

# In-Sewer Fixed Screening of Combined Sewer Overflows



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# IN-SEWER FIXED SCREENING OF COMBINED SEWER OVERFLOWS

by

Envirogenics Company
A Division of
Aerojet-General Corporation
El Monte, California

for the

ENVIRONMENTAL PROTECTION AGENCY WATER QUALITY OFFICE

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# EPA/WQO Review Notice

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#### **ABSTRACT**

A field sampling and analysis program, supplemented with laboratory studies, was conducted to characterize combined sewage contributary to combined sewer overflows, to ascertain the removal of floatables and solid materials that could be effected by the placement of screening devices in combined sewer systems, and to assess the effect of solids removal on chlorination requirements and bacterial concentrations.

Statistics are presented on combined sewage bulk and screenings collected with 0.125-, 0.25-, 0.5-, and 1.0-in. aperture screens for the following constituents (where meaningful): total solids, total volatile solids, total suspended solids, total volatile suspended solids, settleable solids, floatable solids, particle size distribution, biochemical oxygen demand, chemical oxygen demand, hexane extractable material, total coliforms, fecal coliforms, and fecal streptococci.

Regression analyses were performed between all observed combined sewage bulk and screenings constituent pairs. Statistically significant correlations at the 95-% confidence level were obtained for the combined sewage bulk only between total solids and total volatile solids, between total volatile solids and total volatile suspended solids, and between total suspended solids and total volatile suspended solids. For combined sewage screenings, statistically significant correlations at the 95-% confidence level were found between total solids and total volatile solids, between BOD and COD, between BOD and hexane extractable material, and between COD and hexane extractable material.

Removals of total solids, total volatile solids, biochemical oxygen demand, chemical oxygen demand, hexane extractable material, total coliforms, fecal coliforms, and fecal streptococci resulting from placement of the screening devices into the combined sewer were calculated and were marginal.

Fixed screening of combined sewage with aperture sizes ranging from 0.0164 to 1.0 in. appear to have little, if any, effect on total coliform and fecal coliform densities or bacterial kills by chlorination. Chlorination requirements for combined sewage subjected to fixed screening at different practical aperture sizes were reduced only slightly.

This report was submitted in fulfillment of Contract No. 14-12-180 and Program No. 11024 FKJ between the Federal Water Quality Administration and the Aerojet-General Corporation.

Key Words: Combined sewage, combined sewer overflows, combined sewage treatment, combined sewage characteristics, fixed screens, solids removal.

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#### Section I

#### CONCLUSIONS

On the basis of a field sampling and measurement program on the characterization of combined sewage from a high-density residential neighborhood in San Francisco, California, and a laboratory investigation on the effects of solids removal on chlorination practices, a number of conclusions are presented. The findings represent the analysis and evaluation of 60 combined sewage bulk samples and 60 combined sewage screenings samples retained on screens of 0.125-, 0.25-, 0.5-, and 1.0-in. aperture inserted into a sewer to intercept the total flow. Both types of samples were taken with specially designed and manufactured equipment to assure the collection of representative samples.

- 1. Removals of deoxygenating materials (chemical oxygen demand and biochemical oxygen demand), oils and greases (hexane extractable materials), and bacteria by fixed screens placed in combined sewers were marginal.
- 2. Average percentage removals of screenable constituents as a function of screen aperture size were as follows:

		Screen S	ize, in.	
Constituent	1/8	1/4	1/2	11
Total solids	2.3	1.0	1. 1	1.1
Total volatile solids	3.8	2.0	2.9	1.9
Biochemical oxygen demand	5,4	4.9	2.0	3.1
Chemical oxygen demand	5.0	5.4	1.6	2.7
Hexane extractable material	3.0	4.8	1.0	1.8
Total coliforms	4. 3	9.8	4. 2	23.1
Fecal coliforms	0.6	9.4	3.1	13.0
Fecal streptococci	2.6	26.4	2.6	35,0

- 3. Reductions in chlorine requirements to provide a chlorine residual of 1.0 mg/l after 15 minutes as a result of prior solids removal by fixed screening with what are believed to be practical apertures of 0.125 in. or greater appear small.
- 4. Screens with aperture sizes ranging from 0.0164 to 1.0 in. appear to have little, if any, effect on bacterial concentrations or bacterial kills by chlorination.

- 5. The nature of the collected visible screenings, consisting for the most part of fecal material, paper, leaves, and cigarettes, appears to be independent of screen aperture size, over a range from 0.125 to 1.0 in.
- 6. Observed qualities of the combined sewage bulk were highly variable, and had the following overall mean characteristics:

Total solids	209 mg/1
Total volatile solid	105 mg/l
Total suspended solids	67.6 mg/l
Total volatile suspended solids	52.2 mg/1
Settleable solids	2.58 ml/1
Floatable solids	3.89 mg/1
Biochemical oxygen demand	49 mg/1
Chemical oxygen demand	155 mg/1
Hexane extractable material	12.3 mg/1
Total coliforms	8. $32 \times 10^{\frac{5}{2}} \log MPN/100 ml$
Fecal coliforms	$1.55 \times 10^{5} \log MPN/100 ml$
Fecal streptococci	2.09x10 <sup>4</sup> log MPN/100 ml

7. Overall average qualities of the combined sewage screenings were only slightly less variable than the bulk characteristics, and were as follows:

Total solids	21.3 g
Total volatile solid	18.8 g
Biochemical oxygen demand	484 mg/g
Chemical oxygen demand	1940 mg/g
Hexane extractable material	90.5 mg/g
Total coliforms	$3.55 \times 10^8 \log MPN/g$
Fecal coliforms	$4.67 \times 10^7 \log MPN/g$
Fecal streptococci	$9.55 \times 10^6 \log MPN/g$

8. For combined sewage bulk, statistically significant correlations at the 95-% confidence level were observed between total solids and total volatile solids, between total volatile solids and total volatile

suspended solids, and between total suspended solids and total volatile suspended solids. (Relations are given in Table 8, page 35.)

- 9. For combined sewage screenings, statistically significant correlations at the 95-% confidence level were found between total solids and total volatile solids, between biochemical oxygen demand and chemical oxygen demand, between biochemical oxygen demand and hexane extractable material, and between chemical oxygen demand and hexane extractable material. (Relations are given in Table 9, page 39.)
- 10. No statistically significant correlation at the 95-% confidence level was found between the storm flow at the sampling site and the precipitation recorded at an official weather station two miles distant.

#### Section II

#### INTRODUCTION

A major threat to the maintenance of a clean and enjoyable environment in many parts of the United States is the overflow from combined sewer systems to receiving waters during periods of moderate and heavy rainfall. In most instances much of the sanitary sewage contained in these sewers is discharged without treatment to natural water courses, resulting in unacceptably high pollutant loadings of floatable and settleable materials, oxygen-consuming substances, and pathogens.

Many methods of alleviating this pollution have been proposed, including total containment of combined sewer flows for later processing at sewage treatment facilities during low-flow periods, partial and complete treatment of combined sewer overflows at the bypass outfall, and complete separation of storm runoff and municipal sewage by reconstruction.

Because of the diluted state of the pollutants in the combined sewage and the highly intermittent nature of the flows, conventional treatment by sedimentation and biological degradation is extremely difficult to effect. Processes that would appear applicable to the severe operating conditions imposed by combined sewer flows are solids separation and disinfection. To provide a preliminary assessment of the possible effectiveness and benefits of solids separation methods, the character and quantity of solids contained in combined sewage, the pollutional aspects associated with the solids as a function of particle size, and the effect of these solids on disinfection practices must be established.

#### **OBJECTIVES**

The primary purpose of this program was the conduct of a sampling and analysis program to characterize combined sewage contributary to combined sewer overflows, to ascertain the removal of floatables and solid materials that could be effected by the placement of screening devices in combined sewer systems, and to assess the effect of solids removal on chlorination requirements and bacterial densities.

#### SCOPE

To provide an assessment of the effectiveness and benefits of solids separation methods, the character and quantity of solids contained in combined sewage and the pollution aspects associated with the solids as a function of particle size was established. A program was initiated to ascertain the characteristics of combined sewage that would be of significance with respect to solids separation. The sampling methods

provided for the determination of gross particle size distribution by screens in situ; thus the actual effects of screening on particle coalescence and disintegration, solids separation and retention, and flow disturbance were integrated into the results. Special sampling equipment was designed, constructed, and installed in the sampling manhole to meet these objectives.

A study site was selected in the City and County of San Francisco that was typical for both sanitary flow and storm runoff for a high-density residential urban neighborhood. The selected tributary runoff area was characterized as to type, size of drainage area tributary to the sampling manhole, number of domestic sewer connections, land use, topography, and number of street inlets or catch basins. Precipitation data for the area were collated for the period encompassing the sampling period and the preceding three months.

The sampling was conducted to permit the establishment of the concentrations of constituents in each fraction of combined sewage as a function of time and flow condition in the sewer and other factors such as intensity and duration of contributary rainfall. Two sample fractions, screenings and bulk liquid, were collected hourly for five consecutive hours during each separate rainfall event commencing near the start of the first significant rainfall. One size only of four screen sizes, 0.125-, 0.25-, 0.5-, and 1-in. aperture, was employed during each rainfall event. At the conclusion of each rainfall event five samples each of screenings and bulk liquid were collected for laboratory analysis. The foregoing sampling sequence was conducted on twelve separate occasions using each of the four screen sizes during three rainfall events.

Dry-weather flow was measured at the selected manhole for a period of 24 hours on a 2-hour interval basis.

Investigations were conducted on the effect of solids removal on chlorination requirements and bacteria reductions resulting from chlorination.

#### Section III

#### STUDY AREA

The study area is located in the northwest portion of the City and County of San Francisco, and is shown in Figure 1. It is exclusively residential consisting of predominantly two- and three-story structures which occupy the major portion of each lot. There is, however, a moderate degree of unoccupied area which has been landscaped with trees, shrubs, and lawns. The characteristics of surface runoff from this area are believed fairly typical of high-density, high-income residential neighborhoods.

The study area extends easterly along Jackson Street at a block or less width from Cherry Street to a point approximately 300 feet east of Spruce Street. A detailed map of the study area is presented in Figure 2. The total gross area tributary to the sampling and measuring station is 7.65 acres.

Topography of this section of San Francisco can be classified as rolling. The study area is located on the side of a hill with slopes ranging from gentle to moderately steep. Surface elevations based on San Francisco datum vary from a low of 209 feet at the sampling point to a maximum of 282 feet at the intersection of Washington Street and Maple Street.

The street and sidewalk areas tributary to the system are easily defined by the topography, as are the catch basin locations at the various intersections. Determination of the off-street areas contributing runoff was somewhat more difficult because detailed topographic surveys are not available; however, all roof drains are connected to the sewer system as required by City ordinance and the remaining off-street areas are relatively small. The nature and extent of surface types within the drainage area are shown in Table 1.

Table 1
SURFACE CHARACTER OF STUDY AREA

Surface Type	Area, acres	Portion, %
Roof	2,52	33
Street	1.60	21
Sidewalk	1.24	16
Yards & landscaping	2. 29	_30_
Total	7.65	100

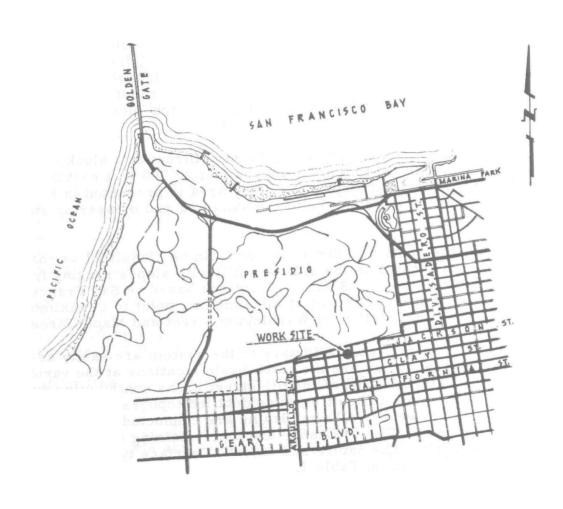


Figure 1. STUDY AREA LOCATION

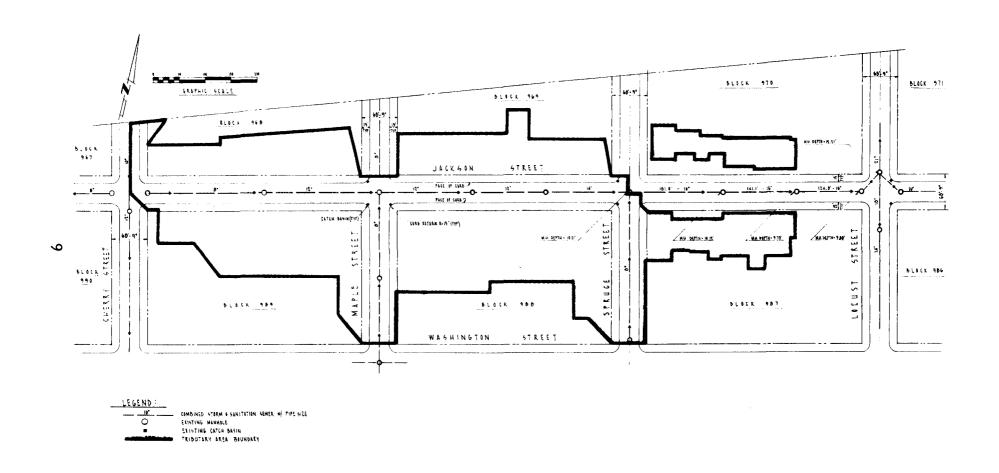


Figure 2. SAMPLING SITE AND TRIBUTARY AREA

San Francisco is situated in the Coast Range of mountains, which has an extreme influence on the climatic conditions of the City. The average annual rainfall for the area is 20.78 inches. Average monthly extremes range from approximately four inches occurring in December and January to one-hundreth of an inch in July.

The structures in the study area consist of 47 single-family residences; two apartment buildings containing a total of 16 living units, and one foreign embassy.

In estimating the population of the area, it was assumed that there are five persons per single-family residence, three persons per apartment unit, and that the embassy staff consists of five persons. On this basis, the total estimated population would be 288 persons in the tributary area distributed as follows: single family residence, 235; apartment unit, 48; and embassy, 5.

The 1960 census gave a population density of 60 persons per net acre and 41 persons per gross acre for the census tract in which the study area is located. Based on these densities, the population in the study area would be 314 on a gross acreage basis and 287 on a net acreage basis.

The contributary population is therefore estimated to be 300 persons.

Sewer grades follow the surface topography and vary from a minimum slope of 1.21% in Jackson Street upstream of the sampling station to a maximum of 21.54% in Spruce Street between Washington and Jackson Streets. The size, location, and slopes of the various collector sewers are shown in Figure 2.

The number of house connections to the tributary area is placed at fifty.

During periods of rainfall, surface runoff from streets, sidewalks, and landscaped areas are intercepted by the street gutters and conveyed to catch basins located at each intersection. Within the study area there are a total of six catch basins which drain on the average about three-quarters of an acre. Individual areas are presented in Table 2.

Detail of a typical catch basin with curb inlet is shown in Figure 3.

Of the total area approximately 59% is drained by catch basins and 41% by various house connections including roof drainage. On a flow basis, assuming 10-% runoff for landscaped areas and 100% for all other surfaces, the contribution of runoff waters would be approximately 54% for catch basins and 46% for house connections.

Table 2
TRIBUTARY AREAS OF CATCH BASINS

	Approximate
Location	Tributary Area, acres
NW Corner of Jackson & Maple	0.69
SW Corner of Jackson & Maple	1.36
SE Corner of Jackson & Maple	0.23
NW Corner of Jackson & Spruce	0.66
SW Corner of Jackson & Spruce	1. 29
SE Corner of Jackson & Spruce	0, 23

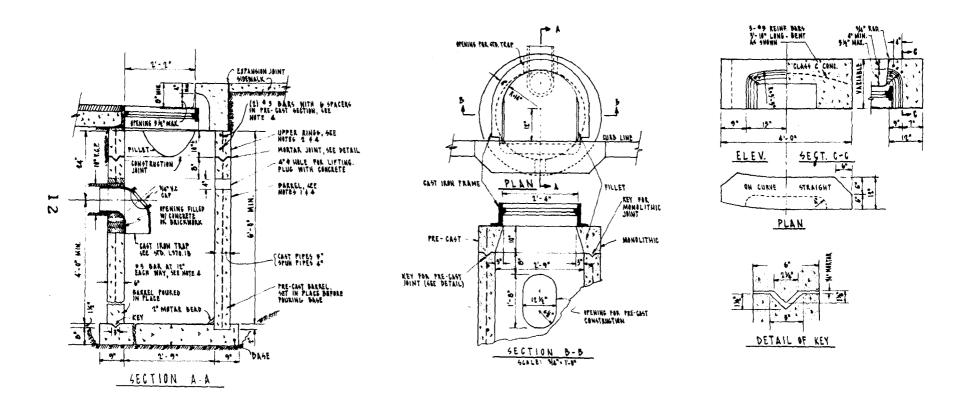


Figure 3. TYPICAL CATCH BASIN WITH CURB INLET

#### Section IV

#### METHODOLOGY

A sampling and analysis program was prepared that provided a characterization of combined sewage contributary to combined sewer overflows and the effect that solids removal by the placement of screening devices in combined sewer systems would have on the abatement of receiving water pollution and on chlorination practices.

#### SAMPLING DEVICES

Special sampling equipment and supporting structure were designed and manufactured by the Envirogenics Company, a Division of Aerojet-General Corporation, to assure representative collection of combined sewage samples. The equipment consisted of two types of samplers—a bulk liquid sampler and a screenings sampler. Both employed the same support structure and the same sampling station manhole. The supporting structure was installed and maintained in the manhole throughout the duration of the sampling program, and consisted of two vertical guide channels situated near the center of the manhole on the shelf edges and secured by braces to the manhole wall. Each sampler was placed by hand and removed by winch.

The sampling devices were designed for a 12-in. diameter sewer, which was initially chosen as the sampling manhole but was subsequently abandoned since it constituted a junction which proved infeasible for sampling. The sampling site was relocated to a nonjunction manhole situated on a 15-in. diameter sewer which did not represent a transition for different upstream and downstream pipe inverts. The channel, however, through the manhole was 16 in. in diameter which required the design and manufacture of a suitable metal channel to compensate for the size differential between sampler and manhole channel.

Structural details of the supporting structure and manhole modifications are shown in Figure 4. Photographs of the installation are shown in Figure 5.

#### Bulk Sampler

Bulk liquid samples were collected with a sampler which allowed the removal of an entire 1-ft long section of combined sewage flow in the sewer. Figure 6 is a photograph of the bulk sampler. Fabrication drawings are provided in Appendix A. The bulk sampler consists of a thin-shell section containing hinged covers at both ends which are mechanically connected to function integrally. The sampler was inserted in the sewer with the covers in the up or open position allowing the combined sewage to

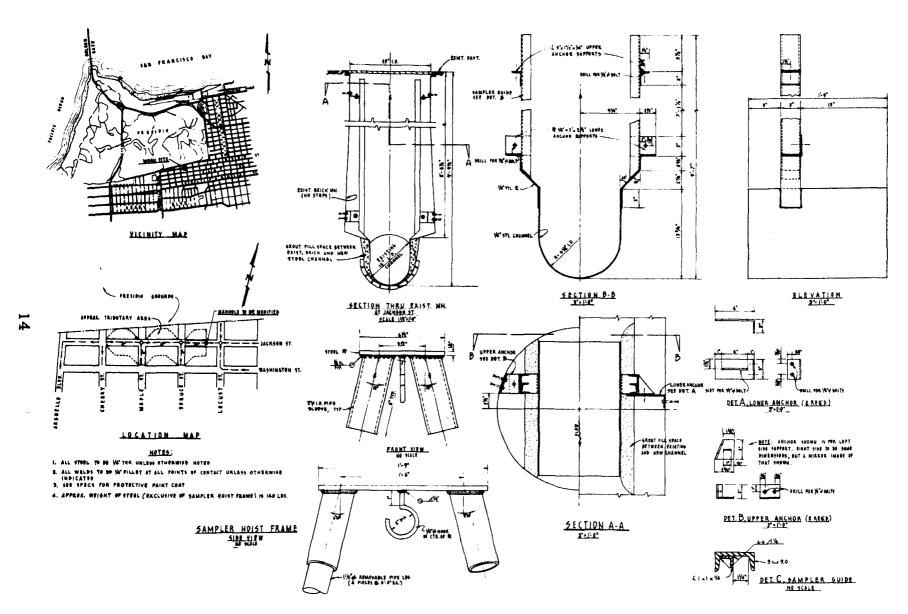


Figure 4. SAMPLER SUPPORTING STRUCTURE AND MANHOLE MODIFICATIONS









Figure 5. INSTALLATION OF SHEET METAL CHANNEL AND GUIDES FOR SAMPLING EQUIPMENT

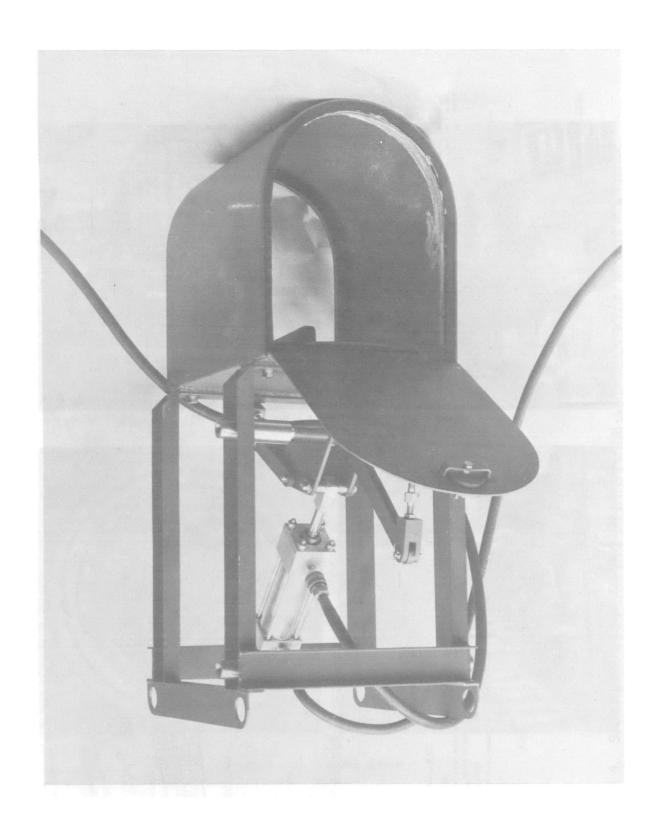


Figure 6. COMBINED SEWAGE BULK SAMPLER

flow through the section reasonably undisturbed. A liquid sample was captured by actuating an air cylinder which released the covers and trapped a plug of combined sewage inside the sampler. The air cylinder also maintained the covers in a closed position and assured maximum sealing pressure during removal of the sampler and sample from the sewer. The seal, cemented to the covers, consisted of a large spongy closed-cell neoprene that provided negligible leakage during transport from the manhole.

#### Screenings Sampler

The screenings samplers consist of a stainless steel basket made in each of four screen sizes--0.125-, 0.25-, 0.5-, and 1-in. aperture. A photograph of the 0.5-in. screening sampler is shown in Figure 7. Fabrication drawings are presented in Appendix B.

#### SAMPLING AND FLOW MEASUREMENTS

Both screenings and bulk samples were collected hourly for five consecutive hours during each of twelve rainfall events commencing as nearly as practical at the start of the first significant precipitation associated with the rainfall event. At the commencement of each wetweather sampling episode, a bulk sample was collected and a screen was inserted for a recorded period of one-half hour or less depending upon the clogging rate of the particular screen. On the second, third, fourth, and fifth hour after commencement, the same sampling sequence was followed using the same screen size throughout the entire 5-hour sampling episode. At the conclusion of each rainfall event, five samples each of screenings and bulk therefore had been collected for laboratory analysis.

The wet-weather sampling sequence was conducted on twelve separate occasions using each of the four screen sizes for three separate rainfall events.

During the single dry-weather monitoring period, only flow measurements were taken over a 24-hour period at 2-hour intervals.

The combined sewage flow at the sampling site was determined just prior to and just after the collection of screenings samples.

Flow measurements were accomplished by using the continuous tracer dilution technique. The tracer rhodamine WT was injected at a controlled rate into a manhole approximately 480 feet upstream of the sampling manhole, which provided a minimum travel time of four minutes between injection and collection of diluted dye for subsequent measurement in the laboratory.

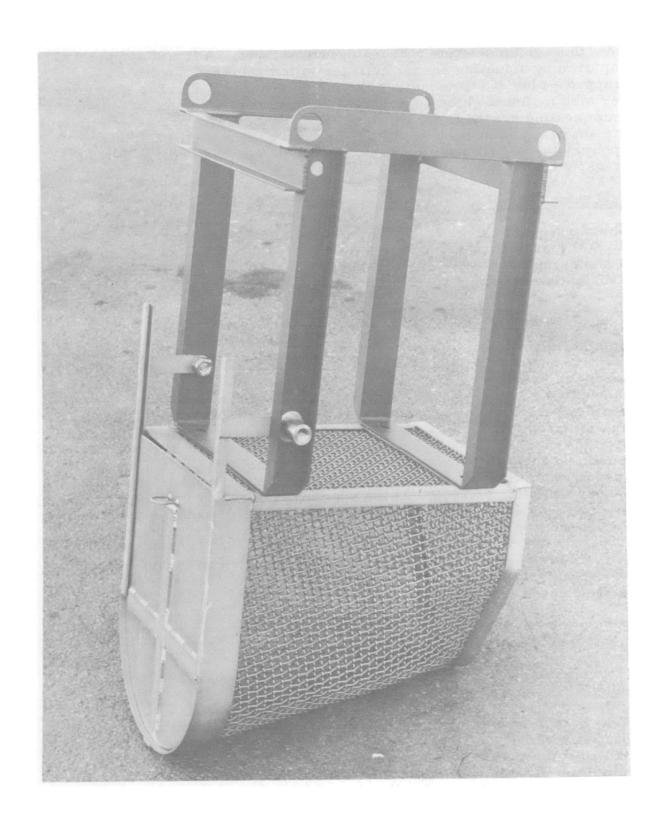


Figure 7. COMBINED SEWAGE SCREENINGS SAMPLER

#### ANALYSES

Physical, chemical, and biological analyses of collected combined sewage bulk and screenings samples were performed in accordance with the schedule presented in Table 3, and the Twelfth Edition of Standard Methods for the Examination of Water and Wastewater, except where noted otherwise. The character of the collected screenings samples were also described from visual observations.

