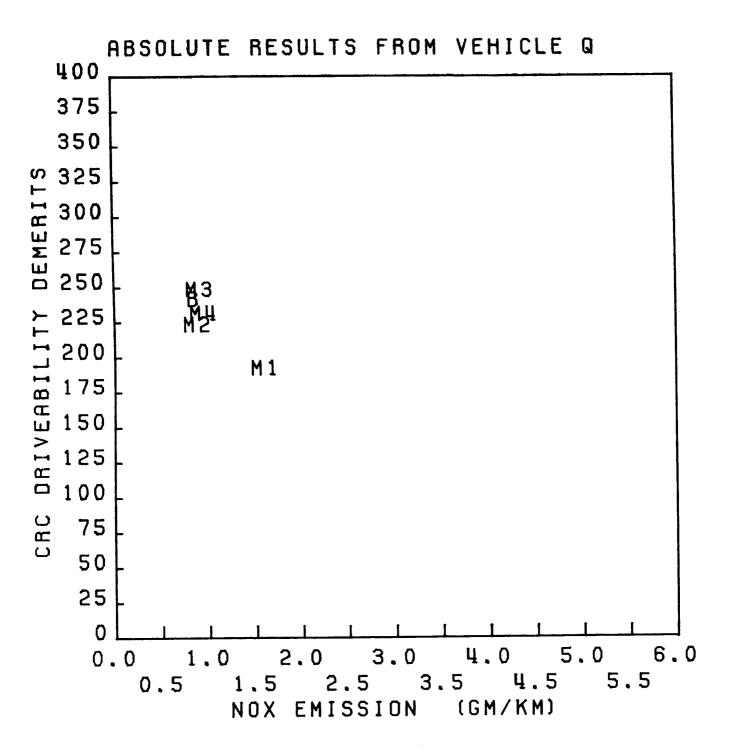


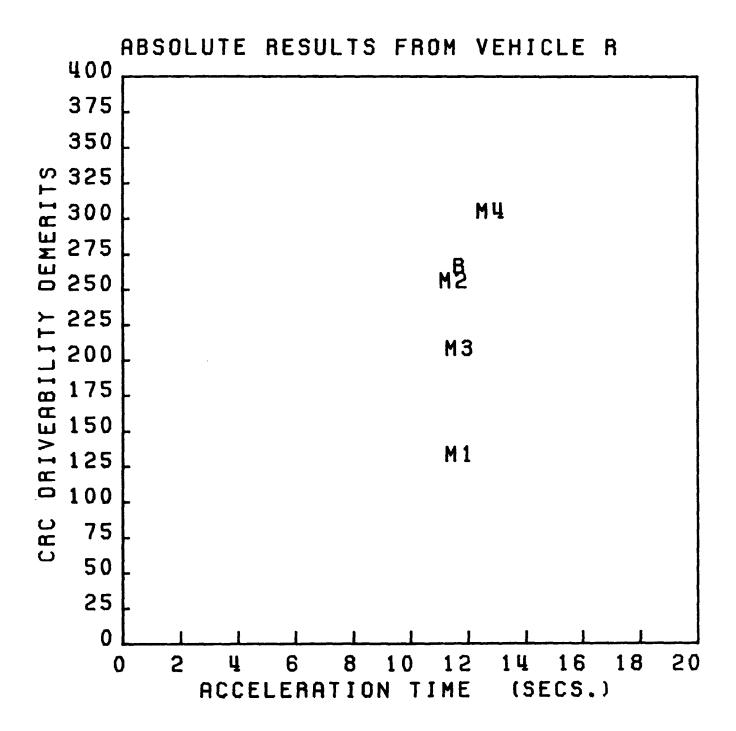


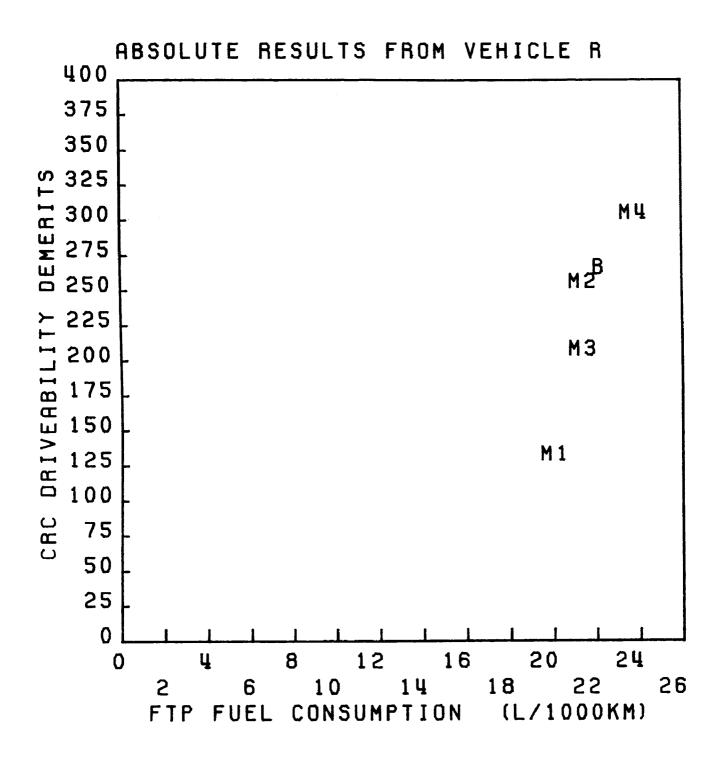


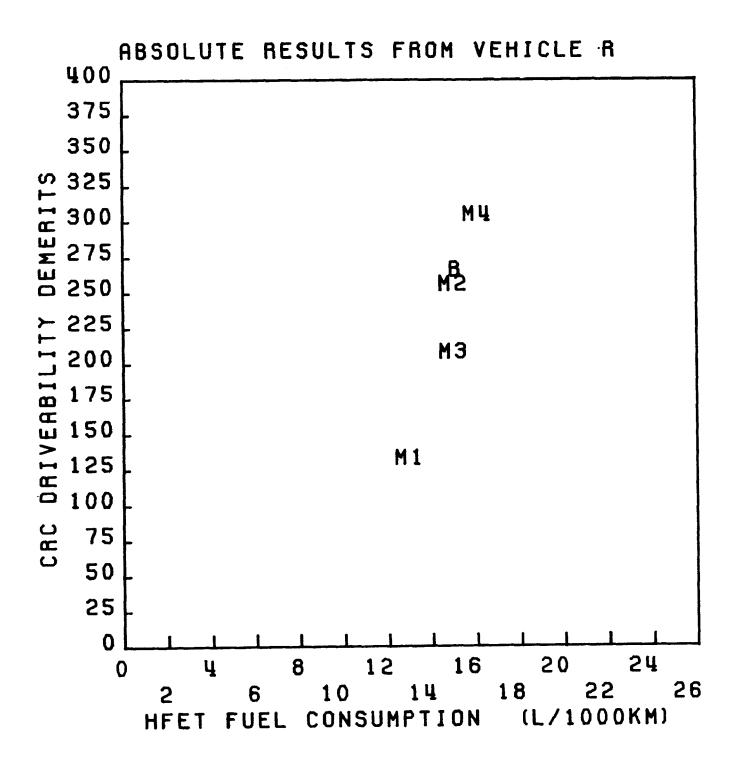


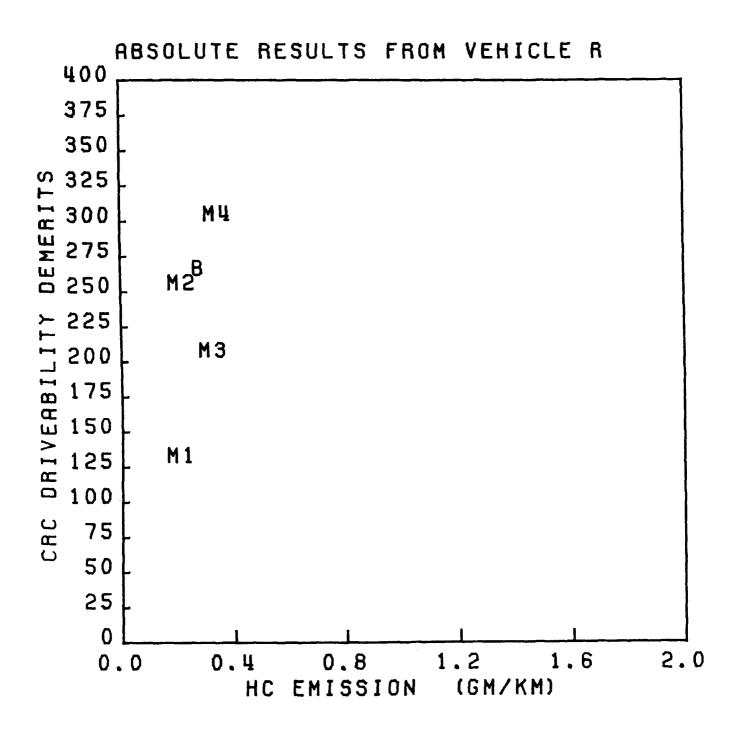


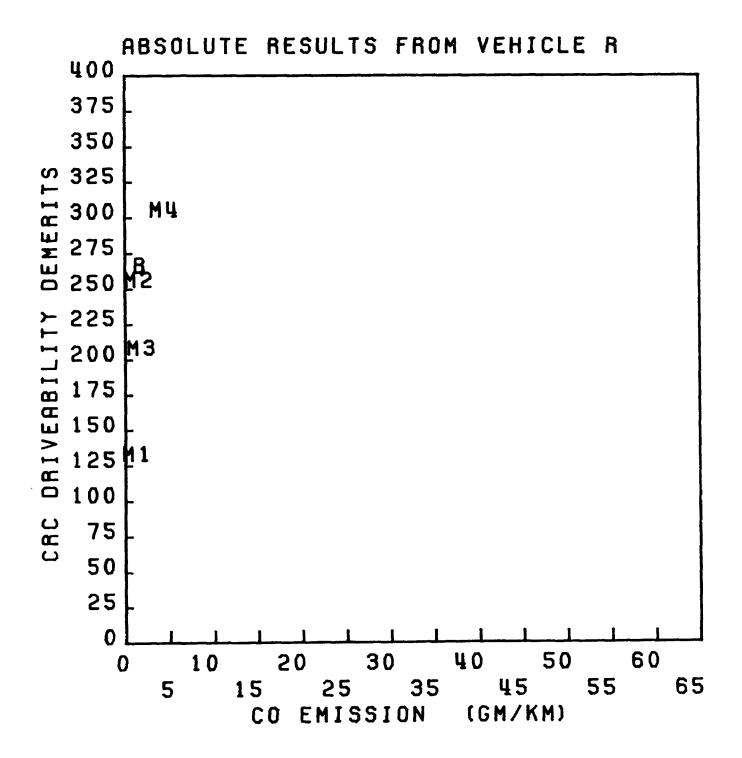


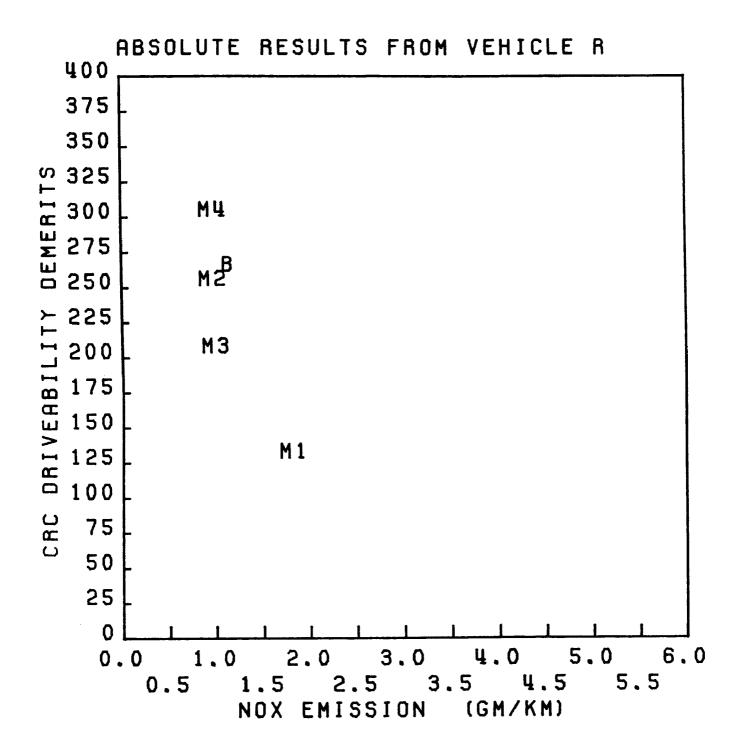


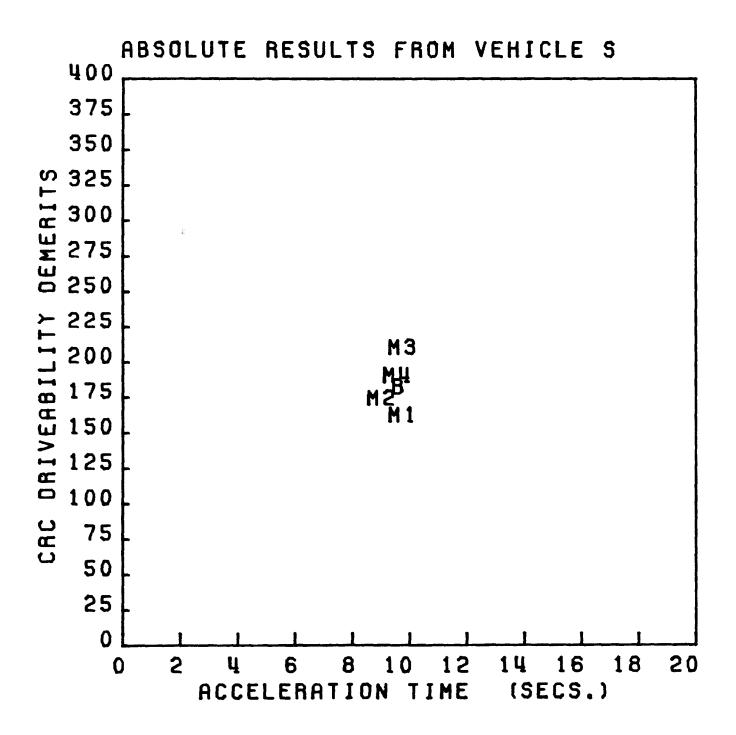


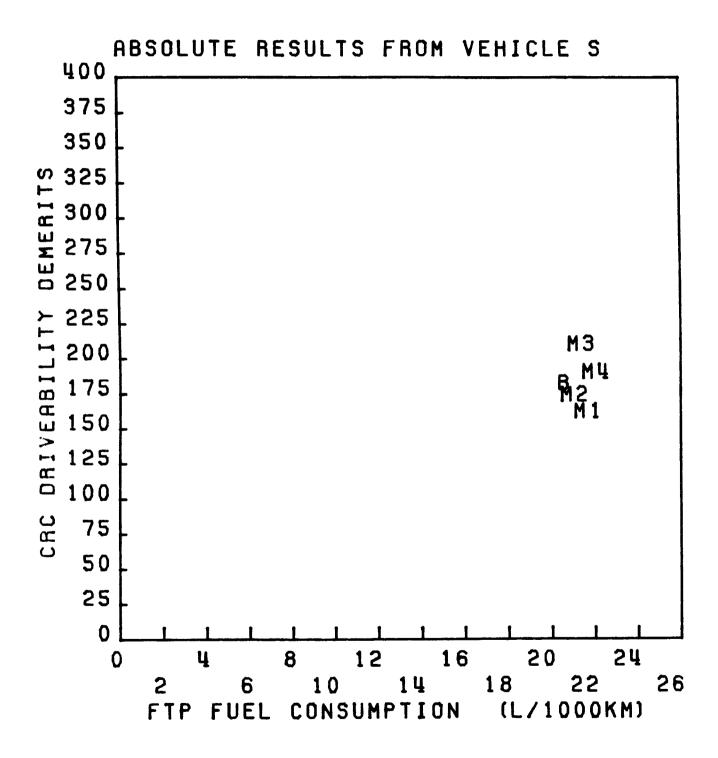


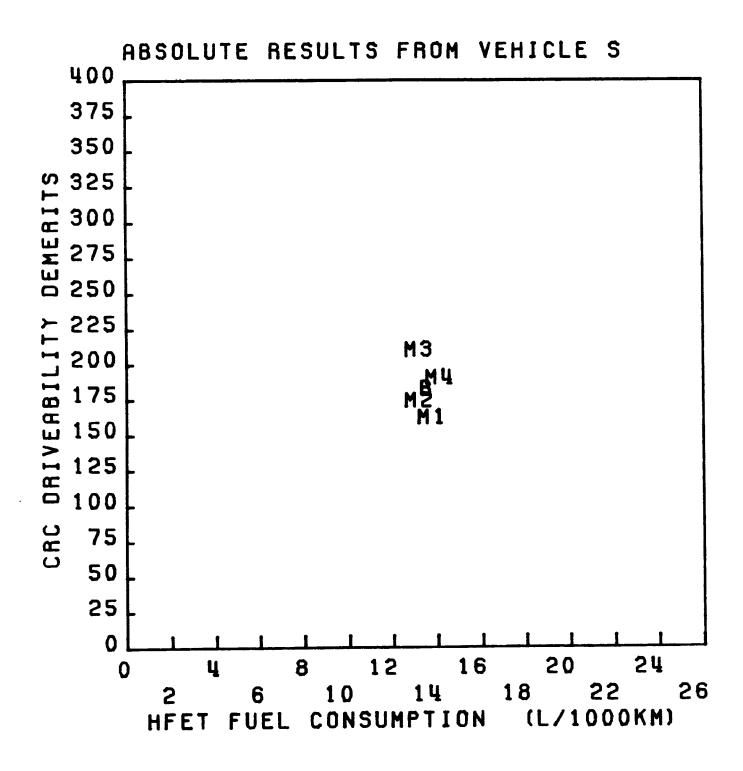


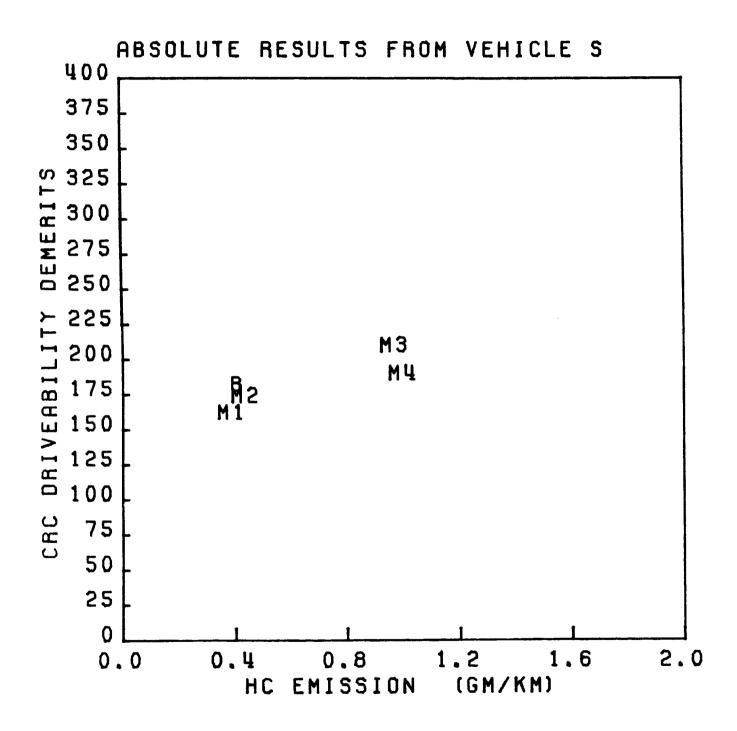


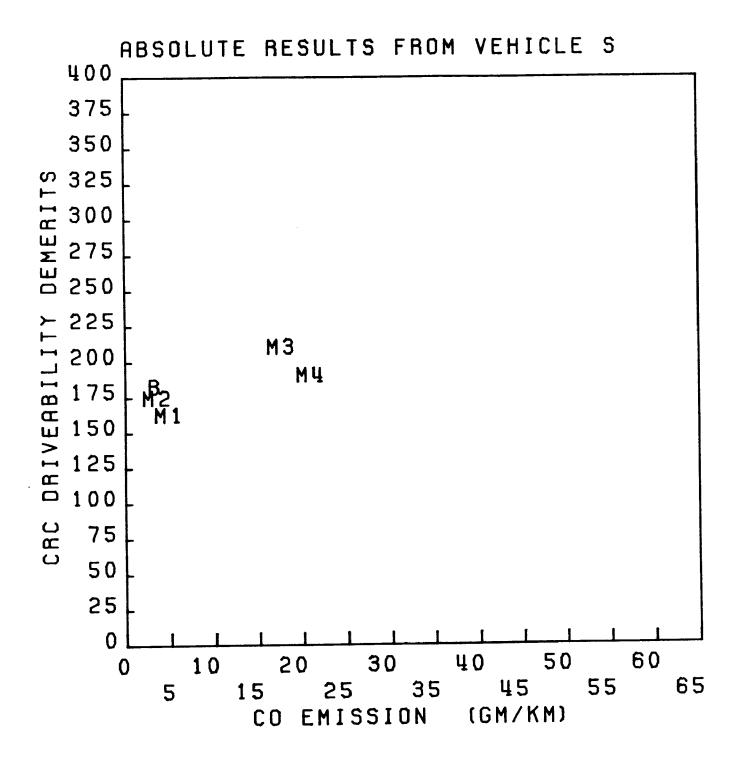


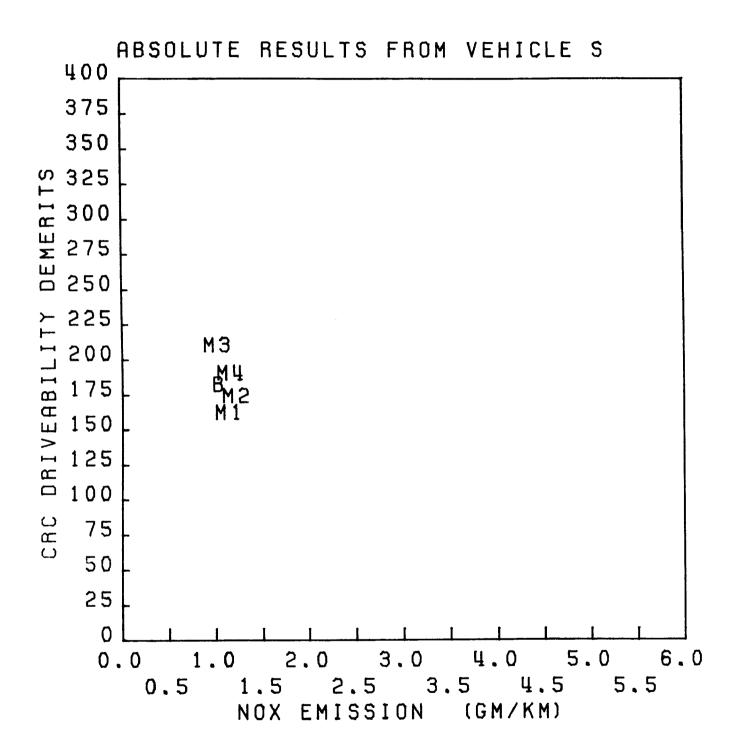


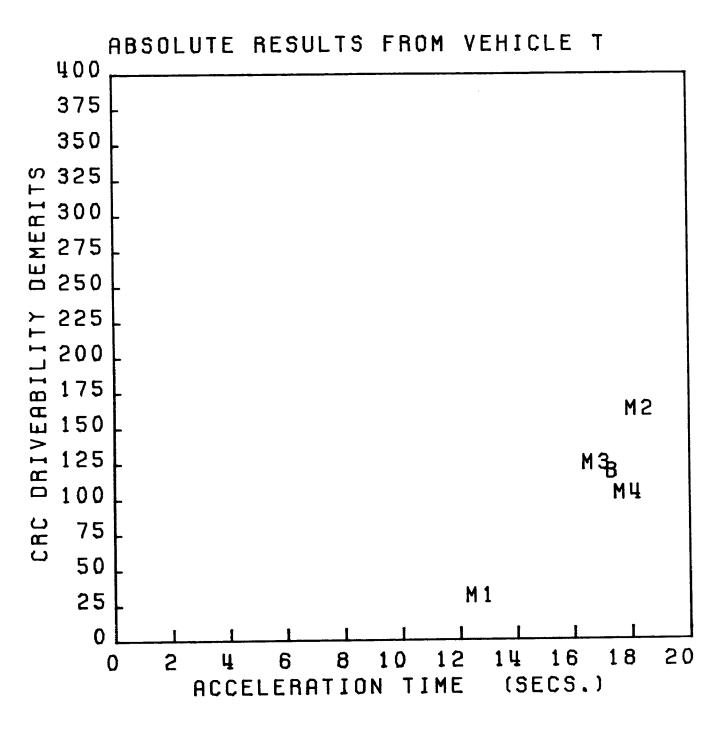


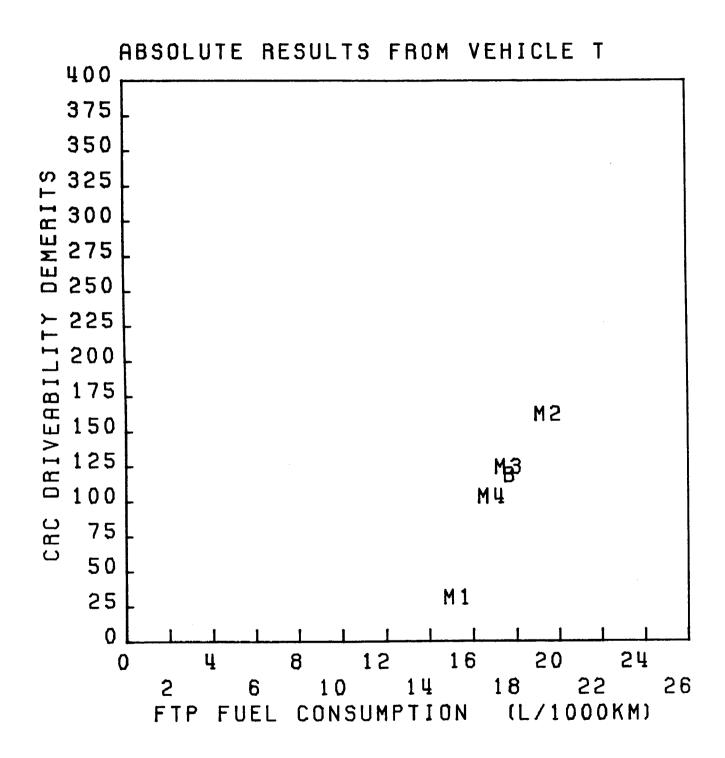


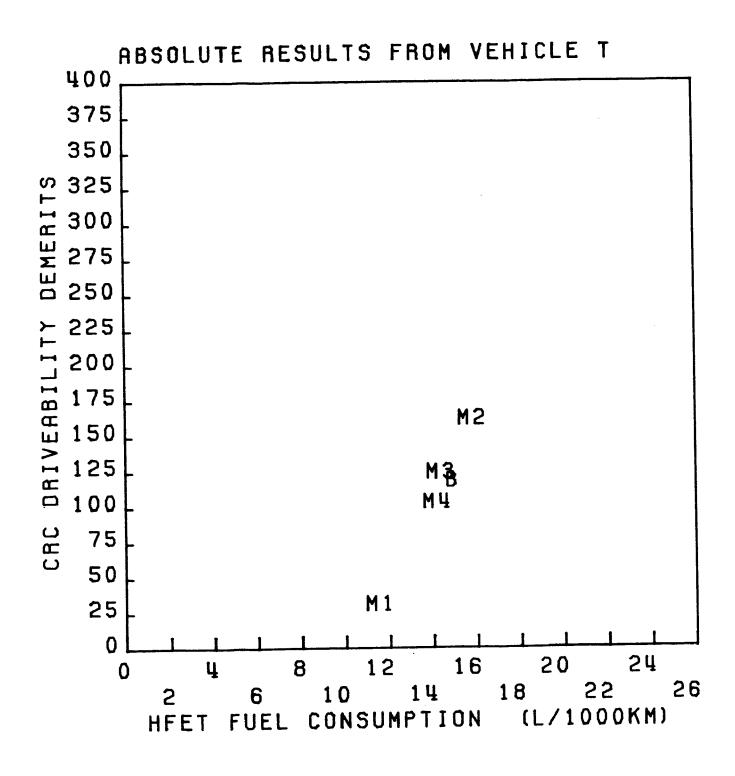


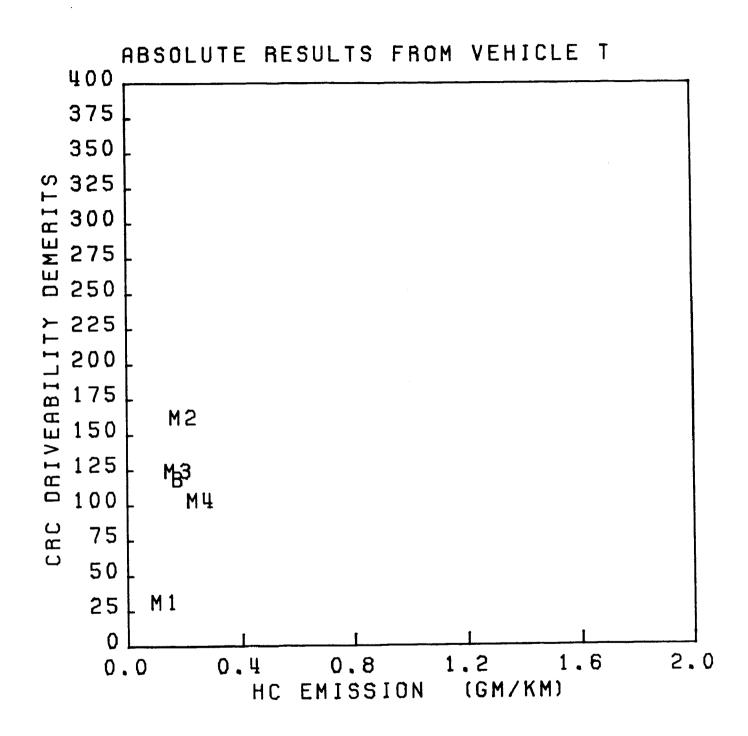


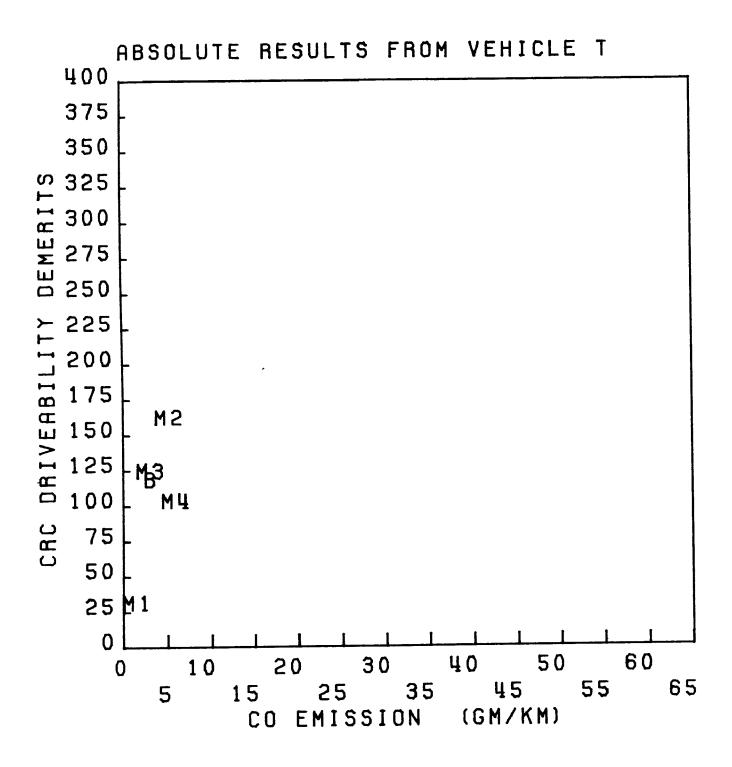


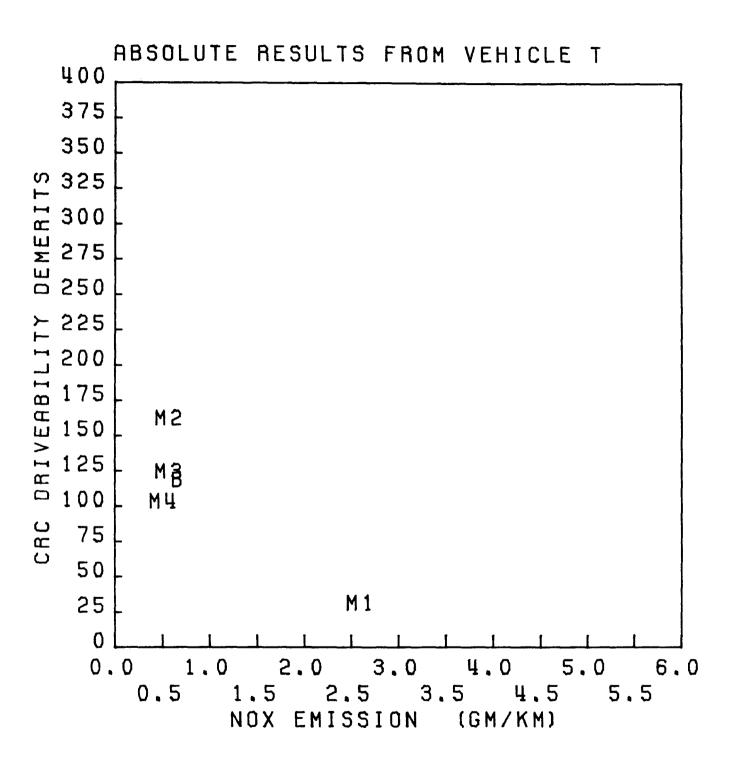


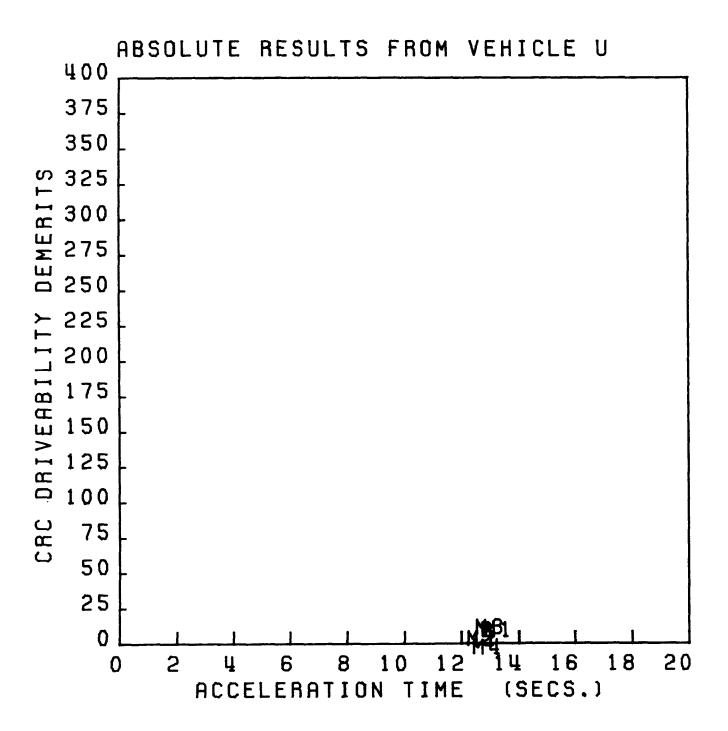


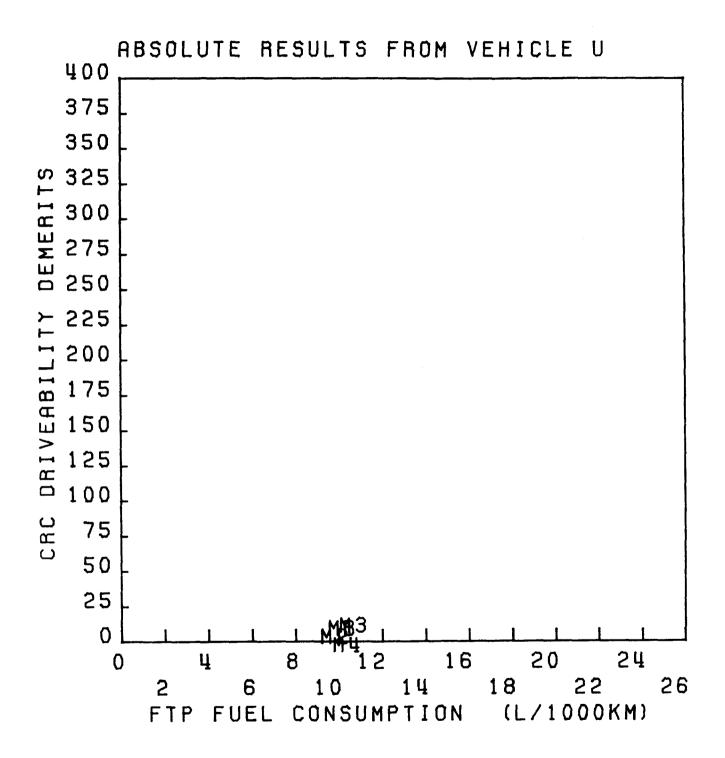


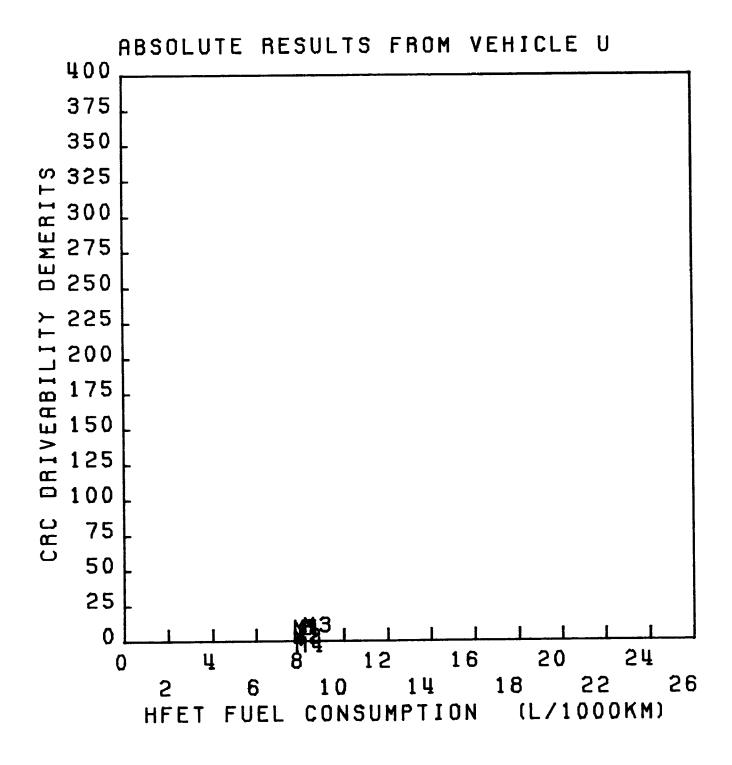


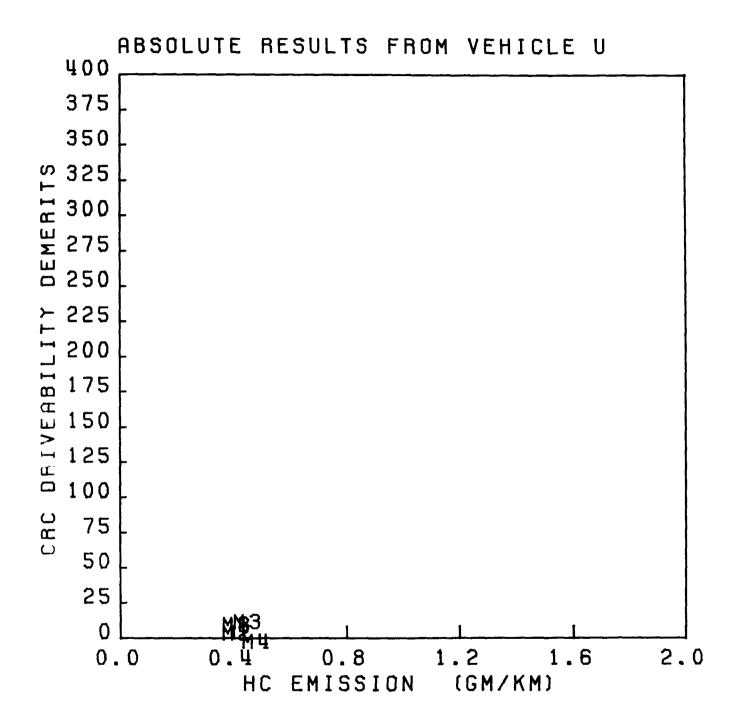


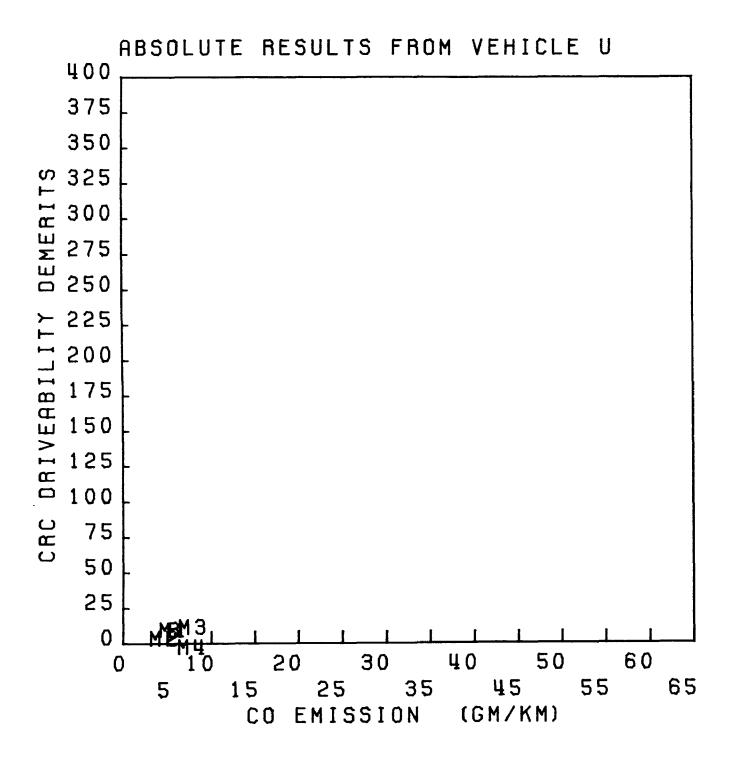


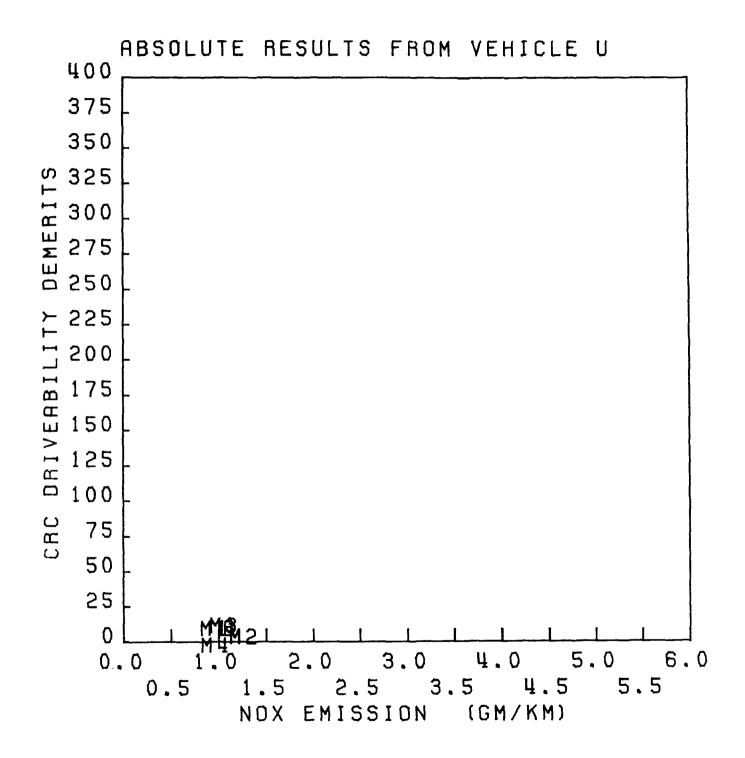


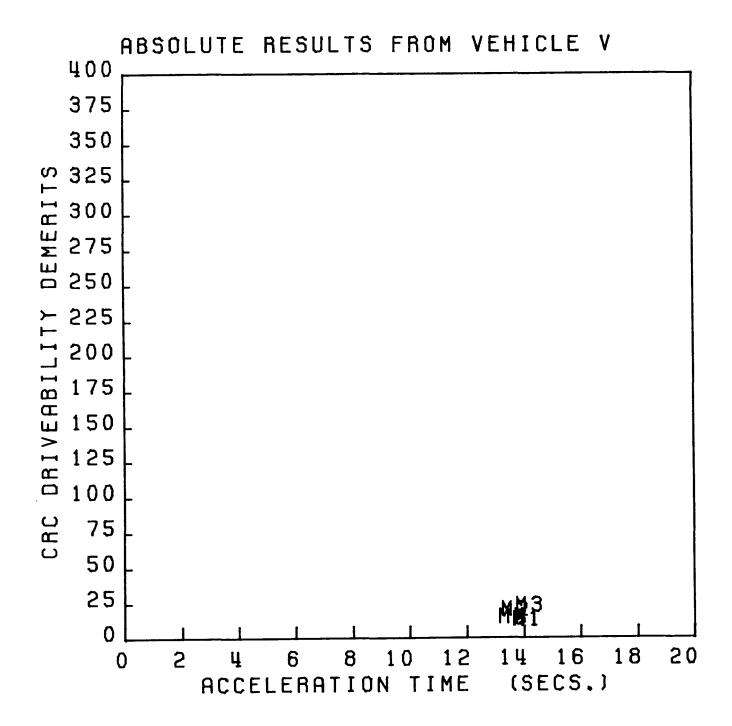


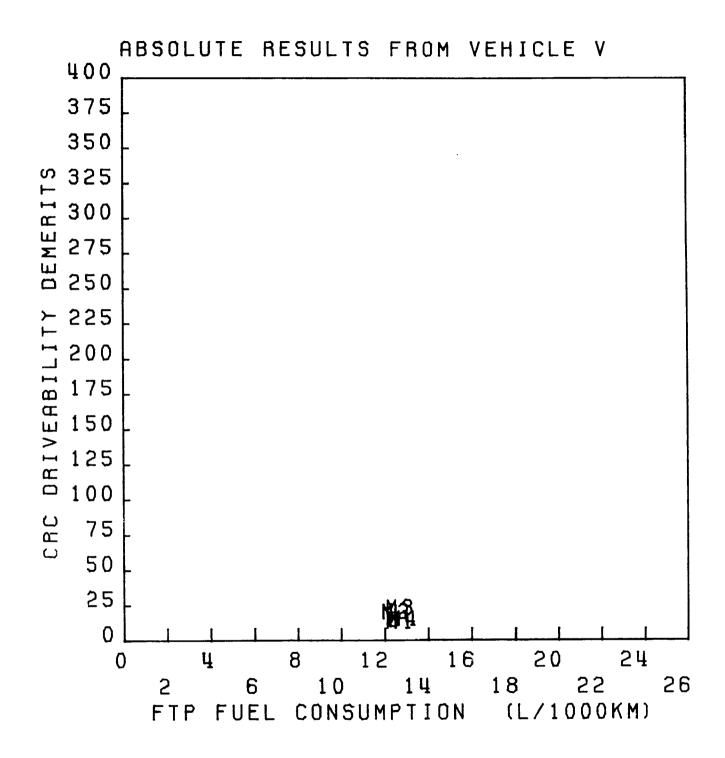


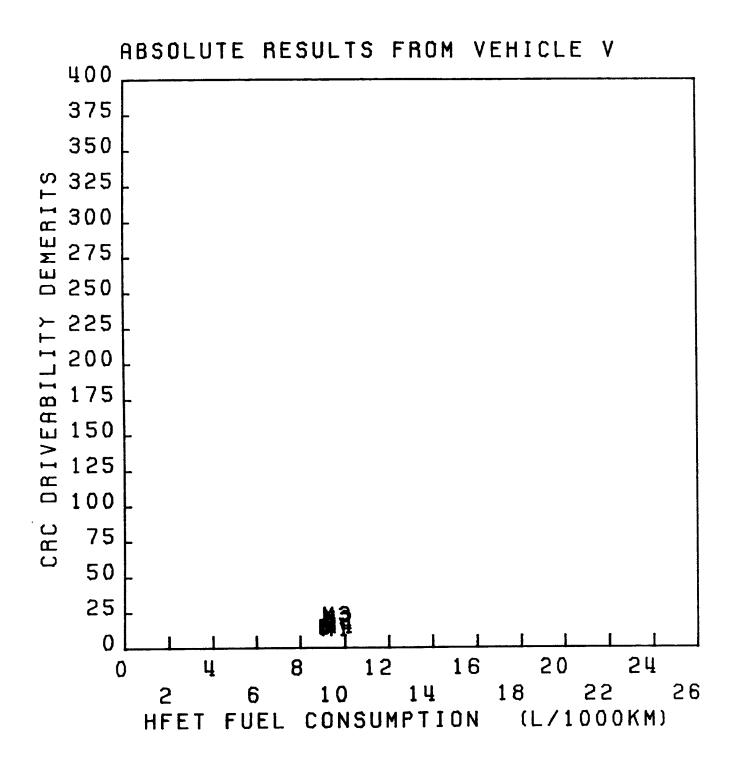


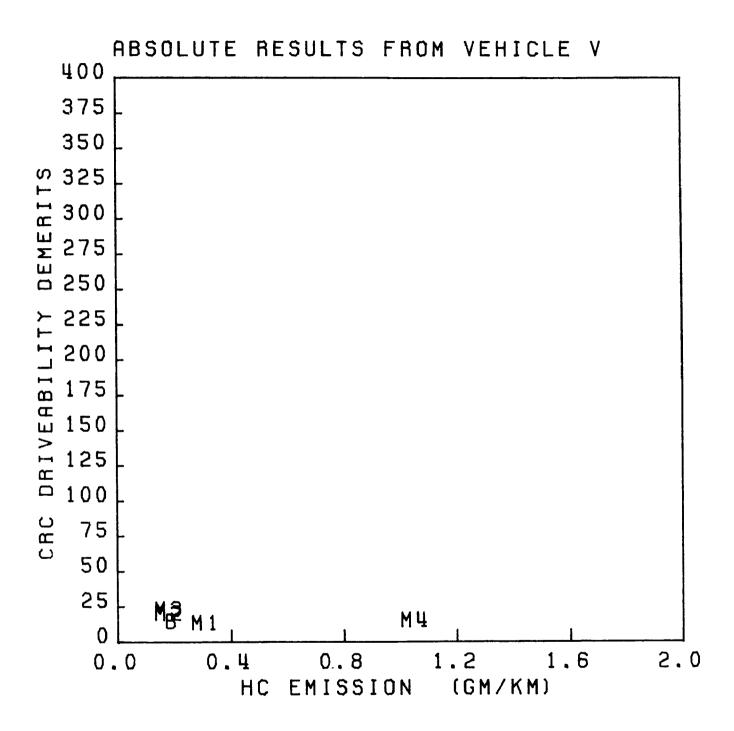


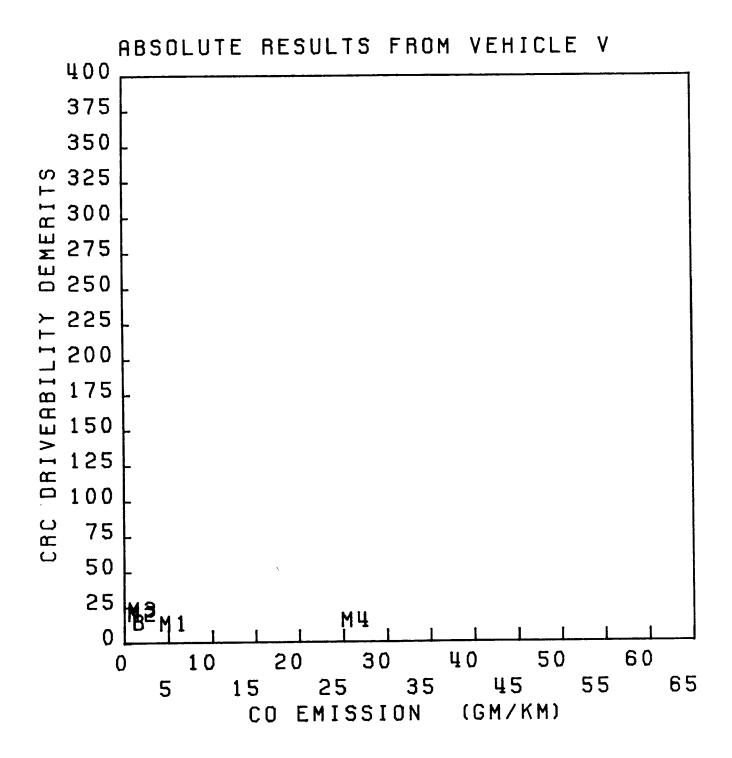


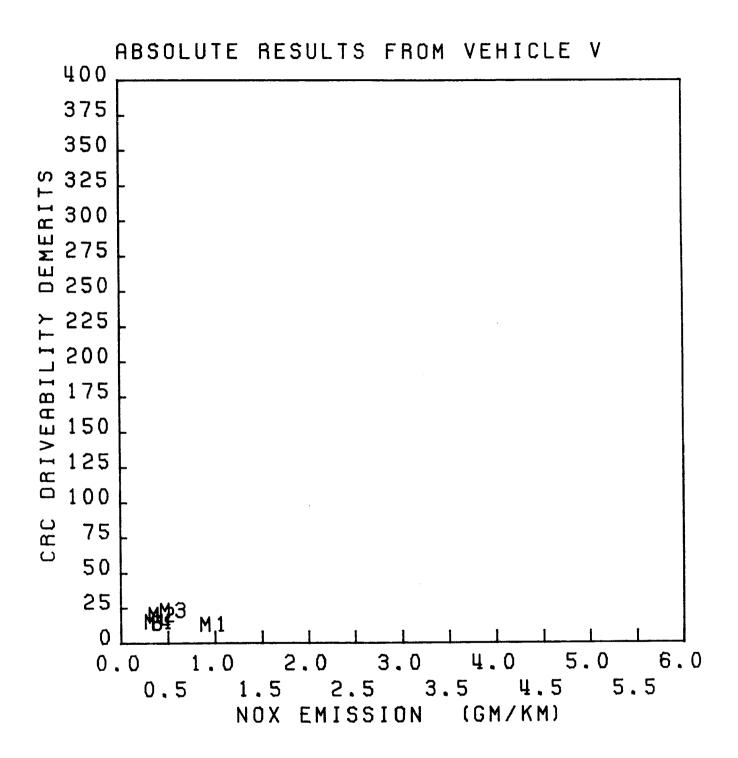


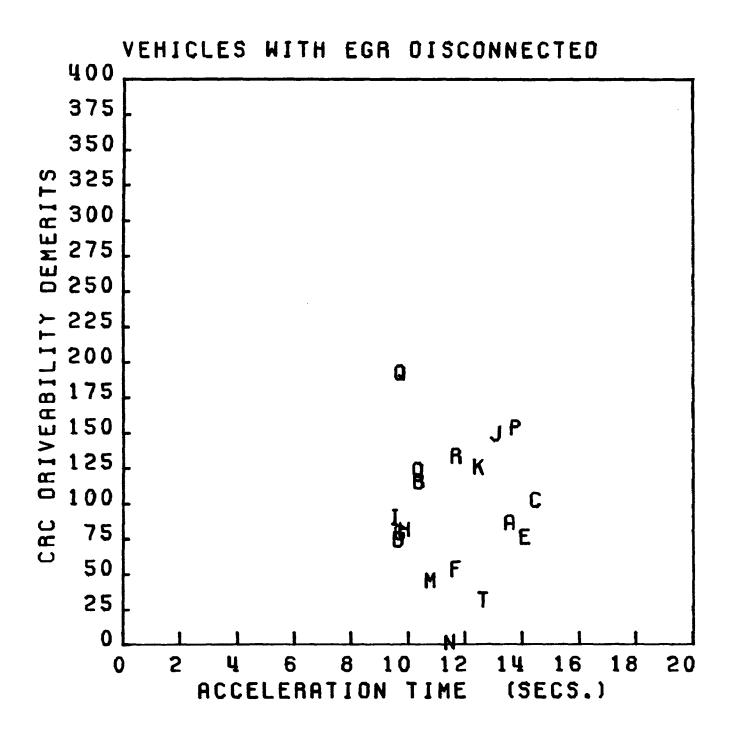


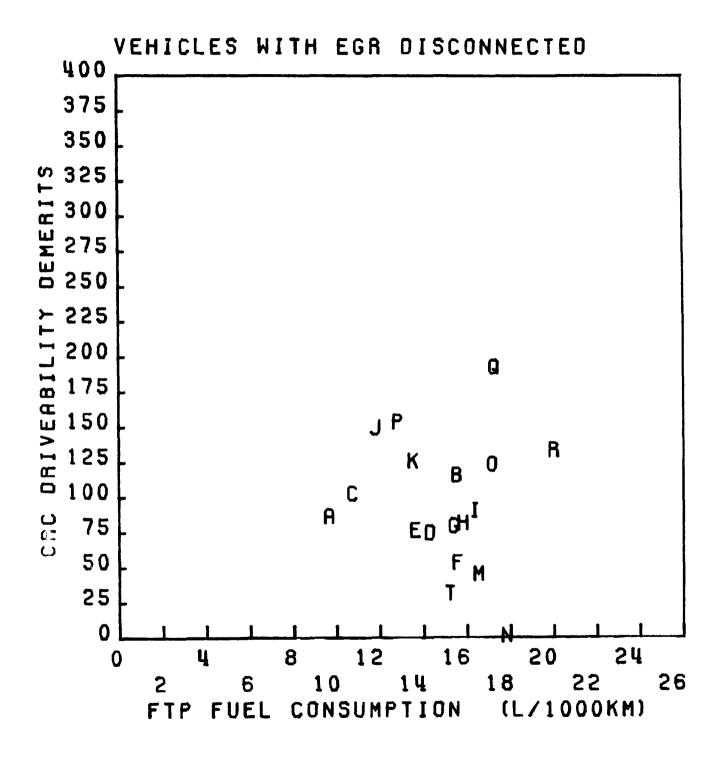


