

SmartWay Fuel Efficiency Test Protocol for Medium and Heavy Duty Vehicles

Working Draft

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Transportation and Regional Programs Division
Office of Transportation and Air Quality
U.S. Environmental Protection Agency

NOTICE

This technical report does not necessarily represent final EPA decisions or positions. It is intended to present technical analysis of issues using data that are currently available. The purpose in the release of such reports is to facilitate the exchange of technical information and to inform the public of technical developments.



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1. Foreword

Advancements in heavy duty vehicle technology offer the potential for significant improvements in important vehicle attributes, including efficiency and emissions performance. In 2004, the U.S. Environmental Protection Agency (EPA) initiated the SmartWaySM Transport Partnership to accelerate the deployment of fuel-efficient, clean technologies for heavy duty vehicles. SmartWay Transport is an innovative collaboration between EPA and the transportation industry to improve energy efficiency, reduce greenhouse gas and air pollutant emissions, and improve energy security. Through SmartWay, EPA works in collaboration with industry and other stakeholders to provide incentives for adopting cleaner, more fuel efficient transportation technologies to benefit the environment.

An important aspect of the SmartWay Transport Partnership is to determine through testing and analysis the environmental benefits of heavy truck technologies, and to provide this information to SmartWay partners and to the general public. SmartWay is developing this fuel efficiency test protocol for heavy duty trucks to better quantify the benefits of various heavy vehicle designs and technologies. EPA currently offers a “SmartWay designation” for over-the-road tractor-trailer combination trucks. It is a design-based specification, developed on this basis of test results for individual components (tires, wheels, aerodynamic equipment, auxiliary power units, engines) that have been demonstrated to improve fuel efficiency and reduce emissions. EPA, its SmartWay partners, and others would like to expand the SmartWay designation for heavy duty vehicles by moving toward a performance-based specification. A performance-based specification would be technology-neutral, and able to quantify a broad range of heavy vehicle configurations and applications, and to measure technical innovations as they emerge.

Moving toward a performance-based specification requires using a test to measure vehicle fuel efficiency. Component testing alone is not sufficient, since the fuel-saving impacts can vary widely based upon vehicle application. However, a standardized, objective, stand-alone fuel efficiency test to measure the fuel efficiency of a heavy duty on-highway vehicle does not currently exist. This absence presents a significant challenge to SmartWay, the Agency and industry. Without a test method, it is difficult to develop a common understanding of how to assess and compare the fuel efficiency of heavy duty vehicles, including vehicles with hybrid powertrain, varying aerodynamic configurations, and other advanced vehicle designs. EPA recognizes that there is a wide variety of truck configurations for each base model and that it may not be possible to test every configuration to see if it meets the SmartWay performance specification. As a result, EPA is looking at methods to extend fuel efficiency testing to cover additional truck configurations. Tools such as the consistent use of vehicle modeling, tire rolling resistance testing, and aerodynamic evaluations could potentially broaden a fuel efficiency testing program.

This test procedure applies to medium and heavy duty vehicles as per 40 CFR §86.082-2. This means any motor vehicle rated at more than 8,500 pounds GVWR or that has a

vehicle curb weight of more than 6,000 pounds or that has a basic vehicle frontal area in excess of 45 square feet. Vehicles in this group are typically tractor-trailer combination trucks, single unit commercial trucks, heavy duty vocational trucks, and buses used in inter-city transit applications. EPA does have an optional chassis certification procedure for heavy duty diesel vehicles under 14,000 pounds GVWR, used in federal regulatory programs (§86.1863-07). This test procedure incorporates many aspects of the optional chassis test procedure, but does not replace it for the purposes of certifying to the standards specified in §86.1816-08.

Heavy duty vehicle manufacturers are required to use engines that are certified to U.S. Environmental Protection Agency (EPA) emission standards (per 40 CFR Part 86, Subpart N) but those test procedures measure engine (rather than vehicle) brake specific fuel consumption performance and focus on emissions rather than fuel efficiency. The existing tests do not quantify fuel efficiency benefits from the unique features of a hybrid drive train (regenerative braking, reductions in engine transient operation, smaller engines) or fuel efficient vehicle components (single wide base tires, aerodynamic equipment.) This test procedure will serve as an objective means to evaluate these and other emerging fuel-saving technologies, and to standardize the measurement of heavy duty vehicle fuel efficiency.

This test procedure is intended to be used on a voluntary basis to determine whether vehicle configurations meet or exceed SmartWay performance specifications. Other users may also wish to apply it for their own purposes. For example, the test procedure can be used to calibrate and verify vehicle software models, allowing for greater consistency among models.

This protocol references various SAE standards, federal regulations, and other source documents. Those documents should be acquired in order to conduct tests in accordance with this protocol.

This “working draft” document contains a number of “reserved” sections. It is presented for stakeholder review in order to assist EPA in resolving certain outstanding technical issues contained in the “reserved” sections and elsewhere. We encourage stakeholders and other interested parties to comment on this document and provide EPA with advice on the technical issues.

2. Purpose and Scope

The purpose of this document is to provide a standardized, objective, consistent test procedure to measure the fuel consumption of heavy duty vehicles used in on-road operation. As mentioned in the Foreword, this test procedure is being developed to support the aims of the EPA SmartWay Transport Partnership, and to fill a real need in the trucking industry. SmartWay Transport is an innovative collaboration between EPA and the transportation industry to improve energy efficiency, reduce greenhouse gas and air pollutant emissions, and improve energy security. An important aspect of the

Partnership is to determine through testing and analysis the environmental benefits of heavy truck technologies, and to provide this information to SmartWay partners and to the general public. SmartWay is developing this fuel efficiency test procedure for heavy duty trucks to better quantify the benefits of various heavy vehicle designs and technologies. This test procedure provides test requirements and methods that are appropriate for a number of different truck types, based on the specific application or service category of the heavy duty vehicle.

This test protocol fills a real need, since there is no widely-accepted, standardized test procedure to measure the real-world fuel consumption performance of a heavy duty vehicle. SAE J1321 (or alternatively, SAE J1526) has been used to partially fill this gap, but these test methods do not measure absolute vehicle fuel efficiency, but an improvement in fuel efficiency from a baseline condition.¹ This is not useful as a stand-alone metric, since the baseline condition is not standardized. More importantly, drive cycles are not standardized.

The test protocol described in this document measures fuel consumption directly, and the desired fuel consumption metric for this test procedure is fuel consumed per unit of work performed (e.g., gallons per mile or per ton-mile; for vocational trucks with power take-off, gallons per hour). Alternatively, the metric can be work performed per volume of fuel consumed (e.g., miles or ton-miles per gallon). A fuel consumption rather than a percent improvement metric allows for a stand-alone efficiency measure for any given truck model. It also provides a consistent, objective, standardized means to compare the fuel efficiency of two or more tested trucks.

The test procedure described here is intended to provide the federal government, states, industry, academia, and others with an objective testing method to assess the fuel efficiency performance of heavy duty vehicles for a variety of purposes. These purposes may include quantifying and benchmarking in-use fuel consumption; verifying fuel savings for federal and state incentives; demonstrating environmental performance to achieve targets for innovative industry, federal and state programs; and, providing quantification of carbon dioxide reductions.

A major challenge to our collective understanding of heavy truck fuel efficiency is the lack of standardized, comparative test data. This test procedure could be used to test several trucks at the same facility, under stable test conditions. The results could be used to establish “environmental reference” vehicles, against which other heavy duty vehicles could be tested in the future. Using this test procedure to establish environmental reference trucks can provide a flexible, cost-effective means to build comparable data sets and improve our ability to analyze and understand heavy truck performance.

This test procedure establishes uniform test conditions for the most common types of heavy duty highway vehicles and applications. Uniform test conditions include:

- vehicle selection
- fuel specification
- test facilities and environment

- test equipment
- drive cycle
- accessory load
- test set-up procedures

The specificity makes the test procedure effective for benchmarking a specific vehicle design, and for comparing fuel-saving vehicle designs within a given application.

The protocol establishes different test requirements and methods depending on vehicle type, based on a classification according to service category, or vehicle application. These categories cover many common types of heavy duty vehicle uses, including tractor-trailer combination line haul and regional haul trucks, local pick up and delivery vehicles, transit buses, neighborhood refuse haulers, utility trucks, and intermodal drayage trucks. This document can be updated at appropriate times to supplement the initial heavy duty vehicle categories with additional heavy duty vehicle drive cycles.

The test procedure is designed to be technology-neutral and applicable to a conventional internal combustion engine or a hybrid powertrain configuration.² However, this test procedure does not provide test or data analysis methods to adequately account for the energy usage of a charge-depleting (“plug-in”) hybrid vehicle. This protocol should only be used to test such vehicles in the charge-sustaining mode.

This test procedure protocol does not provide any test methods or data analysis methods for non-liquid fuels.

This test procedure incorporates references to a number of different resources, including various SAE practices, federal regulations, and other source materials. These materials are referenced for the convenience of the user. It is advisable to acquire the referenced materials prior to conducting this test, to facilitate implementation of this protocol.

The vehicles covered by this test procedure are heavy duty vehicles, as defined by 40 CFR §86.082-2 and §86.090-2, which consist of any motor vehicle rated at more than 8,500 pounds GVWR or that has a vehicle curb weight of more than 6,000 pounds or that has a basic vehicle frontal area in excess of 45 square feet. Vehicles in this group are typically tractor-trailer combination trucks, commercial straight trucks, heavy duty vocational trucks, and buses used in municipal transit applications.

The initial focus in this document will be on heavy duty vehicle applications with the greatest near-term potential to benefit from fuel-saving technology:³

- Highway line haul combination tractor-trailer
- Regional haul combination tractor-trailer
- Local pick up and delivery truck (e.g., parcel, beverage)
- Neighborhood refuse truck
- Utility service truck
- Transit bus

- Intermodal drayage truck

The heavy duty vehicle categories listed in this test protocol overlap but don't fall perfectly within existing intended service categories for heavy duty diesel engines, as defined in the federal emissions certification program. According to 40 CFR §86.090-2, the intended service category for a heavy duty engine is the primary service application group for which a heavy duty diesel engine is designed and marketed, as determined by the manufacturer. The determination is based on factors such as vehicle GVWR, vehicle usage and operating patterns, vehicle design, engine horsepower, and engine design and operating characteristics.

3. Overview of Test Methods

The fuel consumption of the test vehicle is measured by operating the vehicle on either a test track or on a chassis dynamometer over a specified drive cycle and measuring the fuel consumption. Fuel consumption can be calculated on the basis of a mass balance of carbon-bearing emission gases (CO₂, CO, CH₄, other hydrocarbons) as described in 40 CFR Part 86 and SAE test method J1094a⁴ or on the basis of a gravimetric fuel measurement system using portable fuel tanks as described in SAE test method J1321, in which the mass of fuel consumed is converted to volume using measurements of fuel density.

Track tests can be conducted using either the gravimetric method or the carbon mass-balance method using a portable emissions monitoring system, or PEMS.

Chassis dynamometer tests are conducted using the carbon-balance method and laboratory gas analysis instrumentation (preferable) or the gravimetric method.

This test procedure does not address the comparability of track testing to chassis dynamometer testing. More data is needed to develop robust correlation factors. Preliminary testing indicates a dynamometer-to-track difference in the range of 4% to 10%. This difference may be explained by tire/surface interactions and test-to-test variability. However, both track and chassis dynamometer tests demonstrated directionally consistent and statistically equivalent differences to changes in drive cycle for various vehicles.⁵ EPA encourages comments regarding possible methods for correlating results of track tests and dynamometer tests. Comments received to date suggest a preference for laboratory dynamometer testing, but EPA would like to retain a standardized track test method in this document, if only to provide a means to relate the results of dynamometer testing to more realistic on-road performance.

Figure xx shows the steps in the overall conduct of the testing, for whichever path has been chosen.

The following overview is designed to help the user determine which test method is more appropriate for their needs.

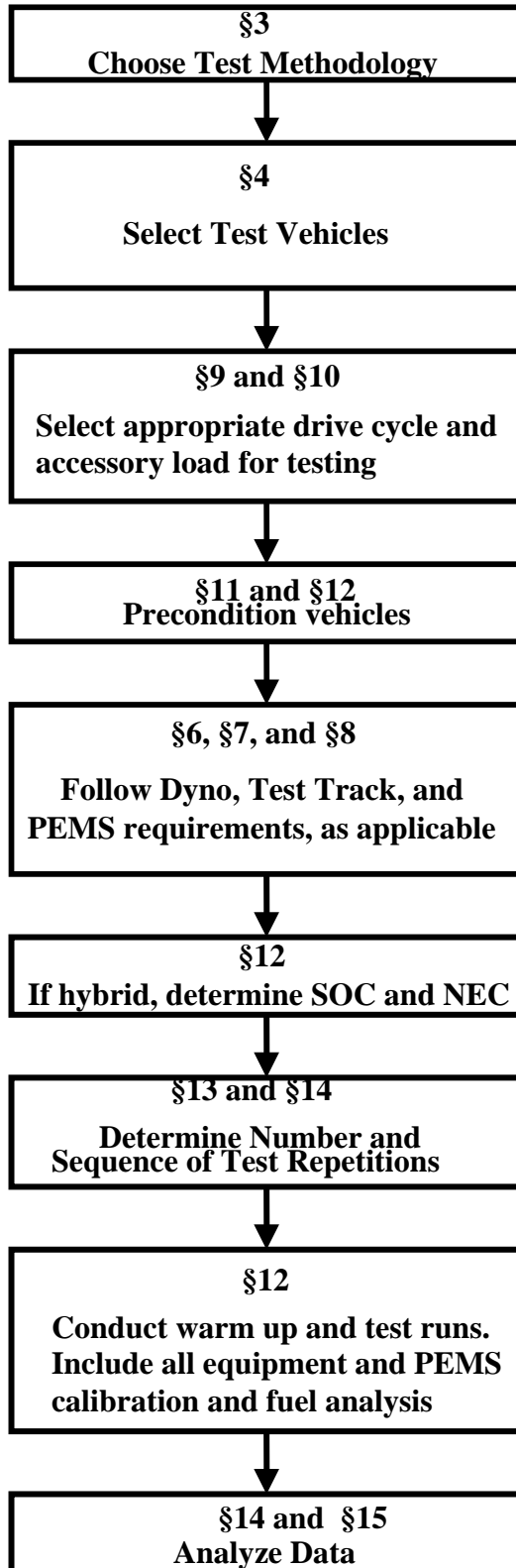
3.1 Track Test

A track test is a vehicle test conducted on an outside test track. Test tracks may be found at vehicle proving grounds or other facilities specifically designed for vehicle or tire performance testing. Although any type of heavy duty vehicle can be tested on a test track, this option may be more suited to typical over-the-road heavy duty vehicles, like combination tractor-trailers.⁶

Because the test involves the vehicle being operated on a road surface in a manner similar to that of on-road driving, rolling resistance, aerodynamic drag, and inertial road load power requirements are incorporated in the test measurement, and do not have to be determined beforehand with a coastdown test and calculations. Although the result of a track test reflects real-world vehicle performance better than a chassis dynamometer test, by directly evaluating the impacts of road effects such as aerodynamic drag of tractors and trailers and rolling resistance effects of tires, variability of ambient conditions may result in greater variability of test results.⁷ This protocol includes specification of ambient conditions as well as specifications for measurement of fuel consumption.

Additionally, a coastdown test should be performed to document the road load force the vehicle experiences during the track test. See section 13.4 for details.

Figure 1. Protocol Sequence



Detailed methodology for the gravimetric method of measuring fuel consumption is described in §§5.7.1 and 5.7.3 of the joint TMC/SAE Fuel Consumption Test Procedure – Type II, Surface Vehicle Recommended Practice J1321 (SAE J1321). Fuel consumption is measured by weighing the fuel consumed using a portable fuel tank. In this method, a portable fuel tank is weighed empty, filled with fuel, weighed again, and then mounted on the test vehicle. The test vehicle’s fuel line is connected to the portable tank the moment the test begins, and disconnected at the conclusion of the drive cycle, after which the portable tank is removed and reweighed. The fuel consumed during the test is calculated using the density of the fuel and the difference in the weight of the portable fuel tank before and after the test, to yield the volume (gallons) of fuel used.