#### CHLORINATION STUDIES

A sufficiently large composite bulk sample was withdrawn prior to a normal screen sampling period in the ongoing basic storm sampling program. Bulk samples, consisting of one or more grab storm samples made with the bulk sampler, were taken for laboratory studies to determine the effects of screening on chlorination practices. A small portion of the sample was withdrawn and split for establishing the breakpoint chlorination curve for 15-minute contact and the dosage required to provide a chlorine residual of 1.0 mg/l after 15-minute contact, and the total and fecal coliform densities before and after the required dosage of chlorine for this sample to provide a chlorine residual of 1.0 mg/l after 15-minute contact time. A characterization of the solids was performed on a portion of this sample.

The entire remaining composite bulk sample was passed through a 1-in. aperture screen. Again a small sample was withdrawn for analysis for the same chlorine, total and fecal coliforms, and solids determinations. The remaining composite bulk sample was successively filtered through Tyler screens or equivalent of 0.5 in., 0.263 in. (3 mesh), 0.131 in. (6 mesh), 0.065 in. (10 mesh), 0.0328 in. (20 mesh), and 0.0164 in. (35 mesh). After each screening the required analyses were performed on a portion of the remaining bulk sample.

Table 3

COMBINED SEWAGE ANALYSIS SCHEDULE

Sample			
Analysis	Bulk	Screenings	Method
Total solids	x	x	Sample aliquot brought to dryness at 103°C, and weighed
Total volatile solids	x	x	Total solids sample fired at 550°C for 15 minutes
Total suspended solids	×		Sample aliquot passed through 0.45-\mu glass filter, brought to dryness at 103°C, and weighed
Total volatile suspended solids	x		Total suspended solids sample fired at 550°C for 15 minutes
Settleable solids (by volume)	x		Standard Methods, p. 425
Floatable material	x		Floatable material concentrated on the surface of aliquot sample in 3-liter Teflon-coated flotation funnel, collected, washed and weighed
Biochemical oxygen demand	x	x	5-day, 20°C BOD, Standard Methods, p. 415
Chemical oxygen demand	x	x	Standard Methods, p. 510
Hexane extractable material (oil & grease)	x	x	Liquid-liquid extraction using Pearson- Thomas extractor. Soxhlet extrac- tion of dry material, Standard Methods, p. 384

Table 3 (continued)

COMBINED SEWAGE ANALYSIS SCHEDULE

		Sa	mple	
	Analysis	Bulk	Screenings	Method
	Total coliforms	x	x	Multiple (3) Tube MPN determination using lactose broth for presumptive test and brilliant green bile broth for confirmed test, Standard Methods, p. 596
21	Fecal coliforms	<b>x</b>	x	Multiple (3) Tube MPN determination using E-C medium and elevated temperature test, Standard Methods, p. 599
	Fecal streptococci	x	x	Multiple (3) tube MPN determination using azide dextrose broth for confirmative test, Standard Methods, p. 620
	Particle size distribution	x	x	Aliquot serially passed through standard sieves, Nos. 6, 18, 50, and 200, with 100 ml of fecal filtrate passed through a GF/C Glass fiber filter. Residues dried at 103°C and weighed

#### Section V

### SEWAGE CHARACTERIZATION

Combined sewage characteristics were observed at the Jackson Street sampling site on twelve separate occasions during the wet-weather seasons of 1968-1969 and 1969-1970. Dry-weather flows were measured at the sampling manhole over a continuous 24-hour period on 24-25 April 1969 to establish background sanitary flow rates.

The first sampling episode occurred on 4-5 April 1969 and was the only one conducted during the 1968-1969 rainy season, which produced an above average (20.78 in.) seasonal precipitation amounting to 25.09 inches. The remaining eleven sampling episodes occurred on 5 November 1969, 19 December 1969, 21 December 1969, 13 January 1970, 20 January 1970, 27 January 1970, 13 February 1970, 28 February 1970, 4 March 1970, 13 April 1970, and 13 May 1970. This wet-weather season resulted in a total precipitation of 20.80 inches, which was very nearly an average wet-weather season.

A summary of rainfall characteristics associated with the twelve wetweather sampling episodes is presented in Table 4. The largest total amount of continuous precipitation, 2.31 inches, occurred during a 29-hour period on 20-21 January 1970. The maximum recorded intensity of that single storm was 0.25 in./hr, which occurred during the same hour that the combined sewage sampling commenced. For the twelve single continuous rainfall events occurring during the wet-weather sampling episodes, the maximum rainfall intensity of 0.39 in./hr was reported two hours prior to commencement of sampling on 4 March 1970.

The last two sampling episodes were conducted during periods of very light rainfall and most likely represent conditions more typical of dryweather flow than wet-weather flow. Therefore results from the last two sampling episodes have been excluded from the analysis in some instances, which are noted by "10 storms," so as not to bias the correlations and evaluations.

Local climatological data for the Federal Office Building during the period extending from January 1969 to June 1970 are given in Appendix C. Rainfall intensity-duration-frequency relations for San Francisco are provided in Appendix D.

#### SEWAGE FLOWS

The temporal distributions of the observed sewage flows in the sampling manhole on Jackson Street and the recorded precipitation at the Federal Office Building on Fulton Street about two miles easterly are shown in Figure 8.

Table 4
SUMMARY OF PRECIPITATION AT FEDERAL OFFICE BUILDING
ASSOCIATED WITH WET-WEATHER MEASUREMENT

	Date	Day	Continuous Total Rainfall in.	Maximum Intensity in./hr	Duration of Storm hr	Antecedent Dry Period hr
	4 Apr 69	Fri	0.51	0.12	13	25
	5 Nov 69	Wed	0.38	0.10	7	461
24	19 Dec 69	Fri	0,51	0.11	12	7
	21 Dec 69	Sun	0.66	0.18	9	21
	13 Jan 70	Tue	0.23	0.07	11	28
	20 Jan 70	Tue	2, 31	0, 25	24	15
	27 Jan 70	Tue	0.49	0.29	4	2
	13 Feb 70	Fri	0.09	0.04	4	12
	28 Feb 70	Sat	0.43	0.10	11	4
	4 Mar 70	Wed	1.17	0.39	9	15
	13 Apr 70	Mon	0.01	0.01	5	718
	13 May 70	Wed	0.03	0.01	3	9

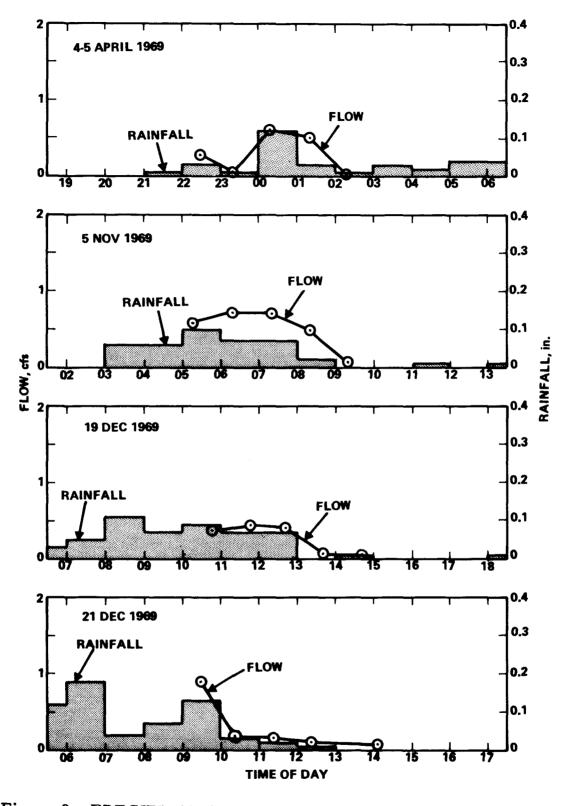


Figure 8. PRECIPITATION AT SAN FRANCISCO FEDERAL OFFICE BUILDING AND COMBINED SEWAGE FLOW AT JACKSON STREET SAMPLING SITE

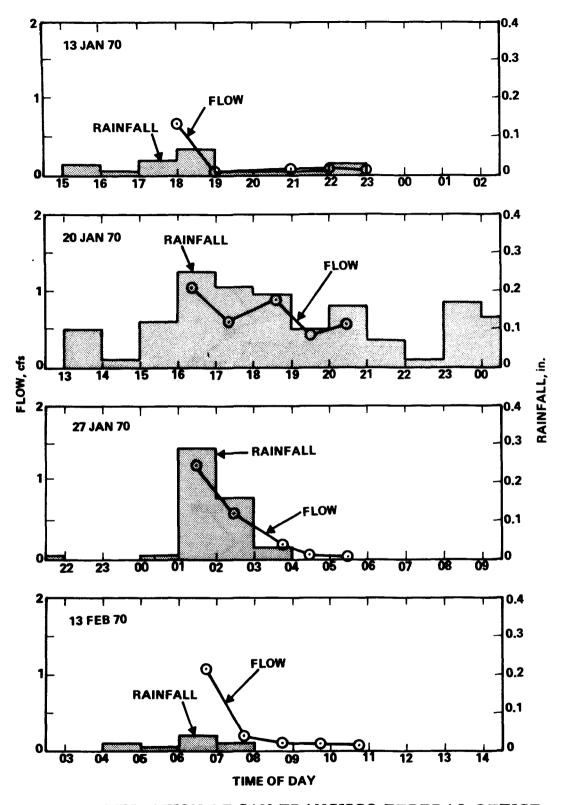


Figure 8. PRECIPITATION AT SAN FRANCISCO FEDERAL OFFICE BUILDING AND COMBINED SEWAGE FLOW AT JACKSON STREET SAMPLING SITE (Continued)

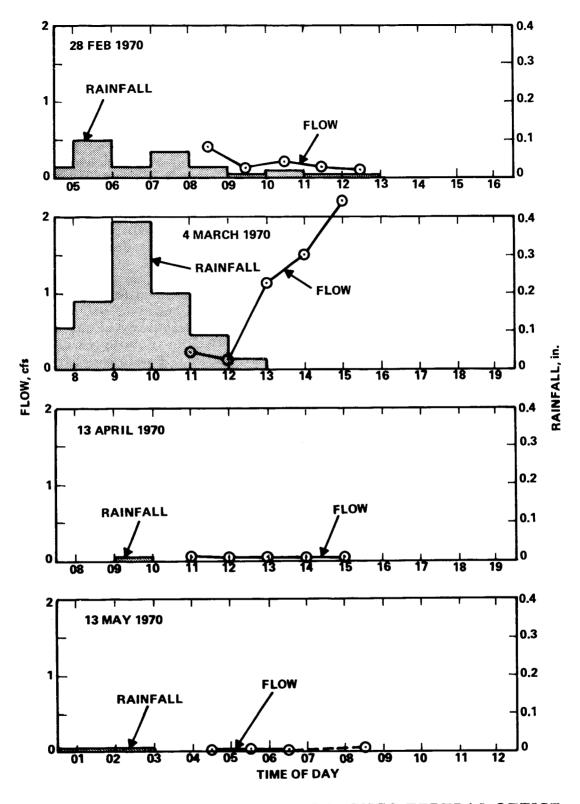


Figure 8. PRECIPITATION AT SAN FRANCISCO FEDERAL OFFICE BUILDING AND COMBINED SEWAGE FLOW AT JACKSON STREET SAMPLING SITE (Continued)

A wide range of combined sewer flow rates were observed representing every hour of the day and night. Extreme combined sewer flows in the 15-in. diameter sewer were a low of 0.022 cfs and a high of 2.22 cfs. The largest variation in flow occurring during any 5-hour sampling episode was a 30-fold decrease from 1.23 to 0.039 cfs. The largest hourly variation was a 9-fold increase from 0.124 to 1.13 cfs.

Averages of the five hourly combined sewer flows observed during each of the twelve sampling episodes were, chronologically, 0.299, 0.516, 0.271, 0.286, 0.202, 0.707, 0.421, 0.309, 0.213, 1.043, 0.058, and 0.036 cfs. All but the last two sampling episodes were conducted during periods where the combined sewer flows contained sizable storm runoff fractions, since for the dry-weather flow the maximum consecutive 5-hour average of observed flows was 0.068 cfs and the daily average was 0.041 cfs.

The dry-weather sewage flow observed at the Jackson Street sampling manhole is presented in Figure 9. Because the hourly flow values were quite variable as one would expect for a small tributary area, the data were smoothed utilizing polynominal curve-fitting techniques and are best represented by the segmented curve shown. From the curve, the average hourly sanitary sewage flow was 0.0423 cfs. The peak hourly flow of 0.103 cfs occurred at 0800 hours and was 243% of the average flow. Minimum flow occurred at 0400 hours and at 0.0080 cfs was 19% of the average. A second peak of 0.049 cfs occurred at 2000 hours and another of 0.045 cfs at midnight.

Regression analyses, summarized in Table 5, revealed no significant correlation at the 95-% confidence level between the calculated storm flow (observed combined flow less the appropriate sanitary sewage flow from the curve of Figure 9) and the reported rainfall upon either advancement or retardation of time to compensate for the distance between the two observation points. The best relation was obtained, however, when the corresponding time of rainfall occurrence to storm runoff flow was increased by one hour, indicating that rainfall occurred on the average at the combined sewage sampling site perhaps one hour before it occurred at the weather recording station. In general this time shift would be expected since most of the weather in the area moves in easterly from the Pacific Ocean.

Due to the poor temporal correlation between the calculated storm flows and the available rainfall intensity, it is difficult to ascertain what relation, if any, existed between the intensity and duration noted at the Federal Office Building two miles distant and that occurring in the study area contributing to surface runoff and subsequent combined sewer flows.

The field sampling activities for the most part were initiated by an observer at the North Point Sewage Treatment Plant, which serves the study area, upon the first sign of combined sewer overflows from the sewer system.

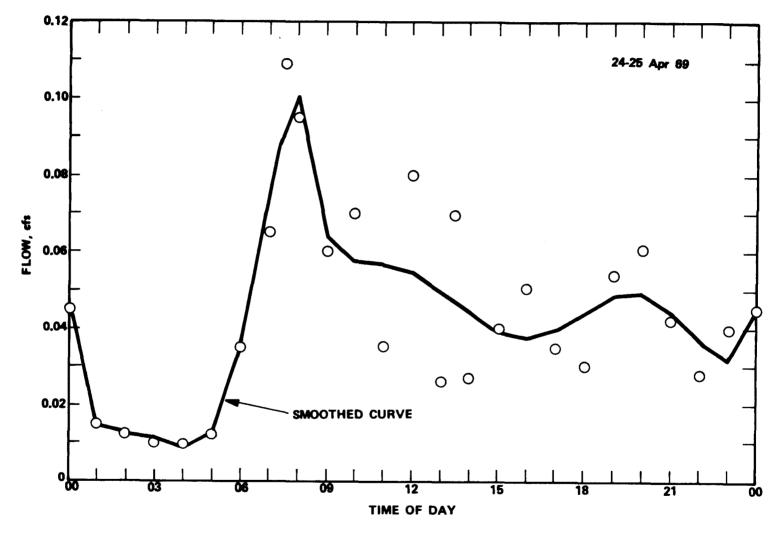


Figure 9. DIURNAL DISTRIBUTION OF DRY-WEATHER SEWAGE FLOW AT JACKSON STREET SAMPLING SITE

Table 5

CORRELATIONS BETWEEN PRECIPITATION AT FEDERAL OFFICE BUILDING
AND CALCULATED STORM RUNOFF FLOW AT SEWAGE SAMPLING LOCATION
10 Storms

				Equat	ion	No.	Signific	ance	
	$\mathbf{X}_{\downarrow}$	Y	Form <sup>a</sup>	Coefficient A	Coefficient B	Correlation Coefficient	of Data	Equation Coefficient <sup>b</sup>	Correlation Coefficient <sup>C</sup>
	Rain_2hr	Flow	1	0.304	1.17	0.217	48	No	No
30	Rain-lhr	Flow	5	18,5	-35, 8	0.127	48	No	No
	Rain	Flow	5	22.1	-87.8	0.311	48	Yes	No
	Rain <sub>+lhr</sub>	Flow	2	0.0889	11.3	0.558	48	Yes	No
	Rain <sub>+2hr</sub>	Flow	2	0.126	9.03	0.326	48	Yes	No

 $a_{1. Y=A+B; 2. Y=A \exp (BX); 3. Y=AX^B; 4. Y=A+(B/X); 5. Y=1/(A+BX); 6. Y=X/(A+BX)}$ 

<sup>&</sup>lt;sup>b</sup>F-statistic significant at the 95-% confidence level

 $<sup>^{\</sup>rm c}$   $\chi^2$ -statistic significant at the 95-% confidence level

#### SEWAGE QUALITY

Complete detailed physical, chemical, and biological analyses of combined sewage bulk samples collected from the Jackson Street manhole are presented in Appendix E.

Average combined sewage bulk statistics observed for the 10 storms are presented in Table 6. In all characteristics the observations, as expected, were highly variable, with the values of the standard deviations nearly as large or larger than the values of the means.

Results of particle size distribution analyses indicates that the "size" of solids contained in the combined sewage were for the most part extremely small. The average median size, which represents the size in the particle distribution which has one-half the total weight of particles above and one-half below that size, was 0.0068 in. Moreover 64% of all bulk samples analyzed for particle size distribution passed completely through a 0.131-in. aperture screen, with no solids retained.

The overall average quality of the screenings collected with all sizes of screens from the combined sewage flow during the 10 storms is presented in Table 7. In comparison to the bulk, the observed physical and chemical characteristics of the screenings were less variable, and the bacterial concentrations were somewhat more variable.

Complete detailed analyses of the physical, chemical, and biological characteristics of the combined sewage screenings collected from the Jackson Street manhole are provided in Appendix F.

## SEWAGE CONSTITUENT CORRELATIONS

Least-squares regression analyses were performed to determine whether statistically significant relationships exist between any pair of combined sewage constituents. Data pairs were assumed to be related by one of six equation forms, which were utilized to ascertain the best correlation. The significance of the resulting correlation was tested at the 95-% confidence level for two conditions. The first check was an F-test (Ref. 1), which tests the hypothesis that the slope of the regression is significantly different from zero. If so, it is assumed, at the selected level of confidence, that the pair of variables are correlated. For example, one constituent concentration increases as the other increases. The hypothesis is accepted if the calculated F is larger than the tabulated F at the selected level of confidence, or in this case  $F > F_{0.95}$ . The value of F is  $\rho^2 (N-2)/(1-\rho^2)$ , where  $\rho$  is the correlation coefficient and N is the number of data points or observations. The degrees of freedom for this test is N-2.

The second, and much more powerful, test was a  $x^2$ -test, which tests the confidence with which the equation can predict one variable given

Table 6

COMBINED SEWAGE BULK QUALITY CHARACTERISTICS
10 Storms

Constituent	Mean	Range	Standard Deviation	No. of Data
Total solids, mg/l	209	44-575	138	50
Total volatile solids, mg/l	105	16-420	87,5	50
Total suspended solids, mg/l	67.6	4-426	80	50
Total volatile suspended solids, mg/l	52.2	4-373	69.7	50
Settleable solids, ml/l	2.58	0.05-14	3, 22	45
Floatable solids, mg/l	3, 89	0.6-22.3	3, 58	45
Biochemical oxygen demand, mg/l	49	<1.5-202	57, 2	47
Chemical oxygen demand, mg/l	155	16.9-626	132	50
Hexane extractable material, mg/l	12.3	1. 3-54. 4	12.9	50
Total coliforms, MPN/100ml	2.88×10 <sup>6</sup>	$2.3 \times 10^{4} - 1.6 \times 10^{7}$	3.98×10 <sup>6</sup>	46
, log MPN/100ml	8.32×10 <sup>5</sup>			46
Fecal coliforms, MPN/100ml	$6.40 \times 10^{5}$	$<3\times10^{3}$ ->1. $1\times10^{7}$	1.09x10 <sup>6</sup>	43
, log MPN/100ml	1.55×10 <sup>5</sup>			43
Fecal streptococci, MPN/100ml	1.29×10 <sup>5</sup>	$<30-2.4\times10^6$	$3.93 \times 10^{5}$	39
, log MPN/100m1	$2.09 \times 10^4$			39

Constitue	nt	Mean	Range	Standard Deviation	No. of Data
Total solids, g		21.3	5-77	14	50
Total volatile solids,	g	18.8	4.6-64.5	12	50
Biochemical oxygen de	emand, mg/g	484	1.2-1,898	369	49
Chemical oxygen dema	and, mg/g	1,940	9.7-5,490	1,577	50
Hexane extractable ma	aterial, mg/g	90.5	0.42-286	60.5	49
Total coliforms, MPN	7/g	$2.15 \times 10^9$	$<5.79 \times 10^5 - 2.8 \times 10^{10}$	4.85×10 <sup>9</sup>	49
, log N	ΛPN/g	3.55x10 <sup>8</sup>			49
Fecal coliforms, MPN	1/g	$3.34 \times 10^{8}$	$<3.6 \times 10^4 - 1.16 \times 10^{10}$	1.87x10 <sup>9</sup>	41
, log l	MPN/g	$4.67 \times 10^{7}$		_	41
Fecal streptococci, M	PN/g	$7.04 \times 10^{7}$	$<2.4\times10^3$ -6.31 $\times10^8$	1.37 <b>x</b> 10 <sup>8</sup>	42
, lo	g MPN/g	9.55x10 <sup>6</sup>			42

the other. The hypothesis for this test is that the explained variance is greater than the product of the residual variance and the value of  $x^2$  at the selected level of confidence, or  $\sigma_E^2 > \chi_{0.95}^2 \sigma_R^2$ . The appropriate degrees of freedom for this test is one. Whereas many correlations passed the F-test, many failed the  $\chi^2$ -test.

Summarizing, the test for correlation (F-test) indicates whether or not it can be assumed that a change in the independent variable will cause a change in the dependent variable. The  $\chi^2$ -test indicates how accurately this change can be predicted.

## Combined Sewage Bulk

Regressions were performed between all of the observed combined sewage bulk constituent concentrations, consisting of total solids (TS), total volatile solids (TVS), total suspended solids (TSS), total volatile suspended solids (TVSS), settleable solids (SS), floatable solids (F), biochemical oxygen demand (BOD), chemical oxygen demand (COD), hexane extractable material (HEM), total coliforms (TC), fecal coliforms (FC), and fecal streptococci (FS). Summaries of all regression analyses on combined sewage bulk characteristics are presented in Appendix G.

Of the regressions performed, only three proved significant at the 95-% confidence level. These are presented in Table 8 with their respective correlation coefficients, indicating that the volatile fractions of the various types of solids contained in combined sewage can be predicted from a measure of the combined fixed and volatile solids. One relation indicates also a statistically significant relation between the volatile fractions of suspended solids and total solids. The statistically significant relations for the combined bulk constituents are presented in Figures 10, 11, and 12 with the observed data points.

Combined sewage bulk samples were characterized by a particle size distribution analysis from which a single descriptor was developed and called the median size, which represents the size in the particle distribution which has one-half the total weight of particles above and one-half below that size. Regression analyses were performed between this parameter and normalized combined sewage bulk characteristics, namely the ratios of settleable solids and floatable solids to total suspended solids and the ratios of biochemical oxygen demand, chemical oxygen demand, hexane extractable material, total coliforms, fecal coliforms and fecal streptococci to total volatile solids. No statistically significant correlations were obtained at the 95-% confidence level; summarized regression analyses of these data are given in Appendix H.

