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DEVELOPMENT OF MODELING TECHNIQUE FOR PHOTOCHEMICAL AIR POLLUTION

by

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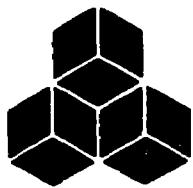
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SYSTEMS, SCIENCE AND SOFTWARE

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PART I
THEORY AND TECHNICAL RESULTS

1. INTRODUCTION

During the past years, the Environmental Protection Agency (EPA) and predecessor organizations have funded the development of photochemical simulation models which are to be used in the evaluation of present photochemical air pollution problems, the prediction of potential control strategies and the impact of new industrial plant siting on an urban region.

Two general methods of approach have evolved for photochemical simulation. The first model, typified by the models developed by Eschenroeder, et.al. (1971) and System Development Corporation (1970) is a Lagrangian method where a parcel of air is followed and chemistry takes place inside the packet of air. The other approach that has been considered is an Eulerian approach where the three-dimensional space is divided into subvolumes or cells and during each time increment pollutants are allowed to move from cell to cell by wind advection and diffusion. Roth, et.al. (1971) have developed a model along these lines. Systems, Science and Software (1971) developed a composite model using the PICK method (Particle-In-Cell with K-theory diffusion) which has Lagrangian characteristics but does chemistry in fixed Eulerian cells.

The objective of the research effort described in this report was to extend the model developed by Systems, Science and Software (S³) so that the photochemical kinetics can be considered in a Lagrangian framework and comparisons between

results using Eulerian and Lagrangian chemistry can be made to determine in actual practice if significant differences between the methods occur. It can be shown that some inherent errors do exist in Eulerian chemistry; however, it is not clear how important quantitatively these errors will be when compared to the results of the Lagrangian chemistry in actual simulations.

1.1 ERRORS IN EULERIAN CHEMISTRY

This illustration of the basis for the inherent errors in Eulerian chemistry was originally presented in the S³ Final Report in partial fulfillment of EPA Contract 68-02-0006.

Consider a one-dimensional problem as illustrated in Figure 1.

CELL	1	2	3	4	5	6
	0.0	1.0	1.0	1.0	0.0	0.0

Figure 1. Initial distribution of primary pollutant A.

Initially, cells 2-4 each have only primary pollutant, A, with cell concentration equal to 1.0. The effects of advection for a wind blowing four-tenths of a cell in time step Δt are simulated first, resulting in the distribution shown in Figure 2. If a quadratic chemical mechanism ($A + A \rightarrow B$) is hypothesized to illustrate the non-linearities in chemical kinetics rate equations, the rate equations can be written as

CELL	1	2	3	4	5	6
	0.0	0.6	1.0	1.0	0.4	0.0

Figure 2. Distribution of primary pollutant A after advection.

$$\frac{d[A]}{dt} = -k[A]^2 \quad \frac{d[B]}{dt} = +k[A]^2 .$$

Furthermore, if k is small, then $k[A]^2 \Delta t \ll [A]$ and the effects of the chemical reaction on the concentration of A can be ignored in order to focus on the secondary pollutant production. With $[A]$ approximately constant during the reactions the equation for production of $[B]$ can be integrated

$$[B] = k[A]^2 \Delta t .$$

That is, the production of the secondary pollutant is proportional to the square of the concentration of the primary pollutant. If, as an Eulerian technique would require, the cell concentrations of A are used in this equation, the distribution of B would be as shown in Figure 3.

CELL	1	2	3	4	5	6
	0.0	0.36 $k\Delta t$	1.0 $k\Delta t$	1.0 $k\Delta t$	0.16 $k\Delta t$	0.0

Figure 3. Distribution of secondary pollutant, B, calculated from cell concentrations given in Figure 2.

On the other hand, the concentration of A inside the puff is 1.0 and outside 0.0. That is, in a Lagrangian frame the production of B would be as shown in Figure 4.

CELL	1	2	3	4	5	6
	0.0	0.6 $k\Delta t$	1.0 $k\Delta t$	1.0 $k\Delta t$	0.4 $k\Delta t$	0.0

Figure 4. Distribution of secondary pollutant, B, calculated from Lagrangian concentration.

This is the physically correct picture. The methodology used in chemical simulation with Eulerian cell concentrations introduced errors of 40% in cell 2 and 60% in cell 5 when compared to the correct Figure 4.

1.2 INITIAL EVALUATION OF ERRORS FOR OBSERVED CONCENTRATIONS

In this section, observed concentrations at the Downtown Los Angeles and Pasadena stations of the Los Angeles County Air Pollution Control District (APCD) are used to illustrate and evaluate the Eulerian concentration errors. At 7:00 a.m., on September 30, 1969, the following concentrations were observed:

	Downtown Los Angeles	Pasadena
NO	51 pphm	19 pphm
NO ₂	1 pphm	9 pphm
HC	9 ppm	5 ppm
O ₃	3 pphm	1 pphm

These sets of concentrations can be used as initial conditions for a chemical reaction simulation. In this illustration, the simulation uses the CHEM computer code as described in the previously referenced S³ Final Report. The results after 5 and 10 minutes are shown in the first column of Table I.

TABLE I

TIME	POLLUTANT	LOS ANGELES	PASADENA	MIXED CELL	
				LAGRANGIAN	EULERIAN
0	NO	51.0	19.0	19.0	19.0
	NO ₂	1.0	9.0	9.0	9.0
	HC	9.0	5.0	5.0	5.0
	O ₃	3.0	1.0	1.0	1.0
5	NO	46.0	16.0	28.0	27.0
	NO ₂	5.8	11.0	9.2	10.0
	HC	9.0	5.0	6.6	6.6
	O ₃	0.02	0.1	0.08	0.06
10	NO	43.0	14.0	37.0	37.0
	NO ₂	8.9	14.0	9.8	7.8
	HC	9.0	5.0	8.2	8.2
	O ₃	0.04	0.2	0.07	0.03

The Lagrangian and Eulerian results listed under "Mixed Cell" correspond to a position intermediate between Downtown Los Angeles and Pasadena. Initially, the air at this position corresponds to that over Pasadena. It has been assumed for this illustration that "Downtown"-type air replaces four-tenths of the "Pasadena" air over this position each five

minutes. Corresponding to Figure 1, the position being examined is similar to cells 2 or 5. The Lagrangian results are just the proper proportions of the two types of air. The Eulerian results show the effects of performing the chemical simulation with "mixed" cell concentrations - an error of approximately 10% in O₃ and 20% in NO₂ in only two cycles (10 minutes). After a few hours errors inherent in the Eulerian simulation may be compounded and the results may be meaningless or, on the other hand, the errors may tend to average out.

This illustration is, like the first illustration, a gross over-simplification. These inherent errors dominate only where large gradients are present. The objective of the present research is to examine the potential differences by completing comparison calculations of the Los Angeles basin using both the Eulerian and Lagrangian chemistry, and then evaluating the two techniques if significant differences occur.

2. DESCRIPTION OF THE LAGRANGIAN METHOD

2.1 THE DIFFUSION EQUATION

In this report a Lagrangian approach to the solution of the "K-theory" equation describing the advection and dispersion of pollutants in the atmosphere is presented. In a previous study, Systems, Science and Software (1971) describes the PICK method where each particle represents an amount of mass which is transported by winds and dispersion is accounted for by a "turbulent flux velocity." The PICK method has been applied to two- and three-dimensional air pollution problems with good results. Artificial dispersion usually found in Eulerian codes is greatly reduced and good definition of distributions can be maintained.

In the Lagrangian approach, it is necessary that the particles do not represent mass but represent concentration of pollutant so that chemistry can be accomplished within each particle as it moves along. The basic ideas of particle representation used by S³ (1971) are utilized in the development of the new computer simulation model.

The basic Eulerian equation which is to be solved is a set of coupled K-theory equations for each chemical specie as shown in Eq. (1).

$$\frac{\partial C_i}{\partial t} + u \frac{\partial C_i}{\partial x} + v \frac{\partial C_i}{\partial y} + w \frac{\partial C_i}{\partial z} = \frac{\partial}{\partial x} \left(K_x \frac{\partial C_i}{\partial x} \right) + \frac{\partial}{\partial y} \left(K_y \frac{\partial C_i}{\partial y} \right) \\ + \frac{\partial}{\partial z} \left(K_z \frac{\partial C_i}{\partial z} \right) + \frac{\partial C_i}{\partial t} \Big|_{\text{chem}} + S_i \quad (1)$$

where

$$C_i = \text{concentration of } i\text{th specie}$$

$$x, y, z = \text{Cartesian coordinates}$$

$$u, v, w = \text{wind velocities}$$

$$K_x, K_y, K_z = \text{diffusivities}$$

$$S_i = \text{source rate of } i\text{th specie}$$

$$\frac{\partial C_i}{\partial t} \Big|_{\text{chem}} = \text{rate of change of } i\text{th specie due to chemical reactions}$$

Equation (1) is not completely general, since the diffusivity should be considered as a tensor and the x, y, z axes are not necessarily principle axes as would be inferred from Eq. (1). However, the current knowledge of diffusivity variation in the atmosphere does not allow a more detailed description than implied by Eq. (1) so the developed model does not consider a more general formulation.

2.2 PARTICLE ADVECTION

In the Lagrangian PICK code each particle represents a specific concentration; that is, associated with each particle is a concentration of pollutant. Therefore, the concentration in an (Eulerian) cell can be determined by appropriately averaging over the total numbers of particles in the cell. The averaging method used is discussed in Section 2.3. If more than one pollutant is being considered, such as in photochemical

simulations, then concentrations of several pollutant species can be associated with the same particle. For example, a single particle could be associated with the concentrations of HC, NO, NO₂, HNO₂ and O₃. Chemical reactions would be carried out for each particle as it travels through the grid. Thus, the description of the change of pollutant concentrations due to the chemical reactions and advection will be described in a purely Lagrangian manner. However, for the purpose of (1) editing the results, (2) introducing pollutant sources into the problem, (3) calculating diffusion fluxes, and (4) inputting a wind field, an Eulerian grid system is still used. This grid system is identical to that used in NEXUS and the method of computing particle velocity by volume averaging is identical to that used for calculating particle velocity in NEXUS. Each cell has a velocity vector located at the cell center. The particles in the cells are then moved for each time step with a velocity obtained by linear interpolation according to the position of the particle between the centers of adjacent cells. This is illustrated for two dimensions in Figure 5. Using \vec{v}^p to denote the total particle velocity vector (u, v)

$$\vec{v}^p(x, y) = \left\{ (y - y_j) \left[\frac{\vec{v}_{i+1, j+1}(x - x_i) + \vec{v}_{i, j+1}(x_{i+1} - x)}{\Delta x} \right] + (y_{j+1} - y) \left[\frac{\vec{v}_{i+1, j}(x - x_i) + \vec{v}_{i, j}(x_{i+1} - x)}{\Delta x} \right] \right\} / \Delta y \quad (2)$$

The shaded rectangular area in Figure 5 is cell-sized and centered at the particle position. Rearranging the terms in Eq. (2) gives:

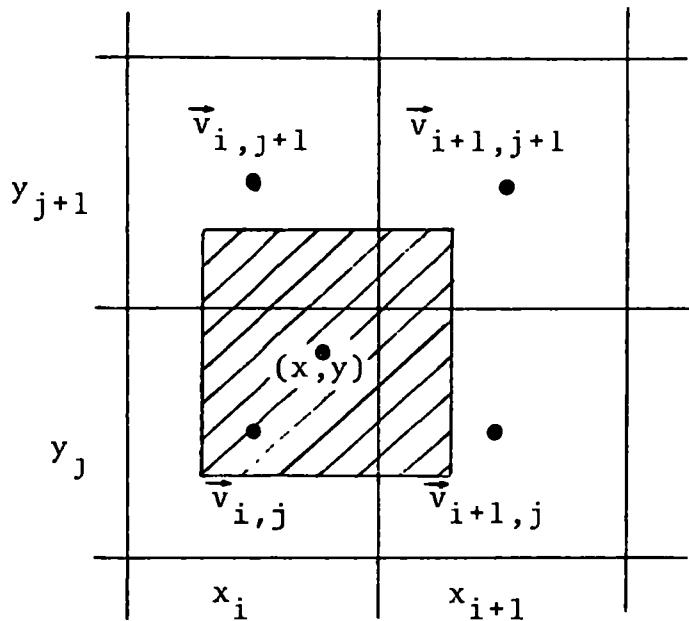


Figure 5. Area weighting interpolation for total velocity.

$$\begin{aligned}
 \vec{v}^p(x, y) = & \frac{1}{\Delta x \Delta y} (x - x_i) (y - y_j) \vec{v}_{i+1, j+1} \\
 & + (x_{i+1} - x) (y - y_j) \vec{v}_{i, j+1} \\
 & + (x - x_i) (y_{j+1} - y) \vec{v}_{i+1, j} \\
 & + (x_{i+1} - x) (y_{j+1} - y) \vec{v}_{i, j} .
 \end{aligned} \tag{3}$$

The product $(x - x_i) (y - y_j)$ multiplying $\vec{v}_{i+1, j+1}$ is the shaded area overlapping cell $(i+1, j+1)$ in Figure 5. Similarly, the other products give the areas of the overlap with the other cells. To simplify notation, the commas used to separate the subscripts will be suppressed for the remainder of this report.

In three dimensions, the analogous volume overlap is used. Therefore, in three dimensions, the velocity for a particle would be determined by the volume fraction in each of the surrounding cells. This would be computed as:

$$\vec{v}^p = \sum_{ijk} \vec{v}_{ijk} f_{ijk}^p$$

where

$$\begin{aligned}\vec{v}^p &= \text{particle velocity} \\ \vec{v}_{ijk} &= \text{velocity in cell } ijk \\ f_{ijk}^p &= \text{the fraction of the } p\text{th particle volume} \\ &\quad \text{in the } ijk \text{ cell}\end{aligned}$$

The sum is over the cells (ijk) where f_{ijk}^p is non-zero. This will normally be eight cells. (For example, four in a plane as shown in Figure 5 and four in the level above or below).

In the PICK method, the calculation to advance the particle configuration in time proceeds in steps or cycles, each of which calculates the desired quantities for time $t + \Delta t$ in terms of those at time t (an "explicit" time advancement procedure)

$$\begin{aligned}x(t + \Delta t) &= x(t) + u \Delta t \\ y(t + \Delta t) &= y(t) + v \Delta t .\end{aligned}\tag{4}$$

The velocities are the total velocities determined for the beginning of the time interval and interpolated to initial particle positions. These are held constant throughout any elementary time interval. It is evident that the magnitude

of the time interval Δt must be restricted, as otherwise a particle could pass through many cells in a cycle and well out of the region for which its velocity was interpolated. This could result in large inaccuracies and instabilities in the solution. Limiting the time step so that no particle moves more than four-tenths of a cell within any one cycle has been used as an empirical rule to avoid this problem.

2.3 EULERIAN CELL CONCENTRATION

The pollutant concentration in each cell is also computed by volume averaging of the particle concentrations. Since each particle carries concentration, it is necessary to have particles everywhere in the domain of interest. The method of computing the Eulerian cell concentrations is to associate with each particle a volume equal to a cell volume. It is not necessary to choose the particle volume to be equal to the cell volume; any choice would be valid. However, if the particle volume were equal to several cell volumes, the pollutant distributions would be necessarily spread out and "smeared." The other choice would be to choose a particle volume smaller than a cell volume. This would increase the number of particles necessary to carry out a calculation, since sufficient particles are required to cover all of the Eulerian grid. It would also increase the computational complexity. Since the fixed grid is governing all other aspects of the problem, such as velocity input and source input, it seems reasonable to assume a particle volume equal to a cell volume.

The Eulerian cell concentration is calculated by computing a volume average from Eq. (5):

$$c_{ijk} = \frac{\sum_{p=1}^{NP} c^p f_{ijk}^p}{\sum_{p=1}^{NP} f_{ijk}^p} \quad (5)$$

where

c_{ijk} = concentration in cell ijk

c^p = particle concentration

NP = total number of particles in the problem

f_{ijk}^p = the fraction of the pth particle volume
in the ijk cell

2.4 SOURCES

The method of attributing sources to a particle is almost the reverse procedure. All sources are treated as volume sources and are expressed in units of concentration per unit time (for example, ppm/min). As with any grid method, the smallest resolvable scale is one cell. Thus, treatment of sources as volume sources is not a serious deficiency. The method of computing the source rate for each particle is to take the fraction of the particle volume in the cell times the source rate of that cell to determine the particle source rate. This procedure is followed for all cells within which a portion of the particle volume lies, resulting in the expression:

$$s^p = \sum_i \sum_j \sum_k s_{ijk} f_{ijk}^p \quad (6)$$

where

s_{ijk} = source strength in ijk cell

f_{ijk}^p = fraction of p th particle volume in cell ijk

For inert pollutants, the change in concentration of a particle due to sources is simply computed by multiplying the particle source rate by the total time step of the computation cycle. For photochemical pollutants, the source is incorporated into the chemistry routine.

In this model, diffusion is also treated as a source or sink. After the concentration is obtained in each of the Eulerian cells, then the time rate of concentration change in each Eulerian cell is computed using the usual centered difference scheme. The resulting difference equation is:

$$D_{S_{ijk}} = \left[\frac{K_{i+\frac{1}{2}jk} \left(\frac{C_{i+1jk} - C_{ijk}}{\Delta x} \right) - K_{i-\frac{1}{2}jk} \left(\frac{C_{ijk} - C_{i-1jk}}{\Delta x} \right)}{\Delta x} \right] + \left[\frac{K_{ij+\frac{1}{2}k} \left(\frac{C_{ij+1k} - C_{ijk}}{\Delta y} \right) - K_{ij-\frac{1}{2}k} \left(\frac{C_{ijk} - C_{ij-1k}}{\Delta y} \right)}{\Delta y} \right] + \left[\frac{K_{ijk+\frac{1}{2}} \left(\frac{C_{ijk+1} - C_{ijk}}{\Delta z} \right) - K_{ijk-\frac{1}{2}} \left(\frac{C_{ijk} - C_{ijk-1}}{\Delta z} \right)}{\Delta z} \right] \quad (7)$$

where

$D_{S_{ijk}}$ = diffusion source in the ijk cell

C_{ijk} = concentration in the ijk cell

K_{ijk} = diffusivity at center of cell ijk (subscripts in Eq. (7) with $\pm \frac{1}{2}$ added to the integer subscripts indicate boundary values; see Figure 6)

$\Delta x, \Delta y, \Delta z$ = cell dimensions

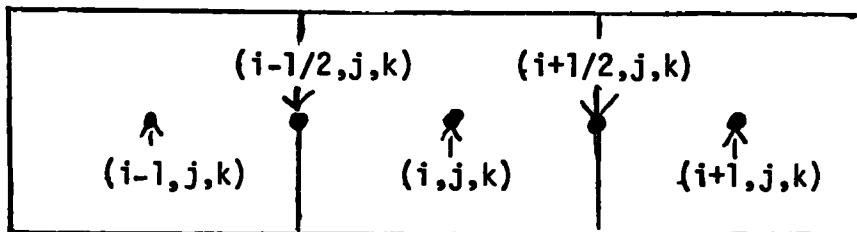


Figure 6. Location of centers of cells and interfaces in (i, j, k) notation.

The Lagrangian version of Eq. (1) is assumed to hold for each Lagrangian particle in the system, so that the equation solved for each particle is:

$$\frac{DC_i^P}{Dt} = \frac{\partial C_i}{\partial t} \Big|_{\text{chem}} + S_{\text{sources}}^P \quad (8)$$

where $\frac{D}{Dt}$ represents the time rate of change moving with a fluid particle (which is represented by the particles used in the numerical method). S_{sources}^P represents the particle source rates, including diffusion, which are computed from the cell source rates using Eq. (6). Thus, the change in concentration of a particle is due to chemistry, diffusion and sources.

2.5 CHEMICAL REACTIONS

As in the NEXUS/P code developed by S³ (1972), the chemistry module is such that it is very simple to implement another chemical reaction system. The basic input to the chemistry routine is: (1) the concentration of each pollutant species, and (2) the source rate of the pollutant due to sources and diffusion. The chemistry routine then solves the coupled non-linear equations:

$$\frac{\partial C_i}{\partial t} = F_i - R_i C_i + S_i$$

where

$F_i = f_i(C_j)$ - formation rate of C_i

$R_i C_i = r_i(C_j)C_i$ - removal rate of C_i

S_i = source rate of C_i

2.6 GENERAL CODE OPERATION

Figure 7 depicts the logical sequence used in each cycle of calculation. Because each particle contains the concentration of all species, the total number of particles required in the calculations are less than required in a NEXUS/P calculation. Consequently, some savings in the use of auxiliary storage is provided.

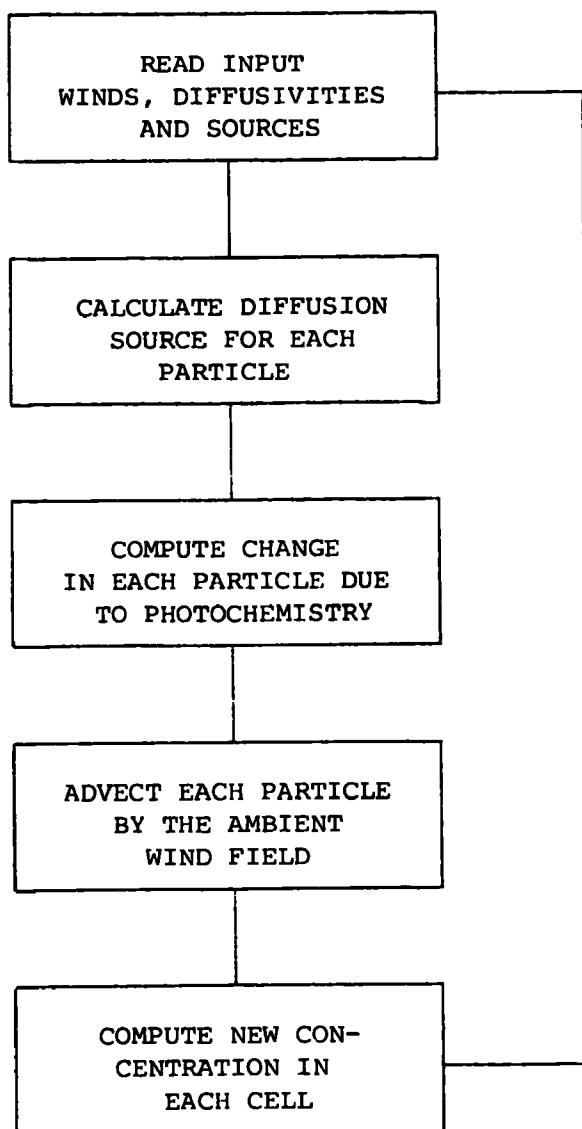


Figure 7. A typical cycle in the NEXUS/L code.