The carbon balance method of measuring fuel consumption on the basis of SAE test method 1094a (and in accordance with CFR 40 Part 86) uses an onboard portable emissions monitoring system (PEMS) to measure the mass of carbon emitted in the exhaust, as well as the exhaust flow. The PEMS records this information via an onboard data acquisitions system.

Details for PEMS requirements can be found in 40 CFR Part 1065, Subpart J. Because PEMS became commercially available only recently, the portable tank gravimetric method has been more extensively used for track tests in the past.

3.2 Chassis Dynamometer Test

A chassis dynamometer test is a test conducted indoors on a hydrokinetic chassis dynamometer. The chassis dynamometer option in this test procedure incorporates many of the methods and requirements established in the federal light duty vehicle and ‘light’ heavy duty vehicle emissions certification chassis test procedure. Although most heavy duty vehicles can be tested on a chassis dynamometer, this option may be more suitable for single unit truck and truck body heavy duty vehicles.⁸

Chassis dynamometers may be found at vehicle test laboratories; typically, facilities used for emissions and vehicle fuel efficiency testing. Because the test is conducted on a chassis dynamometer, rolling resistance, aerodynamic drag and inertial road load power requirements must be determined ahead of time, with coastdown tests and calculations to determine the proper horsepower absorption setting for the chassis dynamometer. Details for conducting coastdown tests are found in the section of this test procedure covering the chassis dynamometer test method.

When using the chassis dynamometer option in this test procedure, fuel consumption can be measured using the carbon balance method, in which fuel consumption can be calculated on the basis of a mass balance of carbon-bearing emission gases (CO₂, CO, CH₄, other hydrocarbons) as described in SAE test method J1094a. In this method, vehicle emissions are collected and analyzed using laboratory gas analyzer equipment. The laboratory equipment measures and records the concentration of carbon-based compounds emitted in the exhaust as well as the exhaust flow. The concentrations and densities of the carbon-based compounds, and exhaust flow values, are used to calculate the mass of fuel consumed. The volume of fuel consumed is determined by the mass of

fuel consumed and the density of the fuel. This method of measuring heavy duty vehicle fuel consumption on a chassis dynamometer is substantially similar to the method used to measure fuel efficiency for passenger vehicles.

Detailed procedures for conducting chassis dynamometer testing are provided in the optional complete vehicle federal emissions certification method for light heavy duty vehicles, applicable to heavy duty vehicles with a GVWR of 8,500 to 14,000 pounds. The chassis emissions test procedure is detailed in 40 CFR §86.1816-05, 40 CFR §86.1816-08, and 40 CFR §86.1863-07. For heavy duty vehicles up to 14,000 pounds, the heavy duty fuel efficiency test procedure described in this document follows the provisions outlined in 40 CFR part §86.1863. The provisions outlined in 40 CFR part §86.1863 dealing with evaporative emission testing, on-board diagnostic (OBD) requirements, smoke emission requirements, and requirements for measuring criteria pollutants do not apply. Although, at the user's discretion, these additional components can be included in a fuel efficiency test.

For test vehicles exceeding 14,000 lbs GVWR, there is no pre-existing federal chassis dynamometer test procedure. For these vehicles, the test procedure described in this document uses many of the precedents established in 40 CFR Part 86, with the exception of the requirement for a higher capacity chassis dynamometer. This procedure provides new chassis dynamometer requirements to accommodate larger vehicle testing. In all cases, the following guidelines should be followed:

- Dynamometer coefficients that simulate road-load forces shall be determined as specified in SAE J2263 and J2264.
- Dynamometer power absorption and inertia simulation shall be set as specified in 40 CFR Part 86-1229-85.
- Test instrumentation equipment (including where appropriate, exhaust emissions sampling and analytical systems) as referenced in 40 CFR Part 86.1301-90 to 40 CFR 86.1326-90 and/or 40 CFR Part 1065 shall be calibrated in a manner that is NIST-traceable.

4. Vehicle Selection

Vehicles shall be representative of production fleet vehicles. The test vehicle must be appropriate for its service category. It should have the same vehicle “package,” that is, body style, equipment, number of axles, gross vehicle weight rating (GVWR), and accessories, that enable the complete vehicle to accomplish the type of service (performance, utility, durability, etc.) for its intended application. Equipment specifications that can affect fuel efficiency (engine size and type, tire size and type, transmission size and type, brakes, gear shift points, rear axle ratio, air suspension, lubricant type, idle RPM, ignition timing, wheel alignment, etc.) must be representative of how that vehicle is driven on the road, and used to perform work.

Test vehicles need not be new, but they must be in good mechanical order and operating condition, with no obvious mechanical or physical defects that might affect fuel efficiency. If new, the vehicle should be broken in per the manufacturer's recommended procedures, at a minimum. Refer to the requirements for mechanical and operating condition described in SAE J1321 §8.7.⁹ All components and equipment shall be calibrated and maintained to within manufacturer-recommended specifications. The exception is any component that has been deliberately modified as part of the test truck design.

To ensure proper vehicle operability, it is recommended that the engine and emission control equipment meet the emissions performance certification for the given model year.

If a heavy duty vehicle is typically used in combination with a trailer or truck body, the test will produce a more comprehensive fuel efficiency result if the vehicle is tested in combination with a trailer or truck body. In certain instances, testing with a trailer or truck body is necessary; for example, in track testing, to provide the proper payload required, or when testing the impact of aerodynamic design elements for use in a tractor-trailer combination vehicle.

If a heavy duty vehicle is tested with a truck body or trailer, then the truck body or trailer shall be appropriate for that vehicle's intended service. It is recommended to use a trailer or truck body that is representative in design, function, weight, and dimension, of the type of trailer or truck body typical for that application. An exception is if modifications to a trailer or truck body are part of the vehicle design being tested. Whenever a trailer or truck body is tested with a heavy duty vehicle, the same trailer or truck body must remain paired with the test vehicle throughout the duration of the testing program.

Unless otherwise indicated, the following trailer specifications are recommended for a typical highway line haul tractor-trailer combination:

- dry van box trailer
- 2 trailer axles
- 53' long, 102" wide, 13'6" high
- minimized trailer gap (maximum of 45" depending upon kingpin setting)
- 11,000 to 14,000 pounds

Truck body specifications shall be appropriate to each intended application.

When selecting a test vehicle, if the purpose is to compare its performance to other vehicles in that application, then the vehicles selected shall be closely matched in class, model year, body style, equipment, fuel type, accessories, mileage, and condition, with the exception of any vehicle design options being tested.¹⁰

5. Test Fuel

For vehicles with compression-ignition engines certified on diesel fuel, the test fuel shall be number 2 distillate ultra-low sulfur diesel fuel (ULSD). The test fuel will meet fuel

specifications outlined in 40 CFR §80.520 for ULSD #2D distillate. The exception is if fuel type is a design option being tested.

Specific fuel parameters include:

- Sulfur content. 15 parts per million (ppm) maximum
- Cetane index and aromatic content. Minimum cetane index of 40 or maximum aromatic content of 35 volume percent.
- Flash/Fire point. 52° C minimum
- Water/Sediment. 0.05% volume maximum
- Particulate Contaminant. 10 mg/L maximum
- Viscosity KIN/CS at 40°C. 1.9 to 4.1

For vehicles with any Otto-cycle engine certified on gasoline, natural gas, propane, or other fuels, the test fuel shall meet the fuel specifications outlined in 40 CFR §86.1313-94, sections c through f.

A supply of test fuel sufficient to complete the test must be procured and fuel parameters including fuel density analyzed prior to the start of the test. If fuel consumption is to be measured by the gravimetric method, the following additional test shall be made:

- ASTM Test Method D-1298, Standard Test Method for Density, Relative Density (Specific Gravity), or API Gravity of Crude Petroleum and Liquid Petroleum Products by Hydrometer.

The test fuel must be sequestered once it is procured and analyzed. If it is necessary to add additional fuel to the test fuel supply during the course of the test, another fuel analysis must be conducted to ensure the test fuel still meets the required fuel parameters. For each test segment, a record must be kept of the fuel parameters of the test fuel, including density.

6. Test Track Specifications and Requirements

If the option for on-road testing is chosen, the testing shall be conducted on a test track, not on a public highway, to provide greater control of test conditions. This section describes the general specifications and conditions for the test track.

6.1 Track Specifications

Setting specifications for the test track can minimize the effect of a track's physical attributes on vehicle performance. The following are specification requirements for a test track that will give good, repeatable results, while still allowing for a reasonable number of track facilities to be used to conduct this test:

- **Shape.** Oval (recommended), figure eight, or serpentine to minimize the effects of yaw angle wind effects and lateral forces. Circular tracks are not permitted.
- **Neutral steering speed.** The radii of the curves in conjunction with the banking grade (superelevation) shall be selected to permit a minimum of 40 mph around the curves. This can require a superelevation of 2% for curves with a 10,000 foot radius or more. For curves with a radius of less than 10,000 feet, the super elevation must be consistent with applicable state and federal DOT roadway

requirements. A minimum neutral steering speed is needed to prevent the test vehicle from losing forward motion to lateral forces when negotiating a curve “hands off.”

- **Length.** A minimum of 1.5 miles, with 5 miles or more recommended. A track of this length minimizes excessive curve radii and prevents the test vehicle from losing forward motion when negotiating curves.
- **Grade.** The maximum grade change shall not exceed 2% longitudinally, to prevent the test vehicle from excessive changes in forward motion due to grade.
- **Surface.** The surface shall be concrete or asphalt, to minimize energy absorption effects of uneven or rough pavement. It is recommended that the friction and surface characteristics comply with federal and state DOT specifications regarding road condition.
- **Altitude.** The track shall be at an elevation no higher than 4,000 feet above sea level, to minimize changes to air density that may alter the vehicle’s forward motion, and to prevent unintended changes in engine and subsystem operation.
- **Maintenance.** The test track shall be well-maintained, inspected at least once a year, and resurfaced as needed to maintain surface integrity and consistency.

6.2 Track Requirements

The track shall have the capacity to measure and record test conditions, in order to ensure that a test is conducted in accordance with the provisions of this test procedure. The following are the minimum requirements needed to conduct a track test:

- **Weather Monitoring.** The track shall be equipped with the capacity to monitor ambient conditions (wind direction and velocity, temperature, humidity, barometric pressure) during each test. It is recommended that the weather sensing equipment is located on the test track, or at a weather station within 50 miles of the test track. Options for on-site weather monitoring equipment include: an anemometer or a marine-type hand held wind indicator to monitor wind direction and velocity¹¹; a thermometer to measure temperature; a barometer to measure barometric pressure; and a hygrometer to measure humidity. The positioning, etc., of ambient condition sensors shall be consistent with provisions outlined in the *Federal Standard for Siting Meteorological Sensors at Airports, FCM-S4-1987*. The track shall have the capacity to record this weather information, as part of the test record.
- **Truck Weight Scales.** The track shall be equipped with properly calibrated truck weight scales (or located within 50 miles of the test track) that conform to the most current provisions established by the National Institute of Standards and Technology (NIST). As of the writing of this test procedure, these provisions are those published in the NIST Handbook 44 – 2007 Edition, *Specifications, Tolerances, and Other Technical Requirements for Weighing and Measuring Devices*. The truck scales must be calibrated annually at a minimum. It is recommended that the truck scales have a National Type Evaluation Program (NTEP) Certificate of Conformance.
- **Portable Scales.** If the portable fuel tank gravimetric method is used, the track shall be equipped with properly calibrated portable scales that conform to provisions established in SAE J1321 §5.7.1 and §8.4. Scales should have a

- resolution of 0.1% of the expected fuel mass consumed, or better. Portable scales must be calibrated annually at a minimum. Portable scale function should be verified with a check weight prior to the weighing operation.
- **Portable Emissions Monitoring System (PEMS).** If the PEMS carbon balance method is used, the operators conducting the test shall have the capability to properly use and maintain a portable emissions monitoring system (PEMS), as recommended by the PEMS manufacturer, and as required by 40 CFR Part 1065. This includes providing all equipment and materials needed to properly use and maintain the PEMS. In addition to the electronic flow meter, gas analyzer, heated lines, etc., integral to the PEMS, ancillary equipment and materials include zero, calibration and span gases; gas pressure and flow regulators and gauges; data loggers; all connectors and hoses. The PEMS and all PEMS-related equipment and supplies shall be calibrated and maintained as recommended by the PEMS manufacturer, and as required by 40 CFR Part 1065 Subpart D. Additional requirements governing the use of PEMS are detailed in Section §8 of this test procedure.
 - **Speed and Distance Equipment.** The test vehicle must be equipped with a means to measure speed and distance. A global position sensor (GPS) is recommended, as an adjunct to vehicle electronic control module (ECM) data and/or speedometer and odometer readings. The accuracy of the odometer and speedometer must be verified and corrections made if necessary. This can be accomplished using a stop watch and the track lane length at the specified speed. Reference SAE J1321 §8.12. The track must be equipped with markers that can be positioned to match target speed and distance parameters of the selected drive cycle, including gear shift and braking points. Using a global position sensor (GPS) is recommended, as an adjunct to ECM data and/or speedometer and odometer readings.

6.3 Track Environmental Requirements

A track test is not intended to replicate the tightly-controlled environment of a laboratory test, since a key attribute of track testing is the ability to more closely simulate in-use operation. Nor would such tight controls be feasible on a track test. However, setting appropriate parameters for ambient conditions can improve the repeatability and reproducibility of track test results. The following limits allow for reasonable variation in the ambient conditions under which track tests can occur:

- **Temperature.** Testing shall occur when the ambient temperature is between 68°F to 86°F (20°C to 30°C). If the ambient temperature changes by more than 20°F over the course of the testing, all testing will be repeated. The temperature in the fuel tank cannot exceed 160°F. Reference SAE J1321 §5.7.3.¹² When using the PEMS method, a test run shall be invalidated if an ambient temperature warning on the PEMS occurs during the test.
- **Humidity.** Testing can be conducted at any humidity level; however, an optimal range is between 35% and 75% relative humidity; 40% is ideal.
- **Wind.** Testing shall occur when wind speeds are at 12 mph or less, with wind gusts no greater than 15 mph.

- **Precipitation.** Testing shall occur during conditions of no visible precipitation and no moisture on the test track surface, which would contact the tires. No visible precipitation is defined as precipitation of 0.1 mm (per hour??) or less. Testing shall occur only when the track is dry, and there is no precipitation or fog.

Information about environmental conditions during a test shall be available during or after the test, to determine the test's validity, and records shall be kept as part of the test documentation.

7. Chassis Dynamometer Specifications and Requirements

Detailed procedures to conduct chassis dynamometer testing are provided in 40 CFR Part 86, Subpart B. If one opts to test to §86.1863, Subpart B can be used. If a test vehicle exceeds 14,000 pounds GVWR, then a higher capacity chassis dynamometer may need to be used. Recommended specifications for a higher capacity chassis dynamometer are listed below.

7.1 Chassis Dynamometer Specifications

The chassis dynamometer specifications for testing heavy duty vehicles with a GVWR of less than 14,000 pounds but more than 8,500 pounds shall be similar to the requirements found in 40 CFR Part 86, Subpart B for the testing of light duty cars and trucks. Section §86.108-00 of the CFR includes provisions for both small twin roll (8.65-inch diameter) and large, single-roll (48-inch) dynamometers. A large, single-roll electric dynamometer is preferable, unless a vehicle is more suited for testing on a twin roll dynamometer (e.g., if disengaging one of the axles on a twin-screw drive axle would create a safety or operational problem). If a twin roll hydrokinetic dynamometer is used, the results must be correlated to that of a single roll electric chassis dynamometer.¹³ For vehicles with a GVWR greater than 14,000 pounds, the heavy duty chassis dynamometer used to test the vehicle shall have a sufficient capacity to test the vehicle at its rated test weight for the application.

If the tested vehicle exceeds 14,000 pounds GVWR, the testing organization shall refer to the following recommended specifications.