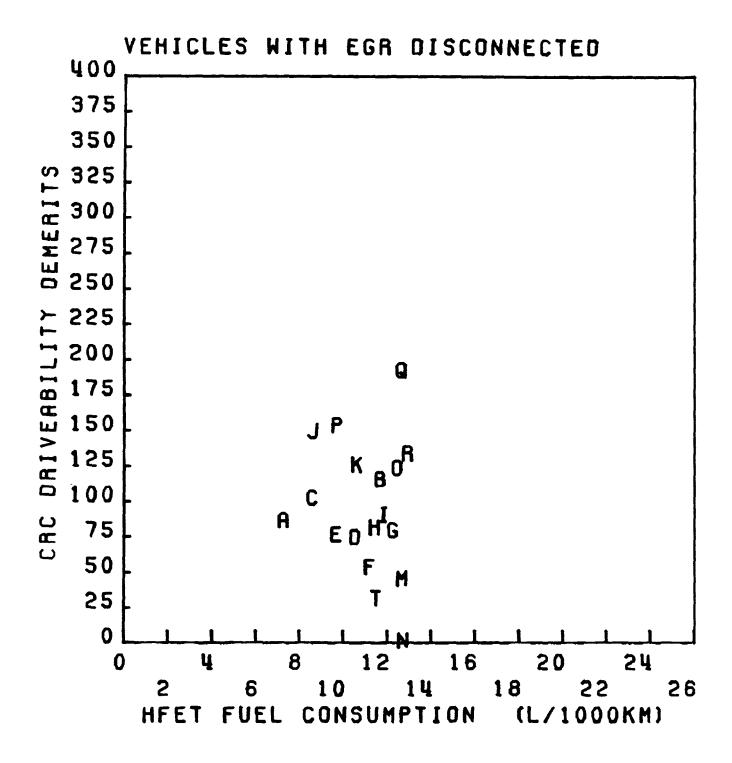


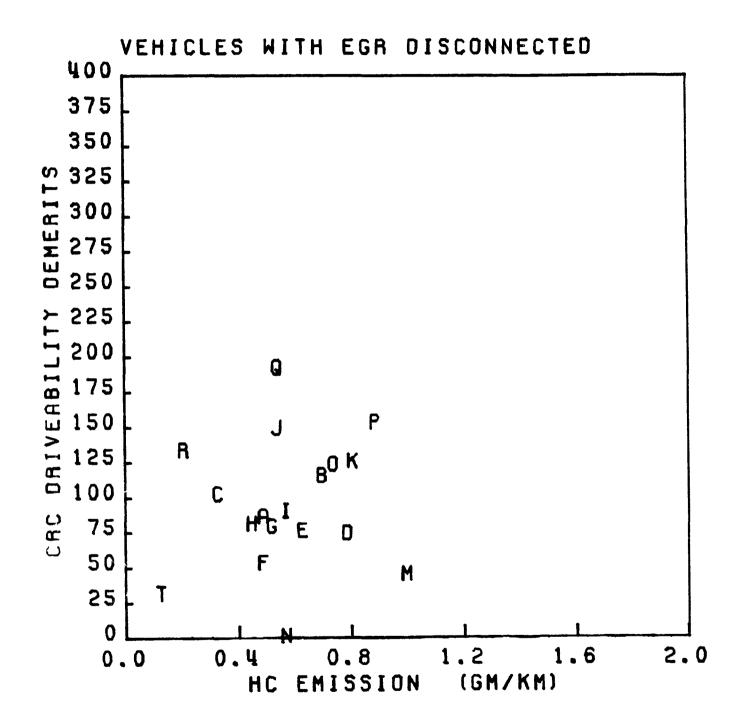


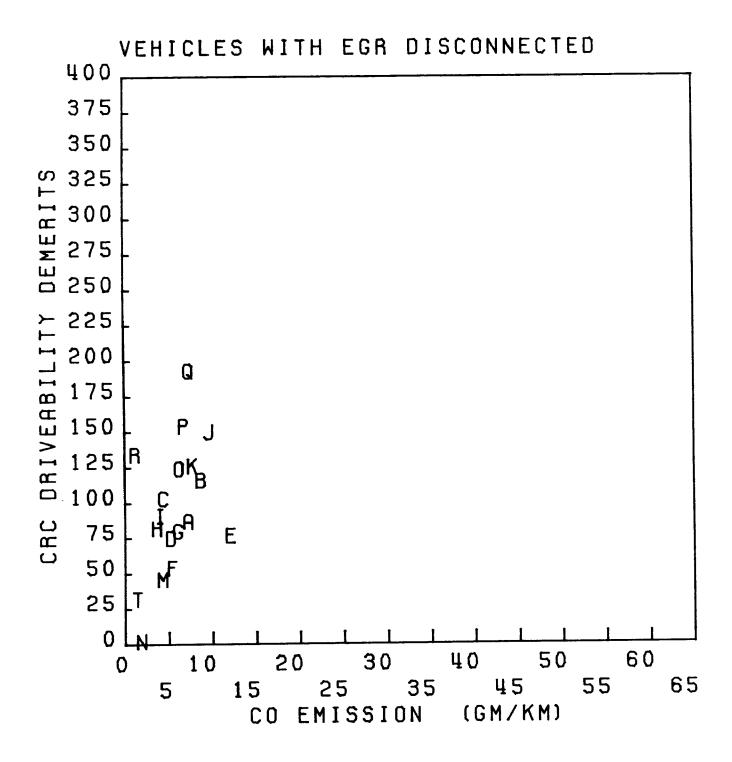


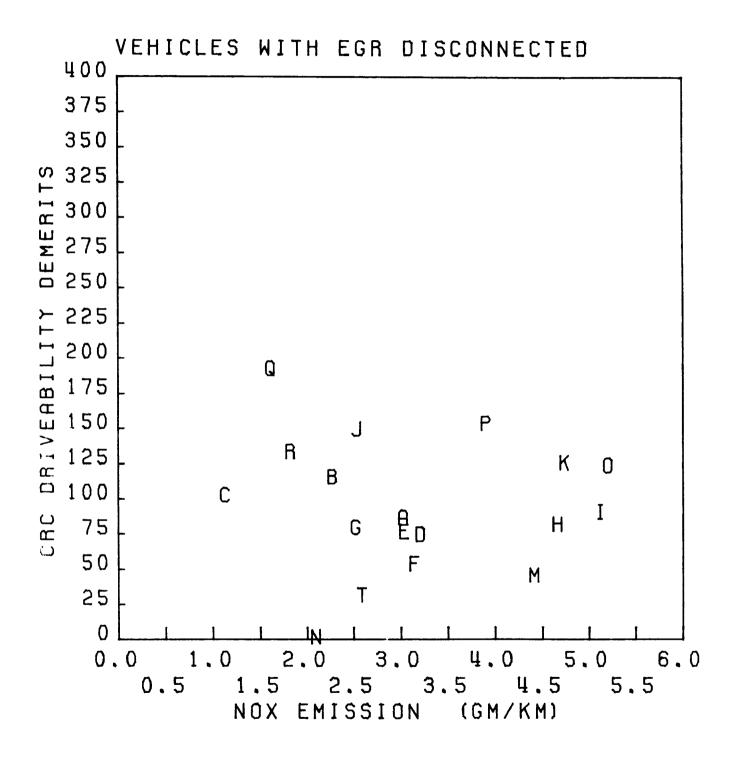


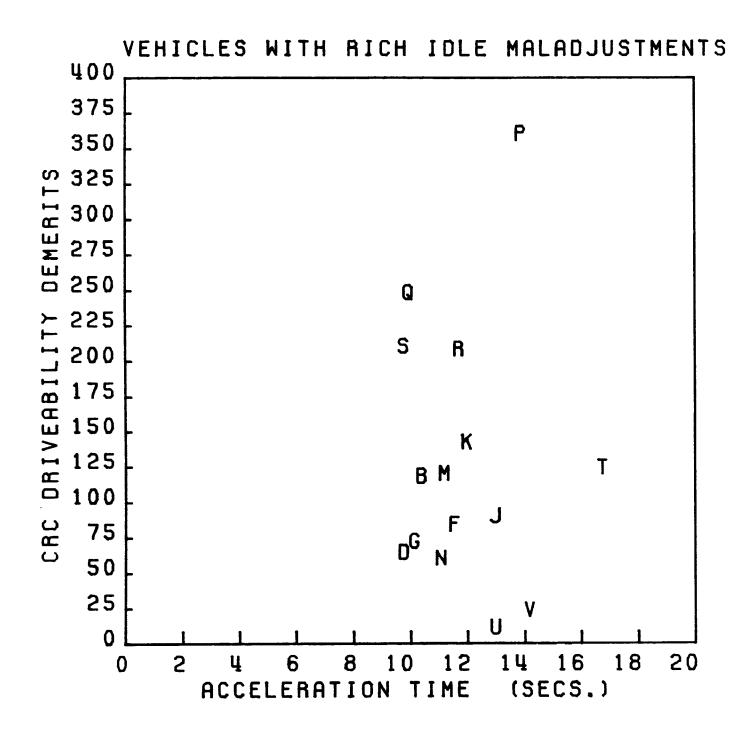


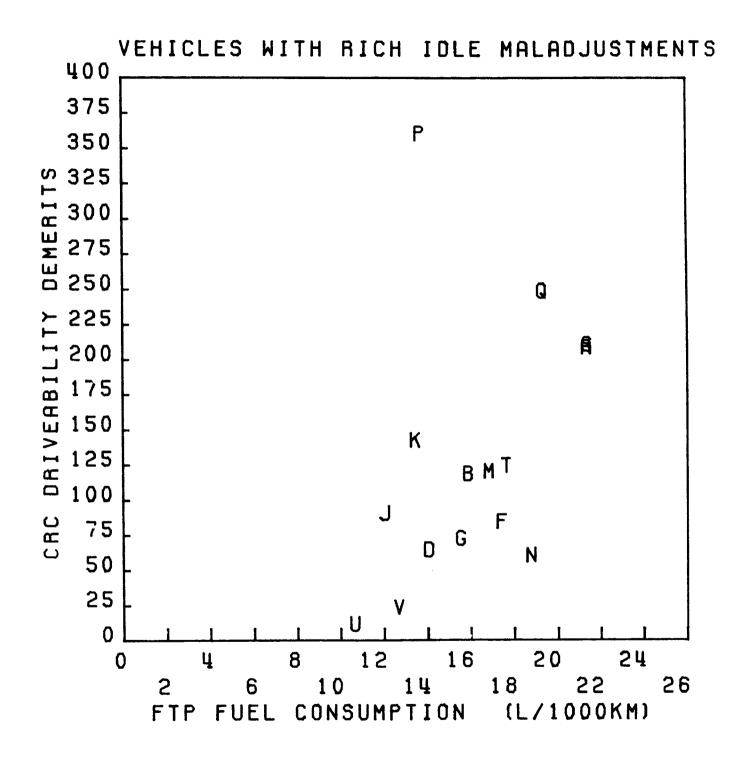


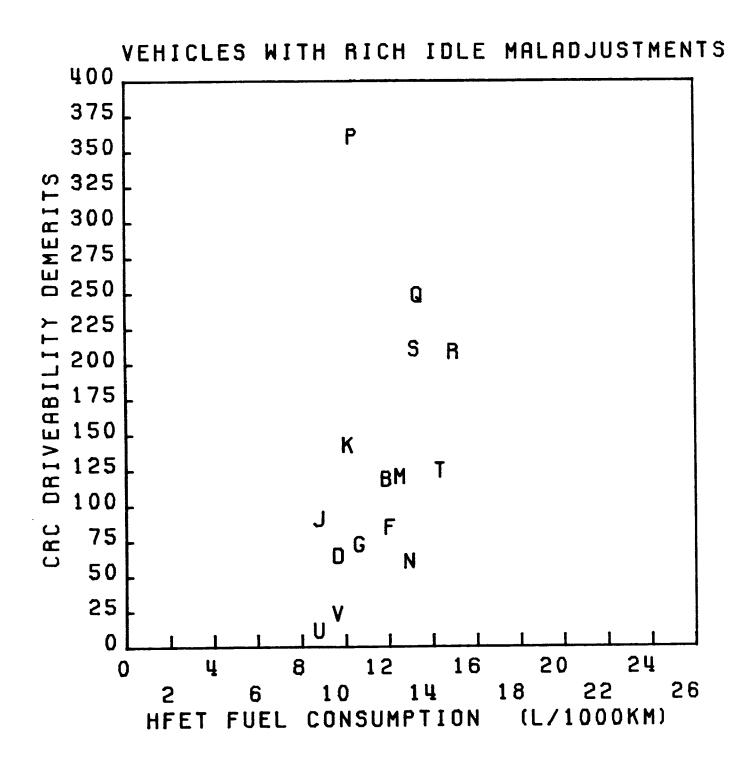


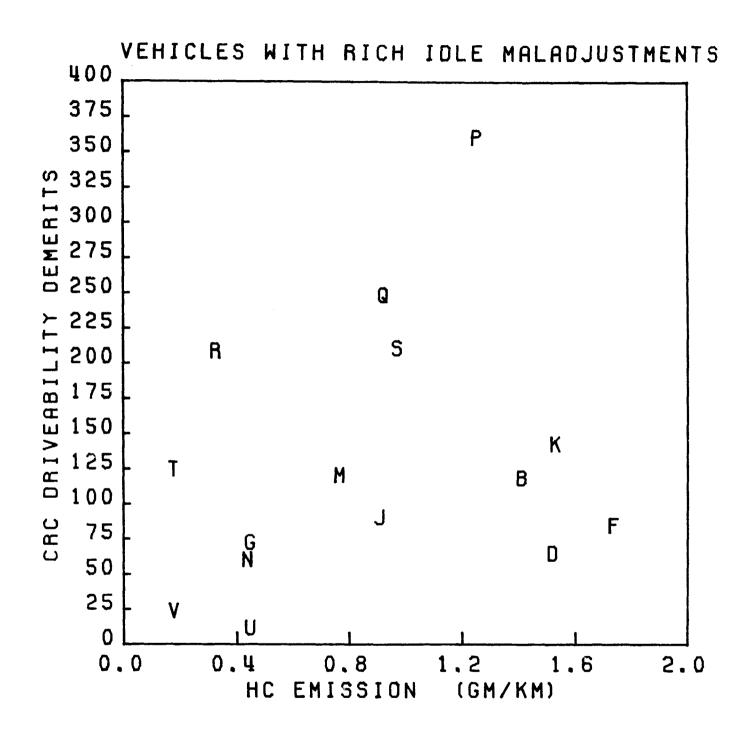


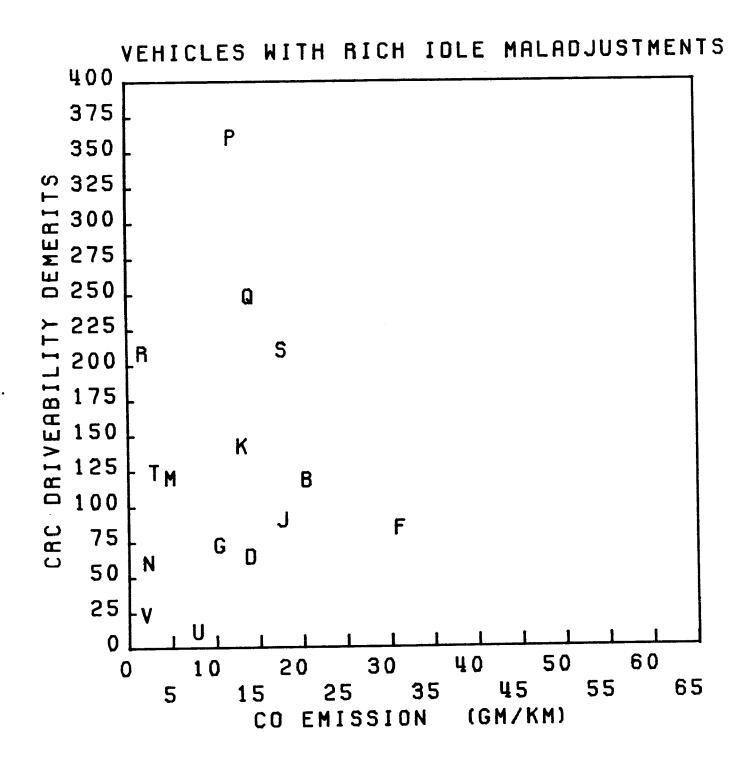


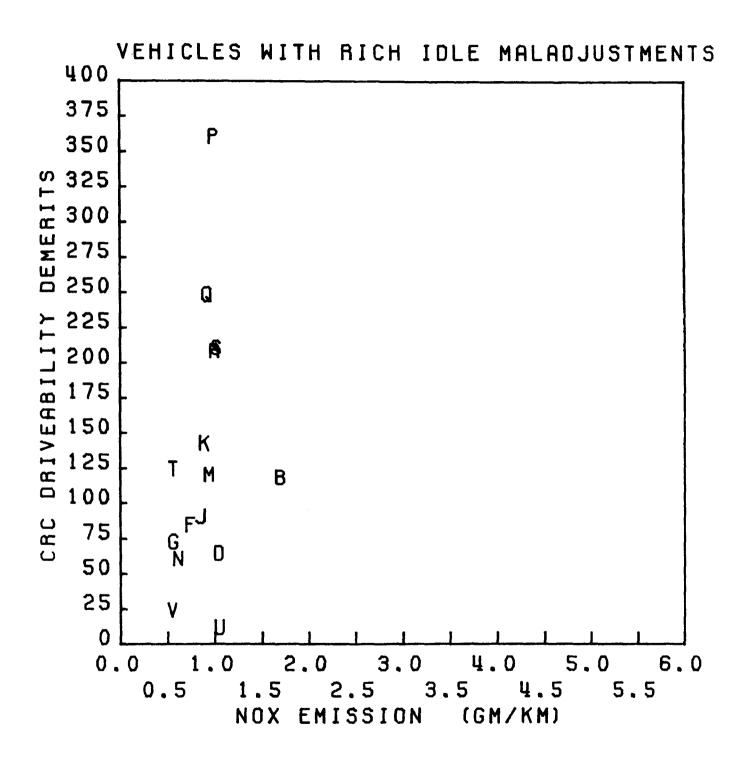


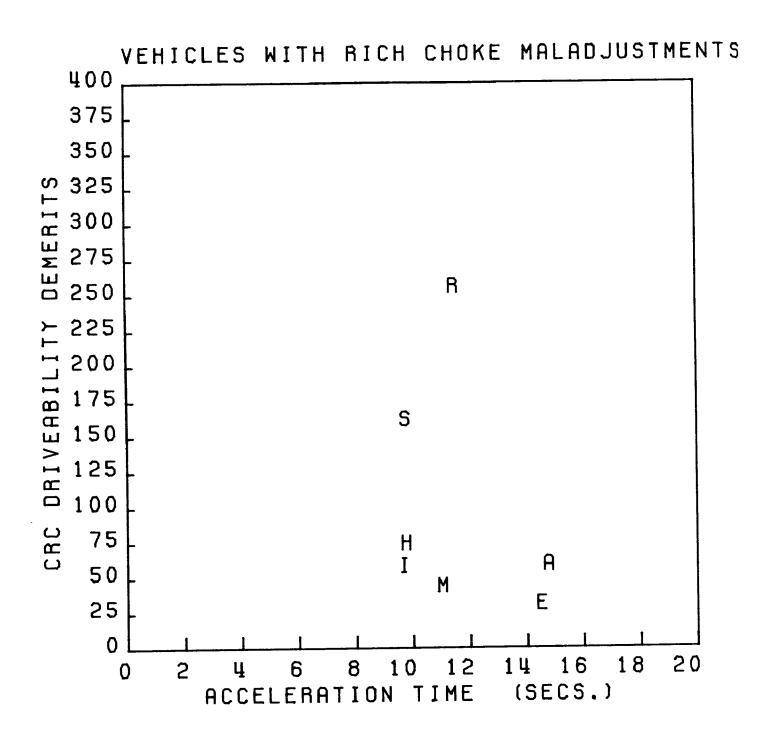


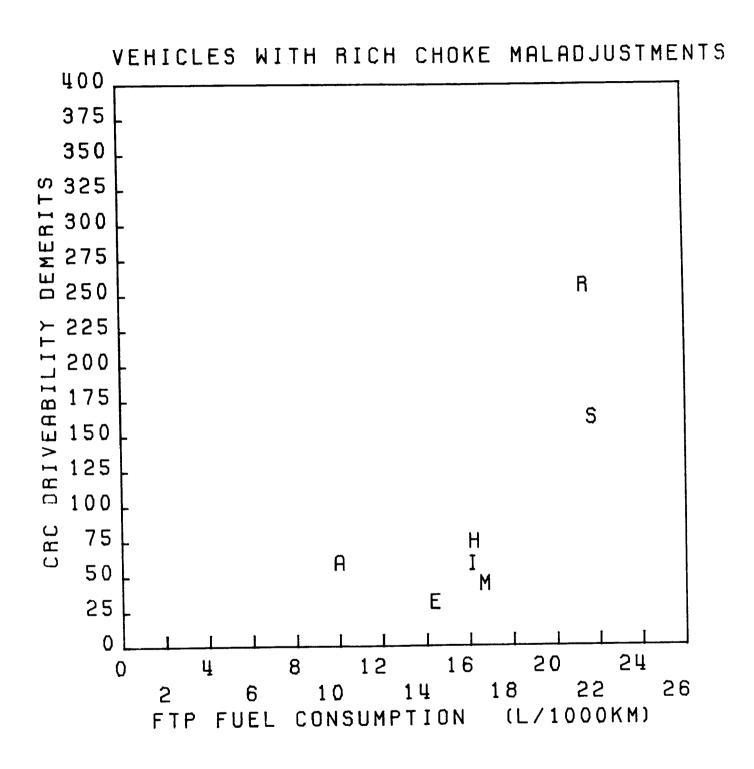


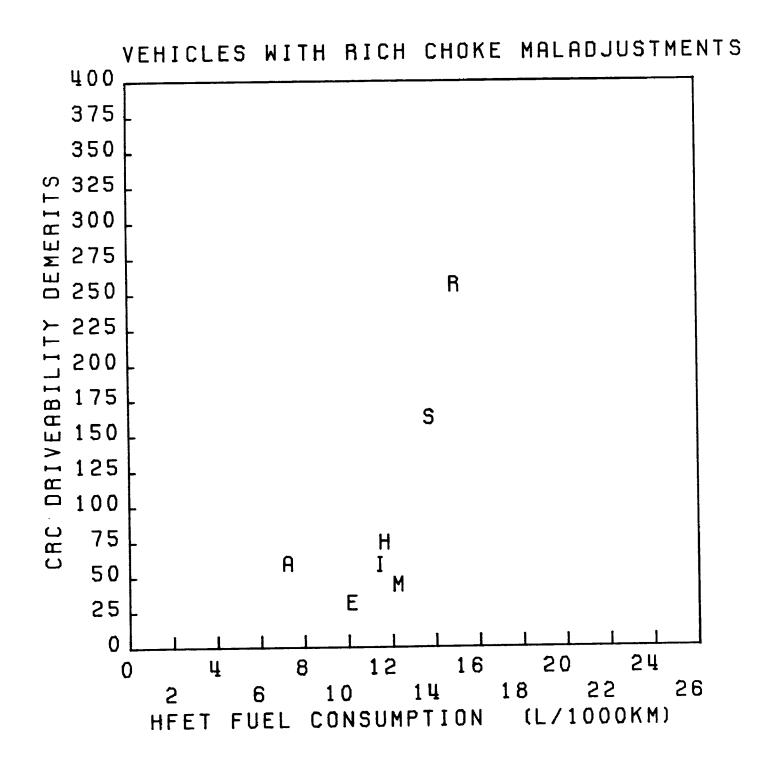






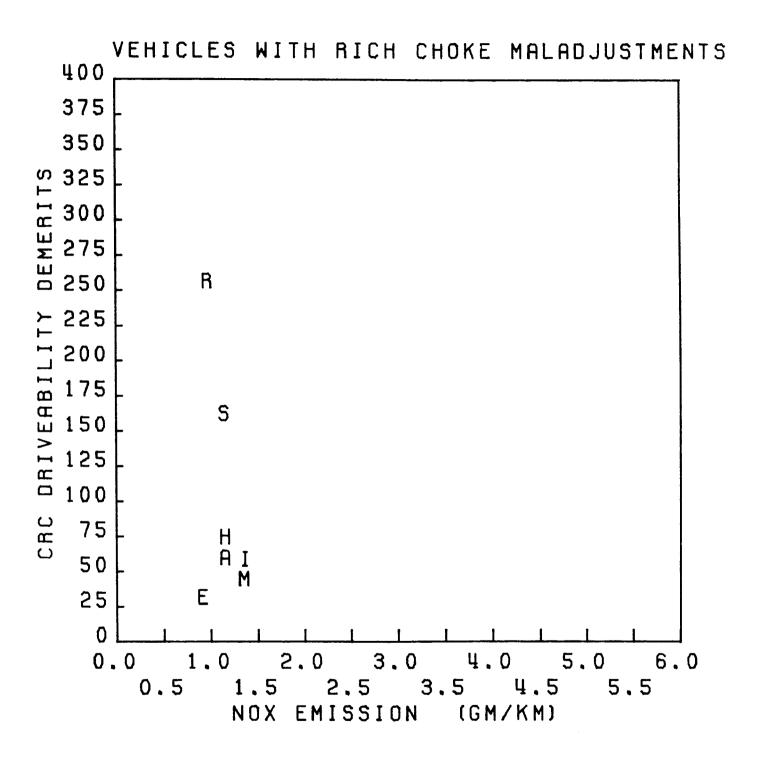


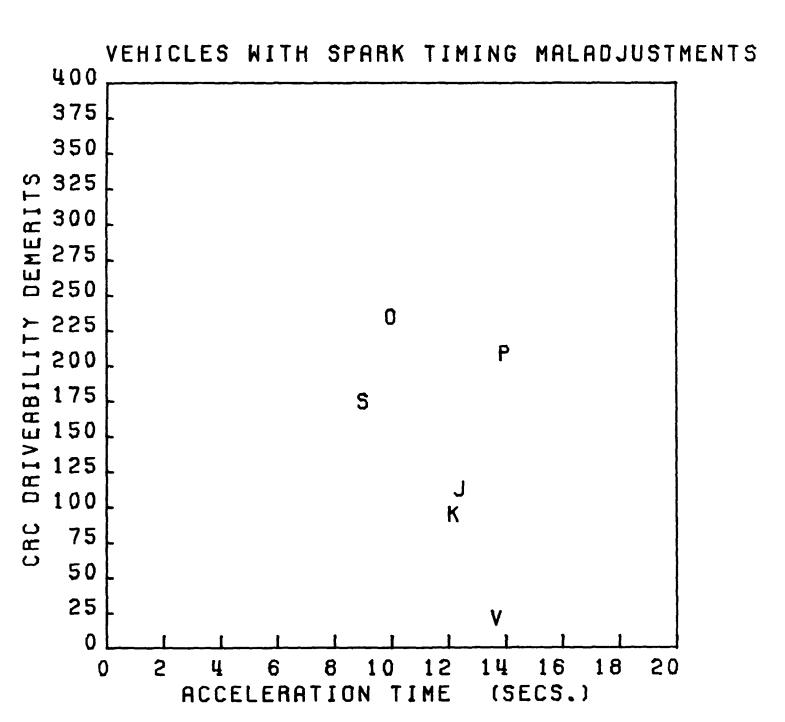


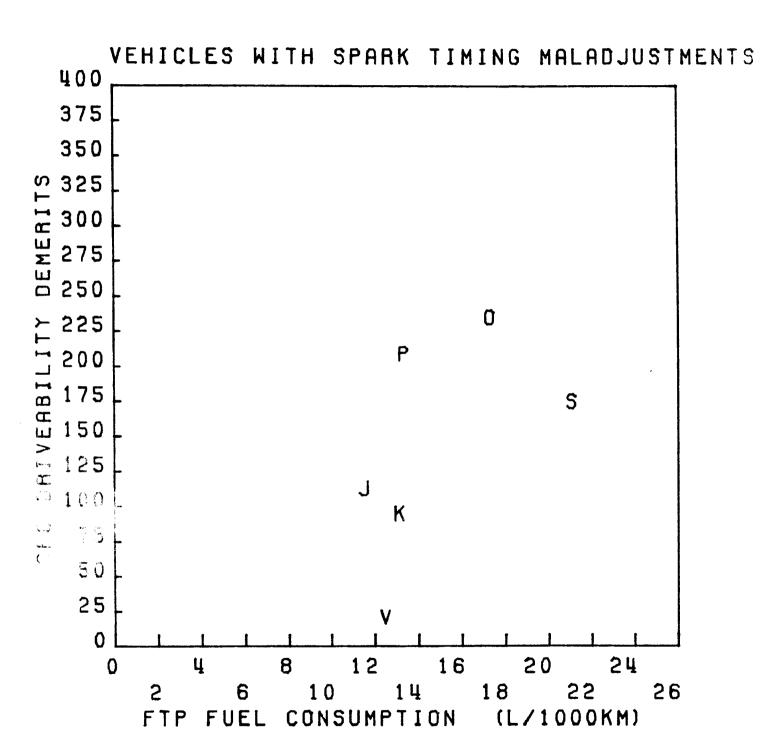


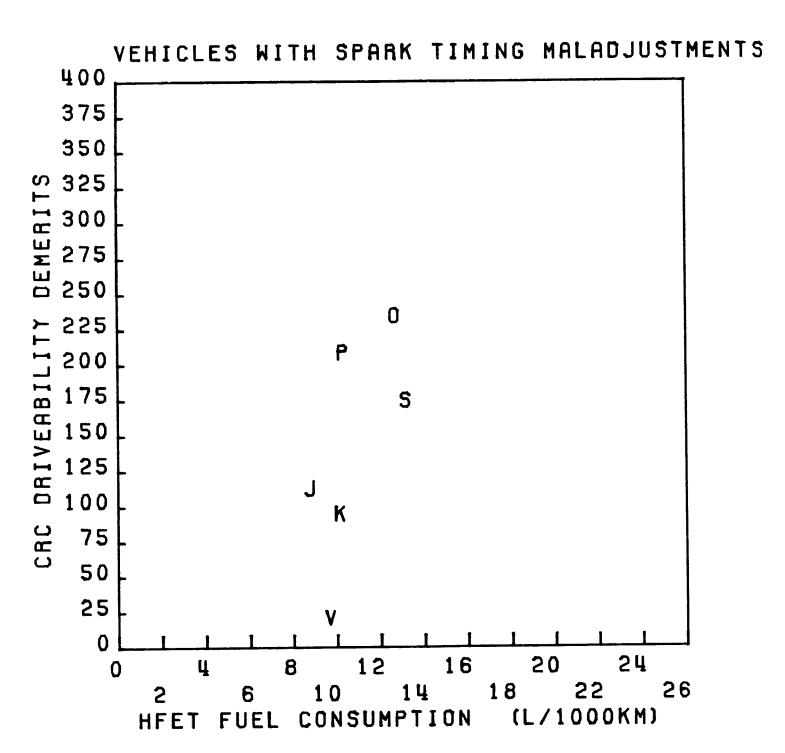
## MALADJUSTMENTS VEHICLES WITH RICH CHOKE 400 375 350 325 300 275 250 R 225 DRIVEABILITY 200 175 S 150 125 100 CRC 75 H A I 50 M E 25 0 2.0 1.2 1.6 0.4 0.8 0.0 (GM/KM) **EMISSION** HC

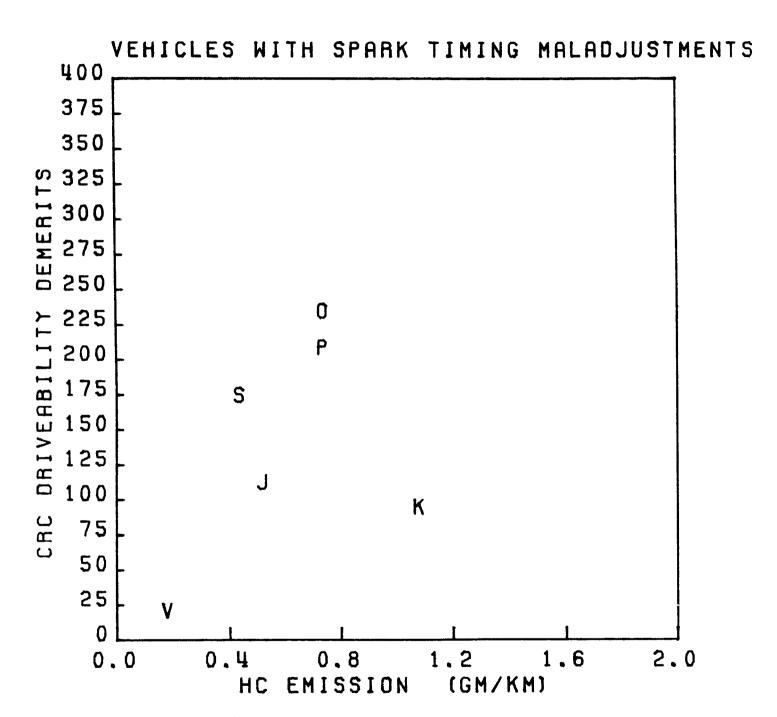
## VEHICLES WITH RICH CHOKE MALADJUSTMENTS S 325 DEWER 300 275 250 DRIVEABILIT 500 125 125 100 100 S CRC H IA E (GM/KM) **EMISSION** CO



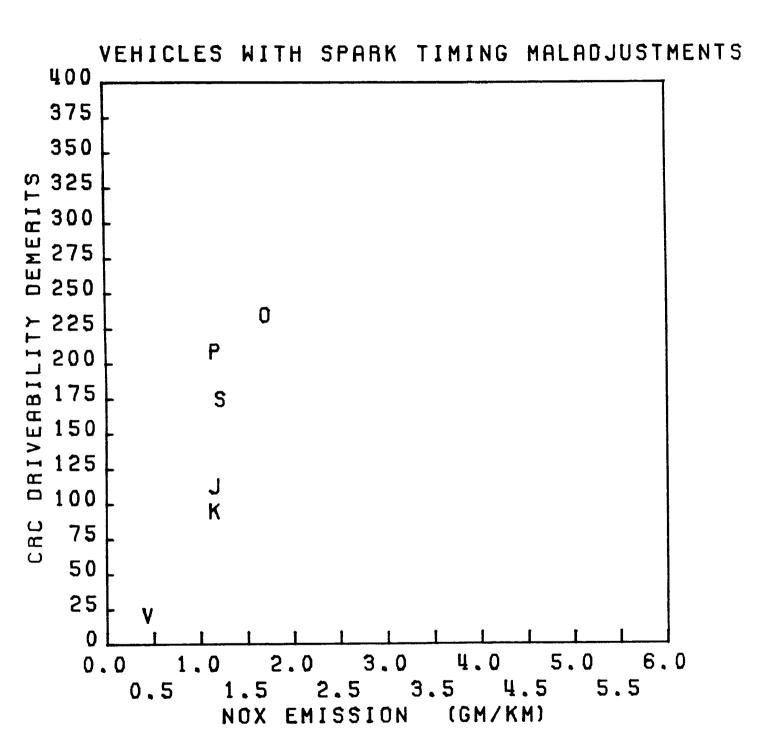


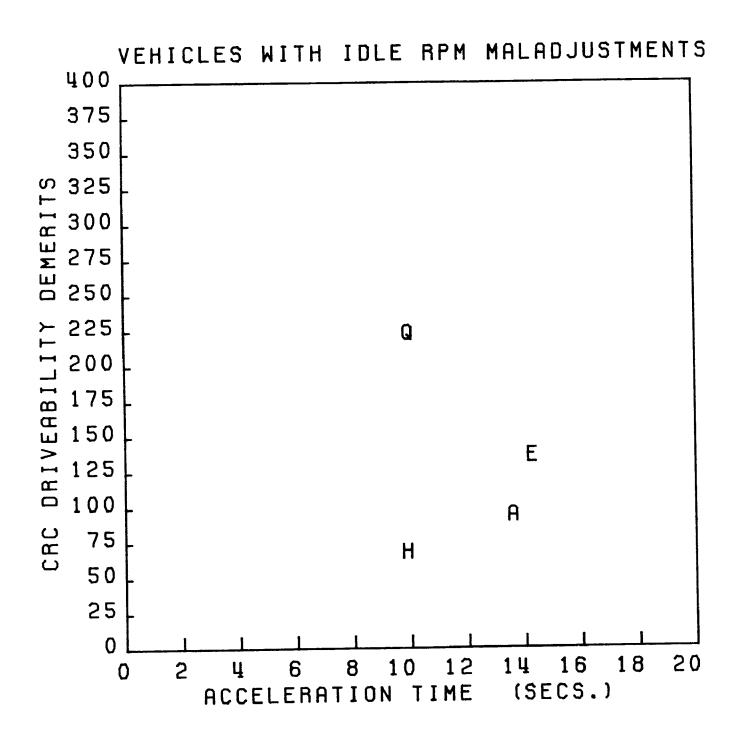


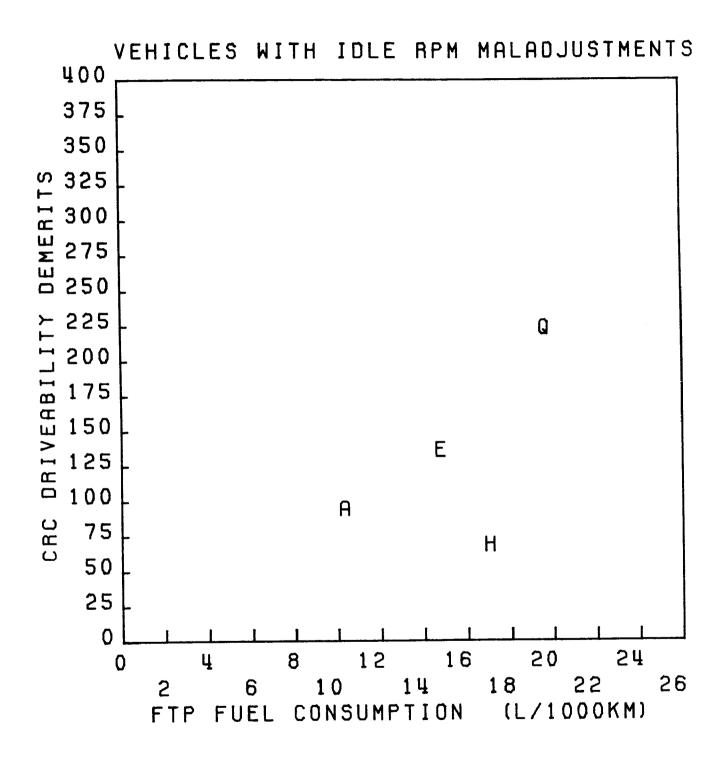


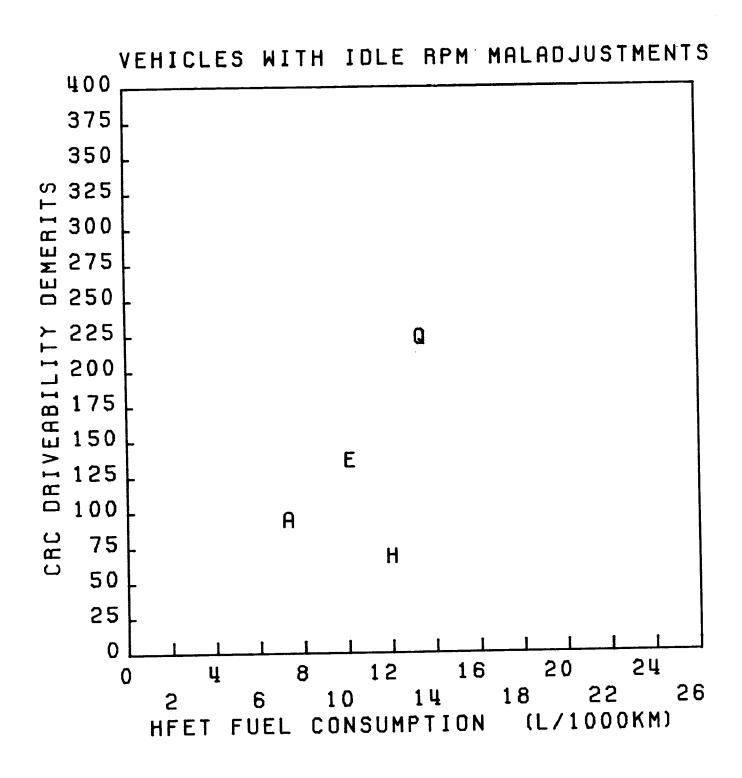


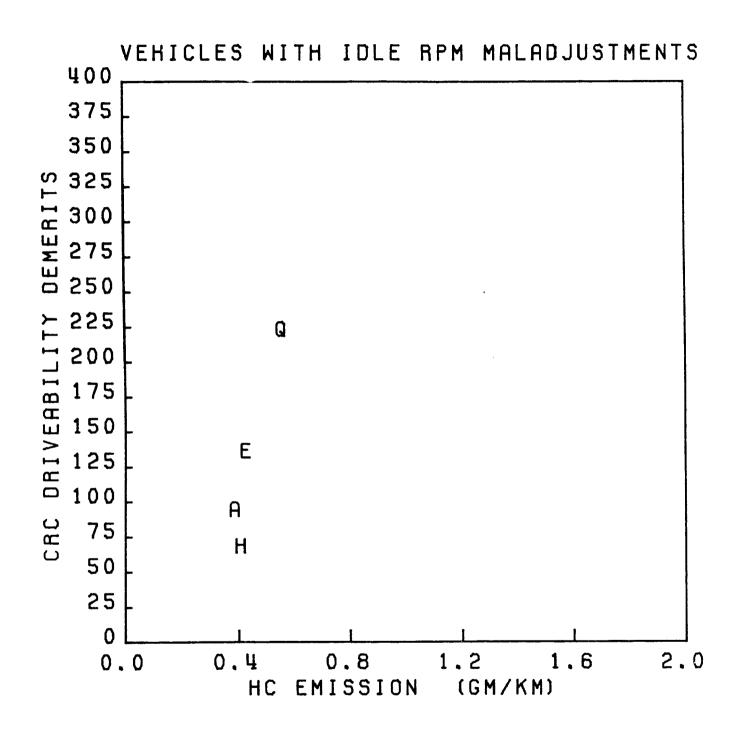
## VEHICLES WITH SPARK TIMING MALADJUSTMENTS 300 275 250 DRIVERBILITY 200 125 100 100 P S J K CRC (GM/KM) **EMISSION** CO