3. TESTING OF THE NEXUS/L CODE

Since each particle in the NEXUS/L code represents a concentration of pollutant, it is necessary to have sufficient particles distributed throughout the grid so that all space is occupied by at least one particle volume. Another difficulty with a Lagrangian code is the accuracy with which the distribution can be interpolated onto the Eulerian grid. If a sharply peaked distribution is being advected then the position of the gradients within a cell can cause the distribution to appear to be distorted. However, when the distribution returns to a position similar to the original, the Eulerian results will agree with the actual distribution.

In a previous report, S³ (1971), describing the PICK method, a test problem used to study the accuracy of the code was the advection of a Gaussian distribution. The same test problem was considered using the NEXUS/L code. The distribution was defined initially by

$$C(x,y,0) = 71.1 \{ \exp -[(x-9)^2 + (y-9)^2/12.5] \} .$$

The velocities were chosen as $\bar{v}_x = 10 \text{ m/sec}$ and $\bar{v}_y = 5 \text{ m/sec}$. Figure 8 shows the motion of the Gaussian distribution across the grid. There is no distortion of the distribution. The peak concentration in each cell remained at its initial concentration value. This particular test problem was run with 1, 2 and 4 particles in each cell. The results were independent

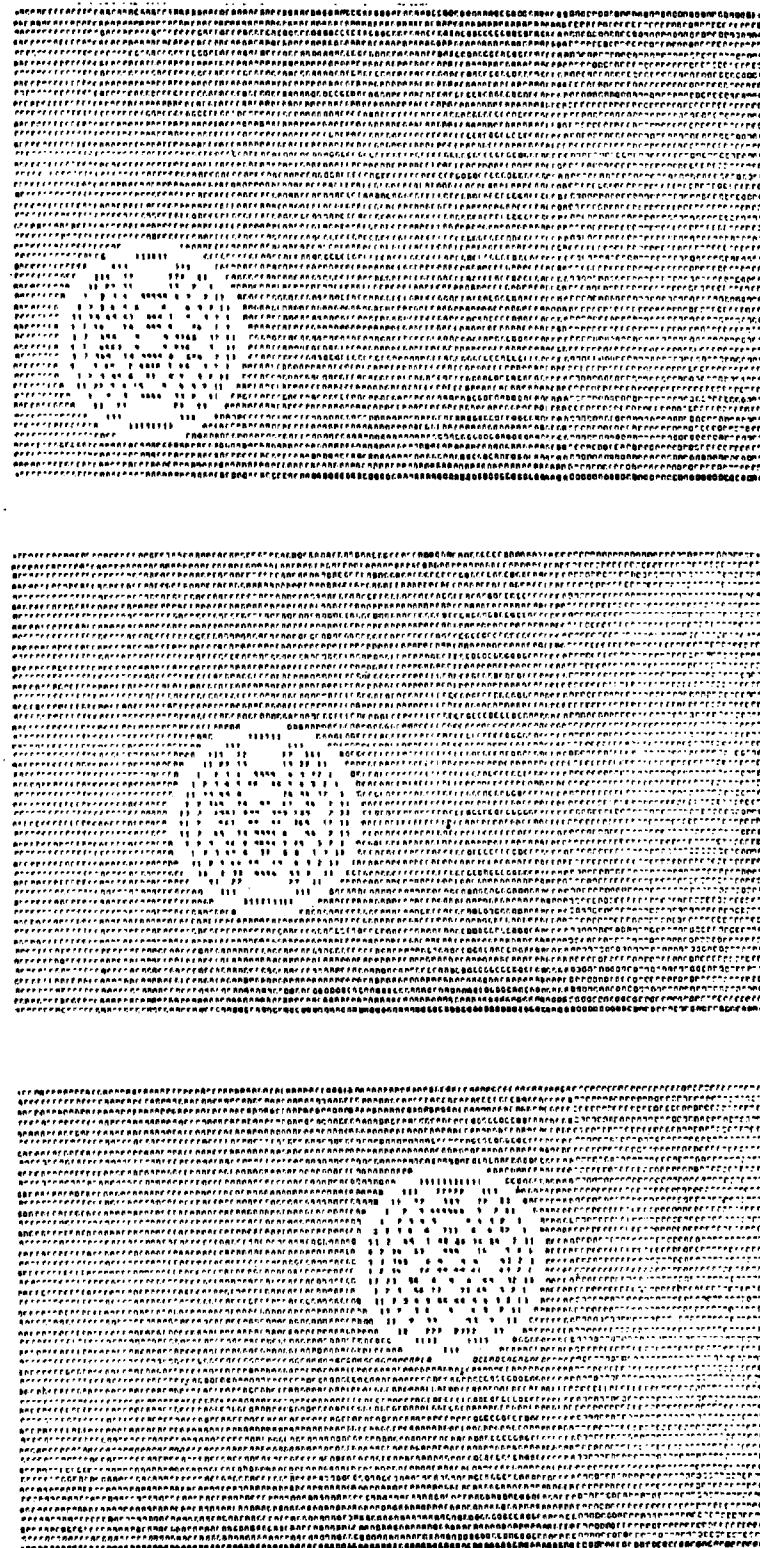


Figure 8. Advection of a Gaussian distribution $v_x = 10$ m/sec and $v_y = 5$ m/sec.

of the number of particles used. This test problem indicates that advection is properly treated using the modified particle method and the advantages attributed to the particle method applied in the modified approach.

4. PHOTOCHEMICAL MECHANISM AND SIMULATION

The photochemical mechanism used for the simulation results presented is a mechanism developed by Eschenroeder and Martinez (1972). Table II gives the mechanism and the rate coefficients used. This mechanism contains three branching factors, b_1, b_2, b_3 in Eqs. (3), (4) and (5), which account for the production of RO_2 , the generalized oxidant radical, and one yield factor, y , in Eq. (6), which affects the amount of OH radical produced.

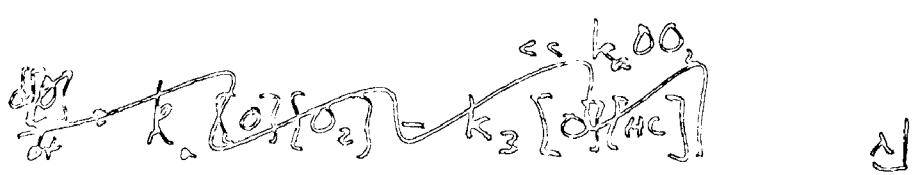
By carefully selecting these parameters, the resulting rate of change of pollutants can be made to agree with almost any desired result. The method of selecting these parameters was to examine the behavior of a "basin average" obtained by averaging the actual pollutant measurements from the APCD stations for the simulation day, September 30, 1969. An average source rate was determined for each pollutant and a series of chemical simulations was made varying the branching factors and yield factor to provide a reasonable fit to the average chemical behavior of the basin. The reason these "free" parameters exist is that the exact composition of the hydrocarbons present is not known and if it were, the chemistry required to include each hydrocarbon species would make the system too complex to be manageable. Thus, a "generalized lumped hydrocarbon" is used and consequently the "free" parameters appear and must be adjusted for any hydrocarbon mix. Eschenroeder and Martinez (1972) discuss this point at some length.

TABLE II
PHOTOCHEMICAL KINETICS SYSTEM

Reaction	Rate Constants
1. $(hv) + NO_2 \rightarrow NO + O$	0.267 min^{-1*}
1a. $O + (O_2) + M \rightarrow O_3 + (M)$	$2.64 \times 10^6 \text{ min}^{-1}$
2. $NO + O_3 \rightarrow NO_2 + (O_2)$	$26.7 \text{ ppm}^{-1} \text{ min}^{-1}$
3. $O + HC \rightarrow (b_1) RO_2$	$2.81 \times 10^{-5} \text{ ppm}^{-1} \text{ min}^{-1}$
4. $OH + HC \rightarrow (b_2) RO_2$	$1.5 \times 10^4 \text{ ppm}^{-1} \text{ min}^{-1}$
5. $O_3 + HC \rightarrow (b_3) RO_2$	$4.0 \times 10^{-3} \text{ ppm}^{-1} \text{ min}^{-1}$
6. $RO_2 + NO \rightarrow NO_2 + (y) OH$	$1.0 \times 10^5 \text{ ppm}^{-1} \text{ min}^{-1}$
7. $RO_2 + NO_2 \rightarrow PAN$	$2.0 \times 10^2 \text{ ppm}^{-1} \text{ min}^{-1}$
8. $OH + NO \rightarrow HONO$	$1.5 \times 10^3 \text{ ppm}^{-1} \text{ min}^{-1}$
9. $OH + NO \rightarrow HNO_3$	$3.0 \times 10^3 \text{ ppm}^{-1} \text{ min}^{-1}$
10. $(hv) + HONO \rightarrow OH + NO$	$1.0 \times 10^{-3} \text{ min}^{-1*}$
11. $NO + NO_2 \xrightarrow{H_2O} 2HONO$	$1.0 \times 10^{-3} \text{ min}^{-1}$
12. $NO_2 + O_3 \rightarrow NO_3 + O_2$	$5.0 \times 10^{-2} \text{ ppm}^{-1} \text{ min}^{-1}$
13. $NO_3 + NO_2 \rightarrow N_2O_5$	$4.5 \times 10^3 \text{ ppm}^{-1} \text{ min}^{-1}$
14. $N_2O_5 \rightarrow NO_3 + NO_2$	$1.4 \times 10^1 \text{ ppm}^{-1} \text{ min}^{-1}$
15. $N_2O_5 + (H_2O) \rightarrow 2HNO_3$	$6.05 \times 10^1 \text{ min}^{-1}$

where $b_1 = 10$, $b_2 = 10$, $b_3 = 0.1$, and $y = 0.1$.

*Corresponding to noon value of solar insolation.



$$\frac{d\text{O}_3}{dt} = k_1[\text{O}] [\text{O}_2][\text{M}] - k_2[\text{NO}_2]\text{O}_3 - k_3[\text{NO}][\text{O}_2] - k_4[\text{NO}_2]\text{O}_3$$
$$= k_1[\text{O}] [\text{O}_2][\text{M}] - k_2[\text{NO}_2]\text{O}_3 + k_3[\text{NO}][\text{O}_2]$$

Response to SD APC D. job offer

I would like to accept

if somehow I could start ^{on} after May 10

If not I must reluctantly refuse

- 1) do may over description changes but am willing to accept a mistake
- 2) must leave unfinished work here (Solar energy talk)
- 3) must forfeit over \$2000 (moving expenses)
- 4) must take possible price penalty on selling home

Would like to remain on the list for future appointments including the possibility on the individuals chosen terminating after a short time.

Photochemical smog in the Los Angeles basin on September 30, 1969, was simulated using NEXUS/P. This calculation was a repeat of the calculation reported by S³ (1971) with a revised chemical mechanism. The chemical mechanism used was the mechanism by Eschenroeder and Martinez, shown in Table II, with five calculated species (NO, NO₂, HC, O₃ and HNO₂) and three species in pseudo-equilibrium (O, RO₂ and OH). The source inventory used was reported by Roberts, et.al. (1971). The required meteorological wind data were obtained from Dickson and Start (1971) and Roth (1971) provided inversion height data. The 16-hour real time simulation required 1.5 hours on a UNIVAC 1108. Approximately one-half hour was spent in chemical simulation and one-half hour in data manipulation.

The NEXUS/L code was used to perform a comparison to the updated NEXUS/P calculation. The same winds, diffusivities and sources were used for this photochemical simulation. A comparison of the results provided by the two codes is shown in Figures 9 through 18. The available APCD data are also presented.

An examination of the basin averaged results, the average of results at all APCD stations, shown in Figure 9, yields some general conclusions regarding the differences exhibited between the two calculations. The NO₂ levels in the NEXUS/P calculations show a general trend of being larger than in the NEXUS/L calculation. The peak value is 15% higher. The NO₂ levels remain above the 10 pphm level throughout the afternoon in the NEXUS/P results, whereas the NO₂ disappears between 1:00 and 2:00 p.m. in the NEXUS/L results. The disparity between the NO₂ results from each calculation causes the oxidant levels, represented by O₃ in the chemical model, to also be different in the two calculations. The basin average results indicate peak values 30% higher for the NEXUS/L calculation and the peak values occur 1-1½ hours later in the day.

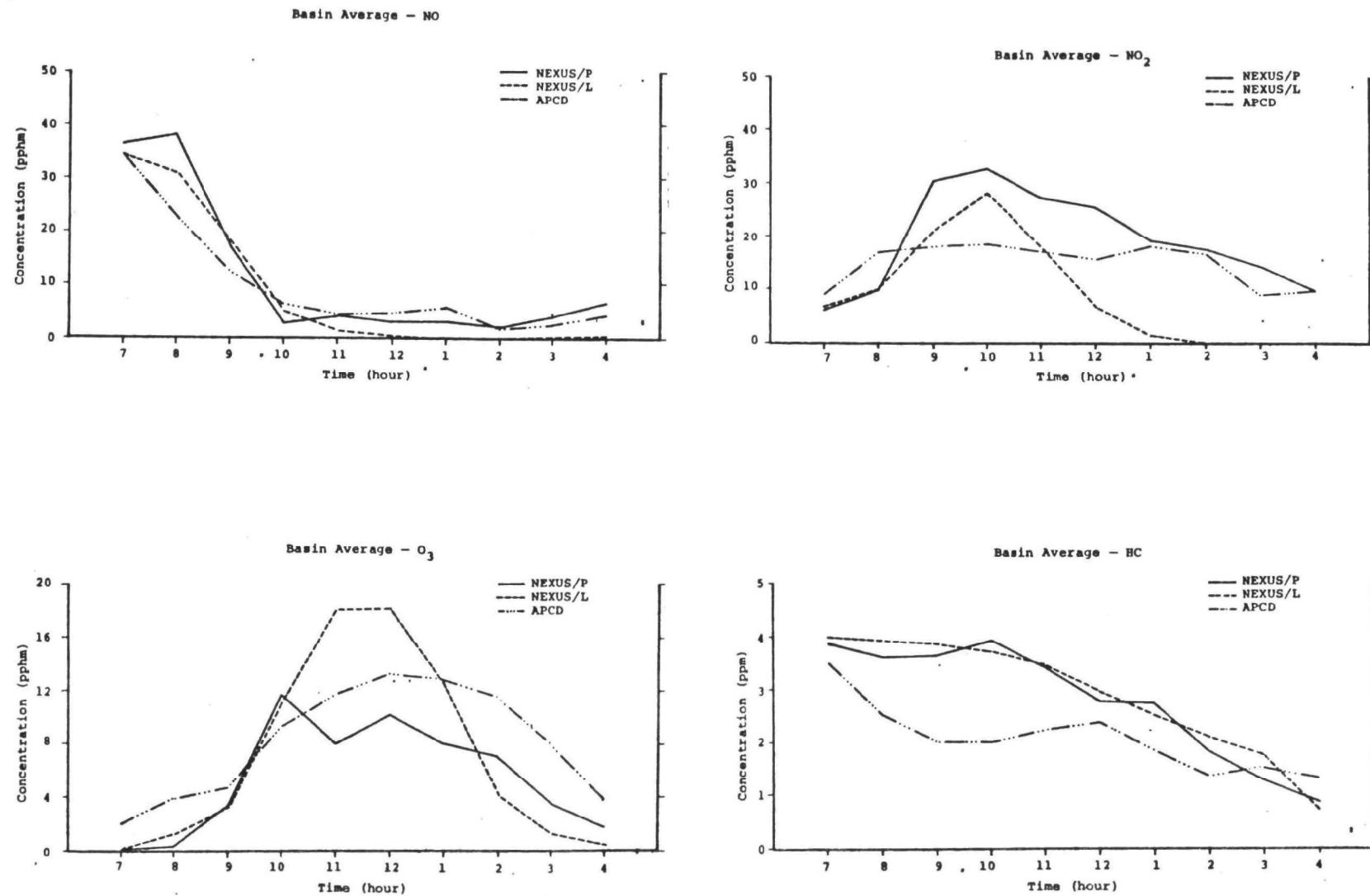


Figure 9. Basin average pollutant concentrations.

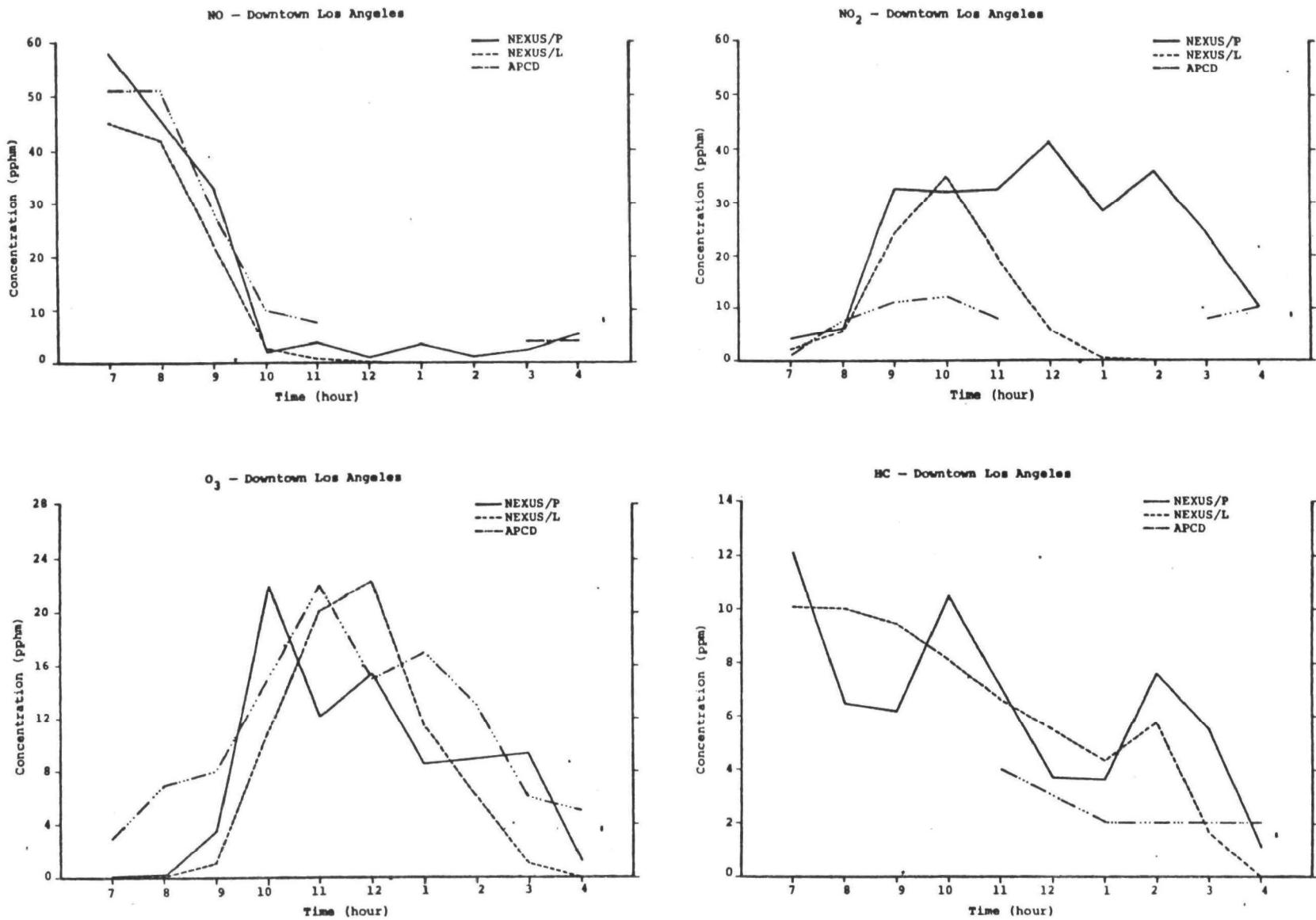


Figure 10. Downtown Los Angeles pollutant concentrations.

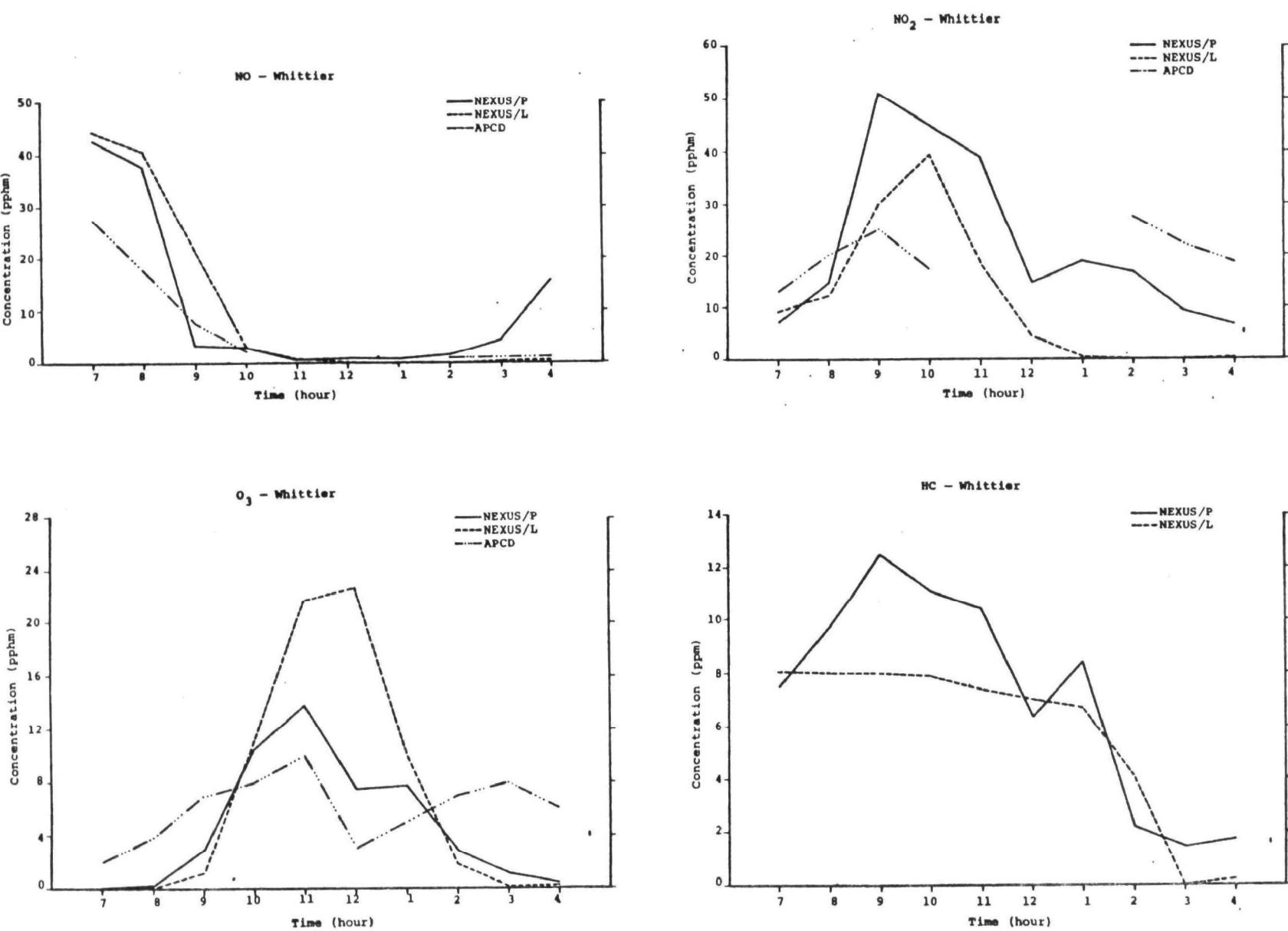


Figure 11. Whittier pollutant concentrations.