HEAVY DUTY VEHICLE CHASSIS DYNAMOMETER SPECIFICATIONS

GENERAL FACILITY INFORMATION	
GVWR capability	> 14,000 lbs
Rear Axle Weight Capability	5,000 to 44,000 lbs
Speed Range	0 to 65 mph
Power absorption	0 to 500 hp
Power motoring	0 to 500 hp
Tractive Force	3000 lbs-f
Roll Diameter	24 to 72 in
Lab Environment Temperature Range	68°F to 86°F
Combustion air temperature	No

control? (y/n)

Combustion air humidity No

control? (y/n)

MOTOR AND POWER CONTROL

Motor Type DC or AC motors (approx range
500 hp)

Manual or automated drive cycle Automated

Nominal power (standard) 400 hp

Nominal power (maximum) 500 hp

Drive Torque (standard) 5000 lb-ft

Drive Torque (maximum) 8000 lb-ft

ACCELERATION MEASUREMENT

Acceleration, maximum 5 to 15 ft/sec²

Deceleration, maximum 5 to 15 ft/sec²

EMISSIONS CAPABILITY

Acceptable types Bag method, or continuous raw
spl.

NOx Not required

PM Not required

HC FID

CO NDIR or FTIR

CO₂ NDIR or FTIR

Fuel flow Carbon balance

Fuel type capability Diesel, CNG, gasoline,
propane

7.2 Chassis Dynamometer Requirements

A requirement for either type of chassis dynamometer (single or twin roll) is that it shall permit the user to convert coastdown data for the test vehicle to the proper horsepower absorption setting for the chassis dynamometer. A coastdown test must be conducted and the results converted to dynamometer settings using published SAE procedures.^{14 15}

Coastdown data shall be taken with the vehicle at full test weight to determine the proper dynamometer settings. Additional details on how to conduct a vehicle coastdown test and convert the results to the proper horsepower absorption setting in chassis dynamometer tests is found in Section §12 of this document.

Either type of chassis dynamometer (single or twin roll) shall be equipped with a cooling fan to provide cooling air flow to the vehicle during testing. Refer to 40 CFR Part 86.107-96 (d) for vehicle cooling fan requirements. A road-speed modulating fan shall be used, rather than a fixed-speed cooling fan.

Refer to 40 CFR Part 86.108-79 and 86.108-00 for chassis dynamometer equipment specifications. Refer to 40 CFR 86.118-00 and 40 CFR 86.118-78 and 40 CFR Part 86.116-90 through 86.116-94 for chassis dynamometer calibration requirements.

Additional details covering the chassis dynamometer test procedure are found in Section §12 of this document.

7.3 Chassis Dynamometer Environmental Requirements

Testing conditions are consistent with the requirements established in 40 CFR Part 86 for federal vehicle emissions testing using chassis dynamometers. These include:

- **Temperature.** Ambient temperature levels shall not be less than 20 degrees C (68 degrees F) nor more than 30 degrees C (86 degrees F). Reference 40 CFR Part 86.
- **Humidity.** Testing can be conducted at any humidity level; however, an optimal range is between 35% and 75% relative humidity; 40% is ideal.
- **Fuel Temperature.** Fuel temperatures of the test vehicle shall be controlled, as specified in 40 CFR Part 86.107-96 (d).

8. Test Equipment Specifications

Fuel consumption is measured by three possible methods: A carbon-balance based on emissions measured in a laboratory test cell, a carbon balance based on emissions measured by a Portable Emissions Monitoring System (PEMS), or using the gravimetric method, in which the mass of fuel consumed during the test is directly measured. The laboratory test cell is suitable only for use in a chassis dynamometer test, whereas the PEMS or gravimetric measurements would be best suited for track tests.

8.1 Laboratory Emissions Monitoring System

This test procedure adopts the requirements for laboratory exhaust gas sampling and analysis systems established in the federal emissions certification program for Otto and Diesel cycle engines used in heavy duty vehicles, described in 40 CFR Part 1065. For equipment and specifications not covered by that citation, 40 CFR Part 86, Subpart N will apply (specifically §86.1301-90 through §86.1326-90). For this procedure, the provisions dealing with evaporative emission testing, the OBD requirements, the smoke emission requirements, and requirements for measuring particulate matter and NO_x do not apply. However, at the user's discretion, these additional components can be included in a fuel efficiency test.

Alternatively for determination of fuel efficiency by carbon balance (e.g., by measurement of gas flow and CO₂ concentration), it is acceptable to use a field sampling type "raw" exhaust gas sampling and analysis system, rather than the dilution tunnel system specified in 40 CFR Part 1065, Subpart B and 40 CFR Part 86, Subpart N. However, it is important to ensure that intake air flow measurements are done in such a way as to simulate the trucks in-use air intake system. If direct measurement of mass fuel

consumption is chosen in lieu of dilute exhaust CO₂ measurement, the fuel measurement device shall be accurate to within 2 percent of actual mass fuel flow.

Additional equipment specifications and calibration and maintenance requirements for laboratory exhaust gas sampling and analysis systems are referenced in 40 CFR Parts 86.314 through 86.317; 40 CFR Parts 86.319 through 86.322; and, 40 CFR Parts 86.328 through 86.331.

8.2 Portable Emissions Monitoring Measurement System

General provisions for field testing using PEMS can be found in 40 CFR Part 1065, Subparts C, D and J.

If the PEMS/carbon balance method is used, the following conditions must be met:

- The PEMS must use the same measurement technologies and meet the same audit criteria as laboratory instrumentation under 40 CFR Part 1065 Subpart D, as applicable.
- The carbon balance method must be conducted to comply with EPA's regulations as outlined in 40 CFR Part 600, and 40 CFR part 86 subpart N.
- Carbon balance fuel efficiency must be calculated using the method outlined in SAE Standard J1094a.¹⁶
- The exhaust routing must meet the requirements specified in 40 CFR Part 1065 to keep crankcase ventilation gas (blowby gas) in the exhaust stream.

Specifications for the PEMS flow meter, analyzer, and data logging requirements are as follow:

[Reserved]

8.3 Gravimetric Fuel Consumption Measurement System

General provisions for field testing using portable fuel tanks and the gravimetric consumption measurement system can be found in SAE J1321 §5.7.1, §5.7.3, and §8.4. A portable overhead hoist can be employed to move the portable tank and position it on the scale and on the test vehicle. It is recommended to mount a frame to the test vehicle to secure the portable tank, and to install self-sealing quick connects and check valves with supply fittings and check valves mounted directly to the fuel tank. Fuel hoses leading to and from the tank should be primed beforehand to prevent errors due to filling the volume of the hoses and also to prevent air entrainment. Quick-connects will facilitate the rapid installation and removal of the portable fuel tank. The tank should be positioned on the vehicle to minimize any impact to the vehicle's aerodynamics during coast down testing and track testing. The portable fuel tank for the test vehicle shall be fueled from the same dispenser during the entire test to ensure consistent fuel grade and quality. See Sections §5 and §11.8 of this documents for details on fuel and fuel analysis requirements.

Consistent with SAE J1321, after conducting pre-test vehicle and equipment check-ups and the required warm-up, the portable fuel tank is topped off and weighed. The weight should be checked a minimum of two times to ensure accuracy. It is recommended that the portable tank is stabilized before and during weighing to avoid weight fluctuations due to fuel sloshing. After weighing, the fill cap is secured, and the weight recorded. Fuel from the portable fuel tank is used only during the drive cycle. It is not used during pre-test checks or warm up laps, and it is not used to move the vehicle to the test starting point, or from the test finish point.

After the portable tank is filled and weighed, it is moved from the filling and weighing area to the test vehicle. A portable hoist is recommended. The portable fuel tank is mounted on the test vehicle and the fuel line connected to the test vehicle using hoses and fittings designed for this purpose. The portable tank fuel connections must permit the test vehicle driver or an in-vehicle assistant to instantaneously switch the vehicle's fuel supply from the permanent fuel tanks to the portable fuel tank, and vice-versa. The configuration should also prevent any backflow into the measurement tank after that tank is switched off-line.

After completing all the necessary pre-test requirements, the test vehicle is moved to the marked starting point and parked, with engines stopped. The moment the test begins, the test vehicle's fuel supply is switched to the portable tank, and disconnected from the portable tank the moment the test ends. The test vehicle is returned to the filling and weighing area, and the portable tank is disconnected, recapped, removed and reweighed. The difference in the weight of fuel consumed during the test is calculated and the density of the fuel (measured during the fuel analysis) is used to determine the volume (gallons) of fuel used. Sections §14 and §16.2 of this document provide details for the fuel efficiency calculation using the gravimetric method, and a sample calculation.

9. Drive Cycle Selection

9.1 Drive Cycle Selection Criteria

Fuel efficiency is known to be strongly related to the duty cycle (also known as the “drive cycle”) of a vehicle. In turn, the duty cycles of heavy-duty vehicles vary greatly by application. Thus, the test protocol requires separate duty cycles for each vehicle application. Included here are descriptions of possible drive cycles the following applications:

- Tractor-trailer combination line haul and regional haul truck;
- Local pick up and delivery vehicle;
- Transit bus;
- Neighborhood refuse truck;
- Utility truck; and

Intermodal (port) drayage truck.

This document will be updated with additional heavy duty vehicle types and corresponding drive cycles as they are developed.

Heavy duty vehicles have widely varying payload and accessory power requirements, depending upon the intended application. This test procedure includes specific payload and accessory load power requirements in the drive cycle sections for each of the heavy duty vehicle applications included in this document. It also extends the test weight basis/test equivalent test weight tables found in 40 CFR Part 86.

The drive cycles are designed to be used on either a test track or a chassis dynamometer. They were developed to simulate “real world” operations. The following sections describe the different drive cycles and corresponding vehicle applications.

Speed-time points for these drive cycles along with summaries of cycle statistics will appear in an updated version of the appendices.

9.2 Highway Line Haul

The highway line haul cycle simulates a combination tractor-trailer commercial freight delivery truck, operating in interstate, predominantly highway, operation. This type of vehicle operation is characterized by long trip lengths, higher average speeds, more steady-state type engine operation, and overnight rest stops, which in some instances involve long-duration idling.¹⁷ The vehicles are powered by heavy duty engines typically used in class 8 trucks (33,001 pounds GVWR or greater). Typically, the tractor has a sleeper cab with 3 axles; it is attached to a tandem axle trailer. Depending upon the type of freight carried, the trailer can be a dry van box, reefer, tanker, car carrier, livestock van, flat bed, or other. A dry van box semi-trailer is recommended for this test, except when testing for applications that require a specific trailer type.

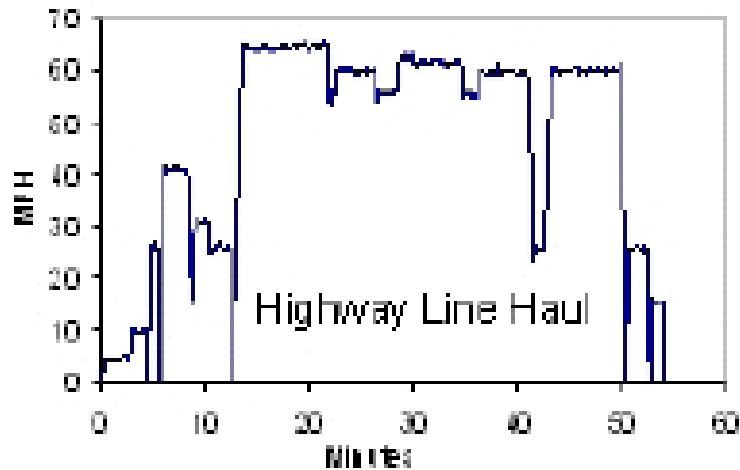
This document describes two options for a highway line haul drive cycle. Both are modifications of the Cruise mode of the California Air Resources Board (ARB) Heavy-Heavy Duty Diesel Truck (HHDDT) emissions test, a four-mode test to represent heavy truck operation, developed using data from 171 instrumented heavy duty trucks.¹⁸ Although the ARB test includes an idle, creep, transient, and cruise mode, only the latter is used as the basis of the highway line haul drive cycle. This is because data to develop the ARB test was collected from a random selection of all heavy duty trucks. However, line haul trucks are a unique subset of heavy duty trucks that spend the majority of their miles at highway speed.

The first drive cycle option was developed by EPA for fuel efficiency and emissions track testing of combination tractor-trailers. In this cycle, the most significant modifications made to the Cruise module were to add in some transient and idling operation, and to reduce deceleration and acceleration rates. Deceleration and acceleration rates in the Cruise module are too severe for a class 8 combination tractor-trailer, especially when loaded to typical weights of 33,000 to 66,000 pounds.

Additionally, if tested on a chassis dynamometer, one risks damaging the dynamometer and the vehicle's brakes.¹⁹

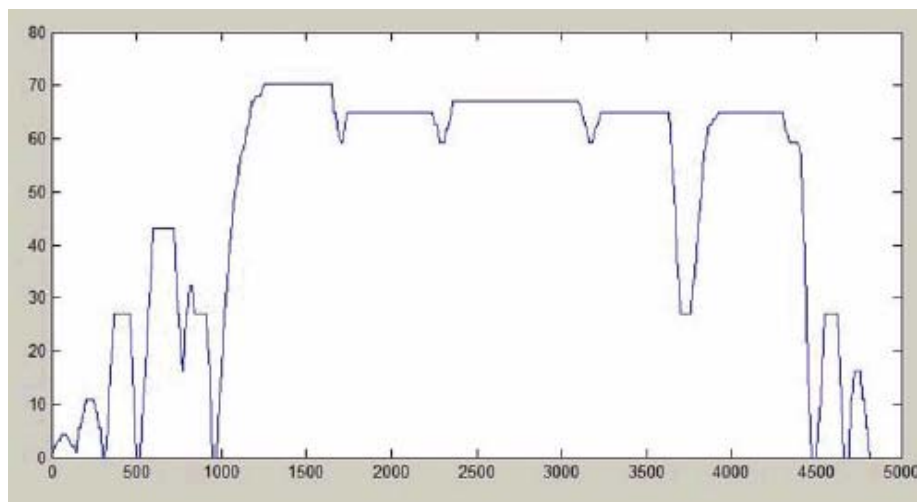
A graphic of this version of the highway line haul drive cycle is provided below in figure 2.

Figure 2



Another version of a highway line haul cycle, suitable for use only on a chassis dynamometer, was created by Southwest Research Institute, using input from a group of stakeholders, including EPA, Northeastern States for Coordinated Air Use Management (NESCAUM), several truck and engine manufacturers, state organizations, and others, for a NESCAUM heavy truck fuel efficiency modeling and simulation project. It is similar to the first option shown above, although top and average speeds are increased, there are grade impacts, there is less transient operation, and idling is handled in a separate cycle. A graphic of this version of the highway line haul drive cycle is provided below in figure 3.

Figure 3



Each of these cycles may be considered, with the potential to combine features of each into a final Highway Line Haul cycle. Data and input on payload and accessory load will also be considered, to develop these aspects of the drive cycle (discussed in Section xx).

9.3 Regional Haul

Regional haul operation is similar to highway line haul, the primary distinction being that regional haul has relatively shorter trip lengths, and includes some suburban-type operation, with lower average speeds, relatively more frequent congested driving, and no (or infrequent) overnight stays. If purchased new for this application, the tractor is typically a day cab, without sleeper accommodation.

EPA is still selecting options for this drive cycle. One promising option is to integrate segments of the Transient mode of the ARB HHDDT test into the finalized Highway Line Haul cycle (which is based upon the Cruise module of the ARB HHDDT test), to create a single drive cycle of sufficient duration and complexity.

Analysis and “filtering” of the ARB Cruise and Transient modes has been conducted by West Virginia University. This work, combined with input on the line-haul cycle, could serve as the basis for a regional haul drive cycle. EPA will begin to formalize recommendations for the regional haul cycle and include specific options in subsequent drafts of this protocol.

9.4 Local Pick Up and Delivery

The local pick up and delivery cycle simulates a package, parcel, or beverage delivery truck operating in urban-type driving, to provide local pick up and delivery service to residences and businesses. This type of truck operation is characterized by very frequent stops and starts, with limited “stem” highway driving to and from the distribution center. The vehicles are powered by heavy duty engines typically used in class 4 to 6 trucks (14,001 to 26,000 pounds GVWR), although some vehicles may be as light as class 2b or 3. The vehicle is typically a single unit truck or a chassis/truck body combination, with 2 axles.