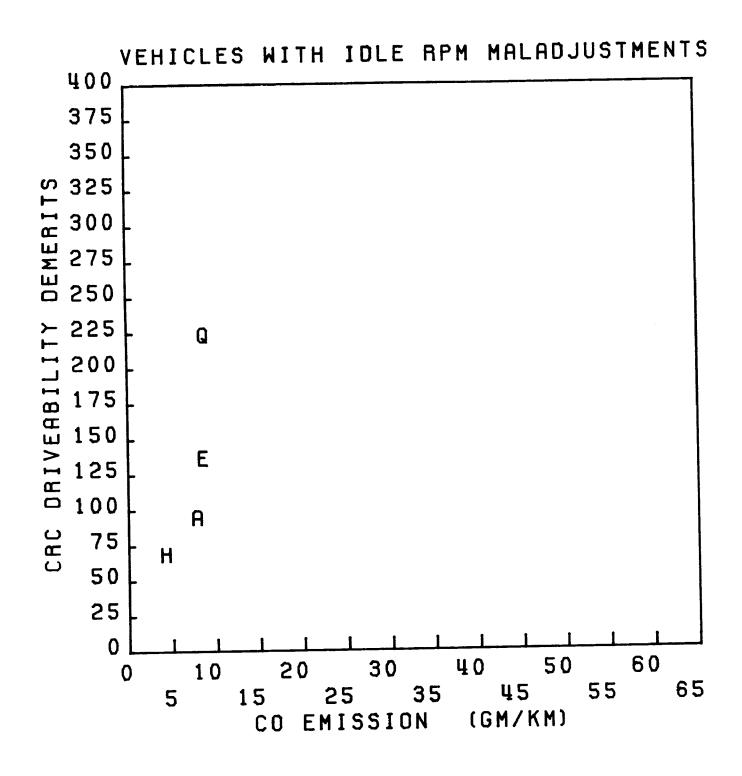


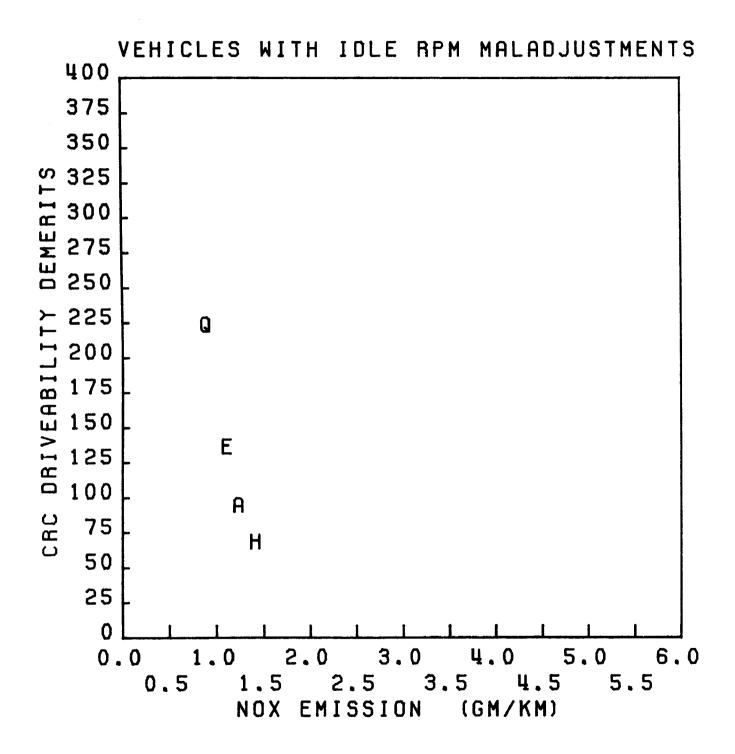


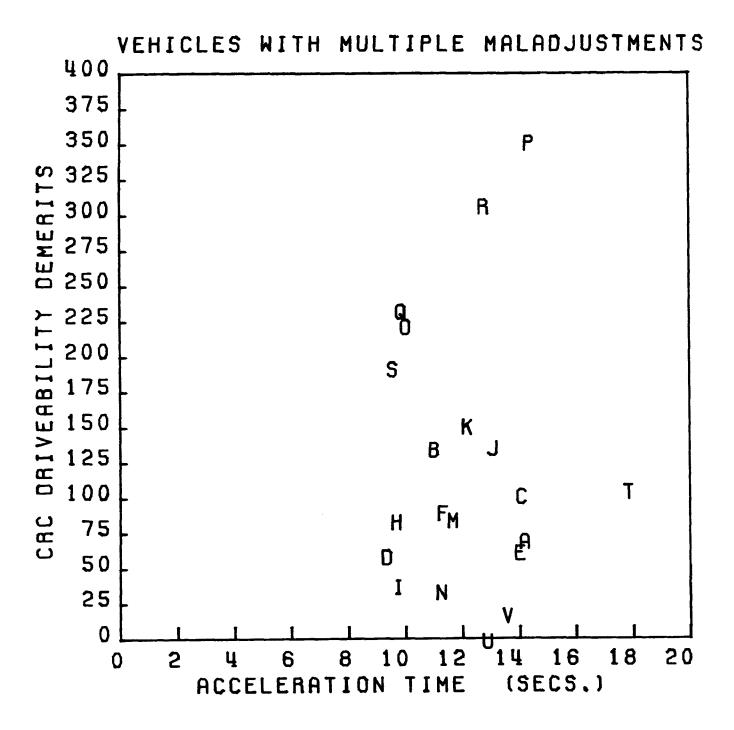


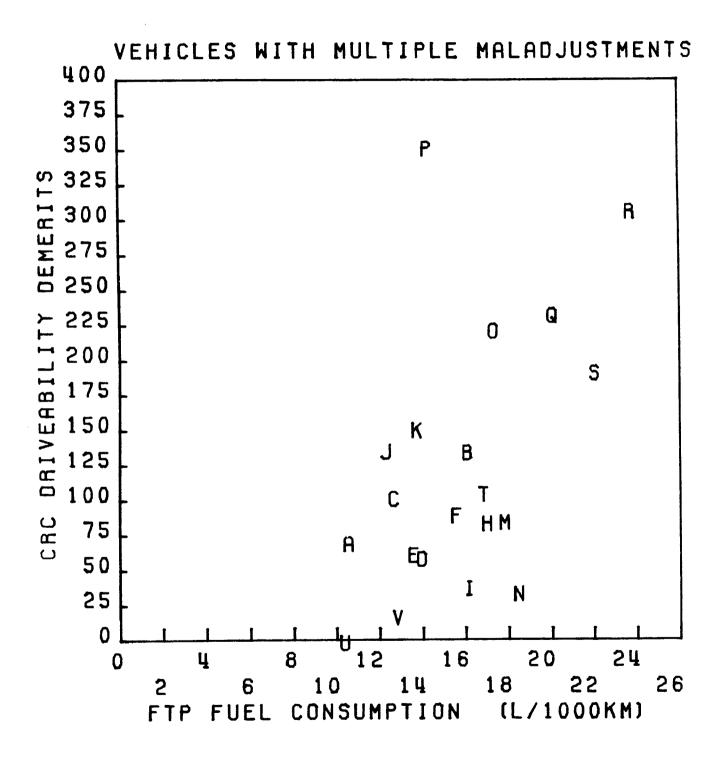


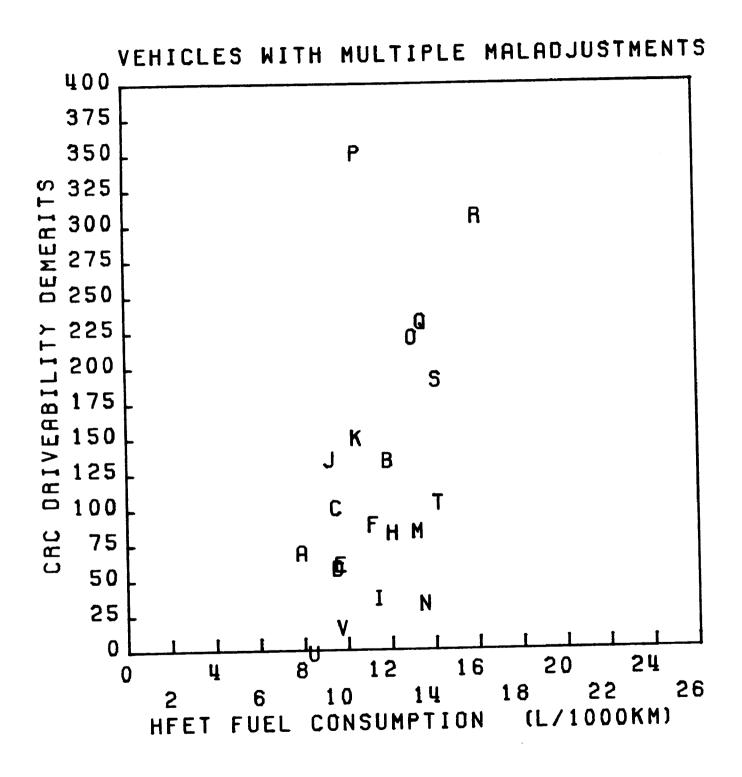


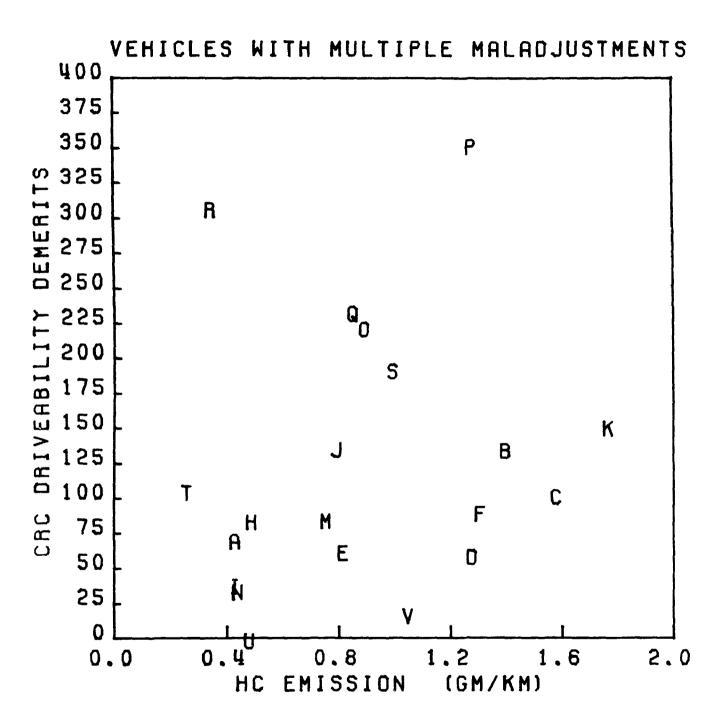


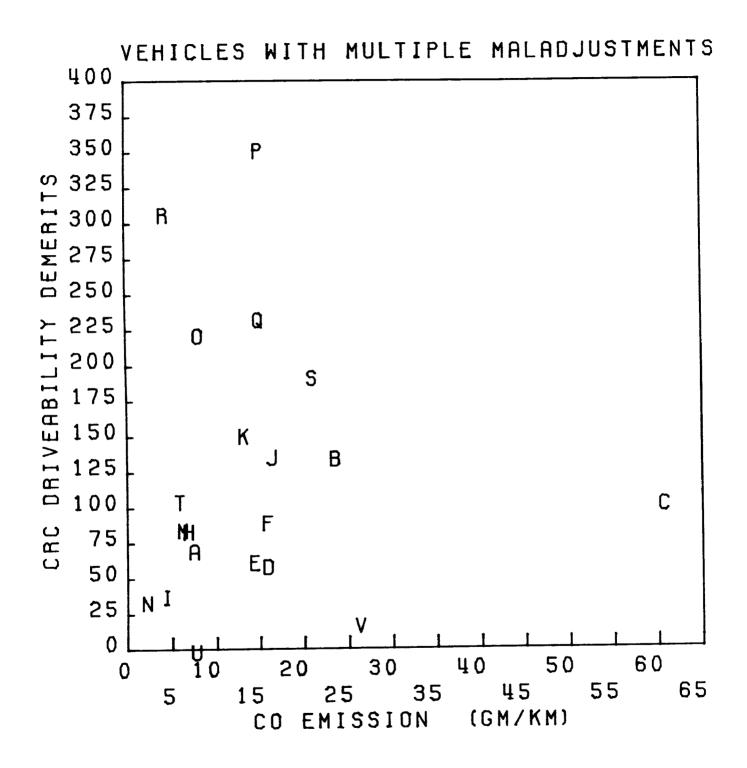


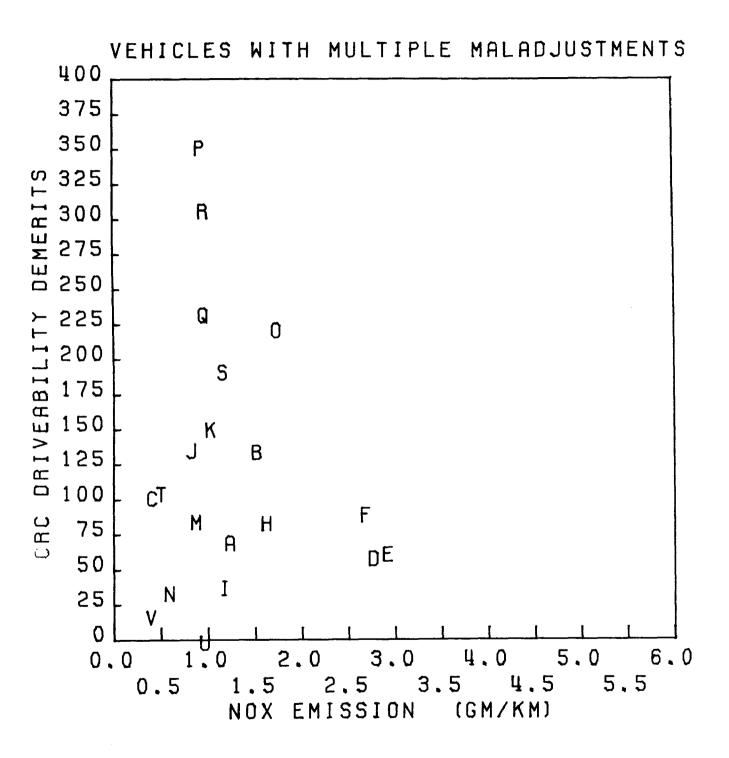


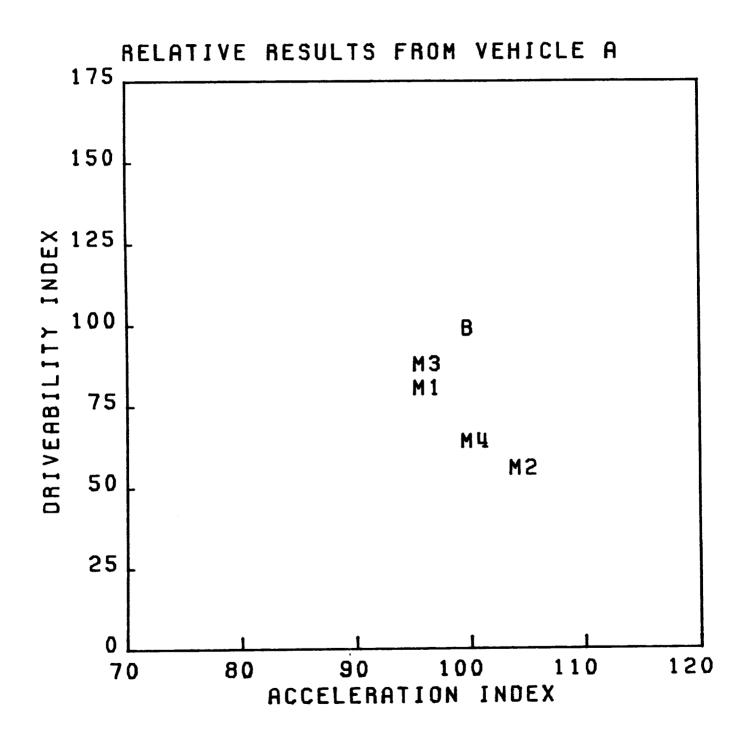


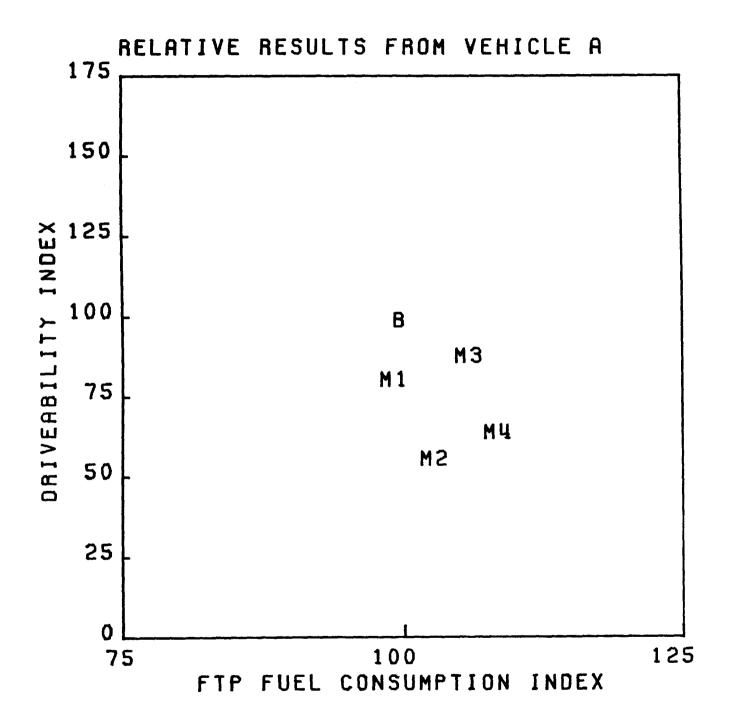


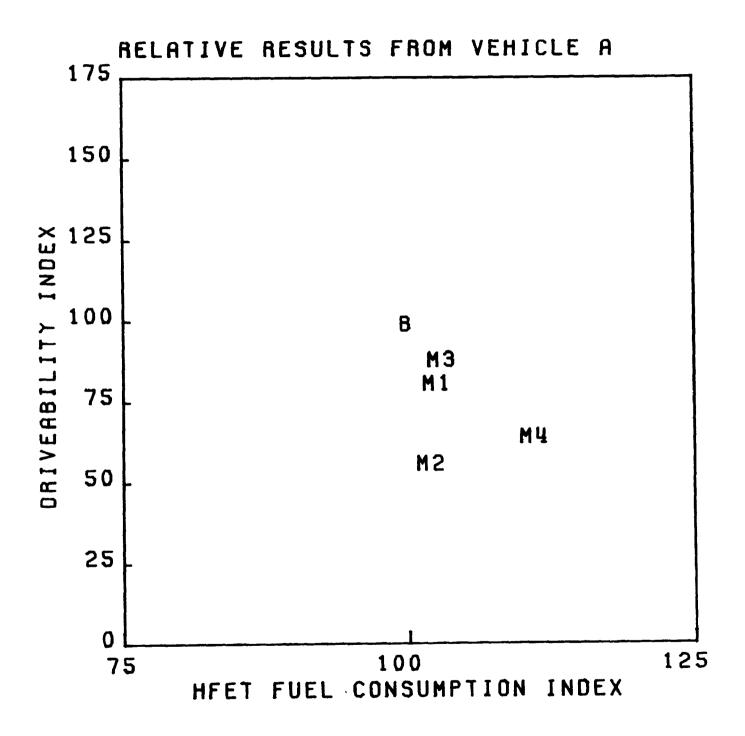


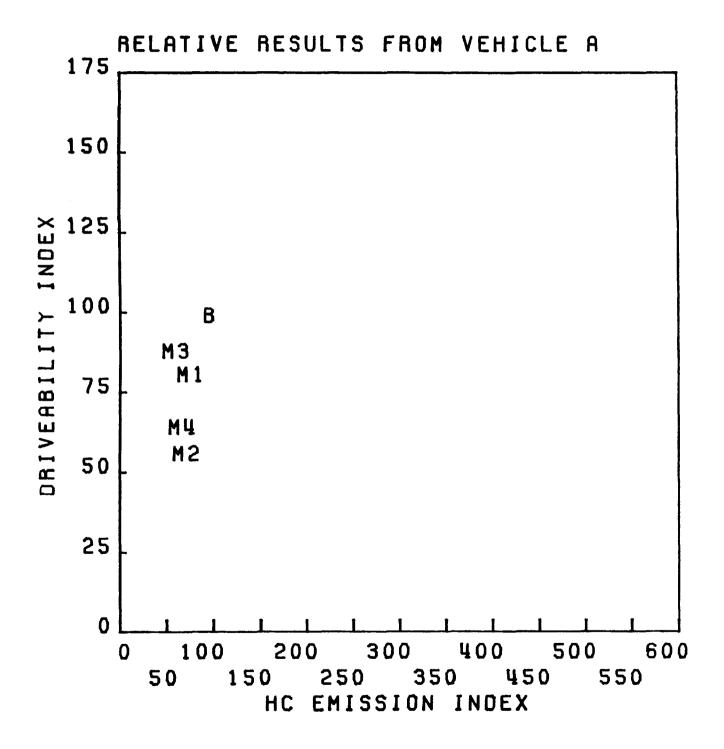


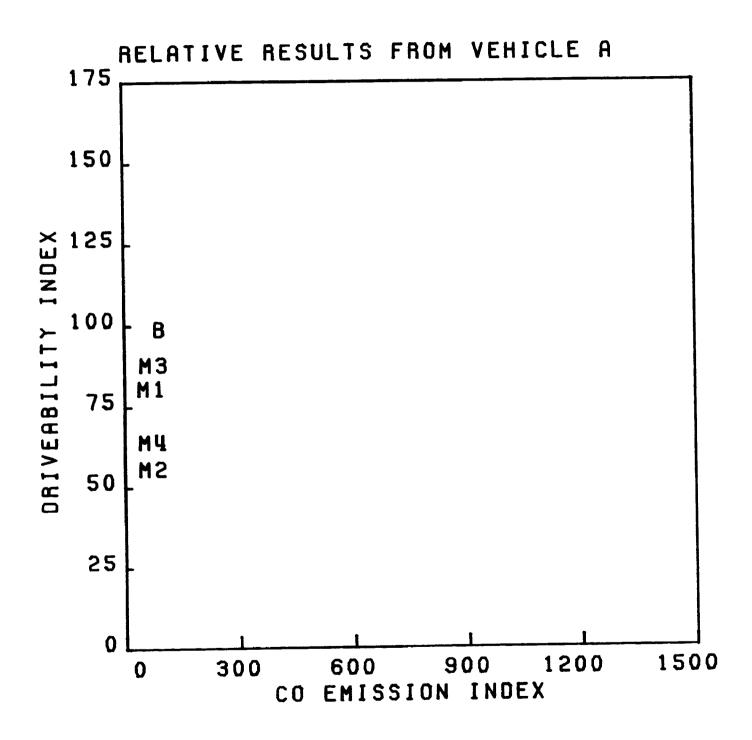


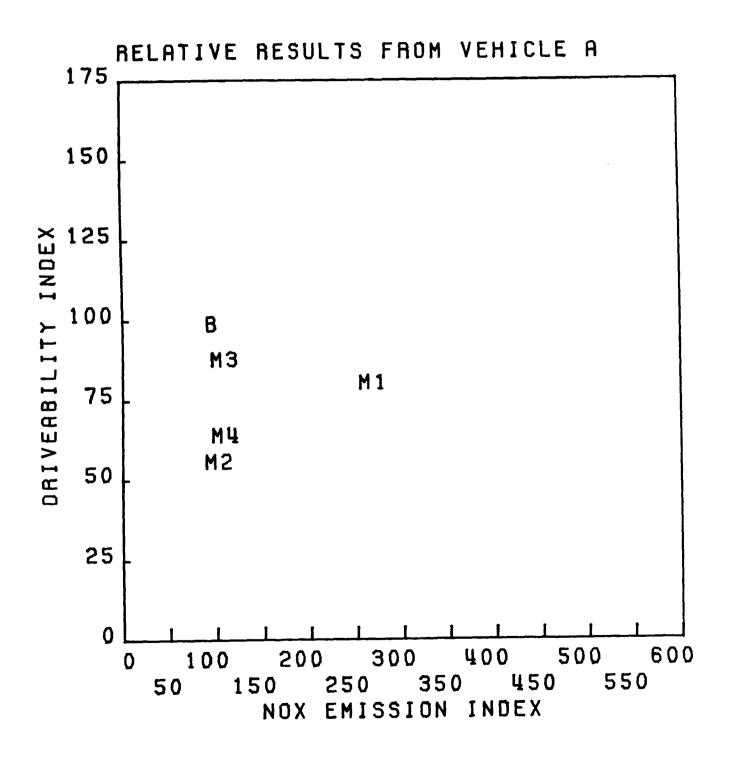


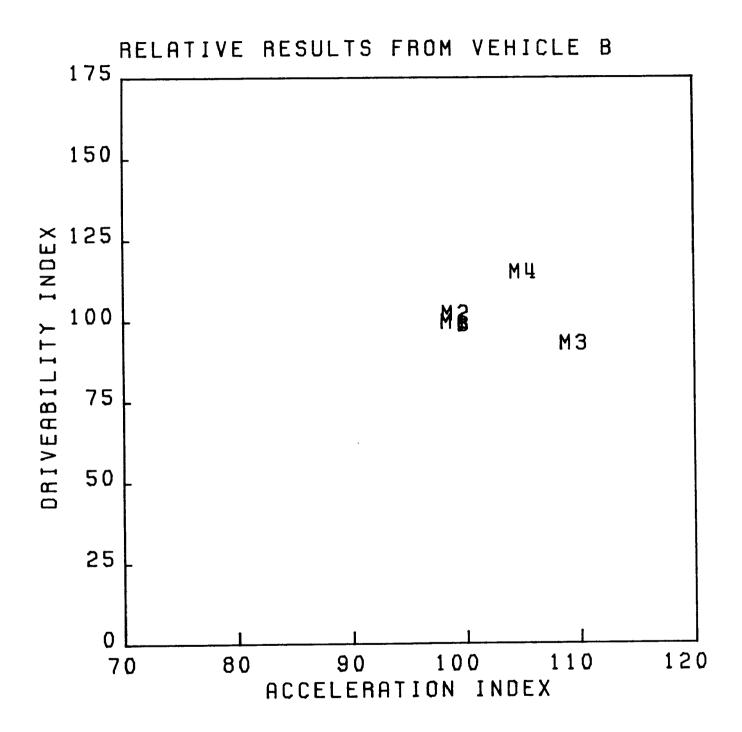


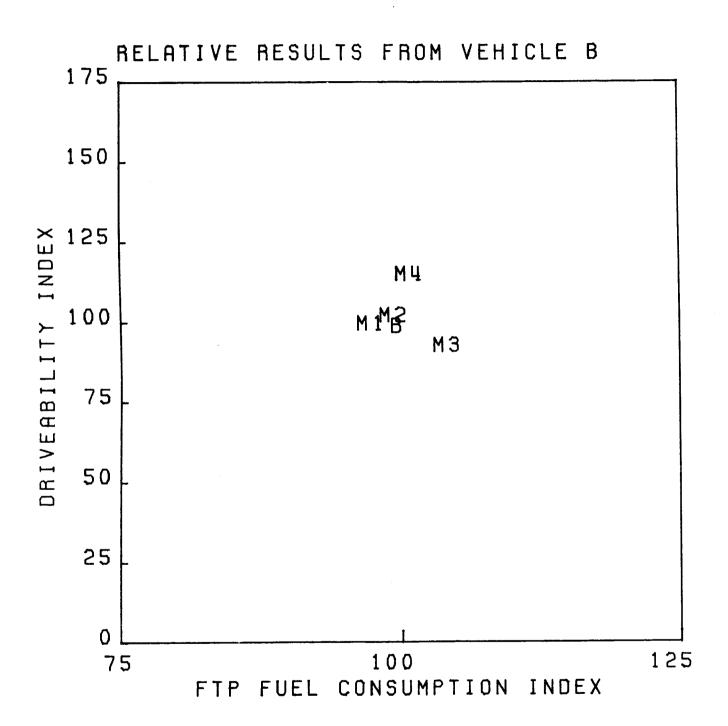


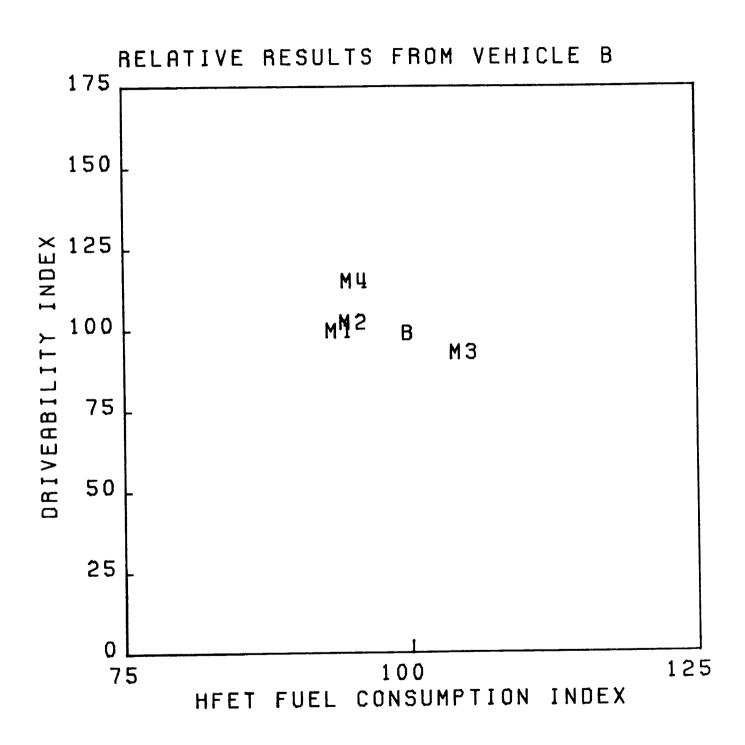


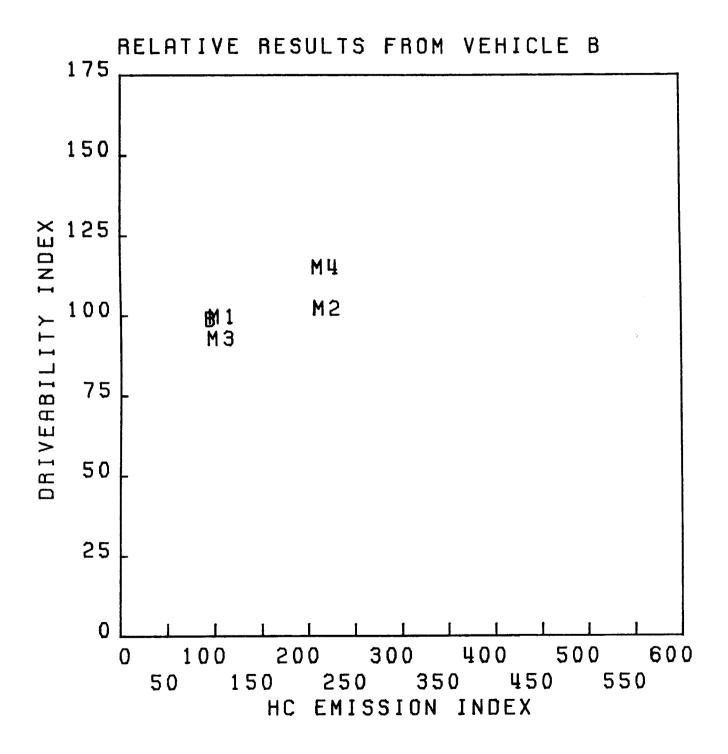


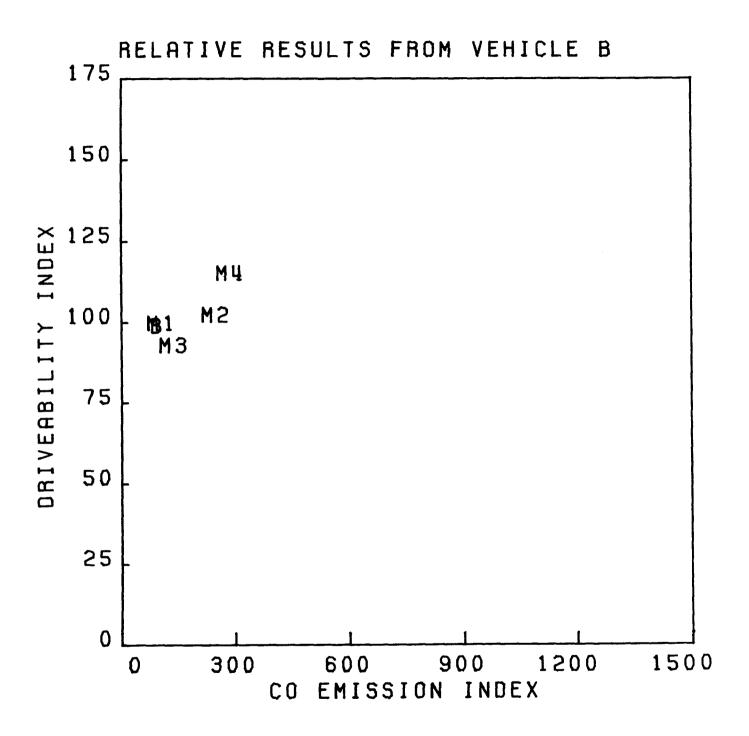


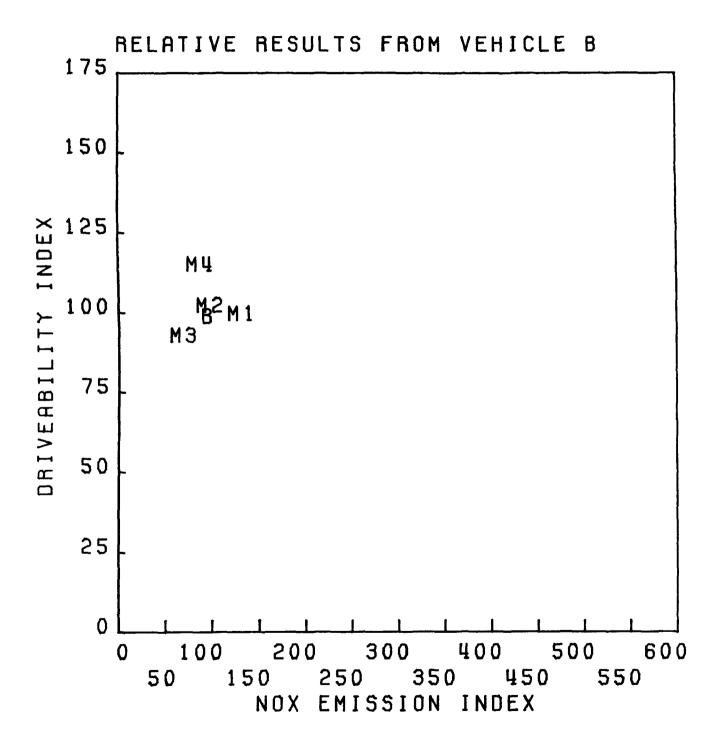


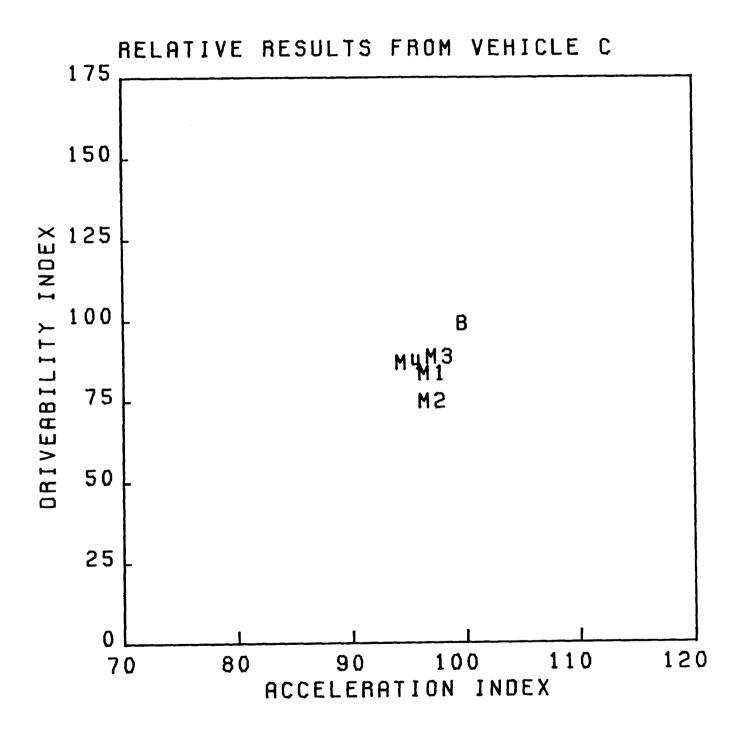


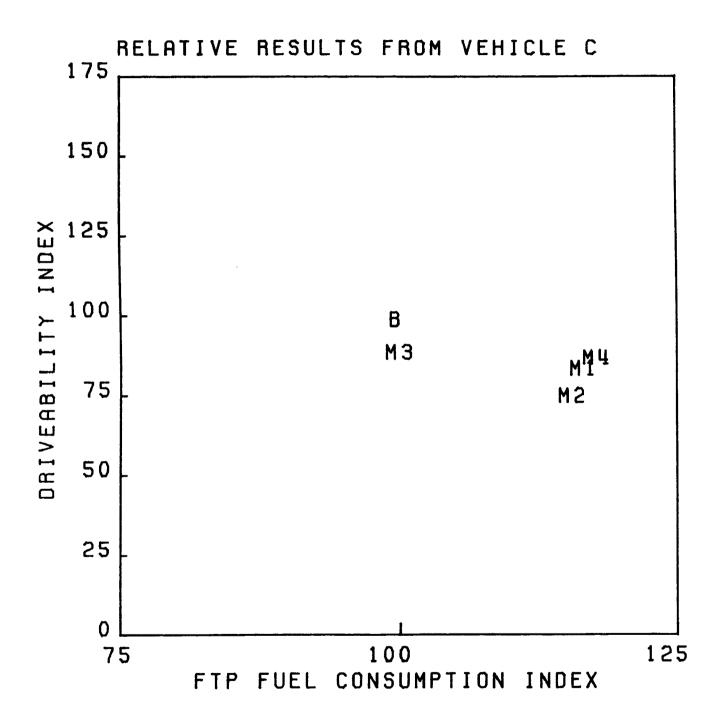


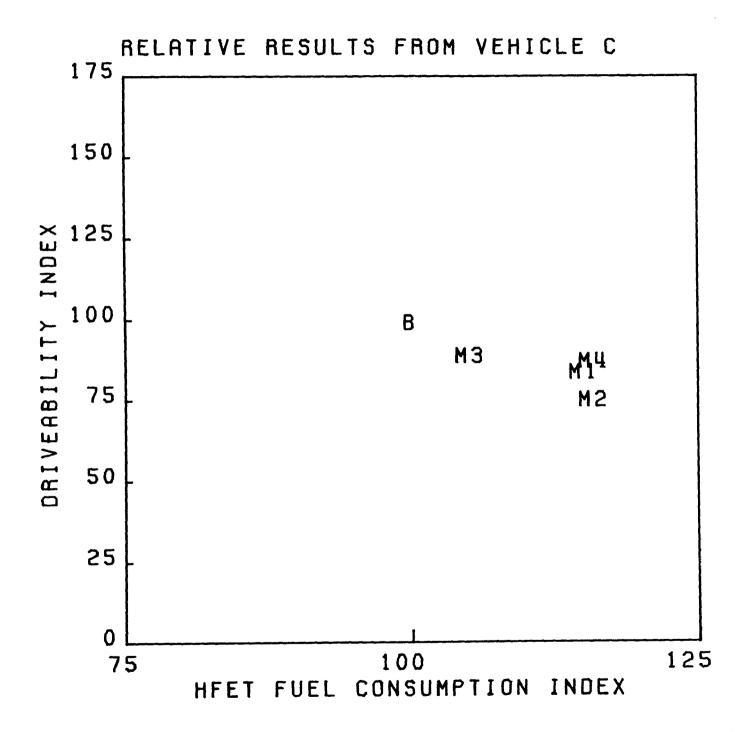


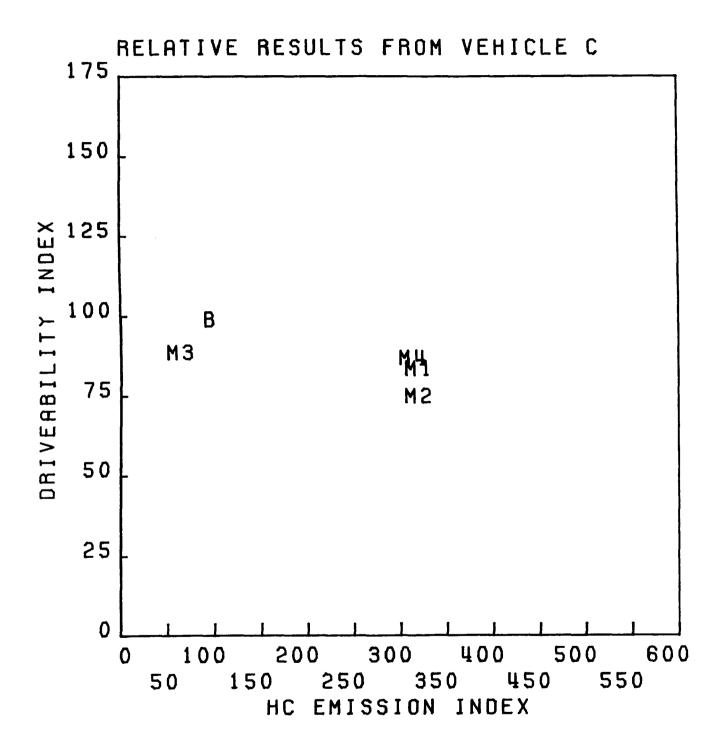


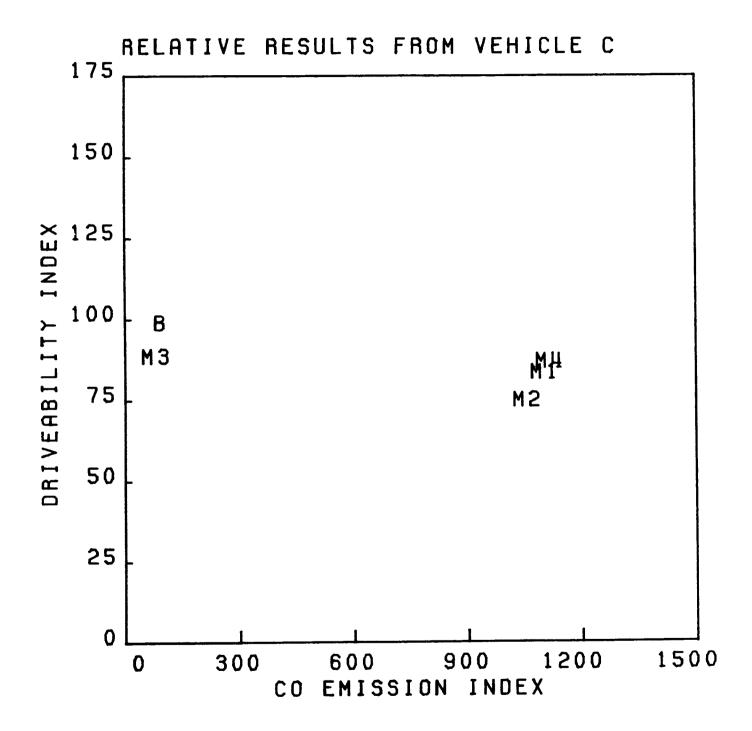


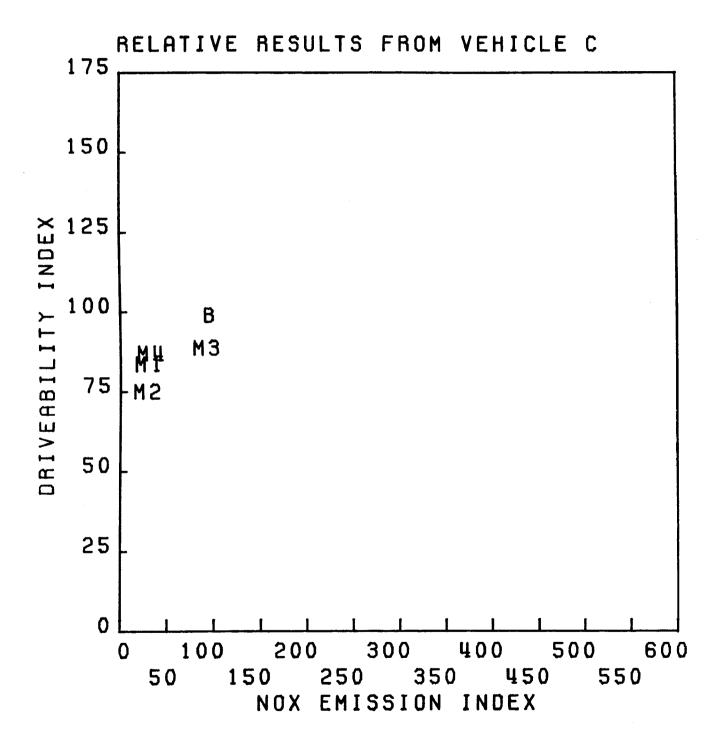


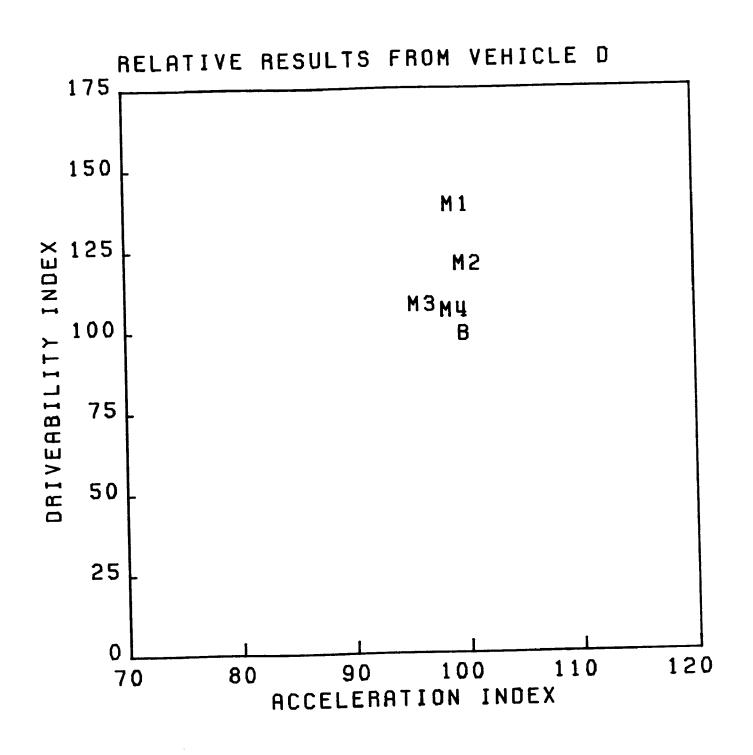


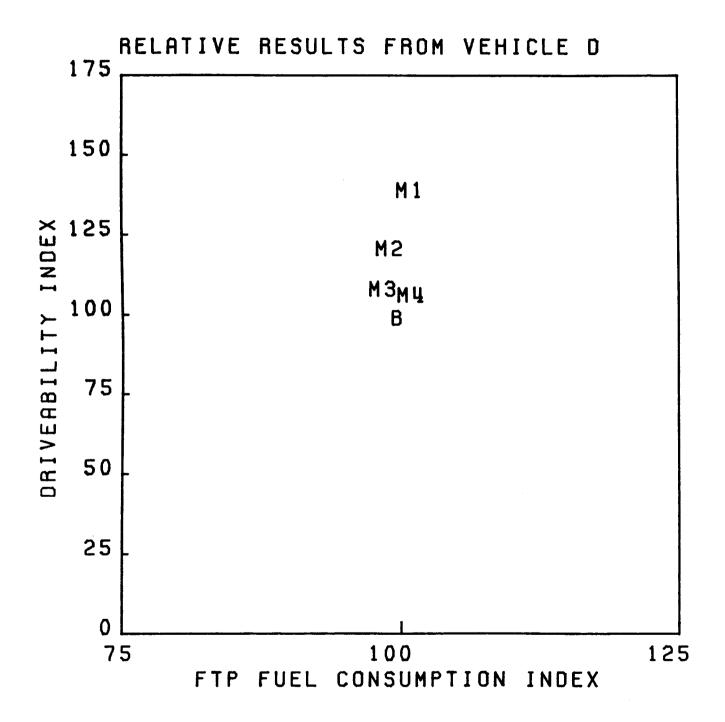


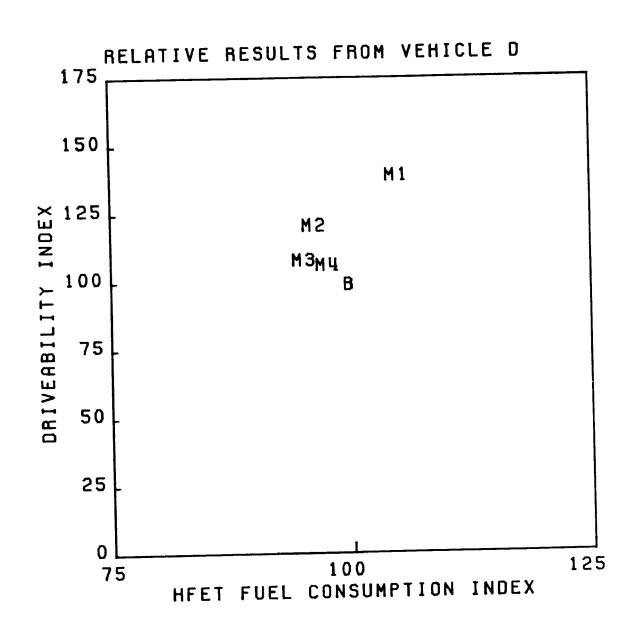


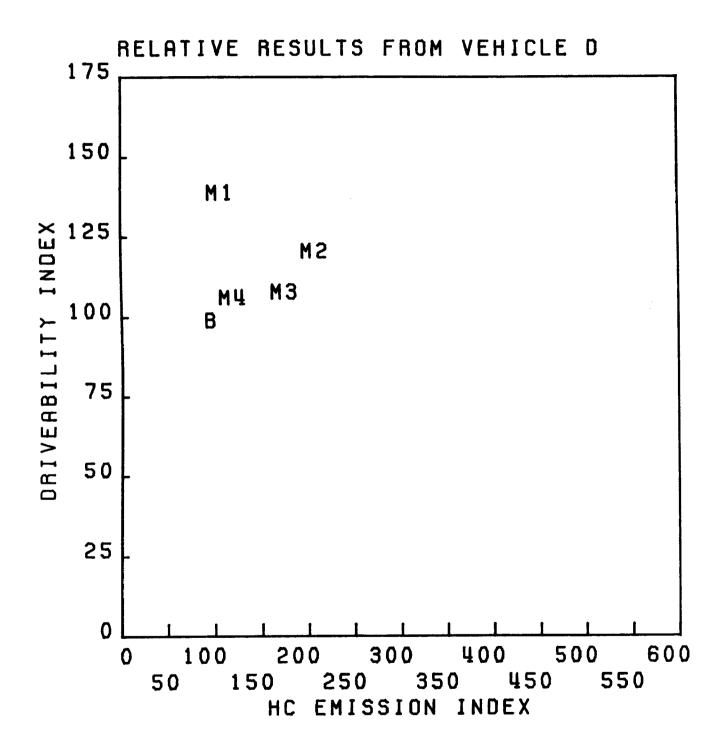


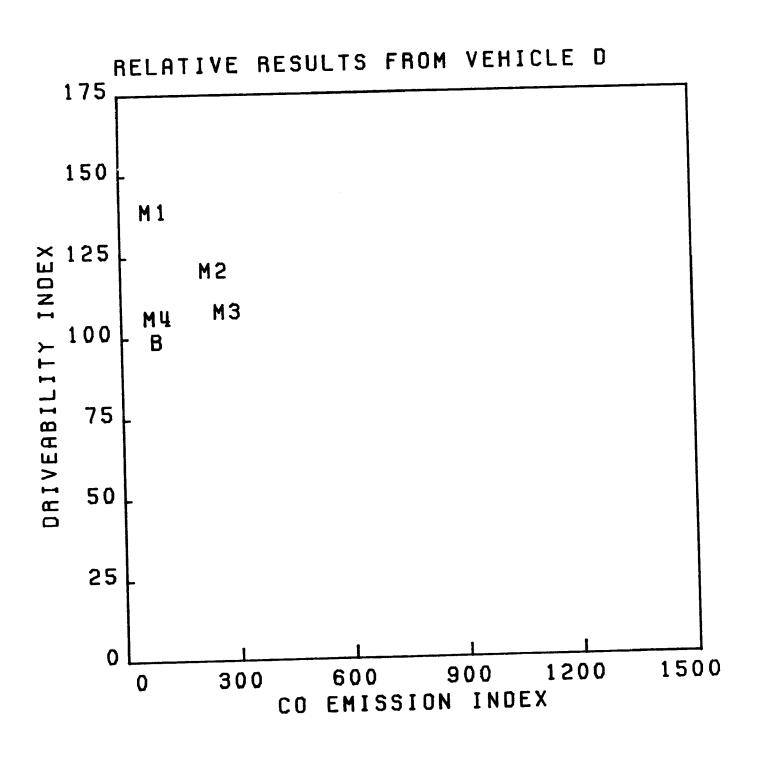


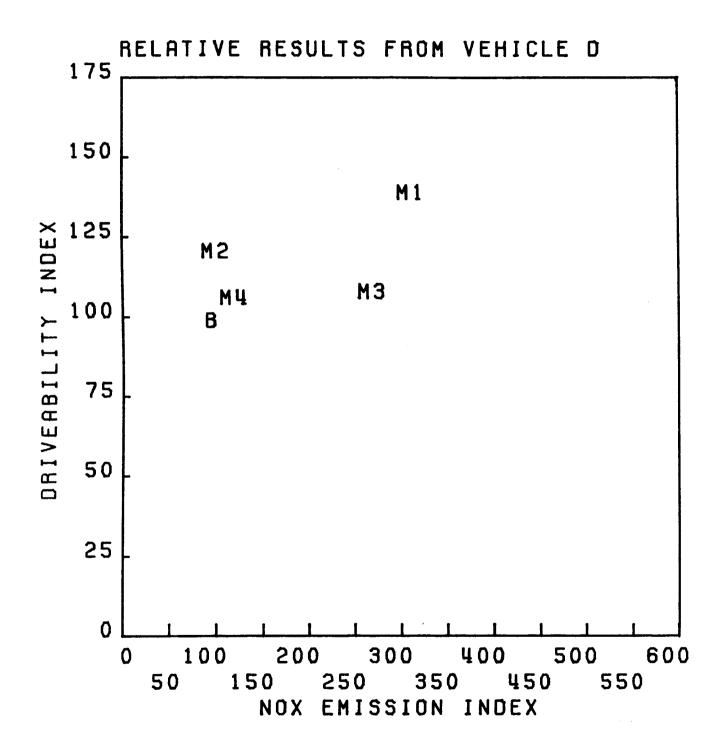


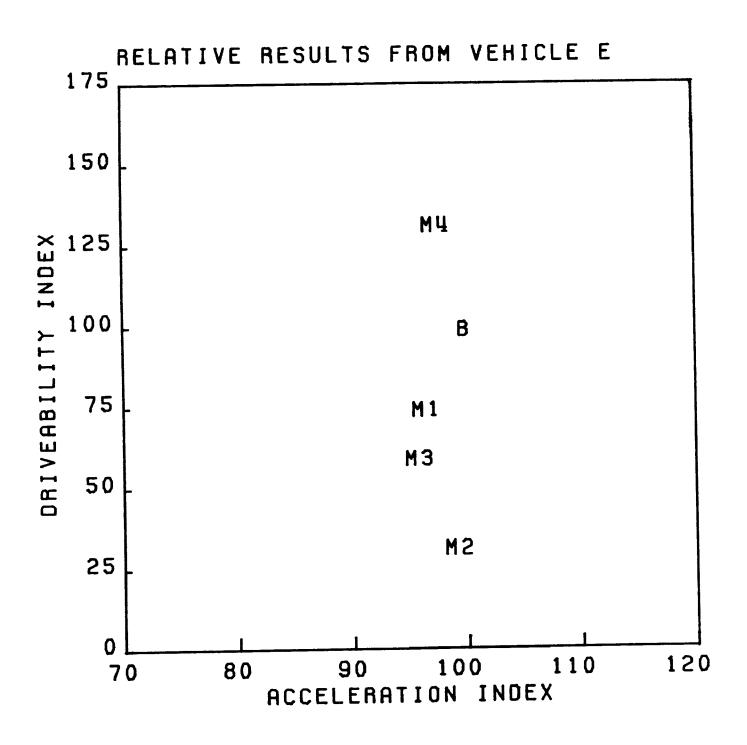


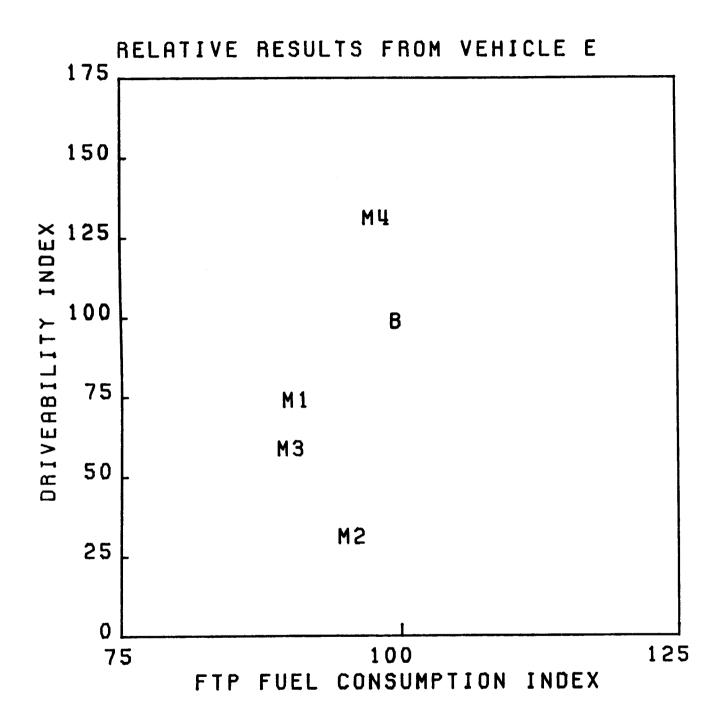


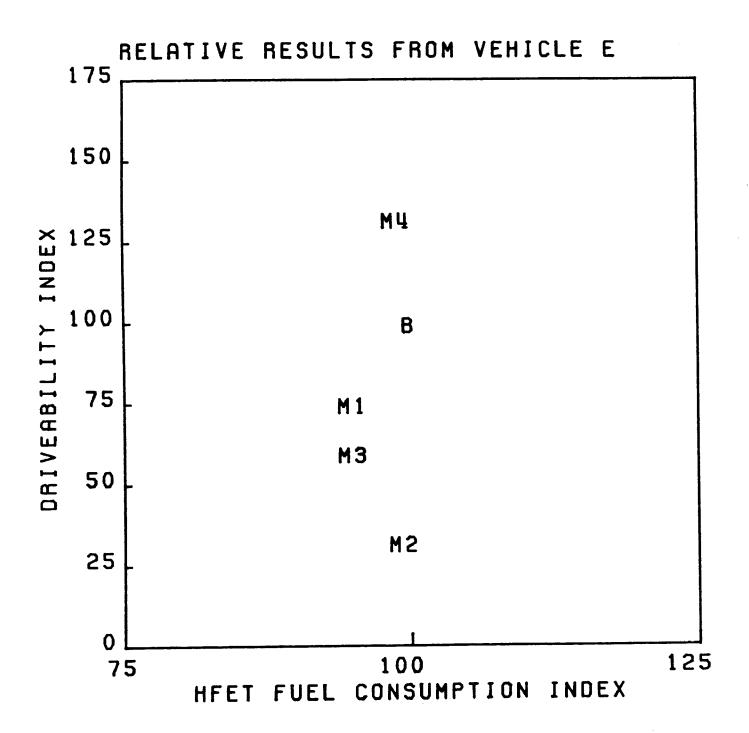


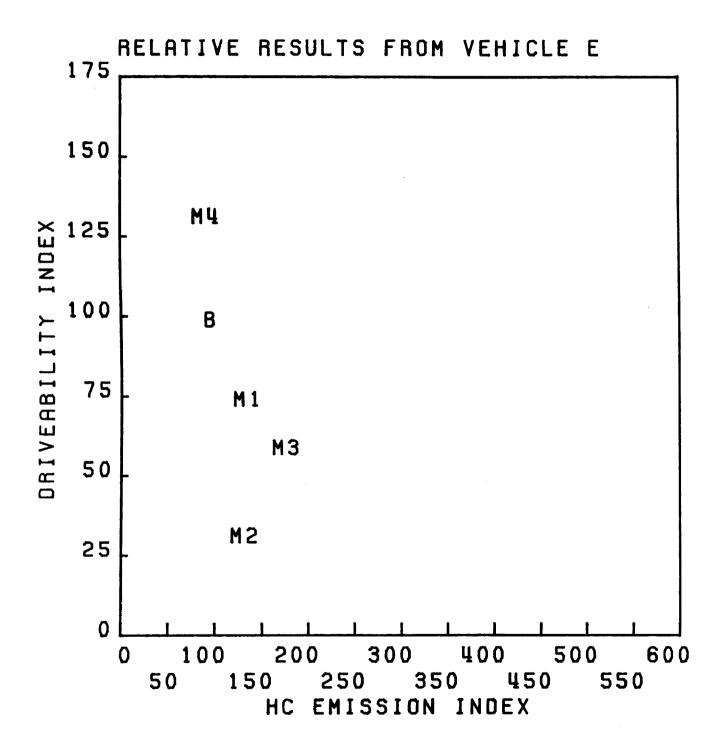


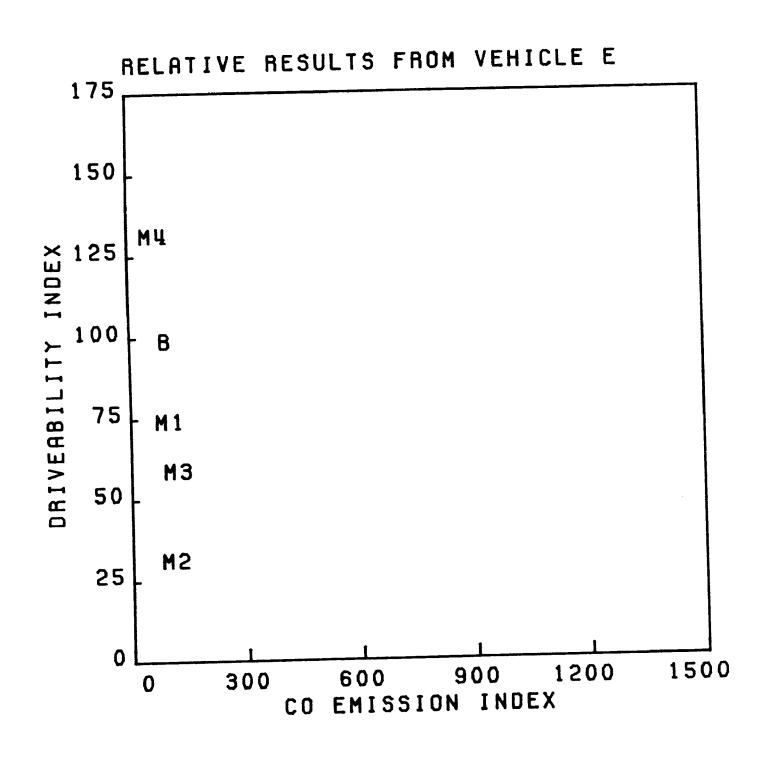