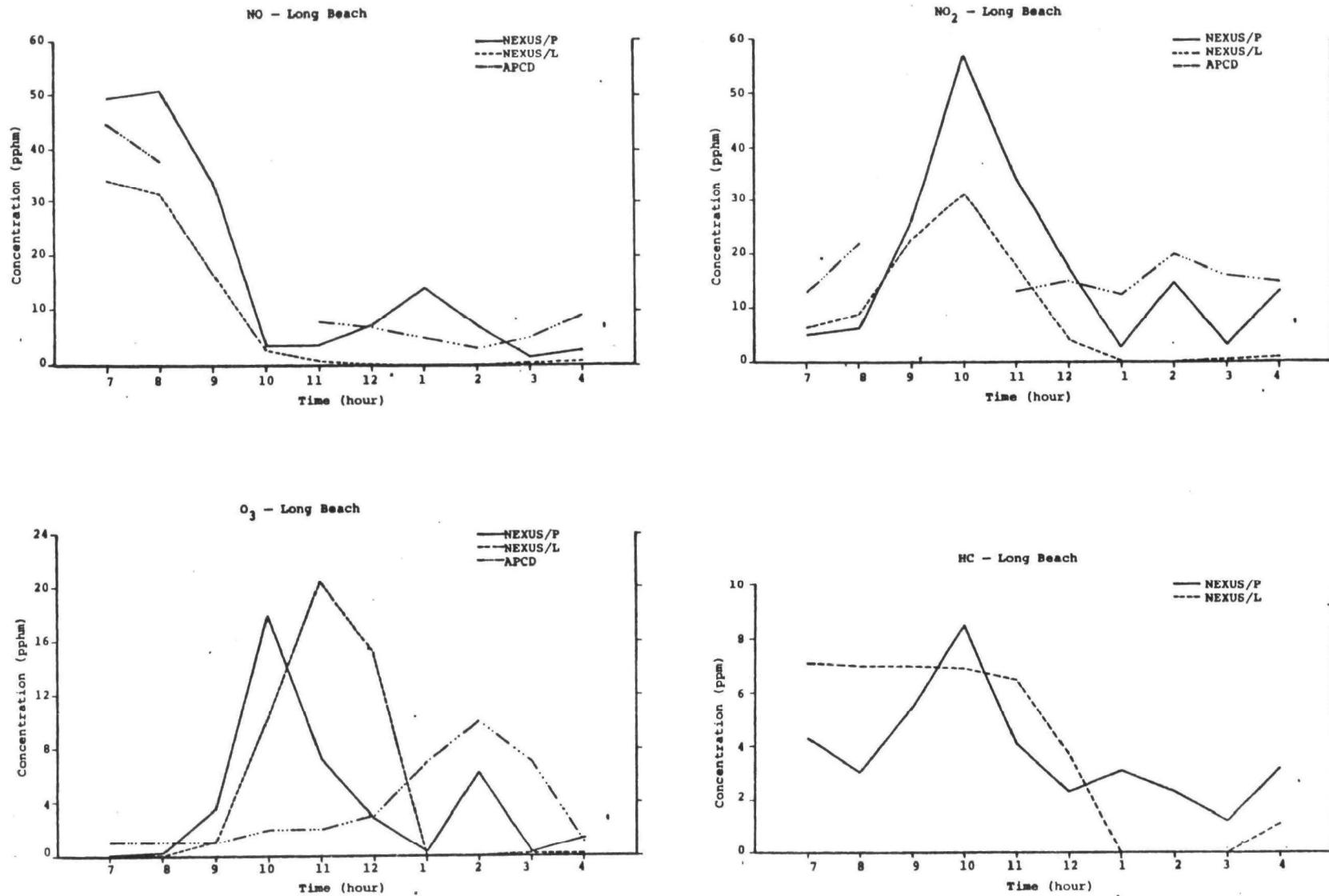


Figure 12. Long Beach pollutant concentrations.

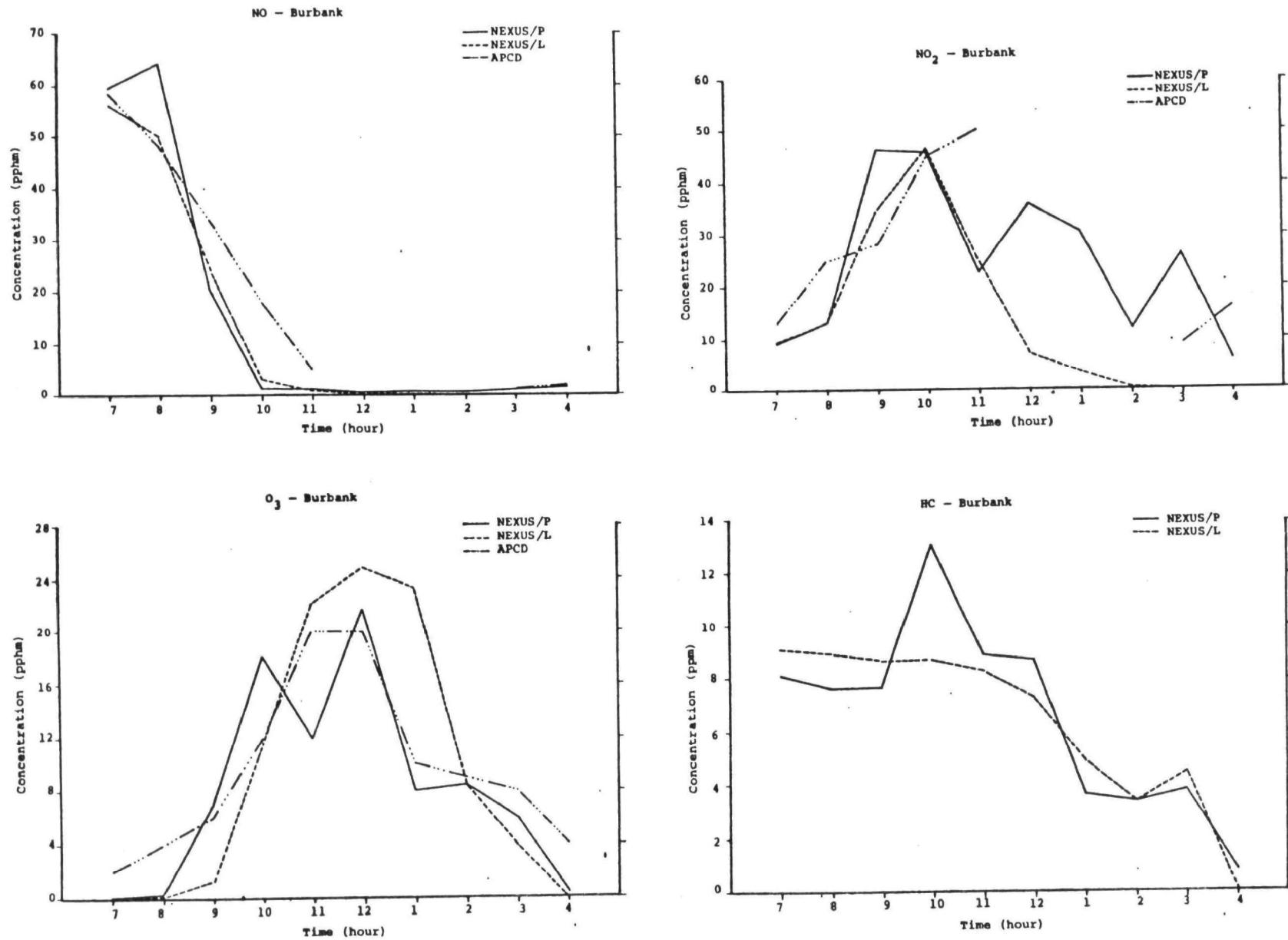


Figure 13. Burbank pollutant concentrations.

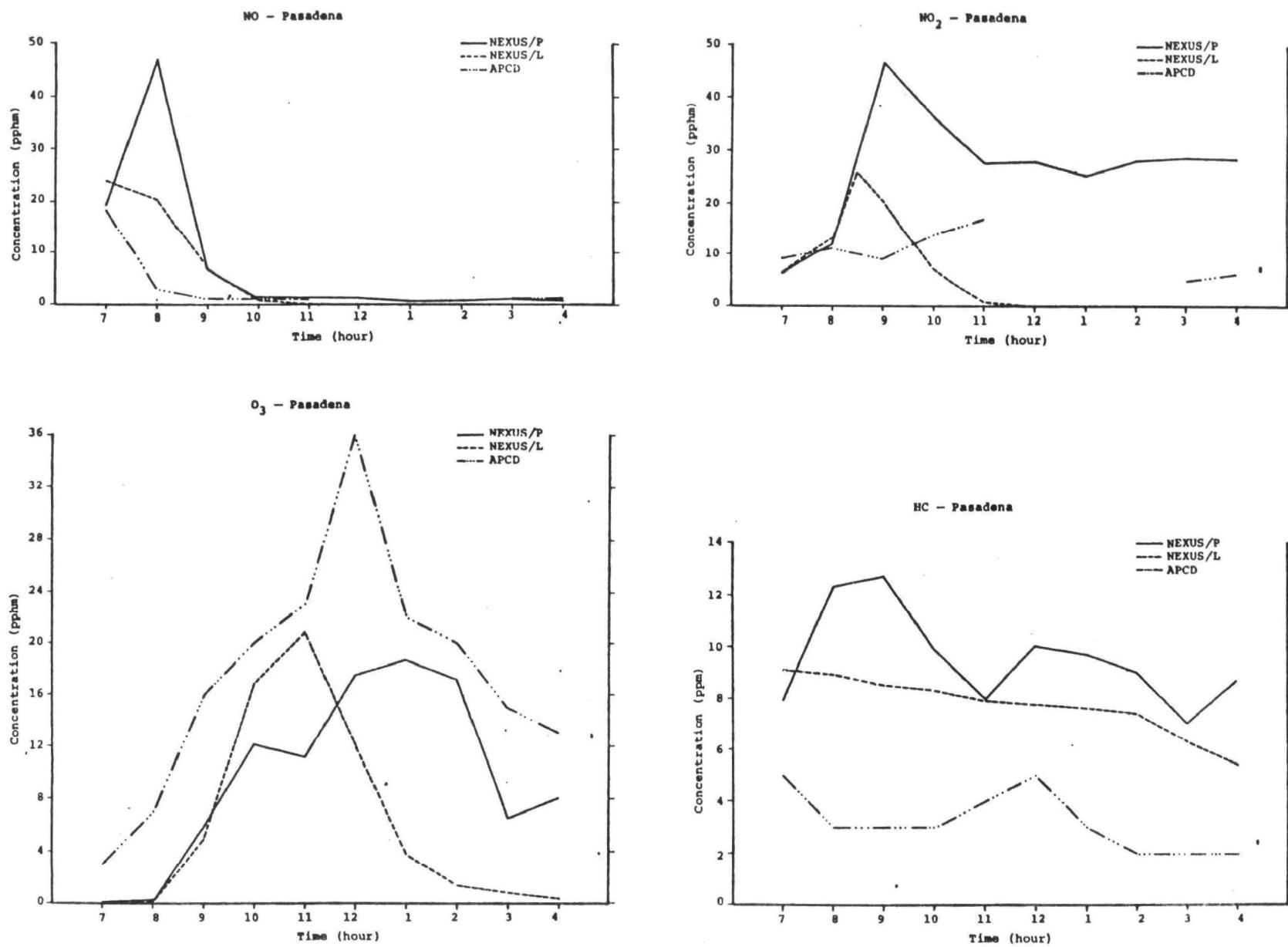


Figure 14. Pasadena pollutant concentrations.

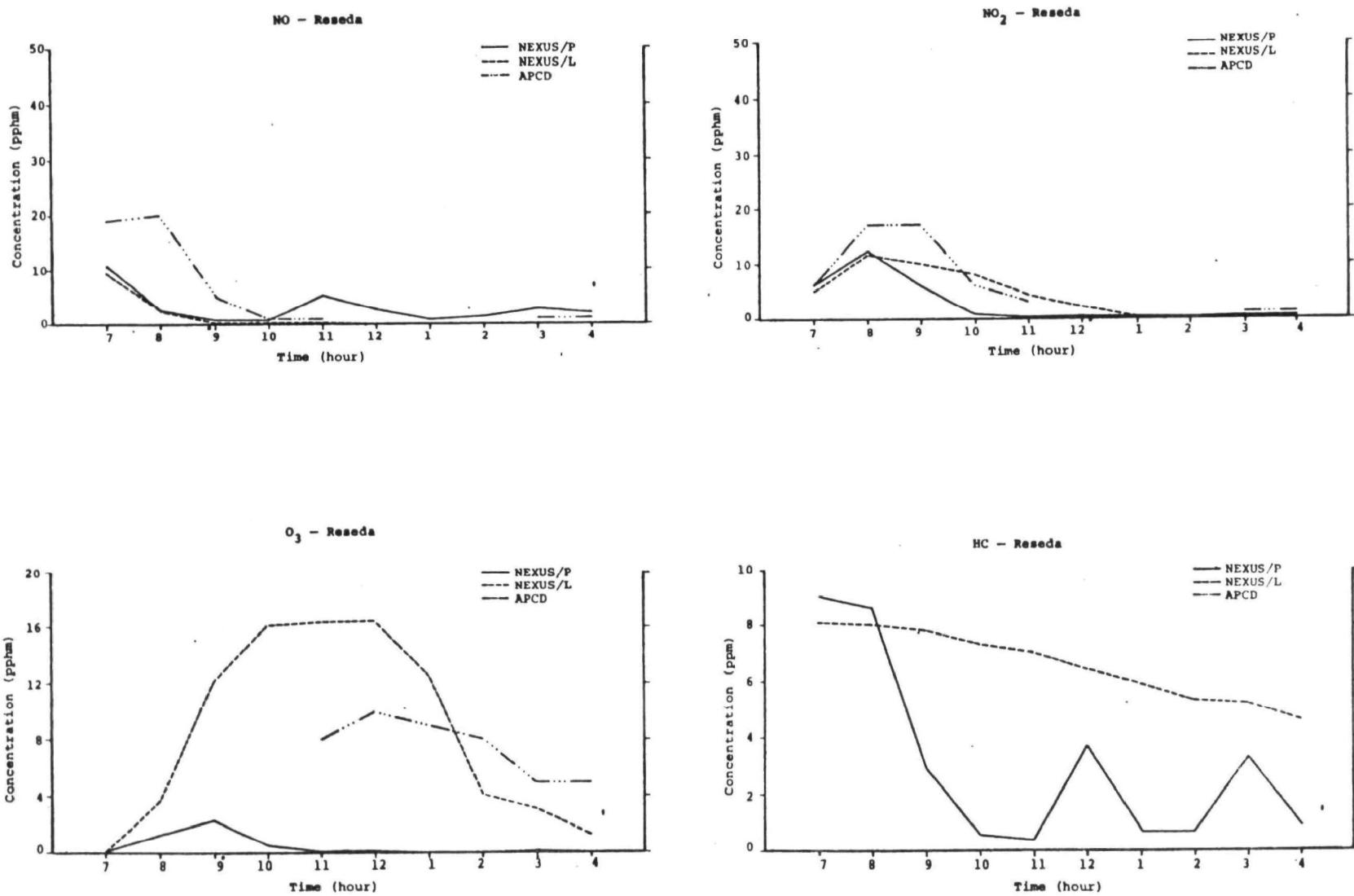


Figure 15. Reseda pollutant concentrations.

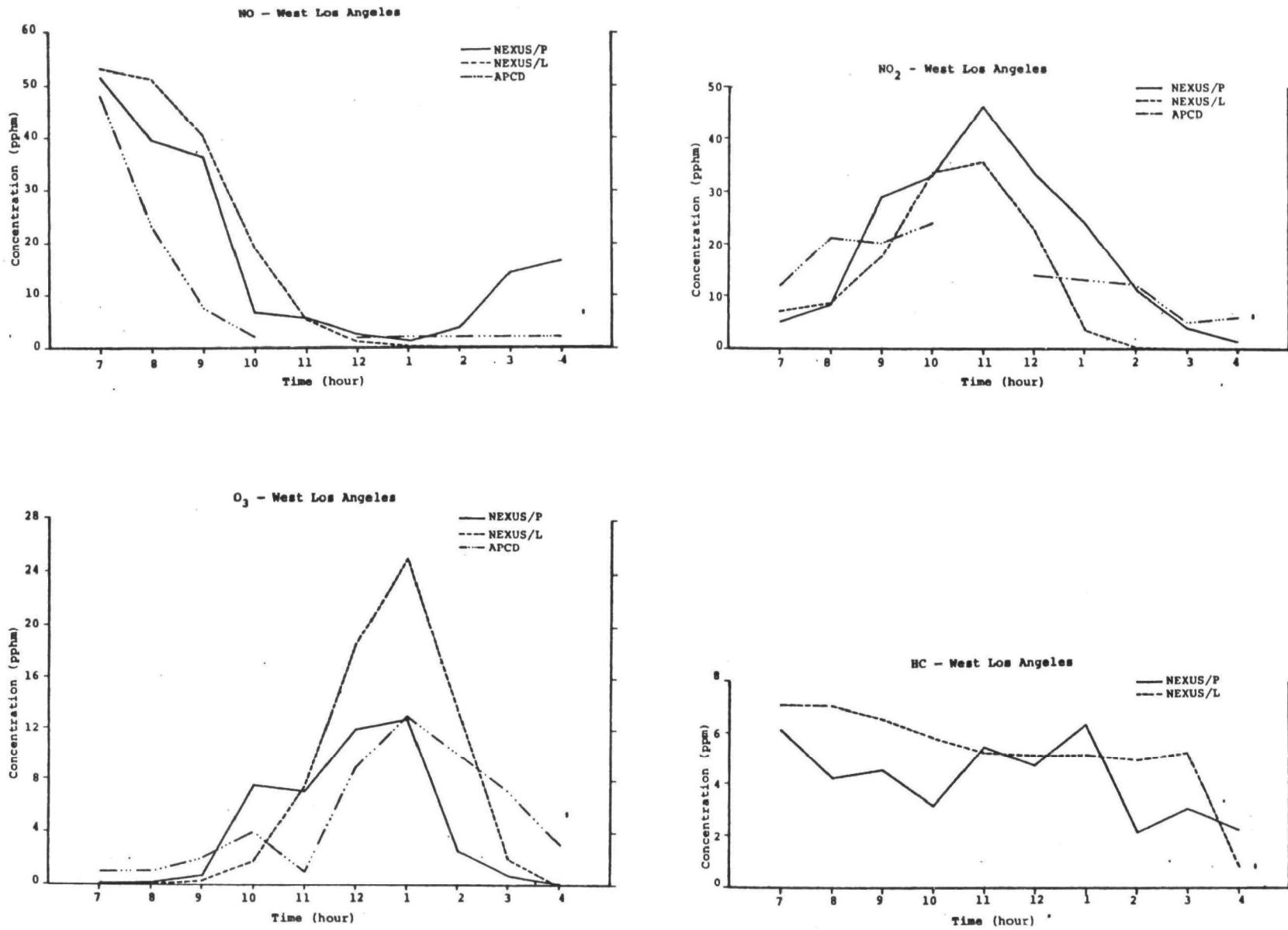


Figure 16. West Los Angeles pollutant concentrations.