## Combined Sewage Screenings

Correlations between total solids (TS), total volatile solids (TVS), biochemical oxygen demand (BOD), chemical oxygen demand (COD), hexane

Table 8

STATISTICALLY SIGNIFICANT CORRELATIONS BETWEEN

COMBINED SEWAGE BULK CONSTITUENTS AT THE

95-% CONFIDENCE LEVEL

## 10 Storms

		Relationa	Correlation Coefficient
TVS	=	0.261TS <sup>1.11</sup>	0.934
TVS	s =	0.715TVS - 23.0	0.898
TVS	S =	0.864TSS - 6.20	0.991

<sup>a</sup>TVS = total volatile solids, mg/1

TS = total solids, mg/1

TVSS = total volatile suspended solids, mg/1

TSS = total suspended solids, mg/l

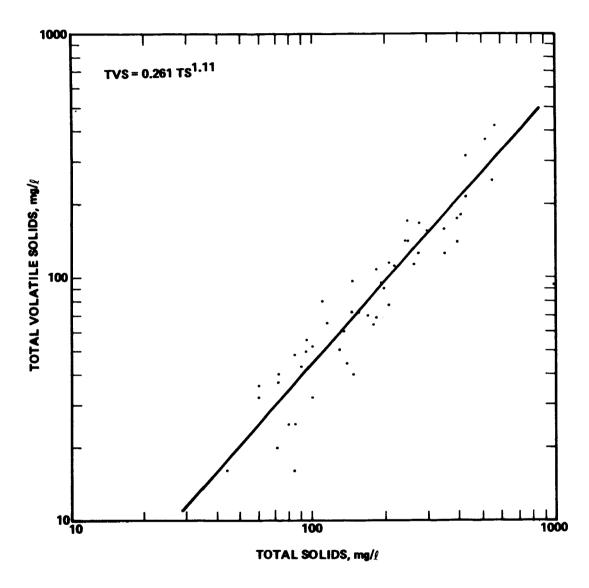


Figure 10. RELATIONSHIP BETWEEN TOTAL SOLIDS AND TOTAL VOLATILE SOLIDS OF COMBINED SEWAGE BULK 10 Storms

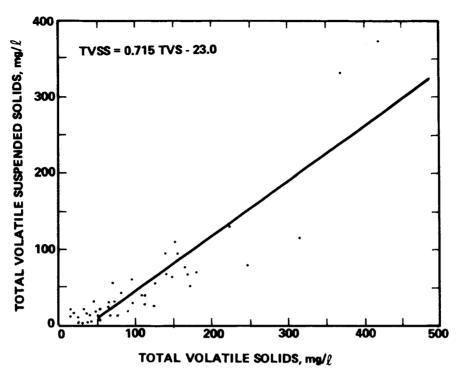


Figure 11. RELATIONSHIP BETWEEN TOTAL VOLATILE SOLIDS AND TOTAL VOLATILE SUSPENDED SOLIDS OF COMBINED SEWAGE BULK

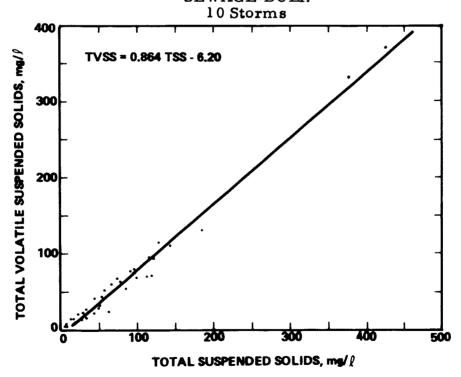


Figure 12. RELATIONSHIP BETWEEN TOTAL SUSPENDED SOLIDS AND TOTAL VOLATILE SUSPENDED SOLIDS OF COMBINED SEWAGE BULK
10 Storms

extractable material (HEM), total coliforms (TC), fecal coliforms (FC), and fecal streptococci (FS) concentrations of screenings collected from the combined sewage by all four sizes of screen apertures revealed four statistically significant relations, which are presented in Table 9.

For the screenings, the total volatile solids concentration is correlated to the total solids concentration, and indicates that at least 85% of the weight of total solids is comprised of volatile solids. Other statistically significant correlations exist between biochemical oxygen demand and hexane extractable material, amd between chemical oxygen demand and hexane extractable material. These relationships and the observed data points are presented in Figures 13, 14, 15, and 16.

Summaries of the 28 regressions performed on the combined sewage screenings are presented in Appendix I.

Table 9
STATISTICALLY SIGNIFICANT CORRELATIONS BETWEEN
COMBINED SEWAGE SCREENINGS CONSTITUENTS
AT THE 95-% CONFIDENCE LEVEL

## 10 Storms

Relationa	Correlation Coefficient
TVS = 0.856 TS + 0.526	0.998
$COD = \frac{BOD}{0.120 + 0.00160BOD}$	0.956
$HEM = \frac{BOD}{2.90 + 0.00840BOD}$	0.999
$HEM = \frac{COD}{22.1 - 0.0166COD}$	0.960

<sup>a</sup>TVS = total volatile solids, g

TS = total solids, g

COD = chemical oxygen demand, mg/g

BOD = biochemical oxygen demand, mg/g

HEM = hexane extractable material, mg/g

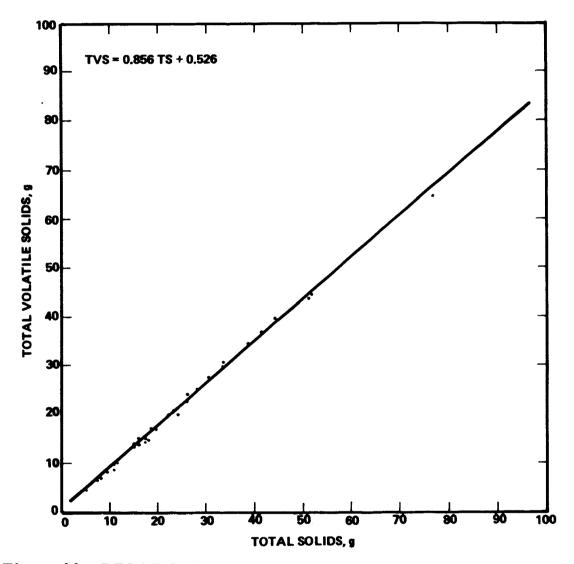


Figure 13. RELATIONSHIP BETWEEN TOTAL SOLIDS AND TOTAL VOLATILE SOLIDS OF COMBINED SEWAGE SCREENINGS
10 Storms

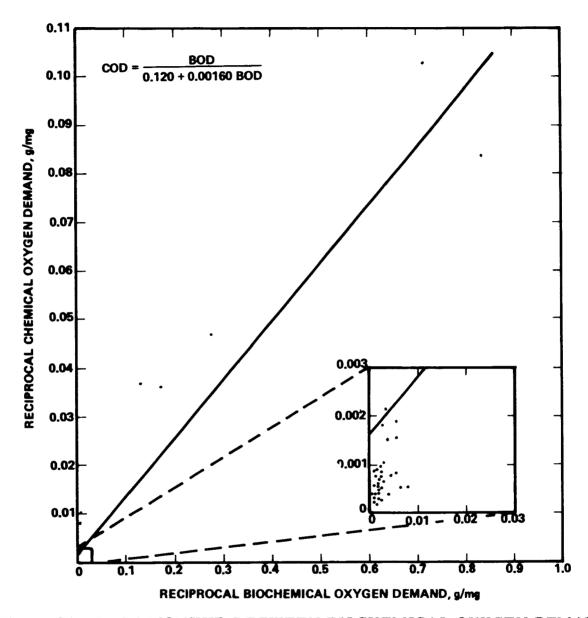


Figure 14. RELATIONSHIP BETWEEN BIOCHEMICAL OXYGEN DEMAND AND CHEMICAL OXYGEN DEMAND OF COMBINED SEWAGE SCREENINGS
10 Storms

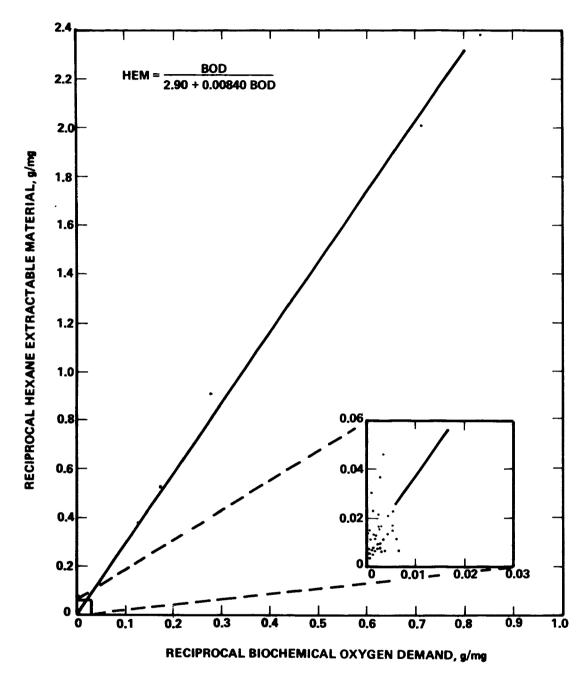


Figure 15. RELATIONSHIP BETWEEN BIOCHEMICAL OXYGEN DEMAND AND HEXANE EXTRACTABLE MATERIAL OF COMBINED SEWAGE SCREENINGS
10 Storms

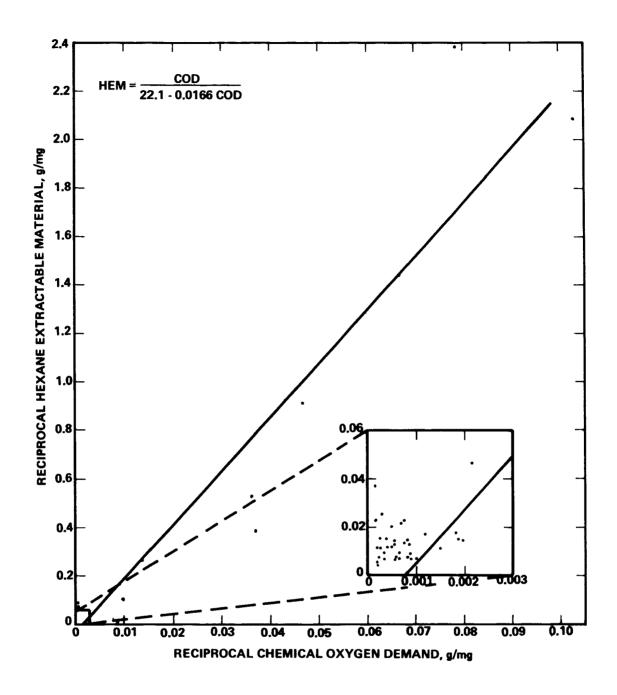


Figure 16. RELATIONSHIP BETWEEN CHEMICAL OXYGEN DEMAND AND HEXANE EXTRACTABLE MATERIAL OF COMBINED SEWAGE SCREENINGS

10 Storms

#### Section VI

#### EFFECTS OF SCREENING DEVICES

The placement of screening devices in combined sewers could perhaps provide two distinct functions. First the screen could remove pollutants from combined sewage prior to its overflow, thereby reducing the pollutant load to receiving waters. Of particular significance would be the removal of floatable and settleable matter, which upon discharge to receiving waters manifests itself by forming objectionable floating aggregations of debris and sewage solids and creating banks of accumulating sludges that can become septic and unsightly in character. Secondly, the removals of solid materials by screens could effect measurable reductions in chlorine requirements where disinfection of combined sewer overflows is practiced or indicated. The presence of solids influence chlorine demand and bacterial kills by immediate and gradual chemical consumption of the available chlorine and by physically shielding the bacteria from the remaining effective chlorine in solution.

Both of these effects were studied in this program to determine the extent to which pollutant loads and chlorination requirements are reduced by the placement of screens in combined sewers.

#### CONSTITUENT REMOVALS

Qualitative descriptions of visible materials collected on the screens placed in the Jackson Street sampling manhole are presented in Table 10. Visible materials collected consisted mostly of fecal matter, paper, leaves, and cigarettes. The nature of the collected visible screenings appears to be independent of the size of screen aperture.

Removal efficiencies of total solids (TS), total volatile solids (TVS), biochemical oxygen demand (BOD), chemical oxygen demand (COD), hexane extractable materials (HEM), total coliforms (TC), fecal coliforms (FC), and fecal streptococci (FS) provided by each insertion of the screenings sampler into the combined sewage were estimated and are presented in Table 11. The amount of constituent passing the screen and subject to removal during the insertion was assumed to be the simple average of the mass rates of the constituent determined from the routine bulk sewage sampling immediately preceding and following the insertion of the screen. Irrespective of screen aperture size, removals of total solids ranged from 0.1 to 8.1%, with an overall average of 1.4%. For total volatile solids, the average removal was larger at 2.7% and individual removals ranged from 0.2 to 11.6%. Biochemical oxygen demand removals averaged 3.9% and ranged from 0.1 to 17.2%. A similar average removal of 3.8% was observed for chemical oxygen demand, with individual removals ranging from 0.1 to 15.6%. Removal efficiencies of hexane extractable material ranged

Table 10
QUALITATIVE DESCRIPTION OF COMBINED SEWAGE SCREENINGS

	Date	Time of Immersion	Screen Size, in.	Description
4	Apr 69	•••	0.5	Not analyzed
5	Nov 69	0520	0.5	Leaves, paper, twigs
		0620		Leaves, cigarettes, fecal material
	•	0720		Leaves, fecal material
		0820		Paper, cigarettes, fecal material
		0920		Paper, fecal material
19	Dec 69	1045	0.25	Leaves, fecal material
		1145		Twigs, paper, fecal material
		1240		Mostly fecal material
		1340		Mostly fecal material
		1440		Paper, Fecal material
2	Dec 69	0930	0.25	Mostly leaves and twigs
		1025		Mostly leaves and twigs
		1125		Mostly fecal material
		1225		Mostly fecal material
		1410		Mostly fecal material
1	3 Jan 70	1800	1.0	Mostly fecal material
		1900		Mostly fecal material
		2100		String, cloth, fecal material
		2200		Mostly fecal material
		2300		Mostly leaves
20	) Jan 70	1625	1.0	Leaves, cigarettes, fecal material
		1725		Leaves, cloth, plastic material
		1835		Leaves, cloth, cigarettes
		1930		Leaves, cloth, cigarettes
		2030		Leaves, cloth, string

Table 10 (continued)

QUALITATIVE DESCRIPTION OF COMBINED SEWAGE SCREENINGS

Date	Time of Immersion	Screen Size, in.	Description
27 Jan 70	0130	0.125	Leaves, paper
	0230		Mostly fecal material
	0345		Mostly fecal material
	0430		Mostly fecal material
	0530		Mostly fecal material
13 Feb 70	0645	0.125	Mostly fecal material
	0745		Mostly fecal material, paper
	0845		Mostly fecal material, paper
	0945		Mostly fecal material, paper
	1045		Mostly fecal material
28 Feb 70	0835	1.0	Mostly fecal material, paper
	0935		Mostly fecal material, paper
	1035		Mostly fecal material, paper
	1130		Mostly paper
	1230		Mostly paper
4 Mar 70	1100	0.5	Paper, fecal material, leaves
	1200		Paper, fecal material, leaves
	1300		Fecal material, paper
	1400		Fecal material, paper
	1500		Fecal material, paper
13 Apr 70	1100	0.125	Brownish pulp appearance, cigarettes, little fecal material
	1200		Brownish pulp appearance, cigarettes, little fecal material
	1 300		Brownish pulp appearance, cigarettes, little fecal material

Table 10 (continued)
QUALITATIVE DESCRIPTION OF COMBINED SEWAGE SCREENINGS

Date	Time of Immersion	Screen Size, in.	Description
13 Apr 70	1400	0.125	Pinkish-grey appearance, cigarettes, little fecal material
	1500		Light brown appearance, cigarettes, little fecal material
13 May 70	0430	0.25	Mostly paper
	0530		Mostly paper, some food matter
	0630		Mostly paper, some fecal material
	0730		Mostly paper, some fecal material
	0830		Mostly fecal material, some paper

Date	Time at Immersion	Screen Size, in.	TS	TVS	BOD	COD	HEM	TC	FC	FS
4Apr69	2240	0.5	0.5	0.6	0.0	0.0	0.1	21.3	0, 2	-
	2330	0.5	0.8	2, 2	0.0	0.0	0.0	0.7	0.1	-
	2030	0.5	1.4	3.9	0.2	0.1	0.0	1.7	0.2	-
5 <b>Apr</b> 69	0130	0.5	4.2	10.8	0.2	0.1	0.0	0.1	0.4	-
5Nov69	0530	0.5	0.2	0.7	0.5	0.5	0.5	0.3	-	0.1
	0630	0.5	0.3	0.7	1.4	0.9	0.5	2.6	0.4	4.6
	0730	0,5	0.5	1.1	1.9	1, 1	2. 4	1.7	0.3	2, 7
	0830	0,5	0.9	1.6	1.5	2, 2	4.5	159.7	-	4. 1
19Dec69	1115	0, 25	0.4	0.6	2.8	1.1	0.5	0.3	0.4	12, 2
	1215	0, 25	0.8	1.4	7.0	7.9	3.3	0.3	1.0	40.6
	1315	0, 25	0.5	1.0	3.8	5. 3	2.8	25.0	50.5	126.3
	1415	0, 25	1.0	2.0	10.9	4.8	1. 1	133.0	25.0	-
21Dec69	1000	0.25	0.6	0.8	0.5	2, 2	3. 3	6. 2	0.8	-
	1100	0.25	1.3	2.0	2.5	6.8	11.4	2.6	0.5	-
	1200	0.25	1.4	2.4	5.0	8.9	13.0	43.1	4.6	-
	1340	0.25	0.8	1.7	1.6	5.3	1.4	103.1	_	_

Table 11 (continued)

COMBINED SEWAGE CONSTITUENT REMOVAL EFFICIENCIES BY FIXED SCREENS

(%)

Date	Time at Immersion	Screen Size, in.	TS	TVS	BOD	COD	HEM	TC	FC	FS
13Jan70	1730	1, 0	0.3	0.6	-	2.2	0.9	1.5	16.9	140.9
•	1830	1.0	1.1	1.5	-	11.0	0.9	8. 1	34.8	130,3
	1930	1.0	0.3	0.4	1.9	1.6	0.4	8, 4	5.4	90.4
	2130	1.0	1.0	1.9	4.6	3.7	1.3	5,4	1.7	-
20Jan70	1658	1.0	0.9	1.8	2.0	0.9	0,5	90.2	-	0,5
	1755	1.0	0.2	0.7	1.0	0.8	0.0	8.1	2, 5	4, 8
	1900	1.0	0.5	1.0	0.9	1.3	0.6	45.3	7. 3	14.6
	2000	1.0	3. 1	5, 0	7.9	4.3	3, 7	-	-	79.7
27Jan70	0158	0.125	0.8	1.3	-	2. 9	1.0	9.3	-	0.0
	0314	0.125	0.9	1.4	-	1.5	0.9	2. 3	-	0.0
	0400	0,125	1.7	2.8	12.5	15.6	3, 4	2.0	-	0.0
	0500	0,125	4.3	8.0	12.3	4.0	2, 2	3, 0	-	0.0
13Feb70	0710	0,125	2.2	2.9	4.8	4. 3	0,4	2.9	-	0.4
	0815	0,125	8. 1	10.9	5.6	11.1	12.5	242.0	-	-
	0915	0,125	1.9	2, 8	-	1.2	2.0	_	_	0.5
	1015	0,125	1.4	2.9	0.6	3, 2	1.5	_	-	2, 2

Table 11 (continued)

COMBINED SEWAGE CONSTITUENT REMOVAL EFFICIENCIES BY FIXED SCREENS

(%)

Date	Time at Immersion	Screen Size, in.	TS	TVS	BOD	COD	HEM	TC	FC	FS
28Feb70	0900	1.0	2, 4	3.9	4.7	2.0	7. 3	7.9	13, 1	_
	1000	1.0	2.0	3.8	1.8	1.5	3. 3	44.8	10.5	-
	1100	1.0	1.4	2.9	3. 3	2.4	•	120.8	477.8	-
	1200	1.0	0.6	1.3	1.3	1.2	-	11.5	24.0	5.1
4Mar70	1130	0.5	3.9	11.6	17.2	13.9	4.0	-	22.6	6.4
	1230	0.5	0.4	0.9	0.3	0.1	0.2	-	0.3	0, 2
	1330	0.5	0.2	0.4	0.1	0.4	0.2	-	4.3	2. 2
	1430	0.5	0.1	0,2	0.1	0.2	0.1	-	-	0.4
13Apr70	1130	0.125	1.8	3.0	2.0	7.7	3.7	0.1	0.7	0.0
	1230	0.125	2.0	4.0	6.2	6.8	3, 2	9.5	154, 2	23.2
	1330	0.125	1.5	3.0	3. 1	3.7	2.6	10.2	0.7	0.6
	1430	0.125	1.3	2.6	2. 1	5.2	2.4	0.7	0, 3	0.8
13May70	0500	0.25	1.3	4.0	9.8	6.0	1.2	0.0	0.1	0.0
	0600	0.25	2.0	$4_{ullet} 4$	5.3	<b>5.4</b>	10.7	0.1	0.0	0.0
	0700	0.25	-	-	-	-	-	200	-	-
	0800	0.25	-	-	-	-	-	***	-	-
	Mean		1.4	2.7	3. 9	3.8	2.7	10.3	6.5	16.7

from 0.0 to 12.5% for an overall average of 2.7%. The observed removals for all three bacterial forms were highly variable, indicating no removals in some instances and more than 100% in others. This irregularity is believed due primarily to the combined effects of the underestimation of bacterial densities in the bulk sample as a result of encapsulation in solids of organisms which do not develop in the analytical test media, and the growth and release of organisms from the collected screenings during sample collection, storage, preparation, and analysis. Reducing to 100% all observed bacterial removals that were greater than 100% provides overall average removals, irrespective of screen aperture size, of 10.3, 6.5, and 16.7%, respectively, for total coliforms, fecal coliforms, and fecal streptococci.

Average removals of combined sewage constituents by fixed screening devices as a function of screen aperture size are shown in Figure 17. Maximum average removals of biochemical oxygen demand, total solids, and total volatile solids resulted with the 0.125-in. screen, and were, respectively, 5.4, 2.3, and 3.8%. The larger 0.25-in. screen provided the maximum average chemical oxygen demand and hexane extractable material removals of 5.4 and 4.8% respectively. Only the average total volatile solids removal was least with the 1.0-in. screen, which was the largest screen aperture used, with intermediate sizes effecting minimum removals of the remaining physical and chemical constituents. Average bacterial removals were consistently lowest with the smallest screen aperture used and greatest with the largest screen aperture. This apparent anomoly is not explained.

For the physical and chemical constituents, the 1.0-in. screen effected removals that ranged from 48 to 60% of those obtained with the 0.125-in. screen. Apparently screens with relatively large openings are capable of removing a majority of the pollutants contained in combined sewage that are amenable to reduction by screening devices.

#### CHLORINATION PRACTICES

Four combined sewage bulk samples were collected from the Jackson Street manhole for use in laboratory studies to determine the effect of solids removal by screens on chlorination practices. The first three samples were collected during the normal sampling episode of 4 March 1970, and the fourth sample was taken between 0900 and 1100 hours on 14 April 1970.

Chlorine demands of screened and unscreened combined sewage samples are shown in Figure 18. The break-point of chlorination was determined on one sample and occurred at a chlorine dosage of about 30 mg/l.

Prebreak-point chlorination of all samples, results of which are shown in the lower half of Figure 18, demonstrated the effect of solids on chlorine requirements. The 15-minute chlorine residuals of Samples

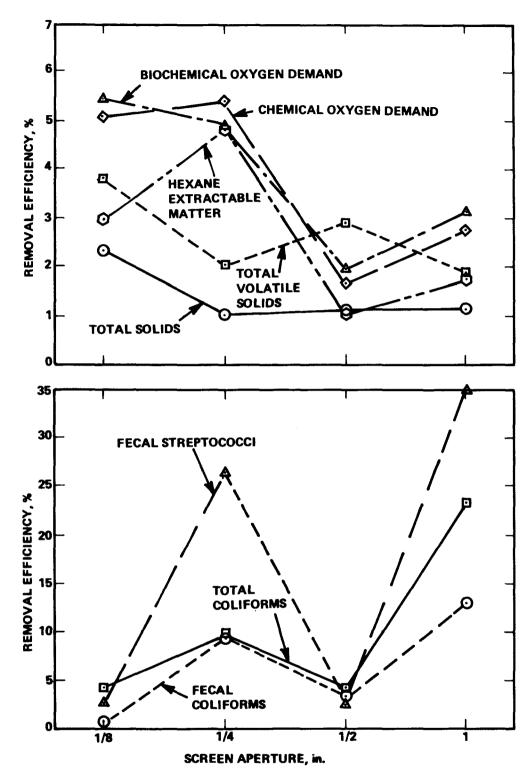


Figure 17. EFFECT OF SCREEN APERTURE SIZE ON COMBINED SEWAGE CONSTITUENT AVERAGE REMOVALS

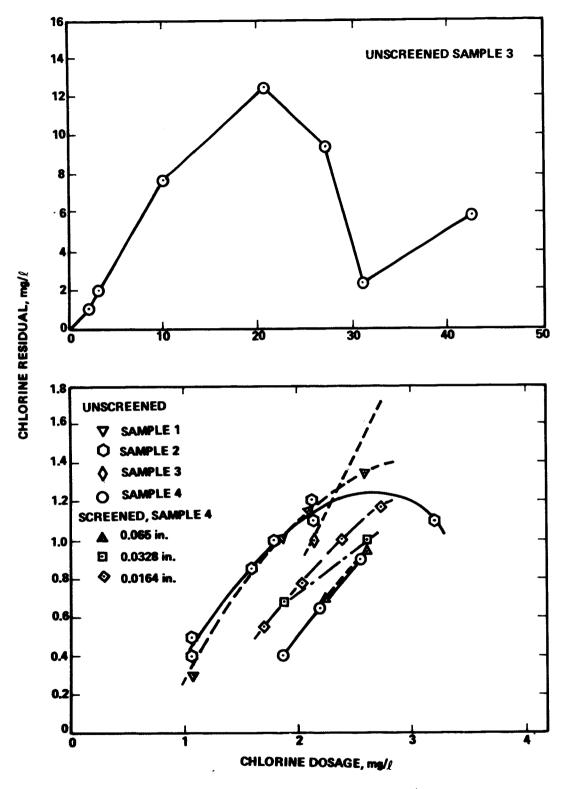


Figure 18. CHLORINE DEMAND OF SCREENED AND UNSCREENED COMBINED SEWAGE SAMPLES

1, 2, and 3 are much higher than the chlorine residual of Sample 4 at the same chlorine dosage due to the marked differences in total suspended solids concentrations. The first three samples contained on the average about 35 mg/l of total suspended solids, whereas the fourth sample had a total suspended solids concentration of 89 mg/l. At a chlorine dosage of 2, 0 mg/l, Sample 4 had a chlorine residual of 0, 5 mg/l after 15 minutes and Samples 1, 2, and 3 had about 1.1 mg/l. The chlorine residual at a fixed chlorine dosage for Sample 4 increased 50% following passage through a screen with 0.0164-in. aperture. A 0.0328-in. screen effected a somewhat smaller increase, and a 0.065in, screen caused no increase in chlorine residual over the unscreened Sample 4. For a fixed chlorine residual of 1.0 mg/l after 15 minutes, the required chlorine dosage of Sample 4 decreased with decreasing screen aperture size, as shown in Figure 19. A reduction in chlorine dosage of only 11%, however, was observed following passage through all the screens, including the small 0.0164-in. screen.