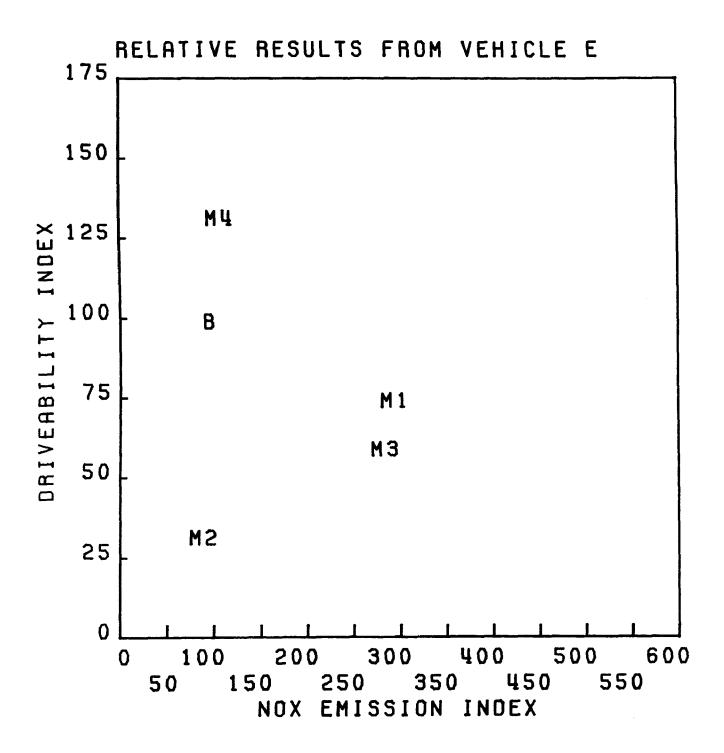


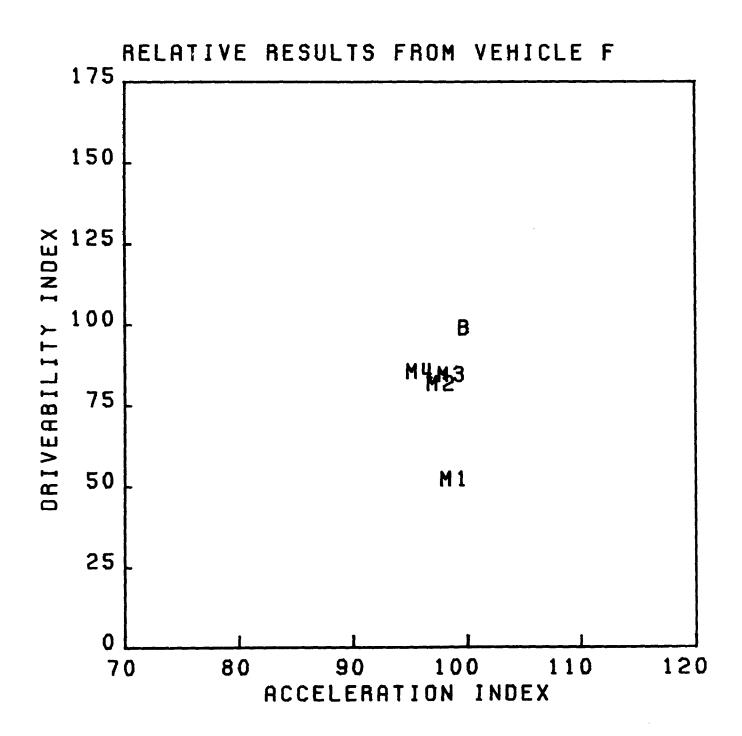


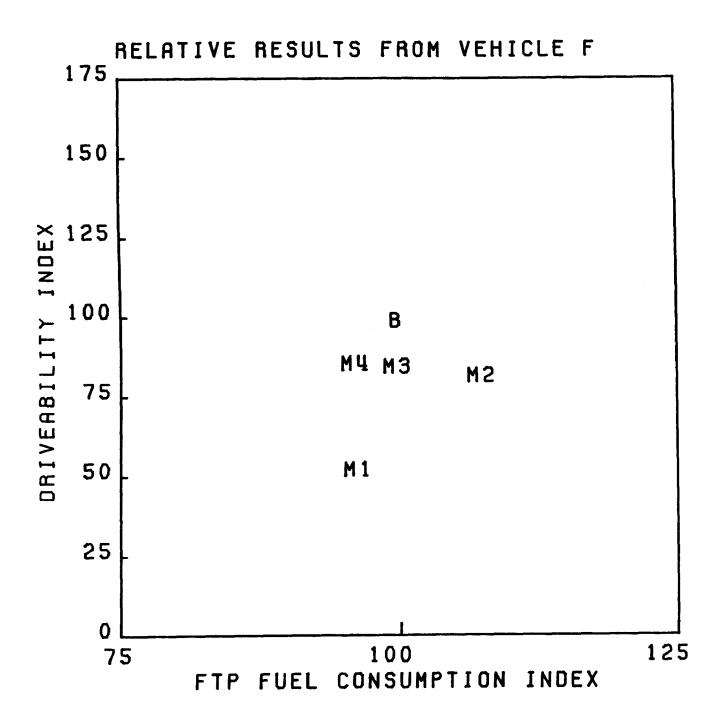


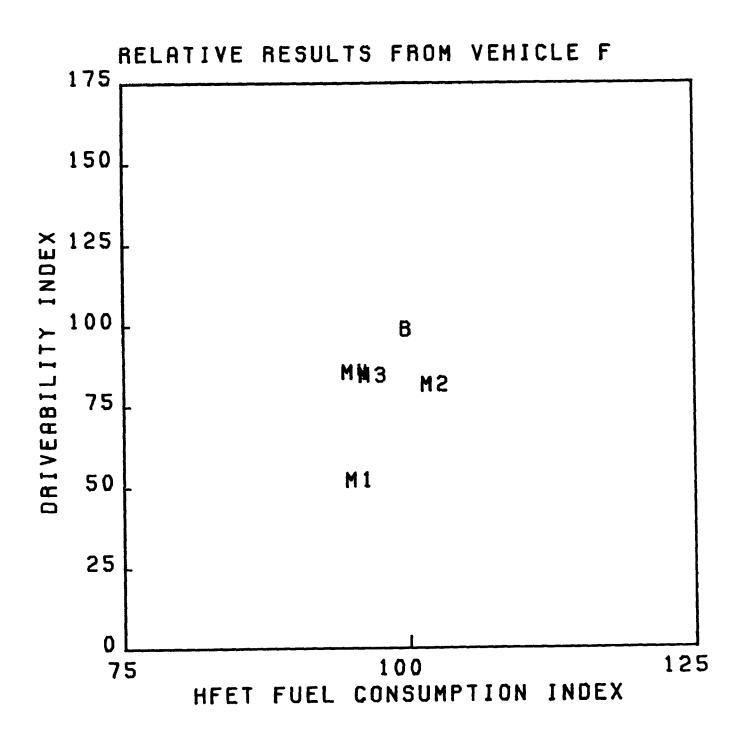


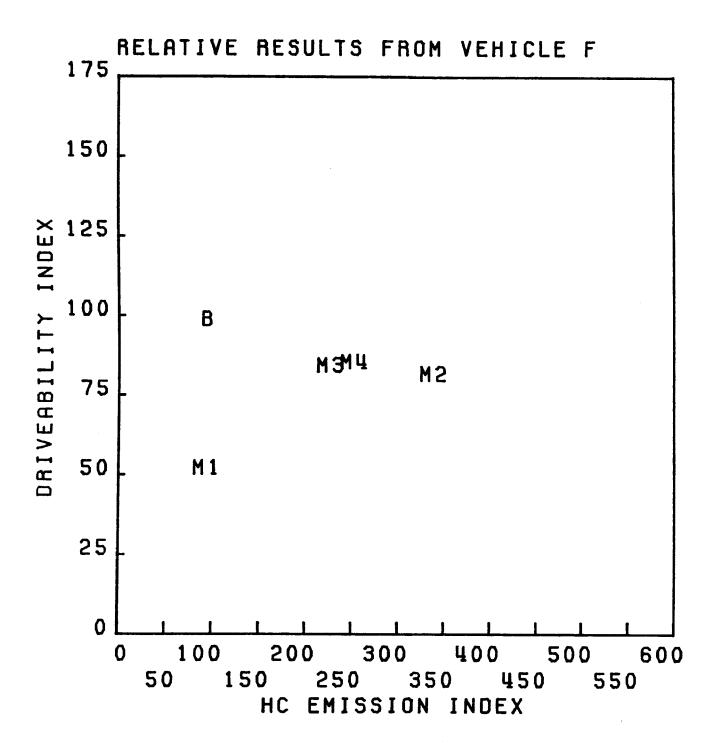


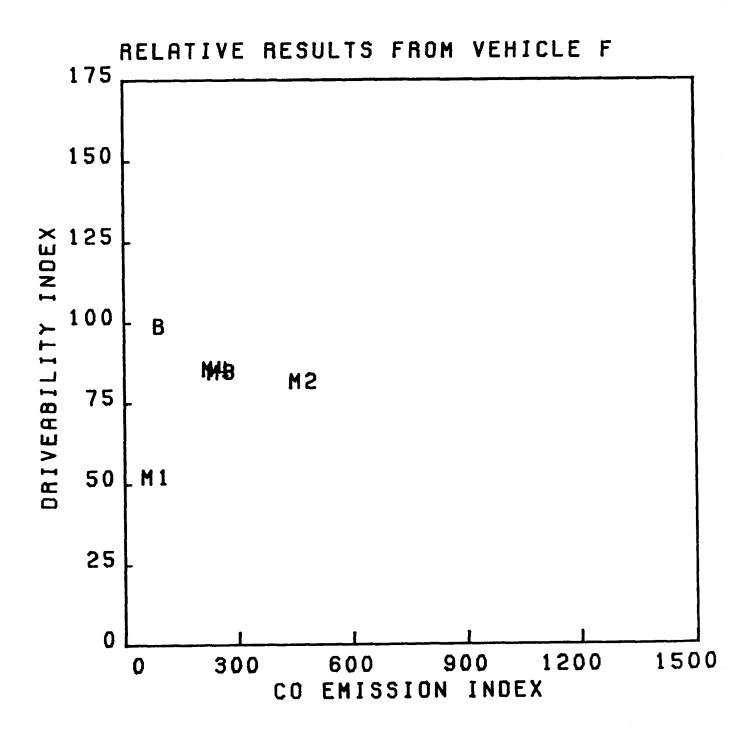


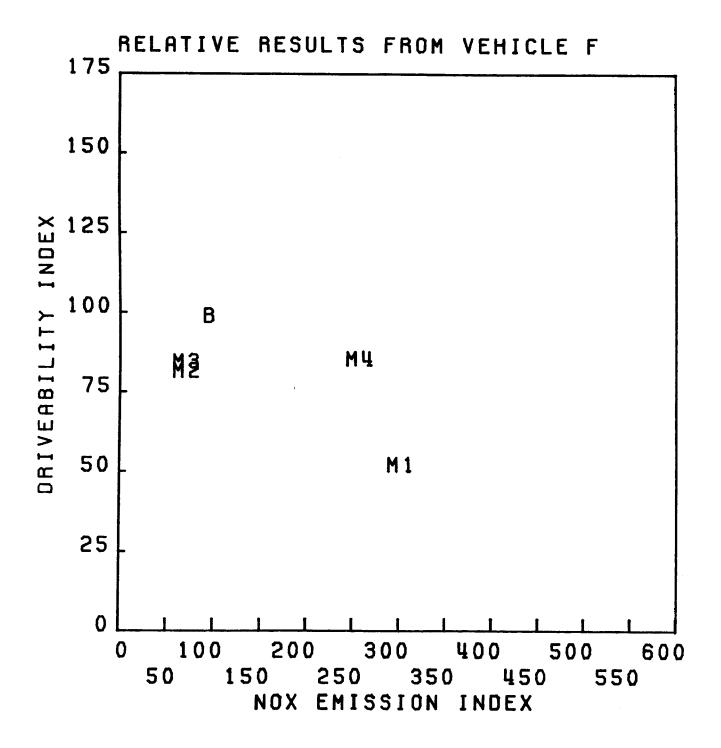


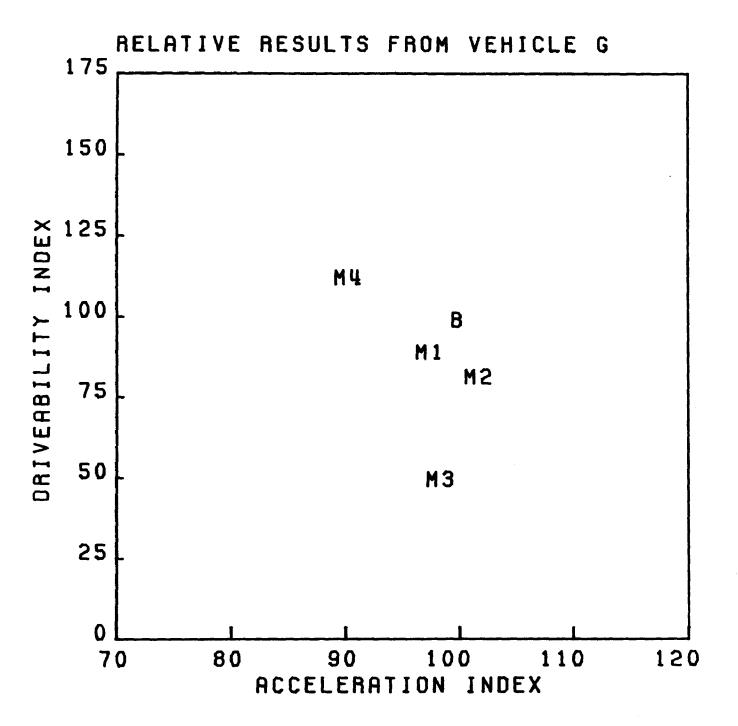


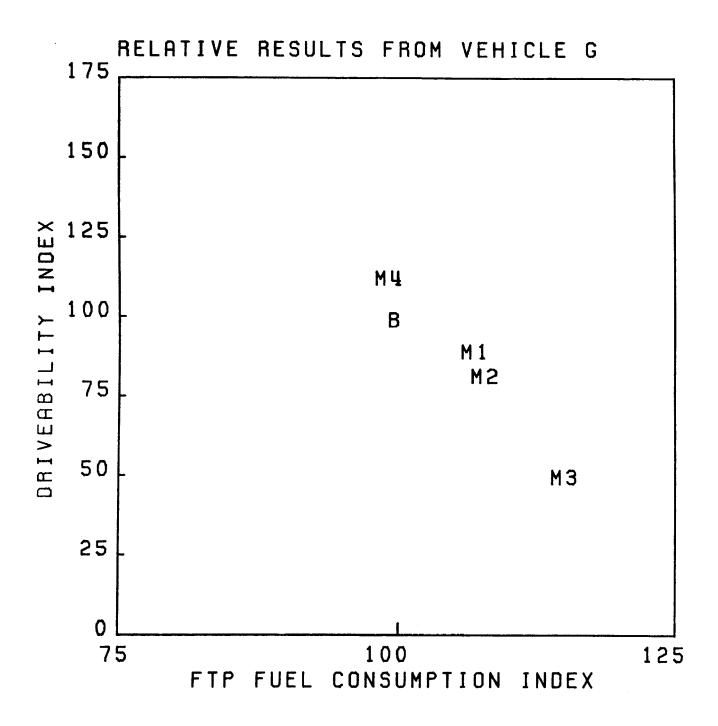


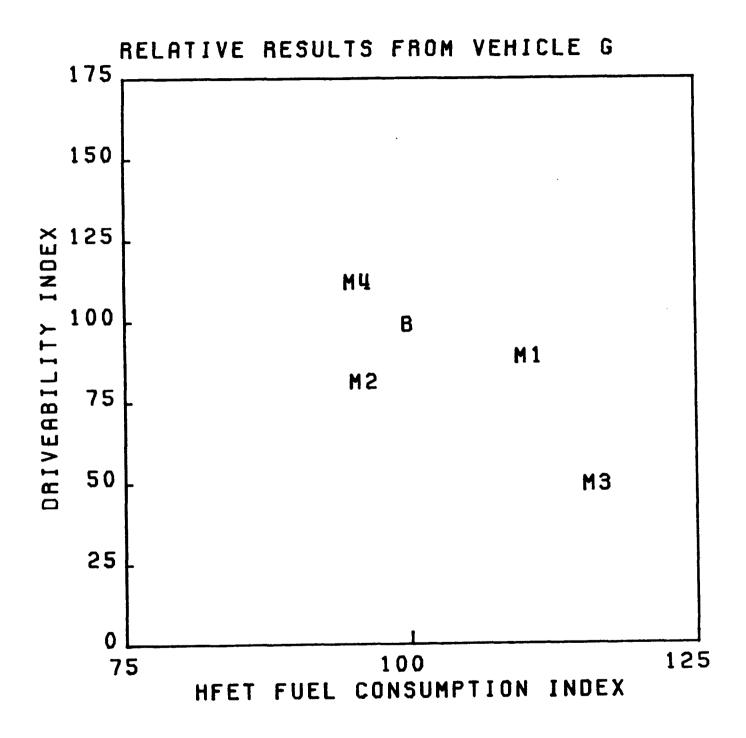


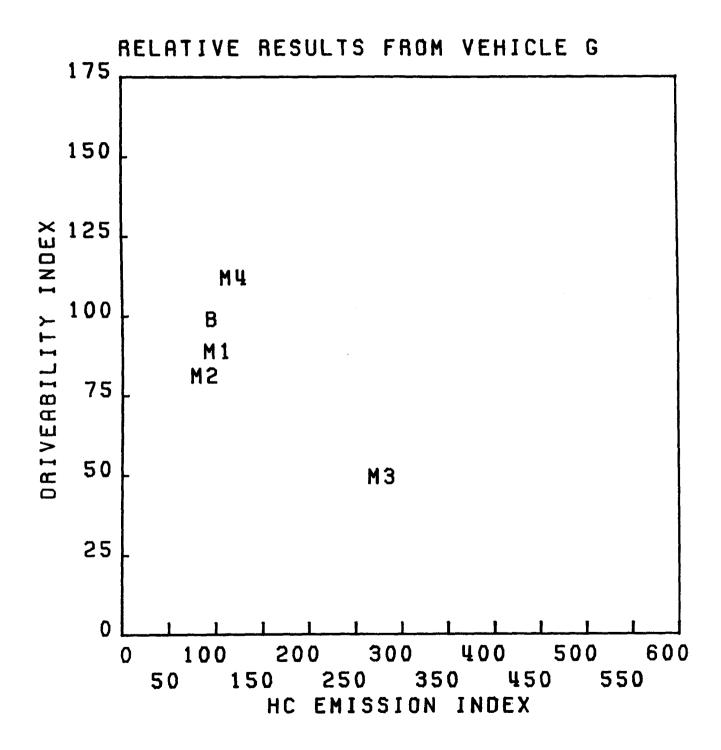


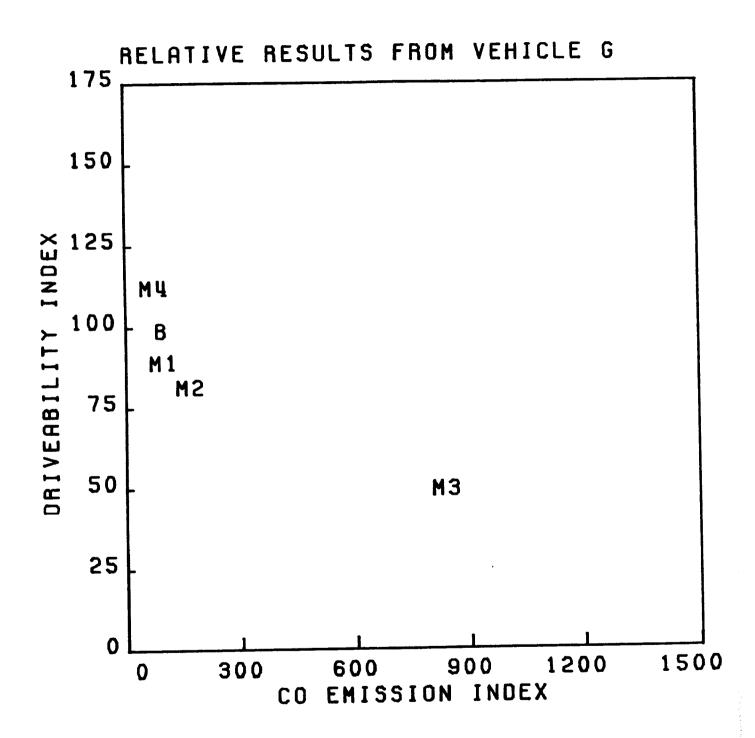


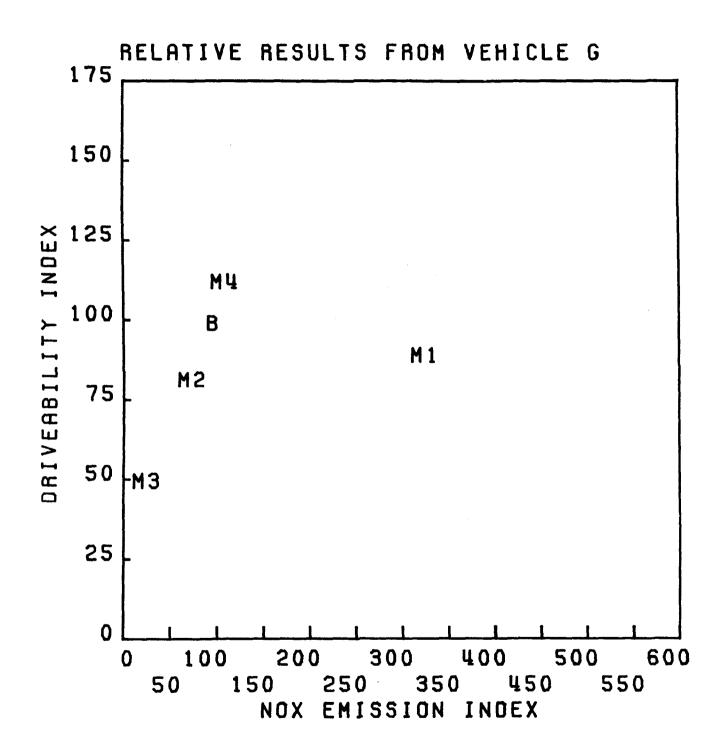


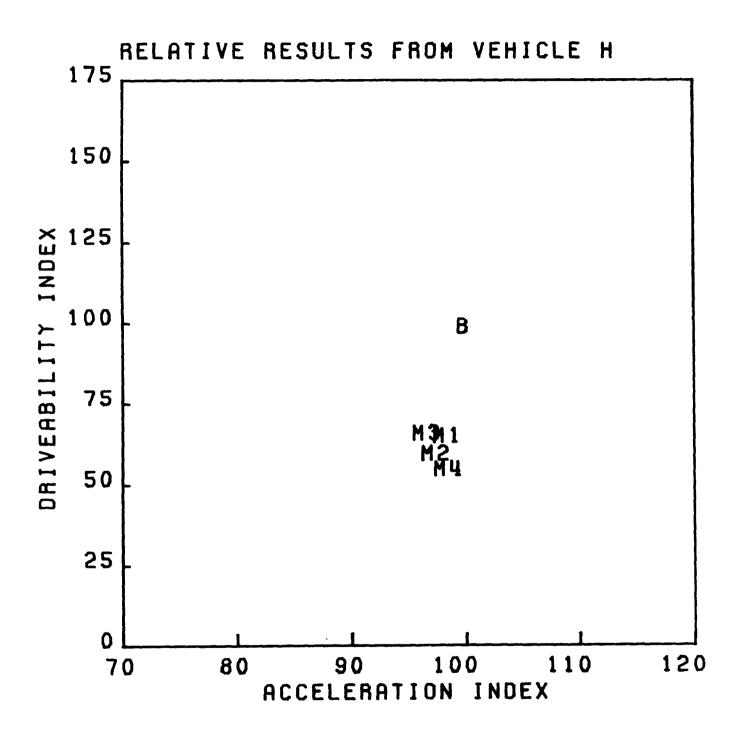


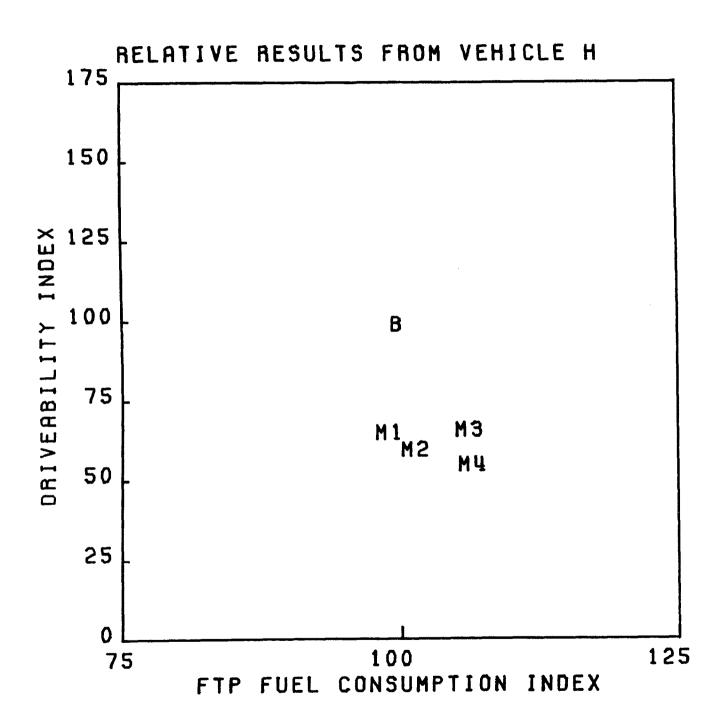


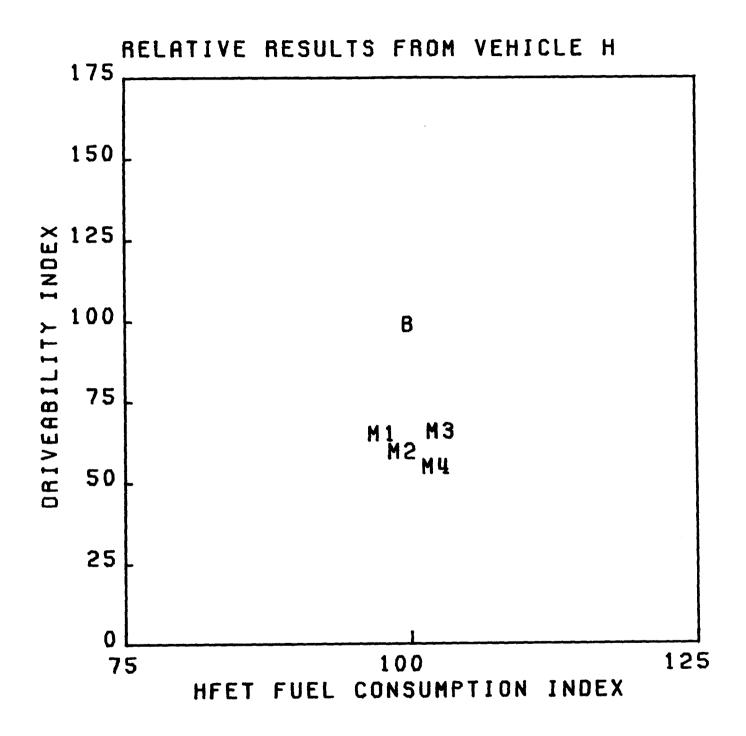


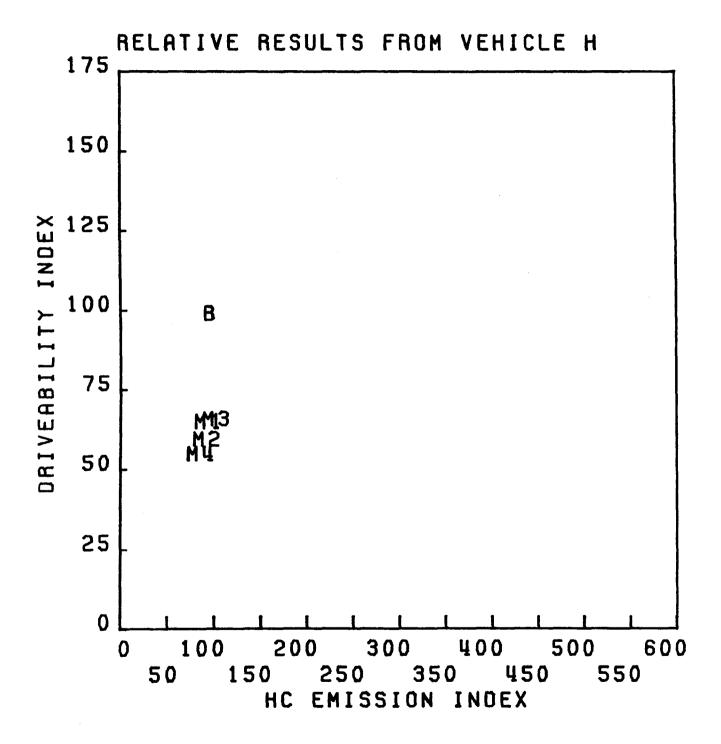


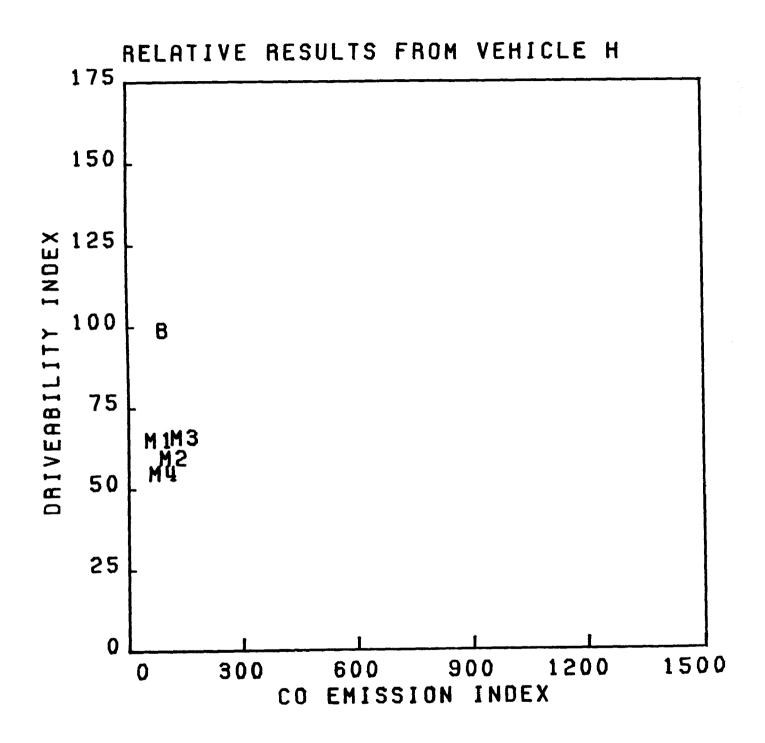


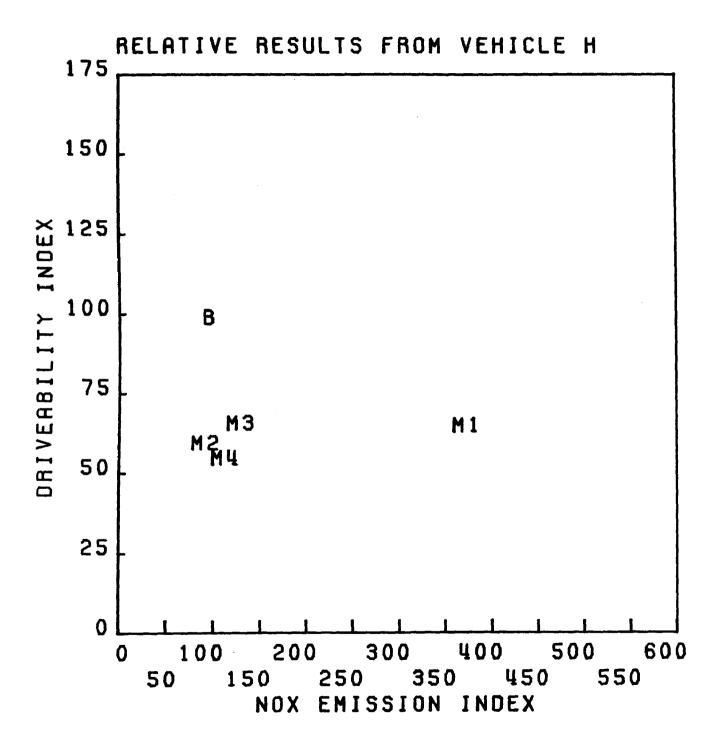


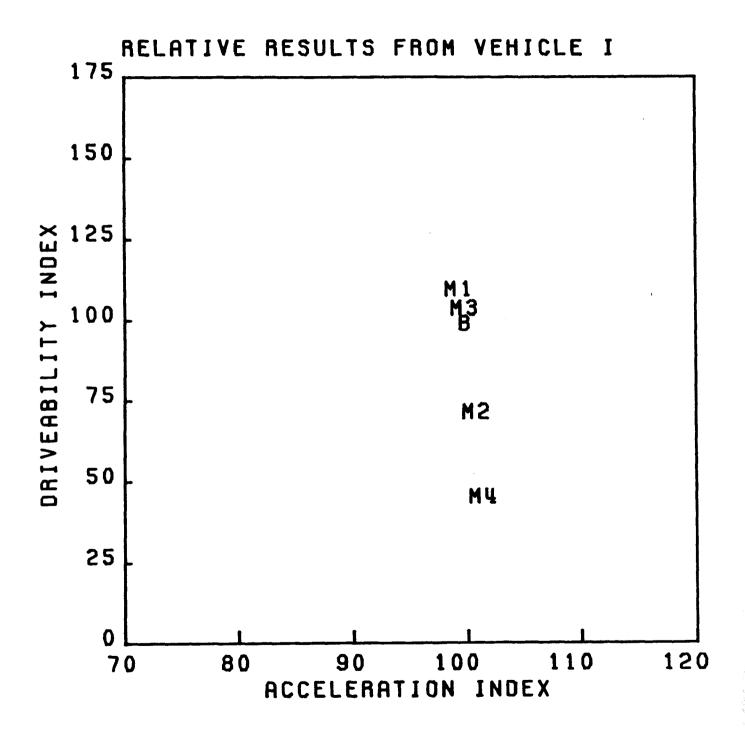


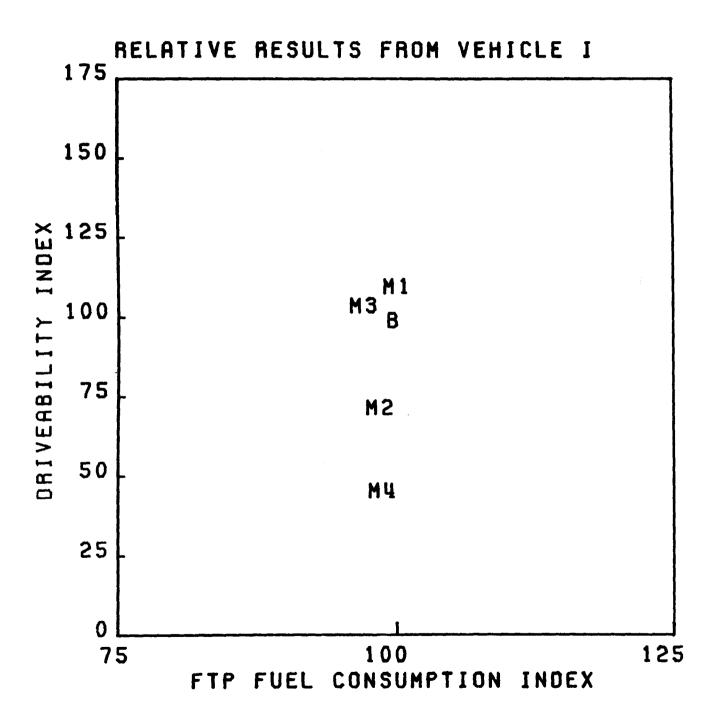


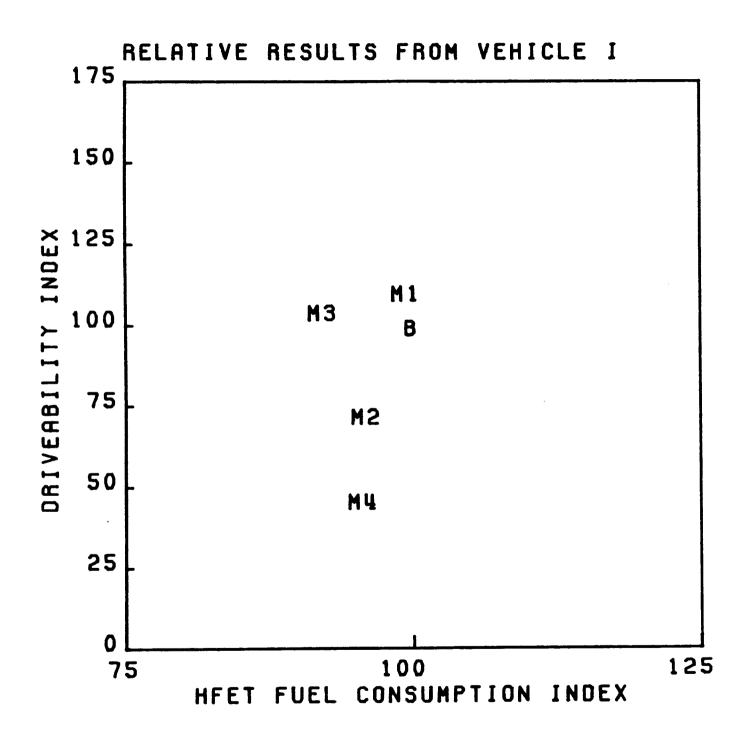


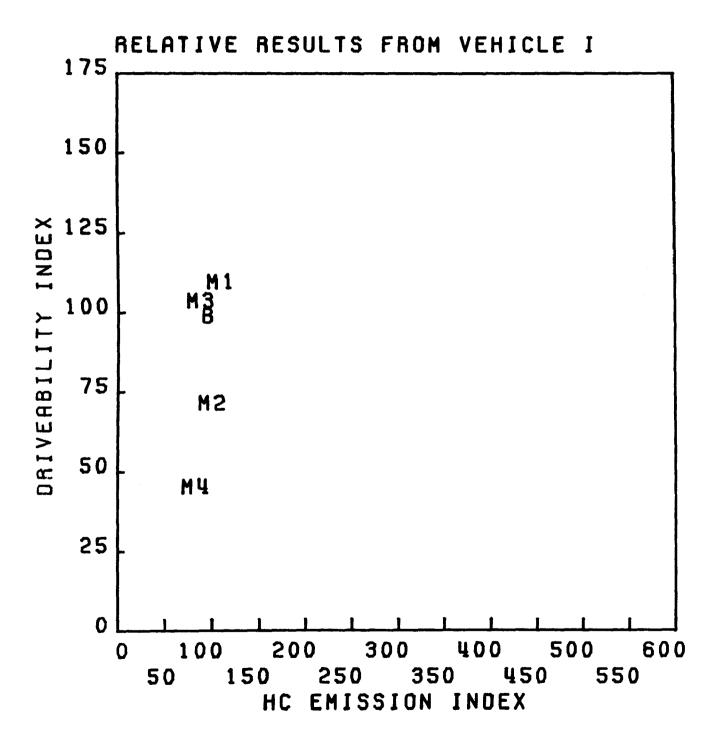


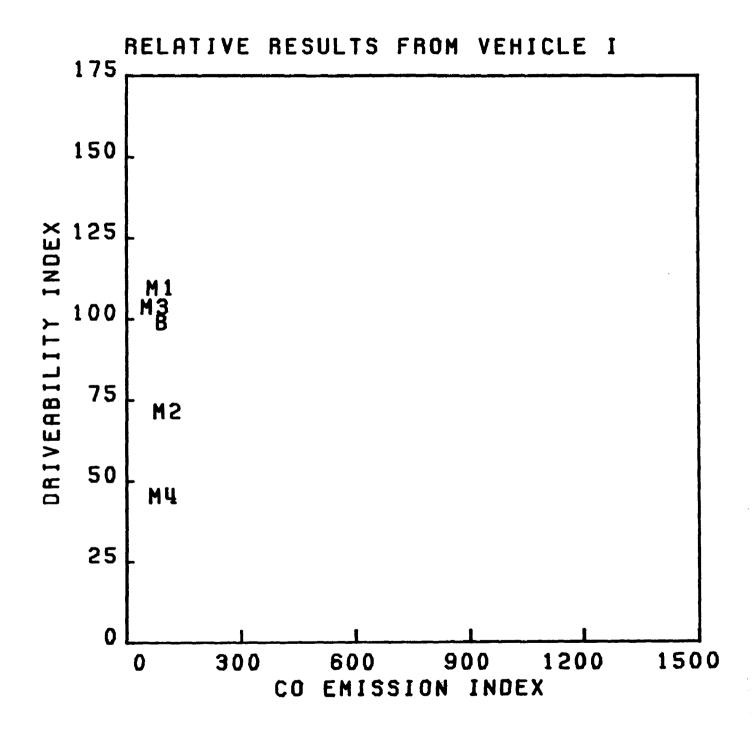


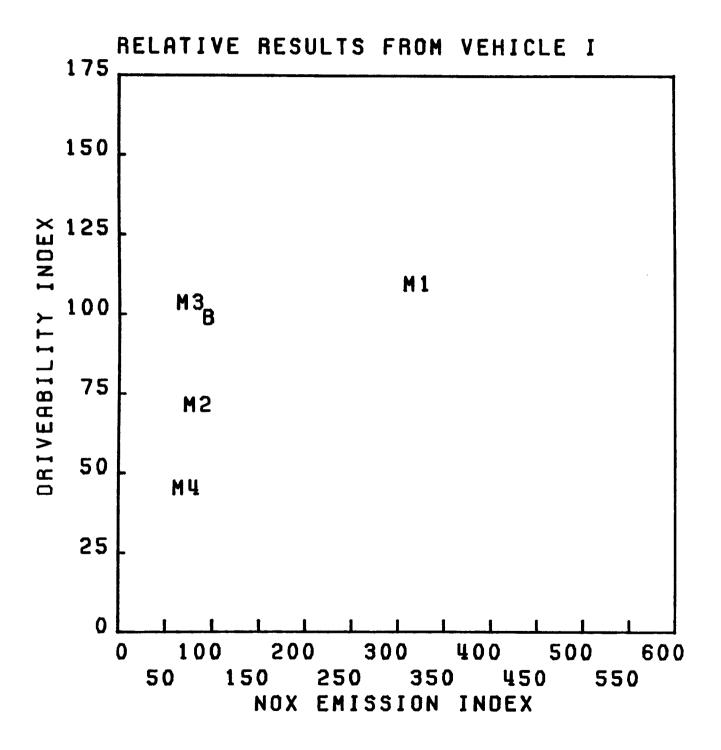


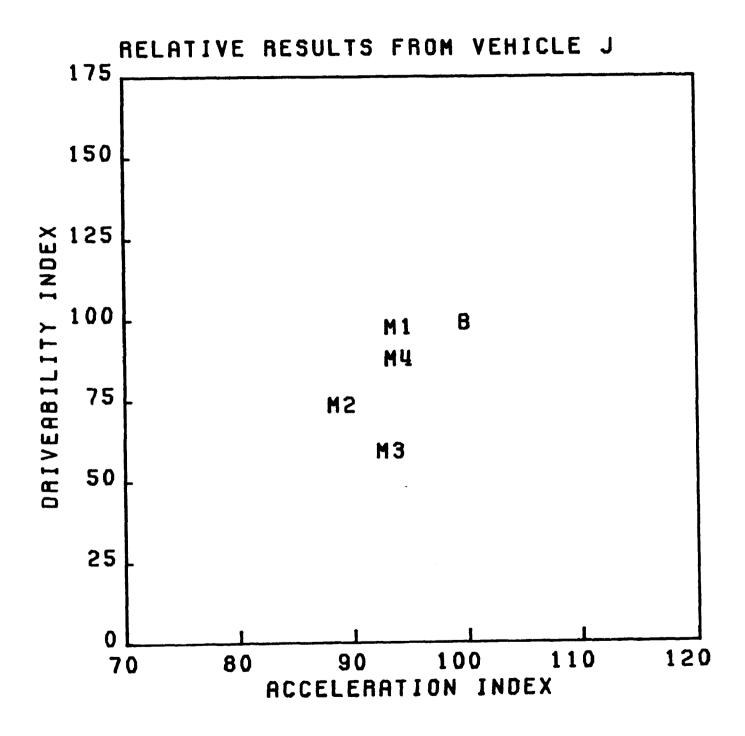


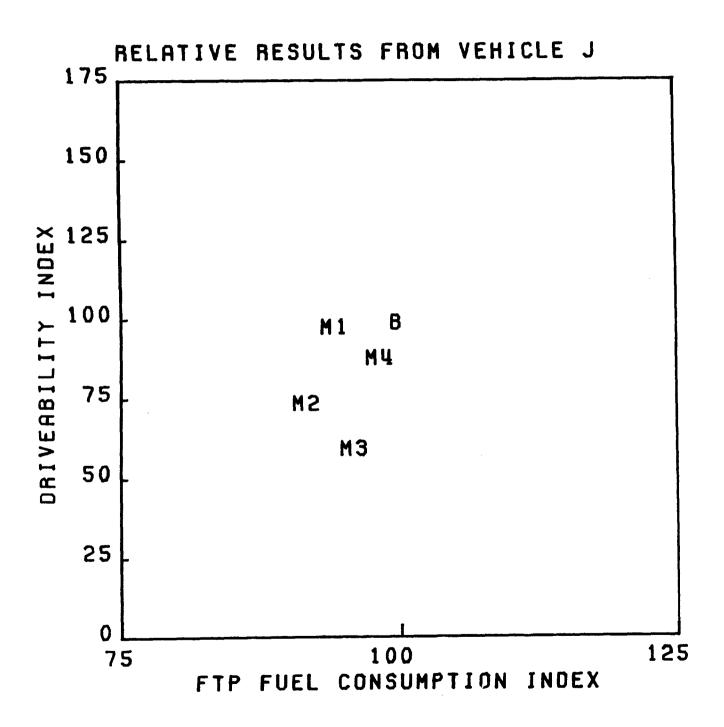


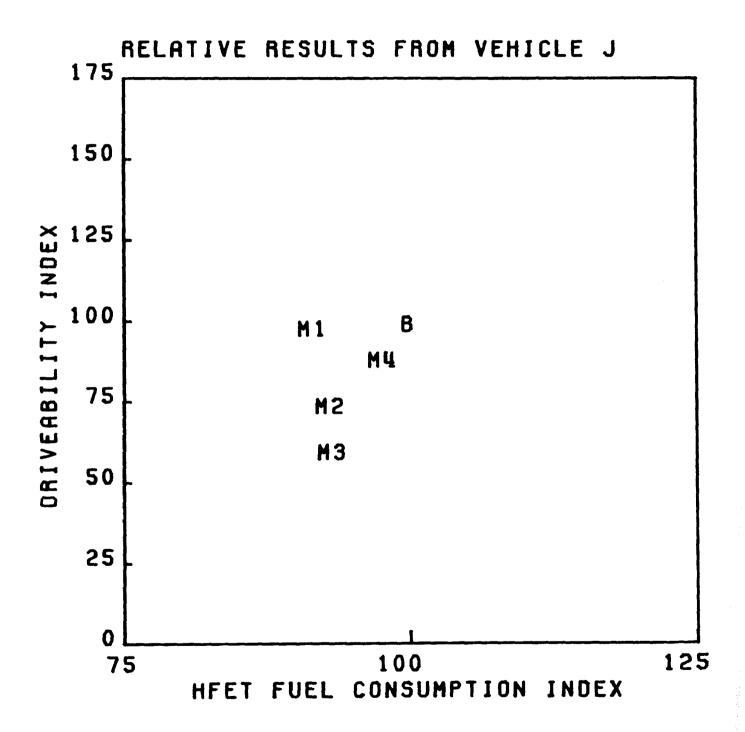


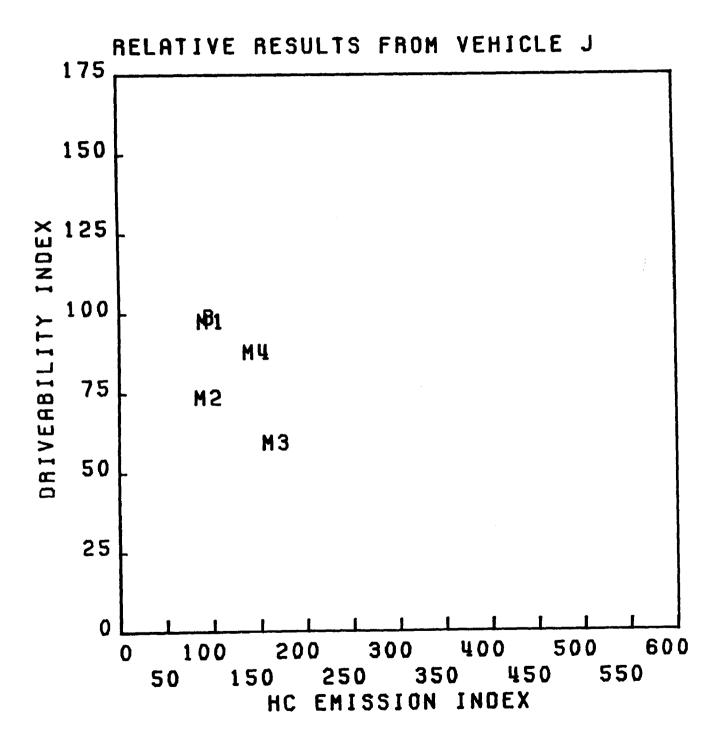


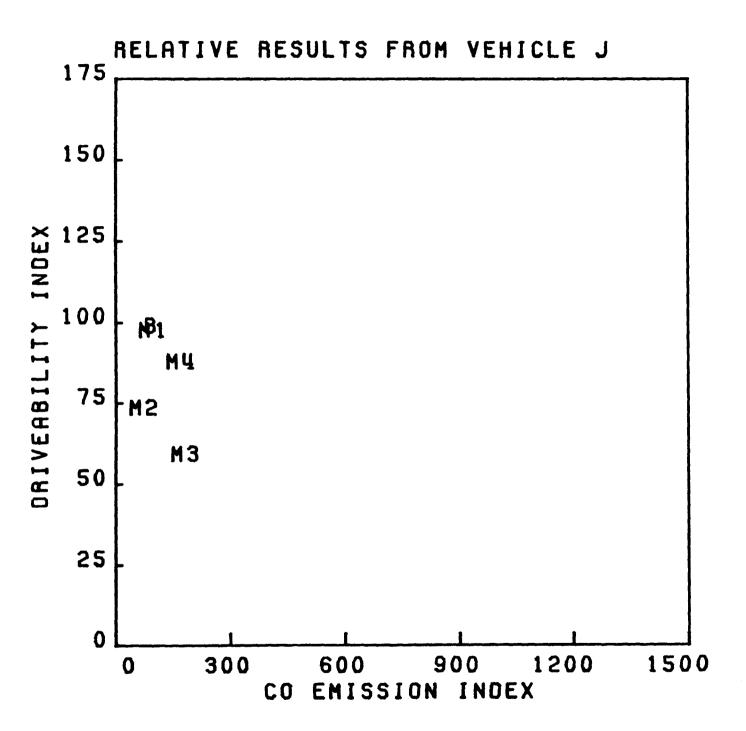


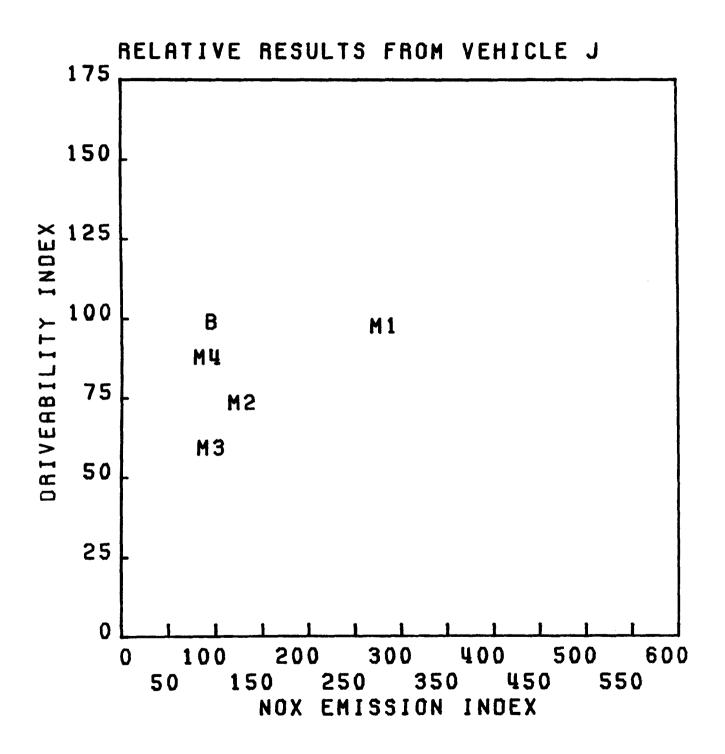


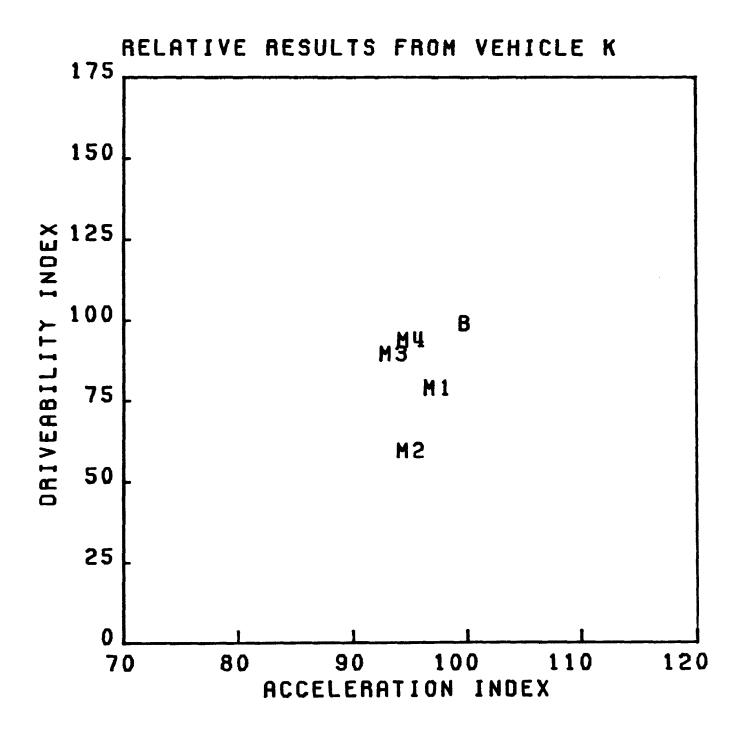


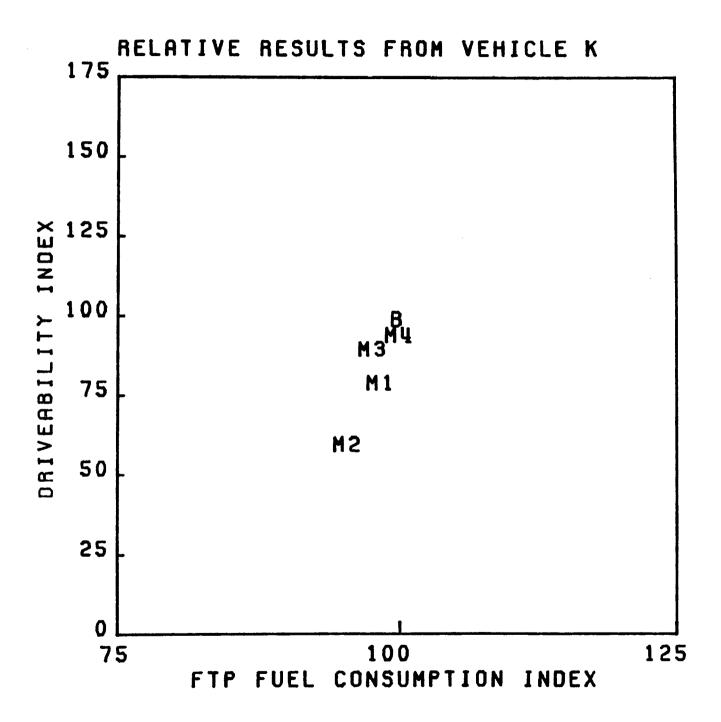


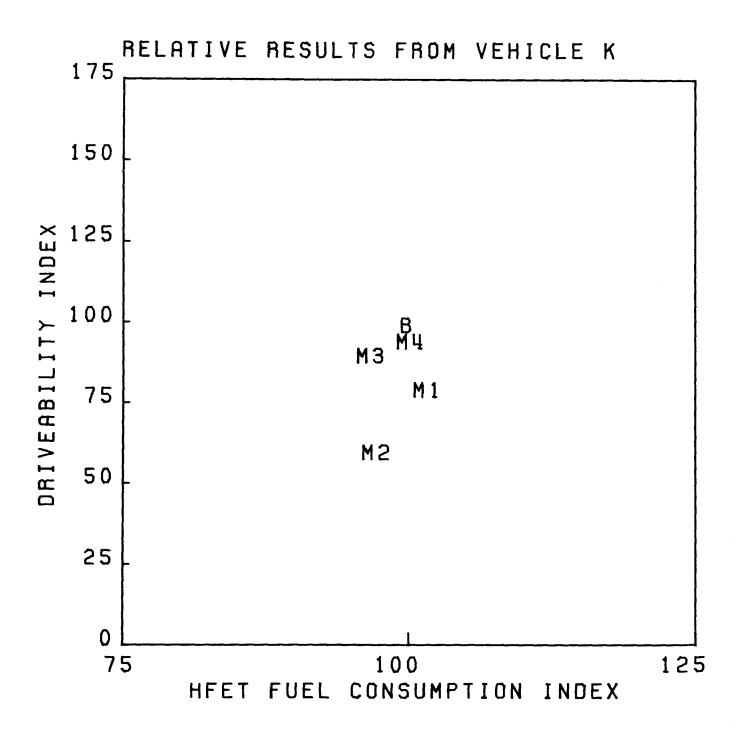


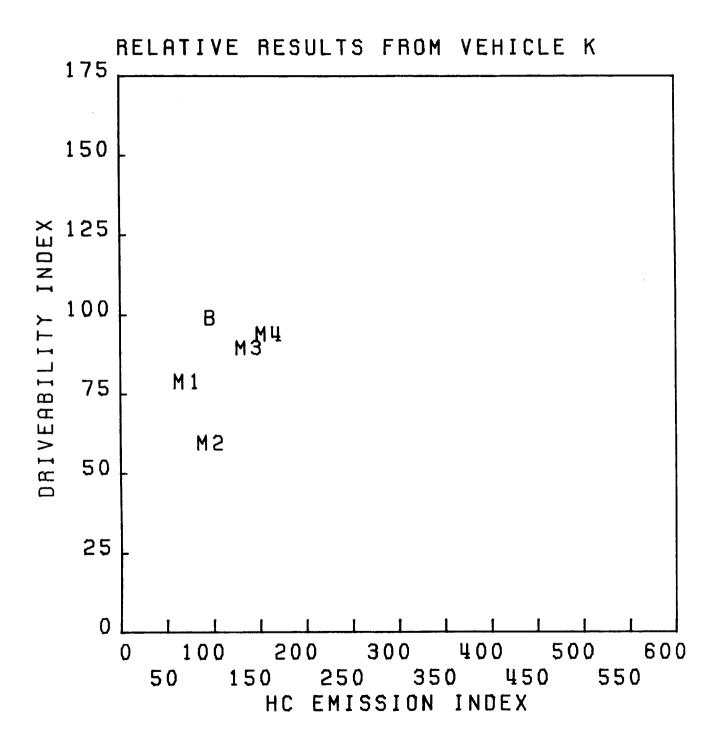


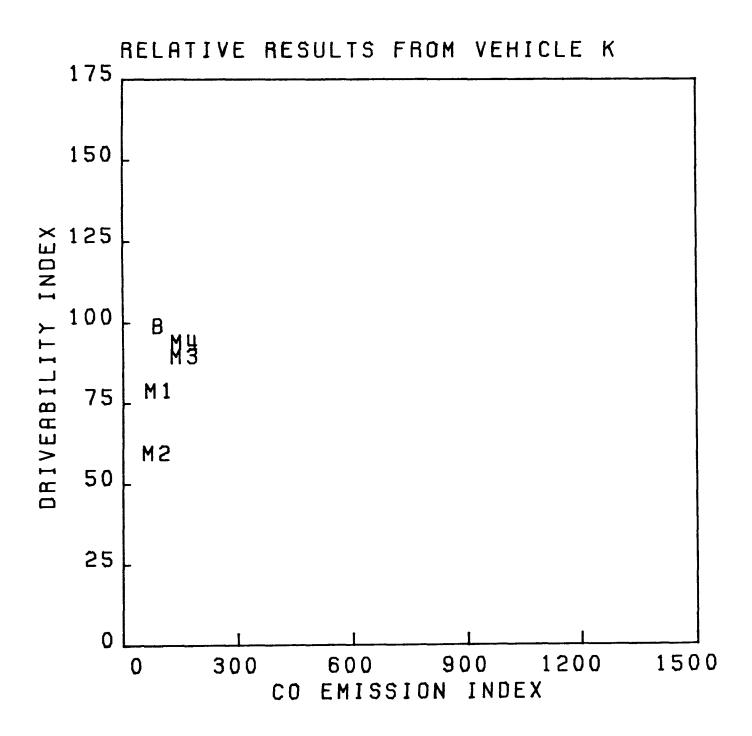