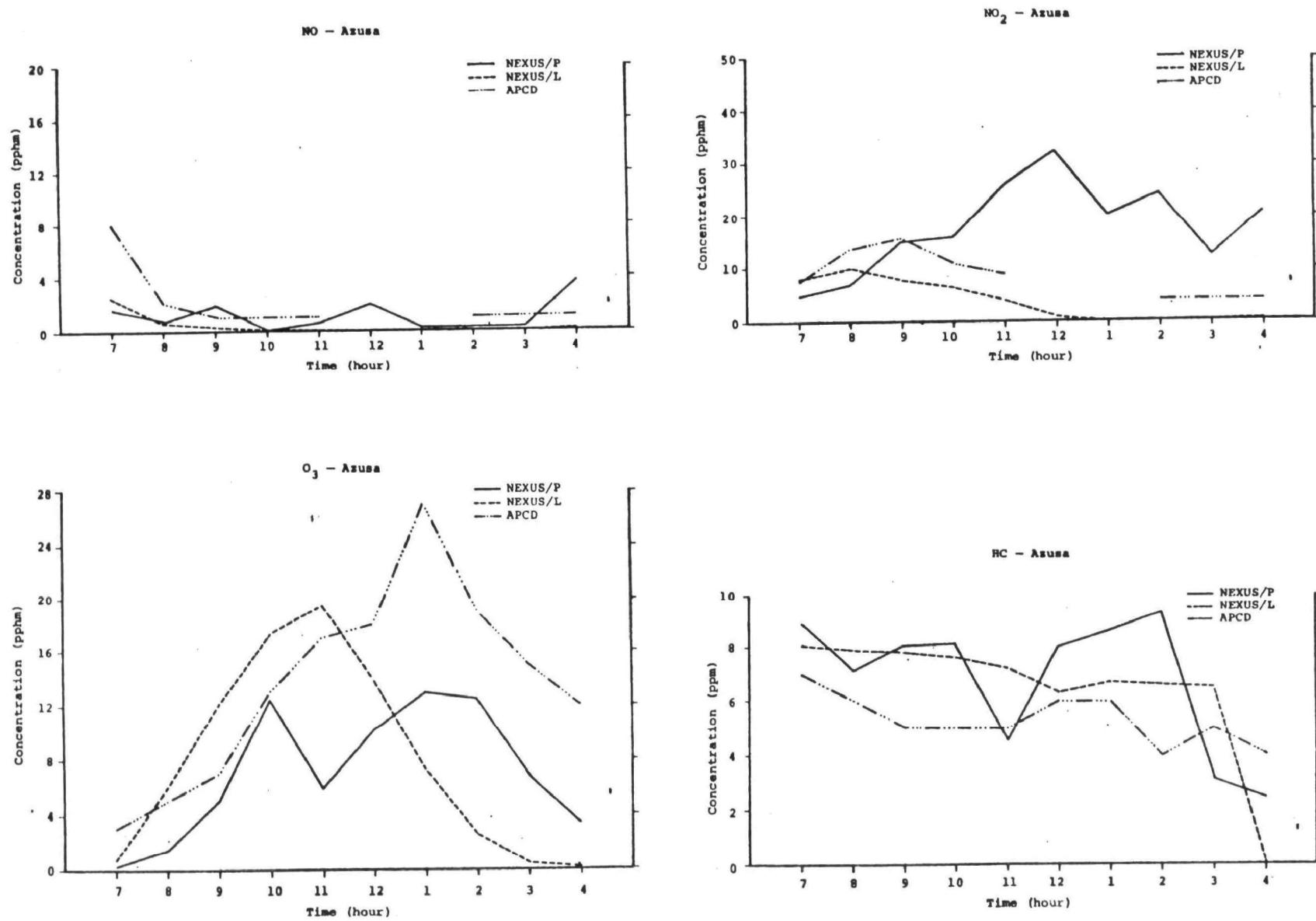


Figure 17. Azusa pollutant concentrations.

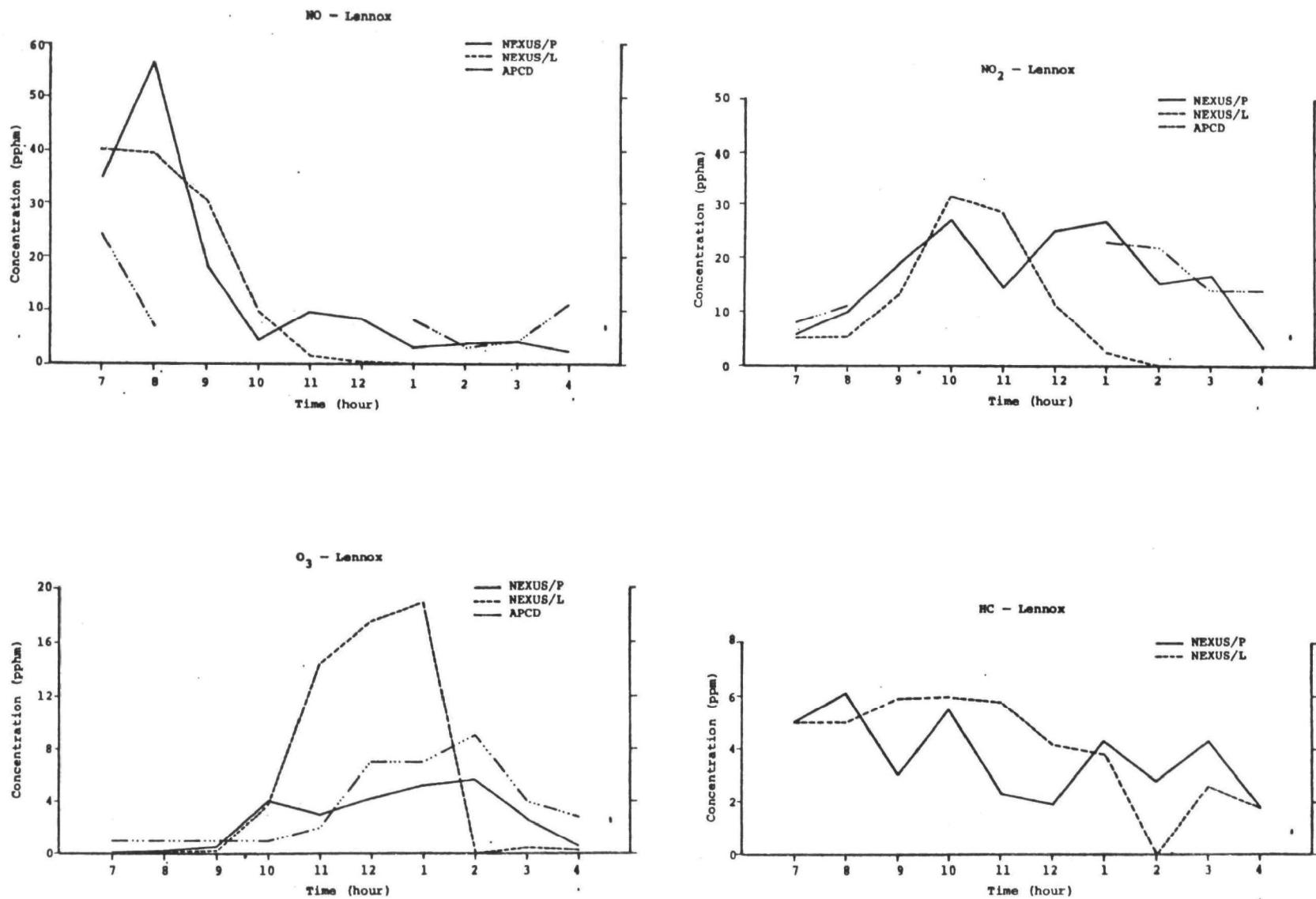


Figure 18. Lennox pollutant concentrations.

The general character of the NEXUS/L results is that they are much smoother than the NEXUS/P results. One reason for this is the averaging technique used to relate particle concentrations to cell concentrations for editing purposes. The general smoothing of the results is also indicated by examining the peak O₃ concentrations at each station. These results are shown in Table III. The NEXUS/L results over-predict at the stations near the coastline and underpredict in the high oxidant areas of Pasadena and Azusa.

TABLE III
PEAK OXIDANT CONCENTRATION

STATION	NEXUS/P	NEXUS/L	APCD
Pasadena	18	20	36
Long Beach	18	20	8
Lennox	4	18	8
West Los Angeles	12	26	12
Whittier	12	24	9
Azusa	12	20	28
Downtown	22	22	22
Burbank	21	24	20
Reseda	2	16	8

An examination of the comparison of the two different simulation results and the actual measurements indicate no trends which would allow one to choose one simulation as being superior to the other. From the results it is possible to determine that inherent errors in the Eulerian photochemistry are not so large that they cannot be overcome by adjusting the chemical reaction parameter. The examination of the chemical reaction system prior to the simulations to determine the rate

constants and branching factors has shown that the system is extremely sensitive to these parameters. The results of the calculations can be significantly affected by rather minor changes in these parameters. Therefore, the parameters themselves are the controlling factors in any simulation, not the simulation technique.

This draws one to the conclusion, that either Eulerian or Lagrangian chemistry is satisfactory given the current state-of-the-art in photochemical lump-parameter modeling.

A second photochemical simulation was run for Los Angeles for the same day using the NEXUS/L code. The purpose of this simulation was to test the sensitivity of the results to the input data. For the second simulation the sources were doubled so that twice as much total emissions were introduced into the problem. Some comparative results are shown in Figures 19 through 21. The calculated results do show a change in the general behavior of the pollutant concentrations. In particular, the NO₂ peak is much increased. However, the ozone peak is not increased particularly but is moved later in time. The same trend is noted at the Burbank and Downtown Los Angeles locations.

These results point out that a photochemical model such as NEXUS/L can be used for sensitivity calculations and will show differences because of changes in emissions.

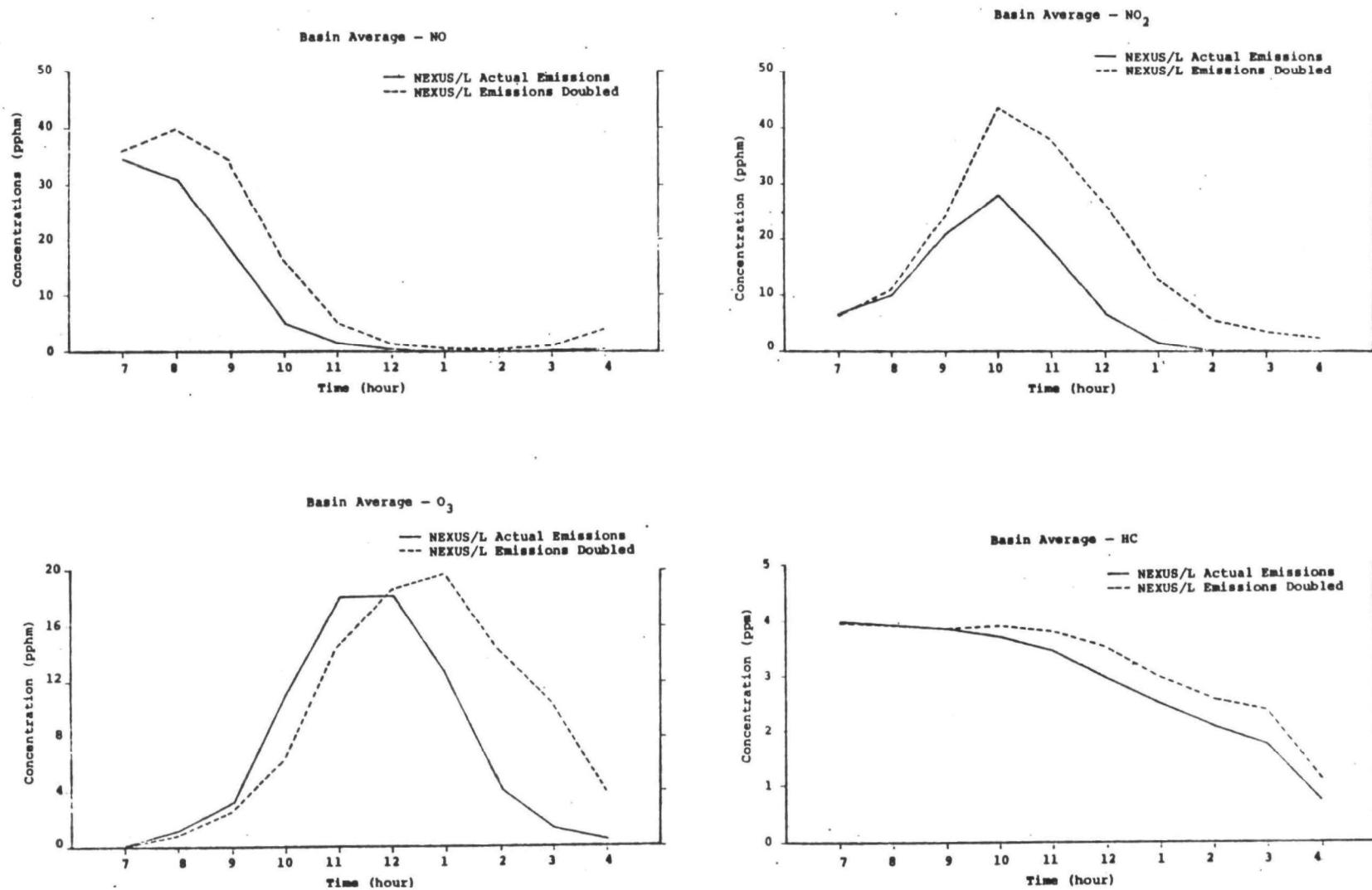


Figure 19. Comparison of basin-average NEXUS/L results using actual emissions and double emission.

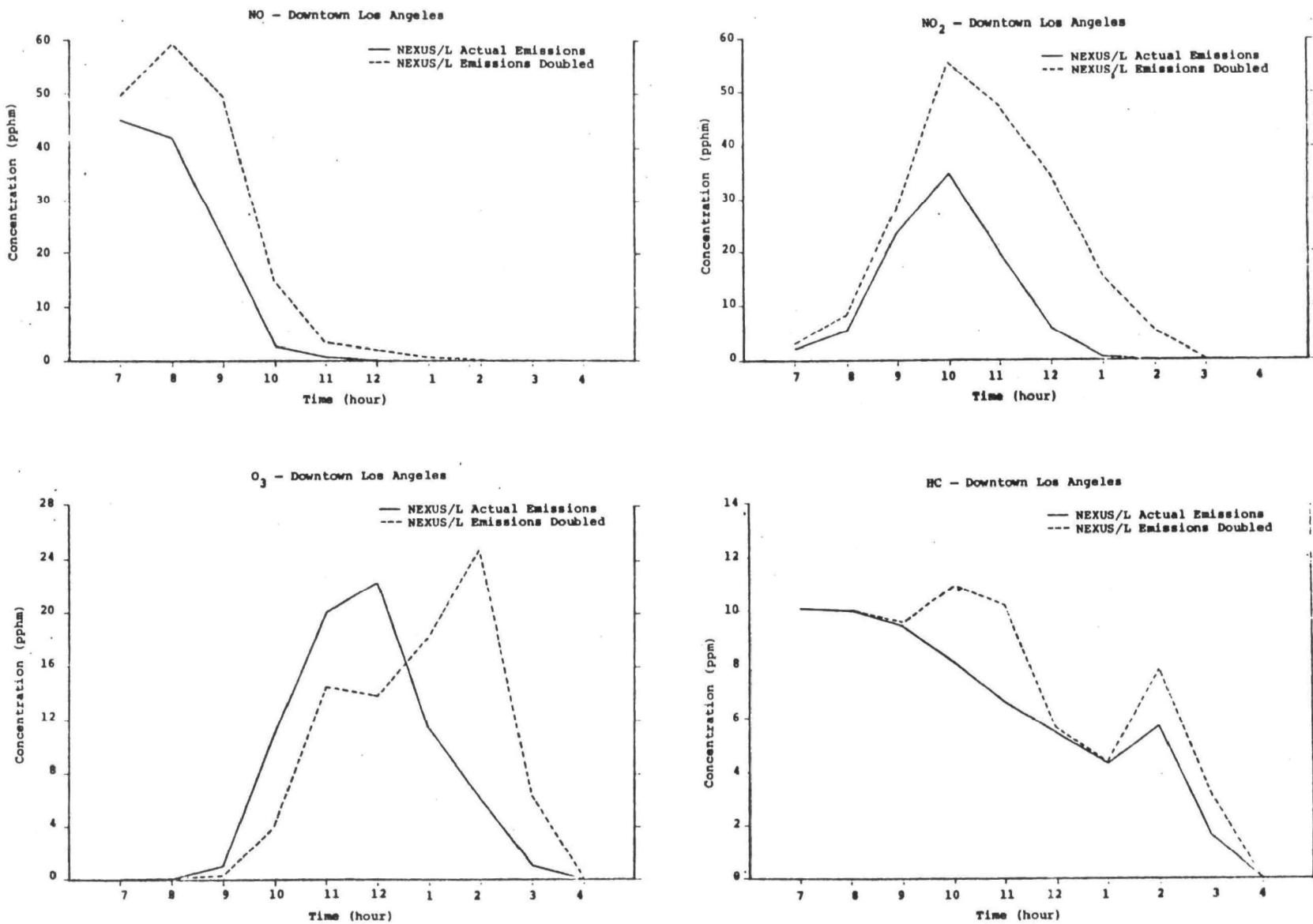


Figure 20. Comparison of Downtown Los Angeles NEXUS/L results for actual emissions and double emissions.

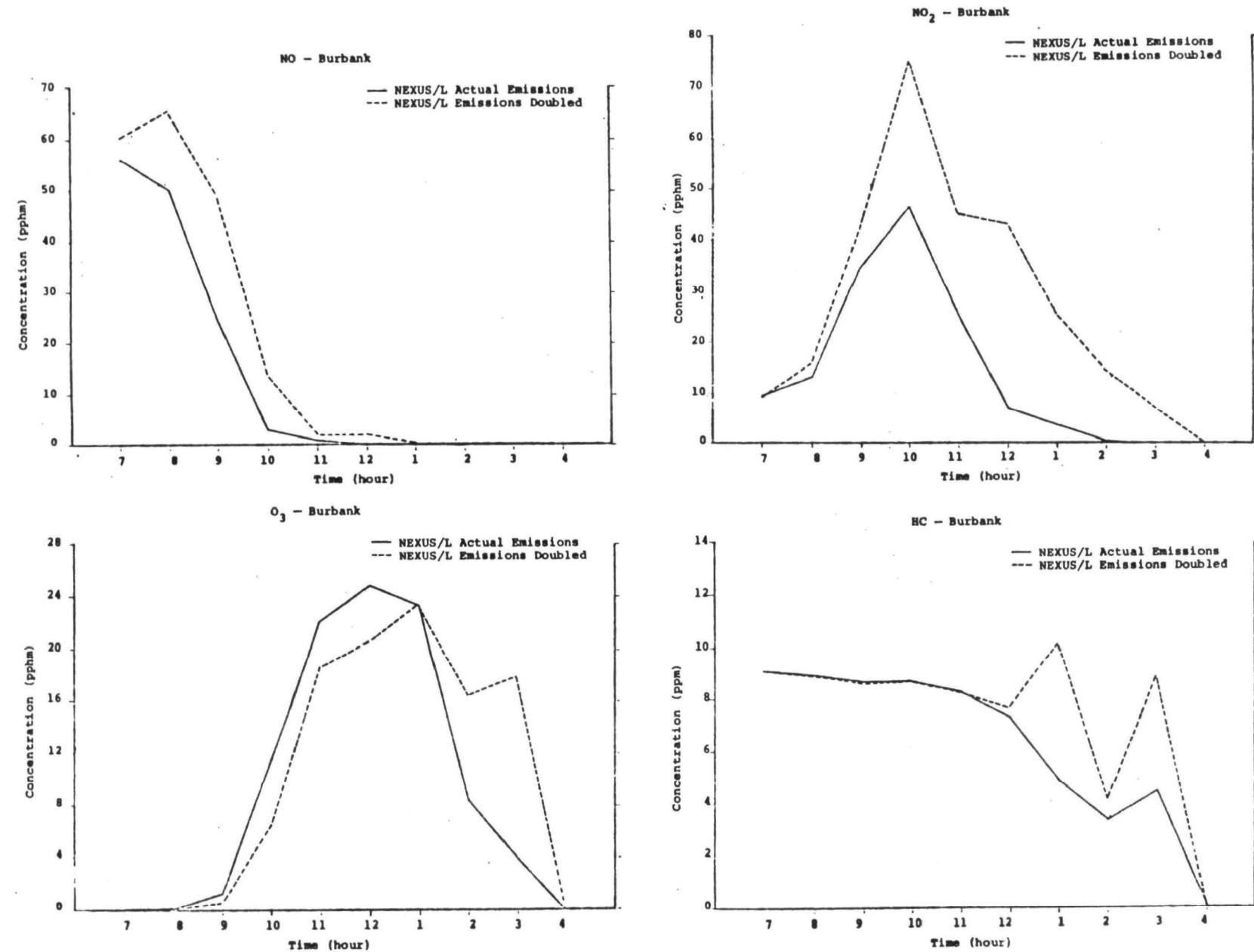


Figure 21. Comparison of Burbank NEXUS/L results for actual emissions and double emissions.

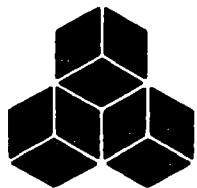
5. SUMMARY AND CONCLUSIONS

A new particle-in-cell code has been developed which employs Lagrangian chemistry and applied to the simulation of photochemical air pollution in the Los Angeles basin. These results are compared with NEXUS/P results and APCD measurements for the selected day. The results of the calculations indicate that either approach, the Eulerian or Lagrangian chemistry, can be used.

An additional calculation was made doubling all of the emissions. The oxidant levels as computed by the simulation were not significantly greater. This is consistent with the expectation that oxidant levels are effected by the NO_x/HC ratio rather than the actual emission levels. These results indicate that care must be taken in extrapolating air quality levels from change in emissions.

REFERENCES

1. Dickson, C.R. and G. Start, private communication (1971).
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4. Roberts, P.J., P.M. Roth and C.L. Nelson, "Contaminant Models in the Los Angeles Basin - Their Sources Rates and Distribution," Report No. 71SAI-6 (1971), Systems Applications, Inc., Beverly Hills, California.
5. Roth, P.M., S.D. Reynolds, P.J. Roberts and J.H. Seinfeld, "Development of a Simulation Model for Estimating Ground Level Concentrations of Photochemical Pollutants," Report No. 71SAI-21 (July 1971), Systems Applications, Inc., Beverly Hills, California.
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7. "A Particle-In-Cell Method for Numerical Solution of the Atmospheric Diffusion Equations, and Applications to Air Pollution Problems," Contract No. 68-02-0006, Report No. 3SR-844 (November 1971), Systems, Science and Software, La Jolla, California.
8. "Mathematical Modeling of Photochemical Smog Using the PICK Method," Contract No. 68-02-0006, APCA Paper No. 72-140 (June 1972), Systems, Science and Software, La Jolla, California.



SYSTEMS, SCIENCE AND SOFTWARE

SSS-R-74-1756

PART II
OPERATIONS MANUAL

1. INTRODUCTION

Systems, Science and Software (S³) has previously developed and documented the computer codes NEXUS/P and [1] SETUP.

A new code, NEXUS/L, has been developed and tested. It differs from the NEXUS/P code in that the photochemical kinetics are considered in a Lagrangian framework, within which each particle contains a specific concentration of each pollutant specie being considered. Previously, in the NEXUS/P code, each particle represented a fixed mass of an individual pollutant.

The purpose of this volume is to document the NEXUS/L code and provide a users guide to its operation.