The solids content of the combined sewage samples after serial processing through the series of screen sizes is presented in Figure 20. The data are irregular, but in general overall settleable solids concentrations were decreased, ranging from 20 to 80% upon final passage through the 0.0328-in. screen. Suspended solids content of the one sample decreased only 2% upon passage through the last, 0.0164-in. screen and actually increased upon passage through the 0.065- and 0.0328-in. screens! The number of samples available for analysis are too few for meaningful evaluation of the suspended solids content of screened combined sewage samples.

Bacterial counts of combined sewage following serial passage through screens of decreasing aperture size prior and subsequent to chlorination at a dosage providing a 15-minute chlorine residual of 1.0 mg/l are shown in Figure 21. (Arrows denote the direction of possible density for those determinations that were indefinite.) For Sample 1, general decreases in both total and fecal coliform densities occurred as screen aperture size was decreased. With the exception of isolated points, this general decrease in bacterial densities prior to chlorination was not observed to occur for any of the other combined sewage samples.

Post chlorination bacterial densities were for the most part indeterminate in Sample 1. In Sample 2, bacterial densities of the various screened portions were variable but demonstrated some decrease (more than one order of magnitude for total coliforms) following passage through the smallest, 0.0164-in. screen. Samples 3 and 4 demonstrated on the contrary that bacterial densities were little effected or increased as screen sizes became smaller. In Sample 3 the fecal coliform concentration increased one order of magnitude following serial passage through all screens, and in Sample 4 the total coliform concentrations likewise increased an order of magnitude.

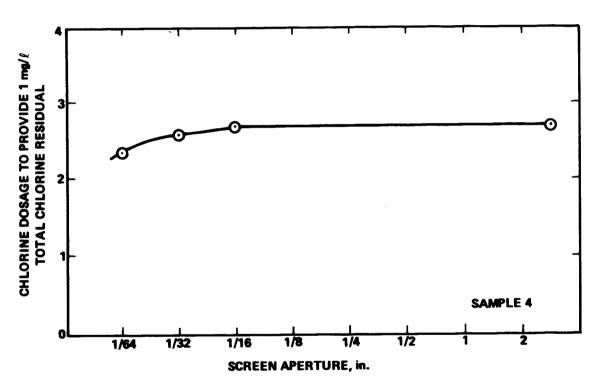


Figure 19. EFFECT OF SCREEN APERTURE SIZE ON CHLORINE DOSAGE OF COMBINED SEWAGE

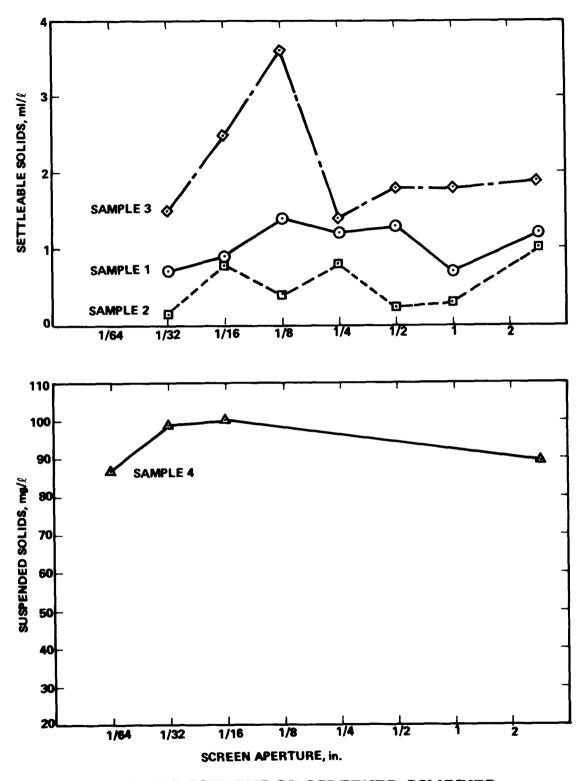


Figure 20. SOLIDS CONTENT OF SCREENED COMBINED SEWAGE SAMPLES

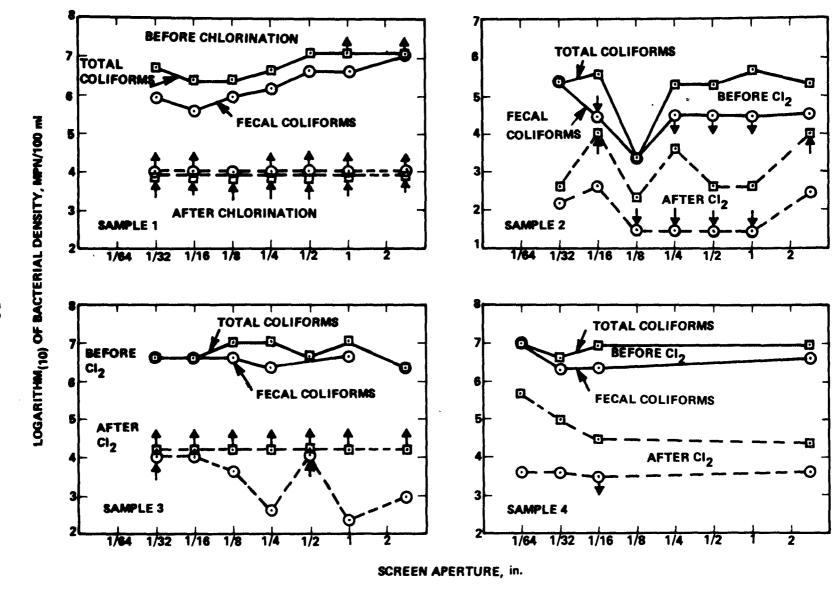


Figure 21. BACTERIAL DENSITIES OF SCREENED COMBINED SEWAGE SAMPLES BEFORE AND AFTER CHLORINATION

The absence of any generally consistent trend in bacterial densities as a consequence of screening of combined sewage suggests that screens of the size considered in this study have little, if any, effect on bacterial concentrations, per se, either associated with or without chlorination.

#### Section VII

## APPLICATION OF SCREENING DEVICES

Combined sewage by nature is highly variable in both quantity and quality, and thus presents an extremely difficult material to control. During periods of rainfall, snow melt, and infiltration when the sewered flow increases to a point where it can no longer be hydraulically accommodated at the sewage treatment plant, the combined sewage is discharged untreated at bypass structures to receiving waters or open drains.

A national survey (Ref. 2) has concluded that combined sewer overflows contribute a significant portion to the nation's water pollution problem. It was estimated that about one-fifth of the country's population is served by combined sewers, of which more than threequarters (of those inventoried) reported overflow occurrence. Also about three-quarters of all overflow sources surveyed was from combined sewers.

A number of methods for the abatement of pollution from combined sewer overflows have been proposed and many are being evaluated and demonstrated. "Total" solutions are available that eliminate combined sewer overflows, by separation of sanitary and storm water flows or by in-line or off-line storage and subsequent treatment of total flow in conventional sewage treatment facilities, but all are quite costly to implement and maintain. Another approach is the treatment of combined sewer overflows at their point of discharge, which suggests the use of high-rate treatment systems that are capable of processing highly variable flow rates and compositions. An extension of this latter scheme is the placement of devices in combined sewers upstream of the overflow bypass to retain certain pollutants in the sewer system during overflow occurrences and to release them back to the sewage subsequent to cessation of the overflow condition.

Of the many types of pollutants contained in combined sewage, particulate matter and especially the floatable and settleable fractions contribute to conditions which can quickly manifest themselves upon discharge to receiving waters by their obvious presence. Moreover, other immediate and potential degradation of receiving waters can occur from these solids so that their separation from combined sewer overflows could greatly reduce the deleterious effects of combined sewer discharges on receiving waters.

Mechanical means of solids removal, such as fixed or moving screens, would appear to possess the desirable characteristic for this application of the acceptance of wide variations in hydraulic loading with relatively little effect on performance compared to systems dependent upon

biological actions, gravity separation, or porous media filtration. In addition, high solids removal efficiencies can be obtained from mechanical screening devices. They are well suited to modular or staged operation and are immediately operable.

Similar reductions in combined sewer overflow pollution could be effected either by screening stations at the points of combined sewer overflows or by the placement of screening devices in the combined sewers upstream of the overflow bypass. The two systems, however, differ greatly in their operation and must be carefully evaluated with regard to their comparative utility. The in-sewer devices would require no additional space for their implementation other than that already allocated to the conveyance of combined sewage, since they would be inserted into manhole sections. Also the choice of locating the in-sewer devices to best control and retain the solids in the system should be almost limitless. The greater number of devices required for in-sewer placement, however, as compared to combined sewer bypass placement. requires careful assessment of the capital and particularly maintenance costs associated with this method of pollution control. Total costs of the in-sewer screens would be greatly dependent upon the character and design of the device, but it is evident that it must be capable of nearly maintenance-free operation. Frequent, periodic inspection and routine maintenance of several larger screening stations located at overflow points would certainly be more convenient and economical. Development and demonstration of satisfactory in-sewer screening devices must be performed before serious consideration can be given this method of solids removal from combined sewer overflows.

The maintenance of acceptably high hydraulic loading rates without incurring impractical pressure drops requires that screen apertures be sufficiently large, which limits the minimum sized particle that can be physically retained by the screen. For the placement of fixed screens in sewers, where tolerable hydraulic head losses are usually quite small, the screen aperture may be only small enough to retain street litter, paper and paper goods, leaves, and fecal matter. These larger solids, however, upon discharge to receiving waters tend to agglomerate into larger, more evident and objectionable, concentrations of water pollution. If the aesthetic quality of receiving waters is to be preserved, these large screenable solids must be remove from combined sewage discharges.

The extent to which screenable solids discharged with combined sewer overflows will produce deleterious effects will depend in large part upon the nature of the receiving waters. The most serious condition in this respect occurs where the solids have the greatest opportunity to become and remain aggregated, such as would occur in lakes and tidal estuaries of low flushing characteristics. Lesser opportunity for agglomeration exists in flowing streams and rivers and in exposed embayments and coastal waters; and therefore the degradation of these

receiving waters caused by release of screenable solids is much less evident and significant.

Although the potential deleterious effects of deoxygenation, eutrophication, and pathogenic inoculation of receiving waters caused by screenable solids should not be overlooked, the primary function of removing these solids is the protection and preservation of the esthetic quality of the environment. Thus those uses of receiving waters that benefit most from the control of screenable solids are those subject to public use and view, namely, recreation and scenic viewing. Of half of the estimated jurisdictional areas served by combined sewers in the nation that were surveyed (Ref. 2), 11.9% reported combined sewer overflows into receiving waters used for body contact recreation, 16.2% indicated overflows to limited body contact recreational waters, and 15.8% reported overflows to receiving waters whose highest use is fishing. The same survey also indicated that an additional 20.6% of the overflows are discharged to open drains which normally are dry and thus are susceptable to intermittent, prolonged exposure of deposited solids.

With respect to land use in the immediate vicinity of combined sewage overflows it was found (Ref. 2) that 13.9% of the overflows occurred in recreational areas and 30.4% in residential areas.

A major portion of the nation's receiving waters therefore would appear to be immediately affected and degraded by the discharge of materials that are amenable to removal from combined sewage overflows by screening devices.

The reduction of pollutants, which exert an early demand on the oxygen resources of the receiving waters as measured by biochemical oxygen demand and chemical oxygen demand, by fixed screening devices was found in this program to be small (~5%); and although any reduction is certainly of benefit, the improvements produced by this treatment are marginal and most probably could not be easily measured in the receiving waters. Also negligible reductions in bacterial densities and chlorine requirements were observed with screens having aperture sizes that are considered practical for insertion into sewers. Thus for conditions requiring reduction either in substances that exert an early oxygen demand or in bacterial quantities, there appears to be no benefit from the placement of a fixed screen into a combined sewer. Reductions effected in these pollutants by moving screening devices are of course another matter and are not quantitatively considered herein.

#### Section VIII

## **ACKNOWLEDGMENTS**

The program was performed during the 1968-1969 and 1969-1970 wetweather seasons by the Envirogenics Company, a Division of Aerojet-General Corporation, at El Monte, California, under the direction of Messrs. John C. Merrell, Jr., Project Officer, and Darwin R. Wright, Federal Water Quality Administration. Aerojet-General personnel participating in the program were Dr. D. L. Feuerstein, Program Manager; Mr. Alfred Grimm, Project Engineer; Mr. T. A. Bursztynsky, Engineer; Messrs. R. C. Hanson and B. H. Putt, Analysts; and Mrs. M. D. Robinson, Secretary.

The field sampling, monitoring, and laboratory analysis for this program were contracted with and performed by Engineering-Science, Incorporated, Oakland, California under the supervision of Drs. W. G. Gates and T. G. Shea.

The cooperation of the City and County of San Francisco in allowing the sampling station manhole modifications for the tests is gratefully appreciated and acknowledged.

## Section IX

# REFERENCES

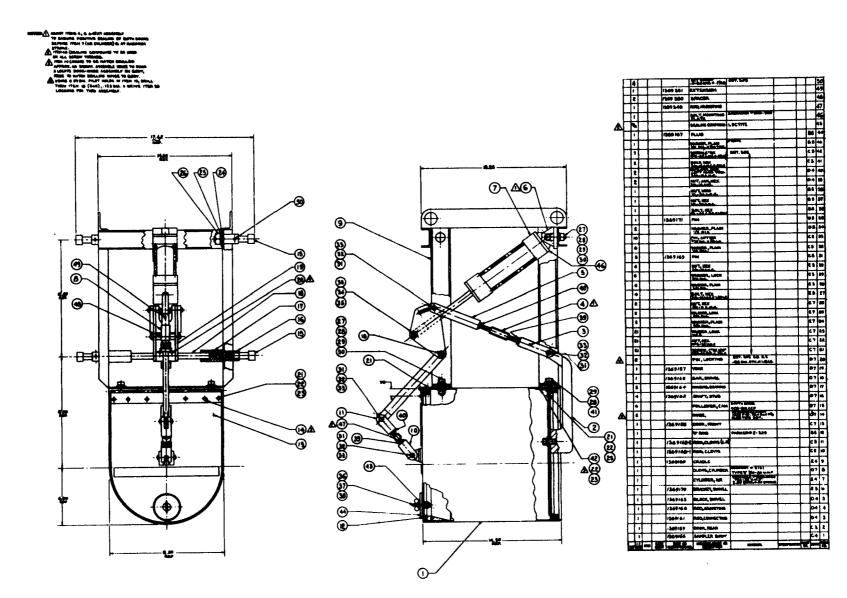
- 1. Dixon, W. J. and F. J. Massey, Jr. Introduction to Statistical Analysis. 2nd ed. New York: McGraw-Hill Book Co., Inc., 1957.
- 2. Problems of Combined Sewer Facilities and Overflows, 1967.

  (WP-20-11), Washington: Federal Water Pollution Control
  Administration, 1 December 1967.

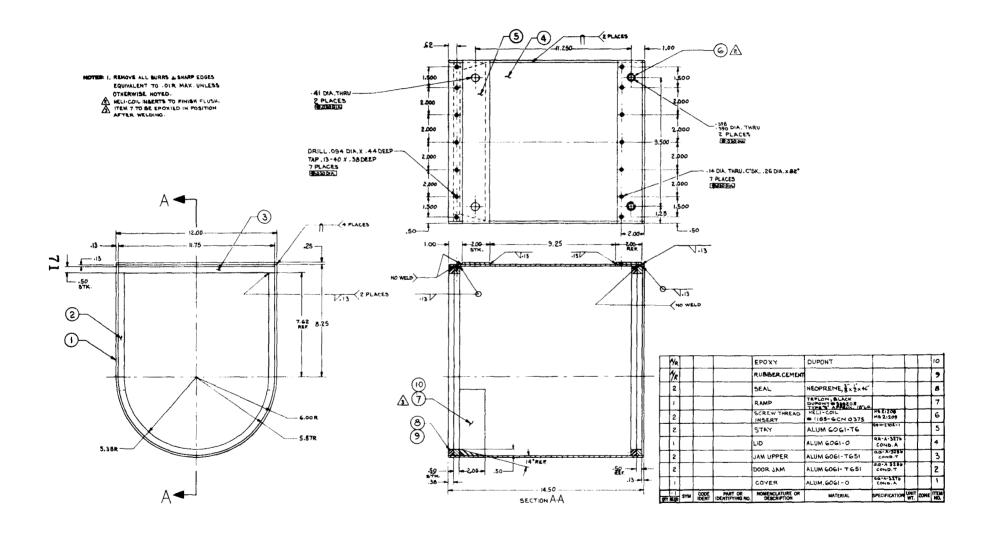
# Section X

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Appendix A. BULK SAMPLER ASSEMBLY



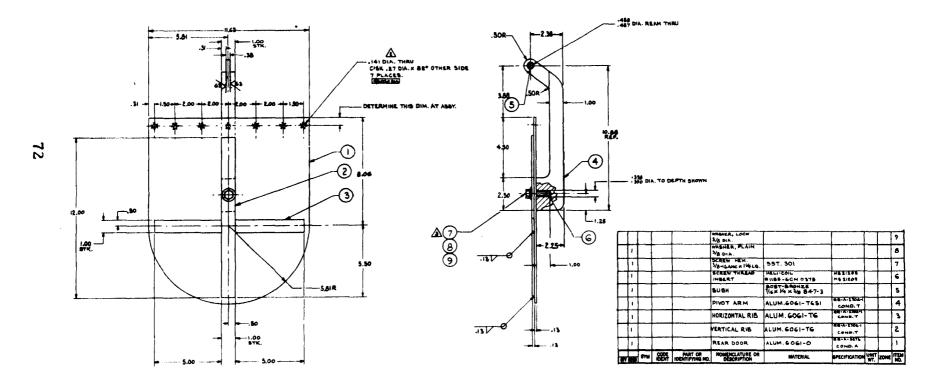
Appendix A (Continued). SAMPLER BODY

NOTES: I, REMOVE ALL BURRS & SHARP EDGES
EQUIVALENT TO . OIR MAX. UNLESS
OTHERWISE. NOTED

A BEFORE DRILLING SES HOTE & DRING 1369185.

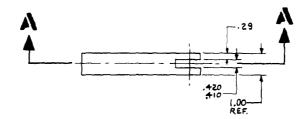
ANSEMBLE HINGE TO DOOR & MATCH DRILL (STAGGER HOLES TO MISS SIMILAR HOLES IN BODY 1369186)

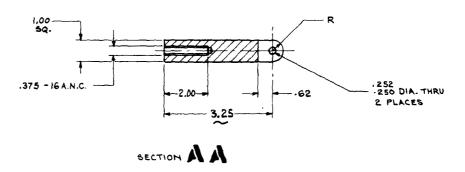
ANSEMBLE OOR IN P/N 1369186 (BODY)
WITH LINKAGE BEFORE LOCATING FOR SCREW ITEM 7,
(288' ASSEMBLY DAWN, 1869185).



Appendix A (Continued). REAR DOOR

NOTES: I, REMOVE ALL BURRS & SHARP EDGES
EQUIVALENT TO . OIR MAX, UNLESS
OTHERWISE NOTED.

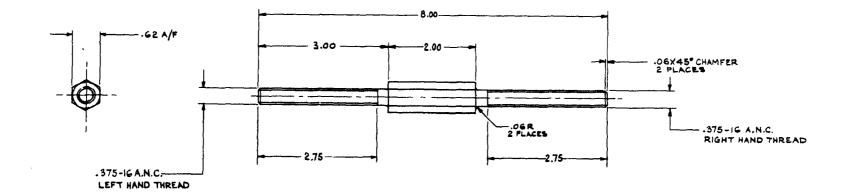




П	7			-1		ALUM GOGI-TG	QQ-A-2702-1			
QTY RE	00	SYM	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	UNIT WT.	ZONE	ITEM NO.

Appendix A (Continued). CONNECTING ROD

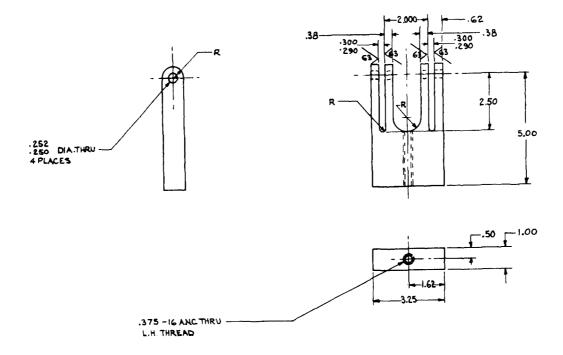




			-1		HEX. BAR SST. 303 C.D. H.T.	M1L-\$-7720	$\dashv$
QTY REQU	SYM	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION UNIT ZONE	TEM NO,

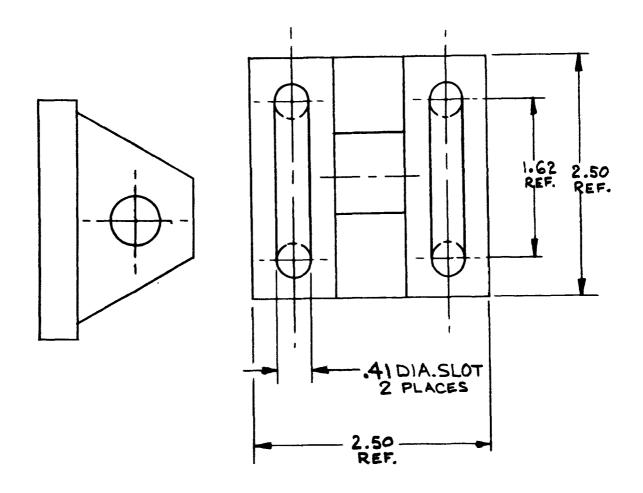
Appendix A (Continued). ADJUSTING ROD

NOTES: I. REMOVE ALL BURRS & SHARP EDGES
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OTHERWISE NOTED.



ALUM. GOGI-TG QA-A-27A-1 COND. TO DESCRIPTION MATERIAL SPECIFICATION UNIT ZONE TEM.

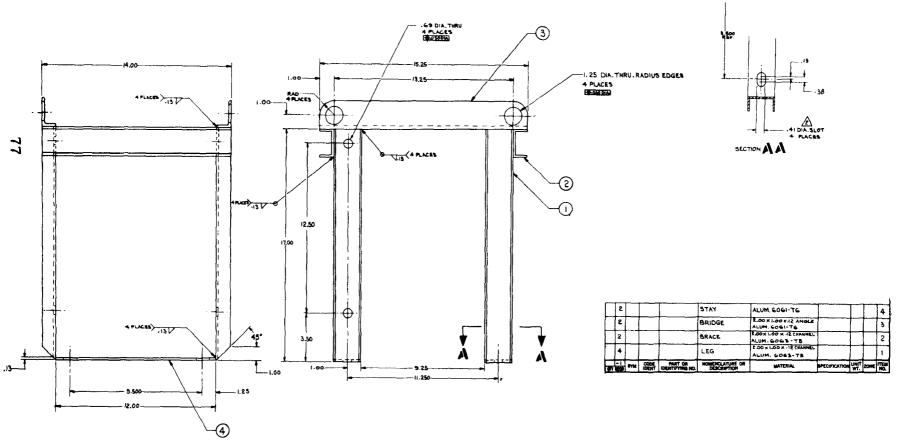
Appendix A (Continued). SWIVEL BLOCK



Appendix A (Continued). SWIVEL BRACKET

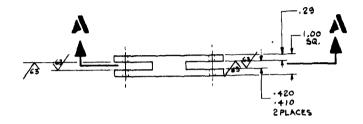
NOTES I. REMOVE ALL BURRS & SHARP EDGES
EQUIVALENT TO .OIR MAX. UNLESS
OTHERWISE MOTED.

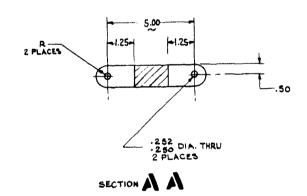
A LOCATE TO PIN 1869186 BODY BEFORE SLOTTING.



Appendix A (Continued). CRADLE

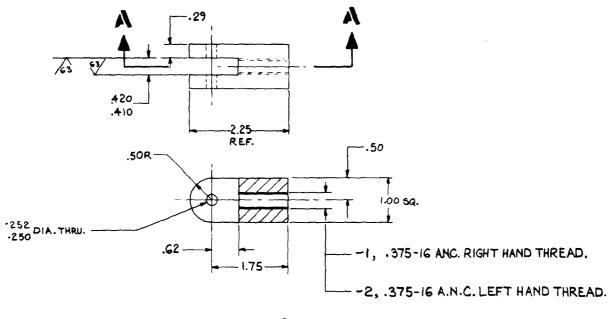
NOTES: I. REMOVE ALL BURRS & SHARP EDGES
EQUIVALENT TO OIR MAX. UNLESS
OTHERWISE NOTED.





-			CODE	PART OR	NOMENCLATURE OR	ALUM GOGI-TG	COND.T	UNIT		1754
QTY	REQU	SYM	IDENT	IDENTIFYING NO.	DESCRIPTION	MATERIAL	SPECIFICATION	WT.	ZONE	NO.