EPA is still collecting information on local pick up and delivery candidate drive cycles. The parcel delivery working group of the Calstart-Weststart Hybrid Truck Users Forum (HTUF) instrumented a small number of parcel delivery trucks in the Florida area, and developed two parcel delivery drive cycles. One represents a class 4 residential delivery truck, and one represents a class 6 commercial delivery truck. The major differences between these two drive cycles are the rate of acceleration, average speed, number of stops, and percent of stops that are idle or engine off.

Graphics of the two parcel delivery drive cycle candidates are provided below in figures 4 and 5.

Figure 4: -- HTUF Class 4 parcel delivery cycle

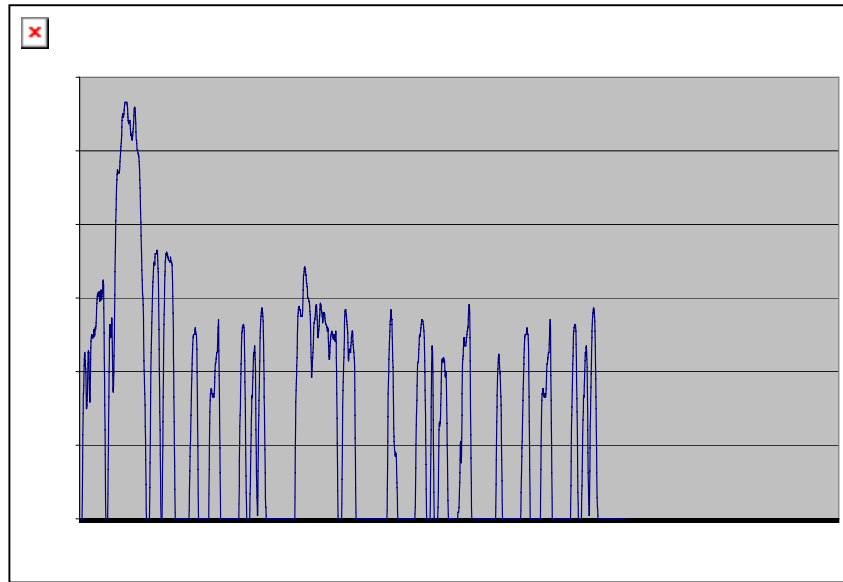
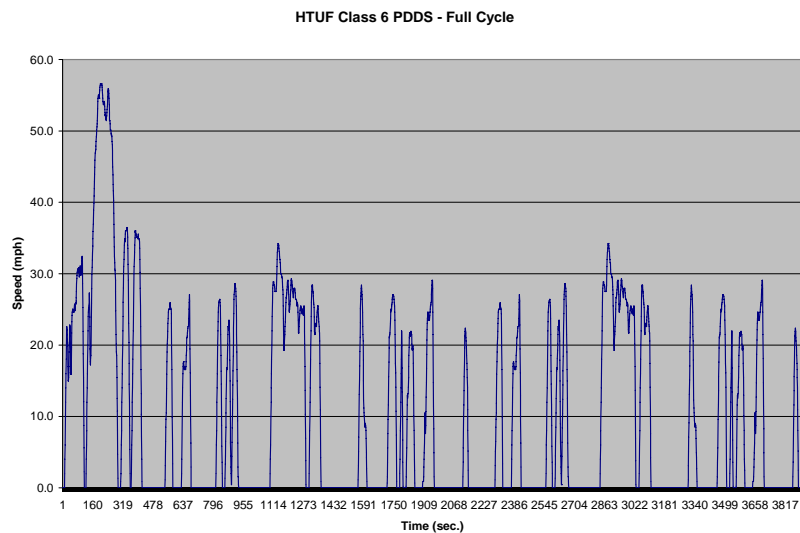


Figure 5:-- HTUF Class 6 parcel delivery cycle



EPA is also instrumenting parcel delivery trucks for its hydraulic hybrid development program. After this data is collected and analyzed, EPA can determine what changes, if any, might be made to the HTUF drive cycles, and whether we want one single cycle, or whether we could develop a formula that allows a testing organization to chose a weighted combination of more than one cycle, depending upon vehicle service characteristics. Data and information on payload and accessory load will also be considered.

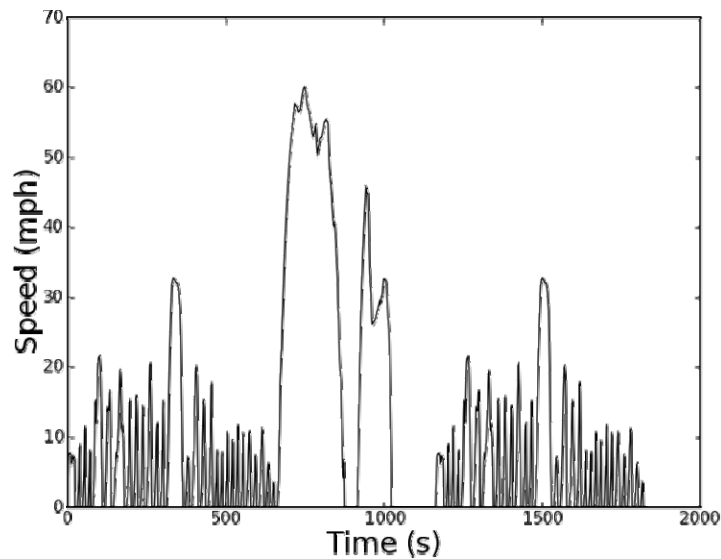
9.5 Neighborhood Refuse Truck

The neighborhood refuse truck drive cycle simulates a trash collection and compacting truck, operating in urban-type driving, to provide residential and commercial solid waste collection within a local community. The vehicle operation is characterized by very frequent stops and starts, with limited “stem” highway or suburban driving to and from the refuse drop-off site. During its operation, the engine or other power source is typically used to operate hydraulic and/or other lifting, compacting, and dumping functions. A significant amount of the fuel used by neighborhood refuse trucks is consumed by these non-motive functions. These vehicles are powered by heavy duty engines typically used in class 7 or class 8 trucks (greater than 26,001 pounds GVWR). The typical refuse haul vehicle is a chassis/truck body combination with a single axle tractor and either a single or tandem axle trash loader/ packer body.

One candidate neighborhood refuse truck drive cycle was developed by the National Renewable Energy Laboratory of Department of Energy using data collected by Ohio State University, from instrumented neighborhood refuse trucks in 5 different cities. It includes vehicle operation during collection, dumping, and driving to and from the dump and neighborhood sites.

A graphic of this candidate neighborhood refuse truck drive cycle is provided in Figure 6. Due to the complexity of this refuse hauler cycle, this cycle should be performed on a heavy duty vehicle chassis dynamometer only.

Figure 6



EPA will request stakeholder input on this drive cycle, including payload and accessory load.

9.6 Utility Service Truck

The utility service truck drive cycle simulates a public utility, cable, or telecom service truck operating in urban-type driving, to furnish electricity, gas, water, or telephone service to local businesses and residences by conducting service calls and fixing “trouble” on utility lines and junctions. Vehicle operation is characterized by periods of using the engine or other power source to operate hydraulic aerial lifts, and/or to supply electrical power to the grid and/or to operate on-board equipment. A significant amount of the fuel used by utility service trucks is consumed during these non-motive functions. The vehicles are powered by heavy duty engines typically used in class 6 or 7 trucks (19,501 to 33,000 pounds GVWR). A typical vehicle is a chassis/truck body combination with a single axle tractor and a single axle truck body equipped with outside-accessible compartments and a 30’ to 50’ hydraulic aerial lift (boom) for lifting workers and tools.

A potential utility service truck cycle is the CILCC drive cycle, a composite cycle developed by DOE/NREL, Eaton, and International Truck and Engine. These organizations developed their cycle by extensive and iterative analysis that compared several candidate drive cycles against key performance needs of hybrid electric urban delivery vehicles. Eaton and Southwest Research Institute have used this cycle in their fuel efficiency tests of hybrid utility service trucks.

Eaton and SwRI also developed hydraulic and electric test cycles to measure power demand for the aerial lift and powering the grid, which could be incorporated into this cycle, along with payload requirements.

The CILCC cycle is shown below, in figure 7.

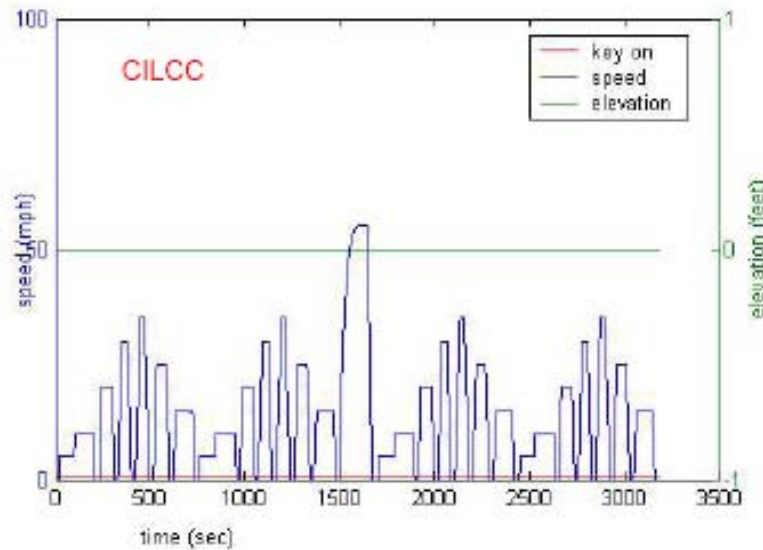


Figure 7

9.7 Transit Bus

The transit bus cycle simulates a 35' to 40' bus operating primarily in local areas, to provide frequent-stop passenger service. This vehicle operation is characterized by low average speed and regular, frequent stops, with relatively short trip lengths between stops. Vehicles typically lack facilities for long-distance operation (e.g., no onboard restrooms or large luggage compartments). However, passenger comfort and information is essential. Transit buses use the engine or other power source to power internal and external signs, interior lighting, and hydraulic lifts, and to supply heat, ventilation, and air conditioning (HVAC). A significant amount of the fuel used by transit buses is consumed by these non-motive “hotel loads.” They are powered by heavy duty engines typically used in class 7 or 8 trucks (over 26,000 pounds GVWR). A typical transit bus is a single body construction with 2 axles. It can accommodate over 15 passengers, and is equipped with 2 sets of doors.

There are significant differences between transit buses operating in suburban neighborhoods, and transit buses operating in more urban neighborhoods. In recognition of the differences, two different candidate drive cycles may be chosen for testing transit buses: the Manhattan bus cycle and Orange County bus cycle, representing urban and suburban transit service, respectively.

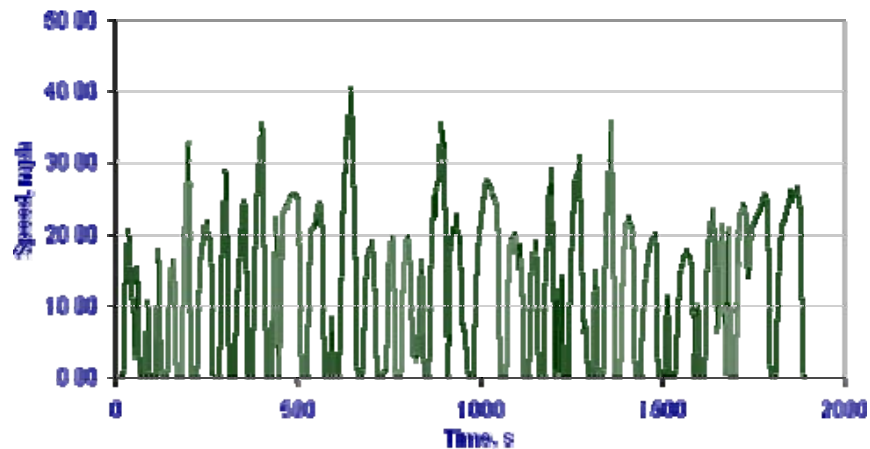
The Manhattan Bus Cycle was developed based upon the driving patterns of buses in the Manhattan core of New York City. The cycle, originally published as a transient chassis dynamometer test cycle for urban transit buses, is characterized by frequent stops and very low speed. The maximum speed is 25.4 mph; the average speed is 6.8 mph (11.0 km/h).

The Orange County Bus Cycle was developed by West Virginia University based upon the driving patterns of urban transit buses in the Los Angeles area. The cycle, originally

published as a chassis dynamometer test cycle for intermediate speed transit bus operation, has a maximum speed of 41.4 mph and an average speed of 12.5 mph.

The speed-time points for the Manhattan and the Orange County bus cycles can be found in *Recommended Practice for Measuring Fuel efficiency and Emissions of Hybrid-Electric and Conventional Heavy duty Vehicles*, SAE Surface Vehicle Recommended Practice J2711. A graphic depicting each of these cycles is found in Figures 8 and 9. Due to the complexity of these bus drive cycles, these cycles should be performed on a heavy duty vehicle chassis dynamometer only.

Figure 8: --Orange County Bus Cycle



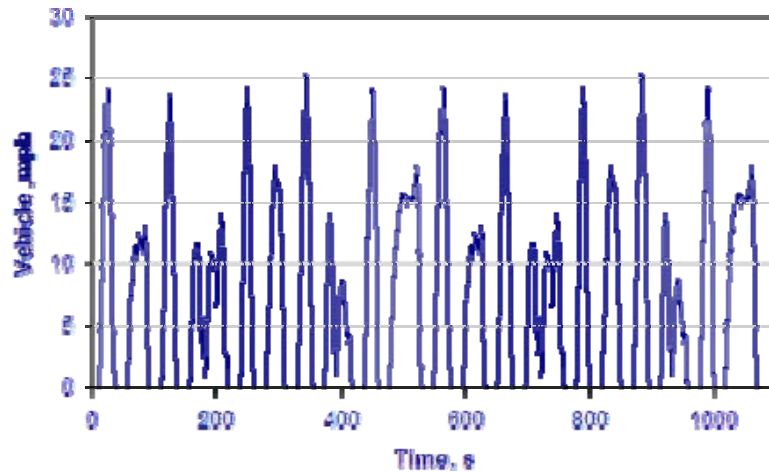


Figure 9: -- Manhattan Bus Cycle

Determining Which Bus Cycle to Use

Assuming that these candidate cycles are accepted, in order for the selected drive cycle to be as close to the intended use of the vehicle as possible, there are certain criteria to determine whether the Manhattan or Orange County drive cycle should be used for a specific vehicle test.

Two major factors that determine transit bus performance and for which data are readily available are average route speed and percent idle (“stopped”) time. Of these, average route speed is the most significant discriminator in predicting performance. These two parameters are combined into an index that determines which of the two drive cycles shall be used to test the fuel consumption of a specific transit bus model.

The midpoint between the average speeds on the two cycles is 9.58 mph, and the midpoint of percent idle is 28.5%. In the combination of these two parameters, the average speed is given twice the weight of percent idle. By equating the ranges of the two quantities and after normalization the following formula is obtained:

$$\text{Cycle Index} = 0.013 \times (\text{percent idle}) + 6.025 \div (\text{average speed in mph})$$

If the cycle index for the proposed average of all anticipated routes is greater than or equal to 1, the Manhattan cycle shall be used. If the cycle index is less than 1, the Orange County cycle shall be used.

As an example, the Cycle Index for a bus fleet with a predicted fleet average speed and idle time exactly that of the Manhattan cycle would be the following:

$$0.013 \times (36) + 6.025/6.83 = 1.35$$

The Cycle Index for a bus fleet with a predicted fleet average speed and idle time exactly that of the OCTA cycle would be the following:

$$0.013 \times (21) + 6.025/12.33 = 0.76$$

The average predicted route speed used for this analysis is for the buses while in-service, and does not include driving to begin the route or to return to the depot after the service has been completed.

In some cases, the intended service for a particular vehicle may be a route that more closely resembles a combination of the Manhattan Cycle and the Orange County cycle than it does either one. Users of this test protocol have the option of running a complete set of tests with each cycle, then reporting the results as a weighted value of the results from each cycle.

Payload (passengers) and accessory loads for transit buses are significant, especially the impacts of air conditioning, heating and defrosting. Power can also be required to lower and raise the bus to accommodate passengers getting on and off, during typical operation. Load factors need to be determined for the transit bus cycle. Work to define these loads started during the development of the *Recommended Practice for Measuring Fuel Economy and Emissions of Hybrid-Electric and Conventional Heavy duty Vehicles*, SAE Surface Vehicle Recommended Practice J2711, and should be considered as a starting basis for continued development of these load factors.