2. DISCUSSION OF THE NEXUS/L CODE

2.1 GRID LABELING CONVENTIONS

It is useful to be able to reference the Eulerian grid in both cell space (dimensionless) and measured space (meters). The principal axes are noted x, y, and z. The horizontal planes form x-y space, and z is the vertical coordinate.

The cells have dimensions DX, DY, and DZ, and the full grid has NX, NY, and NZ cells in the principal axis directions, respectively. Figure 1 shows a two-dimensional cross-section of the grid. The labeling conventions are the same as with the NEXUS/P code. In cell space, the cell centers are integer triplets [I,J,K] in the x, y, and z directions, respectively. The origin in cell space is [0.5, 0.5, 0.5]. In measured space, the origin is at [0, 0, 0] meters. The center of cell [I,J,K], defined in meters, is [(I-0.5)DX, (J-0.5)DY, (K-0.5)DZ].

2.2 THE NEXUS/L PARTICLES

Each pollutant specie has an individual concentration within each particle. The particles have arbitrarily been sized as exactly one Eulerian cell, DX, DY, DZ, in volume. The concentrations are attributed to the entire particle volume. The position of particle N is defined by the position of its center [x_N , y_N , z_N]. It is convenient to use cell space notation for particle position.

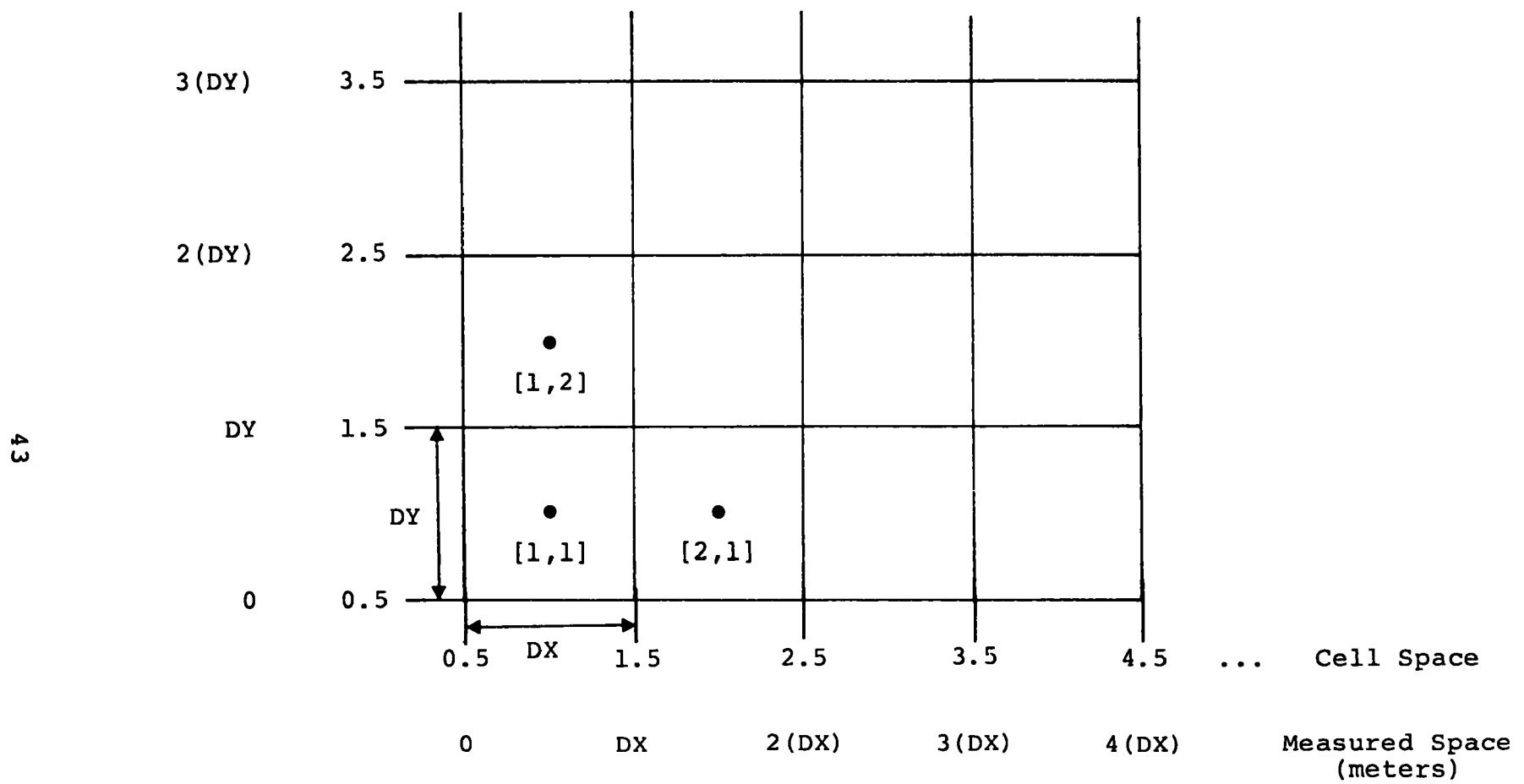


Figure 1. Grid labeling conventions.

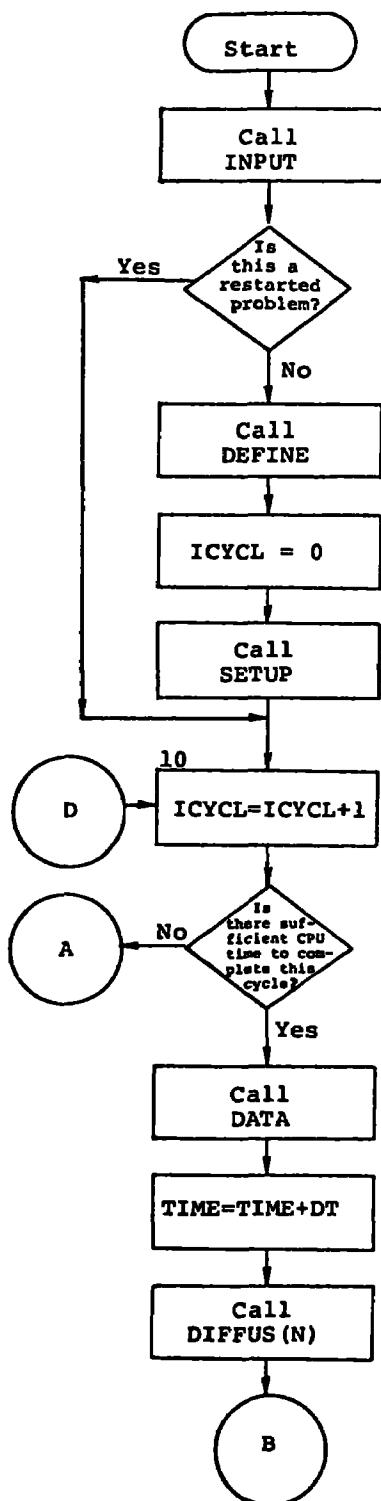
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2.3 FLOW LOGIC OF THE NEXUS/L CODE

The calculational sequence of a typical cycle of the NEXUS/L code is as follows:

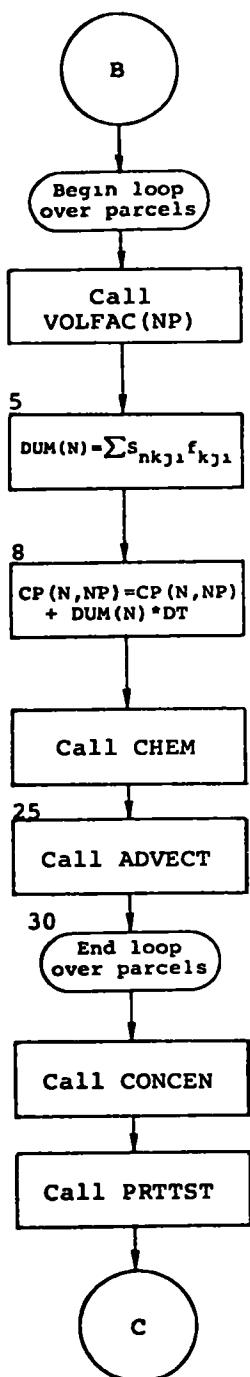
- (1) advance the cycle counter
- (2) obtain updated wind field, diffusivities, and source emission rates (Eulerian framework)
- (3) advance the problem time
- (4) calculate rate of change of concentration due to diffusion (Eulerian framework)
- (5) update the particle concentrations to reflect the effects of source emissions and diffusion and photochemical reactions (Lagrangian framework)
- (6) advect the particles by the wind field to new positions (Lagrangian framework)

A flow chart of the NEXUS/L main program is given in Figures 2(a), (b), and (c).



- determine if problem is to be restarted or generated fresh. Set up all control parameters.
- set up certain indices and constants
- initialize cycle counter
- initialize location and concentration of Lagrangian parcels
- main loop, advance cycle counter
- obtain winds, diffusivities, and sources for this cycle in Eulerian framework
- advance the problem time
- obtain diffusion contribution of each specie in Eulerian framework

Figure 2(a). Flow logic of NEXUS/L main program.



- obtain fractional volumes of this parcel with respect to the Eulerian framework
- use fractional volumes to develop the parcel source term for each specie as a function of the Eulerian sources
- the concentration of each specie is adjusted to reflect the diffusion and new source emissions contributions
- the effects of photochemical reactions are incorporated
- the parcel is advected by the winds to a new coordinate position

- relate concentrations in the Lagrangian parcels to the Eulerian grid framework
- determine if this cycle's results are to be printed, plotted, or saved on a dump file

Figure 2(b). Flow logic of NEXUS/L main program.

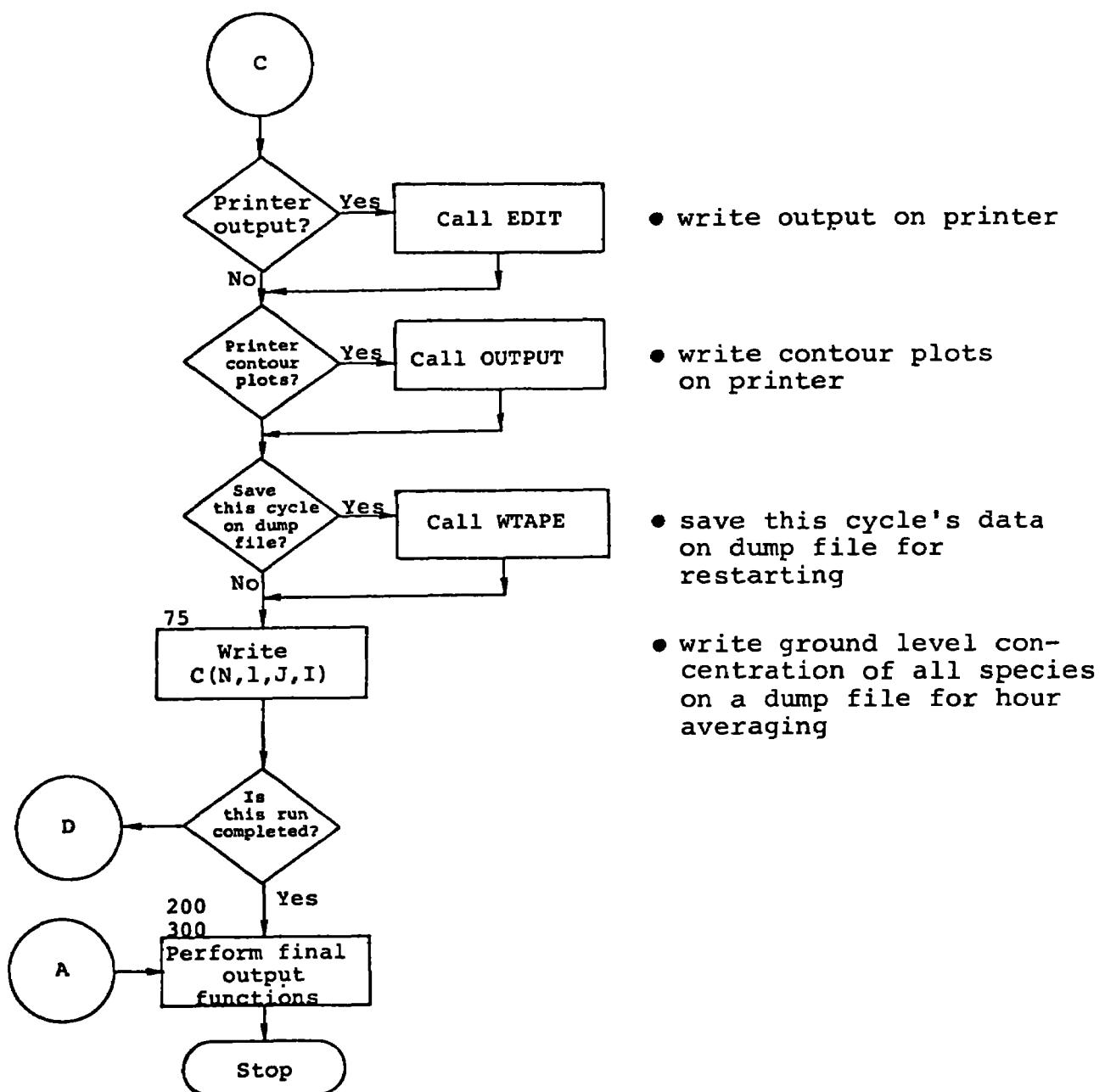


Figure 2(c). Flow logic of NEXUS/L main program.

2.4 GLOSSARY OF KEY QUANTITIES

<u>Quantity</u>	<u>Description</u>	<u>Units</u>
DX	x-direction cell width	m
DY	y-direction cell width	m
DZ	z-direction cell width	m
NX	number of cells in x-direction	
NY	number of cells in y-direction	
NZ	number of cells in z-direction	
NPM	number of Lagrangian particles	
NSP	number of pollutant species	
ICYCL	current problem cycle number	
TIME	current problem time	sec
DT	current cycle time step	sec
U(I,J,K)	x-direction velocity at center of cell i,j,k	m/sec
V(I,J,K)	y-direction velocity at center of cell i,j,k	m/sec
W(I,J,K)	z-direction velocity at center of cell i,j,k	m/sec
EX(I,J,K)	eddy diffusivity for x- and y-direction at center of cell i,j,k	m ² /sec
EZ(I,J,K)	eddy diffusivity for z-direction at center of cell i,j,k	m ² /sec
S(NSP,K,J,I)	specie source rate at center of cell i,j,k	PPM/sec
C(NSP,K,J,I)	specie concentration in Eulerian cell i,j,k	PPM
X(NP)	x-coordinate of particle NP in cell space	
Y(NP)	y-coordinate of particle NP in cell space	
Z(NP)	z-coordinate of particle NP in cell space	
CP(NSP,NP)	specie concentration in particle NP	PPM

2.5 HOW PROBLEMS ARE GENERATED

Subroutine INPUT directs the initialization of calculation. A flow chart of this subroutine appears in Figure 3. Code variables designated "not currently used" exist to permit easy implementation of new code options without major changes to BLANK COMMON and/or subroutine INPUT.

2.5.1 Namelist "START"

"START" is used to provide an overview of the problem to be computed.

RESTRRT: If zero, the problem is to be generated new;

If > 0, the problem is to be restarted and continued.

ISTART: Defines the cycle number at which the problem is to be restarted.

TMAX: A time (in seconds) which, if exceeded in the calculational time, the calculation is to stop.

CYCMAX: A cycle number, which, if exceeded in the calculational process, the calculation is to stop.

CHANGE: If zero, has no effect;

If > 0, and the problem is a restart, requests the variables in namelist "SPECS" to be redefined (see 2.5.2 below).

2.5.2 Namelist "SPECS"

"SPECS" is used to define output control parameters, printer edits, printer contour plots, and dumps on permanent files.

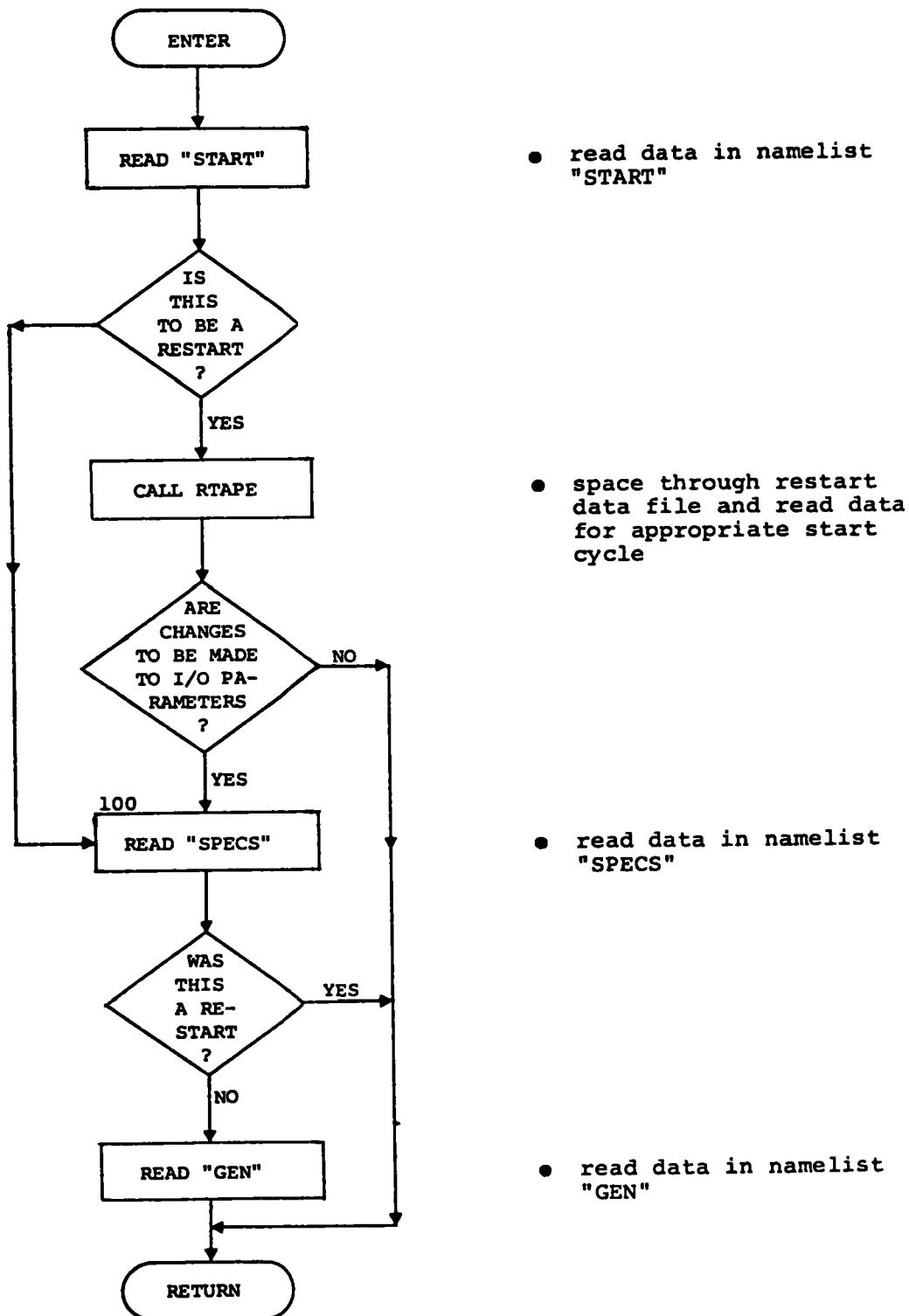


Figure 3. Flow logic of subroutine INPUT.

- IDUMP: Controls dumps of blank common.
If non-zero, dumps will be performed whenever MOD(ICYCL, IDUMP) is zero.
- TDUMP: Permits control of dumps on problem calculational time instead of cycle number.
If non-zero, dumps will be performed each time k*DUMP exceeds TIME.
Note: after each such dump, the integer k is incremented by 1.
- IPRINT: Controls printer edits. Works like IDUMP.
- TPRINT: Works like TDUMP for printer edits.
- IPLOT: Controls printer contour plots. Works like IDUMP.
- TPLOT: Controls printer contour plots. Works like TDUMP.
- LEVELS: Used to shorten printer edits, if desired. The z-levels edited are l-LEVELS rather than l-NZ.
- I1,I2,I3,I4,I5: Not currently used.
- NXY: Number of x-y plane contour plots desired (maximum of 3).
- NXZ: Number of x-z plane contour plots desired (maximum of 3).
- NYZ: Number of y-z plane contour plots desired.
- XYP(3): Used to specify the z-cross sections desired for the (NXY) x-y plane contour plots.
- XZP(3): Used to specify the y-cross sections desired for the (NXZ) x-z plane contour plots.
- YZP(3): Used to specify the x-cross sections desired for the (NYZ) y-z plane contour plots.

ISP(5): Used to choose which species are to be contour plotted.
 If ISP(K) = 0, specie k is not plotted.
 If ISP(K) > 0, specie k is available for plotting.

2.5.3 Namelist "GEN"

"GEN" is used to define the grid characteristics, and in the case of certain test problems, "GEN" can be used to define the winds and diffusivities.

NX: Number of x-direction cells.
NY: Number of y-direction cells.
NZ: Number of z-direction cells.
NSP: Number of pollutant species.
DX: Width of a cell in x-direction.
DY: Width of a cell in y-direction.
DZ: Width of a cell in z-direction.
NPC: Number of Lagrangian parcels to be created for each Eulerian grid cell.
NS: Not currently used.
TIME: Calculation time (sec) at which the problem is to be initialized.
DT: Calculational time step to be used.
FLAG1,
FLAG2,
IFLAG1,
IFLAG2: Not currently used.
CONST: (Logical Variable) Used to quickly set up test problems.
 If input as .TRUE., then winds and diffusivities will be constant throughout the calculation:

The following are input if CONST = .TRUE.

UFIX: u-velocity in each cell

VFIX: v-velocity in each cell

WFIX: w-velocity in each cell

EXFIX: x,y diffusivities in each cell

EZFIX: z diffusivity in each cell

GROUND: (Logical Variable) Set to .TRUE. if it
is desired to dump ground level con-
centrations on a permanent file each
cycle.