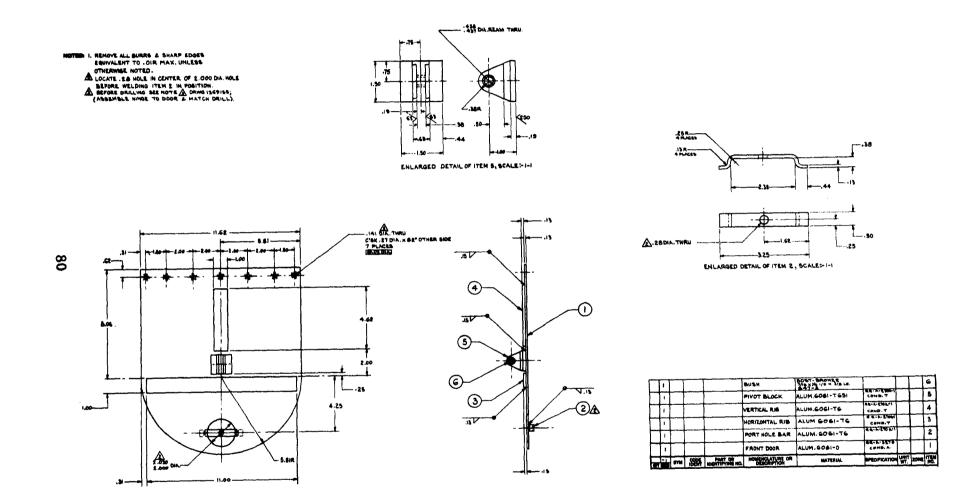
### NOTES: I. REMOVE BURRS & SHARP EDGES



# SECTION A A

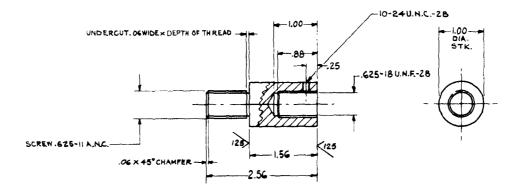
	ı			-2		ALUM.GOGI-TG	QQ-A-2764-1 COND.T.			
Γ	1			-1		ALUM.6061-T6	99-A-2702-1 COND.T.			
<b>E</b>	I REQD	SYM	CODE IDENT	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	WT.	ZONE	NO.

Appendix A (Continued). CLEVIS ROD (L. H.)



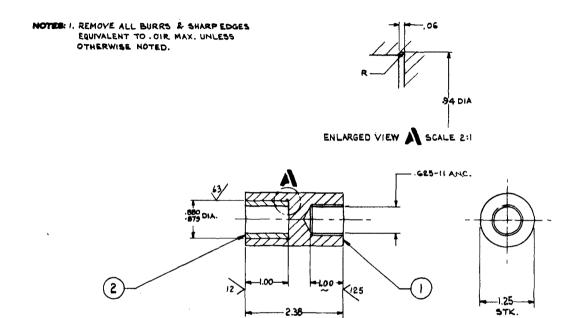
Appendix A (Continued). FRONT DOOR

NOTES: 1. REMOVE ALL BURRS & SHARP EDGES EQUIVALENT TO . DIR MAX. UNLESS OTHERWISE NOTED.



		-1		SST. 303 C.D. H.T.	MIL-8-7720			
QTY REQD SY	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	WT.	ZONE	TEM NO.

Appendix A (Continued). SHAFT STUB



	ı				Bush	BOST-BRONZ 7/8 x 5/8 1.0.x   LG. BIO14 - B			2
	1				BEARING HOUSING	SST. 303 C.D. H.T.	MIL-9-7720		١
9	- I	SYM	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION 1	INIT ZONE	ITEM NO.

Appendix A (Continued). BEARING HOUSING

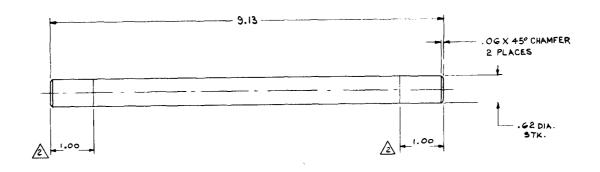
NOTES: I. REMOVE ALL BURRS & SHARP EDGES

EQUIVALENT TO .OIR MAX UNLESS

OTHERWISE NOTED.

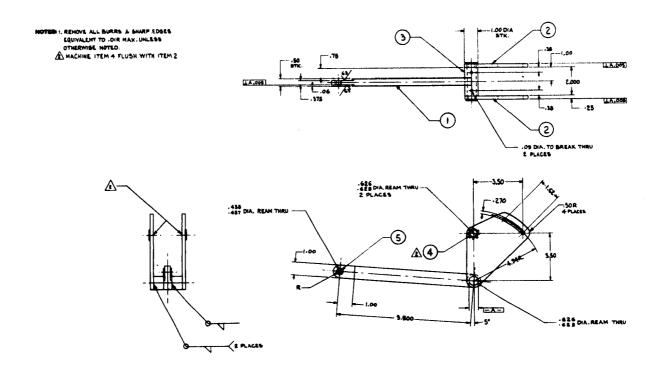
COAT WITH TEFLON "S", DUPONT "939203,

MAX. DEPTH .OOI



			~1		ALUM.6061(615-T6)	QQ-A-325b			
QTY REC	SYM	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	UNIT WT.	ZONE	ITEM NO.

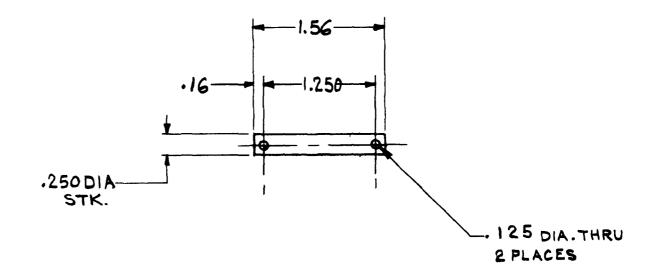
Appendix A (Continued). SWIVEL BAR



F		SYM	CODE	PART OR HO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	UNIT WT.	ZOHE	TEN.
Γ	1				YOKE	ALUM GOGI -TG	COND.T			1
	2				PIVOT PLATE	ALUMGOGI-TE	0 8 - A- 2701-1 COM D.T			2
	ı				CYLINDER	ALUM 6061-T681	COND. T			3
	2				BUSH	606 T BROWNE 6/8 R 1/2 IS X 1/2 LG. F8-810-4				4
	•				BUSH	9087- BROWER 7/6 x 7/4 1.0. x 7/814. 8-47-3				5

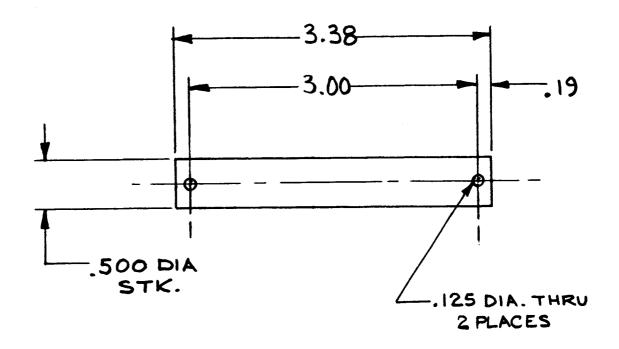
Appendix A (Continued), YOKE

# NOTES. I. REMOVE ALL BURRS & SHARP EDGES EQUIVALENT TO . OIR MAX. UNLESS OTHERWISE NOTED.



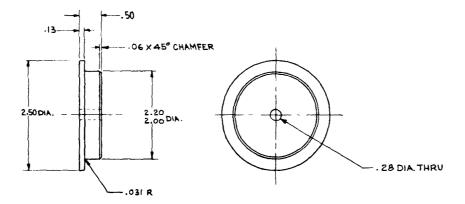
Appendix A (Continued), PIN

# NOTES: REMOVE ALL BURRS & SHARPEDGES EQUIVALENT TO . 010 R MAX.



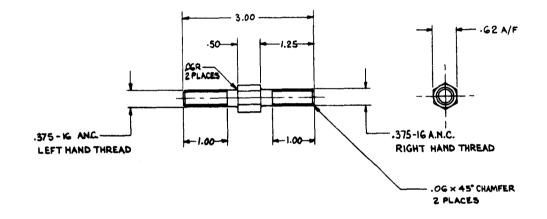
Appendix A (Continued). MAIN PIN

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EQUIVALENT TO .01R MAX. UNLESS
OTHERWISE NOTED.

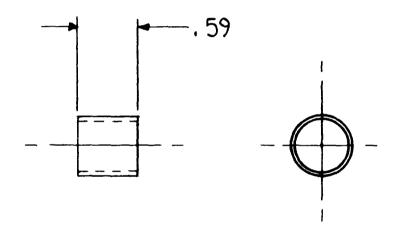


				-1		ALUM.GOGI(GIS-TG)	QQ-A-3256 COND.T			
QTY	REQO	SYM	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	UNIT WT.	ZONE	NO.

Appendix A (Continued). PLUG

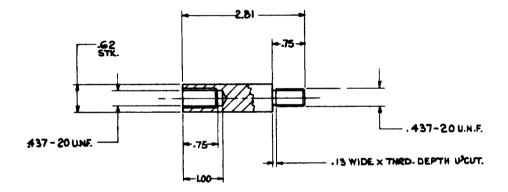


1					HEX. BAR SST 303 C.D. H.T.	MIL-5-7720			
 I	SYM	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	WT.	ZONE	NO.



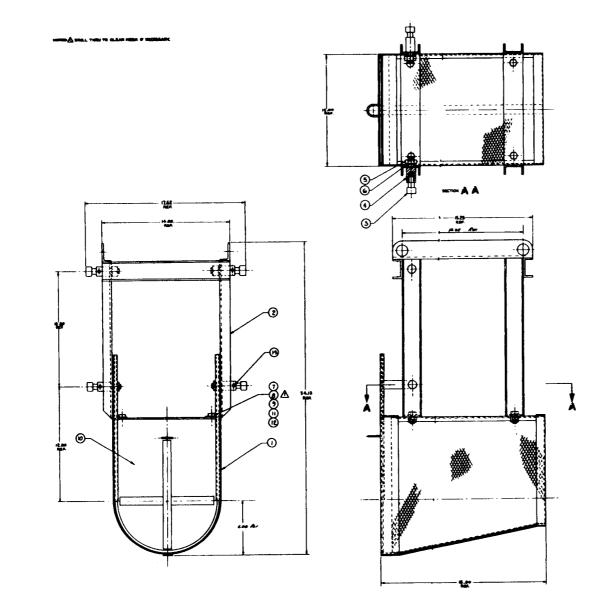
Appendix A (Continued). SPACER

# NOTES: I. REMOVE BURRS & SHARP EDGES.



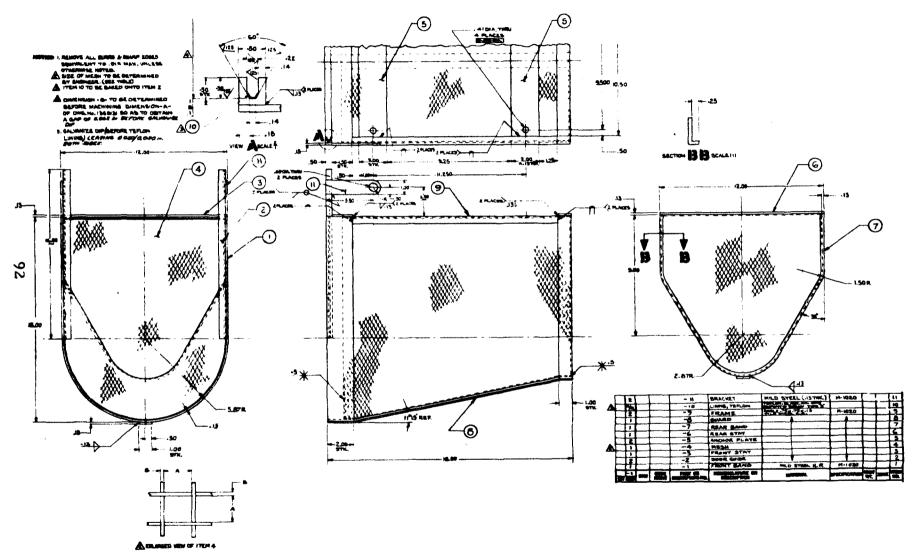
	1					\$\$T. 303 C.D.H.T.	MIL-5-7726			
Ory	- 0	SYM	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	UNIT WT.	ZONE	ITEM NO.

Appendix A (Continued). EXTENSION



Ι	π.	985		**************************************	-	No. of Lot	8	_	п
1	•		1241:29	SAMPLEA BERESHING		Ŀ	_	┕	Ľ
1		T	1369160	CRADLE			L	L	Ľ
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Appendix B. BULK SAMPLER ASSEMBLY



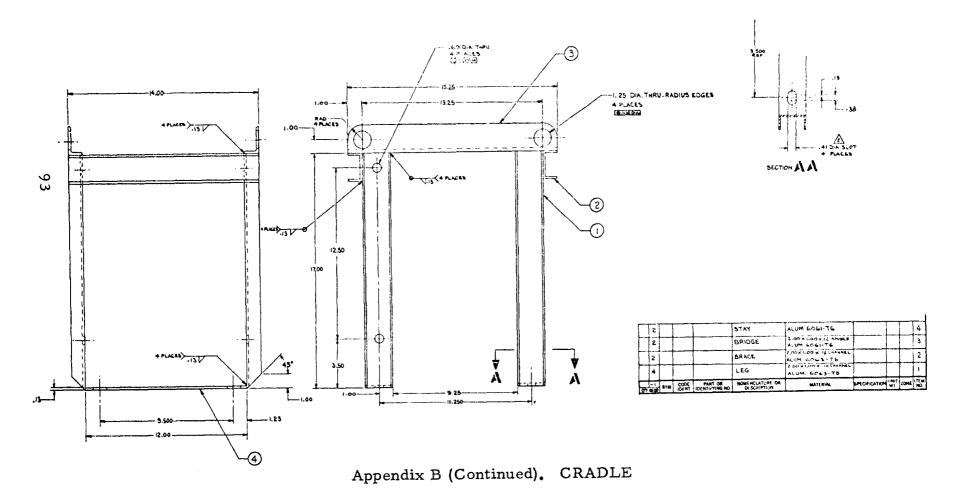
Appendix B (Continued). SCREENING SAMPLER

NOTION 1. REMOVE ALL BURRS & SHARP EDGES

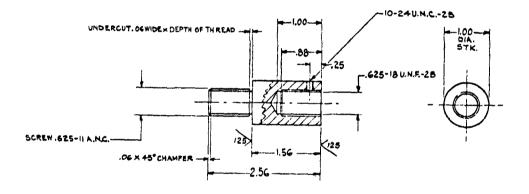
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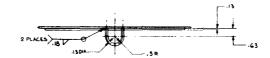


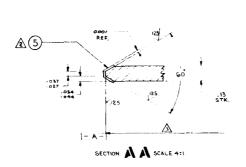
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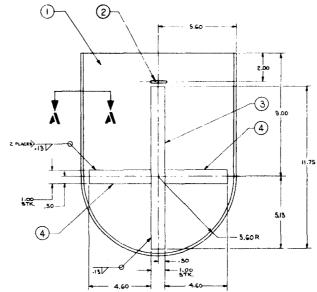
Appendix B (Continued). SHAFT STUB

NOTES: 1. REMOVE ALL BURRS & SHARP EDGES
EQUIVALENT TO .01M MAX. UNLESS OTHERWISE NOTED.
2. ITEM 5 TO BE BAKED ONTO ITEM 1

DIMENSION - A- TO BE MACHINED AFTER DETERMINING
DIMENSION - B- OF DWG.No. 13G9129 50 A6 TO
DETAIN A GAP OF .020/.030 AFTER TEFLON LINING.







	ě	TE GO	SYM	CODE	PART OR IDENTIFYING NO.	NOMENCLATURE OR DESCRIPTION	MATERIAL	SPECIFICATION	WT.	ZONE	ITEM NO.
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		ī			- 2	LIFTING EYE					2
		,			- 3	VERTICAL RIB					3
		2			-4	HORIZONTAL RIB	MILD STEEL	M1020			4
<u> </u>		*			-5	LINING, TEFLON	TEFLON, BLACK DUPONT # 954101 TYPE "S' /LON BANK!				5

# Appendix C

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### LOCAL CLIMATOLOGICAL DATA

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLOG. FEBRUARY 1969 U. S. DEPARTMENT OF COMMERCE - MAURICE H. STANS, Secretary

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HOURLY PRECIPITATION (Water equivalent in inches) ENTRY OF TRACE AMOUNTS MAY BE INCOMPLETE P. M. Hour ending at .01 -04 .01 .01 .07 .10 .10 .04 .03 .07 .24 .14 .05 .02 .02 .02 .10 .03 .02 101 123 145 167 189 22 22 24 25 27 28 .02 10 11 .13 .17 .04 .05 T .02 .01 .13 .10 .11 .14 .03 .06 .09 .03 .07 .19 .09 .03 T .05 .13 .05 .04 .02 T .01 - 06 -02 .02 .08 .04 .01 .05 .01 .02 .04 .03 .01 .02 .05 .03 .01 .04 .02 .02 .08 T .03 .01 .16 .02 .04 T .01 .01 .07 .01 .01 .01 T .01 .12 .01 .01 .04 .01 .01 .09 .03 .02 .06 .09 .11 .08 .03 .01

- Extreme temperatures for the month. May be the last of more than one occurrence.

  Below zero temperature or negative departure from

- Below zero temperature or negative departure from normal. \$70° at Alaskan stations. Also on an earlier date, or dates. Heavy for restricts visibility to ¼ mile or less. In the Hourly Precipitation table and in columna 9, 10, and 11 indicates an amount too small to measure.

9, 10, and 11 indicates an amount too small to measure.

The season for degree days begins with July for heating and with January for cooling.

Data in columns 6, 12, 13, 14, and 15 are based on 8 observations per day at 3-hour intervals.

Wind directions are those from of wind blows.

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Any errors detected will be corrected and changes in summary data will be annotated in the annual summary.

Subscription Price: Local Climatological Data \$1,00 per year including annual Summary if published Single experience of the Company of the Co

I certify that this is an official publication of the Environmental Science Services Administration, and is compiled from records on file at the National Weather Records Center, Asheville, North Carolina 28801.

William X. Haggard Director, National Weather Records Center

USCOMM-ESSA-ASHEVILLE

SUMMARY BY HOURS

Wet bulb C

Hour (Local time) Sky cover (In tenths)

Station pressure (In)

# LOCAL CLIMATOLOGICAL DATA

U. S. DEPARTMENT OF COMMERCE - MAURICE H. STANS, Secretary

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. MARCH 1969

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Subscription Price: Local Climatological Data \$1.00 per year including annual Summary if published. Single copy: 10 ceats for monthly Numnary: 15 cents for annual Summary. Checks or mone or cents for annual Summary. Checks or mone or specific control of the second price of the superintendent of the Superintendent of Documenta, U. S. Government Printing Office, Washington, D. C. 20402.

William H. Haggard

Director, National Weather Records Center

SUMMARY BY HOURS
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# LOCAL CLIMATOLOGICAL DATA

U. S. DEPARTMENT OF COMMERCE - MAURICE H. STANS, Secretary

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLOG, APRIL 1969

-			Гетрега	ture (	F)			shown	ner types by code	Snow,	Precipi	tation	Avg. station			Wind	ACIE		Sunsh	ine	Sky	cover nths)	Γ
	Maximum	Minimum	Average	Departure from normal	Average dew point	Heating Bass	Cooling days	of oc 123	currence 456 789	Sleet, or Ice on ground at OBAM	Water equiva- lent (In.)	Snow, sleet (In.)	pres- sure vin.) Elev. 155 feet m.s.i.	Resultant	Resultant speed (m.p.h.)	Average speed (m.p.h.)		Direction	Hours and tenths	Percent of possible	Sunrise to sunset	Midnight to midnight	- Factor
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- Extreme temperatures for the month. May be the last of more than one occurrence.

  Below zero temperature or negative departure from mormal.

  Also on an earlier date, or date.

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  In the Hourly Precipitation table and in columns and an earlier date and an amount too small to the measure.

  These season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins with July for heating the season for degree days begins the season for

\$, 10, and 11 indicates an amount too small to measure.

The season for degree days begins with July for heating and with January for cooling.

Data in columns 6, 12, 13, 14, and 15 are based on 8 observations per day at 3-hour intervals.

Wind directions are those from which the wind blows. Resultant wind is the vector sum of wind directions and speeds divided by the number of observations. Figures for directions are tens of degrees from treason of the column of the control of the column of the colum

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I certify that this is an official publication of the Environmental Science Services Administration, and is compiled from records on file at the National Weather Records Center, Asheville, North Carolina 28801.

William X. Haggard Director, National Weather Records Center

SUMMARY BY HOURS
A V E R A G E S

WHO THE STATE OF THE ST

# LOCAL CLIMATOLOGICAL DATA

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. MAY 1969 U. S. DEPARTMENT OF COMMERCE - MAURICE B. STANS, Secretary

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- Extreme temperatures for the month. May be the last of more than one occurrence.

  Below zero temperature or negative departure from

2, 16, and 11 indicates an amount, not summarise, neasons for degree days begins with July for heating I with January for cooling.

In the columns 6, 12, 13, 14, and 16 are based on 8 reventions per day at 3-hour internals, the wind blows, mittant wind in the vector sum of wind directions 1 speeds divided by the number of observations, rurse for directions are tens of degrees from true this. 4, 69 = East, 18 = South, 27 = West, 36 = North 16 = East, 18 = South, 27 = West, 36 = North 16 = Calina. When directions are in tens of degrees Cel. 17, earties in Cel. 16 are fashed observed diseate aspeeds. If the / appears in Cel. 17, speeds gents.

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William H. Haggard

Director, National Weather Records Center

Henr Cocal tim	Sky cover (In troths)	Station pressure (In)	Dry bulb	Wet bulb	Ret. hum.	yuod mag	M'ind apred (in p.h.)	Direction	O Perce (u a lu)
	Hear Closest three	Hour (Local time Sky cover (In tenths)	Hour Second Bereaum (In tentral Station (In)	(FP) buller	intro (intro)  (intro	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	# 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1

SUMMARY BY HOURS

# LOCAL CLIMATOLOGICAL DATA

U. S. DEPARTMENT OF COMMERCE - MAURICE H. STANS, Secretary

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. JUNE 1969

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t						Dogre	e days		on dates	Sleet.		_	pres-					test					1
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HOURLY PRECIPITATION (Water equivalent in inches) - ENTRIES OF TRACE MAY BE INCOMPLETE.

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- Extreme temperatures for the month. May be the last of more than one occurrence. Below zero temperature or negative departure from sormal.

  > 70° at Alaskan stations. Also on an earlier date, or dates. Heavy fog restricts visibility to ¼ mile or less. In the Hourly Precipitation table and in columns 9, 10, and 11 indicates an amount too small to measure.

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William W. Haggard

Director, National Weather Records Center

# LOCAL CLIMATOLOGICAL DATA

SAN FRANCISCO, CALIFORNIA

		•	rempera	ture (	12 F)				ther types	·	52 ft. Precip	itation	Stand Avg.	1		Wind			Sunsi	nine	Sky	cover
	Maximum	Minimum	Average	Departure from normal	Average dew point	(Bas	ee days	1-9	E .	Sleet, or Ice on	Water equiva- lent (In.)	Snow, sleet (In.)	pres- sure (In.) Elev. 155 feet m.s.l.	esultant rection	Resultant speed (m.p.h.)	Average speed (m.p.h.)		Direction Direction	Hours and	Percent of possible		Midnight to
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Rute				5	6	ng at	HOUR.	7	10 11	12	1	2	3	P	. M. I	lour er	iding 7	at 8	9	10	11	12
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# LOCAL CLIMATOLOGICAL DATA

U. S. DEPARTMENT OF COMMERCE - MAURICE H. STANS, Secretary

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. AUGUST 1969

		7	l'empera	iture (°	F)			Weather types shown by code	Snow	Precipi	tation	Avg.			$\boldsymbol{Wind}$			Sunsh	ine	Sky	cover nths)
				la:		(Base	e days	1-9 on dates of occurrence	Sleet, or	Water equiva- lent	Snow, sleet (In.)	pres- sure (In.)		p.h.)	paads	Fas m	test ile	F			
	Maximum	Minimum	Average	Departure from normal	Average dew point	i	Cooling	For Heny Fog Thunderator Sheet Hail Glave Duststorm Smoke, Haza Smoke, Haza Blowing Smoke, Haza	at OBAM (In.)	(In.)	•••	1	1 1	Resultant speed 'm.	Average s (m.p.h.)	Speed (m.p.h.)	Direction	Hours and tenths	Percent of possible	Sunrise to	Midnight
	2 59 72 72 73 71 73 71 69 69 65 65 63 66 60 63 66 62 67 73 88 88 88 65 74 87 73 74 88 88 88 86 74 74 74 75 75 75 75 75 75 75 75 75 75 75 75 75	3 51 51 55 56 57 52 52 52 52 52 52 52 52 52 52 52 52 52	of days			-3	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	DATA ARE NOT EXTERED IN THIS COLUMN BECAUSE ARECORDS OF WEATHER TYPES MAY BE INCOMPLETE OF FOR PART OF THE DAY	9 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	0 0 0 0 0 Total 7 Dep.	11 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0		s and	14	mon	Date:		18 12-1 14-1 14-1 14-1 14-1 14-1 14-1 14-1	100 100 100 100 100 100 100 100 98 85 94 100 88 70 93 74 100 88 70 93 100 80 100 100 100 100 100 100 100 100	ound of	Sum Avg
Ľ	≥ 32°	≥ 90° 1	₹ 3	0	<b>0</b> ≤ 0,	_Dep. 26	Dep.	Heavy fog Y PRECIPITAT	X	Ţ	1		_ 0		# NC	DAT	x FOR	0 17TH	DAY.		ETE.
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					T	T	Ŧ														
ı.,		temperatu						ny errors detected				anger :-									

9. 10. and 11 indicates an amount too small to measure.
The acason for degree days begins with July for heating and with January for cooling.
Data in columns 6. 12, 13, 14, and 15 are based on 8 observations per day at 3-hour intervals.
Wind directions are those from which the wind blows.
Wind directions are those from which the wind blows and apeeds divided by the number of observations and apeeds divided by the number of observations. Figures for directions are tens of degrees from true North; i.e., 09 = East, 18 = South, 27 = West, 36: "North. and 00 = Calm. When directions are in tens of degrees in Col. 17, entries in Col. 16 are fastest observed 1-minute apeeds. If the / appears in Col. 17, speeds are gusts.

should be made payable and remittances and correspondence should be sent to the Superintendent of Documents, U. S. Government Printing Office, Washington, D. C. 20402.