9.8 Intermodal Drayage Truck

The intermodal drayage truck cycle simulates a combination tractor-chassis freight truck operating in predominantly local, urban-type driving with relatively short trip lengths. The vehicles provide intermodal cargo drayage by shuttling ocean-going freight containers among marine terminals, chassis and container depots, rail terminals, and local consignees. The operations are characterized by periods of extended creep idle or idle while waiting at distribution hubs, with limited highway and suburban driving between destinations. Drayage trucks are powered by heavy duty engines typically used in class 8 trucks (33,001 pounds GVWR or greater). Typically, the tractor will have 3 axles. The chassis is a framework equipped with 2 axles, on which an ocean-going freight container is loaded. Chassis can have a sliding adjustable center beam to fit containers of either 20 to 28 feet, or containers of 40 to 48 feet. The latter size is more common.

A candidate intermodal drayage truck cycle was developed by the University of Texas based upon a number of instrumented trucks operating in the Port of Houston area. A graphic for the cycle is found in Figure 10.

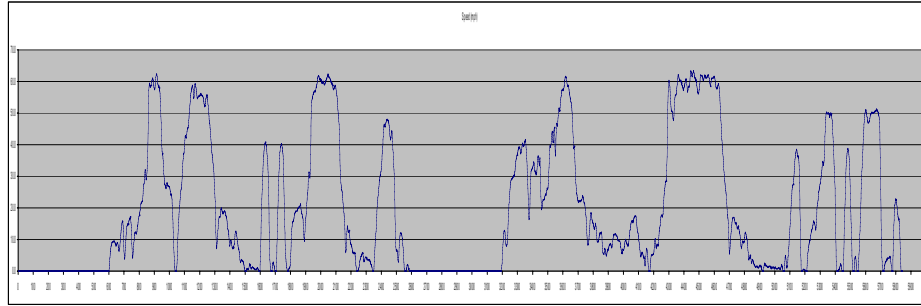


Figure 10

Additional input and data is needed to refine this drive cycle, including data from other major port areas (POLB/POLA, NY/NJ), and to develop payload and accessory loads.

10. Accessory Load

Accessory load refers to vehicle power requirements needed to operate equipment, accessories, and other implements that are essential to the intended vehicle use. These power requirements are considered a “load” on the engine (or other vehicle power source), and must be accounted for when evaluating vehicle fuel efficiency. For the purposes of this test procedure, the following engine/operating components are not considered “accessories” and the loads will not be measured separately:

- Air compressor
- Water pump
- Engine cooling fan
- Power steering
- Power brakes

The following sections describe the main accessory functions essential to the mission of many heavy duty vehicles. The power needed to provide these functions must be accounted for in the fuel efficiency test as an accessory load. The heavy duty fuel efficiency test protocol will require the following accessory loads be used during a specific portion of the drive cycle. EPA is still gathering information to determine what the best options are for including accessory loads and encourages suggestions from readers of this document. EPA will include those recommended requirements in subsequent versions of this protocol.

10.1 Heating and Ventilation, Defrosting

Heating and ventilation refers to loads associated with passenger comfort that do not require operation of the refrigeration cycle of the air conditioner. Heating requires a source of heat (typically waste heat from the engine cooling system, but not necessarily) plus operation of a blower motor with air circulation fans. Ventilation requires only operation of the blower motor and air circulation fans. Defrosting requires a defroster fan.

10.2 Air Conditioning

Air conditioning refers to loads associated with passenger comfort that require operation of the refrigeration cycle of the air conditioner. The air conditioning load may include the power required to operate a compressor (pump), an evaporator (condenser), and a blower motor with air circulation fans.

10.3 Power Take-off (PTO) or Other Vocational/Service Work Load

Power take-off refers to loads associated with the operation of mission functions on a vocational or service truck. For example, hydraulic load to operate the loading lift arms, hopper compacting, and dump operations on a neighborhood refuse truck; hydraulic load to operate the aerial lift on a utility service truck; and, electric load to simulate supplying electrical power to the grid on a utility service truck.

10.4 Lamps and Lights

Lamps and lights refer to loads associated with the operation of headlights, all other exterior vehicle lights (tail light, brake light, marker light, hazard light, turn signal light, license plate light, identification light, clearance light, dome light, etc.), and lights on instruments and gages.

10.5 Miscellaneous

Refers to accessory loads not otherwise specified, but typical for a given heavy duty vehicle's operation, including electric windows, electric fuel pump, radio, and electric wipers.

10.6 Drive Cycle Load Requirements

Work has started to develop accessory load power requirements.²⁰ Substantially more data and input is needed to determine: 1) the power draw of accessory loads for heavy duty vehicles; and, 2) the operational characteristics of each heavy duty vehicle, to determine "typical" hours and intensity of operation for each accessory function. EPA requests specific comments on drive cycle load requirements for each drive cycle described above.

Highway Line Haul Accessory Load

[Reserved]

Regional Haul Accessory Load

[Reserved]

Local Pick Up and Delivery Truck Accessory Load

[Reserved]

Neighborhood Refuse Truck Accessory Load

[Reserved]

Utility Service Truck Accessory Load

[Reserved]

Transit Bus Accessory Load

[Reserved]

Intermodal Drayage Truck Accessory Load

[Reserved]

11. Vehicle Payload and Test Weight

The vehicle test weight is the loaded vehicle weight, as measured at the start of each complete drive cycle for each vehicle test. This weight shall remain constant for each drive cycle for the duration of a vehicle test/s. The vehicle test weight is intended to simulate typical operation for the heavy duty truck application being tested.

Vehicle test weight is generally the vehicle curb weight (weight of empty vehicle without passengers or payload, but including oil, gas, coolant, and other standard equipment), plus the weight of the driver, and a specified payload or cargo weight. In the case of a transit bus, it includes the weight of a specified number of passengers.

The vehicle test weight also includes the weight of the PEMS, plus span and calibration gases, or the portable fuel tanks, plus test fuel.

For heavy duty vehicles under 14,000 pounds GVWR (up to class3), the vehicle test weight is the test equivalent weight specified in 40 CFR Part 86, (specifically §86.129-94).

For all other heavy duty vehicles, a vehicle test weight is stipulated for each of the drive cycles in this test procedure. The test weights for each drive cycle in this test procedure are developed taking into consideration vehicle GVWR, typical payload (or other appropriate weight metrics), average percent empty miles, and weight fluctuation due to typical cargo loading and unloading patterns.

PAYLOAD VALUES:

Highway line haul and regional haul: GVWR is 80,000 pounds. Industry data suggests an average annual cargo weight of about 36,500 pounds for large over-the-road trucks.²¹ Assuming a typical tractor and enclosed van trailer with a curb weight range from 28,000

pounds to 32,000 pounds (16,000 to 18,000 pounds for the day cab or sleeper tractor, and 12,000 to 14,000 pounds for the dry van or refrigerated insulated trailer), the cargo comprises from 70 percent to 76 percent of payload capacity. This information is summarized in Table xx, below:

Curb Weight (tractor & trailer)	Payload	GVWR	Payload Capacity	Percent Load	Total Loaded Weight for Test
28,000	36,500	80,000	52,000	70%	64,500
30,000	36,500	80,000	50,000	73%	66,500
32,000	36,500	80,000	48,000	76%	68,500

Unused capacity is due to empty hauls, non-revenue miles, and loads that “cube out” before they “weigh out.” Given this range, a recommended payload for testing is 75 percent of payload capacity.

Local pick up and delivery vehicle: GVWR and payload depends upon the intended cargo and vehicle configuration (parcel, beverage). The vehicle is gradually emptied during the execution of its duty cycle. A simple approach for a recommended testing payload could be to consider that the vehicle spends roughly half its miles empty, or a 50 percent “effective” payload. However, the vehicle may be volume-limited rather than weight-limited, so the 50 percent would be from volume capacity. More data is needed on typical payloads for different types of local pick up and delivery vehicles.

Neighborhood refuse truck: GVWR can vary between 52,000 to 72,000 pounds. The vehicle is gradually filled during the execution of the duty cycle. A simple approach for a recommended testing payload could be to consider that the vehicle spends roughly half its miles full, or a 50 percent “effective” payload. However, the vehicle may be volume-limited rather than weight-limited, so the 50 percent would be indexed from a volume capacity. More data is needed on typical payloads for different types of neighborhood refuse trucks.

Utility service truck: GVWR varies between 16,001 and 33,000 pounds. Truck weight includes the “payload” weight of the aerial lift and other equipment. More data is needed on GVWR and payload to develop a recommended payload for testing.

Municipal transit bus: Typical GVWR of 19,001 to 26,000 pounds. A suggested payload for testing is curb weight, plus driver, plus 150 pounds multiplied by one-half the seated passenger count. This recommendation is from SAE J2711, §6.3.3.²²

Intermodal drayage truck: GVWR of 80,000 pounds. Industry data suggests a typical cargo weight of about 40,000 for ocean-going containers (based upon agricultural loads). Assuming a tractor, chassis and 40’ container with a curb weight of about 32,000 to 34,000 pounds (16,000 to 18,000 pounds for a tractor; 8,000 for a chassis; 8,000 for an empty container), the cargo comprises about 83 to 87 percent of the remaining 46,000 to 48,000 pounds payload capacity. Assuming that the ocean-going containers are empty

for nearly half their trucked miles, this would bring the effective average weight to 20,000 pounds, or about 42 to 43 percent of rated payload. More data is needed on GVWR and payload to develop a recommended payload for testing.

11.1 Test Equivalent Weight

The test equivalent test weight is the normative weight at which the test shall be conducted, when using the chassis dynamometer method. This weight is used to determine dynamometer inertia weight settings. Test equivalent weight is based upon the vehicle test weight (but not to exceed 250 pounds below the vehicle test weight). For all heavy duty vehicles above 14,000 pounds GVWR, refer to the following table:

Vehicle Test Weight From Drive Cycle (lbs)	Test Equivalent Test Weight (lbs)
13,751 to 14,250	14,000
14,251 to 14,750	14,500
14,751 to 15,250	15,000
15,251 to 15,750	15,500
Numerical pattern repeats up to and including....	
80,251 to 80,750	80,500
80,751 to 81, 250	81,000
81,251 to 81,750	81,500

For all heavy duty vehicles below 14,000 pounds, refer to the test equivalent test weights found in 40 CFR Part 86 (specifically §86.129-94).

11.2 Test Fuel Weight and Volume

In accordance with SAE J1321, maintain fuel volumes as consistently as possible over the course of the test, to minimize random weight variation.

The amount of test fuel in the vehicle fuel tanks shall be topped off at the beginning of each test day. Ideally, this will ensure that tests will be conducted with an initial fuel volume of between 50 and 75 percent of the total capacity of the vehicle fuel tank.

If the fuel efficiency test is conducted using the gravimetric method with portable fuel tanks, the weight of the portable fuel tanks including fuel must be considered in loading the vehicle to its required test weight.

Portable tanks shall be topped off before each test, and the weight recorded as per Section xx of this test procedure.

12. Test Set-Up Procedure

12.1 Test Payload

Where a test payload is required to meet vehicle test weight requirements, the payload shall be evenly distributed throughout the trailer (or bus body) and the over-axle loads must be proportional with federal over-axle weight limits.²³ For example, if testing at 80,000 pounds, the payload would be distributed to achieve a weight of 12,000 pounds over the steer axle, 34,000 pounds over the drive axle, and 34,000 pounds over the trailer axle. If testing the same vehicle at 65,000 pounds, the payload would be distributed to achieve a weight of approximately 12,000 over the steer axle (since the payload does not affect the steer axle that much), 26,500 pounds over the drive axle, and 26,500 pounds over the trailer axle. It is recommended that the test payload be secured by strapping down then blocking the payload with nailed-down chucks, so that the payload will not shift during the test. Payload must not change during a test.

The vehicle must be weighed using properly calibrated truck weight scales that conform to the most current provisions established by the National Institute of Standards and Technology (NIST). It is recommended that the truck scales also have a National Type Evaluation Program (NTEP) Certificate of Conformance.

12.2 Tire Pressure

Tires shall be representative of a typical (e.g., best-selling) tire for a given vehicle application, unless a special tire characteristic (e.g., low rolling resistance) is a condition being tested.

Tire pressure shall be adjusted at cold condition as needed before pre conditioning, and tested to the tire manufacturer's recommended maximum cold inflation pressure. Tire pressure shall also be measured at the end of each completed test run to ensure that, at a minimum, the inflation pressure is consistent with the starting cold pressure.

12.3 Mechanical Preparation of Test Vehicle

Vehicles shall be representative of production fleet vehicles. Test vehicles need not be new, but they must be in good mechanical order and operating condition. All components and equipment shall be calibrated and maintained to within manufacturer-recommended specifications. The exception is any component that has been deliberately modified as part of the test truck design.

Vehicles shall be mechanically prepared and maintained in accordance with SAE J1321, Sections §8.6 to §8.10. Vehicles must not have any mechanical or physical defects that

may affect fuel efficiency. Vehicles must not have any fluid, exhaust, or air suspension leaks. There must be a visual inspection of the tires prior to each test day, to detect any signs of tire or wheel damage or unusual wear.

The air cleaner monitor and engine fault codes must be checked prior to the test, and any abnormal conditions must be corrected, to ensure that the vehicle is in proper working order. It is recommended that the crankcase, differential, and gear lubricant be removed and replaced with fresh lubricant prior to the test.

Test vehicles shall have accumulated a minimum of 2,500 miles prior to testing (10,000 miles are recommended to properly break in a new vehicle).

If the test method uses the carbon balance method of fuel consumption measurement, follow the additional vehicle preparation requirements in CFR 40 §86.131-90.

Vehicles must be fueled from the same fuel dispenser during the entire test to ensure consistent fuel grade and quality. Empty the test fuel tanks by draining, or by vehicle operation, before filling with test fuel. Refer to CFR 40 §86.132-90. If a removable fuel tank is being used, it shall be filled only with the test fuel. Refer to Sections §5.7.1, §5.7.3, and §6.3 of SAE J1321.

If a PEMS is being used, refer to 40 CFR Part 1065 Subpart D for PEMS system set up. If using the carbon balance method with either a PEMS or laboratory gas analyzers, all detectable sources of exhaust gas leaks must be sealed or plugged.

Records of vehicle identification and condition must be kept. Refer to SAE J1321 §4 and the referenced Type II Test Data Forms, and the appendices of this document for more details. Vehicles must be weighed before the test to ensure proper test weight, and over axle weighting, and weight records must be maintained.

12.4 Vehicle Preconditioning

Vehicle preconditioning warms the engine and exhaust emission control equipment, and raises vehicle operating temperatures, so the vehicle is warmed up. Ideally, the engine coolant, oil and drivetrain lubricants should reach an operating temperature that would be consistent with those expected during multiple repetition of the associated test cycle. To accomplish these objectives, the test vehicle shall be driven through a warm up cycle prior to the test. The warm up cycle shall consist of driving the vehicle at least one time through the drive cycle that will be used for the test, or 60 minutes, whichever is greater. Hybrid vehicles may require a lengthier warm up time, to establish an equilibrium state of charge (SOC) in the rechargeable energy storage system (RESS), such that the initial and final SOC values during the subsequent test cycles will be within the stated tolerance. Refer to the following sections for more details.

The test shall commence between 10 and 30 minutes after completion of the warm up. Gas analyzers must be re-calibrated during the interval between warm up and test start.

Intervals between test cycles shall be between 10 and 30 minutes. Gas analyzers shall be checked after completing the test cycle to ensure that excessive drift hasn't occurred.

If there is any change (i.e., equipment failure or vehicle modification) in the test vehicle during testing, all testing will be repeated.

For vehicles equipped with a diesel particulate filter, a manual regeneration of the diesel particulate filter shall be conducted prior to testing.

12.5 Hybrid Vehicles – Additional Vehicle Conditioning

If the vehicle is a hybrid, additional vehicle conditioning is necessary to establish an "equilibrium" state of charge (SOC) in the rechargeable energy storage system or RESS. State of charge is a measure of the amount of energy stored in an RESS, expressed as a percent of the total energy storage capacity of the RESS (battery, flywheel, hydraulic accumulator, capacitor, etc.).