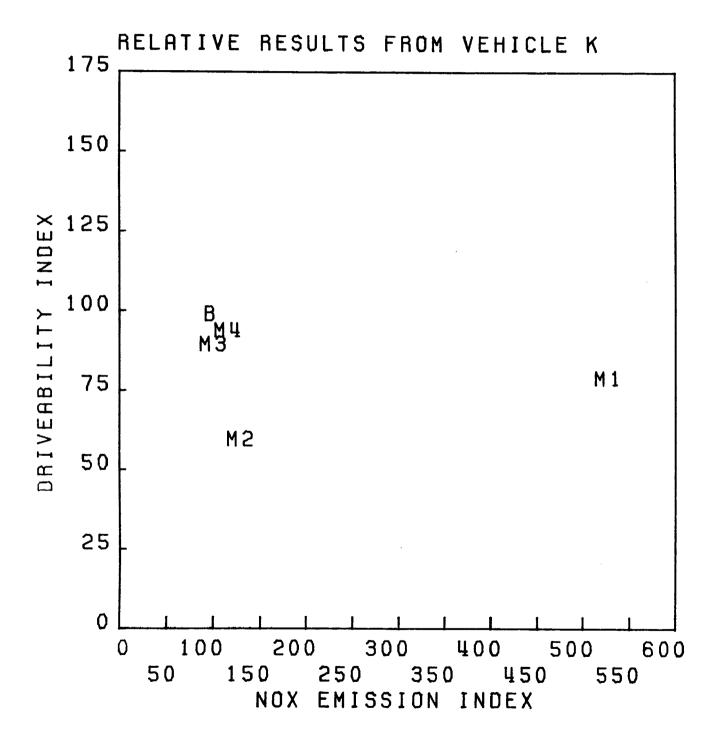


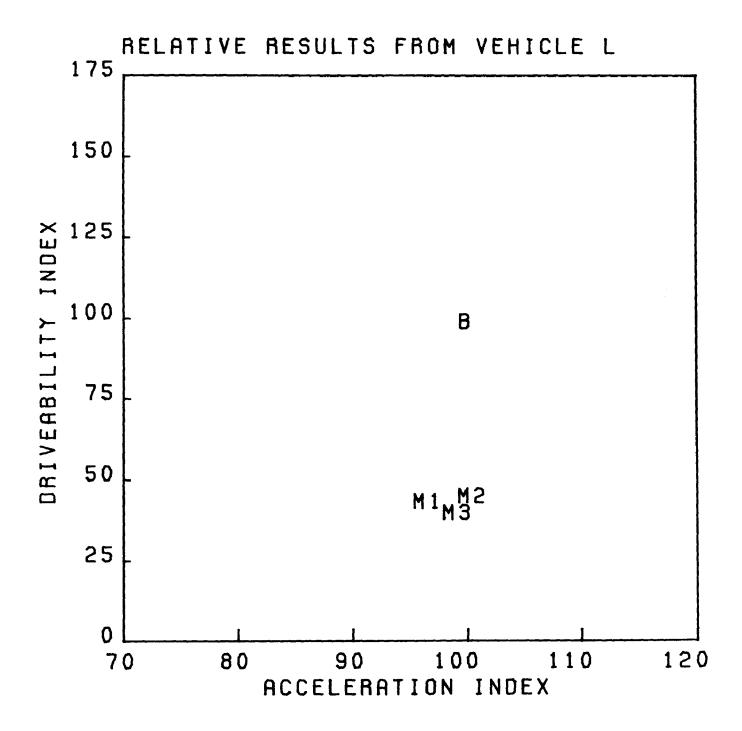


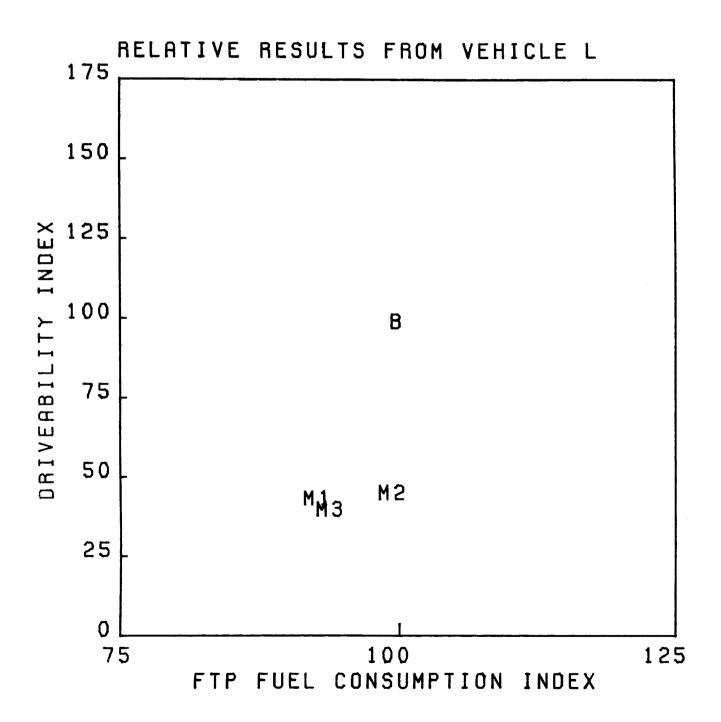


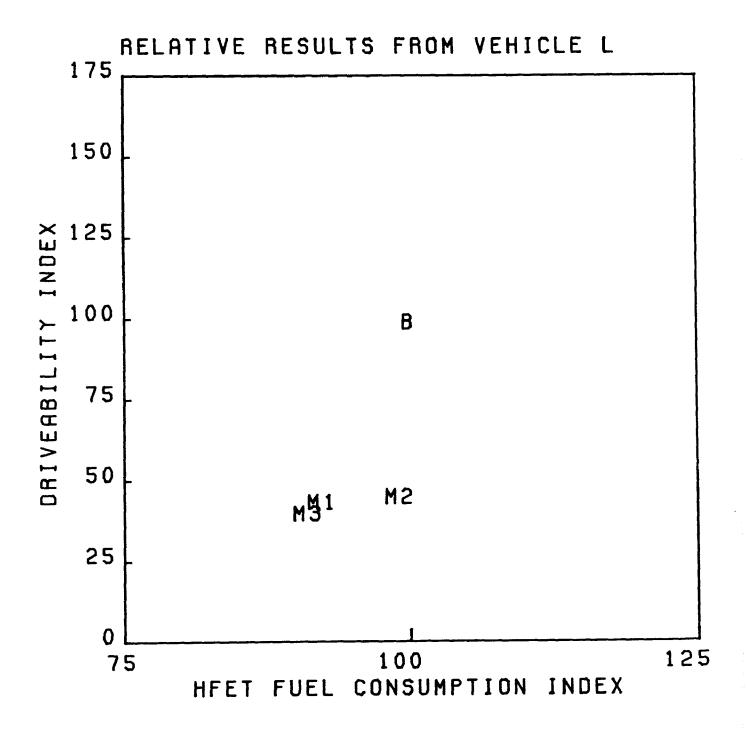


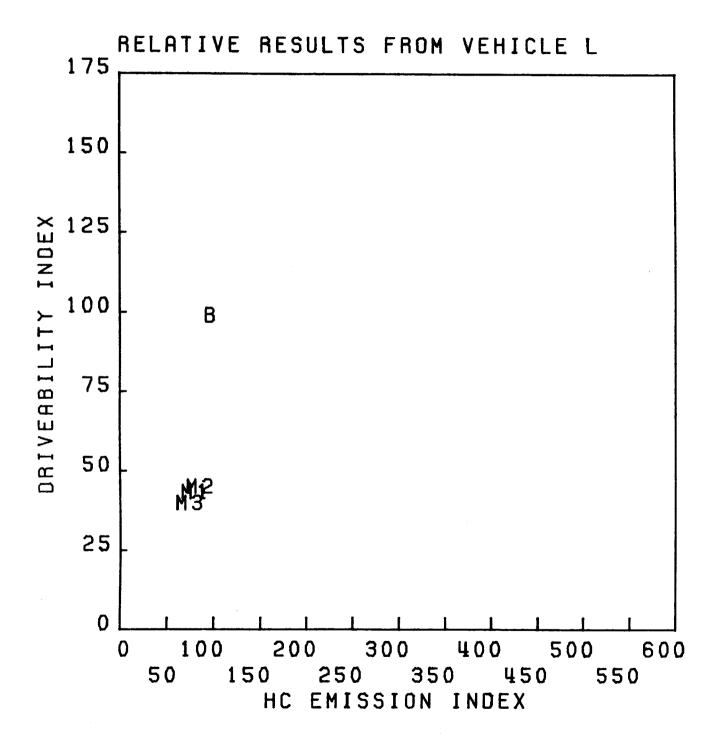


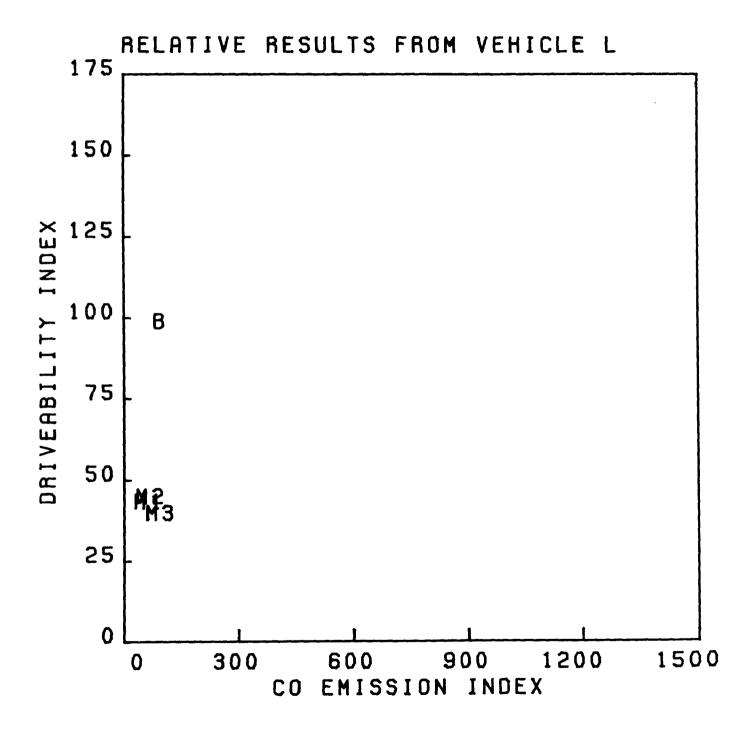


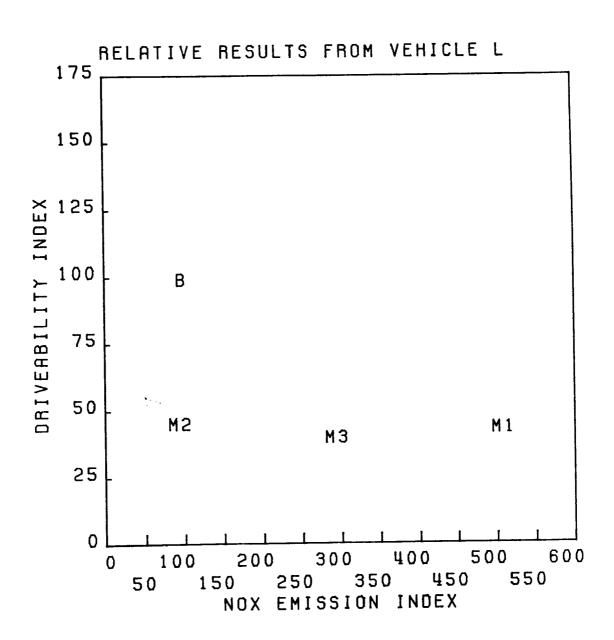


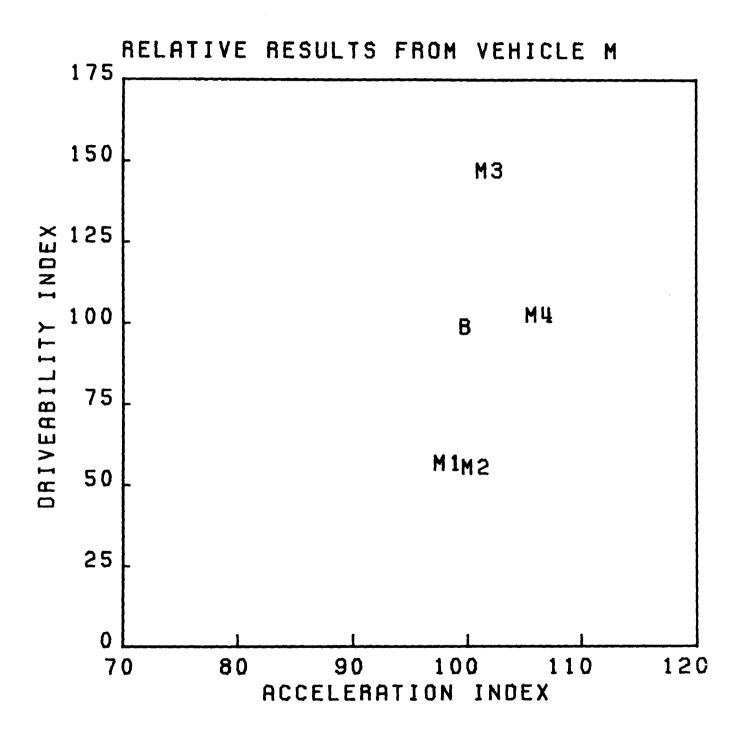


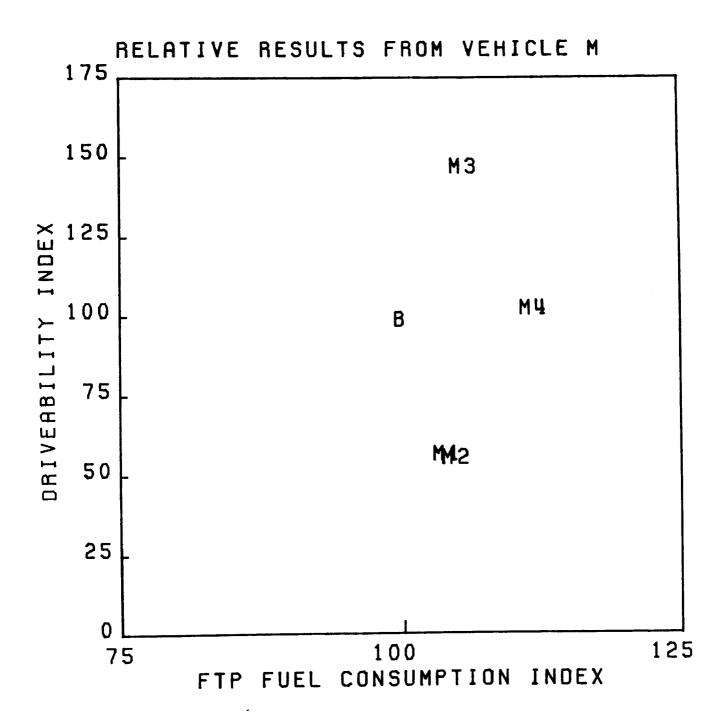


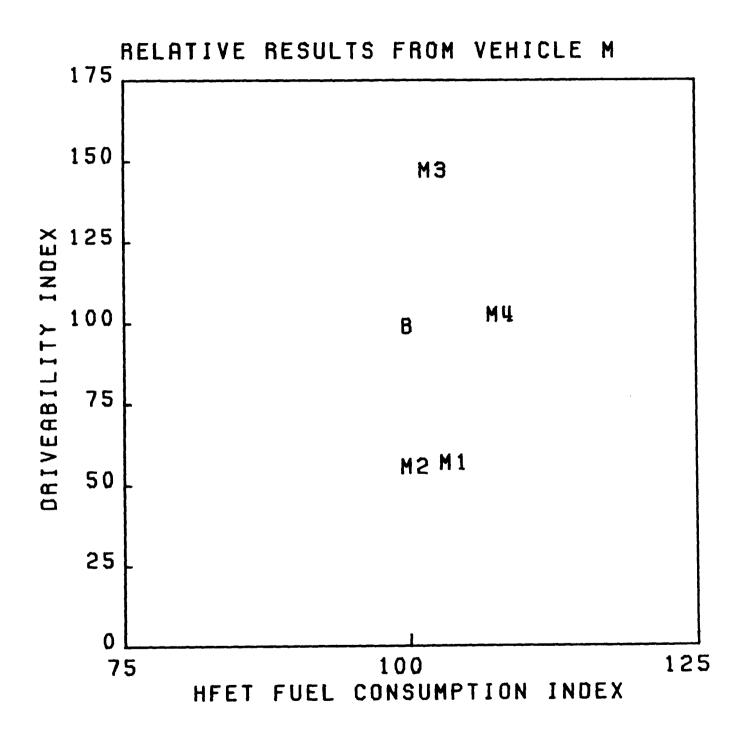


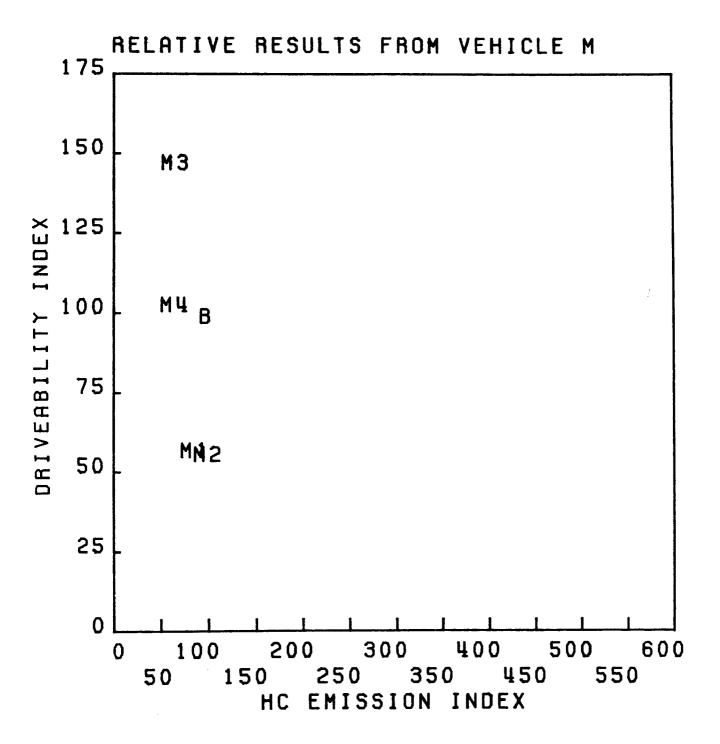


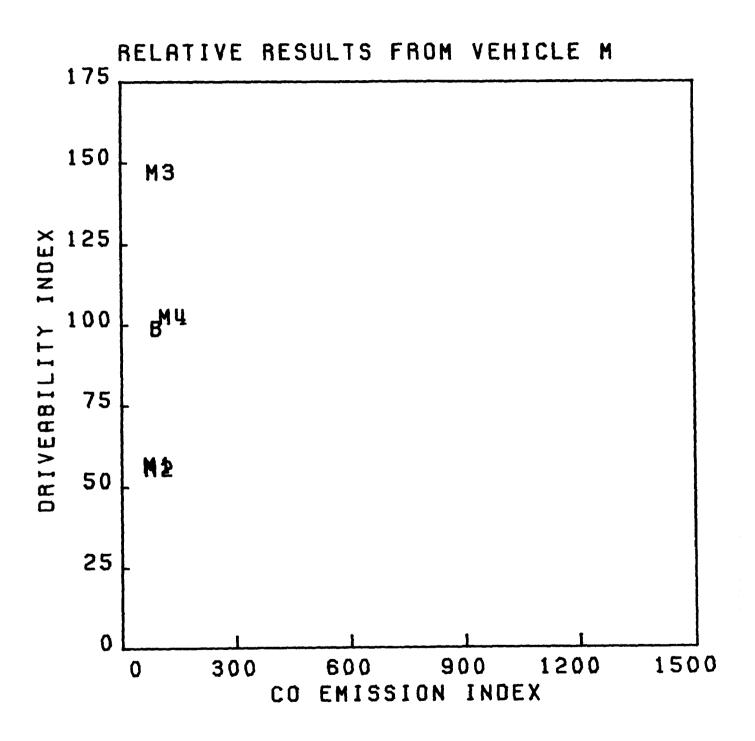


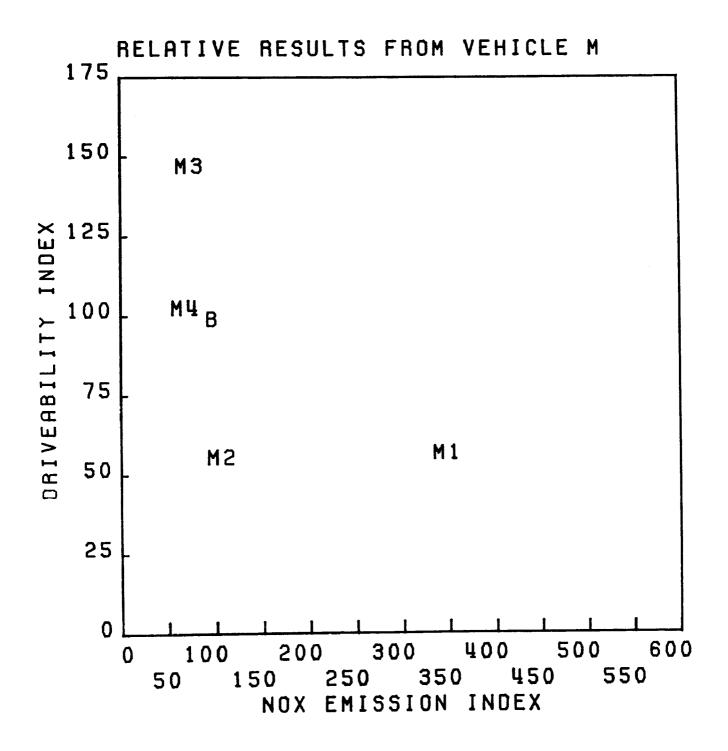


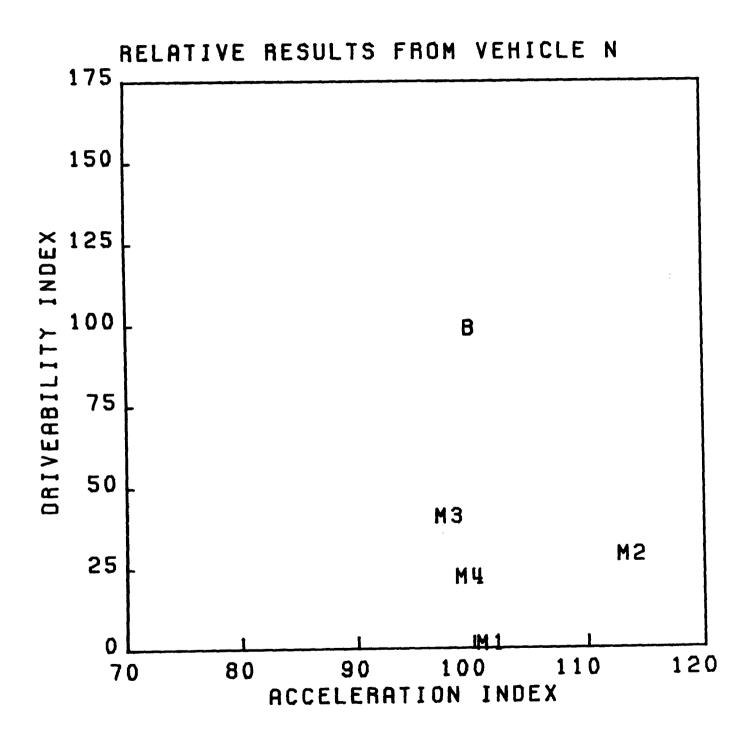


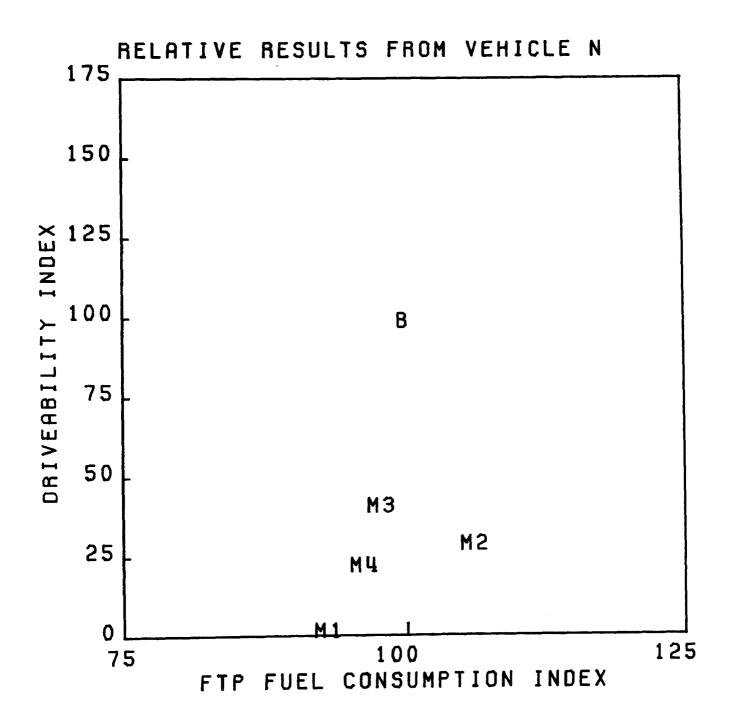


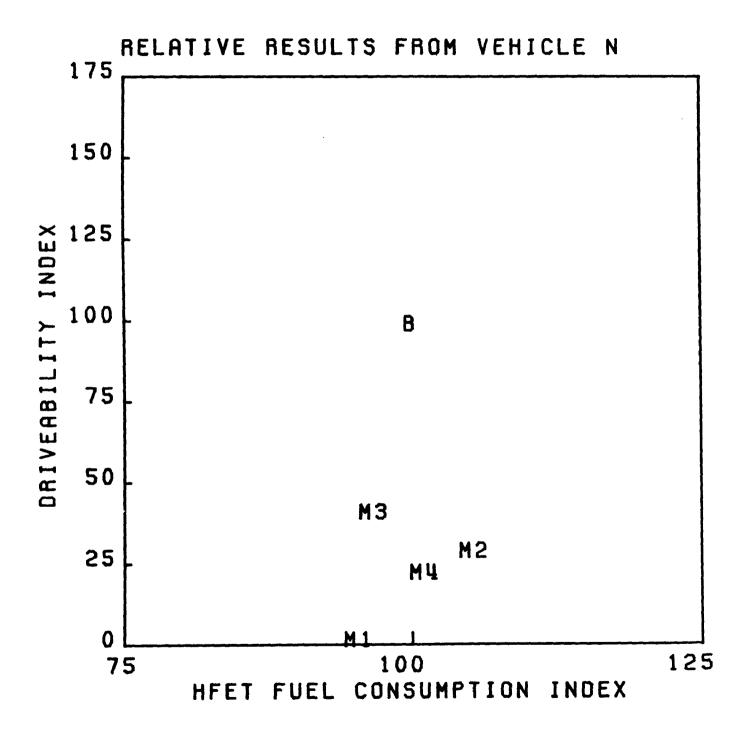


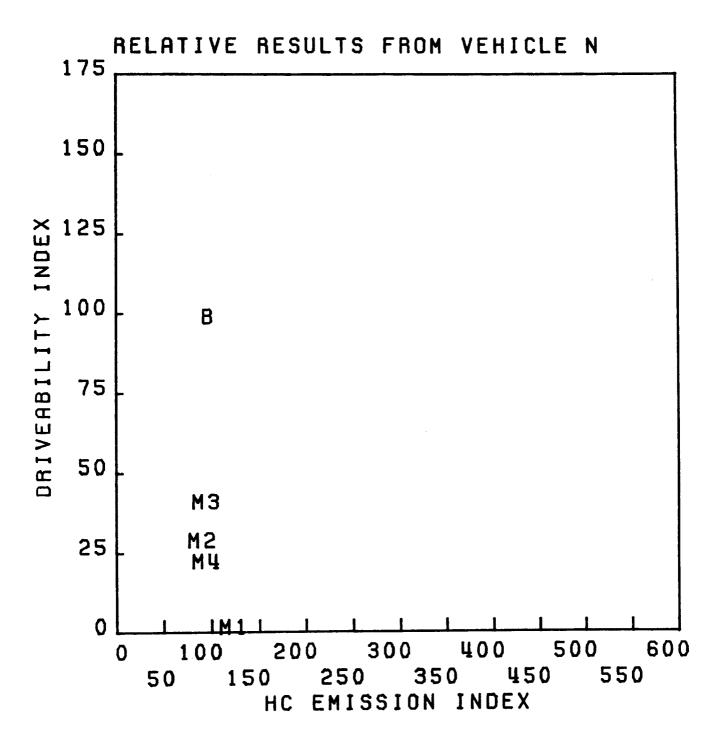


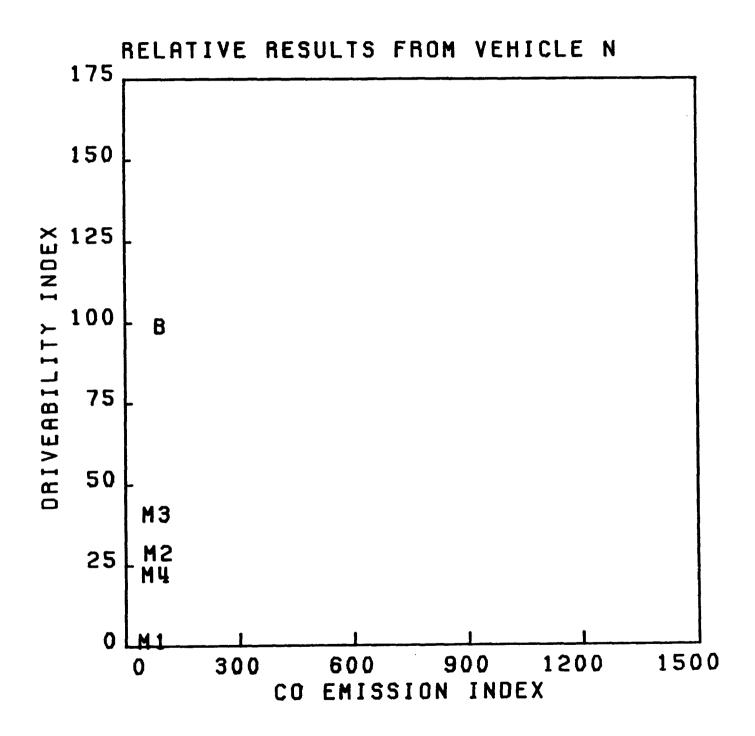


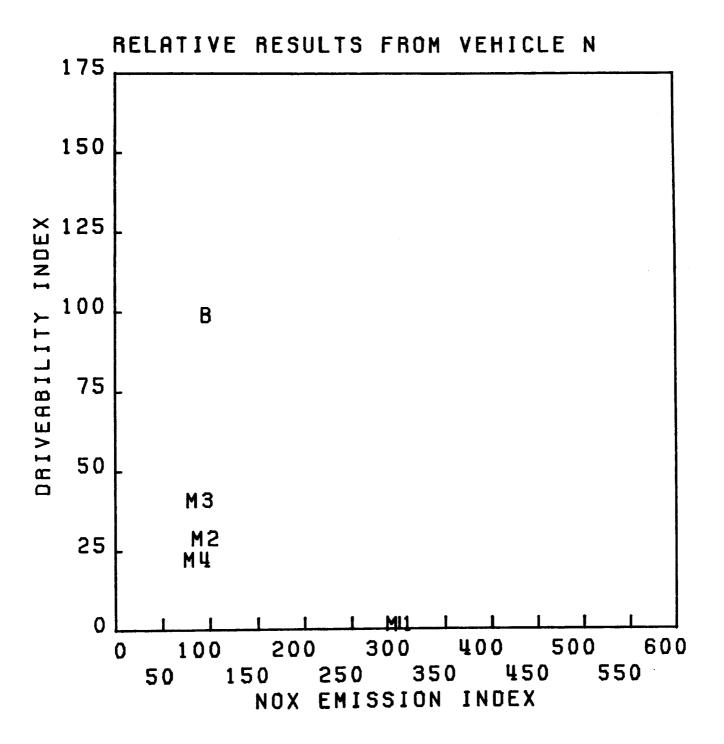


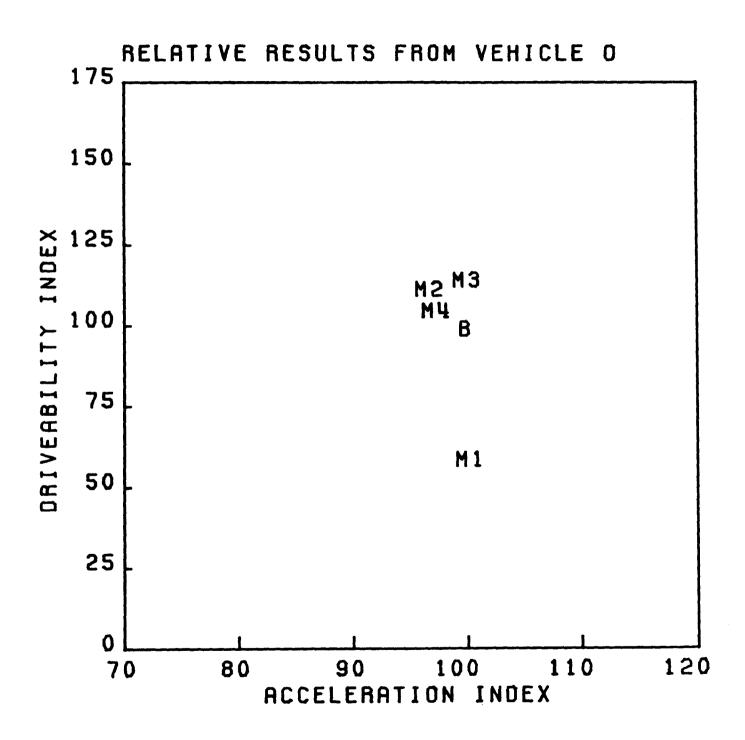


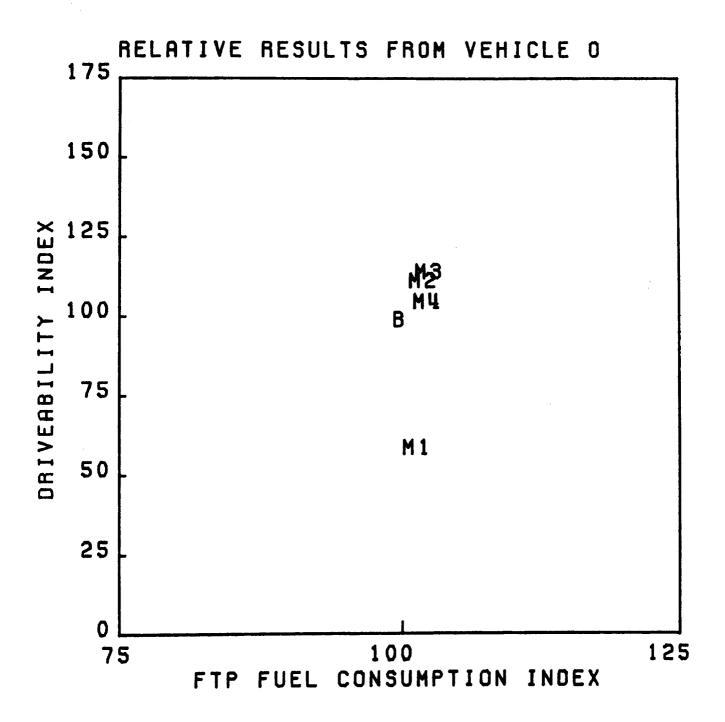


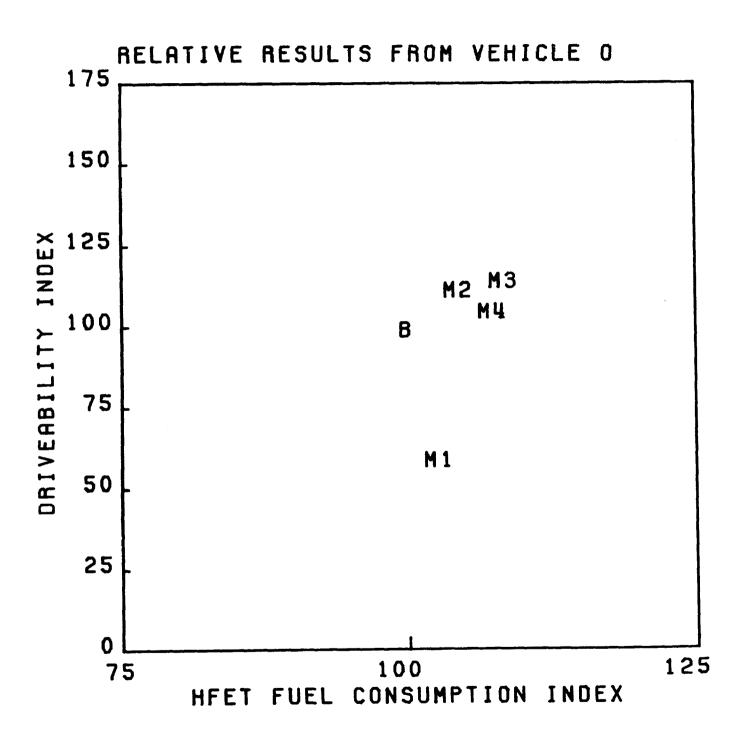


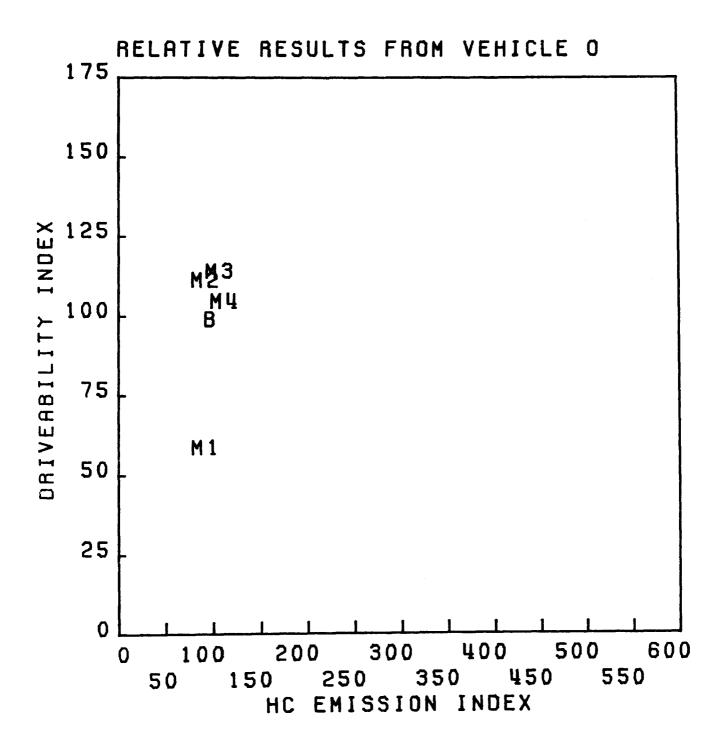


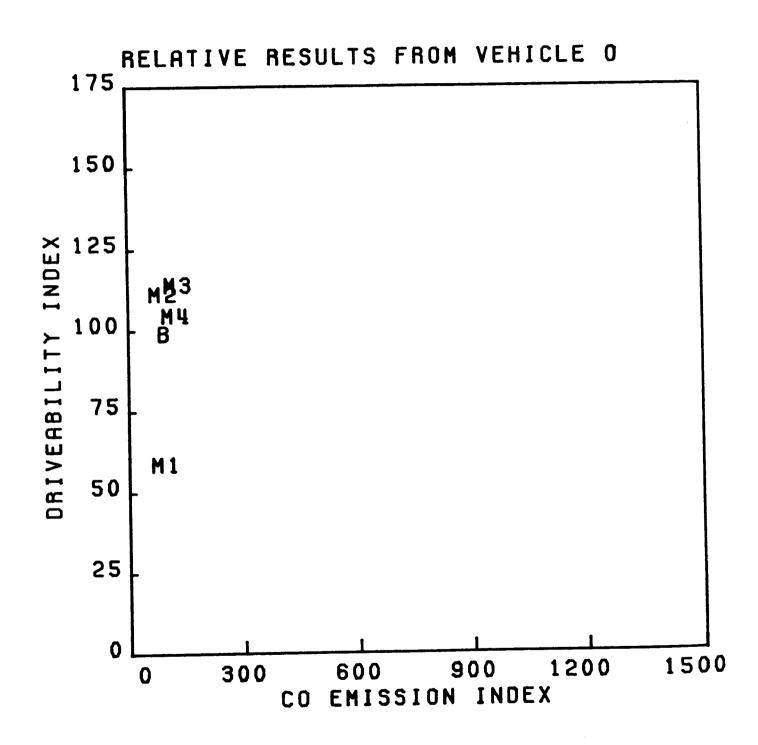


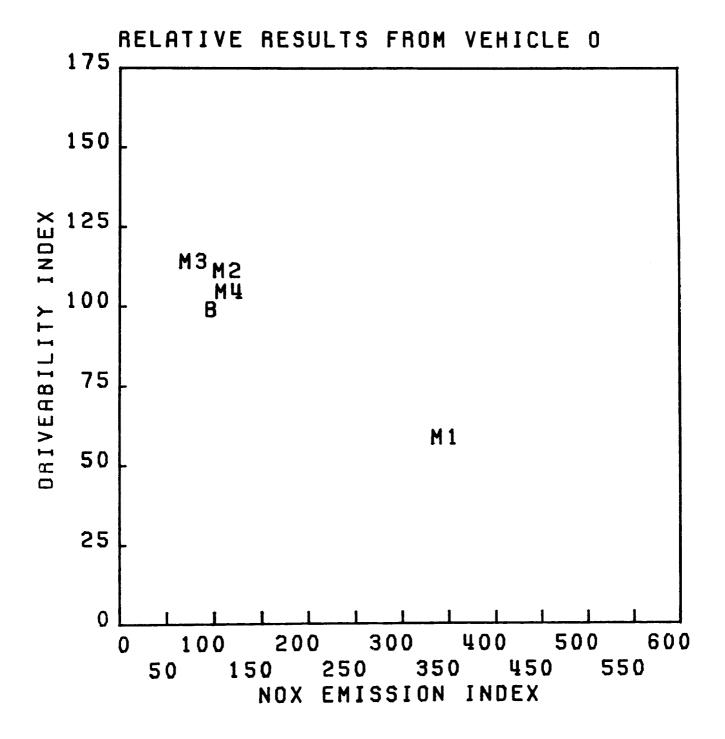


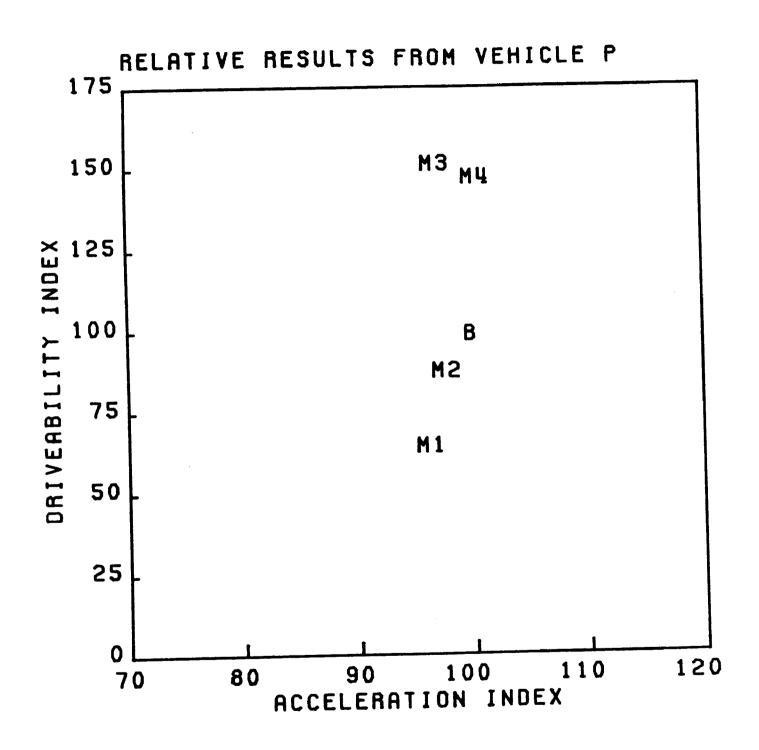


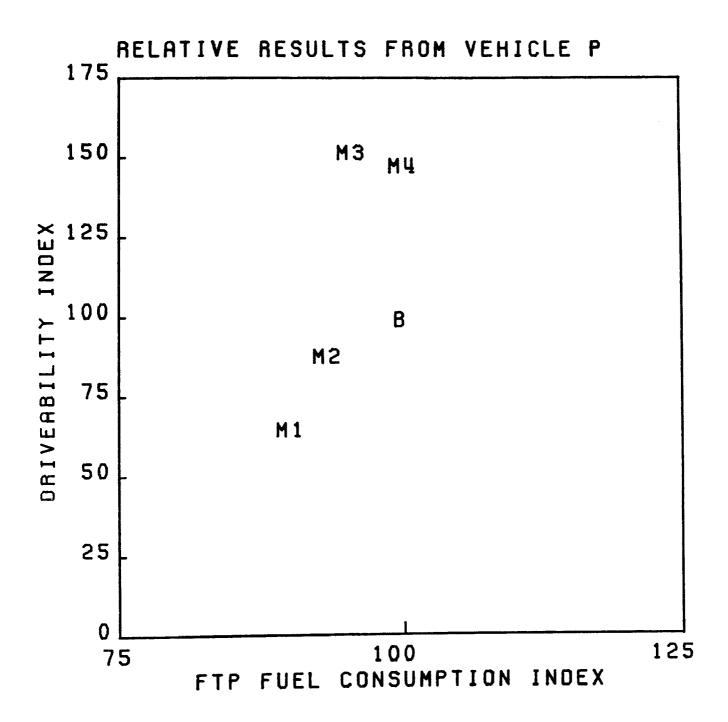


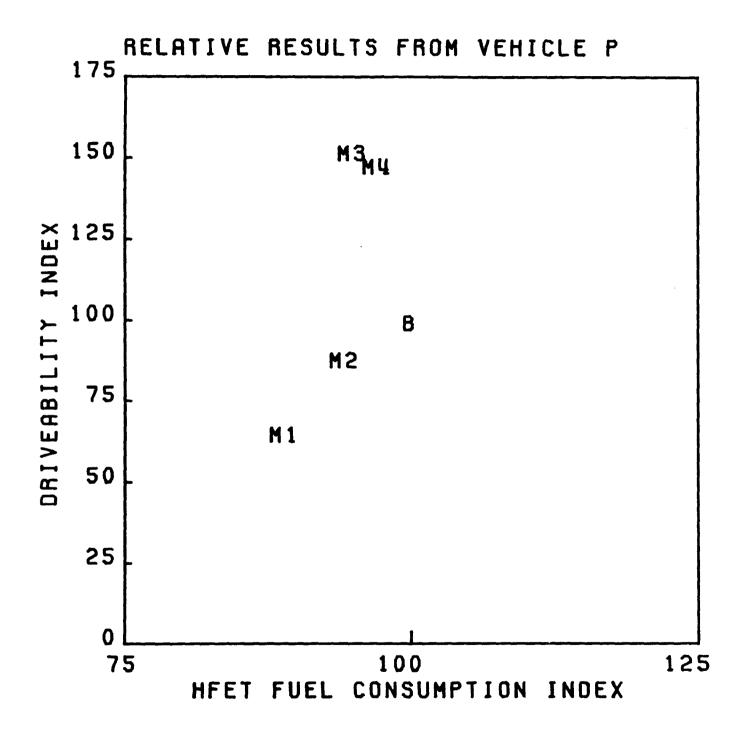


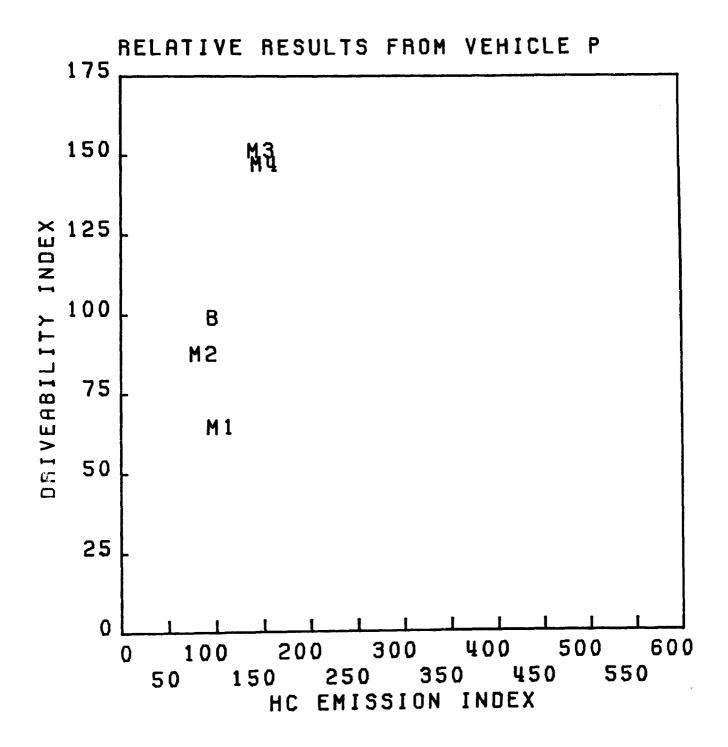


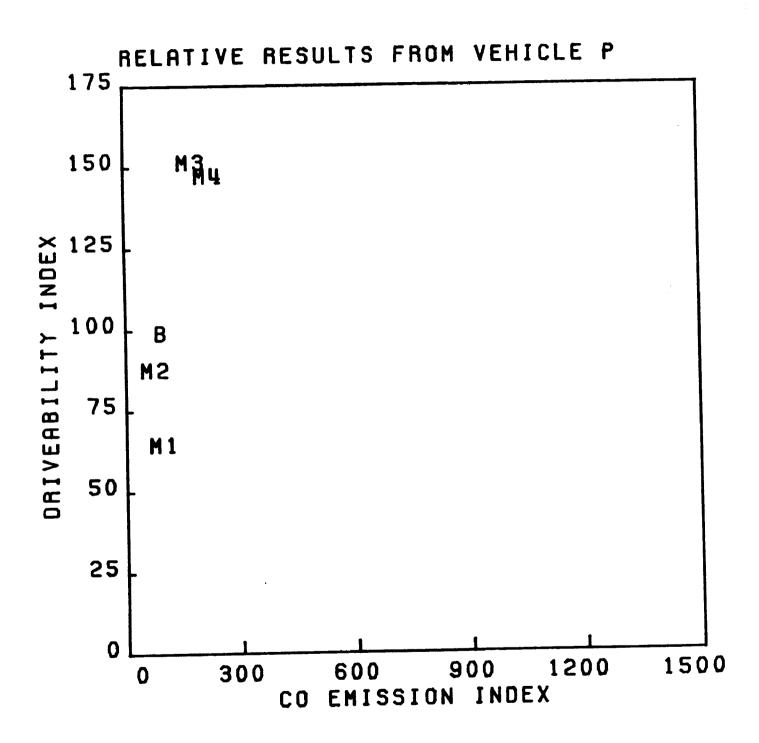


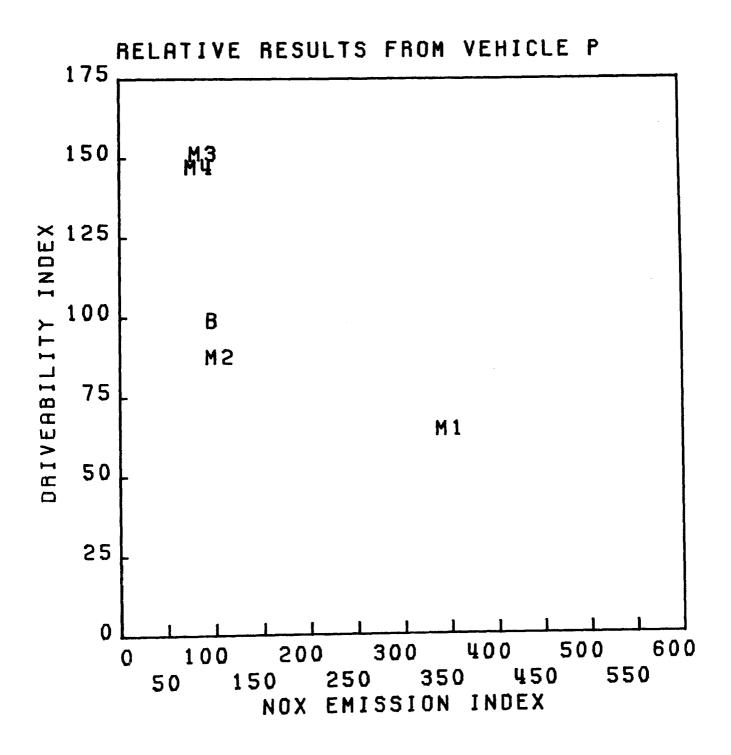


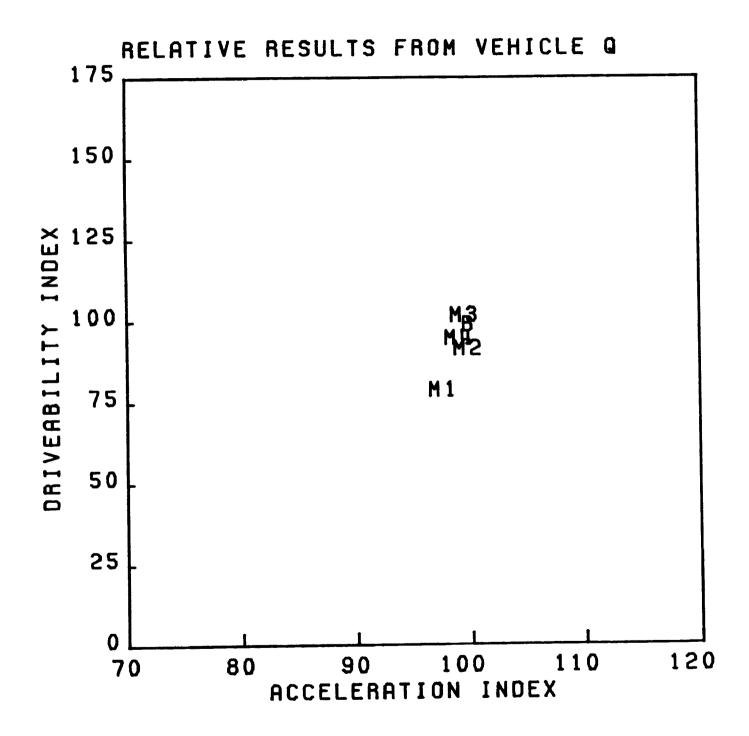


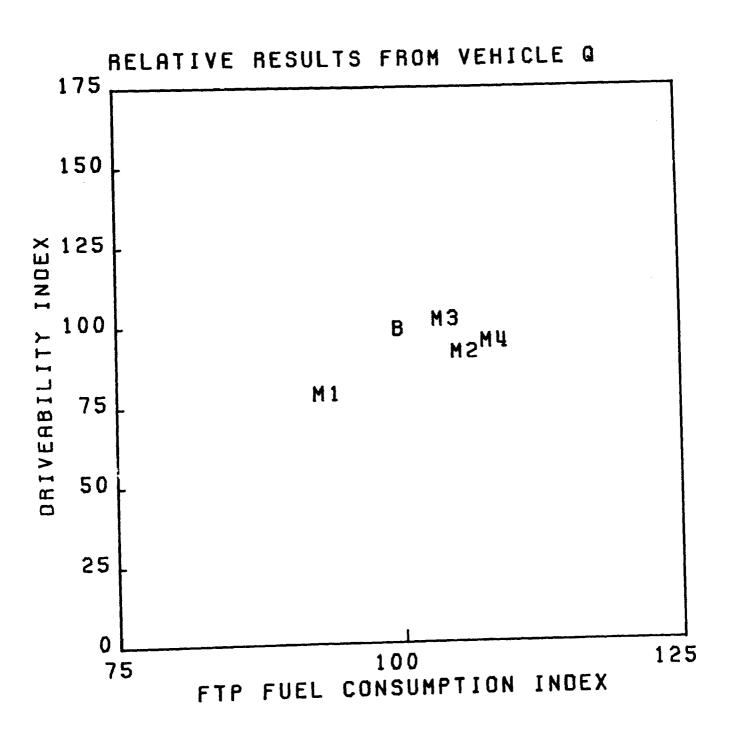


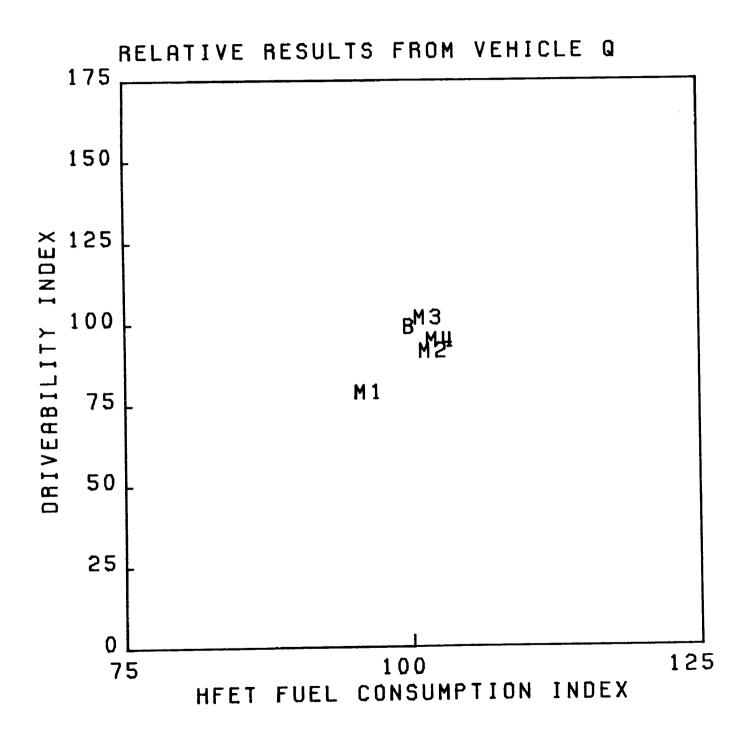


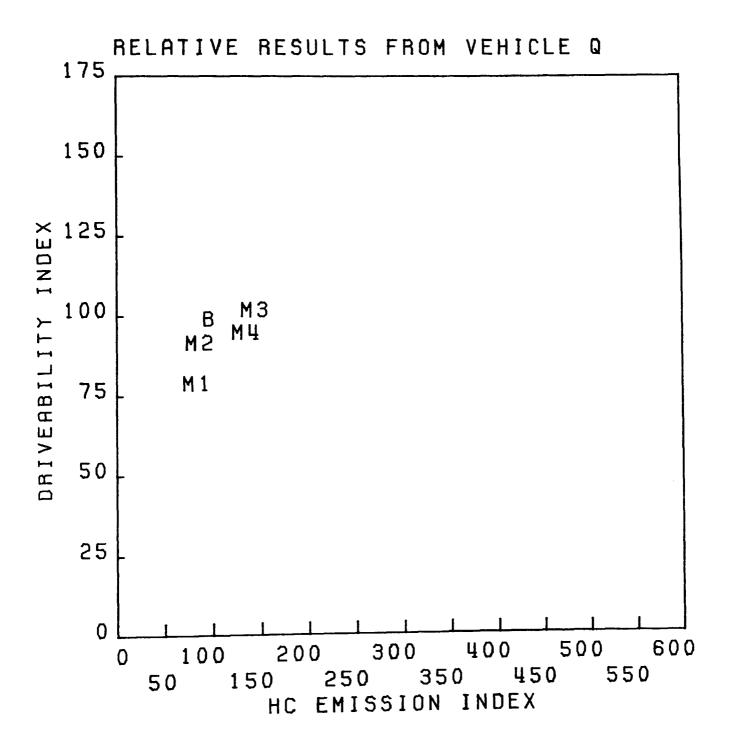


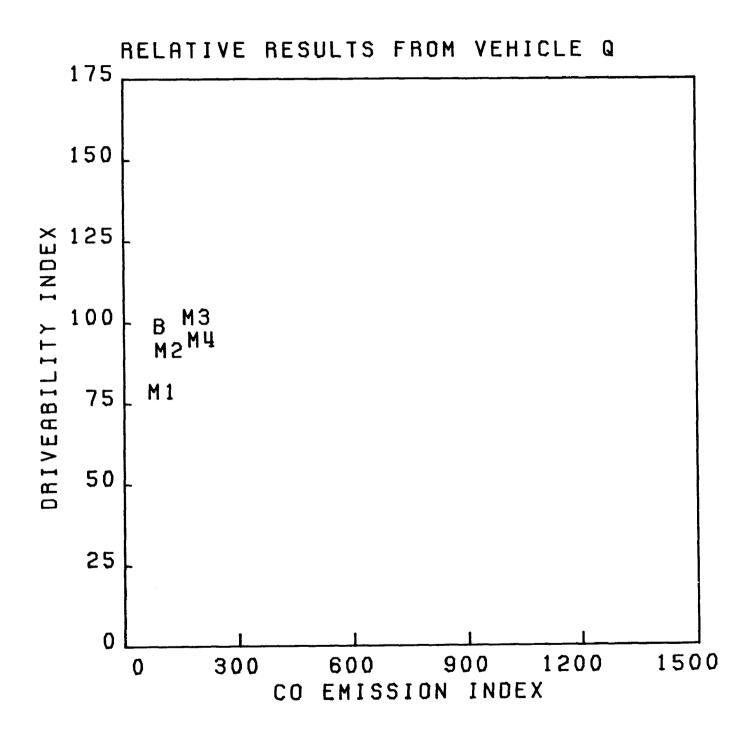


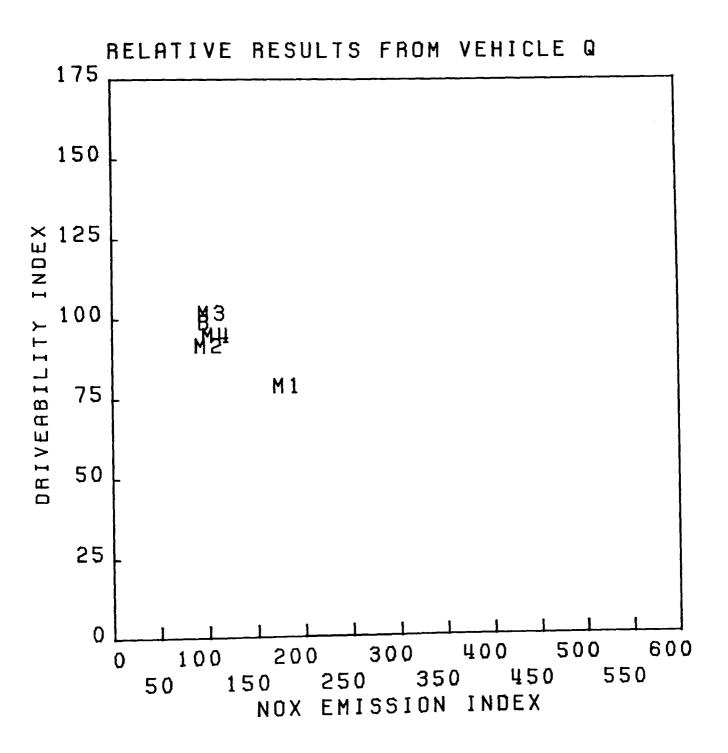