I certify that this is an official publication of the Environmental Science Services Administration, and is compiled from records on file at the National Weather Records Center, Asheville, North Carolina 28801.

William X. Haggard Director, National Weather Records Center



# LOCAL CLIMATOLOGICAL DATA

U. S. DEPARTMENT OF COMMERCE - MAURICE H. STANS, Secretary ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION ENVIRONMENTAL DATA SERVICE

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. SEPTEMBER 1969

La	titude 37	47 N	Lo	ngitude	122	<u>25</u>	¥ .	Elevation (ground	<u> </u>	52 ft.		Standa	rd t	ime u	sed: s	ACLE	10	,				_
]		7	'empera	ture (°	<b>(F</b> )			Weather types shown by code	Snow:	Precipi	tation	Avg.			Wind			Sunst	ine		cover nths)	
	am a	Ę		ure ormal	ge oint	(Base	e days 65°)	1-9 on dates of occurrence	Sleet, or	Water equiva- lent (ln.)	Snow, sleet (In.)	pres- sure (In.) Elev.	ant on	ant (m.p.h.)	paeds ag	n	stest iile	pue	ıt rible	2	Q.	1
Date Date	Maximum	Minimum	Average	Departure from normal	Average dew point	Heating	Cooling	Fog X Heavy Fog X Thunderstorm Thunderstorm Glaze Glaze Dustatorm Blowing Snow	(ln.)			feet m.s.l.	Resultant direction	Resultant speed 'm	Average (m.p.h.)	Speed (m.p.h.	Direction	Hours	Percent of possible	Sunrise	Midnight t midnight	1
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	Maximu			mum Te		524	21	Thunderstorm				<del></del>		w, Sie	et		now,	n i	ice ar	u date		ļ
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HOURLY PRECIPITATION (Water equivalent in inches)—ENTRIES OF TRACE AMOUNTS MAY BE INCOMPLETE

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- nme temperatures for the month. May be the last ore than one occurrence. v zero temperature or negative departure from

8, 10, and 11 indicates an amount too ansall to measure. The season for degree days begins with July for heating and with January for cooling.

Data in columns 6, 12, 1, and 15 are based on 8 but a columns 6, 12, 1, and 15 are based on 8 Wind directions are those from which the wind blows. Resultant wind is the vector sum of wind directions. Resultant wind is the vector sum of wind directions. Regures for directions are tens of degrees from true Rorth; i.e., 60 = East, 18 = South, 27 = West, 35 = Morth, and 60 = Callon. When directions are in tens of degrees in Col. 17, exprise in Col. 16 are fastest observed 1.minute agreeds. If the / appears in Col. 17, speeds are guests.

iption Price: Local Climatological Data \$1.00 har including annual Summary if published copy: 10 cents for monthly Summary: 15 for annual Summary. Checks or more orders be made payable and remittances and cornect should be sent to the Superintendent of checks. Superintendent of the Sup

William # Haggard Director, National Weather Records Center

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Clocal thr	Sky cover (In tenths)	Station pressure (In.)	Dry bulb	Wet bulb	Rel. hum.	Dew Puint	Pared Pile ( u b u)	Direction	Speed (H p.h.)

SUMMARY BY HOURS



LOCAL CLIMATOLOGICAL DATA
U.S. DEPARTMENT OF COMMERCE
MAURICE H. STANS, Secretary
ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION
ENVIRONMENTAL DATA SERVICE

SAN FRANCISCO, CALIFORNIA FEDERAL DEFICE BLDG.

	<u>47′ N</u>		ture (		25	<b>X</b>	Elevation   Weather	types		52 ft. Precipi	tation	Standa Avg.			Wind	ACIE	10	Sunsh	ine	Sky	
Maximum	Minimum	Average	Departure from normal	Average dew point	Heating	65°)	shown by 1-9 on of occur 123 45 Magnetics Average Services 8				Snow, sleet (In.)	station pres- sure (In.) Elev. 155 feet m.s.l.	1 1	Resultant speed 1m.p.h.)	Average speed (m.p.h.)	Fas m ('4'd''E)	ile	Hours and tenths	Percent of possible	O Sunrise to Sunset	25 Midnight to repr
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						HOUR	LY PREC	PITAT	ION 1	Water eq	uivalent	in inch						ES MAY	35	1 NC DM	<u></u>
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# LOCAL CLIMATOLOGICAL DATA U.S. DEPARTMENT OF COMMERCE MAURICE H. STANS, Secretory

ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION ENVIRONMENTAL DATA SERVICE

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. NOVEMBER 1969

	7	Гетрега																			
		conpera	ture (	F)			Weather types shown by code	Snow	Precip	itation	Avg. station	!		Wind			Sunsi	ine		cover nths)	
Maximum	Minimum	Average	Departure from normal	Average dew point		e days : 65°)	1-9 on dates of occurrence 123 456 789	Sleet, or Ice on ground	Water equiva- lent (In.)	Snow. sleet (In.)	pres- sure (In.) Elev. 155 feet m.s.l.	Resultant direction	Resultant speed (m.p.h.)	Average speed (m.p.h.)		Direction	Hours and tenths	Percent of possible	Sunrise to sunset	Midnight to midnight	Date
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- Extreme (emperatures for the month. May be the last of more than one occurrence.

  Below zero temperature or negative departure from

- Below zero temperature or negative departure from normal. 5 70° at Alaskan stations. Also on an earlier date, or dates. Heavy fog restricts visibility to ¼ mile or less. In the Hourly Praccipitation table and in columns 8, 10, and 11 indicates an amount-too small to

B, 10, and 11 indicates an amount too small to measure.

The season for degree days begins with July for heating and with January for coloins.

The season for degree days begins with July for heating and the statement of the st

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certify that this is an official publication of the Environmental Science Services Administration, and is compiled from records on file at the National Weather tecords Center, Asheville, North Carolina 28801.

William pl. Haggar

SUMMARY BY HOURS

A V E R A G E S

OF THE PROPERTY OF THE PROP

USCOMM-ESSA-ASHEVILLE

300



#### LOCAL CLIMATOLOGICAL DATA

U.S. DEPARTMENT OF COMMERCE
MAURICE H. STANS, Socretory
ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION ENVIRONMENTAL DATA SERVICE

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. DECEMBER 1969

L	atitude 37	47' N	L	ongitude	122	25	¥	Elevation (ground	)	52 ft.		Standa	ard t	ime u	sed: p	ACIF	10					
	1	:	Tempera	ature (	<b>F</b> )			Weather types shown by code	Snow	Precip	itation	Avg.			Wind			Sunsi	ine		cover	
							e days		Sleet, or	Water	Snow.	pres- sure			_		stest nile			(16)	iins,	ł
Date	Maximum	Minimum	Average	Departure from normal	Average dew point	Heating	Cooling	123 456 789	Ice on ground at	equiva-	sleet (In.)	(In.)	Resultant direction	Resultant speed (m.p.h.)	Average speed (m.p.h.)	Speed (m.p.h.)	_	Hours and tenths	Percent of possible	Sunrise to sunset	Midnight to midnight	Date
1	2 66*	3	58	5	6	7A 7	7B	8	9	10	_11_	12	13	14	15	16	17	18	19	20	21	22
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	Avg. 60.4	Avg. 51.2	Avg. 55.8	Dep.	Avg.	Dep. -111	Dep.	Precipitation	13	Dep. 1.88						Date:	19	Possible 297.7	month	Avg.	Avg.	1
					-	Season	to date	Snew, sleet														4
	Maximu	Number m Temp.		mum Te	mp.	Total 1074	Total 44	> 1.0 inch Thunderstorm	. 0	Gre	atest in	24 hour	s and	date:	5 a:			t depth				Ì
	≥ 32	≥ 90°‡	₹ 32	2°   :	< 0°	Dep.	Dep.	Heavy fog			19-20	$\pm$	0	w. Die	er		myn,	sleet or	c an	u cate	<del></del>	i
į	0	0	] 0		0	-131																•

HOURLY PRECIPITATION (Water equivalent in inches) - Entries of Trace amounts may be incomplete

- 3				A.	M. Ho	ur endi											P. M.	Hour e	nding	at					13
- 4	1	2	13_	1 4	5	6	7	8	9	10	11	12	1	2	3	4	5	6	7	8	9	10	11	12	ļå
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16		.01	.03 ,01 .01	.18	.08 .01 .07 .02	.09	.25	.10	.01	.01	•02	.04	.01	-02	Ŧ		т	7	.01			.05	.06	.02	12345678901123456
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29 30																									28 29 30

- Extreme temperatures for the month. May be the last of more than one occurrence.
   Below zero temperature or negative departure from normal.
   70° at Alaskan stations.
   Also on an earlier date, or dates.
   Heavy for restricts visibility to ¼ mile or less.
   T la the Hourly Precipitation table and in columns 9, 10, and 11 indicates an amount too small to measure.

9, 10, and 11 indicates an amount too small to measure.

The season for degree days begins with July for heating and with January for cooling.

Data in columns 5, 12, 13, 14, and 15 are based on 8 observations per day at 3-hour intervals.

Wind directions are those from which the wind blows.

Wind directions are those from which the wind blows and speeds divided by the number of observations and speeds divided by the number of observations. Figures for directions are tens of degrees from true North; i.e., 69 = East, 18 = South, 27 = West, 36 = North and 00 = Calm. When directions are in tens of degree in Col. 17, entries in Col. 16 are fastest observed 1.mlaute speeds. If the / appears in Col. 17, speeds are gusts.

Any errors detected will be corrected and changes in summary data will be annotated in the annual summary.

Subscription Price: Local Climatological Data \$1.00 per year including annual Summary if published. Single copy: 10 cents for monthly Summary: 18 summary: 18 to the property of the property

I certify that this is an official publication of the Environmental Science Services Administration, and is compiled from records on file at the National Weather Records Center, Asheville, North Carolina 28801.

William W. Haggard

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0 1 5	Hour (Local trm	Sky cover (In tenths)	Station pressure (In.)	Dry bulb	Wet bulb	Rel hum.	Dew point	(ud u) (u by)	Direction	Speed (H p.h.)	
f f											
he is											

SUMMARY BY HOURS

Director, National Weather Records Center



#### LOCAL CLIMATOLOGICAL DATA

U.S. DEPARTMENT OF COMMERCE

MAURICE H. STANS, Secretory
ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION ENVIRONMENTAL DATA SERVICE

SAN FRANCISCO, CALIFORNI: FEDERAL OFFICE BLDG. JANUARY 1970

	Sky cover (Tenths)  Of service of											
Degree days (Base 65')   Degree days (Base 6	Sunrise to sunset Midnight midnight											
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Maximum Terro   Minimum Temp. 1408   0 Thunderstorms   Precipitation   Snow, Sleet snow, sleet or ice and	ed date											
≥ 32'   > 90' \$   ≥ 32'   ≥ 0' Dep. Dep. Heavy fog X   2,31   20-21   0   0												
HOURLY PRECIPITATION (Water equivalent in inches) ENTRY OF TRACE AMOUNTS MAY BE	: INCOMPLE											

9 10 11 12 234547890112345678901223345678901 .01 .13 .01 .01 .02 ,o1 .01 .01 .07 .03 .05 .01 .01 .02 .01 .02 .05 .04 .01 .01 .01 .01 .06 .07 .04 .02 .01 .01 -01 .03 .04 .01 .01 .03 .31 .00 .08 .01 .09 .13 .17 .12 .0! . 05 . 05 .07 .07 .05 .08 .06 .02 .09 .12 .12 .01

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pormal.

5.76° at Alaskan stations.

Also as an earlier date, or dates.

Heavy 1.ºg restricts visibility to 14 mile or less.

Be the House's Precipitation table and in columns 8, 10, and 11 indicates an amount too small to

8. 10, and 11 solutates an amount too small to measure.

measure for degree days begins with July for heating and with Jar zary for cooling.

Data is columns 6. 12, 13, 4, and 15 are based on 8 observations pre day at those intervals.

Membranes of the state of the state of the state of the state of the state of the state of directions and speeds divided by the number of observations. Figures for directions are tens of degrees from true.

Morth 12. 09 = East, 18 = South, 27 = West, 36 = North, and 60 = Calm. When directions are in tens of degrees in Cel. 17, entries in Col. 16 are fastest observed 1-minute speeds. If the / appears in Cel. 17, speeds are guests.

Any errors detected will be corrected and changes in summary data will be annotated in the annual summary.

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Subscription Price: Local Climatological Data \$1.00 per year including annual Summary if published. Single copy: 10 cents for monthly Summary: 15 cents for annual Summary. Checks or money orders abould be made payable and remittances and correspondence should be sent to the Superintendent of Documents, U. S. Government Printing Office, Washington, D. C. 20402.

I certify that this is an official publication of the Environmental Science Services Administration, and is compiled from records on file at the National Weather Records Center, Asheville, North Carolina 28801.

William W. Haggard

9		Α\	ER	AG	ES			No.	ultent rind
(Local tim	Sky cover in tenthal	Station pressure (In)	Dry bulb	Wet bulb	Rel. hum	Dew point	Wind spec (m.p.h.)	Direction	Speed (m.p.h.)

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LOCAL CLIMATOLOGICAL DATA
U.S. DEPARTMENT OF COMMERCE
MAURICE H. STANS, Secretory
ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION
ENVIRONMENTAL DATA SERVICE

SAN FRANCISCO, CALIFORNIA FEDERAL DEFICE BLDG. FEBRUARY 1970

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				la l			ree day se 65	s of	9 on d occurr 3 456	lates ence 789	Sleet. or Ice on	Water equiva-	Snow, sleet	pres- sure (In.)		, h.i	paads		stest nile				g g
	Maximum	Minimum	Average	Departure from normal	Average dew point	Heating	Cooling		Thunderstor Sheet Hall	Ex	at OBAM	lent (In.)		Elev. 155 feet m.s.l.	Resultant	Resultant speed 'm.j	Average s (m.p.h.)	Speed (m.p.h.)	Direction	Hours and tenths	Percent of possible	Sunrise to sunset	Midnight 1 midnight
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LOCAL CLIMATOLOGICAL DATA
U.S. DEPARTMENT OF COMMERCE
MAURICE H. STANS, Secretary
ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION
ENVIRONMENTAL SERVICE ENVIRONMENTAL DATA SERVICE

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. MARCH 1970

1		Lo Cempera	ture (*	F)			Weather types		Precipi	tation	Avg.			Wind	ACIE	-	Sunst	ine		cover	$\Gamma$
Maximum	Minimum	Average	Departure from normal	Average dew point	(Base	c days (65°)	of occurrence	Sleet, or Ice on ground at	Water equiva- lent (In.)	Snow, sleet (In)	pres- sure (In.) Elev. 155 feet m.s.l.	Resultant	Resultant speed (m.p.h.)	Average speed (m.p.h.)		Direction	Hours and tenths	Percent of possible	Sunrise to	Midnight to says	i
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Entreme temperatures for the month. May be the last of more than one occurrence.

Below zero temperature or negative departure from

are messor: ser eserve only begins with July for heating and with Justimer for cooling.
Data in commune 6, 12, 13, 14, and 15 are based on 8 observations per day at 3-hour intervals.
Wind directions are those from which the wind blows. Bouthant wins in the except manner of observations. Figures for directions are tens of degrees from true Horth, [i.e., 9] = East, 18 = South, 27 = Word, 36 = North, and 69 = Calps. When directions are in tens of degrees in Cal. 17 certies in Cal. 16 are fastest observed Lusiante speech. If the / appears in Col. 17, speech are gentle.

cription Price: Local Climatological Data \$1.00 year including annual Summary if published, e copy: 10 cents for monthly Summary; 15 for annual Summary. Checks or money orders do the made payable and remittances and correlated should be sent to the Superintendent of menta, U. S. Government Printing Office, inserton, D. C. 28402.

William H. Haggard

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Hour Loral 11m	Sky cover in tenthal	Stelner perseure (In)	Dry bulb	Wet bulb	Rel hum	Dew point	Wind appeal (m p h.)	Direction	Speed (m.p.h.)
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# LOCAL CLIMATOLOGICAL DATA U.S. DEPARTMENT OF COMMERCE MAURICE H. STANS, SOCRETORY ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. APRIL 1970

<u></u>				47 . N		ongitud		W	5' w El eather types on dates of occurrence				Avg. station pres-		Standa	rd tim Wind		d: PA	CIFIC Sunsi	nine		cover nths)
Maximum		Minimum	Average	Departure from normal	Average dew point	(Base	e days 65°)	3 4 5 6 7 8	Fog Heavy fog x Thunderstorm Ice pellets Hail Glaze Duststorm Smoke, Haze Blowing snow	or	Water equiva-	ice pellets (In.)	sure	Resultant	Resultant speed (m.p.h.)	Average speed (m.p.h.)	Speed (m.p.h.)	1	Hours and tenths	Percent of possible	Sunrise to sunset	Midnight to midnight
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\* Extrerre temperatures for the month. May be the last of more than one occurrence.

- Below zero temperature or negative departure from normal.

2 No. Alackan stations.

3 No. Alackan stations.

3 No. Alackan stations.

4 Heavy for pertrets visabilist to 1/6 mile or less.

T In the Hourh Precipitation table and in columns.

5 10 and 11 indicates an amount too small to measure.

The season for degree days begins with July for heating and with January for co-ding.

Data in co-lams 6, 12, 13, 14, and 15 are based on 8 observations per day at 3-hour intervals.

With directions to the vector sum of wind directions are income the vector sum of wind directions.

Fig.-res for directions are are tens of degrees from the North, i.e., (5 = East, 18 = South, 27 = West, 36 = North, and 00 = Calim. When directions are in tens of degrees in vol. 17 entries in Col. 16 are fastest observed for use speeds. If the / appears in Col. 17, speeds are guits.

Subscription Price: Local Climatological Data \$1.00 per year including annual Summary if published subscription of the published summary in published summary. Summary, 15 cents for annual Summary, Checks or money orders should be made payable and remittances and correspondence should be sent to the Superintendent of Documents, U. S. Government Printing Office, Washington, D. C. 20402.

I certify that this is an official publication of the Environmental Science Services Administration, and is compiled from records on file at the National Weather Records Center, Asheville, North Carolina 28801.

William H. Haggard

Director, National Weather Records Center

SUMMARY BY HOURS

A V E R A G E S

LEADING A COLOR OF THE Statum pressure (In)

#### LOCAL CLIMATOLOGICAL DATA

U.S. DEPARTMENT OF COMMERCE
MAURICE H. STANS, Secretary
ENVIRONMENTAL SCIENCE SERVICES ADMINISTRATION ENVIRONMENTAL DATA SERVICE

SAN FRANCISCO, CALIFORNIA FEDERAL OFFICE BLDG. MAY 1970

Weather types on dates of occurrence occurrence 1 Fog or lee on 1 Fog occurrence 2 Heavy fog a fee on equivalence of 1 Heavy fog a fee on equivalence occurrence occu Elevation (ground) Standard time used: PACIFIC Latitude 37' 47' N Longitude Ave. Sunshine Sky cover (Tenths) Temperature ('F) station Snow, pres-sure Degree days (Base 65°) ice pellets In. sure III.

Blecklion the Resultant Speed (m.p.h.)

Average speed (m.p.h.) mile Departure from normal Average dew point Percent of possible Sunrise to sunset Midnight to midnight Minimum Speed (m.p.h.) Direction Maximum Cooling Date 7B 10 12 13 14 3544444554455565544465555445555 5 8 8 4 4 4 4 4 3 9 3 5 5 4 0 2 0 2 0 2 0 2 0 3 4 0 4 6 4 2 6 77275580643349 19856247294961373 BECAUSE BE INCOMPLETE COLUMN 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 27 28 29 30 KY TYPES × ENTERED OF WEATHER ĬĢ. ARE Possible month Avg. Avg. 640.6 77 Avg Dep Dep Greatest depth en ground of ice pellets or ice and date Dep. 0

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- Extreme temperatures for the month. May be the last of more than one occurrence. Below zero temperature or negative departure from

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Any errors detected will be corrected and changes in summary data will be annotated in the annual summary.

Subscription Price: Local Climatological Data \$100 per year including annual Summary of published Single copy: 10 cents for monthly Summary: 15 cents for annual Summary. Checks or morey orders should be made payable and remittances and correspondence should be sent to the Superintendent of Documents. U. S. Government Printing Office, Washington, D. C. 20402

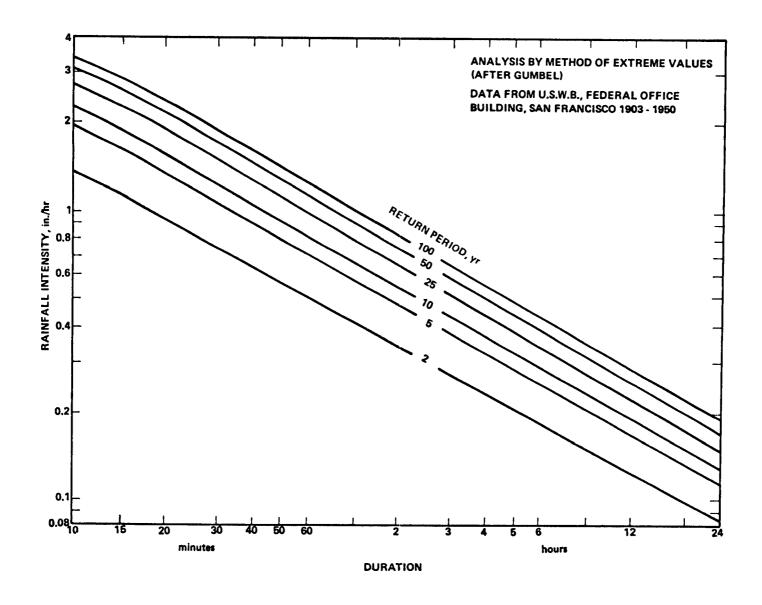
I certify that this is an official publication of the Environmental Science Services Administration, and is compiled from records on file at the Natural Weather Records Center, Asheville, North Carolina 28801.