3. CODE LISTING

The NEXUS/L code, as used to run the Los Angeles photochemical simulation, is documented below. The code elements are in the following order:

procedure	BLANK
subroutine	ADVECT
subroutine	CHEM
subroutine	CONCEN
subroutine	CONTUR
subroutine	DATA
subroutine	DEFINE
subroutine	DIFFUS
subroutine	EDIT
subroutine	INPUT
program	MAIN
subroutine	OUTPUT
subroutine	PL
subroutine	PRTTST
subroutine	RTAPE
subroutine	SETUP
subroutine	VOLFAC
subroutine	WTAPE

BLANK COMMON

```

1      .BLANK
2      BLANK PROC
3      C
4      C*****PARAMETER STATEMENTS
5      C
6      PARAMETER NXI=22,NYI=21,NZI=4,NSPI=5,MAX=2772
7      PARAMETER LUH=NSPI*NXI*NYI*NZI,LUN=NXI*NYI*NZI
8      C*****BLANK COMMON
9      C
10     COMMON DUM(10),IDUM(10),NX,NY,NZ,NSP,NPC,NP,NS,NPM,NCOMM,
11     1  NXP1,NYP1,NZP1,NX1,NY1,NZ1,IPI1,JP1,KP1,IM1,JM1,KM1,
12     2  TIME,DT,TMAX,CYCHAX,SAVE,RESTRT,ICYCL,PPINTX,PLOT,DUMP,GROUND
13     3  ISTART,IPRINT,TPRINT,IPLOT,TPLOT,IDUMP,TDUMP,TIMH,TIMN,
14     4  TIMO,NTAPE,FLAG1,FLAG2,IFLAG1,IFLAG2,11,12,13,14,15,LEVELS,
15     5  DX,DY,DZ,DTDX,DTDY,DTDZ,RDX,RDY,RDX2,RDY2,RDZ2,DUMHIT,CONS
16     6  U(NXI,NYI,NZI),V(PXI,NYI,NZI),V(NXI,NYI,NZI),CP(NSPI,MAX),
17     7  C(NSPI,NZI,NYI,NXI),S(NSPI,NZI,NYI,NXI),X(MAX),Y(MAX),Z(MAX),
18     8  EX(NXI,NYI,NZI),EZ(NXI,NYI,NZI),UFIX,VFIX,WFIX,EXFIX,EZFIX
19     C
20     COMMON /IO/ NAY,NXZ,NYZ,XYP(3),XZP(3),YZP(3),ISP(5),TITLE$15
21     C
22     LOGICAL PLOT,PRINTX,DUMP,SAVE,CONST,GROUND
23     INTEGER DUMMY
24     C
25     END

```

ADVECT

```

1      .ADVECT
2      SUBROUTINE ADVECT
3      INCLUDE BLANK
4      COMMON /PARCEL/ II,JJ,KK,F1,F2,F3,F4,F5,F6,F7,F8,I,J,K
5
6      C
7      VI= U(I,J,K)*F1+U(I,J,K)*F2+U(I,JJ,K)*F3+U(I,JJ,K)*F4 +
8      1   U(I,J,KK)*F5+U(I,I,J,KK)*F6+U(I,JJ,KK)*F7+U(I,JJ,KK)*F8
9      V2= V(I,J,K)*F1+V(I,J,K)*F2+V(I,JJ,K)*F3+V(I,JJ,K)*F4 +
10     2   V(I,J,KK)*F5+V(I,J,KK)*F6+V(I,JJ,KK)*F7+V(I,JJ,KK)*F8
11      C*****SPECIAL DEAL FOR THE BOTTOM LEVEL
12      IF(Z(NP) .LT. 1.5) GO TO 4
13      V3= W(I,J,K)*F1+W(I,I,J,K)*F2+W(I,JJ,K)*F3+W(I,JJ,K)*F4 +
14      3   W(I,J,KK)*F5+W(I,I,J,KK)*F6+W(I,JJ,KK)*F7+W(I,JJ,KK)*F8
15      GO TO 8
16      4 V3=(Z(NP)-G.5)*0.5*((F1+F5)+(F2+F6)+W(I,JJ,2)
17      1 +(F3+F7)+W(I,JJ,2)+(F4+F8)+W(I,JJ,2))
18      C
19      C
20      8 X(NP)= X(NP) + VI * DTDX
21      Y(NP)= Y(NP) + V2 * DTDY
22      Z(NP)= Z(NP) + V3 * DTDZ
23      C
24      ZERO=0.0
25      IF(X(NP) .GL. 0.5) GO TO 10
26      C
27      *X < 0.5
28      X(NP)=X(NP)+NX
29      ZERO=1.0
30      10 IF(X(NP) .LT. NX+0.5) GO TO 20
31      C
32      *X > NX+0.5
33      X(NP)=X(NP)-NX
34      ZERO=1.0
35      20 IF(Y(NP) .GL. 0.5) GO TO 30
36      C
37      *Y < 0.5
38      Y(NP)=Y(NP)+NY
39      ZERO=1.0
40      30 IF(Y(NP) .LT. NY+0.5) GO TO 40
41      C
42      *Y > NY+0.5
43      Y(NP)=Y(NP)-NY
44      ZERO=1.0
45      40 IF(Z(NP) .GE. 0.5) GO TO 50
46      C
47      *Z < 0.5
48      Z(NP)=.501
49      50 IF(Z(NP) .LT. NZ+0.5) GO TO 100
50      Z(NP)=Z(NP)-NZ
51      ZFRO=1.0
52      C
53      100 IF(ZERO .LT. 0.5) GO TO 200
54      DO 150 N=1,NSP
55      CPIN(NP)=0.0
56      150 CONTINUE
57      C
58      200 RETURN

```

```

ADVECTG1
ADVECT02
ADVECT03
ADVECTG4
ADVECT05
ADVECT06
ADVECT07
ADVECT08
ADVECTG9
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ADVECT52
ADVECT53

```

ADVECT

54 C
55 END

ADVECT54
ADVECT55

57

SSS-R-74-1756

ANSCHK

```
1      .ANSCHK
2          SUBROUTINE ANSCHK(XX,XY)
3          LOGICAL XY
4          XY=.FALSE.
5          IF(XX .EQ. 'YES') GO TO 50
6          IF(XX .EQ. ' YES ') GO TO 50
7          IF(XX .EQ. ' YES') GO TO 50
8          IF(XX .EQ. ' YES') GO TO 50.
9          GO TO 100
10         50 XY=.TRUE.
11
12         C
13         100 RETURN
14         C
15         END
```

CHEM

```

1      .CHEM
2      1  DELTAT,TIM
3      C THIS ROUTINE SOLVES THE CHEMICAL RATE CHANGE EQUATIONS AND RETURN SCHEM0001
4      C THE FRACTIONAL CHANGE IN CONCENTRATION OF EACH SPECIE. SCHEM0002
5      DATA C0NE, CIA, C2, C3, C4, C5, C6, C7, C8, C9, CTEN, C11, C12, SCHEM0003
6      1 C13, C14, C15 / .267, 2.64E6, 26.7, 2.81E-5, 1.5E4, .004, SCHEM0004
7      2 1.E5, 200., 1500., 3000., .001, .001, .05, 4500., 14., 60.5 / SCHEM0005
8      DATA R1, R2, R3, R4 / 2*10., 2*1/
9      REAL NO, NO2, NO3, NO25
10     DIMENSION Y(10), YS(10), A(5), B(5), R(5), E(3), LF(3)
11     DATA ER / .625 /
12     EQUIVALENCE(Y(1),NO), (Y(2),NO2), (Y(3),O3), (Y(4),HNO2),
13     1 (Y(5),HC), (Y(6),O), (Y(7),OH), (Y(8),RO2), (Y(9),NO3),
14     2 (Y(10),NO25)
15     NAMELIST// CIA,C2,C3,C4,C5,C6,C7,C8,C9,CTEN,C11,C12,C13,
16     1 C14,C15,L1,B2,R3,R4,ER
17     C
18     DEFINE F1 = C6*NO + C7*NO2
19     DEFINE F2 = C6*P4*NO
20     DEFINE F3 = C14 + C15
21     DEFINE F4 = C4*HC + C8*NO + C9*NO2
22     DEFINE F5 = C6*P4*RO2*NO + C10*HNO2
23     DEFINE FNO = C1*NO2 + C10*HNO2
24     DEFINE RN0 = C2*O3 + C6*RO2 + C8*OH + C11*NO2
25     DEFINE RN02 = 1(C2*O3 + C6*RO2)*NO + C14*NO25
26     DEFINE RN02 = L1 + C7*RO2 + C9*OH + C11*NO + C12*O3 + C13*NO3
27     DEFINE F03 = CIA*O
28     DEFINE NO3 = C2*NO + C5*HC + C12*NO2
29     DEFINE HNO2 = C8*OH*NO + Z*C11*NO*NO2
30     DEFINE HNO2 = C10
31     DEFINE HMC = C3*O + C4*OH + C5*O3
32     DEFINE EO = C1*P2/(CIA + C3*HC)
33     DEFINE LOH = (F2*C3*B1*O*HC + F2*C5*B3*O3*HC + F1*C10*HNO2)/
34     1 (F1+F4 - F2*C4*B2*HC)
35     DEFINE ERC2 = HC*(C3*B1*O + C4*B2*OH + C5*B3*O3)/F1
36     DEFINE EN03 = C12*O3*F3/(C13*C15)
37     DEFINE EN205 = C13*NO2*NO3/F3
38     DEFINE RATE(1) = (A(1) - B(1)*Y(1))/TT
39     C
40     C
41     3 ITEST=0
42     TIME = 0.
43     C PHOTOCHMICAL REACTION RATE VARIES SINUSOIDALLY FROM 6 AM TO 6 P
44     TIMH=TIME/3600.
45     5 DT = 1.0E-6
46     TT=DELTAT/60.0
47     NO = ONG
48     NO2 = CNO2
49     HC = OHLC
50     O3 = O03
51     HNO2 = OHNO2
52     10 NT = 1
53     SINC = SIN(2*PI*TIMH - 6.0 + TT/60.0 + TIME/60.0*2618)
```

CHEM

```

54      IF (SINC .LT. 0.0) SINC=0.0          CHEM0054
55      CI = CONC*SINC                      CHEM0055
56      C10 = CTEN*SINC                     CHEM0056
57      12 O = EO                          CHEM0057
58      OH = EOH                          CHEM0058
59      RO2 = EHO2                         CHEM0059
60      NO3 = EHO3                         CHEM0060
61      N2O5 = EN2O5                        CHEM0061
62      C *ADD SOURCE RATES TO FORMATION RATES   CHEM0062
63      A(1)=FNO+DUM1                      CHEM0063
64      A(2)=FNO2+DUM2                     CHEM0064
65      A(3)=FO3+DUM3                      CHEM0065
66      A(4)=FHIO2+DUM4                     CHEM0066
67      A(5)=DUM5                         CHEM0067
68      B(1) = HNO                         CHEM0068
69      B(2) = HNO2                        CHEM0069
70      B(3) = HO3                          CHEM0070
71      B(4) = RHNO2                       CHEM0071
72      B(5) = RHC                          CHEM0072
73      IF (NT .EQ. 2) GO TO 38           CHEM0073
74      NT = 2                           CHEM0074
75      C TEST TO SEE IF SIGNIFICANT PHOTOCHEMICAL REACTION WILL OCCUR THIS   CHEM0075
76      TIME STEP, AND, IF NOT, USE SIMPLE RATE EQUATION AND RETURN           CHEM0076
77      IF (TEST .NE. 0) GO TO 19          CHEM0077
78      TEST = 1                         CHEM0078
79      DO 15 I=1,5                      CHEM0079
80      R(I)=RATE(I)                    CHEM0080
81      15 CONTINUE
82      XTEST = ABS((Y(1) + R(1)) - (Y(2) + R(2)) / ABS(Y(1))/Y(2))    CHEM0082
83      IF(ABS(R(1)) .LT. 1.0E-10 .AND. ABS(R(2)) .LT. 1.0E-10) XTEST= 1.0E-10  CHEM0083
84      IF (ABS(R(3)) .GT. .01 .OR. XTEST .GT. 1.0 .OR. XTEST .LT. -.9)    CHEM0084
85      1 GO TO 19                      CHEM0085
86      DO 16 I = 1, 3                  CHEM0086
87      LF(I) = 0                      CHEM0087
88      E(I) = A(I)/B(I)                CHEM0088
89      IF (Y(I) .LT. E(I)) LF(I) = 1    CHEM0089
90      16 CONTINUE
91      DO 17 I=1,5                  CHEM0090
92      QI=EXP(-B(I)*DT)              CHEM0091
93      QTEST=(1.0-LI)*A(I)/B(I)+QI*Y(I)    CHEM0092
94      Y(I)=MAX(0.0,LI*QTEST)        CHEM0093
95      17 CONTINUE
96      E(3) = FO3/RO3                CHEM0094
97      DO 18 I = 1, 3                CHEM0095
98      IF (Y(I) .LT. E(I) .AND. LF(I) .EQ. 0 .OR. Y(I) .GT. E(I) .AND.    CHEM0096
99      LI*LF(I) .EQ. 0) Y(I) = E(I)    CHEM0097
100     18 CONTINUE
101     XTEST = (Y(1)/Y(2))/(ONO/ONO2)    CHEM0098
102     IF(XTEST.GT.0.9 .AND. XTEST.LT.1.1) GO TO 900    CHEM0099
103     GO TO 5                         CHEM0100
104     19 CONTINUE
105     DO 30 I = 1, 5                CHEM0101
106     YS(I) = Y(I)                  CHEM0102
107     IF (B(I)*DT .GT. 1.0E-7) GO TO 20    CHEM0103

```

CHEM

```

108      Y(1) = .5*A(1)*DT + Y(1)          CHEMO108
109      GO TO 30                         CHEMO109
110      20 Y(1) = (A(1)/B(1) + (Y(1) - A(1)/B(1))*EXP(-B(1)*DT) + Y(1))*0.5  CHEMO110
111      30 CONTINUE                      CHEMO111
112      GO TO 12                         CHEMO112
113      38 DO 50 I = 1, 5                CHEMO113
114      IF (R(I)*DT .GT. 1.E-7) GO TO 40  CHEMO114
115      Y(I) = A(I)*DT + YS(I)          CHEMO115
116      GO TO 50                         CHEMO116
117      40 Y(I) = A(I)/B(I) + (YS(I) - A(I)/B(I))*EXP(-R(I)*DT)  CHEMO117
118      50 CONTINUE                      CHEMO118
119      TIME = TIME + DT                CHEMO119
120      IF (TIME .GE. TT) GO TO 900    CHEMO120
121      C = 0.                          CHEMO121
122      DO 60 I = 1, 5                CHEMO122
123      IF (Y(I) .LT. 1.E-4) GO TO 60  CHEMO123
124      C = MAX(C, ABS((Y(I) - YS(I))/(Y(I) + YS(I))))  CHEMO124
125      60 CONTINUE                      CHEMO125
126      C = MAX(C, .1*ERI)            CHEMO126
127      DT = MIN(ER/C*DT, TT - TIME)  CHEMO127
128      GO TO 10                         CHEMO128
129      ***** *UPDATE CPL(1) ARRAY AND RETURN TO MAIN PROGRAM *CHEMO129
130      C
131      900 END=END                     CHEMO130
132      OH02=H02                        CHEMO131
133      OHC=HC                          CHEMO132
134      O03=O3                          CHEMO133
135      OHH02=HH02                      CHEMO134
136      RETURN                         CHEMO135
137      END                           CHEMO136

```

61

CONCEN

```

1      .CONCEN
2          SUBROUTINE CONCEN
3              INCLUDE BLANK
4              COMMON /PARCEL/ II,JJ,KK,F1,F2,F3,F4,F5,F6,F7,F8,I,J,K
5
6      C      **ZERO OUT C,S ARRAYS
7          CALL S3ZERO(C,HUM)
8          CALL S3ZERO(S,HUM)
9
10     C      DO 100 NP=1,NPM
11     C      CALL VOLFAC(NP)
12     C      DO 50 N=1,NSP
13     C
14         C(N,K,J,II) = C(N,K,J,II) + F1*CP(N,NP)
15         S(N,K,J,II) = S(N,K,J,II) + F1
16         C(N,K,J,II) = C(N,K,J,II) + F2*CP(N,NP)
17         S(N,K,J,II) = S(N,K,J,II) + F2
18         C(N,K,JJ,II) = C(N,K,JJ,II) + F3*CP(N,NP)
19         S(N,K,JJ,II) = S(N,K,JJ,II) + F3
20         C(N,K,JJ,II) = C(N,K,JJ,II) + F4*CP(N,NP)
21         S(N,K,JJ,II) = S(N,K,JJ,II) + F4
22         C(N,K,JJ,II) = C(N,K,JJ,II) + F5*CP(N,NP)
23         S(N,K,JJ,II) = S(N,K,JJ,II) + F5
24         C(N,KK,J,II) = C(N,KK,J,II) + F6*CP(N,NP)
25         S(N,KK,J,II) = S(N,KK,J,II) + F6
26         C(N,KK,J,II) = C(N,KK,J,II) + F7*CP(N,NP)
27         S(N,KK,J,II) = S(N,KK,J,II) + F7
28         C(N,KK,JJ,II) = C(N,KK,JJ,II) + F8*CP(N,NP)
29         S(N,KK,JJ,II) = S(N,KK,JJ,II) + F8
30
31     C      50 CONTINUE
32
33     C      100 CONTINUE
34
35     C      DO 200 I=1,NX
36         DO 200 J=1,NY
37         DO 200 K=1,NZ
38         DO 200 N=1,NSP
39         C(N,K,J,II)=C(N,K,J,II)/S(N,K,J,II)
40
41     C      200 CONTINUE
42
43     C      RETURN
44     C      END
45

```

```

CONCEN01
CONCEN02
CONCEN03
CONCEN04
CONCEN05
CONCEN06
CONCEN07
CONCEN08
CONCEN09
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CONCEN41
CONCEN42
CONCEN43
CONCEN44
CONCEN45

```

CONTUR

```
1      .CONTUR
2      SUBROUTINE CONTUR(IJMAX,IX,IY,X,K,TIXX,KK,TAB,KKK)
3      COMMON /TFIX/ICYCL,TIME
4      DIMENSION TAB(2),X(IJMAX,IY)
5      DATA NC,CMIN,CHAX,LOGFL / 10.0,.0,.0 /
6      C   **ADJUST PRINTER SPACING
7      CALL PRTCN(*M,66,0,0,*)
8      CALL PPTCN(*L,4,*)
9      WRITE(6,1000) TAB(1),I=1,2,ICYCL,TIME
10     CALL PLNC,A,IX,IY,IJMAX,CMIN,CHAX,LOGFL)
11     C   **RESET NORMAL PRINTER SPACING
12     CALL PRTCN(*M,66,6,6,*)
13     C
14     C   RETURN
15     C
16     C   **FORMATS
17     1000 FORMAT(5X,4H0000,3X,2A6,4H0000,10X,RHCYCLE = ,15,6X,7HTIME = ,
18           1   F10.3)
19     END
```

```
CONTUR1
CONTUR2
CONTUR3
CONTUR4
CONTUR5
CONTUR6
CONTUR7
CONTUR8
CONTUR9
CONTUR10
CONTUR11
CONTUR12
CONTUR13
CONTUR14
CONTUR15
CONTUR16
CONTUR17
CONTUR18
CONTUR19
```

DATA

```

1      .DATA
2          SUBROUTINE DATA
3          INCLUDE BLANK
4          DIMENSION U1(NX1,NY1),U2(NX1,NY1),U3(NX1,NY1)
5          EQUIVALENCE (U(1,1,1),U3(1,1,1),(V(1,1,1),U2(1,1,1)),(U(1,1,2),
6              U(1,1,1)))
7          DINFUSION SS(5,NZ1,NY1,NX1), FACTOR(5)
8          EQUIVALENCE (S,SS)
9          DATA FACTOR / 30.,46.,0.,0.,13. /
10         DATA VOLUME /1.036E9/
11         C   **ZERO OUT S ARRAY
12         CALL SSZERO(S,NUM)
13         C
14         IF(ICONST) GO TO 100
15         C*****TAPE DATA
16         C*****READ DATA
17         IS READ (IU) UT,U1,U2,U3,EX,EZ
18         READ (IG) (((SS(L,K,J,1),L=1,31,K=1,NZ1,J=1,NY1),I=1,NX1)
19         C
20         C
21         IF(DT .LT. 0.0) STOP NEG DT
22         RDT=1.0/DT
23         DO 20 I=1,NX
24         DO 20 J=1,NY
25         U(I,J,2)=U(I,J,1)
26         U(I,J,3)=-U(I,J,1)
27         U(I,J,4)=U(I,J,3)
28         V(I,J,2)=V(I,J,1)
29         V(I,J,3)=-V(I,J,1)
30         V(I,J,4)=V(I,J,3)
31         W(I,J,1)=0.0
32         W(I,J,2)=2.0*W(I,J,1)
33         W(I,J,3)=W(I,J,2)
34         W(I,J,4)=0.0
35         DO 19 K=1,NZ
36         EX(I,J,K)=EX(I,J,K)*RDT
37         EZ(I,J,K)=EZ(I,J,K)*RDT
38         19 CONTINUE
39         20 CONTINUE
40         C   **MOVE SS ARRAY TO S ARRAY AND CONVERT KG TO PPM
41         C
42         DO 50 J=1,NY
43         DO 50 I=1,NX
44         S(5,K,J,1)=SS(3,K,J,1)
45         S(3,K,J,1)=6.0
46         C   AIR DENSITY 1.23 KG/M3 MOLE WEIGHT 28.4
47         DO 45 L=1,NSP
48         IF(FACTOR(L) .LT. 1.0E-8) GO TO 45
49         SIL(K,J,1)=SIL(K,J,1)+28.4*1.0E6*RDT/(FACTOR(L)*1.23*VOLUME)
50         45 CONTINUE
51         50 CONTINUE

```

```

DATA0001
DATA0002
DATA0003
DATA0004
DATA0005
DATA0006
DATA0007
DATA0008
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DATA0010
DATA0011
DATA0012
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DATA0014
DATA0015
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DATA0017
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DATA0020
DATA0021
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DATA0040
DATA0041
DATA0042
DATA0043
DATA0044
DATA0045
DATA0046
DATA0047
DATA0048
DATA0049
DATA0050
DATA0051
DATA0052
DATA0053