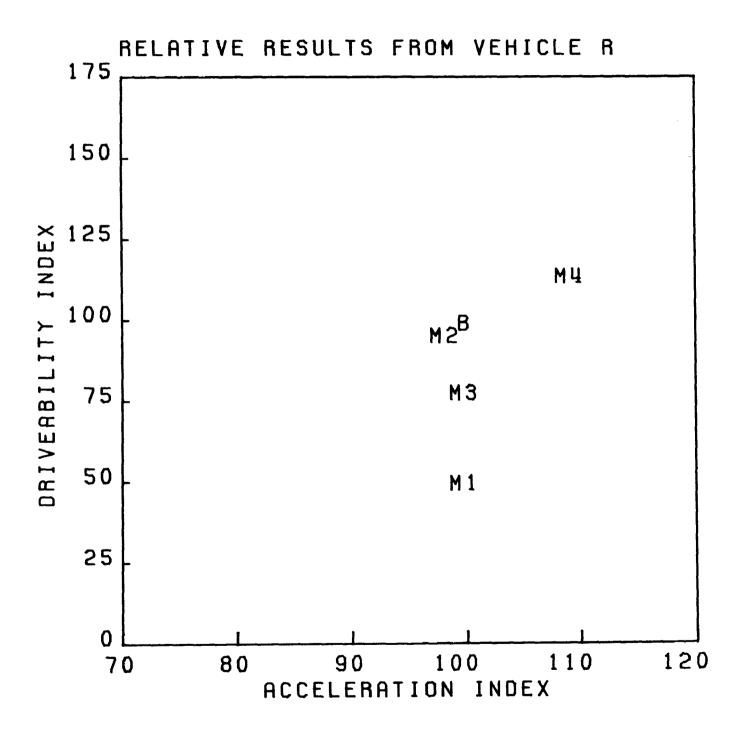


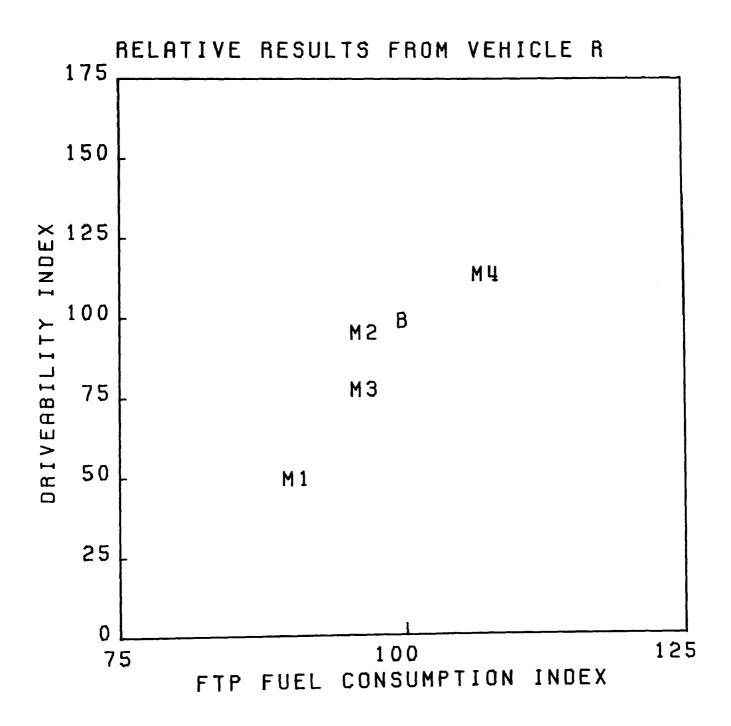


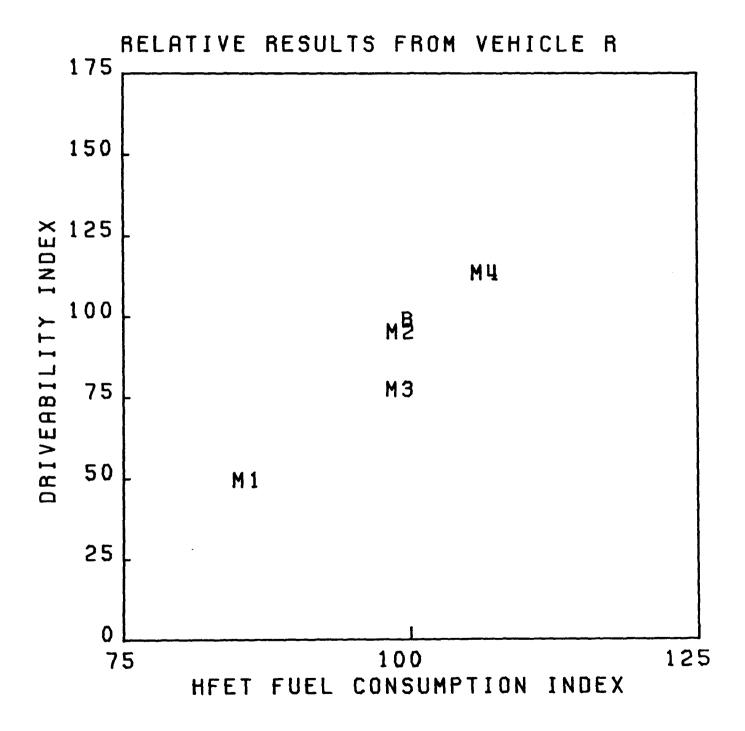


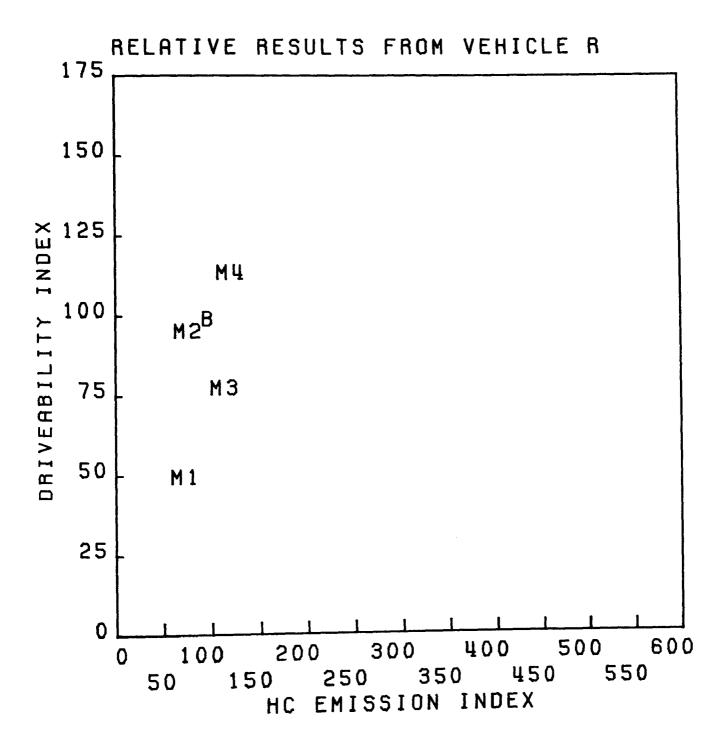


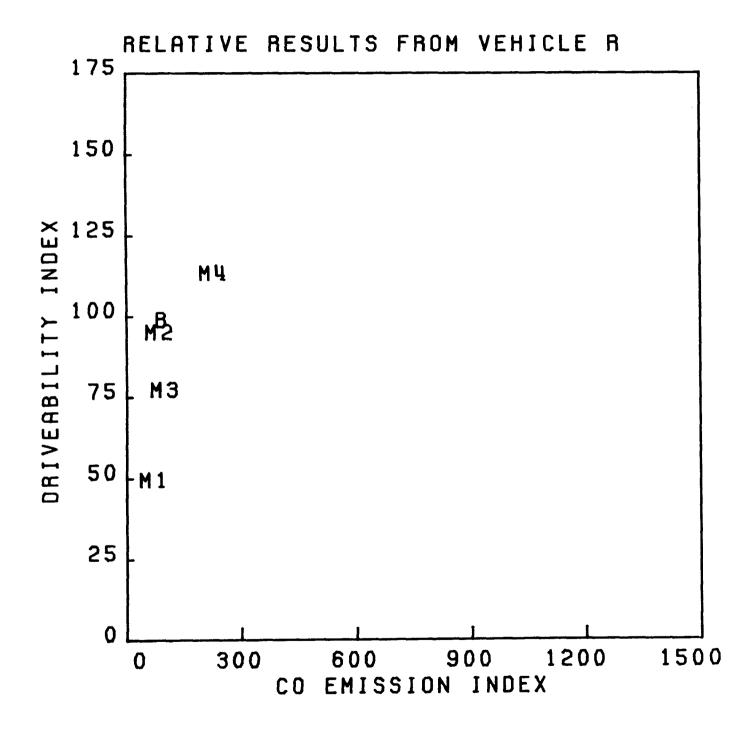


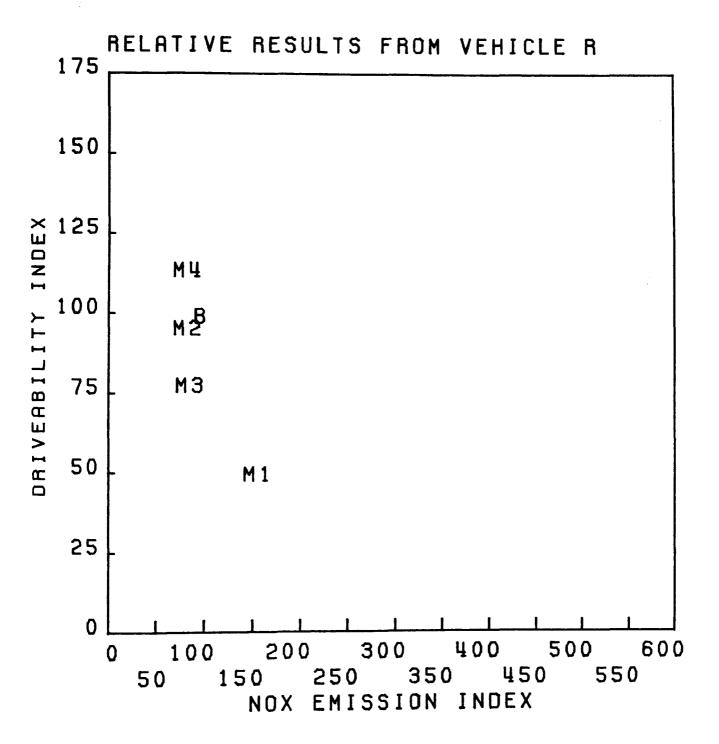


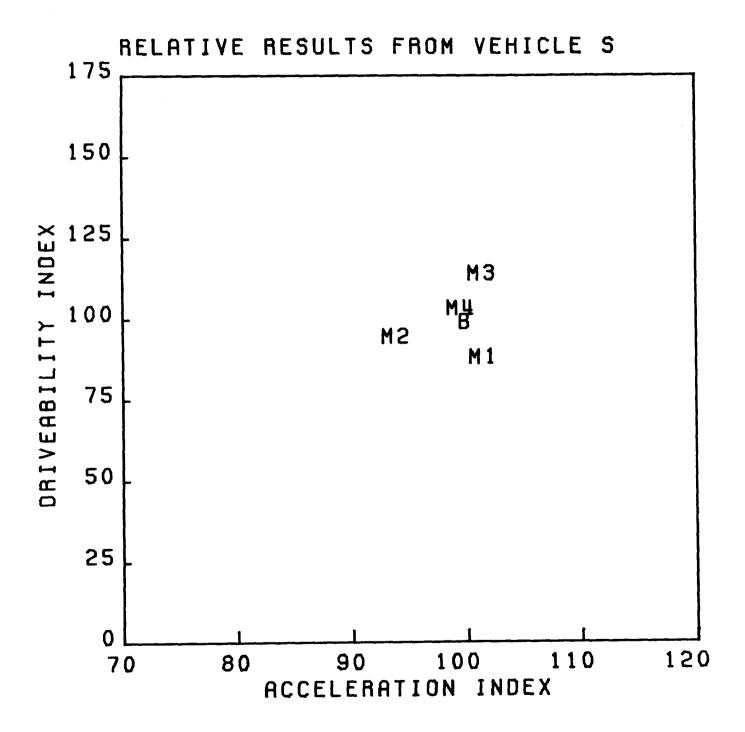


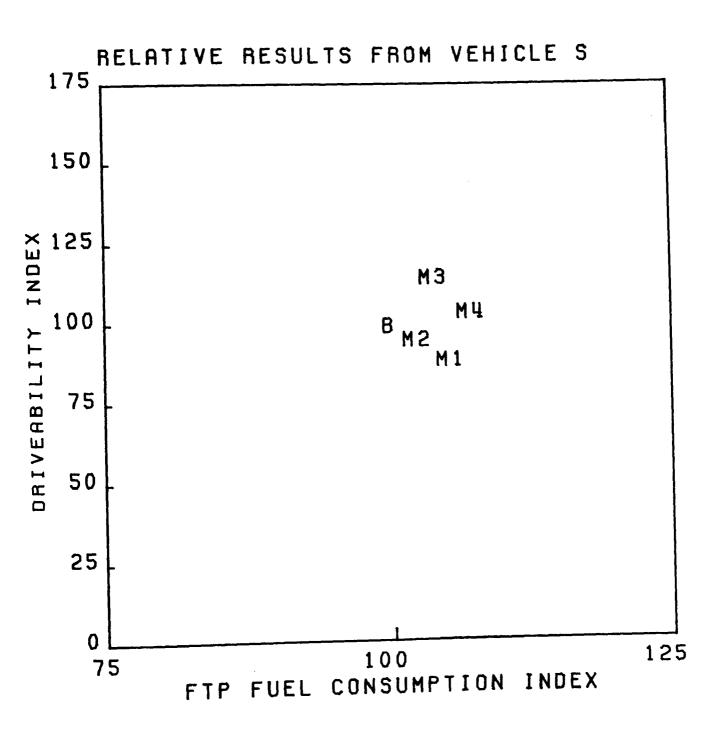


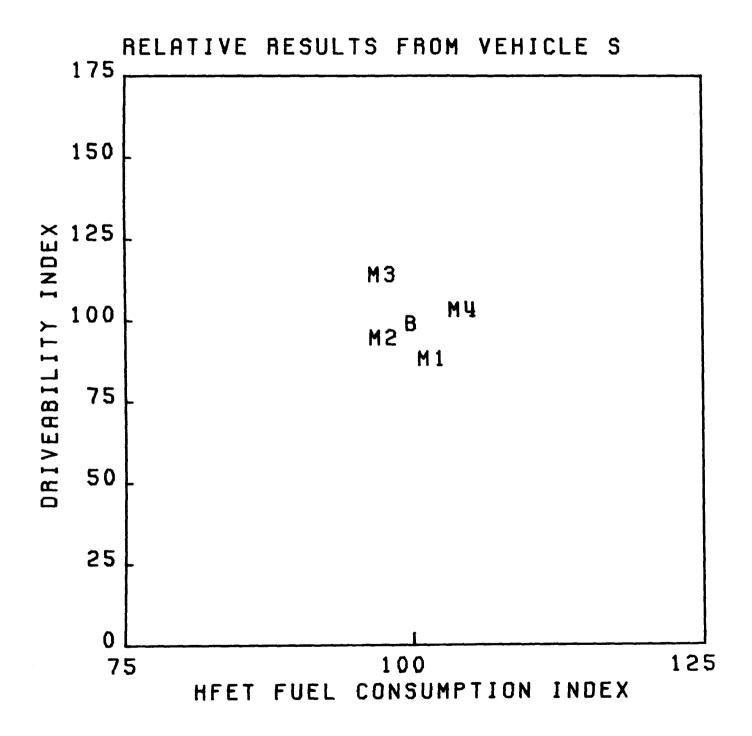


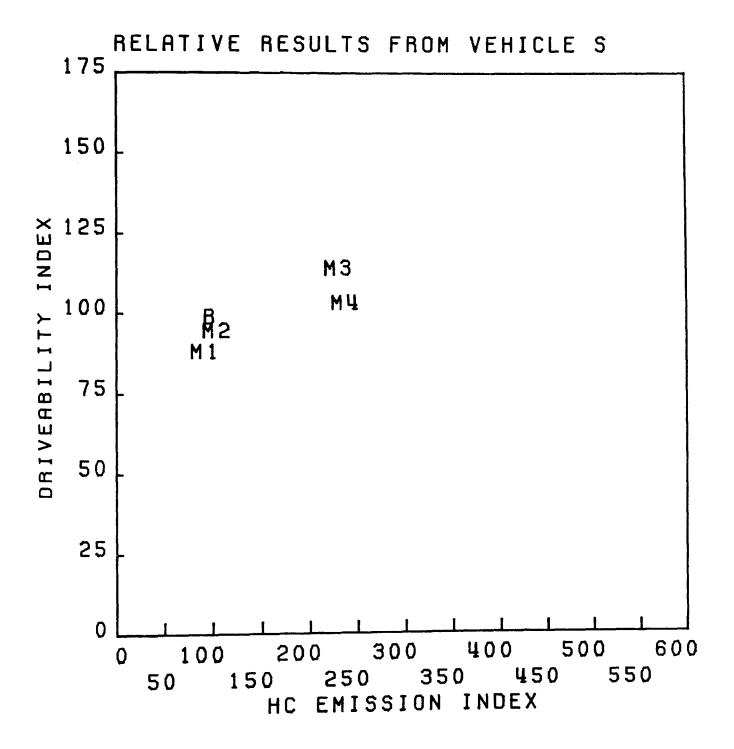


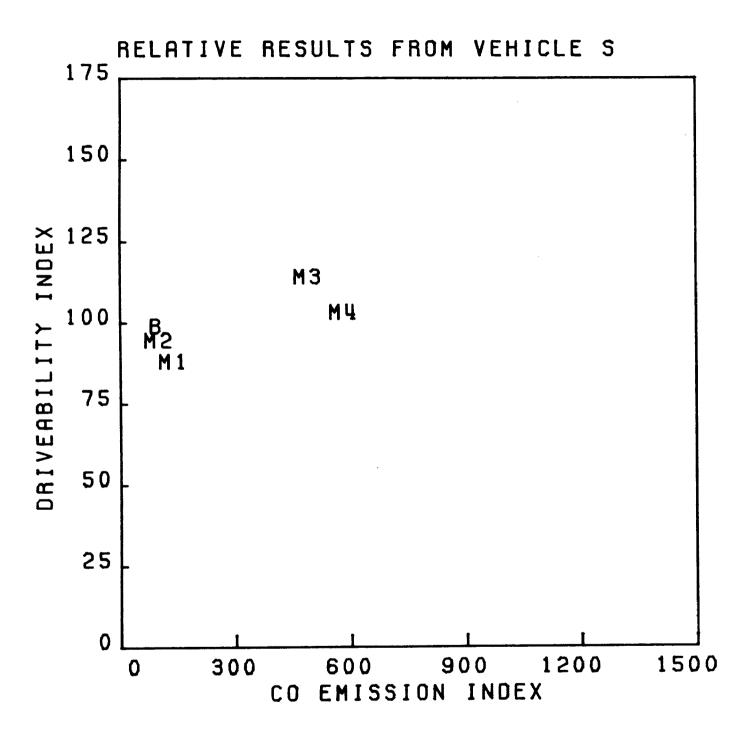


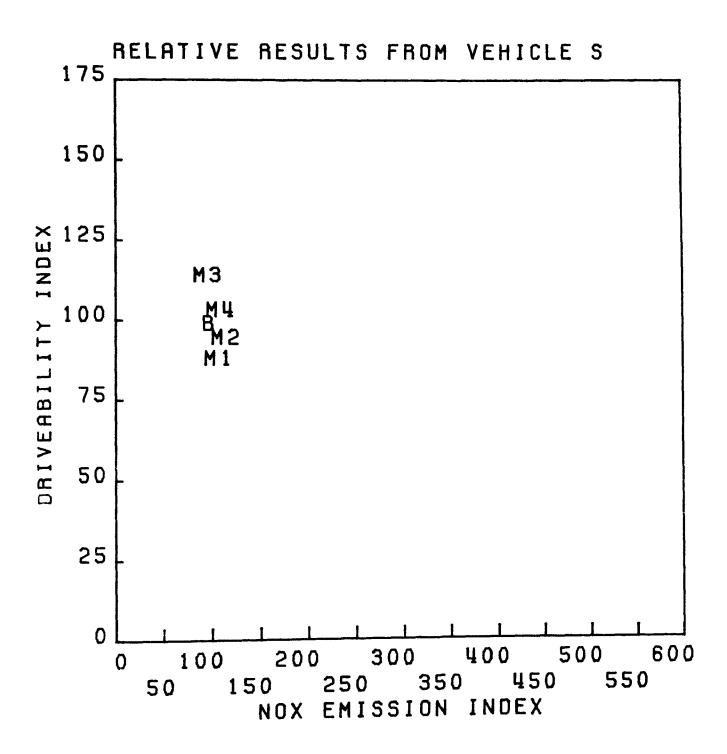


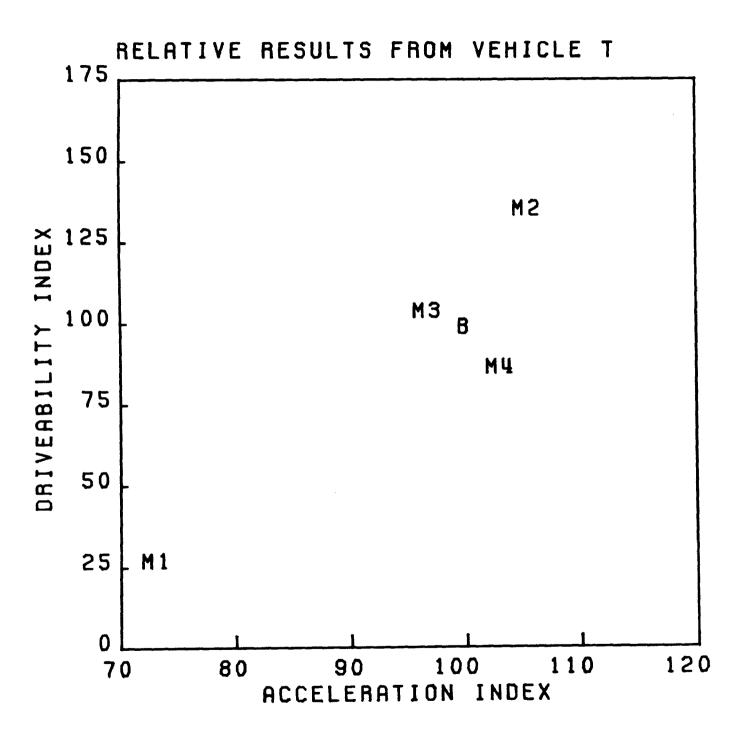


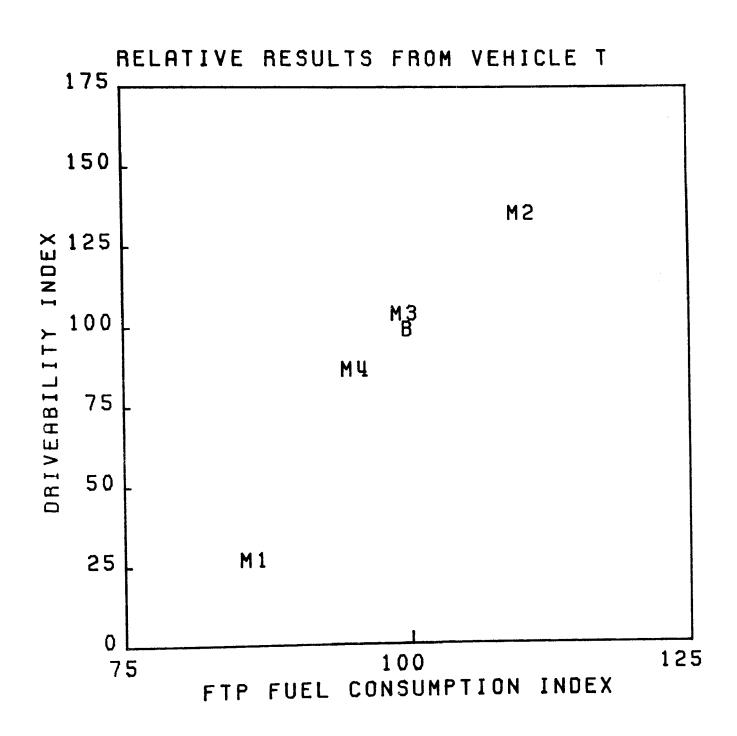


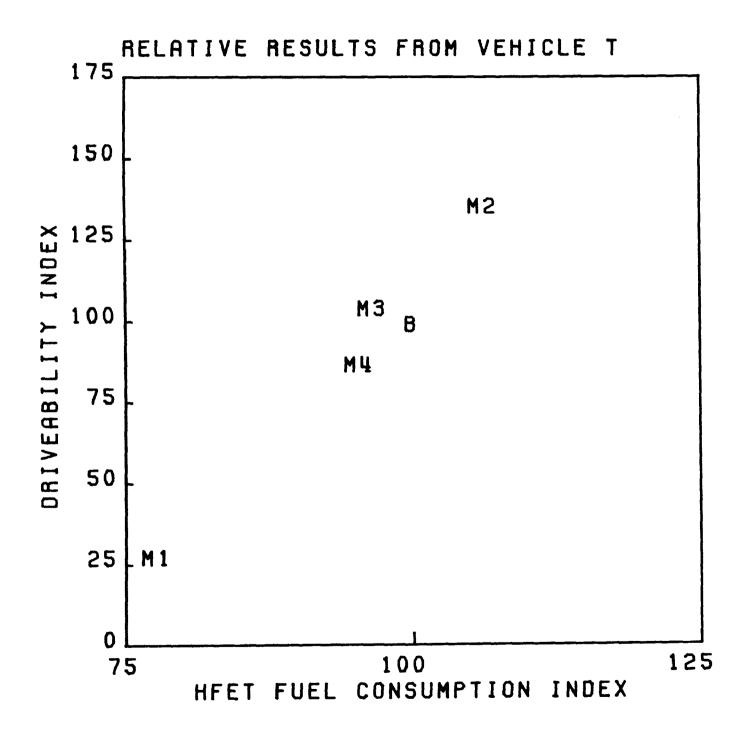


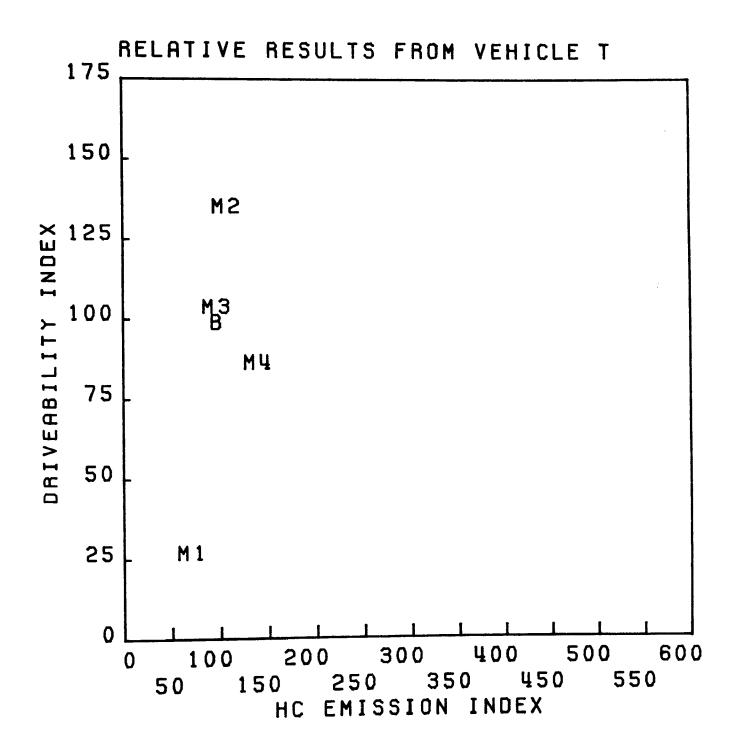


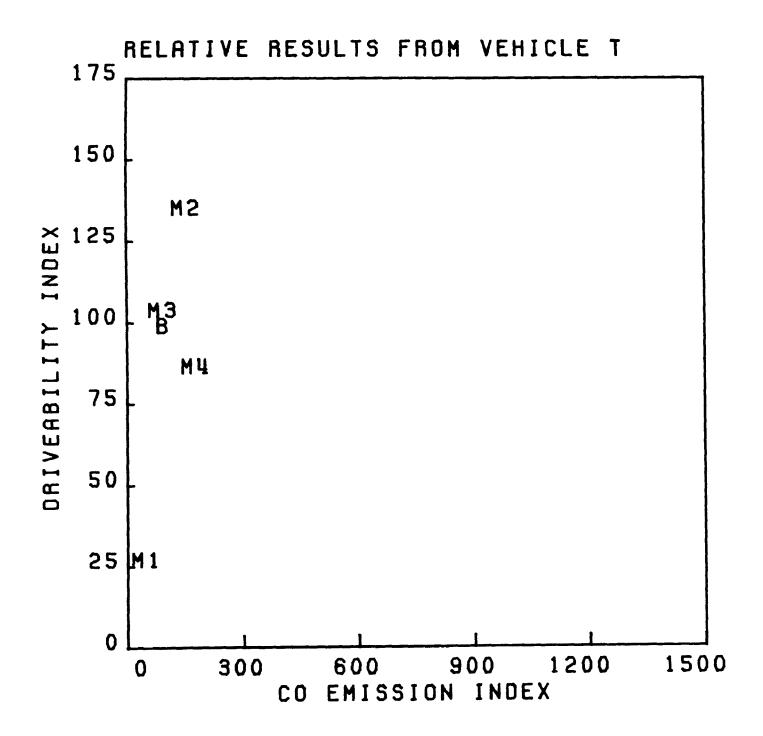


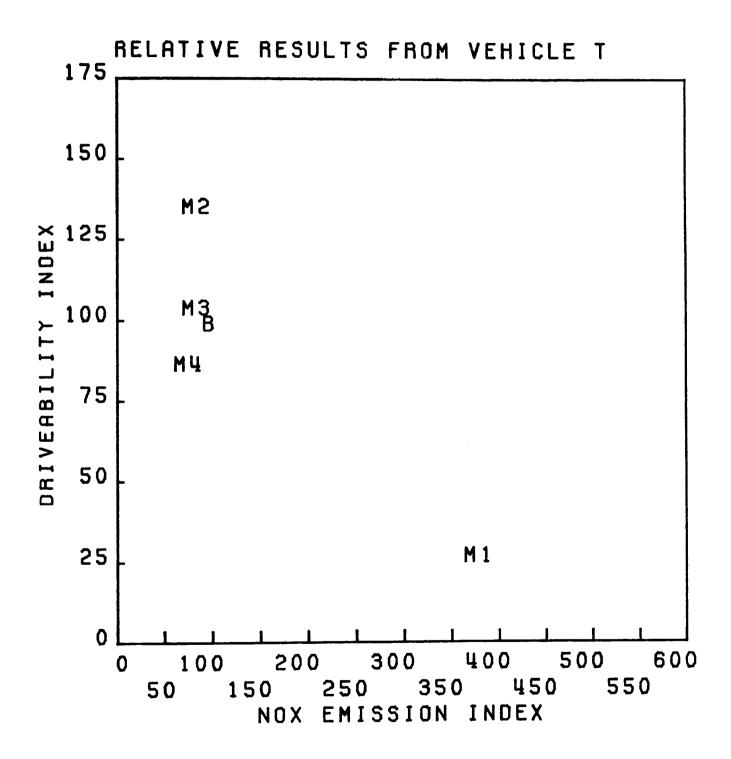


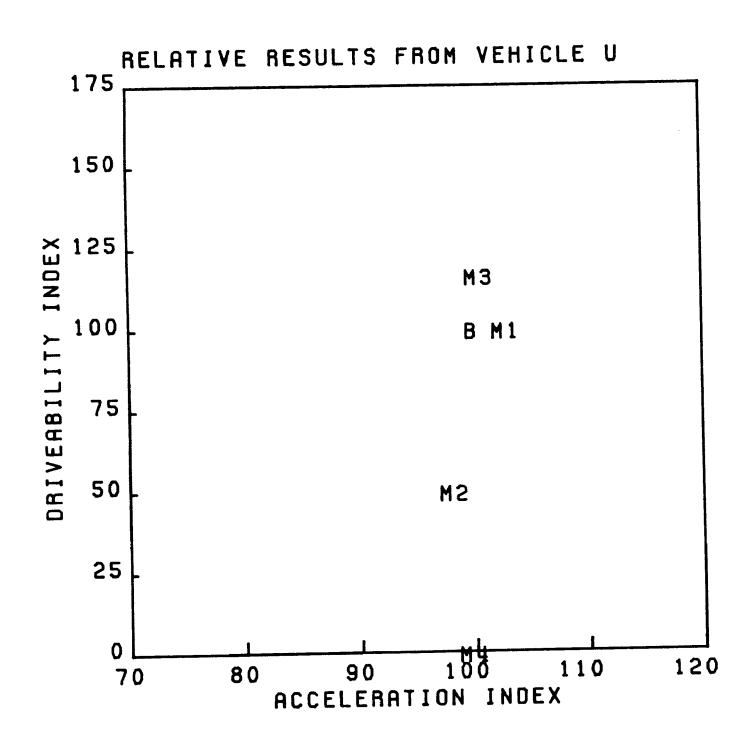


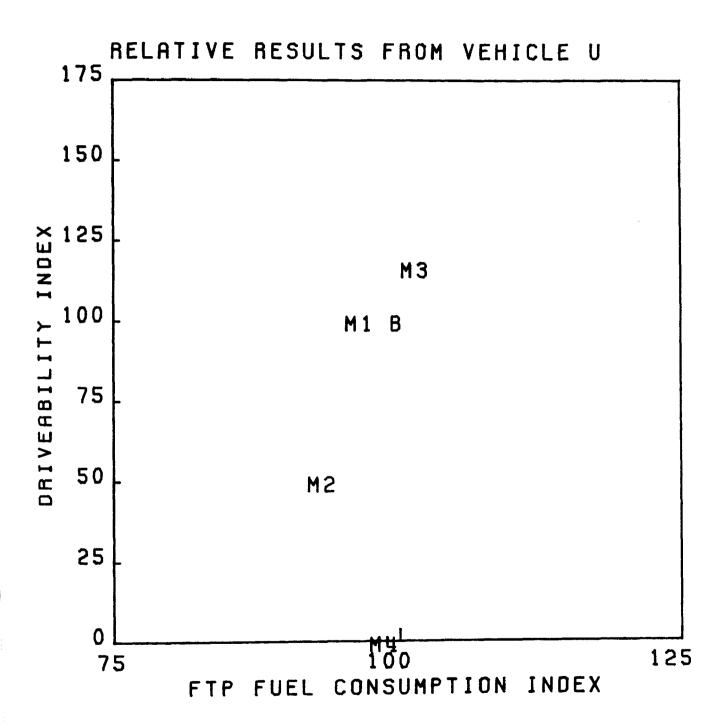


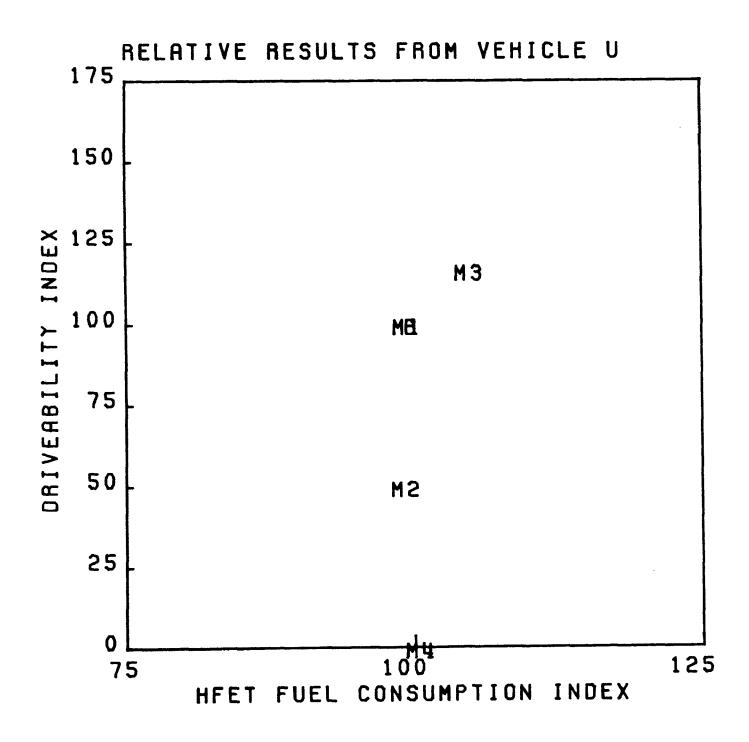


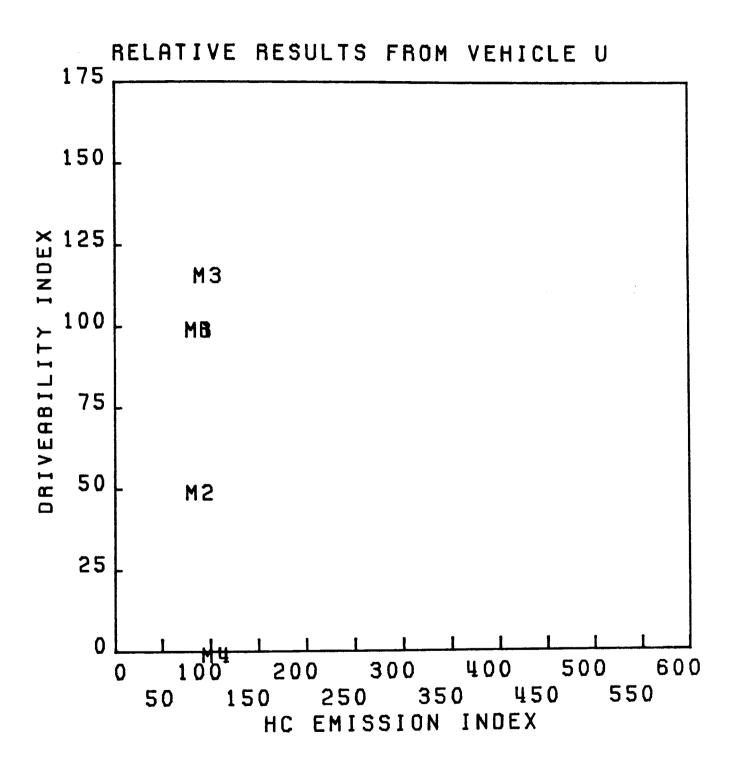


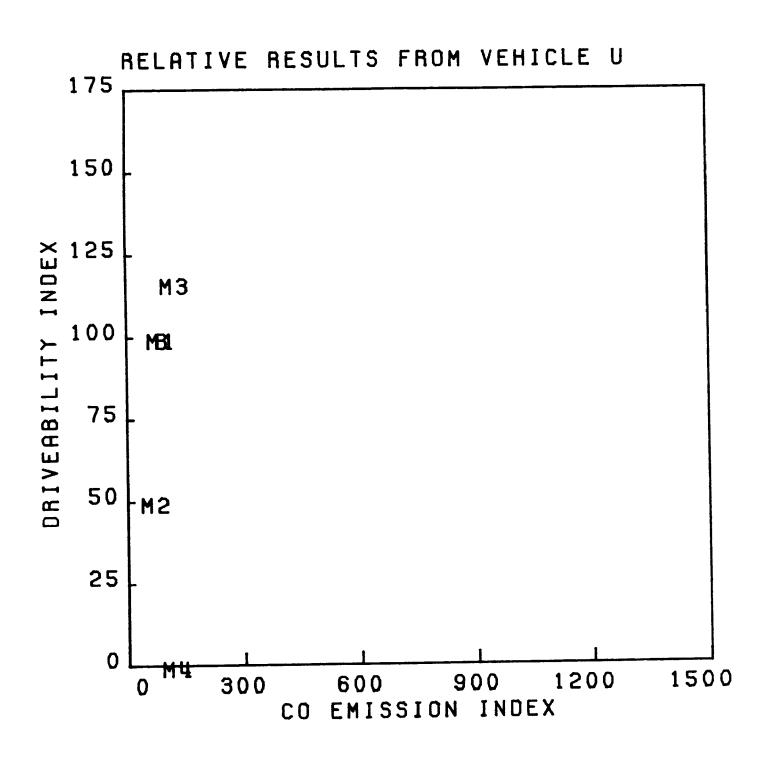


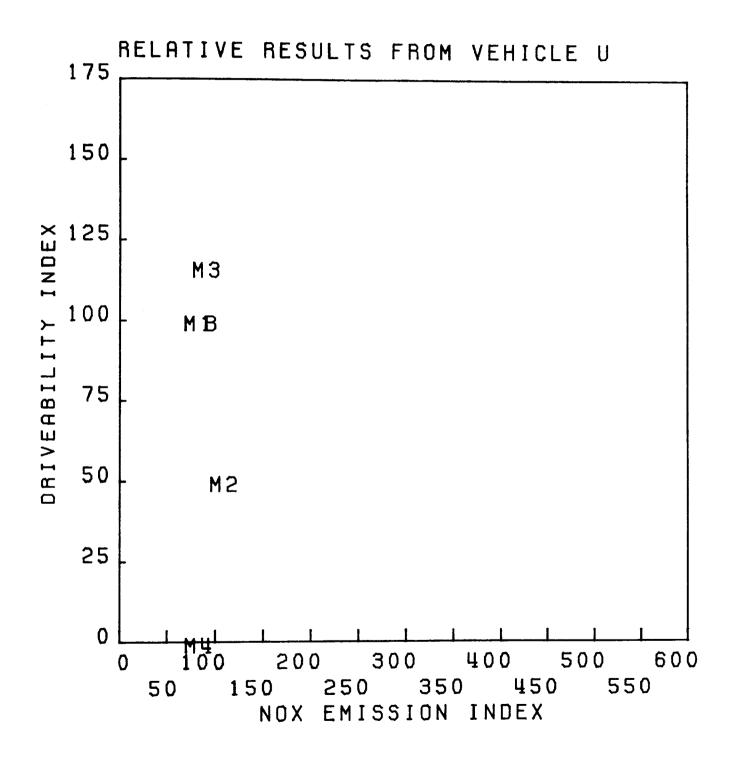


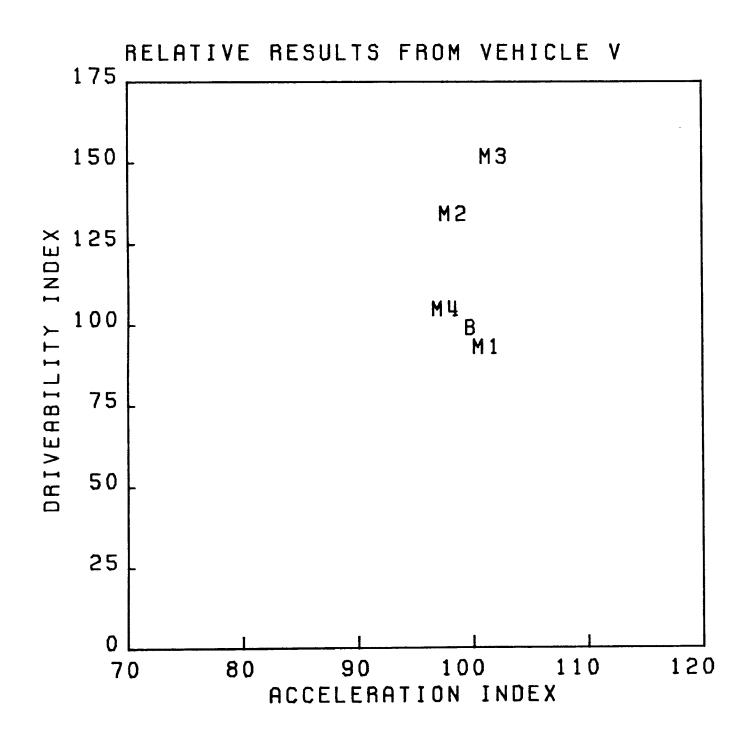


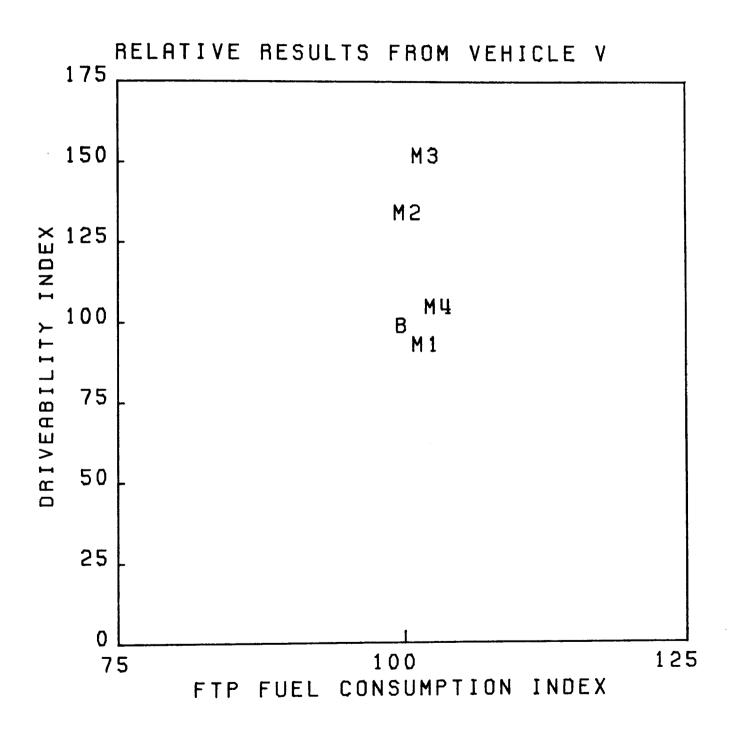


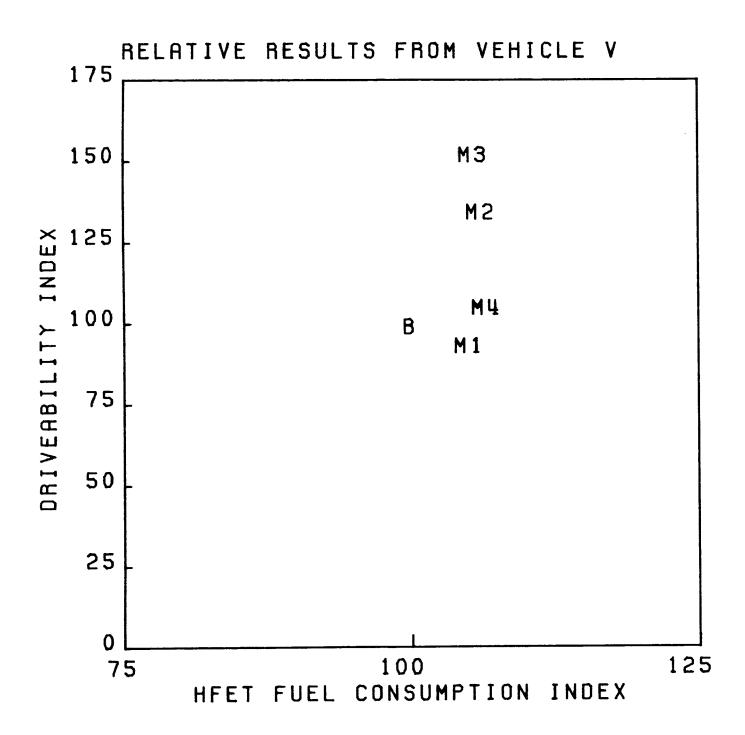


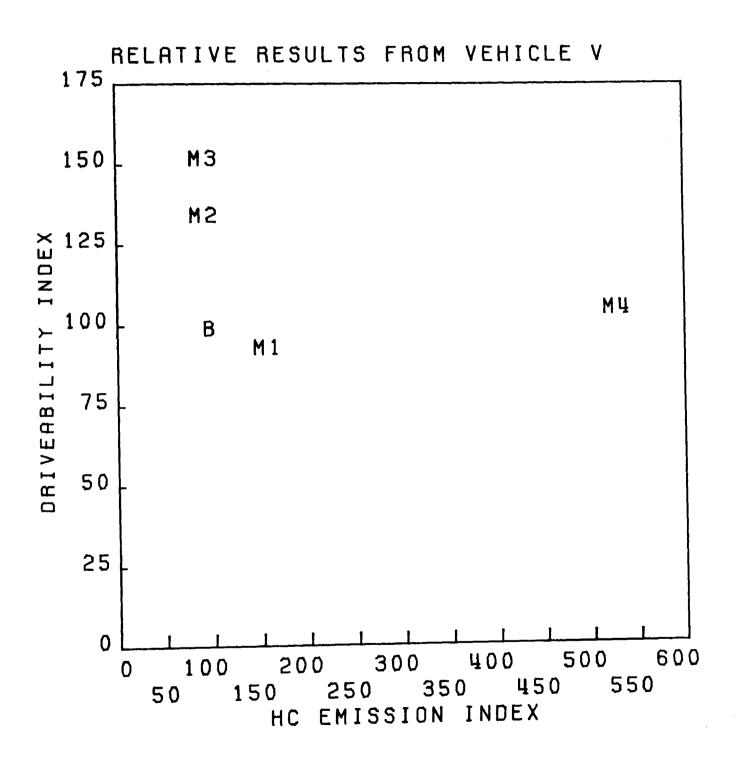


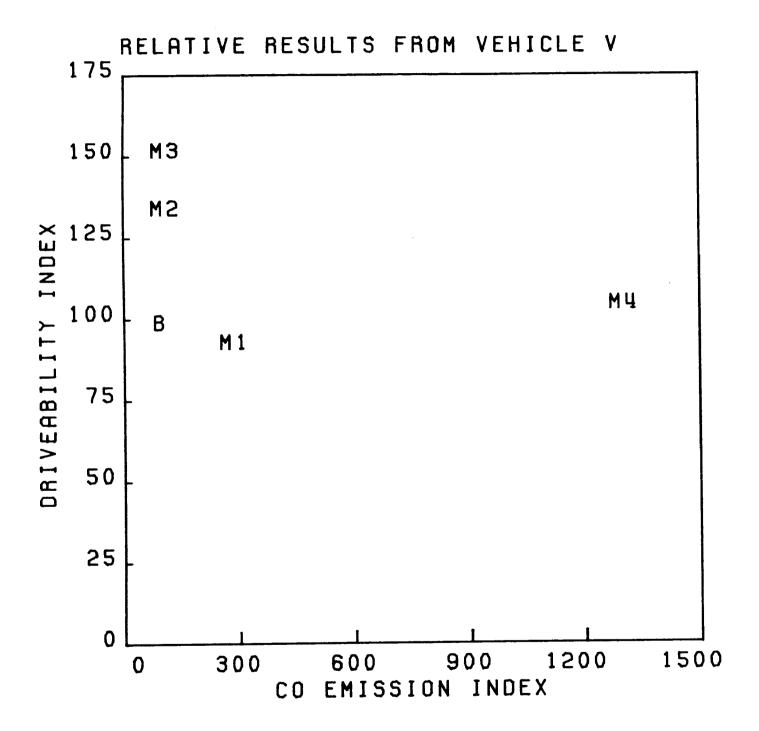


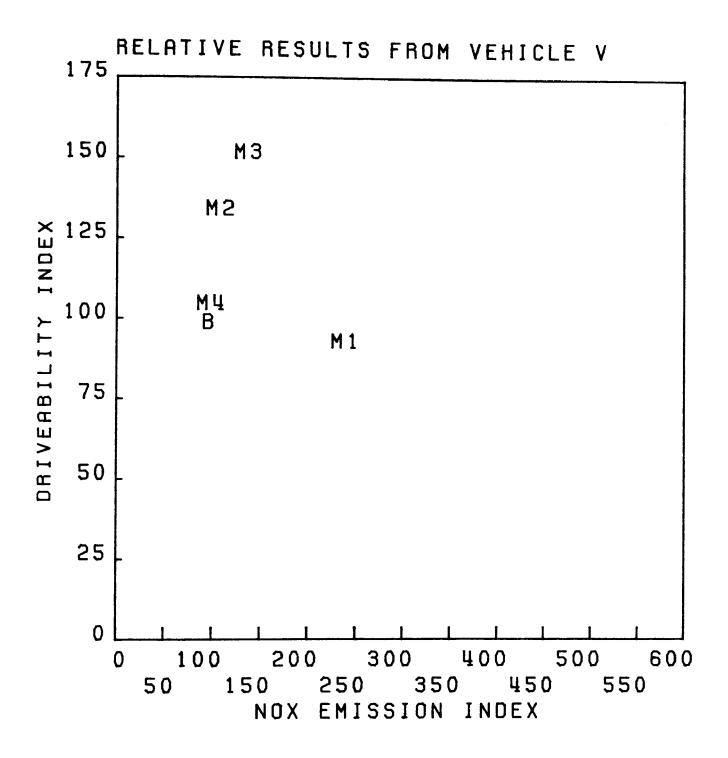


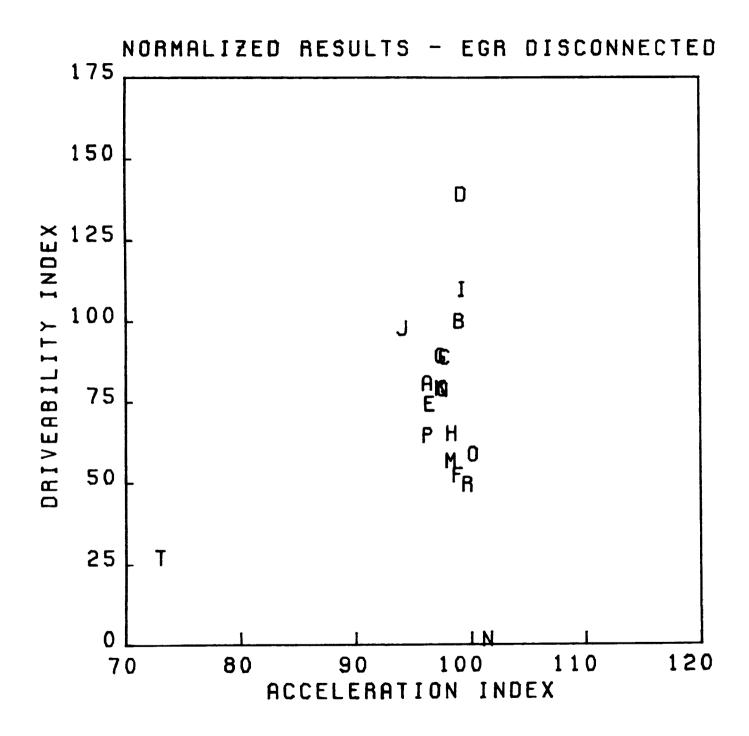


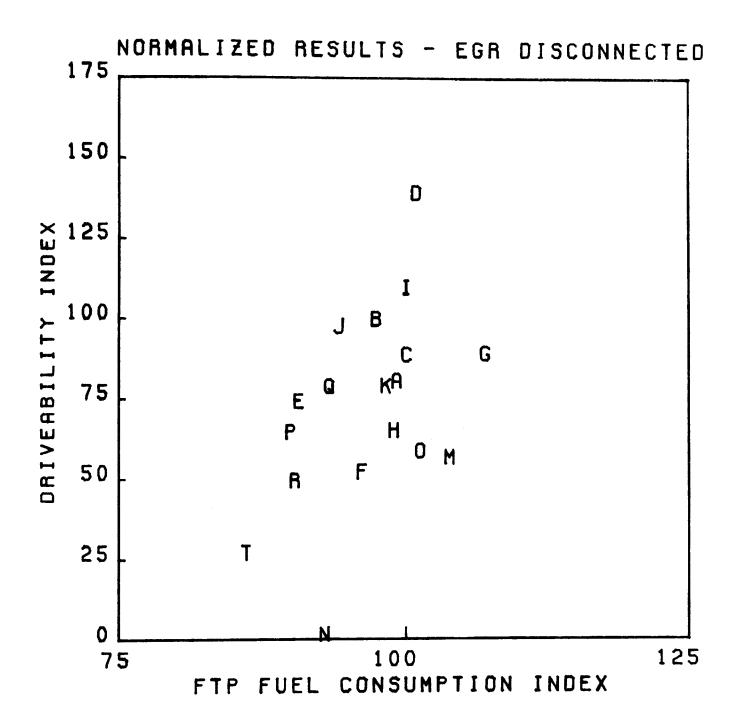


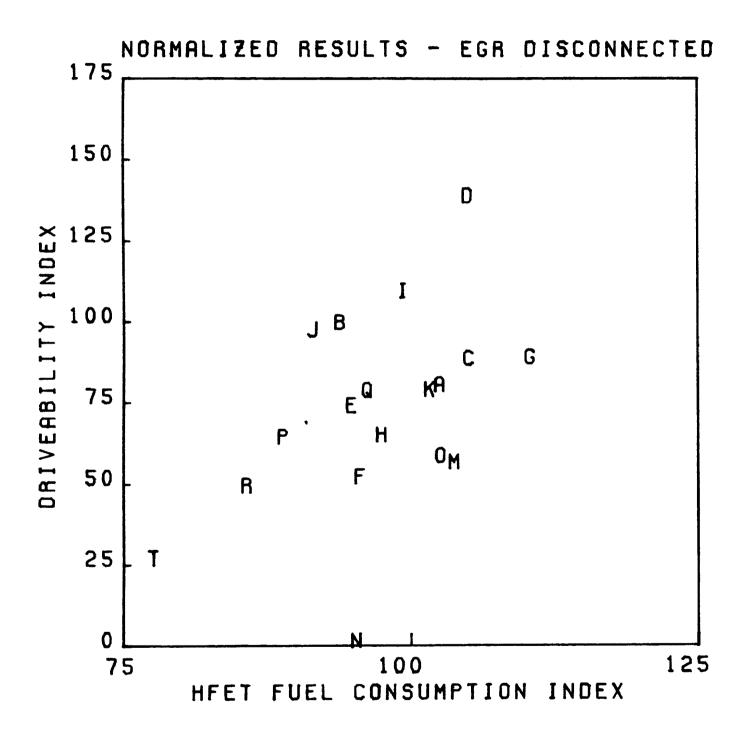


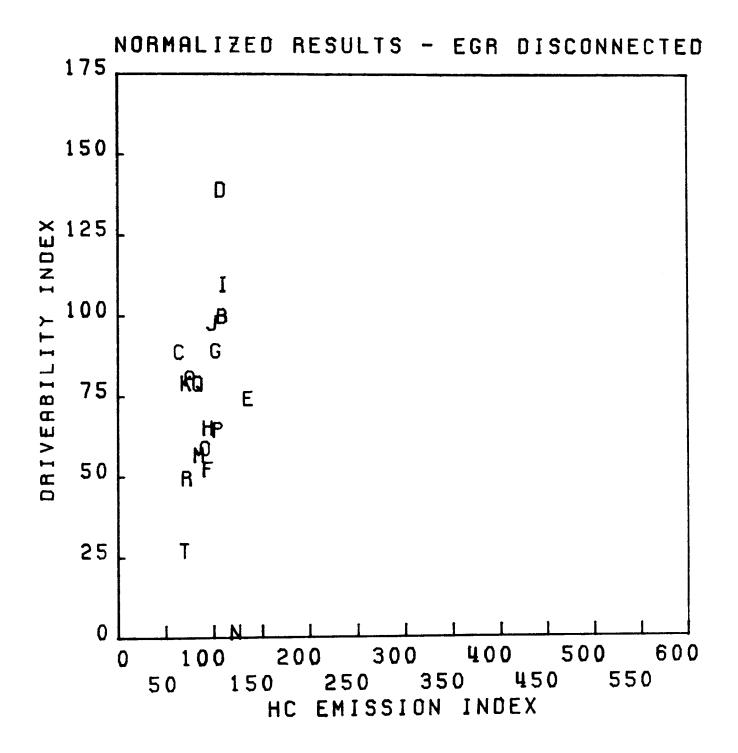


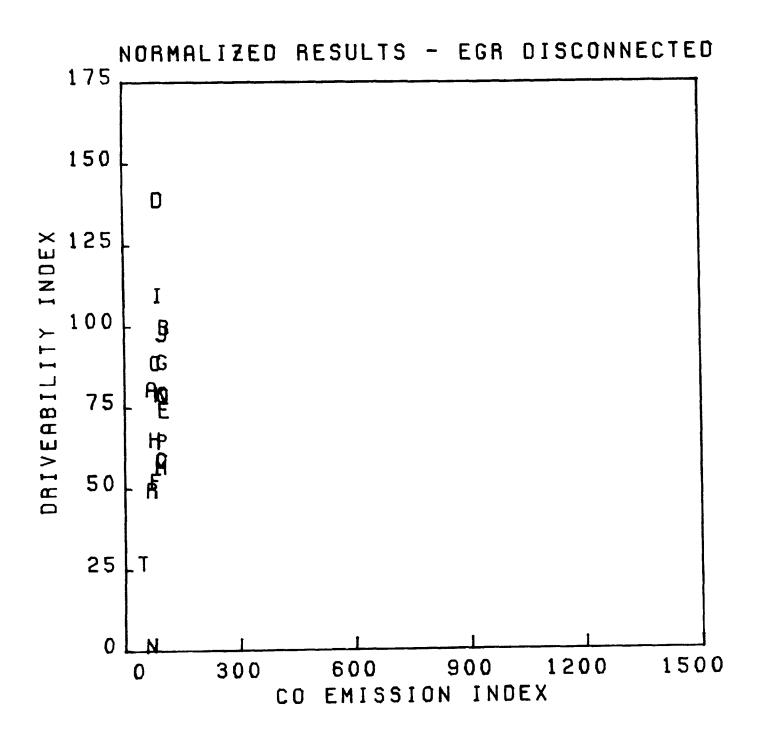


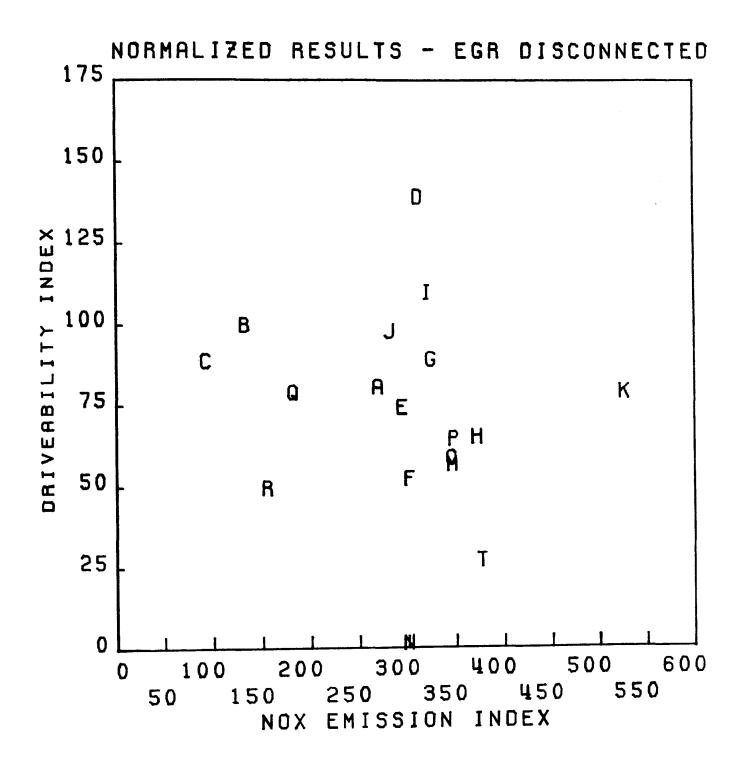


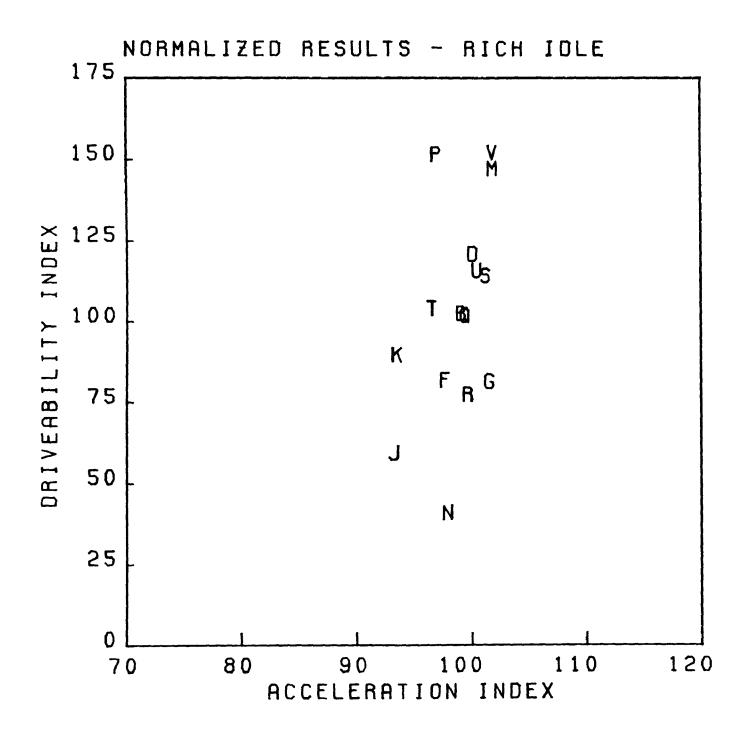