Willia N. Haggar

Director, National Weather Records Center

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SUMMARY BY HOURS



Appendix D. RAINFALL INTENSITY-DURATION-FREQUENCY RELATIONSHIPS

# Appendix E CHARACTERISTICS OF COMBINED SEWAGE BULK SAMPLE 4-5 April 1969

Time	2230	2320	0020 ·	0120	0220
Flow, cfs	0.297	0.050	0.606	0.518	0.022
Total Solids, mg/l	575	130	80	44	85
Total Volatile Solids, mg/l	420	50	25	16	25
Total Suspended Solids, mg/l	426	26	9	19	22
Total Volatile Suspended Solids, mg/l	373	15	5	12	12
Settleable Solids, ml/l	_	_	-	_	-
Floatables, mg/l	-	-	_		-
Particle Size Distribution, mg/l	-	st-s	=-	-	_
>3. 327 mm	-	-	-	-	-
3. 327-0. 991 mm	-	-	-	-	-
0.991-0.295 mm	-	-	-	-	-
0.295-0.074 mm	-	-	-	-	=
<0.074 mm	-			-	-
size at 50-percentile by weight, mm	•••	-	-	-	<del>-</del>
BOD, mg/l	202	11	3	4	5
COD, mg/l	480	55	19	38	38
Hexane Extractable Material, mg/l	12.7	2,5	1.3	10.3	1.7
Total Coliforms, MPN/100 ml	$1.5 \times 10^{7}$	$2.8 \times 10^{5}$	$9.3 \times 10^4$	2. <b>1</b> ×10 <sup>5</sup>	$2.4 \times 10^{6}$
Fecal Coliforms, MPN/100 ml	$4.6 \times 10^{5}$	$9.1 \times 10^{3}$	$4.3 \times 10^4$	$2.3 \times 10^4$	$2.3 \times 10^4$
Fecal Streptococci, MPN/100 ml	$<7.3 \times 10^4$	$<1.5 \times 10^3$	$<4.3 \times 10^3$	$<7.5 \times 10^3$	$<4.3 \times 10^3$

#### 5 November 1969

Time	0520	0620	0720	0820	0920
Flow, cfs	0.591	0.711	0.706	0.499	0.075
Total Solids, mg/l	148	140	180	220	432
Total Volatile Solids, mg/l	40	44	64	112	224
Total Suspended Solids, mg/l	34	45	63	57	185
Total Volatile Suspended Solids, mg/l	15	31	24	40	131
Settleable Solids, ml/l	5	0.7	1	0.6	0.7
Floatables, mg/l	1.4	2.4	3.9	2.3	11.8
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0.991 mm 0. 991-0. 295 mm 0. 295-0.074 mm <0.074 mm size at 50-percentile by weight, mm	0 0 trace trace 16.3	trace trace trace 4.1 18.4	trace trace 5.5 5.6 34.5 0.018	14. 4 11. 2 42. 5 22. 9 69. 5 0. 14	29.5 14.3 36.5 33.4 135.7 0.05
BOD, mg/l	9.5	11.0	11	61	175
COD, mg/l	51.6	62,5	82.5	132.4	626
Hexane Extractable Material, mg/l	4.1	4	3.8	7.2	14.5
Total Coliforms, MPN/100 ml	$2.3 \times 10^{5}$	$2.3 \times 10^5$	$3\times10^4$	$4.3 \times 10^6$	$2.3 \times 10^6$
Fecal Coliforms, MPN/100 ml	$3 \times 10^{4}$	$3\times10^4$	$3x10^4$	$4.3 \times 10^{6}$	9x10 <sup>5</sup>
Fecal Streptococci, MPN/100 ml	$9 \times 10^{3}$	$4.3 \times 10^4$	$9 \times 10^{3}$	$4.3 \times 10^5$	$3\times10^4$

#### Appendix E (continued)

#### CHARACTERISTICS OF COMBINED SEWAGE BULK SAMPLE 19 December 1969

Time	1045	1145	1240 ·	1340	1440
Flow, cfs	0.375	0.447	0.413	0.073	0.046
Total Solids, mg/l	95	115	135	415	275
Total Volatile Solids, mg/l	50	65	60	180	125
Total Suspended Solids, mg/l	19	46	31	112	84
Total Volatile Suspended Solids, mg/l	9	31	21	70	55
Settleable Solids, ml/l	0.2	1.5	1	3. 5	2, 5
Floatables, mg/l	7.1	3, 6	4. 2	4.4	3.9
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0.991 mm 0. 991-0. 295 mm 0. 295-0. 074 mm <0. 074 mm size at 50-percentile by weight, mm	0 0 2.9 5.3 10.8 0.054	0 1.7 4.2 12.5 27.6 0.049	0 4.8 11.6 11.8 2.8 0.34	56.9 5.1 16.3 27.7 6 0.45	6.3 4 8.9 24.6 44.2 0.074
BOD, mg/l	14.7	15	16.8	77.4	40.5
COD, mg/1	76.8	57.6	57.6	221	144
Hexane Extractable Material, mg/l	4.1	6.1	4.8	36. 3	1.6
Total Coliforms, MPN/100 ml	$1.5 \times 10^{5}$	$4.6 \times 10^{6}$	$4.6 \times 10^6$	$2.4 \times 10^6$	$4.6 \times 10^6$
Fecal Coliforms, MPN/100 ml	9. $3 \times 10^4$	$4.3 \times 10^{5}$	$2.4x10^6$	$4.6 \times 10^{5}$	$4.6 \times 10^{5}$
Fecal Streptococci, MPN/100 ml	$7.5 \times 10^3$	$4.3 \times 10^3$	$2.3 \times 10^3$	$1.1 \times 10^{5}$	$>1.1 \times 10^{5}$

#### 21 December 1969

	Time	930	1025	1125	1225	1410
	Flow, cfs	0.910	0.175	0.169	0.105	0.070
	Total Solids, mg/l	110	280	210	250	400
	Total Volatile Solids, mg/l	80	165	115	140	140
	Total Suspended Solids, mg/l	55	89	79	98	118
	Total Volatile Suspended Solids, mg/l	42	76	64	68	94
	Settleable Solids, ml/l	2.5	13	4.5	2, 5	7
	Floatables, mg/l	2.3	1.5	3.6	3.5	4.2
117	Particle Size Distribution, mg/l >3. 327 mm 3. 327-0.991 mm 0. 991-0. 295 mm 0. 295-0. 074 mm <0. 074 mm size at 50-percentile by weight, mm	8.8 14.1 9 15.1 8 0.54	0 8.6 32.4 18.1 29.9 0.22	0 5.9 13.0 14.7 45.4 0.047	0 20.2 16.3 25.8 35.7 0.15	0 8.3 34.7 19.5 50.7 0.11
	BOD, mg/1	32.6	75.9	56.4	62.4	102
	COD, mg/1	86.4	158	182	154	257
	Hexane Extractable Material, mg/l	4.4	2.5	5.1	6.7	28, 5
	Total Coliforms, MPN/100 ml	4.6x10 <sup>5</sup>	$2.4 \times 10^6$	$2.4 \times 10^{6}$	$9.3 \times 10^{5}$	$4.6 \times 10^{6}$
	Fecal Coliforms, MPN/100 ml	4. $3 \times 10^4$	$2.4 \times 10^6$	$2.4 \times 10^6$	$4.6 \times 10^{5}$	$4.6 \times 10^6$
	Fecal Streptococci, MPN/100 ml	$9.1 \times 10^{2}$	-	•	-	$2.4x10^4$

## CHARACTERISTICS OF COMBINED SEWAGE BULK SAMPLE 13 January 1970

Time	1800	1900	2100	2200	2300
Flow, cfs	0.685	0.056	0.094	0.095	0.080
Total Solids, mg/l	170	520	250	195	245
Total Volatile Solids, mg/l	70	370	170	95	140
Total Suspended Solids, mg/1	75	376	72	66	119
Total Volatile Suspended Solids, mg/l	56	332	67	61	74
Settleable Solids, ml/l	2.3	2.8	3	4.5	2, 8
Floatables, mg/l	6	9.5	5.2	6.9	<b>3.</b> 6
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0. 991 mm 0. 991-0. 295 mm 0. 295-0. 074 mm <0. 074 size at 50-percentile by weight, mm	- - - -	- - - -	- - - -	- - - -	- - - -
BOD, mg/l	<10	-	33	35	17
COD, mg/l	96	297	129	144	77
Hexane Extractable Material, mg/l	5.9	54.4	29.5	16.9	7.6
Total Coliforms, MPN/100 ml	1.6x10 <sup>7</sup>	$4.3 \times 10^6$	$9.3 \times 10^6$	$2.9 \times 10^{6}$	$9.3 \times 10^6$
Fecal Coliforms, MPN/100 ml	1.2x10 <sup>6</sup>	$2.3 \times 10^{5}$	$1.4 \times 10^{5}$	$4.3 \times 10^{5}$	9.1x10 <sup>4</sup>
Fecal Streptococci, MPN/100 ml	$1.4 \times 10^4$	$4.3 \times 10^4$	$3.6 \times 10^3$	$9.1 \times 10^{3}$	$< 3 \times 10^{3}$

## 20 January 1970

Time	1625	1725	1835	1930	2030
Flow, cfs	1.05	0.605	0.894	0.431	0.556
Total Solids, mg/l	84	84	184	148	60
Total Volatile Solids, mg/l	48	16	68	72	36
Total Suspended Solids, mg/1	29	30	15	33	17
Total Volatile Suspended Solids, mg/l	19	23	14	28	16
Settleable Solids, ml/1	0.2	1.2	0.2	0.2	0.6
Floatables, mg/l	4.2	22.3	3.9	4.7	2.8
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0.991 mm 0. 991-0. 295 mm 0. 295-0.074 mm <0.074 mm size at 50-percentile by weight, mm	0 0.5 2.1 6.2 10.2 0.065	0 1.6 5.7 5.1 17.6 0.036	0 1.3 2.6 4 7.1 0.084	0 2,6 2 4,2 25,2 0,01	0 0.9 1.5 4.8 9.8 0.055
BOD, mg/1	21. 2	18.2	7.97	30.4	12.7
COD, mg/1	72	127	311	349	43
Hexane Extractable Material, mg/l	2	44	3.8	10.4	5
Total Coliforms, MPN/100 ml	$3\times10^4$	$3.6 \times 10^4$	$7.3 \times 10^4$	$3.6 \times 10^4$	$3.6 \times 10^4$
Fecal Coliforms, MPN/100 ml	<3x10 <sup>4</sup>	$3.6 \times 10^4$	$7.3 \times 10^4$	$3.6 \times 10^4$	$3.6 \times 10^4$
Fecal Streptococci, MPN/100 ml	$2.3 \times 10^4$	$2.3 \times 10^4$	$9.1 \times 10^3$	$3.6 \times 10^{3}$	$7.3 \times 10^3$

#### Appendix E (continued)

#### CHARACTERISTICS OF COMBINED SEWAGE BULK SAMPLE 27 January 1970

Time	0130	0230	0345.	0430	0530
Flow, cfs	1, 23	0.603	0.176	0.058	0.039
Total Solids, mg/l	95	60	73	72	90
Total Volatile Solids, mg/l	55	32	40	37	43
Total Suspended Solids, mg/l	8	4	6	6	6
Total Volatile Suspended Solids, mg/l	7,5	4	6	5	6
Settleable Solids, ml/l	0.3	0.1	0.2	0.05	0.05
Floatables, mg/l	1, 4	1	0.8	0.6	0.9
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0.991 mm 0.991-0.295 mm 0.295-0.074 mm <0.074 mm size at 50-percentile by weight, mm	0 1.4 3.7 9.6 12.9 0.082	0 0.2 0.9 2.4 7 0.035	0 0.2 1.7 5.5 3.9 0.11	0 0.3 0.5 1.9 7.9 0.023	0 2 1.1 1.9 8 0.028
BOD, mg/l	3. 3	<1.5	4.65	1.95	17.7
COD, mg/l	64	16.9	31	31	52 <b>.</b> 5
Hexane Extractable Material, mg/l	3. 2	3.8	2.6	2	5.4
Total Coliforms, MPN/100 ml	$2.3 \times 10^6$	9x10 <sup>5</sup>	$9 \times 10^{5}$	4. $3x_{1}^{10}$	$7x10^{5}$
Fecal Coliforms, MPN/100 ml	$4 \times 10^{4}$	<3x10 <sup>3</sup>	$<3\times10^{5}$	$<3\times10^5$	<3x10 <sup>5</sup>
Fecal Streptococci, MPN/100 ml	$2.3 \times 10^4$	$4.3 \times 10^4$	4x10 <sup>3</sup>	$2.4 \times 10^6$	1,5x10 <sup>5</sup>

#### 13 February 1970

Time	0645	0745	0845	0945	1045
Flow, cfs	1.069	0.199	0.1024	0.0932	0.079
Total Solids, mg/l	148	152	432	552	348
Total Volatile Solids, mg/l	96	72	316	248	156
Total Suspended Solids, mg/l	49	50	127	95	115
Total Volatile Suspended Solids, mg/l	29.5	33	115	80	94
Settleable Solids, ml/l	0.6	2.5	11.5	4	14
Floatables, mg/l	4.65	1.83	3.68	3.36	1.73
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0.991 mm 0. 991-0. 295 mm 0. 295-0. 074 mm <0. 074 mm size at 50-percentile by weight, mm	0 9.4 10.6 42.2 33.4 0.116	0 11.6 24.2 3.4 2.6 0.64	34. 2 9. 8 28 22. 6 12. 4 0. 64	126 56 47 43 78 1.12	0 29 18 16 62 0.076
BOD, mg/l	21	55.8	139.1	168	121.4
COD, mg/l	88, 4	176.8	353.6	402.2	371.3
Hexane Extractable Material, mg/l	12	7.7	20.2	44.1	21.5
Total Coliforms, MPN/100 ml Fecal Coliforms, MPN/100 ml	1.1×10 <sup>7</sup> 9×10 <sup>4</sup>	$2.4 \times 10^6$ $4.3 \times 10^5$	$2.4 \times 10^{6}$ $2.4 \times 10^{6}$	>1. 1x10 <sup>7</sup> >1. 1x10 <sup>7</sup>	1. 1×10 <sup>6</sup> 9. 3×10 <sup>5</sup>
Fecal Streptococci, MPN/100 ml	$4.3 \times 10^4$	$4.6 \times 10^{5}$	$2.4 \times 10^5$	$4.6 \times 10^{5}$	9. $3 \times 10^4$

#### Appendix E (continued)

# CHARACTERISTICS OF COMBINED SEWAGE BULK SAMPLE 28 February 1970

Time	0835	0935	1035	1130	1230
Flow, cfs	0.422	0.139	0.231	0,155	0.116
Total Solids, mg/l	100	184	264	200	404
Total Volatile Solids, mg/l	52	108	112	90	172
Total Suspended Solids, mg/l	23.6	43, 3	31.6	23.3	57
Total Volatile Suspended Solids, mg/l	23.3	40	27.7	20.3	52
Settleable Solids, ml/l	0.3	4.5	0.4	2.6	2.7
Floatables, mg/l	2. 2	3. 4	1.4	3.5	1.1
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0.991 mm 0. 991-0. 295 mm 0. 295-0. 074 mm <0. 074 mm size at 50-percentile by weight, mm	0 2.3 3.1 9.3 40.4 0.021	11.4 9.6 12.5 14.1 38.1 0.116	- - - -	- - - -	- - - -
BOD, mg/l	16.2	27.3	61	25	199
COD, mg/1	137	157	167	117	292
Hexane Extractable Material, mg/l Total Coliforms, MPN/100 ml Fecal Coliforms, MPN/100 ml Fecal Streptococci, MPN/100 ml	5. 4 4. $3 \times 10^5$ 2. $3 \times 10^5$ 9. $1 \times 10^2$	4. 1 2. 3×10 <sup>5</sup> 2. 3×10 <sup>5</sup> 3. 6×10 <sup>4</sup>	13 2. 3x10 <sup>4</sup> 9. 3x10 <sup>3</sup> <30	12. 2 9. 3x10 <sup>5</sup> 2. 3x10 <sup>5</sup> 4. 3x10 <sup>4</sup>	$ \begin{array}{c} 12 \\ 2. \ 3 \times 10^{4} \\ 2. \ 3 \times 10^{4} \\ 2. \ 4 \times 10^{3} \end{array} $

## 4 March 1970

Time	1100	1200	1300	1400	1500
Flow, cfs	0.230	0.124	1.130	1.51	2, 22
Total Solids, mg/l	72	100	208	300	352
Total Volatile Solids, mg/l	20	32	76	156	124
Total Suspended Solids mg/l	33,6	43	28.6	144	34
Total Volatile Suspended Solids, mg/l	17	22.3	14.6	110	26.6
Settleable Solids, ml/l	1.2	1.5	0.3	2.7	2.5
Floatables, mg/l	2, 2	2.2	1.9	3	5
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0.991 mm 0. 991-0. 295 mm 0. 295-0. 074 mm <0. 074 mm size at 50-percentile by weight, mm	1.8 0.4 2.6 5.5 7 0.108	1.4 33.2 28.5 17 22 0.49	1.1 1.6 4.1 7.6 14 0.076	3.8 2.6 6.7 11.1 118	3.8 5.1 9.2 8.9 36 0.036
BOD, mg/l	8.4	8. 2	38.8	192	31.2
COD, mg/l	18.8	59.3	115.6	306.3	146.2
Hexane Extractable Material, mg/l Total Coliforms, MPN/100 ml	6.4 4.6x10 <sup>5</sup>	12.6 >1.1x10 <sup>6</sup>	33, 2 $4.6 \times 10^{5}$	37.4 >1.1x10 <sup>6</sup>	13.2 >1.1x10 <sup>6</sup>
Fecal Coliforms, MPN/100 ml	$9.3 \times 10^4$	1.5×10 <sup>5</sup>	$4.6 \times 10^{5}$	$2.4 \times 10^{5}$	$2.4 \times 10^{5}$
Fecal Streptococci, MPN/100 ml	$4.3x10^3$	$1.1 \times 10^5$	$9.1 \times 10^{2}$	$1.1 \times 10^{5}$	$2.4 \times 10^4$

#### Appendix E (continued)

# CHARACTERISTICS OF COMBINED SEWAGE BULK SAMPLE

13 April 1970

Time	1100	1200	1300	1400	1500
Flow, cfs	0.056	0.043	0.053	0.045	0.042
Total Solids, mg/l	648	512	784	648	472
Total Volatile Solids, mg/l	392	160	392	252	184
Total Suspended Solids, mg/l	168	98	184	138	276
Total Volatile Suspended Solids, mg/l	136	88	162	132	176
Settleable Solids, ml/l	5	15	28	10	8
Floatables, mg/l	14.4	7.8	21.8	11.2	19.6
Particle Size Distribution, mg/l >3. 327 mm 3. 327-0. 991 mm 0. 991-0. 295 mm 0. 295-0. 074 mm <0. 074 mm Size at 50-percentile by weight, mm	trace 3.1 15.6 3.8 123	15 9.8 12.6 17.3 45.5 0.15	25.1 37.9 40.3 26.8 101 0.18	8.6 9.4 39.4 25.4 90 0.05	22 24, 4 21, 5 32, 6 127 0, 01
BOD, mg/l	313	134	178	2.77	145
COD, mg/l	461	299	236	567	304
Hexane Extractable Material, mg/l	55.3	26.9	83.4	59.7	34.6
Total Coliforms, MPN/100 ml	$4.6 \times 10^{7}$	$4.6 \times 10^{1}$	1. 1x10 <sup>7</sup>	1. 1×10 <sup>1</sup>	4.6x10 <sup>6</sup>
Fecal Coliforms, MPN/100 ml	$4.6 \times 10^6$	$9.3 \times 10^{5}$	4.6x10 <sup>6</sup>	$2.4 \times 10^6$	$1.5 \times 10^6$
Fecal Streptococci, MPN/100 ml	1.5x10 <sup>5</sup>	$1.1 \times 10^{7}$	1.1x10 <sup>7</sup>	4.6x10 <sup>6</sup>	$2.4 \times 10^6$

#### 13 May 1970 0630 0730 0830 Time 0430 0530 0.056 0.022 0.024 0.043 Flow, cfs 412 496 Total Solids, mg/l 372 468 748 136 104 220 312 216 Total Volatile Solids, mg/1 60.5 108 484 188 Total Suspended Solids, mg/1 69.5 83 Total Volatile Suspended Solids, mg/l 31.5 31 210 138 6 10 0.9 1.5 17 Settleable Solids, ml/l 2.2 5.3 0.6 2 3.5 Floatables, mg/1 Particle Size Distribution, mg/1 >3.327 mm 21.1 4.4 5.6 13.5 8.9 3. 327-0. 991 mm 28.3 18 22.7 15 0.991-0.295 mm 10.3 32.9 93 47.6 30.3 0.295-0.074 mm 15.6 72 168 13 14 50 <0.074 mm 0.09 0.15 0.25 size at 50-percentile by weight, mm 0.20 253 49 60.1 143 224 BOD, mg/1450 307 723 156 COD, mg/1254 12,5 20, 2 37.7 Hexane Extractable Material, mg/l 5.7 6.5 2.4x10<sup>8</sup> 1.1x10<sup>15</sup> 1. 1×10<sup>9</sup> 4. $3 \times 10^7$ 4.6x10<sup>8</sup> Total Coliforms, MPN/100 ml $2x10^7$ 1. $5 \times 10^{7}$ $3.6 \times 10^6$ $3.6 \times 10^6$ $2.3 \times 10^{7}$ Fecal Coliforms, MPN/100 ml 2.3x10<sup>12</sup> $2.9 \times 10^6$ $4.3x10^4$ $4.3 \times 10^6$ 9. $3x10^6$ Fecal Streptococci, MPN/100 ml

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Appendix F
CHARACTERISTICS OF COMBINED SEWAGE
0.5-in. SCREEN SAMPLE
4-5 April 1969

Time Start	2240	2330	2030	0130	0230
Finish	2310	0000	0100	0200	0300
Flow, cfs Start Finish	0.265 0.224	0.049 0.298	0,508 0,872	0.492 0.242	0.022 0.018
Total Solids, g	24. 4	11.4	26	26.3	9.7
Total Volatile Solids, g	20.8	10.1	23.3	24.4	8.9
BOD, mg/g	7.6	1.4	5.8	<b>3.</b> 6	1.2
COD, mg/g	27.1	9.7	27.5	21.3	12.7
Hexane Extractable Material, mg/g	2.6	0.48	1.9	1.1	0.42
Total Coliforms, MPN/g	1. $3 \times 10^8$	$1.1 \times 10^{7}$	$2.7 \times 10^{7}$	$1.3 \times 10^6$	$1.0 \times 10^6$
Fecal Coliforms, MPN/g	2.6x10 <sup>6</sup>	$4.1 \times 10^{5}$	$6.5 \times 10^{5}$	$5.0 \times 10^{5}$	$1.0 \times 10^{5}$
Fecal Streptococci, MPN/g	$<2.8 \times 10^{7}$	$< 8.4 \times 10^5$	$<1.7\times10^{7}$	$<2.9 \times 10^6$	$<2.4 \times 10^3$

#### 0.5-in. SCREEN SAMPLE

#### 5 November 1969

Time					
Start	0530	0630	0730	0830	0930
Finish	0600	0700	0800	0900	1000
Flow, cfs Start	0.603 0.693	0.595 0.509	0.516 0.508	0.399 0.088	0.058 0.055
Finish	-				
Total Solids, g	10.4	15.9	30.6	33.7	27.7
Total Volatile Solids, g	9.4	13.9	27.2	30.4	24.5
BOD, mg/g	180	349	603	507	438
COD, mg/g	864	1,428	1,122	1,865	1,200
Hexane Extractable Material, mg/g	59.3	45.2	127	160	142
Total Coliforms, MPN/g	$2.21 \times 10^{7}$	$7.55 \times 10^{7}$	$3.1 \times 10^{8}$	$2.8 \times 10^{10}$	8. 32x10
Fecal Coliforms, MPN/g	$1.42 \times 10^6$	$2.52 \times 10^6$	$4.9 \times 10^{7}$		$3.92 \times 10^6$
Fecal Streptococci, MPN/g	8.95x10 <sup>6</sup>	$2.7 \times 10^{7}$	$4.9 \times 10^{7}$	$6.8 \times 10^{7}$	1.55x10'

#### Appendix F (continued)

#### CHARACTERISTICS OF COMBINED SEWAGE 0.25-in. SCREEN SAMPLE 19 December 1969

Time Start Finish	1115 1145	1215 1240	1315 1340	1415 1440	1515 1540
Flow, cfs Start Finish	0.448 0.447	0.831 0.413	0.117 0.073	0.054 0.046	0.157 0.083
Total Solids, g	8.63	17.72	9.48	9.18	17, 42
Total Volatile Solids, g	6.98	15.62	8.08	8.08	14.19
BOD, mg/g	1,008	1,150	1,070	1,898	494
COD, mg/g	1,824	4,720	4,710	2,516	2,039
Hexane Extractable Material, mg/g	67.4	184	286	68	81.5
Total Coliforms, MPN/g	$1.74 \times 10^{8}$	$1.35 \times 10^{8}$	1.16x10 <sup>10</sup>	$1.2 \times 10^{10}$	2.64x10 <sup>9</sup>
Fecal Coliforms, MPN/g	$2.6 \times 10^{7}$	$1.35 \times 10^{8}$	$1.16 \times 10^{10}$		1.66x10 <sup>8</sup>
Fecal Streptococci, MPN/g	$1.7 \times 10^{7}$	$1.4 \times 10^{7}$	$2.54 \times 10^{8}$	1.6x10'	6.31x10 <sup>8</sup>

# 0.25-in. SCREEN SAMPLE 21 December 1969

Time					
Start	1000	1100	1200	1340	1415
Finish	1025	1125	1225	1410	1445
Flow, cfs					
Start	0.567	0.164	0.107	0.069	0.075
Finish	0 <b>.1</b> 75	0.169	0.105	0.070	0.075
Total Solids, g	19.40	24.10	18.26	11.56	15.94
Total Volatile Solids, g	17.44	20.36	17.24	10.41	14.96
BOD, mg/g	256	506	924	477	145
COD, mg/g	2,578	3,520	4,849	4,000	1,867
Hexane Extractable Material, mg/g	161	130	236	83.5	151
Total Coliforms, MPN/g	5.66×10 <sup>8</sup>	1.91x10 <sup>8</sup>	2.52x10 <sup>9</sup>	9.51×10 <sup>9</sup>	$5.7 \times 10^8$
Fecal Coliforms, MPN/g	$3.9 \times 10^{7}$	$3.9 \times 10^{7}$	$2.4x10^{8}$	1.82×10 <sup>9</sup>	$<1.8 \times 10^{7}$
Fecal Streptococci, MPN/g	$>5.7 \times 10^{7}$	1.91×10 <sup>8</sup>	5.08×10 <sup>8</sup>	<3x10 <sup>6</sup>	$4$ $ imes$ 10 $^{7}$

#### CHARACTERISTICS OF COMBINED SEWAGE 1-in. SCREEN SAMPLE 13 January 1970

Time Start Finish	1730 1800	1830 1900	1930 2045	2130 2200	2230 2300
Flow, cfs Start Finish	0.247 0.685	0.219 0.056	0.064 0.094	0.130 0.095	0.102 0.080
Total Solids, g	11.88	15.18	8.14	9.54	7.57
Total Volatile Solids, g	10.26	13.91	7.42	8,93	6.92
BOD, mg/g	1,028	783	937	823	555
COD, mg/g	3,800	5,320	3,035	2,710	1,650
Hexane Extractable Material, mg/g	132	87.6	156	108	132
Total Coliforms, MPN/g	$3.62 \times 10^9$	1.52x10 <sup>9</sup>	$1.14 \times 10^{10}$	$7.96 \times 10^{8}$	$9.91 \times 10^{7}$
Fecal Coliforms, MPN/g	$3.03 \times 10^{9}$	1.52x10 <sup>8</sup>	$1.12 \times 10^8$	$3.78 \times 10^{7}$	$3.04 \times 10^{7}$
Fecal Streptococci, MPN/g	$3.62 \times 10^{8}$	$6.0 \times 10^{7}$	$4.79 \times 10^{7}$	1.57x10 <sup>7</sup>	5.67x10 <sup>6</sup>