```

DATA

```
54      IF(FLAG1 .LT. 1.0E-6) GO TO 200
55      C   •OPTION TO TURN OFF DIFFUSION
56      CALL S3ZERO(EX,LUM)
57      CALL S3LERC(EZ,LUM)
58      GO TO 200
59      C
60      C*****DATA SPECIFIED BY INPUT
61      C
62      100 DO 150 I=1,NX
63      DO 150 J=1,NY
64      DO 150 K=1,NZ
65      EX(I,J,K)=LXFIX
66      EZ(I,J,K)=LZFIX
67      U(I,J,K)=UFIX
68      V(I,J,K)=VFIX
69      W(I,J,K)=WFIX
70      150 CONTINUE
71      C
72      200 DTDX=DTeRDX
73      DTDY=DTeRDY
74      DTDZ=DTeRDZ
75      C
76      RFTURN
77      END
```

```
DATA0054
DATA0055
DATA0056
DATA0057
DATA0058
DATA0059
DATA0060
DATA0061
DATA0062
DATA0063
DATA0064
DATA0065
DATA0066
DATA0067
DATA0068
DATA0069
DATA0070
DATA0071
DATA0072
DATA0073
DATA0074
DATA0075
DATA0076
DATA0077
```

DEFINE

```
1      .DEFINE
2          SUBROUTINE DEFINE
3          INCLUDE BLANK
4          DATA DU,IHY/5/
5          NCOMM=7+LUM*(2*NSPI+5)+MAX*(NSPI+3)
6          NXPI=NX+1
7          NYPI=NY+1
8          NZPI=NZ+1
9          NXHI=NX-1
10         NYHI=NY-1
11         NZHI=NZ-1
12         RDX=1.0/DX
13         RDY=1.0/DY
14         RDZ=1.0/DZ
15         RDX2=RDX*RDX
16         RDY2=RDY*RDY
17         RDZ2=RDZ*RDZ
18         PRINT 100, NCOMM
19         100 FORMAT(1X, '*****NCOMM = ', I6, '*****')
20         RETURN
21         END
```

DEFINE01
DEFINE02
DEFINE03
DEFINE04
DEFINE05
DEFINE06
DEFINE07
DEFINE08
DEFINE09
DEFINE10
DEFINE11
DEFINE12
DEFINE13
DEFINE14
DEFINE15
DEFINE16
DEFINE17
DEFINE18
DEFINE19
DEFINE20

```

1      DIFFUS
2      .DIFFUS
3      SUBROUTINE DIFFUS(NX,NY,NZ)
4      INCLUDE BLANK
5      C
6      DO 100 I=1,NX
7      DO 100 J=1,NY
8      DO 100 K=1,NZ
9      C
10     CALL INDEX(I,J,K)
11
12     C***** X-Y DIFFUSION
13     C
14     TERM1=EX(I,J,K)*(C(N,K,J,IP1)-2.0*C(N,K,J,I)+C(N,K,J,IM1)).RUX 10
15     I+(C(N,K,JP1,I)-2.0*C(N,K,J,I)+C(N,K,JM1,I))*RDY2)
16     C***** Z DIFFUSION
17     C
18     TERM2=EZ(I,J,K)*(C(N,KP1,J,I)-2.0*C(N,K,J,I)+C(N,KM1,J,I))*RUZ2
19     C
20     C***** INCREMENT SOURCE ARRAY
21     C
22     C
23     SIN(K,J,I)=SIN(K,J,I)+TERM1+TERM2
24     100 CONTINUE
25     RETURN
26     C***** SUBROUTINE INDEX(I,J,K)
27     C
28     C
29     C          TEMP B.C.
30     IP=I+1
31     IM1=I-1
32     JP1=J+1
33     JM1=J-1
34     KP1=K+1
35     KM1=K-1
36     IF(I.EQ.1)      IH=NX
37     IF(J.EQ.1)      JH=NY
38     IF(K.EQ.1)      KH=NZ
39     IF(I.EQ.NX)     IP=1
40     IF(J.EQ.NY)     JP=1
41     IF(K.EQ.NZ)     KP=1
42     C
43     C
44     RETURN
45     C***** END
46

```

DIFFUS01
DIFFUS02
DIFFUS03
DIFFUS04
DIFFUS05
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DIFFUS07
DIFFUS08
DIFFUS09
DIFFUS10
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DIFFUS41
DIFFUS42
DIFFUS43
DIFFUS44
DIFFUS45
DIFFUS46

EDIT

```

1      .EDIT
2          SUBROUTINE EDIT
3              INCLUDE BLANK
4              DIMENSION CLIN(NX)
5              DIMENSION FACT(5)
6              DATA FACT /4*100.0,1.0/
7
8          C
9          C      **ISP SELCTS WHICH SPECIES ARE EDITED
10         C
11         48 DO 100 J=1,NSP
12             IF((ISP(J) .EQ. 0) GO TO 100
13             SP=TITLES(J)
14
15             SUM=0.0
16             DO 60 K=1,LEVELS
17                 IF(MOD(K+1,2) .EQ. 0) PRINT 6005
18
19                 6005 FORMAT(1H1)
20                 TIMEX=TIME/3600.
21                 PRINT A$10,SP,K,TIMEX,ICYCL
22                 6010 FORMAT(1X,'CONCENTRATIONS OF ',A6,', IN X-Y SPACE FOR LEVEL ',I2
23                 I ,/,A5,'TIME = ',F8.2,4X,'CYCLE = ',I5,/)
24                 DO 50 J = NY, 1, -1
25                 DO 49 I=1,NA
26                     CLIN(I)=FACT(N)*C(N,K,J,I)
27                     SUM=SUM+CLIN(I)
28
29                     49 CONTINUE
30                     50 PRINT 6350, (CLIN(I),I=1,NXM)
31
32                     6050 FORMAT(2X,21F6.2)
33                     60 CONTINUE
34                     WRITE(6,1006) SUM
35                     1000 FORMAT(1X,'SUM OF ALL CONCENTRATIONS = ',F12.3)
36                     100 CONTINUE
37
38                     5000 RETURN
39                     END

```

EDIT0001
 EDIT0002
 EDIT0003
 EDIT0004
 EDIT0005
 EDIT0006
 EDIT0007
 EDIT0008
 EDIT0009
 EDIT0010
 EDIT0011
 EDIT0012
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 EDIT0015
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 EDIT0021
 EDIT0022
 EDIT0023
 EDIT0024
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 EDIT0028
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 EDIT0034
 EDIT0035
 EDIT0036

INPUT

```

1      .INPUT
2          SUBROUTINE INPUT                               INPUT001
3          INCLUDE BLANK                                INPUT002
4          C                                           INPUT003
5          NAMELIST /START/RESTRT,ISTART,TMAX,CYCMAX,CHANGE   INPUT004
6          C                                           INPUT005
7          DATA NX,NY,NZ,NSP,DX,DY,DZ,CONST / 4,4,1,5,10.,10.,10.,10.,.TRUE.    INPUT006
8          DATA NPC,DT,TIME / 1,600.,21600. /             INPUT007
9          DATA TITLES /6HNO ,6HN02 ,6H03 ,6HHH02 6HHC   INPUT008
10         DATA ISP /5+1 /
11         NAMELIST /SPEC5/ IDUMP,T_DUMP,IPRINT,TPRINT,IPLOT,T_PLOT,
12           LEVELS,11,12,13,14,15,NXY,NXZ,NYZ,XYP,XZP,YZP,ISP   INPUT011
13         NAMELIST /GEN/ NX,NY,NZ,NSP,DX,DY,DZ,NPC,NS,TIME,DT,FLAG1,FLAG2,   INPUT012
14           FLAG1,FLAG2,CONST,UFIX,VFIX,WFIX,EXFIX,EZFIX,GROUND   INPUT013
15         C                                           INPUT014
16         READ(5,START)                                INPUT015
17         C                                           INPUT016
18         IF(RESTRT.LT.1.E-6) GO TO 100                INPUT017
19         C                                           INPUT018
20         TAPE RESTRT                                INPUT019
21         C                                           INPUT020
22         CALL RTAPE                                 INPUT021
23         C                                           INPUT022
24         IF(CHANGE.LT.1.E-6) GO TO 200                INPUT023
25         100 CONTINUE                                INPUT024
26         READ(5,SPEC5)                                INPUT025
27         IF(RESTRT.GT.1.E-6) GO TO 200                INPUT026
28         READ(5,GEN)                                 INPUT027
29         200 CONTINUE                                INPUT028
30         ICYCMX=CYCMAX                            INPUT029
31         RETURN                                     INPUT030
32         END                                     INPUT031

```

```

INPUT001
INPUT002
INPUT003
INPUT004
INPUT005
INPUT006
INPUT007
INPUT008
INPUT009
INPUT010
INPUT011
INPUT012
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INPUT015
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INPUT018
INPUT019
INPUT020
INPUT021
INPUT022
INPUT023
INPUT024
INPUT025
INPUT026
INPUT027
INPUT028
INPUT029
INPUT030
INPUT031
INPUT032

```

```

1      .MAIN
2      INCLUDE BLANK,LIST
3      COMMON /PARCELS/ II,JJ,KK,F1,F2,F3,F4,F5,F6,F7,F8,I,J,K
4
5      C
6      CALL INPUT
7
8      IFIRESTNT.GT.0.01 GO TO 10
9
10     C
11     CALL DEFINE
12     C*INITIALIZE ICYCL,SAVE
13     ICYCL=0
14     SAVE=.FALSE.
15     IFITDUMP .GT. U.O .OR. IDUMP .GT. 0) SAVE=.TRUE.
16     C
17     C*OBTAIN INITIAL PARTICLE POSITIONS
18     C
19     CALL SETUP
20
21     Coooooooooooooooooooooooooooooooooooooooooooooooooooooooooooo
22     10 ICYCL=ICYCL+1
23     TXI=TICKER(IV)
24
25     C
26     C*SWARN CHECK
27     C
28     IF(SAVE) CALL SJWARN(20,1,$300)
29
30     C
31     C*OBTAIN WINDS,DIFFUSIVITIES,AND SOURCES
32
33     C
34     C
35     TIME=TIME+DT
36
37     C
38     C*PUT DIFFUSION CONTRIBUTIONS IN SOURCE ARRAY
39     DO 20 N=1,NSP
40     CALL DIFFUSIN
41     20 CONTINUE
42
43     CoooooooooooooooooooooPAPICLE LOOPooooooooooooooINDEX NP
44     DO 30 NP=1,NPH
45
46     C
47     C*OBTAIN VOLUME AVERAGING FACTORS
48
49     C
50     CALL VOLFAC(NP)
51
52     C
53     DO 5 N=1,NSP
54     DIJM(N) = SIN(K,I,J,1)*F1*SIN(K,J,1)*F2*SIN(K,JJ,1)*F3*
55     I           SIN(K,JJ,1)*F4+S(N,KK,J,1)*F5*S(N,KK,J,1)*F6*
56     2           S(N,KK,JJ,1)*F7+S(N,KK,JJ,1)*F8
57
58     5 CONTINUE
59

```

```

54      CPSUM=0.0          MAIN0054
55      DO 8 N=1,NSP        MAIN0055
56      CPIN(NP)=CP(N,NP)+DUM(N)*DT   MAIN0056
57      IF(CPIN(NP) .LT. 0.0) CPIN(NP)=0.0  MAIN0057
58      CPSUM=CPSUM+CPIN(NP)    MAIN0C58
59      8 CONTINUE          MAIN0C59
60      C
61      C      **PHOTOCHEMICAL CONTRIBUTIONS
62      C
63      C      AVOID CHEMISTRY IF SUM OF CONCENTRATIONS IS < 0.01 PPM
64      C      IF(CPSUM .LT. 0.01) GO TO 25  MAIN0064
65      C      PREPARE CP ARRAY FOR CHEMISTRY  MAIN0065
66      C      DO 9 N=1,NSP        MAIN0066
67      CPIN(NP)=CP(N,NP)+DUM(N)*DT   MAIN0067
68      IF(CPIN(NP) .LT. 0.0) CPIN(NP)=0.0  MAIN0C68
69      9 CONTINUE          MAIN0069
70      CALL CHM(CH(1,NP),CP(2,NP),CP(3,NP),CP(4,NP),CP(5,NP),DUM(1),  MAIN0G70
71      1 DUM(2),DUM(3),DUM(4),DUM(5),DT,TIME)  MAIN0071
72      C
73      C      **ADVECTION
74      C
75      25 CALL ADVECT        MAIN0075
76      30 CONTINUE          MAIN0076
77      *****END PARTICLE LOOP*****  MAIN0C77
78      C
79      C      **COMPUTE CONCENTRATIONS
80      C
81      CALL CONCEN          MAIN0081
82      C
83      C      **DETERMINE IF THIS CYCLE'S RESULTS ARE TO BE PLOTTED,
84      C      PRINTED, OR DUMPED  MAIN0083
85      C
86      PLOT=.FALSE.          MAIN0C86
87      PRINTX=.FALSE.        MAIN0C87
88      DUMP=.FALSE.         MAIN0088
89      CALL PRTYST          MAIN0C89
90      C
91      C      **SELECT OUTPUT ROUTINES
92      IF(PRINTX) CALL EDIT        MAIN0091
93      IF(PLOT) CALL OUTPUT       MAIN0092
94      IF(DUMP) CALL WTAP          MAIN0093
95      IF(.NOT. CROUND) GO TO 100  MAIN0094
96      C
97      C      **WRITE OUT GROUND LEVEL CONCENTRATIONS
98      WRITE (11) ICYCL,TIME      MAIN0095
99      DO 75 N=1,NSP        MAIN0096
100     WRITE (11) ((C(N,I,J,T),J=1,NY),I=1,NX)  MAIN0097
101     75 CONTINUE          MAIN0098
102     PRINT 1250, ICYCL        MAIN0099
103     TX2=TICKER(TV)          MAIN0100
104     TELAPS=TA2-TX1          MAIN0101
105     PRINT 1200, TIME,DT,TELAPS  MAIN0102
106     1200 FORMAT(1X,'TIME = ',F10.3,4X,'DT = ',F8.3,9X,'ELAPSED = ',F9.5)  MAIN0104
107     1250 FORMAT(1X,'CYCLE = ',14.5X,'**LEVEL 1 CONCENTRATIONS DUMPED****')  MAIN0105
108     C
109     C      **IS THIS RUN COMPLETED?

```

```

108      C
109      100 IF(ETIME .GE. TMAX .AND. TMAX .GT. 0.0) GO TO 200          MAINO1C8
110      IF((CYCL .GE. CYCMAX .AND. CYCHAX .GT. 0.0) GO TO 200          MAINO1D9
111      C
112      C      **RETURN TO MAIN LOOP FOR ANOTHER CYCLE          MAINO1E0
113      C
114      GO TO 10          MAINO1E1
115      Coooooooooooooooooooooooqooooooooooooooo          *MAINO1E5
116      Coooooooooooooooooooooooqooooooooooooooo          *MAINO1E6
117      C
118      C      **NORMAL EXIT          MAINO1E7
119      200 IF(SAVE .AND. (.NOT. DUMP)) CALL WTAPP          MAINO1E8
120      IF(.NOT. PLUT) CALL OUTPUT          MAINO1E9
121      IF(.NOT. PRINTX) CALL FDIT          MAINO1E0
122      STOP NORMAL          MAINO1E1
123      C      **$3WARN TERMINATION          MAINO1E2
124      300 CALL WTAPE          MAINO1E3
125      CALL EDIT          MAINO1E4
126      STOP $3WARN          MAINO1E5
127      C
128      C
129      END          MAINO1E6

```

OUTPUT

```

1      .OUTPUT
2          SURROUNGE OUTPUT
3          INCLUDE BLANK
4          COMMON /TFIX/ 100,T00
5          DIMENSION BIGPLT(700),XYPL(NX,NY),XZPL(NX,NZ),YZPL(NY,NZ)
6          EQUIVALENCE (XYPL(1,1),BIGPLT(1)),(XZPL(1,1),BIGPLT(1)),
7          (YZPL(1,1),BIGPLT(1))
8          C
9          C
10         IQG=ICYCL
11         T00=TIME
12         C
13         C**DETERMINE CONTOUR PLOTS DESIRED
14         C
15         DO 1000 N=1,NSP
16         NQ=N
17         C
18         C**ISP SELECTS WHICH SPECIES ARE PLOTTED
19         TAB(1)=TITLE$IN)
20         TAB(2)=6NPLUT
21         IF(IISP(N).EQ.0) GO TO 1000
22         IF(INXY.EQ.0) GO TO 100
23         C*****X-Y CONTOUR PLOTS
24         DO 50 L=1,NXY
25         C
26         DO 10 I=1,NA
27         DO 10 J=1,NY
28         LEVEL=XYPL(I,J)
29         XYPL(I,J)=CINQ(I,LEVEL,J,1)
30         10 CONTINUE
31         CALL CONTRUR(NX,NY,XYPL,O,T,O,TAB,1)
32         50 CONTINUE
33         100 IF(INXZ.EQ.0) GO TO 200
34         C*****X-Z CONTOUR PLOTS
35         DO 150 L=1,NXZ
36         C
37         DO 110 I=1,NX
38         DO 110 K=1,NZ
39         LEVEL=XZPL(I,K)
40         XZPL(I,K)=CINQ(I,K,LEVEL,1)
41         110 CONTINUE
42         CALL CONTRUR(NX,NZ,XZPL,O,T,O,TAB,1)
43         150 CONTINUE
44         200 IF(INYZ.EQ.0) GO TO 300
45         C*****Y-Z CONTOUR PLOTS
46         DO 250 L=1,NYZ
47         C
48         DO 210 J=1,NY
49         DO 210 K=1,NZ
50         LEVEL=YZPL(J,K)
51         YZPL(J,K)=CINQ(K,J,LEVEL)
52         210 CONTINUE
53         CALL CONTRUR(NY,NZ,YZPL,O,T,O,TAB,1)

```

OUTPUT01
 OUTPUT02
 OUTPUT03
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 OUTPUT53

OUTPUT

```
54      250 CONTINUE  
55      C  
56      300 CONTINUE  
57      C  
58      1000 CONTINUE  
59      C  
60      RETURN  
61      C  
62      END
```

```
OUTPUT54  
OUTPUT55  
OUTPUT56  
OUTPUT57  
OUTPUT58  
OUTPUT59  
OUTPUT60  
OUTPUT61  
OUTPUT62
```

PL

.PL

```

1 SUBROUTINE PL(NINC, Z, NX, NY, NXMX, AMIN, AMAX, LOGFL)          PL000001
2 DIMENSION LU(72), L(131), Z(NXMX,NY)                                PL000002
3 DATA LU / 'U', ' ', '1', ' ', '2', ' ', '3', ' ', '4', ' ', '5',
4   ' ', '6', ' ', '7', ' ', '8', ' ', '9', ' ', 'A', ' ', 'B', ' '
5   'C', ' ', 'D', ' ', 'E', ' ', 'F', ' ', 'G', ' ', 'H', ' ', 'I',
6   'J', ' ', 'K', ' ', 'L', ' ', 'M', ' ', 'N', ' ', 'O', ' ', 'P',
7   'R', ' ', 'Q', ' ', 'S', ' ', 'T', ' ', 'U', ' ', 'V',
8   'W', ' ', 'X', ' ', 'Y', ' ', 'Z', ' ' /
9 DATA ISTAR / 100 /, IMAX / 131 /                                 PL000003
10 JMAX = .6*NY/NX*IMAX + .5                                         PL000004
11 NC = MIN(NINC, 36)                                                 PLC00011
12 ZMIN = AMIN                                                       PLC00012
13 ZMAX = AMAX                                                       PLC00013
14 AMX = NX                                                       PL000014
15 ANY = NY                                                       PLC00015
16 IF(ABS(ZMAX-ZMIN) .GT. 1.0E-5) GO TO 20                         PLC00016
17 ZMAX = Z(1,1)                                                       PLC00017
18 ZMIN = ZMAX                                                       PL000018
19 DO 10 I = 1, NX                                                 PL000019
20 DO 10 J = 1, NY                                                 PL000020
21 ZMAX = MAX(ZMAX, Z(I,J))                                         PL000021
22 10 ZMIN = MIN(ZMIN, Z(I,J))                                       PL000022
23 IF(ABS(ZMAX-ZMIN) .LT. 1.0E-20) RETURN                           PL000023
24 20 IF (LOGFL .EQ. 0) GO TO 30                                     PL000024
25 IF (ZMIN .GT. 0.) GO TO 25                                     PL000025
26 PRINT 6J20                                                       PL000026
27 6020 FORMAT( //////////////////////////////////////////////////////////////////NON-POSITIVE VALUE IN ARRAY      OPL000027
28 1 OF CONTOURED LOGARITHMICALLY. PL IS RETURNING WITHOUT PLOTTING )PLC00028
29 RETURN                                                       PL000029
30 HZMAX = ZMAX                                                       PL000030
31 HZMIN = ZMIN                                                       PL000031
32 ZMAX = ALOG10(ZMAX)                                              PL000032
33 ZMIN = ALOG10(ZMIN)                                              PL000033
34 30 SC = (NC**2 - 1.E-5)/(ZMAX - ZMIN)                            PL000034
35 DX = AMX/IMAX                                                    PL000035
36 DY = ANY/JMAX                                                    PL000036
37 Y = ANY + DY                                                    PL000037
38 DO 80 J = JMAX, 1, -1                                           PL000038
39 Y = Y - DY                                                    PL000039
40 M = Y                                                       PL000040
41 IF (M .LE. 0) M = 1                                             PL000041
42 IF (M .GE. NY) M = NY - 1                                       PL000042
43 DM = Y - M                                                    PL000043
44 X = 0.                                                       PL000044
45 DO 70 I = 1, IMAX                                              PL000045
46 X = X + DX                                                    PL000046
47 IF (I*J .EQ. 1 .OR. I*J .EQ. IMAX*JMAX) GO TO 60               PL000047
48 IF (I .EQ. 1 .AND. J .EQ. JMAX .OR. J .EQ. 1 .AND.
49 I .EQ. IMAX) GO TO 60                                         PL000048
50 N = X                                                       PL000049
51 IF (N .LE. 0) N = 1                                             PL000050
52 IF (N .GE. NX) N = NX - 1                                       PL000051
53 DN = X - N                                                    PL000052
54