A stable SOC ensures that the energy stored in the RESS will not fluctuate too widely during the test. If the energy in the storage device fluctuates too widely during a test, then the amount of energy that the RESS provides to the vehicle relative to total vehicle fuel consumption will be atypical, and measured vehicle fuel efficiency will not be representative of that vehicle's true operation. To measure fuel consumption that is within +/- 3 percent of a vehicle's true, representative fuel consumption, the change in energy stored in the RESS should be less than +/- 1 percent of the total fuel energy consumed during a test cycle.²⁴ A stable SOC is within a stated tolerance for the initial and final SOC values during a test cycle, as described below.

To accomplish this, the hybrid vehicle shall be operated (driven) at least twice through the drive cycle that will be used for the test in order to verify that the initial and final SOC values are within the stated tolerance. This vehicle operation can count toward the requirement for warm-up laps, provided that the test occurs within the time required from completion of warm up lap.

If the selected drive cycle results in a net increase or decrease in the SOC, then the initial SOC of the RESS may be adjusted externally following a trial-and-error approach using the specific procedures detailed below.

If the energy storage capability of the RESS falls below the minimum level specified by the manufacturer, testing data generated with that vehicle should be discarded and the vehicle should be repaired or replaced prior to conducting additional testing. (SAE J1711 §4.1.2.3.)

Specific preconditioning information for different types of hybrid vehicles is described below.

Hybrid Electric Vehicles with Batteries

Off-vehicle charging of the battery pack is permissible in order to achieve the desired “equilibrium” SOC.

Hydraulic Hybrid Vehicles

The goal is to have the accumulator pressure at the end of the test be similar to the accumulator pressure at the start of the test so as to ensure meeting the stated tolerance in Section 4.6 above. To accomplish this, operate the vehicle over a cycle identical to the test driving cycle prior to conducting the test. As described above, this vehicle operation can count toward the requirement for warm-up laps, provided that the test occurs within the time required from completion of warm up lap.

The hydraulic accumulators can only store about as much energy as is generated over a typical stop; that energy is usually less than what is needed to accelerate the vehicle for the next drive event. Therefore, the pressure in the accumulator is dependant on the last few hills of the drive cycle and is usually at a fairly consistent value at the end of any drive cycle. A “hill” is a complete start-stop sequence on the drive cycle.

Hybrid Electric Vehicles with Capacitors

Follow a procedure similar to that described for hydraulic hybrid vehicles.

Preconditioning Hybrid Vehicles with Electromechanical Flywheels

Follow a procedure similar to that described for hydraulic hybrid vehicles.

12.6 Hybrid Vehicles – Procedures for Determining State of Charge (SOC) and Net Energy Change (NEC)

The objective of this protocol is to quantify the fuel efficiency of a vehicle, relative to the fuel that is consumed. There is to be no net energy provided from the RESS. Thus, the net energy change (NEC) during a valid test run must be zero, or within a small tolerance of zero, as defined below.²⁵

In general, the approach to follow, per SAE J2711 §4.3, is to measure the State of Charge (SOC) at the beginning of the drive cycle/test run, measure the SOC at the end, and calculate the Net Energy Change as SOC_{final} minus SOC_{initial} . The NEC is compared to the Total Cycle Energy (TCE) where TCE is defined as the total fuel energy (TFE) of the fuel consumed during the test cycle (in consistent units) minus the NEC. The sign convention for NEC is that negative means that energy was extracted from the RESS during the test. In that case, the TCE will be larger than the TFE when NEC is negative. The NEC is calculated as a percentage of the TCE to determine if a test run is valid, can be made valid with SOC corrections, or is invalid. Follow the procedure outlined in SAE J1711, §4.3.1.4, with the exception that the selected drive cycle will be used in place of the UDDS that is cited. More than one drive cycle may be needed to achieve a long enough test run to achieve the NEC “window”, as explained in Section 4.6.

The criteria for the absolute value of the NEC/TCE ratio are as follows:

≤1% means the test run is valid and can be used without correction;

>1% and ≤5% means that the test run values for emissions and fuel consumption must have a SOC correction applied to them; and,

>5% means that the test run is invalid.

Achieving runs that fall within this “5-percent window” is a matter of some trial and error. Preconditioning of the vehicles will be required, as discussed in Section xx. The drive cycle may be repeated to make a longer test run, if that is advantageous to achieving the “5-percent window.”

Specific procedures for each type of RESS are described in the following sections.

12.6.1 Batteries

The SOC of the battery in a charge-sustaining hybrid electric vehicle can theoretically be determined by measuring the amp-hours stored, but in practice it is difficult to do with sufficient accuracy. Thus, for batteries the NEC must be determined indirectly. The approach is to measure continuously (using a totalizing ammeter) the flow of current into and out of the battery. The integrated (totalized) value, with the appropriate conversion factors applied, is the NEC. The specific methodology is shown in SAE J2711, §4.2.1. Equations 1 and 2. Absolute measures of initial and final SOC will not be available for the battery; only the net change in stored energy (totalized amp-hours) can be measured. The correct sign convention must be followed: a negative NEC means a net loss of charge from the battery.

12.6.2 Capacitors

The SOC for capacitors can be determined with acceptable accuracy by measuring the voltage across the capacitor pack. Thus the NEC for a test cycle can be readily calculated by difference of the final and starting SOC. The specific methodology is described in SAE J2711, §4.2.2, Equation 3.

12.6.3 Electromechanical Flywheels

The SOC for electromechanical flywheels can be determined with acceptable accuracy by measuring the inertia and speed of the flywheel (revolutions per minute). Thus the NEC for a test cycle can be readily calculated by difference of the final and starting SOC. The specific methodology is described in SAE J2711, §4.2.3, Equation 4.

12.6.4 Hydraulic Accumulators

The SOC for hydraulic accumulators can be determined with acceptable accuracy by measuring the accumulator pressure (pounds per square inch [psi]). For an accumulator the SOC can be determined using Equation 1.

$$SOC = \frac{(P_c * 144 * V_c) - \left(P * 144 * V_c * \left(\frac{P_c}{P} \right)^{(1/k)} \right)}{(1 - k)} \quad (1)$$

where:

SOC = State of Charge of the accumulator (lb-ft)

P_c = pre-charge pressure of the accumulator (psi)

- V_c = volume of gas in the accumulator at pre-charge (ft^3)
- P = current accumulator pressure (psi)
- k = ratio of specific heats for the pre-charge gas (1.8 for nitrogen at the high pressures typical of hydraulic accumulators²⁶).

To convert the units of SOC from lb-ft to joules, multiply by 1.3558.

The NEC is calculated as the difference in the ending SOC and starting SOC, following a procedure analogous to that of capacitors and electromechanical flywheels described above.

12.6.5 SOC Correction and Net Energy Charge

The SOC correction follows the procedure described in SAE J2711, §4.4 that cites a 2000 SAE paper by Clark, et al.²⁷ A separated SOC correction calculation must be made for each measured pollutant (if applicable) and for fuel consumption. The measured values from at least 3 replicate runs are plotted as a function of NEC. A linear regression line is drawn through the data. If the coefficient of determination, R^2 , is equal to or greater than 0.80, then the data are acceptable for SOC correction.

Using the regression equation, each y-value (i.e., each individual pollutant emission rate or the fuel consumption value) is calculated for an x-value (NEC) of zero. These calculated numbers are the SOC-corrected values that are then used for the comparison calculations in Section xx.

12.7 Fuel Analysis

A supply of test fuel sufficient to complete the test must be procured and fuel parameters including fuel density analyzed prior to the start of the test. The test fuel should be sequestered once it is procured and analyzed. If it is necessary to add additional fuel to the test fuel supply during the course of the test, another fuel analysis must be conducted to ensure the test fuel still meets the required fuel parameters. For each test segment, a record must be kept of the fuel parameters of the test fuel, including density.

The test fuel shall meet fuel specifications summarized in the section of this document entitled “Test Fuel.”

13. Test Procedure

Refer to Figure 11 for an overview of the steps in the overall conduct of the testing, for either a track or a chassis dynamometer test.

13.1 General Requirements

Driver Conduct

Drivers must be skilled in test driving. Drivers shall be in compliance with existing state and federal laws governing driver licensing. Generally speaking, a commercial motor vehicle driver’s license or CDL is required in the United States to operate any type of

vehicle with a weight over 26,000 pounds GVWR, including (but not limited to) tow trucks, tractor trailers and buses. However, these requirements may not apply in all states and/or on non-public roadways (e.g., a privately-owned test track facility.) It is recommended that the test facility ensure that all drivers comply with existing state and federal laws. Pre-determined driving procedures (e.g., gear shifting) shall be specified prior to the test. Reference SAE J1321 §§5.2 and 5.5. Drivers shall learn the drive cycle thoroughly prior to the test, and drive test vehicles precisely according to the drive cycle in terms of required speed at a given time.

Practice runs of the driving cycle are encouraged, to permit driving cycle adjustments and to allow drivers to learn the drive cycle, so they can meet the speed-time trace accuracy requirements. Gear-shifting representative of real-world driving shall be encouraged (neither too smooth nor too aggressive).

For track tests, an observer shall ride in the vehicle with the driver. The observer, using a stop watch, will coach the driver to meet the target times for each marker, and for the test overall. The observer will record the actual time to each marker, in accordance with SAE J1321. Reference SAE J1321 §6.5, and Fuel efficiency Test Forms 2-3 and 2-4.

The same driver (and observer, if applicable) must stay with each vehicle for the duration of the test.

Track and Chassis Dynamometer Preparation

If the chassis dynamometer has not been used in over two hours prior to the test, it shall be necessary to warm up the chassis dynamometer for at least 15 minutes prior to the test. The test vehicle shall not be used for this warm-up. The track shall be prepared for the specific drive cycle being used by setting up cones, markers, stop signs, and any other aids to achieve a consistent, repeatable test run. Creating a repeatable test run will be an iterative process, requiring multiple trial runs.

Fuel Consumption Measurement Equipment Preparation

Follow general specifications for the fuel measurement method selected. For PEMS, use 40 CFR Part 1065, Subparts C and J. For gravimetric/portable fuel tank, use SAE J1321 §§5.7.1 and 5.7.3. For laboratory emissions equipment, use 40 CFR Part 86.315-79.

Section 8 of this document provides more details on each of these fuel measurement methods.

Additional Steps Required for Hybrid Vehicles

If the vehicle is a hybrid, the RESS SOC should be measured at the start and stop of each test run. For each different test cycle a minimum of three test runs must be performed to provide sufficient data for a SOC correction, if needed. It is also recommended that at least one test run have a net positive and another a net negative NEC value so that net SOC calculations are based on interpolation and not extrapolation. The NEC must meet the requirements given in SAE J2711 and vary according to the RESS used.

Test Timing

Only “hot start” tests will be used in data reporting and/or data analysis. A hot start is a test that starts between 10 and 30 minutes of “hot soak” time following a previous test cycle or preconditioning cycle.

Engine Starting and Restarting

Follow general specifications for starting the vehicle as described in 40 CFR §86.1236-85.

Drive Trace Accuracy

The test vehicle must be driven according to the drive cycle in terms of required speed at a given time as closely as possible, to ensure a reproducible test result. The criteria for determining whether the vehicle met the drive cycle differ for each test method, as described below. EPA requests comments about whether these accuracy requirements are reasonable or necessary.

Track Test Drive Trace Accuracy

The requirements for drive trace accuracy for a track test are adapted from 40 CFR 86.115-78. A test run is considered valid if the driven values fall within the drive cycle (the “commanded” values) according to the following speed tolerances:

- The upper limit is 2 mph higher than the highest point on the drive cycle, within 1 second of the given time.
- The lower limit is 2 mph lower than the lowest point on the drive cycle, within 1 second of the given time.

Speed variations greater than the tolerances (such as may occur during gear changes or braking spikes) are acceptable, provided they occur for less than 2 seconds on any occasion and are clearly documented as to the time and speed at that point of the drive cycle.

Additionally, to be valid, the total test run shall fall within the ± 0.5 percent time requirement as specified in SAE J1321 §8.5.

Chassis Dynamometer Test Drive Trace Accuracy

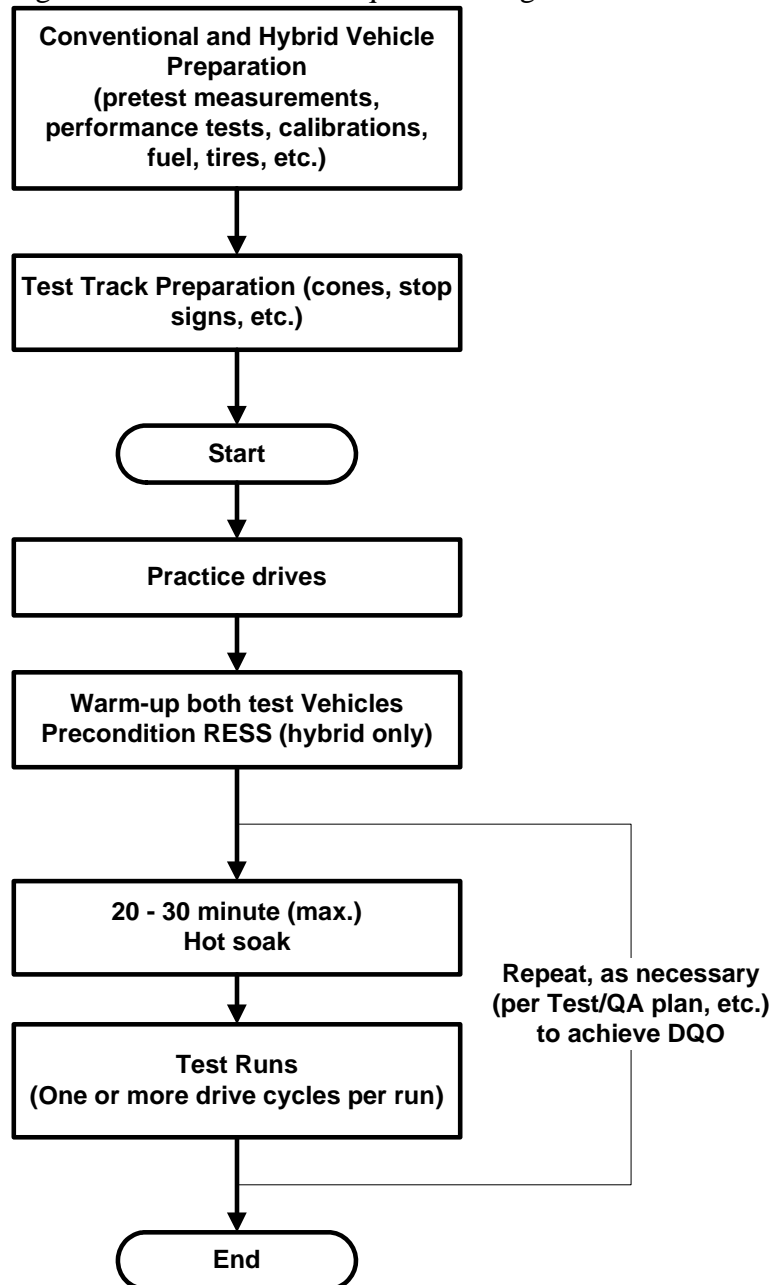
The requirements for drive trace accuracy for a chassis dynamometer test are adapted from SAE J2711, §7.10 using a regression analysis of the “driven” versus the “commanded” speed at each time point. A test run is considered valid if the slope of the regression line is between 0.90 and 1.10, and the R-squared value is 0.80 or greater. Tests that fail to meet this requirement will be deemed invalid.

Running tests in accordance with the light duty vehicle certification procedures in CFR Part 86 Subpart B also would be considered valid tests.

13.2 Test Procedure for Test Track

Figure 11 below is a general outline of the test sequence for a test conducted on a test track.