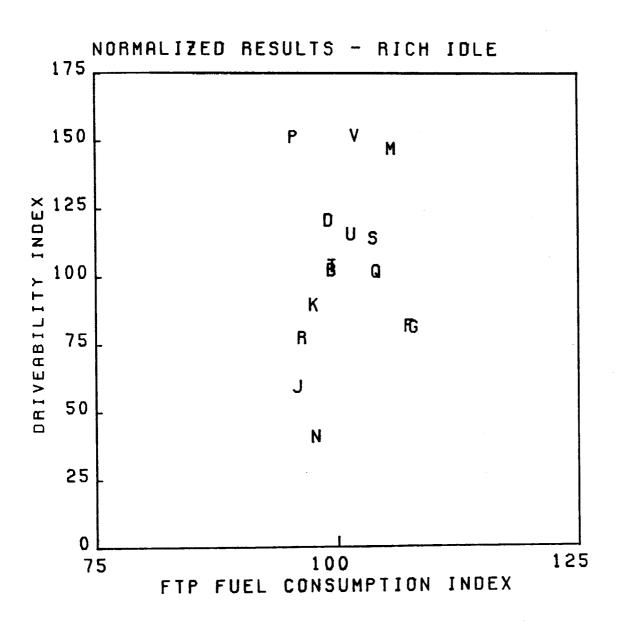


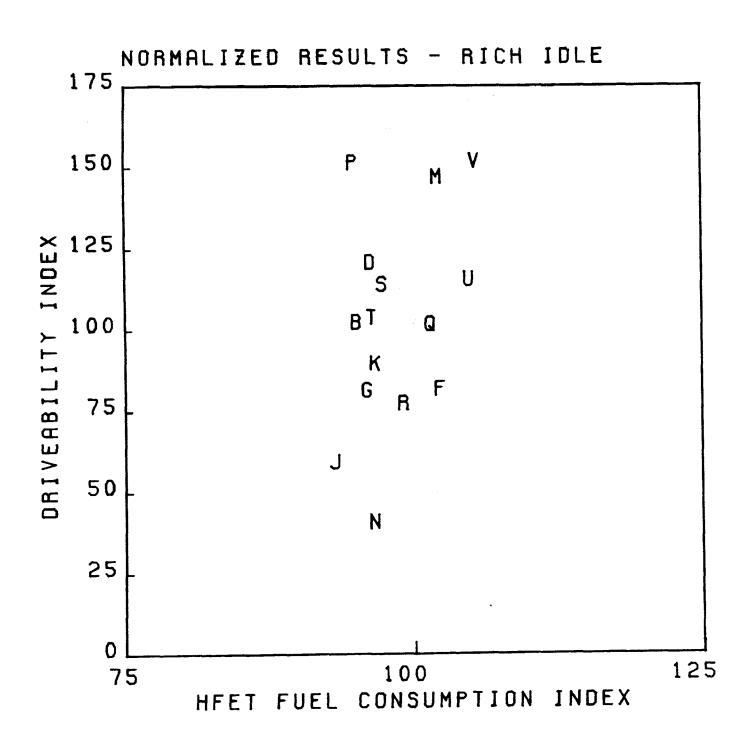


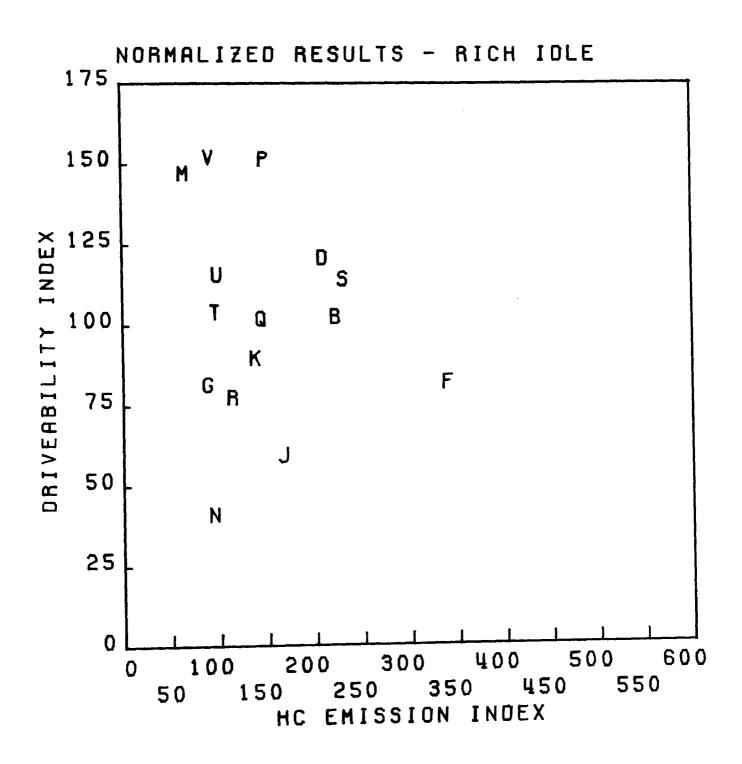


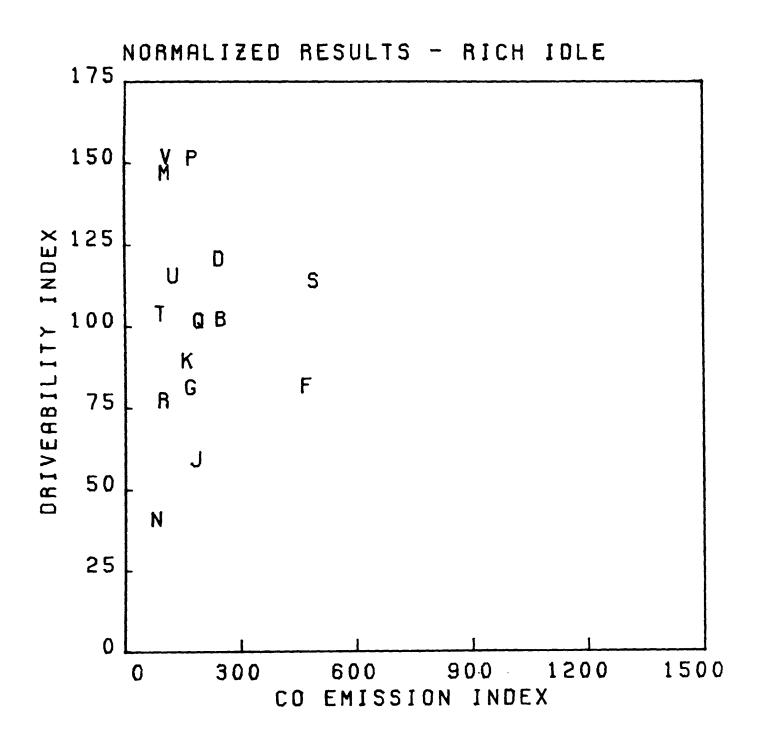


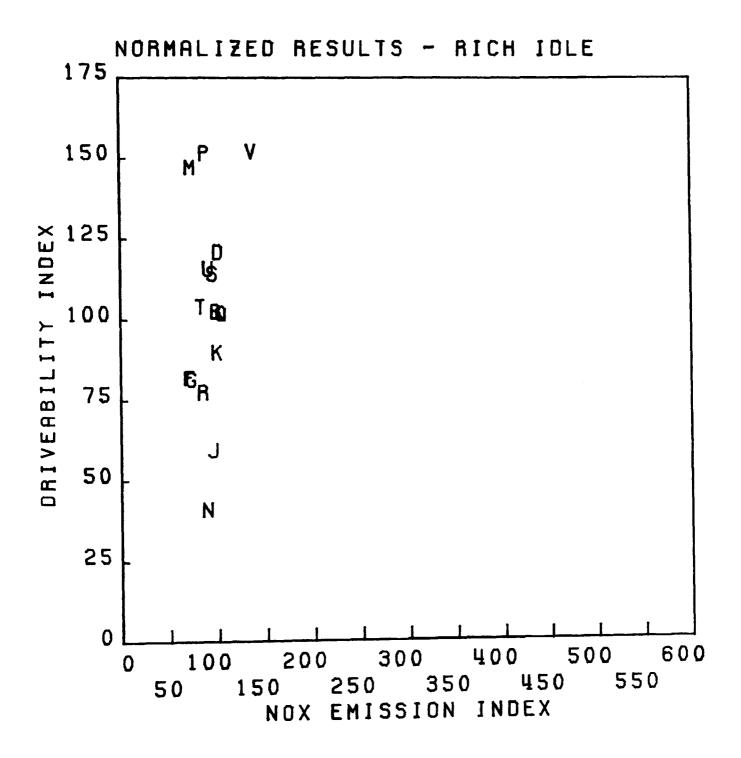


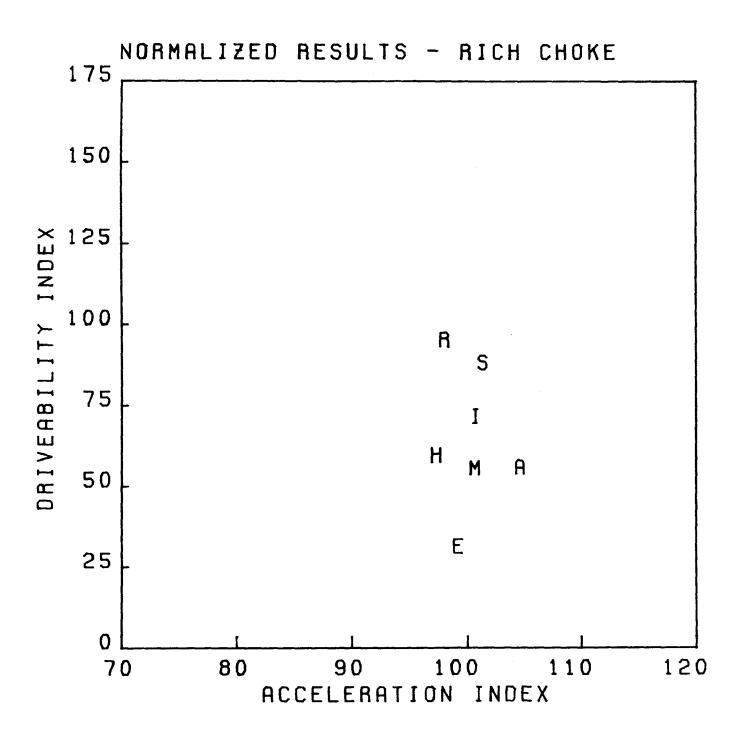


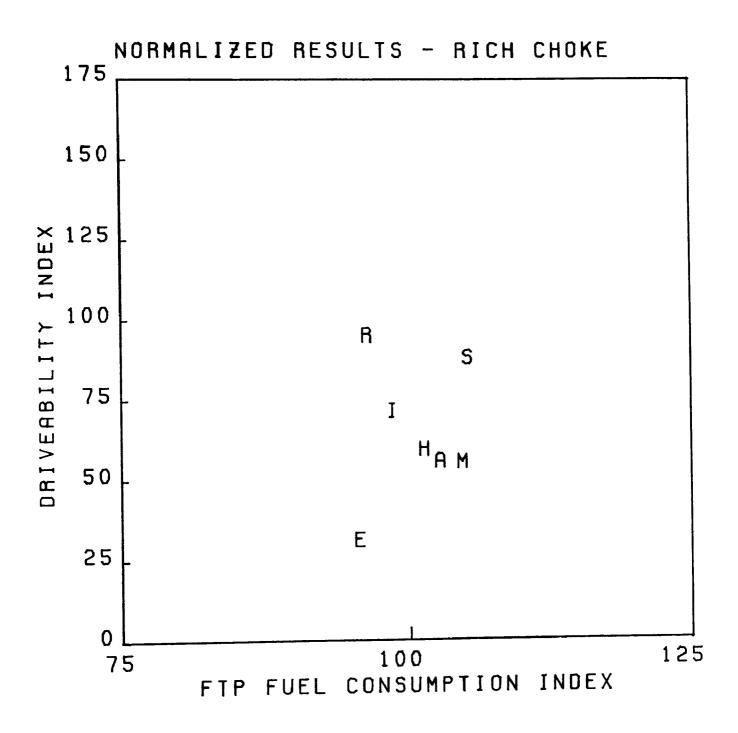


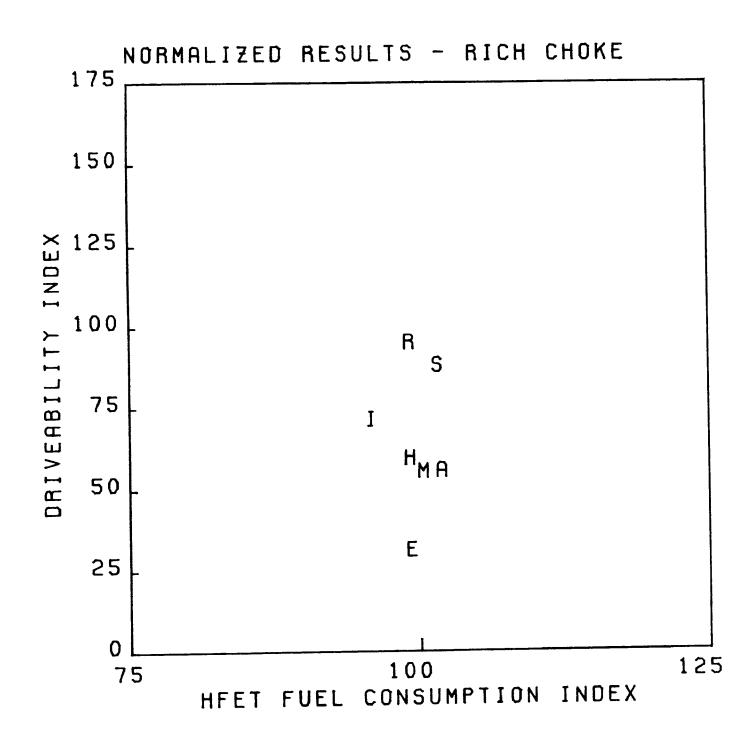


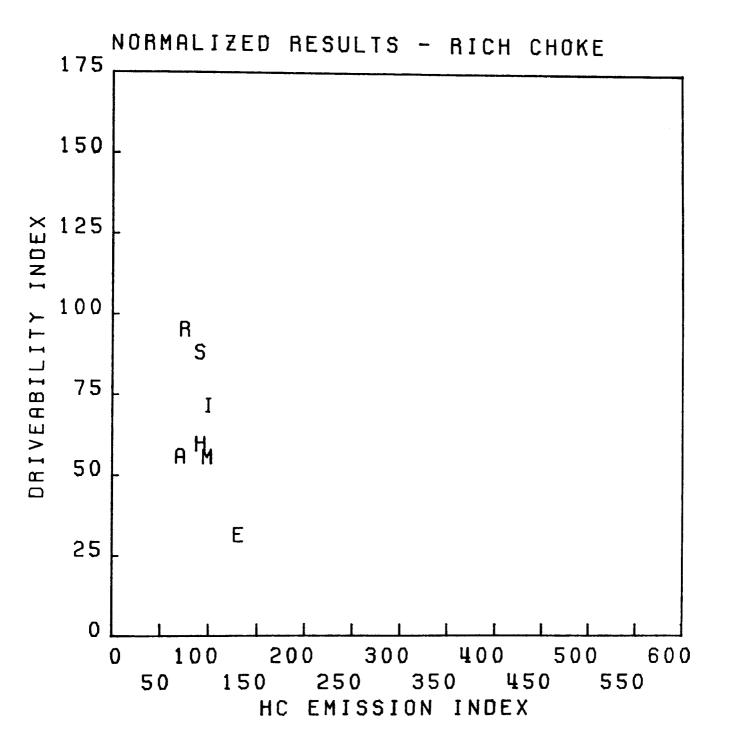


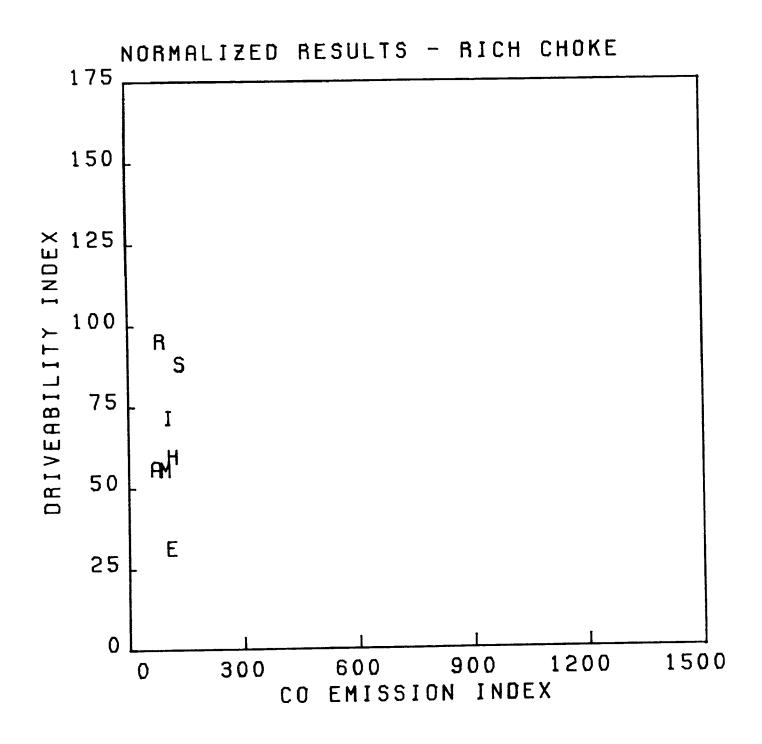


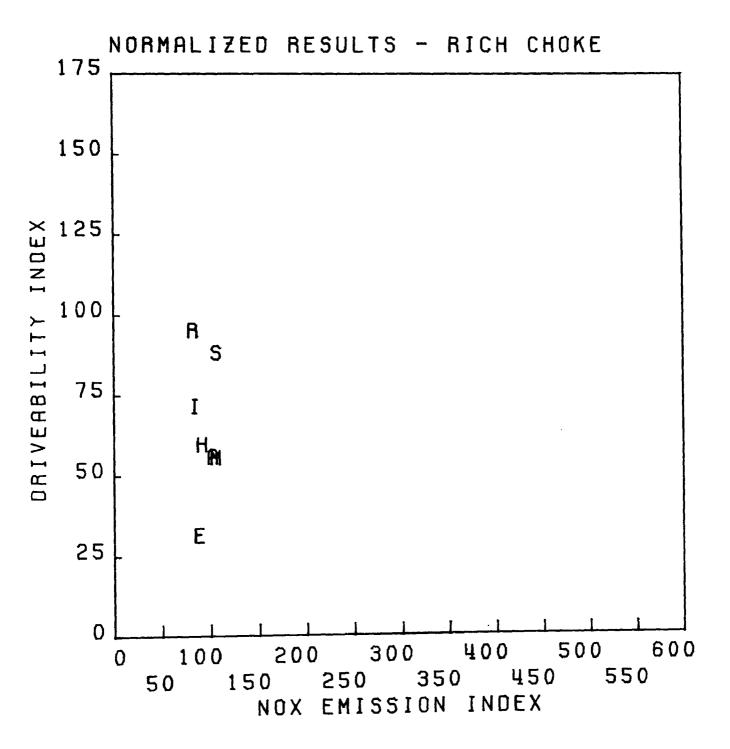


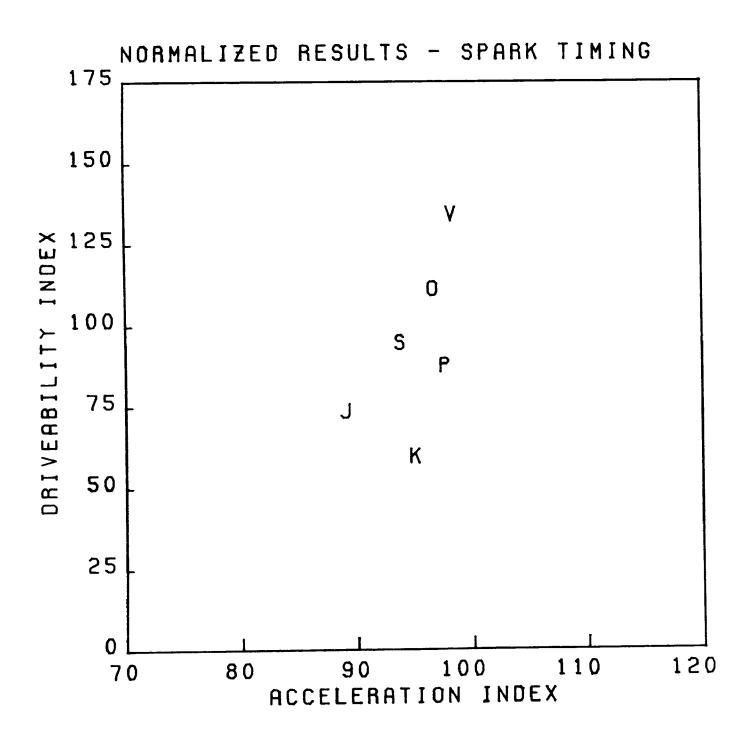


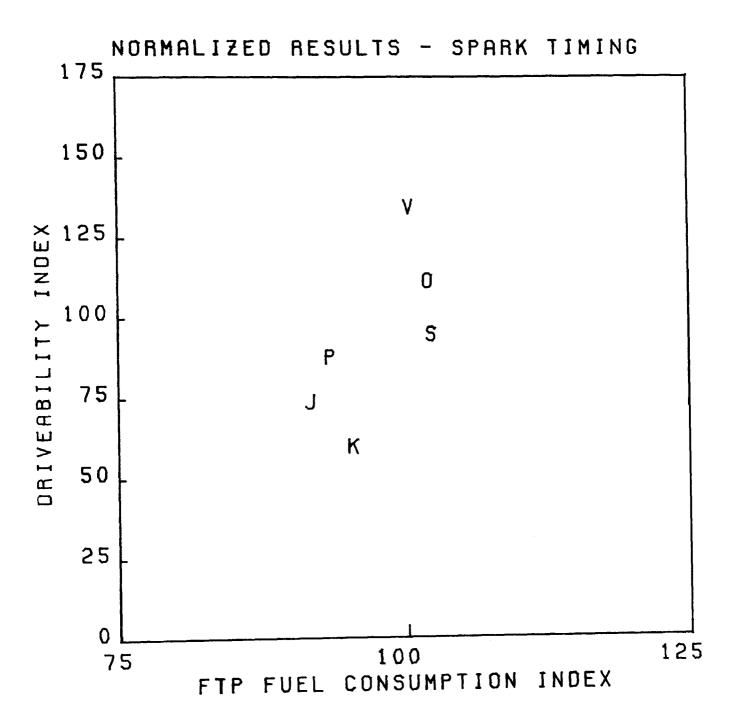


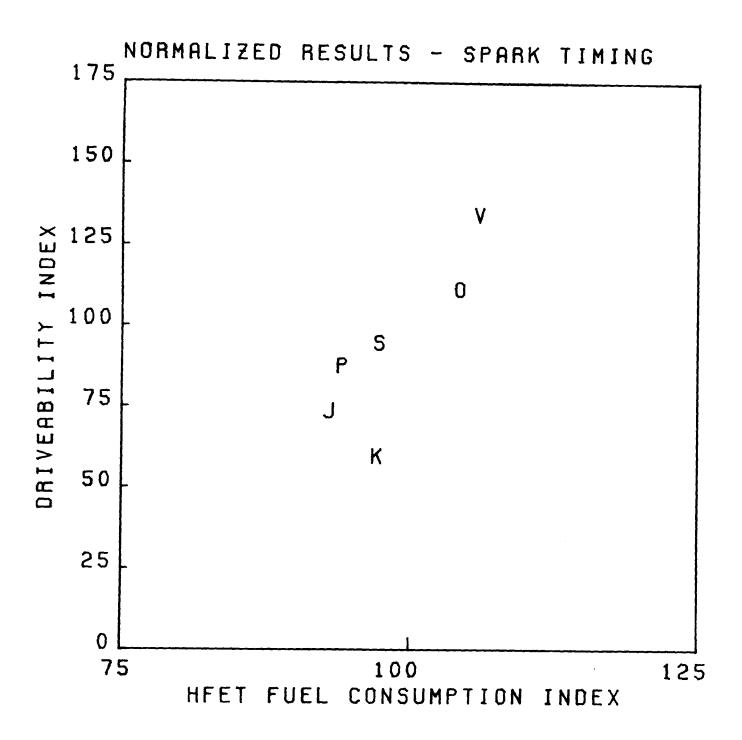


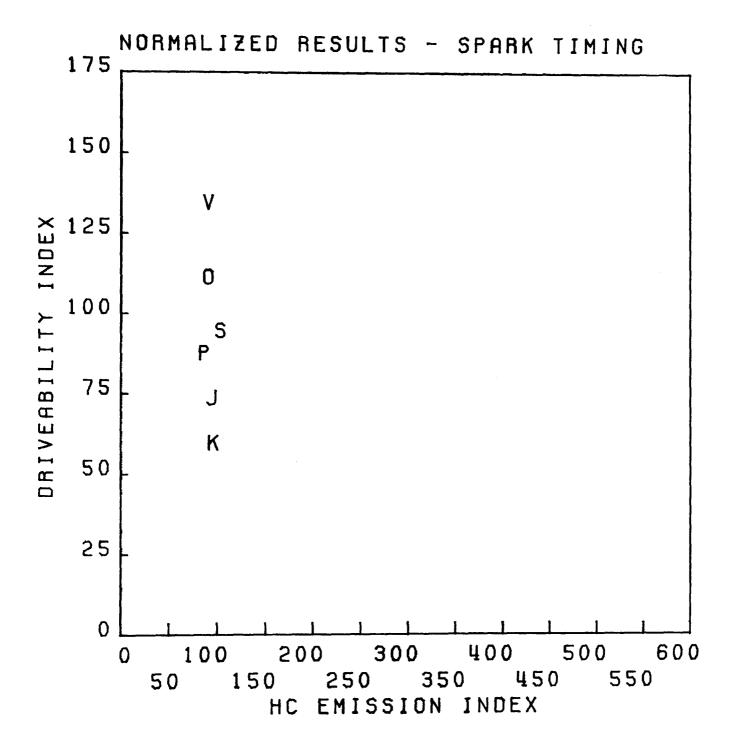


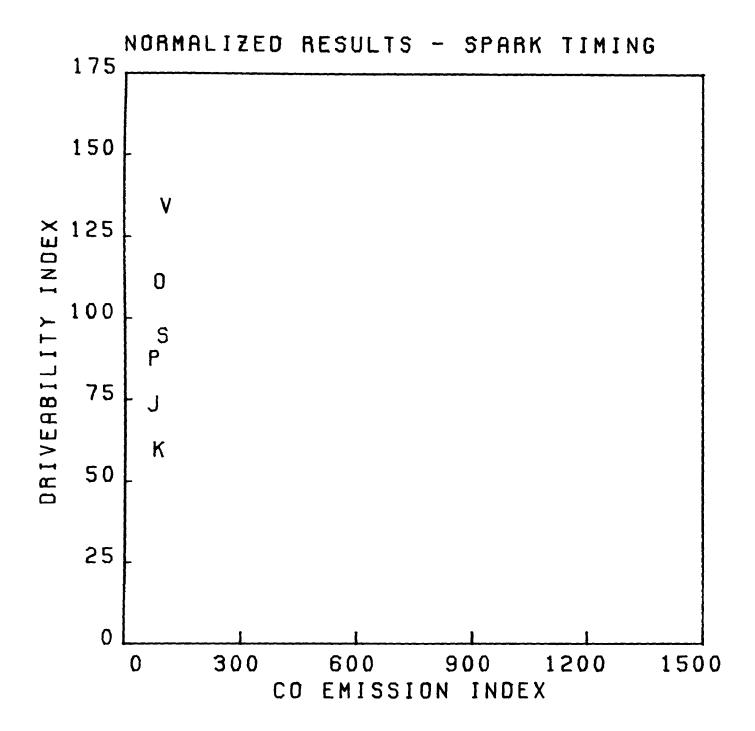


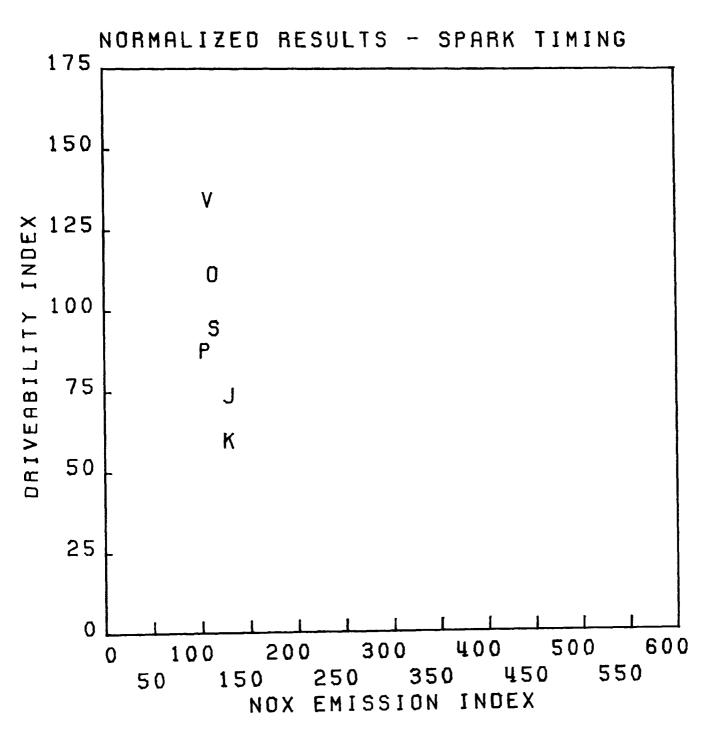


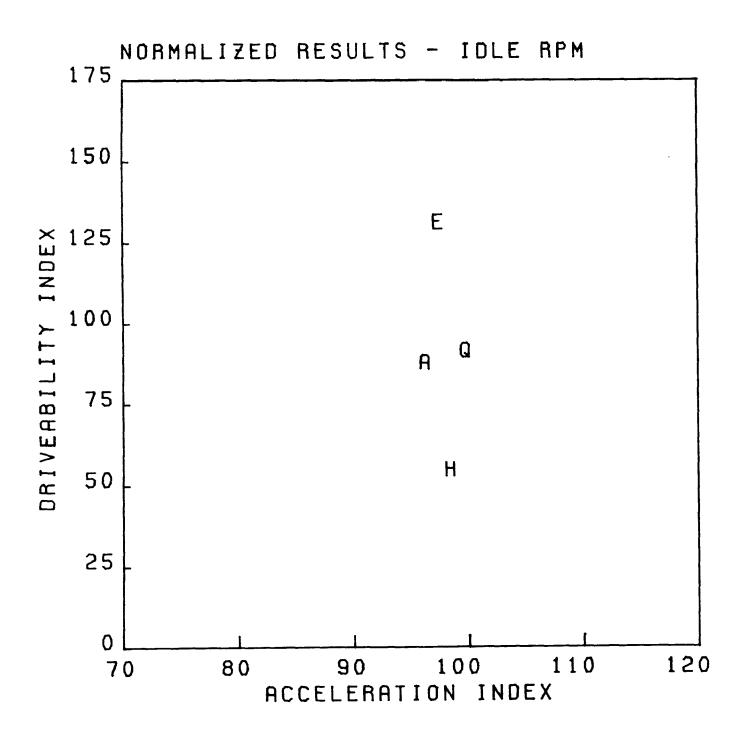


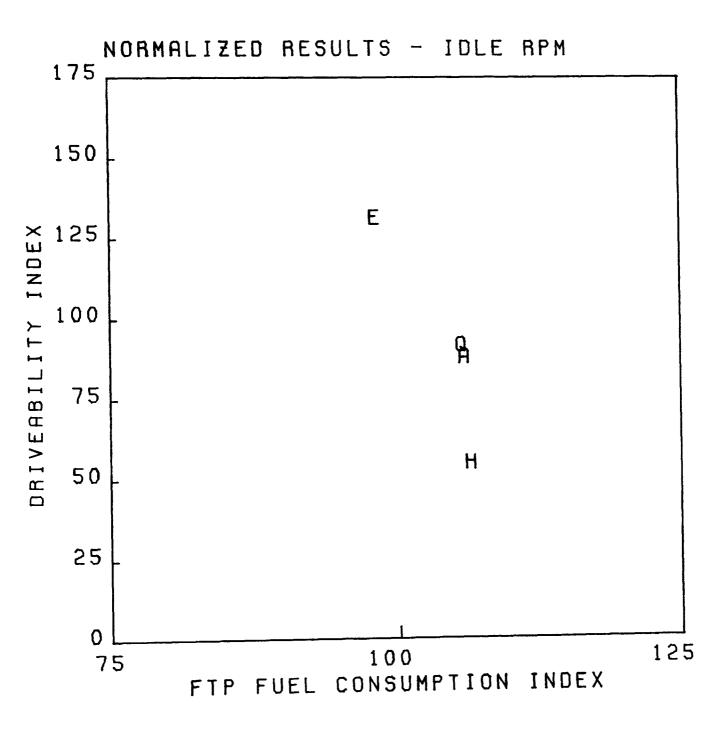


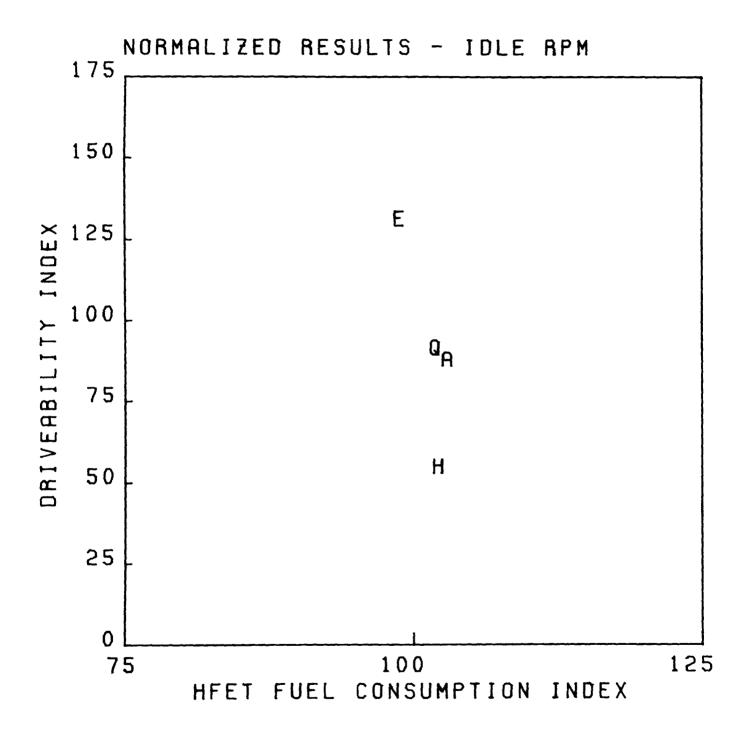


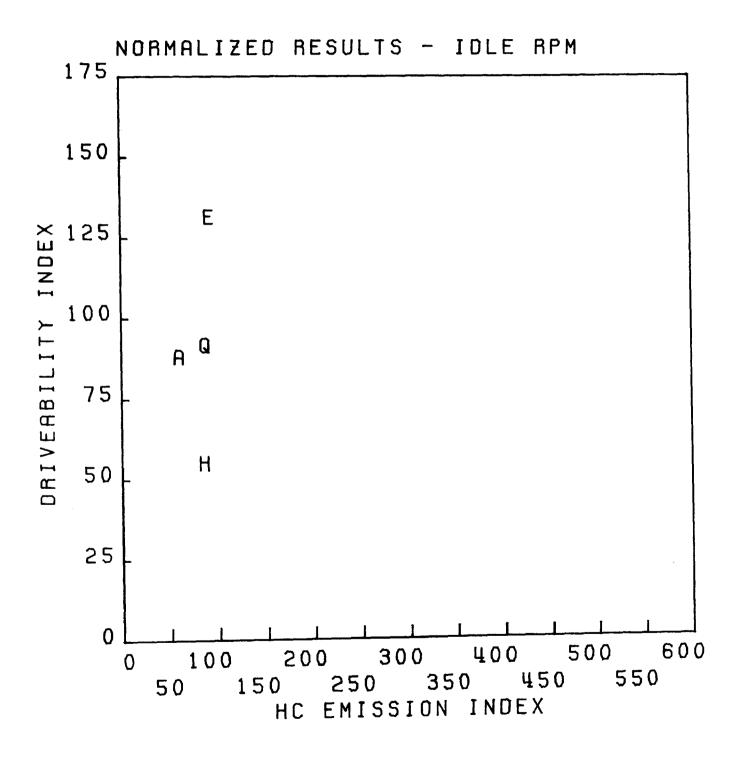


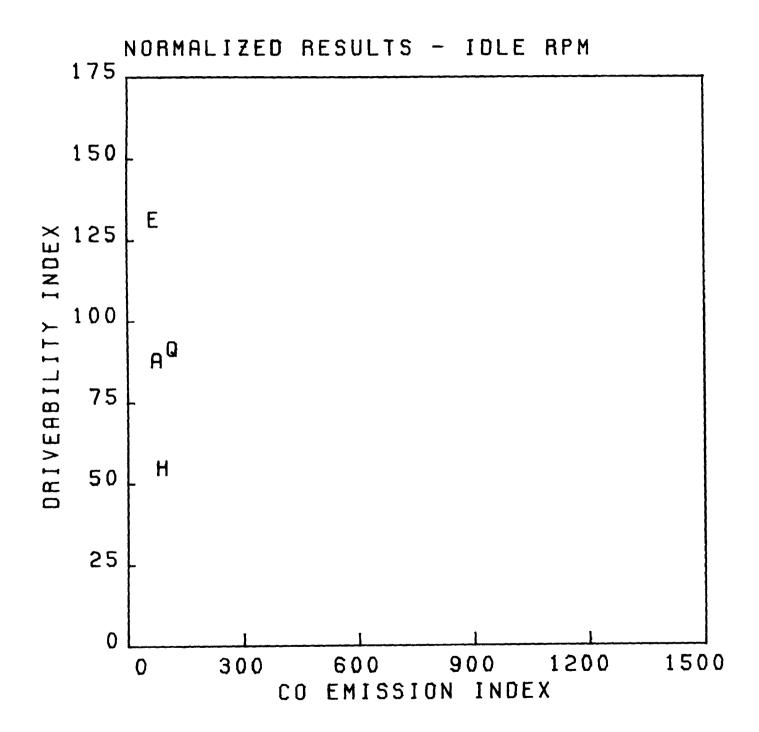


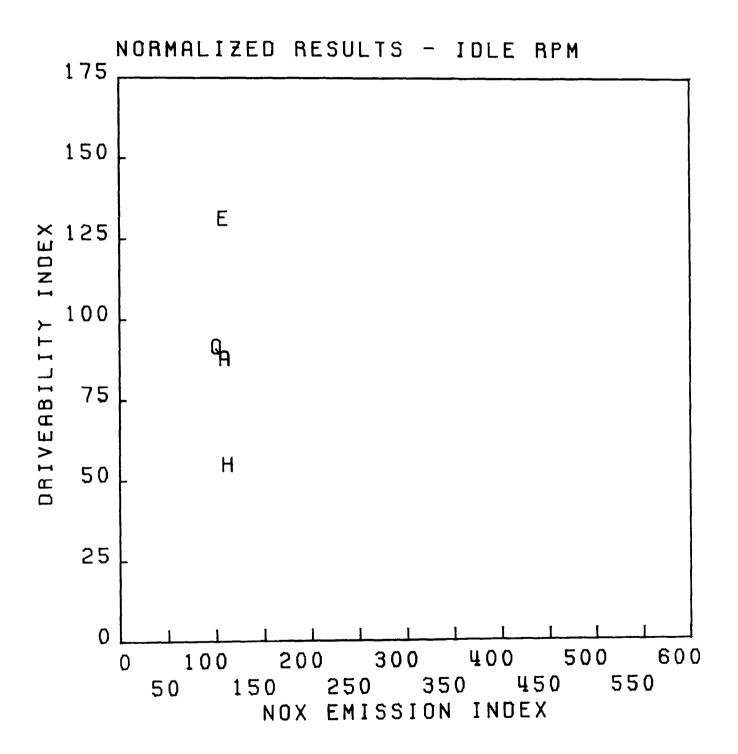


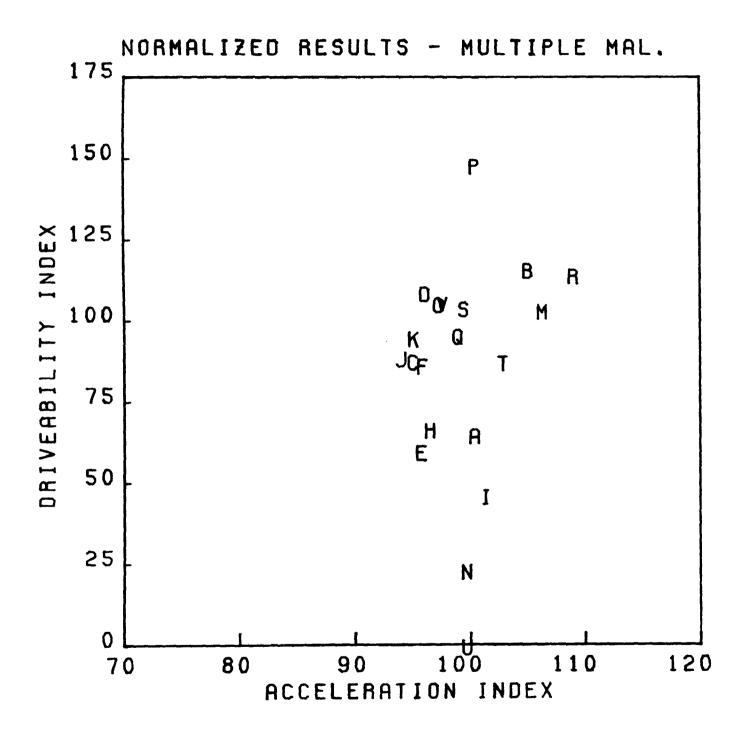


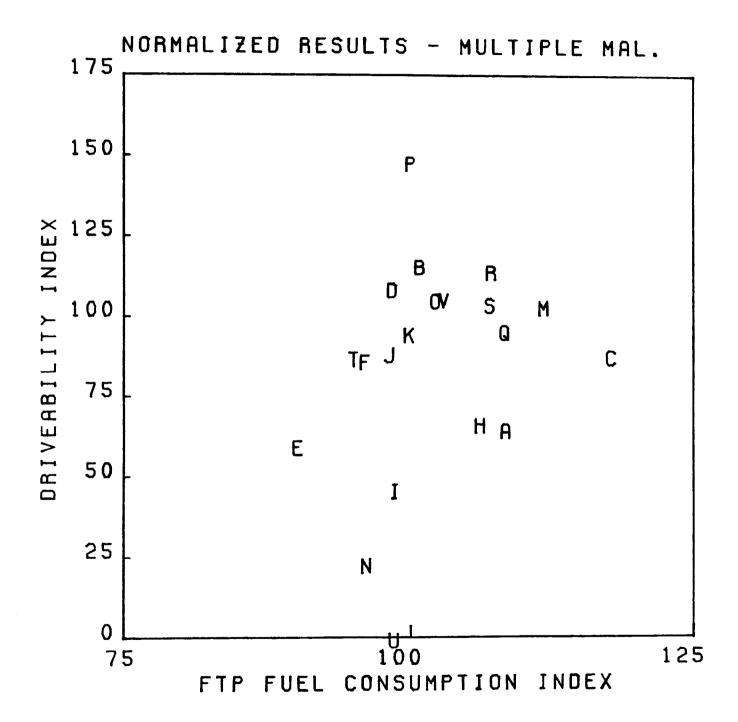


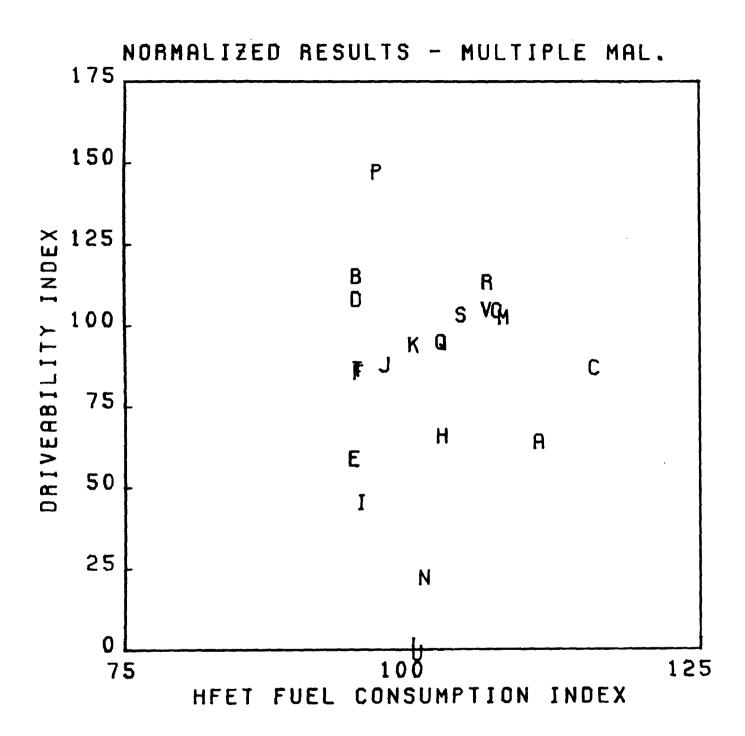


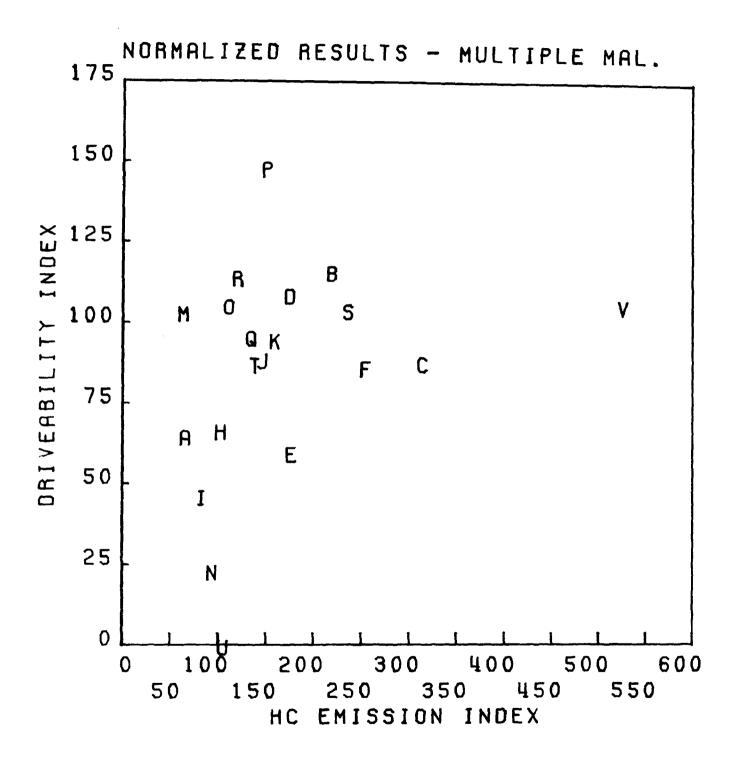


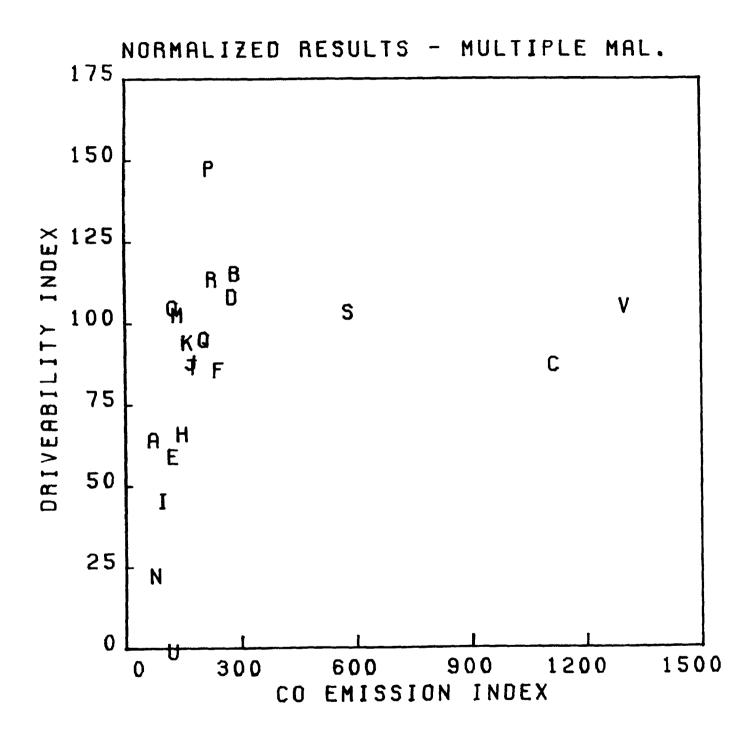


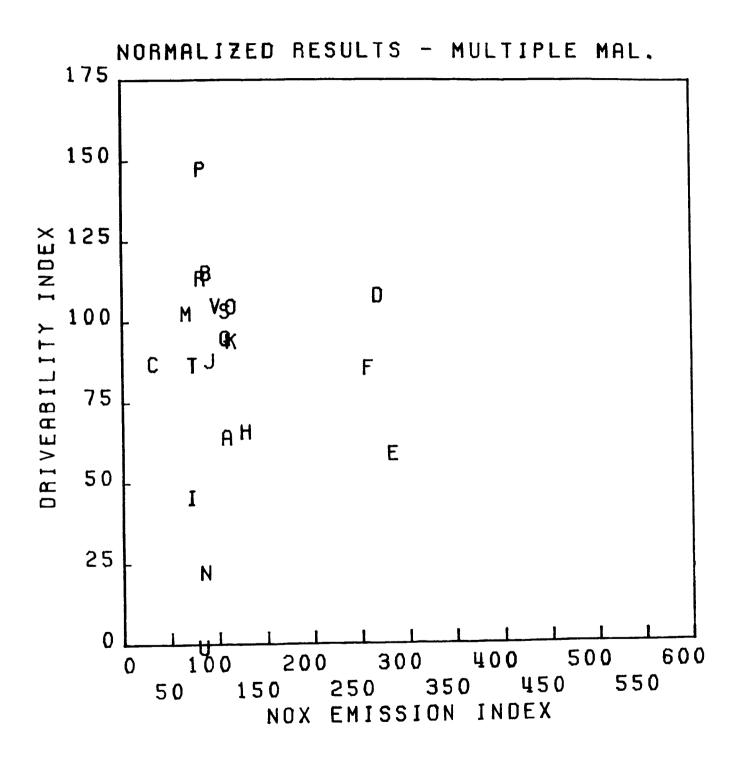












TECHNICAL REPORT DATA (Please read Instructions on the reverse before completing)			
1. REPORT NO.	2.	3. RECIPIENT'S ACCESSION NO.	
EPA-460/3-78-012			
4. TITLE AND SUBTITLE  Light Duty Vehicle Driveability Investigation		5. REPORT DATE	
		December, 1978	
		6. PERFORMING ORGANIZATION CODE	