```

PL

```
54      IF (LOGFL .NE. 0) GO TO 40          PL000054
55      C = DM*(DM*Z(N+1,M+1) + (L - DM)*Z(N+1,M)) + (L - DM)*
56      I (DM*Z(N,M+1) + (L - DM)*Z(N,M))
57      GO TO 50
58      40 C = DM*(DM*ALOG10(Z(N+1,M+1)) + (L - DM)*ALOG10(Z(N+1,M)) +
59      I (L - DM)*ALOG10(Z(N,M+1)) + (L - DM)*ALOG10(Z(N,M)))
60      50 IND = I + SC*(C - ZHIN)
61      IF (IND .LE. 0) IND = 1
62      IF (IND .GT. 2*NC) IND=2*NC
63      L(1) = L0(IND)
64      GO TO 70
65      60 L(1) = 1STAR
66      70 CONTINUE
67      80 PRINT 6080, (L(I),I=1,IMAX)        PL000067
68      6080 FORMAT (1X, 13(1I))
69      IF (LOGFL .EQ. 0) GO TO 90
70      ZMAX = HZMAX
71      ZMIN = HZMIN
72      90 PRINT 6090, ZMIN, ZMAX
73      6090 FORMAT (1'DMINIMUM VALUE = ', 1PE9.3, 5X, 'MAXIMUM VALUE = ', E9.) PLC00073
74      C
75      RETURN
76      END
```

PRTTST

```
1      .PRTTST
2          SUBROUTINE PRTTST
3          INCLUDE BLANK
4
5          C      **THIS SUBROUTINE CONTROLS PRINTER EDITS, PLOTS, AND TAPE DUMPS
6          C
7          C      ****PLOTS
8          IF(IPLOT .EQ. 0) GO TO 30
9          IF(MOD(ICYCL,IPLOT) .GT. 0) GO TO 30
10         PLOT=.TRUE.
11         30 IF(ITFLOT .LT. 1.0E-8) GO TO 50
12         DUM(5)=TIM0+TPLOT
13         IF(ITIME .LT. DUM(5)) GO TO 50
14         TIM0=DUM(5)
15         PLOT=.TRUE.
16         C      ****PRINTER EDITS
17         50 IF(IPRINT .EQ. 0) GO TO 60
18         IF(MOD(ICYCL,IPRINT) .GT. 0) GO TO 60
19         PRINTX=.TRUE.
20         60 IF(ITPRINT .LT. 1.0E-8) GO TO 80
21         DUM(6)=TIMN+TPRINT
22         IF(ITIME .LT. DUM(6)) GO TO 80
23         TIMN=DUM(6)
24         PRINTX=.TRUE.
25         C      ****TAPE DUMPS
26         80 IF(ICUMP .EQ. 0) GO TO 90
27         IF(MOD(ICYCL,1DUMP) .GT. 0) GO TO 90
28         DUMP=.TRUE.
29         90 IF(TDUMP .LT. 1.0E-8) GO TO 100
30         DUM(7)=TIMN+TDUMP
31         IF(ITIMF .LT. DUM(7)) GO TO 100
32         TIMN=DUM(7)
33         DUMP=.TRUE.
34         C      *ALWAYS PLOT CYCLE ONE, AND DUMP IF DUMPS HAVE BEEN REQUESTED
35         100 IF(ICYCL .NE. 1) GO TO 150
36         PLOT=.TRUE.
37         PRINTX=.TRUE.
38         IF(ISAVE) DUMP=.TRUE.
39
40         C
41         150 RETURN
        END
```

PRTTST01
PRTTST02
PRTTST03
PRTTST04
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PRTTST40
PRTTST41

RTAPE

```

      .RTAPE
      SURROUNGE RTAPE
      INCLUDE BLANK
      C
      C   ::SAVE RESTARTING DATA
      SAVE1=PLSTART
      SAVE2=TMAX
      SAVE3=CYCHAA
      ISAVE1=ISTART
      C
      WRITE(6,1000) ISTART
      25 READ (12) ICYCL,TIME,NCOMM
      WRITE(6,1011) ICYCL,TIME
      IF(ICYCL .NE. ISTART) GO TO 100
      READ (12)
      GO TO 25
      C
      C   ::READ BLANK COMMON
      100 READ(12) (DUM(I)), I=1,NCOMM
      C
      C   ::RESTORE RESTARTING DATA
      RESTRT=SAVE1
      TMAX=SAVE2
      CYCHAA=SAVE3
      ISTART=ISAVE1
      C
      C   ::GET SETUP TAPE SPACED CORRECTLY FOR RESTART
      27
      TTEST=2160G.
      C
      SPACE PAST INITIAL CONCENTRATIONS
      READ (10) DUMM
      C
      125 READ (10) DTT,DUMM,DUMM,DUMM,DUMM,DUMM
      READ (10) DUMM
      TTEST=TTEST+DTT
      CHECK=AUS(TTEST-TIME)
      IF(CHECK .LT. 1.0E-8) GO TO 140
      GO TO 125
      140 PRINT 1700,TTEST
      C
      C
      C   ::GET GROUND LEVEL CONCENTRATION FILE SPACED CORRECTLY
      43
      C
      45   IF(.NOT. GROUND) GO TO 200
      . 150 READ (11) TTEST,TTEST
      DO 160 N=1,NSP
      READ (11)
      160 CONTINUE
      IF(TTEST .NE. ISTART) GO TO 190
      GO TO 150
      190 PRINT 1600
      C

```

RTAPE001
RTAPE002
RTAPE003
RTAPE004
RTAPE005
RTAPE006
RTAPE007
RTAPE008
RTAPE009
RTAPE010
RTAPE011
RTAPE012
RTAPE013
RTAPE014
RTAPE015
RTAPE016
RTAPE017
RTAPE018
RTAPE019
RTAPE020
RTAPE021
RTAPE022
RTAPE023
RTAPE024
RTAPE025
RTAPE026
RTAPEC27
RTAPE028
RTAPE029
RTAPE030
RTAPE031
RTAPE032
RTAPE033
RTAPE034
RTAPE035
RTAPE036
RTAPE037
RTAPE038
RTAPE039
RTAPE040
RTAPE041
RTAPE042
RTAPE043
RTAPE044
RTAPE045
RTAPE046
RTAPE047
RTAPE048
RTAPE049
RTAPL050
RTAPE051
RTAPE052
RTAPE053

RTAPE

```
54      200 RETURN
55      C
56      C    ::FORMATS
57      C
58      1000 FORMAT(1H1,///,43H ::*****TAPE RESTART REQUESTED FOR CYCLE ,15
59      I   2X,1UH***** ,///)
60      1010 FORMAT(1X, 6HCYCLE ,15,2X,14HFOUND. TIME = ,1PF14.6)
61      1700 FORMAT(1X,'SETUP TAPE SPACED FOR RESTART. TTEST = ',F10.3)
62      1600 FORMAT(1X,'GROUND LEVEL CONC FILE SPACED FOR RESTART')
63      END
```

```
RTAPE054
RTAPE055
RTAPE056
RTAPE057
RTAPE058
RTAPE059
RTAPE060
RTAPE061
RTAPE062
RTAPE063
```

SETUP

```

1      .SETUP
2      SUBROUTINE SETUP
3      INCLUDE BLANK
4      COMMON /PARCEL/ II,JJ,KK,F1,F2,F3,F4,F5,F6,F7,F8,I,J,K
5      DIMENSION CC(5,NZ),NYI,NXII
6      EQUIVALENCE (C,CC)
7      C      *INITIALIZE CONCENTRATIONS
8      CALL S3ZERO(C,NUM)
9      C
10     9 NP=0
11     C
12     READ (10) (((CC(L,K,J,II),L=1,3),K=1,NZ),J=1,NY),I=1,NX
13     C
14     DO 10 I=1,NZ
15     DO 10 J=1,NY
16     DO 10 K=1,NX
17     C15,K,J,II)=CC(3,K,J,II)
18     C13,K,J,II)=NP
19     10 CONTINUE
20     WRITE (11) ICYCL,TIME
21     DO 22 N=1,NSP
22     WRITE (11) ((CIN,I,J,II),J=1,NY),I=1,NX
23     22 CONTINUE
24     C
25     PRINT 1250, ICYCL
26     1250 FORMAT(1X,'CYCLE = ',14.4X,'*LEVEL 1 CONCENTRATIONS DUMPED**')
27     C
28     C      LOOP OVER CELLS
29     C
30     DO 50 KP=1,NZ
31     DO 50 IP=1,NX
32     DO 50 JP=1,NY
33     NPCC=NP
34     NPCC=NP
35     DO 40 L=1,NPCC
36     IFIL = EJ* 2 + AND( KP ,GT, 2) GO TO 40
37     NP=NP+1
38     X(NP)=IP
39     Y(IP)=JP
40     Z(IP)=KP
41     C      *COMPUTE VOLUME FACTORS
42     CALL VOLFAC(NP)
43     C      *COMPUTE INITIAL PARCEL CONCENTRATIONS
44     DO 30 NN=1,NSP
45     C
46     CP(NN,NP)= C(INN,K,J,II)*F1+C(NN,K,J,II)*F2+C(INN,K,JJ,II)*F3
47     1           + C(INN,K,J,II)*F4+C(NN,KK,J,II)*F5+C(NN,KK,J,II)*F6
48     2           + C(INN,KK,JJ,II)*F7+C(INN,KK,JJ,II)*F8
49     30 CONTINUE
50     40 CONTINUE
51     IF (NP.GT.MAX) RETURN 0
52     50 CONTINUE
53     NP=NP

```

```

SETUP001
SETUP002
SETUP003
SETUP004
SETUP005
SETUP006
SETUP007
SETUP008
SETUP009
SETUP010
SETUP011
SETUP012
SETUP013
SETUP014
SETUP015
SETUP016
SETUP017
SETUP018
SETUP019
SETUP020
SETUP021
SETUP022
SETUP023
SETUP024
SETUP025
SETUP026
SETUP027
SETUP028
SETUP029
SETUP030
SETUP031
SETUP032
SETUP033
SETUP034
SETUP035
SETUP036
SETUP037
SETUP038
SETUP039
SETUP040
SETUP041
SETUP042
SETUP043
SETUP044
SETUP045
SETUP046
SETUP047
SETUP048
SETUP049
SETUP050
SETUP051
SETUP052
SETUP053

```

SETUP

```
54      PRINT 151, NPM
55      151 FORMAT(1X,'*****NUMBER OF PARTICLES =',I6)
56      C
57      CALL EDIT
58      C
59      RETURN
60      C
61      C  **FORMATS
62      C
63      C
64      C  **FORMATS
65      C
66      1000 FORMAT()
67      1100 FORMAT(1X,'USER: REPLY YES TO ENTER INITIAL CONCENTRATIONS  ')
68      1110 FORMAT(1X,'USER: ENTER I,J,K    ')
69      1120 FORMAT(1X,'USER: ENTER C(+,K,J,I) VALUES   ')
70      1105 FORMAT(A6)
71      END
```

```
SETUP054
SETUP055
SETUP056
SETUP057
SETUP058
SETUP059
SETUP060
SETUP061
SETUP062
SETUP063
SETUP064
SETUP065
SETUP066
SETUP067
SETUP068
SETUP069
SETUP070
SETUP071
```

VOLFAC

```

1      *VOLFAC
2      SUBROUTINE VOLFAC(N)
3      INCLUDE BLANK
4      COMMON /PARCEL/ II,JJ,KK,F1,F2,F3,F4,F5,F6,F7,F8,I,J,K
5
6      I=X(N)
7      J=Y(N)
8      K=Z(N)
9      II=I+
10     JJ=J+
11     KK=K+
12     FX=X(N)-I
13     FY=Y(N)-J
14     FZ=Z(N)-K
15     FX=I.-FXI
16     FY=J.-FYI
17     FZ=K.-FZI
18     F1=FX*FY*FZ
19     F2=FXI*FY*FZ
20     F3=FXI*FYI*FZ
21     F4=FX*FYI*FZ
22     F5=FXI*FY*FZI
23     F6=FXI*FYI*FZI
24     F7=FXI*FYI*FZI
25     F8=FX*FYI*FZI
26     IF(II.EQ.NAP1) II=1
27     IF(JJ.EQ.NYP1) JJ=1
28     IF(II .EQ. 0) I=NX
29     IF(J .EQ. 0) J=NY
30     IF(K .NE. 0) GO TO 50
31     F5=F5+F1
32     F6=F6+F2
33     F7=F7+F3
34     F8=F8+F4
35     F1=0.0
36     F2=0.0
37     F3=0.0
38     F4=0.0
39     GO TO 100
40     SO IF(K .NE. NZP1) GO TO 100
41     F1=F1+F5
42     F2=F2+F6
43     F3=F3+F7
44     F4=F4+F8
45     F5=0.0
46     F6=0.0
47     F7=0.0
48     F8=0.0
49
50     C
      100 RETURN
      END

```

VOLFAC01
 VOLFAC02
 VOLFAC03
 VOLFAC04
 VOLFAC05
 VOLFAC06
 VOLFAC07
 VOLFAC08
 VOLFAC09
 VOLFAC10
 VOLFAC11
 VOLFAC12
 VOLFAC13
 VOLFAC14
 VOLFAC15
 VOLFAC16
 VOLFAC17
 VOLFAC18
 VOLFAC19
 VOLFAC20
 VOLFAC21
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 VOLFAC35
 VOLFAC36
 VOLFAC37
 VOLFAC38
 VOLFAC39
 VOLFAC40
 VOLFAC41
 VOLFAC42
 VOLFAC43
 VOLFAC44
 VOLFAC45
 VOLFAC46
 VOLFAC47
 VOLFAC48
 VOLFAC49
 VOLFAC50

```

1      *WTAPE
2      SUBROUTINE WTAPE
3      INCLUDE BLANK
4      C
5      MTAPE=12
6      WRITE(MTAPE) ICYCL,TIME,NCOMM
7      WRITE(MTAPE) (UUM(I),I=1,NCOMM)
8      C
9      RETURN
10     C
11     1000 FORMAT(1X,      '*****CYCLE = ',15.2X,'TIME = ',1PE14.6,2A,
12     1           'DUMPED ON TAPE*****')
13     END

```

```

      WTAPE001
      WTAPE002
      WTAPE003
      WTAPE004
      WTAPE005
      WTAPE006
      WTAPE007
      WTAPEC08
      WTAPE009
      WTAPE010
      WTAPE011
      WTAPE012
      WTAPE013

```

```

1      *RTAPE
2      SUBROUTINE *RTAPE
3      INCLUDE BLANK
4      C
5      HTAPE=12
6      WRITE(HTAPE) (CYCL,TIME,NCOMM)
7      WRITE(HTAPE) (DUM(I),I=1,NCOMM)
8      WRITE(6,1000) (CYCL,TIME)
9      C
10     RETURN
11     C
12     1000 FORMAT(1X,      '*****CYCLE = ',15.2X,'TIME = ',1PE14.6,2X,
13           'DUMPED ON TAPE*****')

```

*TAPE001
 *TAPE002
 *TAPE003
 *TAPE004
 *TAPE005
 *TAPE006
 *TAPE007
 *TAPEC08
 *TAPE009
 *TAPE010
 *TAPE011
 *TAPE012
 *TAPE013

4. A SAMPLE TEST CALCULATION

In this section a test calculation is presented, including copies of the computer print output.

The calculation considered is the advection of a Gaussian distribution, previously considered in Reference 1, page 32.

4.1 CODE CHANGES

Some modifications to the NEXUS/L code used in the Los Angeles photochemistry simulation and documented in the report were made. In particular,

(a) the structure of blank common was reorganized to permit a grid 50 x-cells by 30 y-cells. Thus, the procedure BLANK was modified so that NXI=50, NYI=30, NZI=1, NSPI=1, MAX=9000.

(b) a change to subroutine SETUP was made to properly initialize the concentrations to the desired distribution,

$$c(x,y) = 71.1 \exp\{-[(x-9)^2 + (y-9)^2]/12.5\}$$

Here, $\sigma_x = \sigma_y = 2.5$ km. Also, as before, the concentration at the center of cell <9,9> is set to 69.0.

(c) subroutine SETUP was further changed to permit the initial positions of some of the Lagrangian particles to be away from the cell center. For the fair Lagrangian parcels per cell case documented here, the initial positions for cell I,J are

$$(i) \quad x = I - 0.3$$

$$y = J + 0.3$$

$$(ii) \quad x = I + 0.3$$

$$y = J - 0.3$$

$$(iii) \quad x = I - 0.3$$

$$y = J - 0.3$$

$$(iv) \quad x = I - 0.3$$

$$y = J + 0.3$$

Figure 4 displays the Fortran coding of subroutine SETUP used.

4.2 INPUT TO GENERATE TEST CALCULATION

The problem configuration was maintained exactly as the previous Gaussian advection reported in Reference 1.

- (1) The cells are 1 km cubes, (DX=DY=DZ=1000 m).
- (2) There are 50 x-direction cells, 30 y-direction cells. There is only one level (NX=50, NY=30, NZ=1).
- (3) The u-velocity is everywhere 10 m/sec, the v-velocity is everywhere 5 m/sec, creating an off-axis net wind direction. (UFIX=10, VFIX=5, WFIX=0)
- (4) The initial Gaussian distribution is set to zero in all cells more than eight cells from the center of the distribution.

```

-- 00101 -- 10      SUBROUTINE SETUP
 00103 20      INCLUDE BLANK
 00111 20      END
 00112 30      COMMON /PARCEL/ IT, JJ, KK, F1, F2, F3, F4, F5, F6, F7, F8, I, J, K
 00117 40      C
 00118 50      C      READ INITIAL DATA FROM SETUP TAPE
-- 00119 -- 60      C
 00119 70      DD 10 I=1,NX
 00120 80      DD 10 J=1,NY
 00121 90      DD 10 K=1,NZ
 00124 100      C11,K,J,I=0,0
 00125 110      10 CONTINUE
-- 00131 -- 120      DD 14 I=1,1?
 00134 130      DD 14 J=1,1?
 00137 140      C(I,J,I) = 71.1*EXP(-(I-I)+(J-J)+(K-K)+0.08)
 00140 150      14 CONTINUE
 00143 160      C(I,J,K) = 69.0
 00144 170      NP=0
-- 00149 -- 180      C
 00149 190      C      L700 OVIP CELLS
 00149 200      C
 00151 210      DD 50 I=1,NX
 00150 220      DD 50 J=1,NY
 00153 230      DD 50 K=1,NZ
-- 00156 -- 240      NPCCNPS
 00157 250      DD 40 L=1,NPCC
 00152 260      NO=NAP+1
 00163 270      IFIL, JF, 31, M, IP, 11
 00165 280      DO 10 (I1,I2,J1,J2)=L
 00166 290      11 XNP1=I1-0,1
 00167 300      YNP1=J1-0,1
-- 00170 -- 310      ZNP1=K1-0,1
-- 00171 -- 320      GO TO 20
 00172 330      12 XNP1=I1-0,3
 00173 340      YNP1=J1-0,3
 00174 350      ZNP1=K1-0,3
-- 00175 -- 360      GO TO 20
 00176 370      13 XNP1=I1-0,3
 00177 380      YNP1=J1-0,3
 00200 390      ZNP1=K1-0,3
 00201 400      15 XNP1=I1-0,3
 00202 410      YNP1=J1-0,3
 00203 420      ZNP1=K1-0,3
 00204 430
 00205 440
 00206 450      20 CALL VOLFACT(P)
 00206 460      C      COMPUTE INITIAL PARCEL CONCENTRATIONS
 00207 470      DD 30 NV=1,NS
-- 00208 -- 480      C
 00212 490      C(INN,N)=C(INN,K,J,I)+F1+C(INN,K,J,I,I)+F2+C(INN,K,J,I,I,I)+F3
 00212 -- 500      1      * C(INN,K,J,J,I)+F4+C(INN,KK,J,I)+F5+C(INN,KK,J,I,I)+F6
 00212 510      2      * C(INN,KK,J,I,I)+F7+C(INN,KK,J,I,I,I)+F8
-- 00213 -- 520      30 CONTINUE
 00215 530      40 CONTINUE
-- 00217 -- 540      IF (NO,GT,MAX) RETURN 0
 00221 550      50 CONTINUE
 00225 560      NO=4-N0
 00226 570      PRINT 151, NV
 00231 580      151 FORMAT(1X,*,*,*,NUMBER OF PARTICLES =*,16)
 00232 590      RETURN
 00233 600      END
-- END OF COMPILETIME:      NO DIAGNOSTICS.

```

INITIAL
CONCENTRATIONS
IN GAUSS
DIST^N

CHANGES TO
INITIAL POSITION
OF PARCELS

Figure 4. Subroutine SETUP version used for Gaussian advection test problem.

- (5) The time step is 400 sec/cycle (DT=400).
- (6) There is no diffusion, only advection (EXFIX=0, EZFIX=0).

The namelist input used to generate this test calculation is shown in Figure 5.

4.3 CYCLE 1 OUTPUT

Figure 6 displays the printer output, cell-by-cell, of the problem configuration resulting at the end of Cycle 1. Figure 7 presents a contour plot representation of the same data.

REFERENCE

Sklarew, R.C., et.al., "A Particle-In-Cell Method for Numerical Solution of the Atmospheric Diffusion Equation, And Application to Air Pollution Problems," Report No. 3SR-844 (November, 1971), Systems, Science and Software, La Jolla, Calif.

TEST CASE PROBLEMS

```

***  

*START* = .00000000E+00  

*P* = .00  

*Q* = .00000000E+00  

*R* = .10000000E+00  

*T* = .00000000E+00  

*P* = .00  

*Q* = .00  

*R* = .00000000E+00  

*T* = .00000000E+00  

*U* = .00000000E+00  

*V* = .00000000E+00  

*W* = .00000000E+00  

*X* = .00000000E+00  

*Y* = .00000000E+00  

*Z* = .00000000E+00  

*P* = .00  

*Q* = .00000000E+00  

*T* = .00000000E+00  

*U* = .00000000E+00  

*V* = .00000000E+00  

*W* = .00000000E+00  

*X* = .00000000E+00  

*Y* = .00000000E+00  

*Z* = .00000000E+00  

*P* = .00  

*Q* = .00000000E+00  

*T* = .00000000E+00  

*U* = .00000000E+00  

*V* = .00000000E+00  

*W* = .00000000E+00  

*X* = .00000000E+00  

*Y* = .00000000E+00  

*Z* = .00000000E+00  

***  

*TEST* = .00000000E+00  

*P* = .00000000E+00  

*Q* = .00000000E+00  

*R* = .00000000E+00  

*T* = .00000000E+00  


```

NAMELIST "START"

NAMELIST
"SPEC'S"NAMELIST
"GEN"

Figure 5. Namelist input to generate test calculation.

555-R-14-1756

THE P.M. ALL CONCESSIONS = 2771.551

Figure 6. Concentrations in Eulerian cells at end of cycle 1.

Figure 7. Printer contour representation of concentrations at end of cycle 1.

SSSS-R-7.4-1756