Figure 11. Generic Test Sequence Using Test Track



Steps to Conduct a Track Test

This test protocol incorporates the test procedure elements outlined in SAE J1321 §§6.1 through 6.9, 6.11, and 6.12. The referenced sections cover details for conducting a test, which consist of:

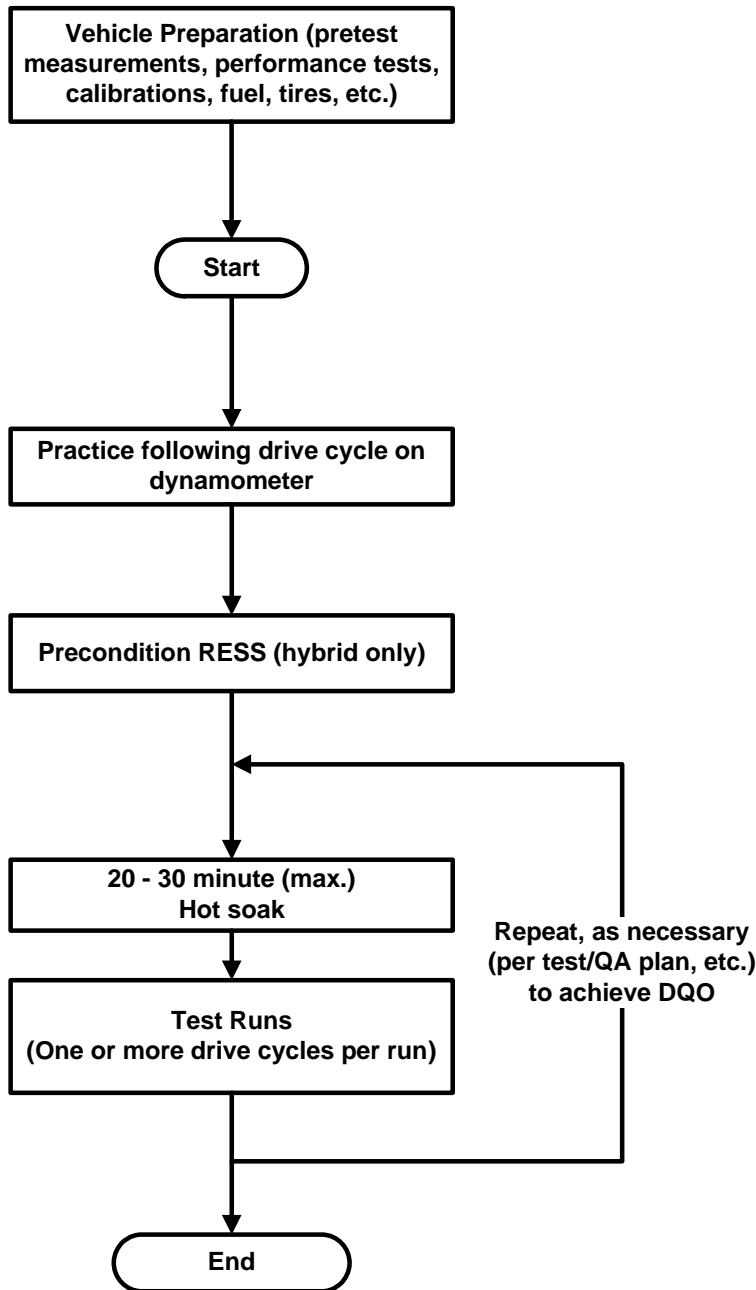
- Warm up reference SAE J1321 §6.1,
- Ambient condition recording reference SAE J1321 §6.2,
- Start of test reference SAE J1321 §6.3,
- Initial test run reference SAE J1321 §6.4,
- Test run recording and coaching reference SAE J1321 §§6.5 and 6.6,
- End of test run reference SAE J1321 §6.7,
- Interval between test runs reference SAE J1321 §6.8,
- Test run repeats reference SAE J1321 §6.9,
- One test vehicle, different configurations reference SAE J1321 §6.11,
- Two complete test vehicles reference SAE J1321 §6.12.

For §6.8 and 8.13; substitute the phrase “checking data from PEMS” for the word “refueling” if using the PEMS/carbon balance method instead of the gravimetric method.

13.3 Test Procedure for Chassis Dynamometer

Figure 12 below is a general outline of the test sequence for a test conducted on a chassis dynamometer.

Figure 12. Generic Test Sequence Using Chassis Dynamometer



Steps to Conduct a Chassis Dynamometer Test

This test protocol incorporates the test procedure elements outlined in 40 CFR Part 86, Subpart B. Although Subpart B is written for light duty certification procedures, the steps in Subpart B are in principle the same for performing heavy duty chassis dynamometer runs.

Certain aspects of Subpart B shall be modified for this test. For example, the dynamometer roll specifications per 86.108-00 will differ for heavy duty chassis dynamometer rolls.

References in Subpart B to FTP driving schedules and provisions dealing with evaporative emission testing, the OBD requirements, and the smoke emission requirements do not apply.

13.4 Coastdown Test Procedure to Calculate Road Load

When conducting a fuel efficiency test using a chassis dynamometer, coast down testing needs to be conducted to supply road load inputs to the chassis dynamometer. The vehicle must be tested at its test weight including the payload specified for that drive cycle.

Depending upon the type of chassis dynamometer used, the appropriate choice of SAE coast down test shall be conducted: SAE J1263, SAE J2263, or SAE J2264.²⁸ Refer to these coastdown procedures for details. For example, if a single roll electric dynamometer is used, J2264 is the appropriate coastdown procedure.

14 Required Number of Test Runs

Multiple tests will be needed to establish whether a vehicle meets the performance standard for a SmartWay designation, as test to test variability (precision) will affect the results of any single test. We expect that precision will be lower for a track test than for the dynamometer tests, but in both cases, statistical data will be developed to compute the required number of tests to provide confidence that the vehicle meets the performance-based designation. The criterion for meeting this designation is an 80 percent probability that the test results exceed the fuel efficiency designation by an amount equal to the lower tail of the 95 percent confidence interval of the test measurements. For example, if the performance based designation of a particular type of truck was 7.5 miles per gallon, and replicate measurements showed that the 95 percent confidence interval for the test was 0.05 miles per gallon, then the results of the statistical computation described below and in Appendix I should provide evidence of an 80 percent probability that the test result was 7.5 mile per gallon or greater.

The specific values underlying the statistical assumptions and statistical formulae are different will be slightly different for track and dynamometer test data, and these are presented below and in Appendix I. *[A note to readers: We invite comment on this method.] It is important to note that the following statistical techniques are relevant to conducting the testing against a known environmental reference truck (discussed in Purpose and Scope section on page 6 of this document). Testing against an environmental reference can minimize the number of tests needed to produce appropriate confidence in the test results.*

14.1 General Requirements

The number of tests required for fuel efficiency and emission testing is determined from the following criteria:

1. A minimum of three (3) tests are required to provide the basic result of a mean emission reduction and 95 percent confidence interval on that mean based on measured variability for each of the measurements and test parameters.
2. Additional tests may be required to meet the requirement that the vehicle meets the performance criterion. These criteria become controlling for low carbon emission/fuel consumption reductions and/or high test variability. The procedure to determine the appropriate number of tests is given in the following sections, with additional information in Appendix I
3. Additional tests may be desired by the applicant to reduce the width of the 95 percent confidence interval on the mean carbon emission/fuel consumption reduction. Appendix I provides additional explanation and example scenarios. This third criterion is a consequence of applying standard statistical procedures to the test design and data analysis. At fixed measurement variability, normal statistical procedures lead to a small number of tests giving a broader 95 percent confidence interval than a larger number of tests. To any potential technology user, a reported reduction in emissions/fuel consumption of 40 percent \pm 5 percent is better than a reported value of 40 percent \pm 20 percent, and will be given more credence.

Confidence Interval on the Result

A consequence of the unavoidable variability in test measurements is that the mean of a small number of measurements has a small probability of giving the true fuel consumption/emission reduction. In some cases it may not be possible to make a statistically-significant determination that the measured reduction is different from zero. The results of measurements conducted using this protocol will be presented as the mean and 95% confidence interval on that mean, calculated using the sample standard deviations determined from the test data. Because sample standard deviations are available, the t-statistic is applied to compute the confidence intervals (as opposed to the “z” statistic that was used for the sample size calculation).

14.2 Number of Test Runs for Test Track Test

This protocol requires that sufficient tests be conducted to have an 80 percent probability of detecting whether the fuel efficiency meets or exceeds the performance standard, computed from the expected experimental variability for the various measurements. In this context, “detecting” means that the performance standard is less than or equal to the lower tail of the 95 percent confidence interval. Insufficient replication can result in inability to detect a statistically significant fuel consumption benefit.

A sample-size equation was derived to explicitly compute the number of tests required for normally distributed measurements having known standard deviations. However, since the actual testing procedure will be based on sample standard deviations and t-statistics, a correction factor was applied to the sample-size equation to account for the extra variation in the t-distribution relative to that of the normal distribution. Some results of applying that calculation are presented in Table 1 for emission reductions and fuel efficiency increases. Equations used to compute the number of tests required are presented in Appendix I.

Table xx presents the variability of emissions (in this example, NO_x), and fuel efficiency measurements based on standard deviations calculated from an analysis of actual test track data of Kenworth truck tractors driving a suburban drive cycle.²⁹ The results in Table 1 are based on the sample-size equation with the correction factor for the one-tailed t-distribution. More tests than are shown in Table 1 may be required under conditions of higher variability.

The column headings in the first row of the table give the assumption that the hybrid vehicle will show an emission reduction or a fuel efficiency improvement of 5 percent, 20 percent, 50 percent, or 85 percent from the baseline conventional emission/fuel efficiency levels. In developing the Test/QA plan, selection of this value will be based on the applicant’s experience and expectation. The second row gives the constant and known baseline conventional vehicle variability. The third row is the assumed measurement variability for the hybrid vehicle based on the variability of the conventional vehicle. (Variability is expressed as the known standard deviation at the emission/fuel efficiency level divided by the corresponding conventional vehicle mean emission/fuel efficiency level and multiplied by 100 percent.) The fourth row gives the

calculated number of tests required to have 80 percent probability that the 95 percent confidence interval about the mean expected emission reduction or fuel efficiency improvement would not include zero.

Table x. Number of replicate test track tests (for both conventional and hybrid vehicle) to achieve an 80 percent probability of detecting emission reductions and fuel efficiency improvements at a confidence level of 95 percent

Expected emission reduction or fuel efficiency improvement	5%	20%	50%	85%
Variability for baseline conventional vehicle NO _x measurement ^b	2.58%	2.58%	2.58%	2.58%
Variability for hybrid vehicle NO _x measurement (assumed to be same as for conventional vehicle)	2.58%	2.58%	2.58%	2.58%
Number of tests required to have 80 percent probability of detecting expected NO _x emission reduction ^a	5	2	2	2
Variability for baseline conventional vehicle fuel efficiency measurement (MPG) ^b	2.46%	2.46%	2.46%	2.46%
Variability for hybrid vehicle fuel efficiency measurement (MPG) (assumed to be same as for baseline conventional vehicle)	2.46%	2.46%	2.46%	2.46%
Number of tests required to have 80 percent probability of detecting expected fuel efficiency improvement ^a	5	2	2	2

^a Computed under the assumption of normally distributed measurements having known variability. Additional tests may be required if sample standard deviations obtained during testing are higher.

^b Computed from standard deviation values from actual track testing of diesel trucks. Citation: ____.

The fifth through the seventh rows (shaded) repeat the calculation for the fuel efficiency measurement. Table 1 shows that, for both NO_x and fuel efficiency, six tests are sufficient to distinguish between zero and emission reductions/fuel efficiency improvements as low as 5 percent, based on the assumption that the variability values in Table x represent the true variability values. Two tests would be sufficient to detect the other emission reductions/fuel efficiency improvements, but three are required by this protocol to provide a measured standard deviation.

14.3 Number of Test Runs for Chassis Dynamometer Test

This protocol requires that sufficient tests be conducted to have a high probability of detecting the emission reductions/fuel efficiency improvements expected by the applicant. This requirement was implemented to ensure, as much as was practical, that the test program will accomplish the applicant's goals. This requirement will generally

only be important to testing intended to measure low emission reductions/fuel efficiency improvements and/or measurements having high variability.

Specifically, the test program is to be designed such that there is an 80% probability of detecting the emission reductions/fuel efficiency improvements expected by the applicant, computed from the expected experimental variability for the various measurements. In this context, “detecting” means that the 95% confidence interval does not include zero emissions reduction or zero fuel efficiency improvement. Insufficient replication can result in inability to detect a statistically significant benefit of a change in fuel consumption, as illustrated below with a specific example of a hybrid technology.

A sample-size equation was derived to explicitly compute the number of tests required for normally distributed measurements having known standard deviations. However, since the actual testing procedure will be based on sample standard deviations and t-statistics, a correction factor was applied to the sample-size equation to account for the extra variation in the t-distribution relative to that of the normal distribution. Some results of applying that calculation are presented in Table 2 for particulate matter (PM) and NO_x emission reductions. The equation used to compute the number of tests required is presented in Appendix C.

In Table 2 the baseline conventional vehicle is assumed to be operating at a fixed emission value for PM (top half of table) and NO_x (bottom three rows). PM and NO_x measurements are used in Table 2 because dynamometer laboratory-based measurement standard deviations were known from previous work. The results in Table 2 are based on the sample-size equation with the correction factor for the t-distribution. More tests than shown in Table 2 may be required under conditions of higher variability, and careful examination of the number of tests needed will be required during test/QA plan development.

The column headings in the first row of the PM and NO_x sections of the table give the assumption that the hybrid vehicle will show emissions reductions of 5%, 20%, 50%, or 85% from the baseline conventional vehicle emissions levels. In developing the Test/QA plan, selection of this value will be based on the applicant’s experience and expectation. The second row gives the constant and known baseline conventional vehicle variability. The third row is the assumed measurement variability for the hybrid vehicle based on the variability of the conventional vehicle. (Variability is expressed as the known standard deviation at the emission level divided by the corresponding conventional vehicle mean emission and multiplied by 100%.) The fourth row gives the calculated number of tests required to have 80% probability that the 95% confidence interval about the mean expected emission reduction would not include zero.

Table xx. Number of replicate chassis dynamometer tests (for both conventional and hybrid vehicle) to achieve an 80% probability of detecting emission reductions at a confidence level of 95%

Expected emission reduction (relative to the respective 1990 certification levels for PM and NO _x , respectively)	5%	20%	50%	85%
Variability of baseline conventional vehicle PM measurement ^c	2%	2%	2%	2%
Variability of hybrid vehicle PM measurement (assumed to be the same as for conventional vehicle)	2%	2%	3%	10%
Number of tests required to have 80% probability of detecting expected PM emission reduction ^a	4	2	2	2
Variability for conventional vehicle NO _x measurement at 1990 levels ^c	2%	2%	2%	2%
Variability of hybrid vehicle NO _x measurement (assumed to be the same as for conventional vehicle)	2%	2%	7%	NA ^b
Number of tests required to have 80% probability of detecting expected NO _x emission reduction ^a	4	2	2	NA ^b

^a Computed under the assumption of normally distributed measurements having known variability. Additional tests may be required if sample standard deviations obtained during testing are higher.

^b NA = Not Available.

^c Variability of emission measurements from a chassis dynamometer is assumed to be the same as historical data from an engine dynamometer laboratory running a baseline uncontrolled engine and the same engine with add-on emission control technologies offering varying levels of control.

The fifth through the seventh rows (shaded) repeat the calculation for the NO_x measurement. No estimate of variability was available for the NO_x measurement at an 85% reduction. Table xx shows that, for both PM and NO_x, five tests are sufficient to distinguish between zero and emissions reductions as low as 5%, based on the assumption that the variability values in Table 2 represent the true variability values. Two tests would be sufficient to detect the other emissions reductions, but three are required by this protocol to provide a measured standard deviation.

15 Fuel Efficiency Calculation

FUEL CONSUMPTION - GRAVIMETRIC

At the conclusion of a test lap, the portable fuel tank is detached and weighed. The mass of fuel consumed is the difference between the pre-test and post-test mass of the fuel tank and fuel. The volume of fuel is calculated by dividing the mass consumed by the measured density of the fuel:

$$V = m/p$$

Where V is the volume of fuel consumed during the test lap

M is the mass of fuel consumed during the test lap, and

P is the density of fuel as measured using ASTM method D-1298

For calculation of fuel efficiency from gravimetric data conversion factors are involved, as the data are in mass units, but fuel efficiency is expressed in volumetric units (mi/gal or k/L). SAE J1321, §A.3 describes the method of calculation and supplies the conversion factors.