7. AUTHOR(S)		8. PERFORMING ORGANIZATION REPORT NO.	
H. A. Toulmin, Jr.			
9. PERFORMING ORGANIZATION NAME AND ADDRESS		10. PROGRAM ELEMENT NO.	
Suntech, Inc.			
P.O. Box 1135 Marcus Hook, PA 19061		11. CONTRACT/GRANT NO.	
		68-03-2607	
12. SPONSORING AGENCY NAME AND ADDRESS		13. TYPE OF REPORT AND PERIOD COVERED	
Environmental Protection Ag	ency		
2565 Plymouth Road		14. SPONSORING AGENCY CODE	
Ann Arbor, MI 48105			

## 15. SUPPLEMENTARY NOTES

## 16 ARSTRACT

This report describes the results of an automobile driveability, emission, fuel economy and performance testing program conducted for the U.S. Environmental Protection Agency. A total of twenty-two 1977 and 1978 model vehicles were subjected to a series of tests when adjusted to the manufacturers' recommended settings and when adjusted to simulate maladjustments found on in-use vehicles in an earlier EPA Restorative Maintenance Evaluation Project. The CRC driveability tests were performed on a weather controlled large roll chassis dynamometer at 16°C and the emissions and fuel economy tests were conducted according to the 1975 Federal Test Procedure, except that evaporative emissions tests were not conducted.

17. KEY WORDS AND DOCUMENT ANALYSIS			
I. DESCRIPT	b. IDENTIFIERS/OPEN ENDED TER	MS c. COSATI Field/Group	
Driveability Exhaust Emissions Fuel Economy Acceleration Performance	Light Duty Vehicles 1975 FTP Emission Test Driveability Tests Performance Tests	ts	
18. DISTRIBUTION STATEMENT	19. SECURITY CLASS (This Report)	21. NO. OF PAGES 425	
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