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# 1-in. SCREEN SAMPLE 20 January 1970

Time					
Start	1658	1755	1900	2000	2100
Finish	1725	1835	1930	2030	2130
Flow, cfs					
Start	1, 18	1.33	0.900	0.454	0.573
Finish	0.605	0.894	0.431	0.556	1.11
Total Solids, g	28.4	17.6	26. 2	77	51.8
Total Volatile Solids, g	25.1	15.9	23	64.5	44.3
BOD, mg/g	545	346	186	525	425
COD, mg/g	1,140	5,490	5,470	2,485	1,206
Hexane Extractable Material, mg/g	117	26.5	44. 1	87.6	68
Total Coliforms, MPN/g	$2.88_{x}10^{8}$	1.36x10 <sup>8</sup>	3.56×10 <sup>8</sup>	$1.43 \times 10^8$	<5.79x10 <sup>5</sup>
Fecal Coliforms, MPN/g	<1.06×10 <sup>7</sup>	4. $16 \times 10^{7}$	$5.74 \times 10^{7}$	$5.97 \times 10^{7}$	$<5.79 \times 10^{5}$
Fecal Streptococci, MPN/g	$1.52 \times 10^{8}$	$2.04 \times 10^{7}$	$1.38 \times 10^{7}$	$1.43 \times 10^{7}$	1.80x10 <sup>6</sup>

#### CHARACTERISTICS OF COMBINED SEWAGE 0.125-in. SCREEN SAMPLE 27 January 1970

Time Start Finish	0158 0216	0314 0345	0400 0430	0500 0530	0600 0630
Flow, cfs Start Finish	1.79 0.763	0.416 0.176	0,268 0,058	0.051 0.039	0.040 0.050
Total Solids, g	19.7	11.1	7.4	8.4	5
Total Volatile Solids, g	17.1	9.9	6.5	7.8	4.6
BOD, mg/g	370	341	402	299	877
COD, mg/g	1,980	552	3,890	464	1,188
Hexane Extractable Material, mg/g	49	59.4	66.3	21.6	76.8
Total Coliforms, MPN/g	2.44×10 <sup>9</sup>	3,88×10 <sup>8</sup>	$2.74 \times 10^8$	$2.50 \times 10^8$	4.2×10 <sup>9</sup>
Fecal Coliforms, MPN/g	$7.63 \times 10^{7}$	8.11x10 <sup>6</sup>	$2.02 \times 10^{7}$	$<3.6 \times 10^4$	<6x10 <sup>4</sup>
Fecal Streptococci, MPN/g	$7.6 \times 10^3$	$3.96 \times 10^4$	$3.11 \times 10^4$	$1.11 \times 10^4$	$7.8 \times 10^4$

0.125-in. SCREEN SAMPLE
13 February 1970

Time Start	0710	0815	0915	1015	1110
Finish	0715	0825	0930	1025	1120
Flow, cfs Start Finish	0.728 0.199	0.1545 0.1024	0.0872 0.0932	0.0932 0.079	0.1374 0.079
Total Solids, g	17.9	51.2	22.5	9.7	11.1
Total Volatile Solids, g	14.5	43.3	20	8.8	8.6
BOD, mg/g	386	234	-	124	892
COD, mg/g	1,339	1,312	503	1,859	3,265
Hexane Extractable Material, mg/g	13.7	74.8	69.5	75.7	38.8
Total Coliforms, MPN/g	$8.4 \times 10^{8}$	2.9x10 <sup>9</sup>	$1.9 \times 10^{8}$	$2.48 \times 10^9$	$8.4 \times 10^{8}$
Fecal Coliforms, MPN/g	$1.7 \times 10^{7}$	5.9x10 <sup>6</sup>	$4 \times 10^7$	$2.4 \times 10^{8}$	$2.1 \times 10^{8}$
Fecal Streptococci, MPN/g	1.3×10 <sup>6</sup>	$>2.15\times10^{7}$	1.9×10 <sup>6</sup>	9.6x10 <sup>6</sup>	1.35 $\times$ 10 <sup>7</sup>

## CHARACTERISTICS OF COMBINED SEWAGE 1-in. SCREEN SAMPLE 28 February 1970

Time					
Start	0900	1000	1100	1200	1300
Finish	0930	1030	1130	1230	1330
Flow, cfs					
Start	0.570	0.111	0.195	0.109	0.116
Finish	0.139	0.231	0.155	0.116	0.011
Total Solids, g	41.4	44.3	33.5	12	20
Total Volatile Solids, g	36.9	39.9	29.7	11.16	17.9
BOD, mg/g	309	184	453	761	338
COD, mg/g	976	529	1,039	1,368	1,119
Hexane Extractable Material, mg/g	128	68.1		44.9	156
Total Coliforms, MPN/g	$1.04 \times 10^{8}$	$9.61 \times 10^{7}$	1,37×10 <sup>9</sup>	$3.58 \times 10^{8}$	$1.2 \times 10^9$
Fecal Coliforms, MPN/g	$1.04 \times 10^{8}$	$2.06 \times 10^{7}$	1. $37 \times 10^9$	1.95×10 <sup>8</sup>	$1.2 \times 10^{9}$
Fecal Streptococci, MPN/g	2.66x10 <sup>8</sup>	$1.02 \times 10^8$	$1.37 \times 10^8$	7.59x10 <sup>6</sup>	$7.5 \times 10^6$

#### 0.5-in. SCREEN SAMPLE

## 4 March 1970

Time Start	1130	1230	1330	1430	1530
Finish	1200	1300	1400	1500	1600
Flow, cfs Start Finish	0.238 0.124	0. 262 1. 130	1.33 1.51	1, 80 2, 22	2. 28 2. 66
Total Solids, g	29.1	23.4	38.7	23, 2	15
Total Volatile Solids, g	25.3	21	34.7	20.9	13.1
BOD, mg/g	443	154	321	377	295
COD, mg/g	1,420	423	1,460	1,490	659
Hexane Extractable Material, mg/g	106	97	145	102	90
Total Coliforms, MPN/g	$7.9 \times 10^{7}$	$1.54 \times 10^{7}$	$2.47 \times 10^{8}$	1.85×10 <sup>8</sup>	6. 1×10'
Fecal Coliforms, MPN/g	$7.9 \times 10^{7}$	$1.54 \times 10^{7}$	$2.47 \times 10^{8}$	9.9x10'	<2x10
Fecal Streptococci, MPN/g	8.25x10 <sup>6</sup>	3.9x10 <sup>5</sup>	$2.47 \times 10^{7}$	$9.9 \times 10^{6}$	$6.07 \times 10^6$

#### CHARACTERISTICS OF COMBINED SEWAGE 0.125-in. SCREEN SAMPLE 13 April 1970

	Time Start Finish	1130 1200	1230 1300	1330 1400	1430 1500	1530 1600
	Flow, cfs Start Finish	0.041 0.043	0.029 0.053	0.061 0.045	0.0278 0.042	0.030 0.027
_	Total Solids, g	27.4	32.8	27.9	16.8	18.1
36	Total Volatile Solids, g	22, 2	28.1	24, 2	12.8	12.6
	BOD, mg/g	429	729	623	584	586
	COD, mg/g	1,110	1,345	1,280	3,010	1,518
	Hexane Extractable Material, mg/g	147	140	171	149	113
	Total Coliforms, MPN/g	$5.8 \times 10^{7}$	1.9×10 <sup>9</sup>	1×10 <sup>9</sup>	$7.8 \times 10^{7}$	1.7 $\times 10^5$
	Fecal Coliforms, MPN/g	$1.9 \times 10^{7}$	$3.4 \times 10^9$	$2.2 \times 10^{7}$	$7.3 \times 10^6$	$3.6 \times 10^6$
	Fecal Streptococci, MPN/g	$1.1 \times 10^{5}$	1.9×10 <sup>9</sup>	$4 \times 10^7$	$3.9 \times 10^{7}$	$1.4 \times 10^{8}$

## 0.25-in. SCREEN SAMPLE

## 13 May 1970

Time					
Start	0500	0600	0700	0800	0900
Finish	0530	0630	0730	0830	0930
Flow, cfs					
Start	0.024	0.021		0.055	0.080
Finish	0.022	0.043	-	0.056	-
Total Solids, g	5.99	14.61	69.58	110.88	104.24
Total Volatile Solids, g	5.57	13.42	57.08	84.01	89.64
BOD, mg/g	1,047	707	521	569	272
COD, mg/g	2,315	1,608	1,237	10,800	786
Hexane Extractable Material, mg/g	13.8	129.7	82.2	100.6	133.5
Total Coliforms, MPN/g	$7.18 \times 10^{7}$	$7.52 \times 10^{8}$	$6.89 \times 10^{7}$	$1.99 \times 10^{14}$	$8.84 \times 10^{7}$
Fecal Coliforms, MPN/g	6.01x10 <sup>6</sup>	$2.46 \times 10^{6}$	6.51x10 <sup>6</sup>	$2.71 \times 10^{7}$	$3.82 \times 10^6$
Fecal Streptococci, MPN/g	$7.18 \times 10^4$	2.94x10 <sup>6</sup>	2.67x10 <sup>6</sup>	$4.57 \times 10^{11}$	5.56x10 <sup>5</sup>

APPENDIX G

CORRELATIONS BETWEEN COMBINED SEWAGE BULK CONSTITUENTS
10 Storms

			Equation		No.	Significance		
X	Y	Form <sup>a</sup>	Coefficient	Coefficient	Correlation	of Data	Equation	Correlation
			Α	В	Coefficient	- ;	Coefficient	Coefficient <sup>C</sup>
TS	TVS	3	0.261	1.11	0.934	50	Yes	Yes
TS	TSS	3	0.0708	1.24	0.808	50	Yes	No
TS	TVSS	3	0.0370	1. 31	0.839	50	Yes	No
TS	SS	3	$5.16 \times 10^{-4}$	1.50	0.651	45	Yes	No
TS	F	6	35.5	0.187	0.439	45	Yes	No
TS	BOD	1	-27.5	0.370	0.862	47	Yes	No
TS	COD	3	0.326	1.13	0.849	50	Yes	No
TS	HEM	2	3. 17	0.00425	0.609	50	Yes	No
TS	TC	1	4.89x10 <sup>5</sup>	1. $20 \times 10^4$	0.397	46	Yes	No
TS	FC	3	$3.59 \times 10^{2}$	0.0116	0.320	43	Yes	No
TS	FS	2	$9.71 \times 10^3$	0.00368	0.270	39	No	No
TVS	TSS	1	-17.9	0.813	0.889	50	Yes	No
TVS	TVSS	1	-23.0	0.715	0.898	50	Yes	Yes
TVS	SS	3	0.00710	1. 16	0.574	45	Yes	No
TVS	F	5	0.566	-0.00132	0.303	45	Yes	No
TVS	BOD	3	0.0775	1. 33	0.844	47	Yes	No

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	TVS	COD	3	2.01	0.915	0.815	50	Yes	No
	TVS	HEM	2	4. 16	0.00587	0.532	50	Yes	No
	TVS	TC	1	$7.99 \times 10^{5}$	$2.04 \times 10^4$	0.450	46	Yes	No
	TVS	FC	3	$2.81 \times 10^{3}$	0.901	0.313	43	Yes	No
	TVS	FS	2	$1.11 \times 10^4$	0.00617	0.262	39	No	No
	TSS	TVSS	1	-6.20	0.864	0.991	50	Yes	Yes
	TSS	SS	6	65,5	-0.209	0.788	45	Yes	No
	TSS	F	6	4.65	0.244	0.736	45	Yes	No
	TSS	BOD	3	0.506	1.05	0.811	47	Yes	No
	TSS	COD	3	10.1	0.636	0.734	50	Yes	No
<b>1</b>	TSS	HEM	3	1.09	0.523	0.549	50	Yes	No
39	TSS	TC	1	$1.24 \times 10^{6}$	2.47×10 <sup>4</sup>	0.511	46	Yes	No
	TSS	FC	4	9.90×10 <sup>5</sup>	$-1.25 \times 10^{7}$	0.293	43	No	No
	TSS	FS	4	$3.14 \times 10^4$	2, 25×10 <sup>6</sup>	0.316	39	Yes	No
	TVSS	SS	6	64.2	-0.783	0.802	45	Yes	No
	TVSS	F	6	4. 44	0.209	0.729	45	Yes	No
	TVSS	BOD	3	0.613	1.10	0.863	47	Yes	No
	TVSS	COD	3	10.6	0.680	0.796	50	Yes	No
	TVSS	HEM	3	1. 18	0.549	0.584	50	Yes	No
	TVSS	TC	1	1. $46 \times 10^{6}$	2.76x10 <sup>4</sup>	0.499	46	Yes	No
	TVSS	FC	3	$9.72 \times 10^{3}$	0.764	0.315	43	Yes	No
	TVSS	FS	4	$-4.57 \times 10^3$	2.48×10 <sup>6</sup>	0.358	39	Yes	No
	SS	$\mathbf{F}$	6	0.0528	0.302	0.694	45	Yes	No

			Equation					Significance		
	X	Y	Form <sup>a</sup>	Coefficient Coefficient		Correlation Coefficient	of Data	Equation Coefficient <sup>b</sup>	Correlation Coefficient <sup>C</sup>	
	SS	BOD	6	0.0130	0.0353	0.610	42	Yes	No	
	SS	COD	3	$1.11 \times 10^{2}$	0.275	0.476	45	Yes	No	
	SS	HEM	3	8.00	0.261	0.396	45	Yes	No	
	SS	TC	2	4.93x10 <sup>5</sup>	0.202	0.345	41	Yes	No	
	SS	FC	1	$3.06 \times 10^{5}$	$1.44 \times 10^{5}$	0.423	38	Yes	No	
140	SS	FS	4	$-2.06 \times 10^3$	$4.96 \times 10^4$	0.582	39	Yes	No	
	F	BOD	6	0.186	-0.0148	0.658	42	Yes	No	
	F	COD	6	0.0189	0.00408	0.518	45	Yes	No	
	F	HEM	1	6.10	1.78	0.478	45	Yes	No	
	F	TC	4	3.60×10 <sup>6</sup>	-1.83×10 <sup>6</sup>	0.170	41	No	No	
	F	FC	1	8, 26×10 <sup>5</sup>	$-2.71 \times 10^4$	0.088	38	No	No	
	F	FS	4	-1.51x10 <sup>5</sup>	6.50x10 <sup>5</sup>	0.574	39	Yes	No	
	BOD	COD	3	15.6	0.605	0.858	47	Yes	No	
	BOD	HEM	3	1.57	0.484	0.616	47	$\mathbf{Y}  \mathbf{e}  \mathbf{s}$	No	
	BOD	TC	1	1.47×10 <sup>6</sup>	$2.53 \times 10^4$	0.370	43	Y e s	No	
	BOD	FC	3	$7.05 \times 10^3$	0.901	0.452	41	Yes	No	
	BOD	FS	4	$-6.77 \times 10^4$	2.86×10 <sup>6</sup>	0.681	36	Yes	No	
	COD	HEM	3	0.341	0.665	0.605	50	Yes	No	

COD	TC	1	1.77×10 <sup>6</sup>	$7.54 \times 10^3$	0.247	46	No	No
COD	FC	3	$1.21 \times 10^3$	1.00	0.362	43	Yes	No
COD	FS	2	1. $35 \times 10^4$	0.00267	0.191	39	No	No
HEM	TC	4	$3.93 \times 10^6$	$-5.06 \times 10^6$	0.221	46	No	No
HEM	FC	3	$6.03 \times 10^4$	0.433	0.179	43	No	No
HEM	FS	4	$-4.77 \times 10^4$	1.11x10 <sup>6</sup>	0.356	39	Yes	No
TC	FC	3	$3.72 \times 10^{2}$	0.438	0.376	40	Yes	No
TC	FS	3	$1.52 \times 10^{2}$	0.349	0.367	35	Yes	No
FC	FS	1	$3.28 \times 10^4$	0.0414	0.426	32	Yes	No

<sup>&</sup>lt;sup>a</sup>1. Y=A+B; 2. Y=A exp (BX); 3. Y=AX<sup>B</sup>; 4. Y=A+(B/X); 5. Y=1/(A+BX); 6. Y=X/(A+BX)

<sup>&</sup>lt;sup>b</sup>F-statistic significant at the 95-% confidence level

 $<sup>^{\</sup>rm c}$   $\chi^2$ -statistic significant at the 95-% confidence level

APPENDIX H CORRELATIONS BETWEEN COMBINED SEWAGE PARTICLE SIZE AND BULK CONSTITUENTS 10 Storms

				Equ	No.	Significance			
x		Y	Form <sup>a</sup>	Coefficient A	Coefficient B	Correlation Coefficient	of Data	Equation Coefficient	Correlation Coefficient <sup>C</sup>
	SS/TSS	PS	3	0.824	0.597	0.479	34	Yes	No
142	F/TSS	PS	3	0.0175	-0.661	0 <b>.4</b> 98	34	Yes	No
,,	BOD/TVS	PS	3	0.147	0.386	0.234	33	No	No
	COD/TVS	PS	5	9.57	4.90	0.356	34	Yes	No
	HEM/TVS	PS	6	20.6	-0.157	0.125	34	No	No
	TC/TVS	PS	6	11.9	$2.13 \times 10^4$	0.611	31	Yes	No
	FC/TVS	PS	6	7.49	$1.83 \times 10^4$	0.543	28	Yes	No
	FS/TVS	PS	5	18.1	$3.43 \times 10^{-4}$	0.193	30	No	No

<sup>&</sup>lt;sup>a</sup>1. Y=A+B; 2. Y=A exp (BX); 3. Y=A $^{B}$ ; 4. Y=A+(B/X); 5. Y=1/(A+BX); 6. Y=X/(A+BX)

<sup>&</sup>lt;sup>b</sup>F-statistic significant at the 95-% confidence level

 $<sup>^{\</sup>rm c}$   $\chi$   $^{\rm 2}$ -statistic significant at the 95-% confidence level

APPENDIX I

CORRELATIONS BETWEEN COMBINED SEWAGE SCREENINGS CONSTITUENTS
10 Storms

			Equation			No.	Signific	ance
х	Y	$\mathtt{Form}^\mathtt{a}$	Coefficient	Coefficient	Correlation	of Data	Equation	Correlation
			Α	В	Coefficient	Data	Coefficient	Coefficient C
TS	TVS	1	0.526	0.856	0.998	50	Yes	Yes
TS	BOD	4	$2.49 \times 10^{2}$	$3.53 \times 10^3$	0.370	49	Yes	No
TS	COD	1	$2.35 \times 10^3$	-19.2	0.170	50	No	No
TS	HEM	5	0.230	-0.00421	0.127	49	No	No
TS	TC	3	1.95×10 <sup>9</sup>	-0.600	0.160	49	No	No
TS	FC	4	$-1.90 \times 10^{8}$	1.10x10 <sup>10</sup>	0.197	41	No	No
TS	FS	3	2.35x10 <sup>5</sup>	1. 29	0,283	42	No	No
TVS	S BOD	4	$2.32 \times 10^{2}$	$3.36 \times 10^3$	0.391	49	Yes	No
TVS	S COD	1	$2.38 \times 10^3$	-23.6	0.179	50	No	No
TVS	S HEM	5	0.229	-0.00476	0.123	49	No	No
TVS	S TC	3	2.05×10 <sup>9</sup>	-0.644	0.171	49	No	No
TVS	s FC	4	$-2.54 \times 10^8$	$1.06 \times 10^{10}$	0.215	41	No	No
TVS	s FS	3	2.84x10 <sup>5</sup>	1.28	0.279	42	No	No
вој	D COD	6	0.120	0.00160	0.956	49	Yes	Yes
во	D HEM	6	2.90	0.00840	0.999	48	Yes	Yes

## APPENDIX I (Continued)

			Equati	ion		No.	Signific	cance
X	Y	Form <sup>a</sup>	Coefficient	Coefficient	Correlation	of	Equation	Correlation
			Α	В	Coefficient	Data	Coefficient	Coefficient <sup>C</sup>
BOD	TC	6	$8.32 \times 10^{-7}$	$6.41 \times 10^{-9}$	0.749	48	Yes	No
BOD	FC	6	$8.24 \times 10^{-6}$	$1.13 \times 10^{-9}$	0.884	40	Yes	No
BOD	FS	2	$3.59 \times 10^6$	0.00181	0.230	41	No	No
COD	HEM	6	22.1	-0.0166	0.960	49	Yes	Yes
COD	TC	3	7.55×10 <sup>5</sup>	0.887	0.659	49	Yes	No
COD	FC	6	$5.52 \times 10^{-5}$	$-1.26 \times 10^{-8}$	0.744	41	Yes	No
COD	FS	3	$3.08 \times 10^{3}$	1.09	0.359	42	Yes	No
HEM	TC	6	$2.90 \times 10^{-7}$	$3.70 \times 10^{-9}$	0.757	48	Yes	No
HEM	FC	6	$2.82 \times 10^{-6}$	$-1.56 \times 10^{-8}$	0.878	40	Yes	No
HEM	FS	2	$7.24 \times 10^{5}$	0.0250	0.507	41	Yes	No
TC	FC	6	7. 29	$6.48 \times 10^{-8}$	0.870	41	Yes	No
TC	FS	2	7.68x10 <sup>6</sup>	$1.08 \times 10^{-10}$	0.199	41	No	No
FC	FS	3	6.56×10 <sup>2</sup>	0.549	0.394	34	Yes	No

 $a_{1. Y=A+B; 2. Y=A \exp (BX); 3. Y=AX^B; 4. Y=A+(B/X); 5. Y=1/(A+BX); 6. Y=X/(A+BX)}$ 

<sup>&</sup>lt;sup>b</sup>F-statistic significant at the 95-% confidence level

 $<sup>^{\</sup>rm c}$   $\chi^2$ -statistic significant at the 95-% confidence level

BIBLIOGRAPHIC: Envirogenics Company, In-Sewer Fixed Screening of Combined Sewer Overflows, FWQA Publication No. 11024FKJ10/70

with laboratory studies, was conducted to characterize combined sewage contributary to combined sewer overflows, to ascertain the removal of floatables and solid materials that could be effected by the placement of screening devices in combined sewer systems, and to assess the effect of solids removal on chlorination requirements and bacterial concentrations. Statistics are presented on combined sewage bulk and screenings collected with 0,125-, 0,25-, 0,5-, and 1,0-in, aperture screens for the following constituents (where meaningfull: total solids, total volatile solids, total suspended solids, particle size distribution, biochemical oxygen demand, chemical oxygen demand, hexane extractable material, total coliforms, fecal coliforms, and fecal streptococci, Regression analyses were performed between all observed combined sewage bulk and screenings constituent pairs. Statistically significant correlations at the 95-% confidence level were obtained for the combined sewage bulk only between total solids and total volatile suspended solids, between total suspended solids and total volatile suspended solids. For combined sewage screenings, statistically significant correlations at the 95-% confidence level were found between total solids and total volatile suspended solids. For combined sewage screenings, statistically significant correlations at the 95-% confidence level were found between total solids and total volatile solids, biochemical oxygen demand, chemical oxygen demand, hexane extractable material, Removals of total solids, total volatile solids, biochemical oxygen demand, chemical oxygen demand, hexane extractable material, total coliforms, fecal coliforms, and fecal streptococci resulting from placement of the screening devices into the combined sewer were calculated and were marginal.

KEY WORDS

Combined sewage

Combined sewer overflows

Combined sewage treat-

Combined sewage characteristics

Fixed screens

Solids removal

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Fixed screening of combined sewage with aperture sizes ranging from 0,0164 to 1,0 in, appear to have little, if any, effect on total coliform and fecal coliform densities or bacterial kills by chlorination, Chlorination requirements for combined sewage subjected to fixed screening at different practical aperture sizes were reduced only slightly. This report was submitted in fulfillment of Contract No. 14-12-180 and Program No. 11024 FKJ between the Federal Water Quality Administration and the Aerojet-General Corporation,

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5	Organization			
	Envirogenics C	ompany, E	l Monte	, California
6	Title			
	In-Sewer Fixed S	creening of	Combi	ned Sewer Overflows
10	Author(s)		1 1 ( ) 1	ject Designation
F	euerstein, D. L.		21 Not	WQA Program 11024 FKJ Contract 14-12-180
22	Citation			
23	Waste water treats sewage, combined characteristics, fi	sewer ove	rflows,	astewater, storm runoff, sewers, combined combined sewage treatment, combined sewage is removal.
25	Identifiers (Starred First)			

Abstract A field sampling and analysis program, supplemented with laboratory studies, was conducted to characterize combined sewage contributary to combined sewer overflows, ascertain the removal of floatables and solid materials that could be effected by the placement of screening devices in combined sewer systems, and assess the effect of solids removal on chlorination requirements and bacterial concentrations. Statistics are presented on combined sewage bulk and screenings collected with 0, 125-, 0.25-, 0.5-, and 1.0-in. aperture screens. Statistically significant correlations at the 95-% confidence level were obtained for the combined sewage bulk only between total solids and total volatile solids, between total volatile solids and total volatile suspended solids, and between total suspended solids and total volatile suspended solids. For combined sewage screenings, statistically significant correlations at the 95-% confidence level were found between total solids and total volatile solids, between BOD and COD, between BOD and hexane extractable material, and between COD and hexane extractable material. Removals of total solids, total volatile solids, biochemical oxygen demand, chemical oxygen demand, hexane extractable material, total coliforms, fecal coliforms, and fecal streptococci resulting from placement of the screening devices into the combined sewer were marginal. Fixed screening of combined sewage with aperture sizes ranging from 0.0164 to 1.0 in. appear to have little, if any, effect on total coliform and fecal coliform densities or bacterial kills by chlorination with chlorination requirements being reduced only slightly.

Abstractor
D. L. Feuerstein

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