FUEL CONSUMPTION – CARBON-BALANCE

Fuel consumption can be measured by the carbon balance method, using data from the exhaust gas analysis as described in SAE standard J1094a. This method calculates fuel consumption from measured emissions of carbon-bearing gases. The calculations require input of the emission rates (in grams/mile) of the total hydrocarbons (THC), carbon monoxide (CO), and carbon dioxide (CO₂).

These emissions can be measured using a conventional laboratory test cell or a portable emissions monitoring system (PEMS). The laboratory test cell can only be used to measure emissions of vehicles tested on a chassis dynamometer, whereas the PEMS can be used to measure emissions of both dynamometer and track tests. The method of calculation of fuel efficiency from emissions data shall be consistent with the procedure described for automobiles in 40 CFR 600.113-93.

DISTANCE DRIVEN

Distance driven may be determined either by use of the vehicle odometer, or by the use of global positioning system (GPS) data. The use of GPS data would be applicable only to track tests.

MASS-DISTANCE SPECIFIC METRICS

In some circumstances it might be appropriate to report the results in mass-distance specific form, that is in a metric such as ton-miles per gallon. In most cases, this is not necessary because the test payload is standardized, which means that the payload mass remains a constant percentage of the maximum payload. However, if a truck is designed to improve fuel efficiency through reduction of weight, it is possible that the maximum payload will increase and thus the test payload, expressed as a percent of maximum payload would also increase. In such a case, it would be informative to have the metric reflect this increased efficiency. Reporting of a mass-distance specific metric, however, should be accompanied with all relevant information about payloads and percent of maximum payload.

16 Reporting and Documentation

This section describes the procedures for reporting data, including what data must be included and what format should be used.

16.1 Reports

The test report will contain the following topics:

1. Introduction;

2. Description and identification of vehicle tested. Refer to SAE J2711 §6.2 and SAE J1321 Type II Test Data Form 1;
3. Procedures and methods used in testing. Refer to SAE J1321 Type II Test Data Forms 2-2 and 2-4;
4. Statement of operating range over which the test was conducted;
5. Discussion of results including:
 - a. Explanation and documentation of necessary deviations from the protocol, and
 - b. Discussion of QA issues;
6. References; and
7. Appendices:
 - a. QA/QC activities and results,
 - b. Raw test data, and
 - c. Equipment calibration results.

16.2 Data and Metrics

The primary data collected is units of fuel consumption over units of time, distance, or power. The mean of the test replicates and confidence limits shall be presented. The carbon balance measurement method provides a methodology to convert carbon mass to fuel consumed.

Metrics may include a fuel consumption rate per distance (gallons per mile) and/or per time (gallons per hour). The fuel consumption per time metric accommodates vocational trucks that consume fuel while conducting non-tractive mission work (operating a refuse truck side arm and compacting trash; operating a utility aerial lift and supplying power to the grid). This metric may be weighted into the fuel consumed per distance metric for convenience and ease of comparison, using an appropriate weighting for that vehicle application, which would be described in the “drive cycle.” For over-the-road freight truck applications like highway line haul and regional haul, a gallon per ton-mile metric, as described in the previous section, “mass-distance specific metrics,” may be most reasonable, since the main function of these vehicles is to carry tonnage. This metric could be readily calculated using the test results of fuel consumption, distance, and payload factors in the drive cycle.

If a testing organization wishes to collect emissions data other than carbon, this data shall be reported as emission rates in grams/kilowatt-hour (g/kW-h) [grams/brake horsepower-hour (g/bhp-hr)], grams/mile (g/mi) [grams/kilometer (g/km)] or as grams per cycle, depending on the test method (track or chassis) and the user’s decision as to which is the most appropriate.

16.3 Quality Assurance and Control

Quality assurance and quality control procedures are used to ensure the accuracy and precision of test results. Accuracy of fuel consumption measurements is primarily dependent on the accuracy of the following measurements:

- For fuel consumption measured by carbon-balance method:
 - Accuracy of gas analyses for CO₂, CO and HC
 - Accuracy of exhaust flow determination
 - Accuracy of fuel carbon and density
- For fuel consumption measured by gravimetric method:
 - Accuracy of scales used to weigh fuel
 - Accuracy of measurements of fuel density and temperature correction
- For tests conducted on a dynamometer
 - Accuracy of dynamometer force simulation
 - Accuracy of estimates of road load and aerodynamic drag
 - Accuracy of speed and distance measurements
- For tests conducted on a test track
 - Accuracy of speed measurements
 - Accuracy of distance measurements

Accuracy of these measurements is primarily documented by the use of calibration of the instruments and other measuring devices against known standards. The specific calibration details for the measurements needed are given in the appropriate test descriptions, including SAE and ASTM test method documentation of the relevant parts of the Code of Federal Regulations.

In addition to such documentation, the accuracy of the fuel efficiency metric can be directly tested by comparison of standardized reference trucks, for which the fuel efficiency has been tested multiple times by multiple laboratories.

The short-term precision of a fuel efficiency test method is estimated by use of replicate tests. The acceptable level of precision is determined by the final user of the test results, and sufficient replicate measurements should be taken to ensure that the acceptable level of precision can be documented.

Quality assurance activities should be documented by the following:

- Standard Operating Procedures to ensure that test procedures are done properly
- Records of instrument calibrations
- Records of replicate tests and calculations of precision estimates
- Records of calculations of fuel efficiency
- Daily test log that documents all testing activities, including anomalous behavior and events that could affect test results.

16.4 Assessment

Each testing organization should conduct an internal assessment of its quality and technical systems and should allow external assessments of these systems by QA personnel. After an assessment, the testing organization will be responsible for developing and implementing corrective actions in response to the assessment's findings.

As appropriate, an organization with oversight responsibilities may conduct assessments to determine the testing organization's compliance with its test/QA plan. Examples of assessments are described in EPA's ETV QMP.³⁰ It is highly recommended that assessments be conducted with a rigor comparable to those described in EPA's *Guidance on Technical Audits and Related Assessment for Environmental Data Operations*³¹ and *Guidance on Assessing Quality Systems*.³²

17 Appendices

17.1 Appendix A

Abbreviations and Acronyms

ACEEE	American Council for an Energy Efficient Economy
bhp	brake horsepower
Btu	British thermal unit
CARB	California Air Resources Board
CBI	confidential business information
cfm	cubic feet per minute
CFR	Code of Federal Regulations
CO	carbon monoxide
CO ₂	carbon dioxide
cu. yd.	cubic yard
DQO	data quality objective
EPA	Environmental Protection Agency
EPAct 2005	Energy Policy Act of 2005
ETV	Environmental Technology Verification Program
ft	feet
FTA	Federal Transit Administration
FTP	federal test procedure
gal	gallon
g/mi	grams per mile
g/bhp-hr	grams per brake horsepower-hour
g/kWh	grams per kilowatt-hour
GVWR	gross vehicle weight rating
H/C ratio	Hybrid Vehicle Fuel Used/Comparable Baseline Vehicle Fuel Used
HAP	hazardous air pollutant
HDHV	heavy duty hybrid vehicle
hp	horsepower
HVAC	heating, ventilation, and air conditioning
in	inches
IRS	Internal Revenue Service
km	kilometer
L	liter
lb	pound
mph	miles per hour
NEC	net energy change
NO	nitric oxide
NO ₂	nitrogen dioxide
NO _x	nitrogen oxides
NREL	National Renewable Energy Laboratory
NYCT	New York City Transit
OBD	on-board diagnostics
ORD	Office of Research and Development
OTAQ	Office of Transportation and Air Quality

PEMS portable emissions monitoring system
PM particulate matter
[Reserved]

17.2 – 17.8 Appendices B – H

[Reserved]

17.9 Appendix I

Statistics – Test Track Testing

Example Sample Size Calculation for Emission Reduction

This appendix presents sample calculations for determining the minimum number of tests required to detect a significant emissions or fuel consumption reduction. The calculation is based on:

- 1) The emissions variability is taken to be known for the population of measurements;
- 2) A known baseline conventional vehicle mean emission;
- 3) A mean hybrid vehicle emission (the product of the conventional vehicle emission and the expected emissions reduction); and
- 4) One part of the equation is based on the assumption of known standard deviations and the normal distribution. However, since the actual testing procedure is based on sample standard deviations and t-statistics, a correction factor is added to the sample-size equation to account for the extra variation in the t-distribution relative to that of the normal distribution.

The criterion being used is that the minimum number of tests required for use of this protocol is the number of tests required to have an 80% probability of detecting the specified emission reduction at the 95% confidence level. The basic equation being used for the calculation is:

$$n \approx (z_\alpha + z_\beta)^2 \left[\sigma_H^2 + \sigma_C^2 (1 - \delta/100)^2 \right] / \delta^2 + z_\alpha^2 / 2 \quad (\text{C-1})$$

where:

- n = sample size in each group, rounded up to the next integer;
- z_α = normal distribution value corresponding to upper-tail probability of α ;
and
- z_β = normal distribution value corresponding to upper-tail probability of β .
- $1 - \alpha$ = confidence coefficient on comparison of means (0.95 minimum);
- $1 - \beta$ = probability of detection of reduction/increase (0.80 minimum);
- σ_C^2 = squared standard deviation of conventional vehicle emission data,
expressed as a percent of the conventional vehicle emission value;
- σ_H^2 = squared standard deviation of hybrid vehicle emission data, expressed as a
percent of the conventional vehicle emission value;
- δ = difference between conventional and hybrid vehicle emissions mean,
expressed as a percent of the conventional vehicle emission value.

Note that σ_C^2 , σ_H^2 , and δ are expressed as percentages of the conventional vehicle emission. This transformation was used to simplify the equation and allow its use for Table 1 in Section 5.3.1. For Table 1, the baseline conventional vehicle mean emission value was 12.495 grams/mile, taken from the suburban drive cycle of the Kenworth data.¹ The parameter ‘z’ is tabulated under different names in statistics reference texts. It is the ‘z’ value corresponding to ‘the tail area of the unit normal distribution’ in Box, Hunter, and Hunter (1978). In the Standard Mathematical Tables (CRC, 1968), ‘z’ is known as ‘x’, and the tail area is labeled ‘1 – F(x)’, where F(x) is the cumulative distribution function of a standardized normal random variable. To obtain the value of ‘z’ from the statistical tables, α (or β) is the probability (ranging from 0.5000 to 0.0000) in the body of the table, and ‘z’ is read (or interpolated) from the appropriate column and/or row, ranging from 0.00 to 4.00 over that range. The value ‘z’ can be calculated within an EXCEL[®] or QUATTRO PRO[®] spreadsheet as the absolute value of the function returning the inverse of the standard normal cumulative distribution, NORMSINV(probability), by setting probability equal to α or β , as appropriate. A derivation of the correction factor, $z_\alpha^2/2$, is available in Appendix A of the EPA G-4 guidance document (*Guidance on the Data Quality Objectives Process* (EPA/600/R-96/055)).

Table C-1 gives a step-by-step calculation example drawn from Table 1 for an 80% probability ($\beta = 0.20$) of detecting a 5% and a 50% emission reduction at the 95% confidence level ($\alpha = 0.05$).

¹ _____ Proper citation is needed, here, for the Kenworth truck testing dataset.

Table C-1. Example calculation of minimum number of replicate test track tests required to achieve an 80% probability of detecting emission reductions at a confidence level of 95%.

	Table 1, Col.1	Table 1, Col. 3
Emission reduction relative to conventional vehicle emission, δ , %	5	50
Known measurement variability for conventional vehicle, σ_C , %	2.58	2.58
Known measurement variability for hybrid vehicle, σ_H , %	2.58	2.58
α	0.05	0.05
z_α	1.645	1.645
β	0.20	0.20
z_β	0.842	0.842
$\left[\sigma_H^2 + \sigma_C^2 (1 - \delta/100)^2 \right] / \delta^2$	0.514	0.003
$(z_\alpha + z_\beta)^2 \left[\sigma_H^2 + \sigma_C^2 (1 - \delta/100)^2 \right] / \delta^2$	3.18	0.02
$z_\alpha^2 / 2$	1.35	1.35
$(z_\alpha + z_\beta)^2 \left[\sigma_H^2 + \sigma_C^2 (1 - \delta/100)^2 \right] / \delta^2 + z_\alpha^2 / 2$	4.53	1.37
Number of tests required ^a , n	5	2 ^a

Note: ^a The minimum number of tests is three. If 'n' is less than three, 'n' equals three.

Example Sample Size Calculation for Fuel efficiency Improvement

This appendix presents example calculations to illustrate calculation of the minimum number of tests required to detect a significant fuel efficiency improvement.

The calculation is based on:

- 1) The fuel efficiency variability is taken to be known for the population of measurements;
- 2) A known baseline conventional vehicle mean fuel efficiency;
- 3) A mean hybrid vehicle fuel efficiency; and
- 4) One part of the equation is based on the assumption of known standard deviations and the normal distribution. However, since the actual testing procedure is based

on sample standard deviations and t-statistics, a correction factor is added to the sample-size equation to account for the extra variation in the t-distribution relative to that of the normal distribution.

The criterion being used is that the minimum number of tests required for use of this protocol is the number of tests required to have an 80% probability of detecting the specified fuel efficiency increase at the 95% confidence level. The basic equation being used for the calculation is:

$$n \approx (z_\alpha + z_\beta)^2 \left[\sigma_H^2 + \sigma_C^2 (1 + \delta / 100)^2 \right] / \delta^2 + z_\alpha^2 / 2 \quad (\text{C-1})$$

where:

- n = sample size in each group, rounded up to the next integer;
- z_α = normal distribution value corresponding to upper-tail probability of α ;
- and
- z_β = normal distribution value corresponding to upper-tail probability of β .
- $1 - \alpha$ = confidence coefficient on comparison of means (0.95 minimum);
- $1 - \beta$ = probability of detection of reduction/increase (0.80 minimum);
- σ_C^2 = squared standard deviation of conventional vehicle fuel efficiency data, expressed as a percent of the conventional vehicle fuel efficiency value;
- σ_H^2 = squared standard deviation of hybrid vehicle fuel efficiency data, expressed as a percent of the conventional vehicle fuel efficiency value;
- δ = difference between conventional and hybrid vehicle fuel efficiency mean, expressed as a percent of the conventional vehicle fuel efficiency value.

Note that σ_C^2 , σ_H^2 , and δ are expressed as percentages of the conventional vehicle fuel efficiency. This transformation was used to simplify the equation and allow its use for Table 1. The parameter 'z' is tabulated under different names in statistics reference texts. It is the 'z' value corresponding to 'the tail area of the unit normal distribution' in Box, Hunter, and Hunter (1978). In the Standard Mathematical Tables (CRC, 1968), 'z' is known as 'x', and the tail area is labeled '1 - F(x)', where F(x) is the cumulative distribution function of a standardized normal random variable. To obtain the value of 'z' from the statistical tables, α (or β) is the probability (ranging from 0.5000 to 0.0000) in the body of the table, and 'z' is read (or interpolated) from the appropriate column and/or row, ranging from 0.00 to 4.00 over that range. The value 'z' can be calculated within an EXCEL[®] or QUATTRO PRO[®] spreadsheet as the absolute value of the function returning the inverse of the standard normal cumulative distribution, NORMSINV(probability), by setting probability equal to α or β , as appropriate. A derivation of the correction factor, $z_\alpha^2 / 2$, is available in Appendix A of the EPA G-4

guidance document (*Guidance on the Data Quality Objectives Process* (EPA/600/R-96/055)).

Table C-2 gives a step-by-step calculation example drawn from Table 1 for an 80% probability ($\beta = 0.20$) of detecting a 5% and a 50% fuel efficiency increase at the 95% confidence level ($\alpha = 0.05$).

Table C-2. Example calculation of minimum number of tests.

	Table 1, Col.1	Table 1, Col. 3
Fuel efficiency increase relative to conventional vehicle fuel efficiency, δ , %	5	50
Known measurement variability for conventional vehicle, σ_C , %	2.46	2.46
Known measurement variability for hybrid vehicle, σ_H , %	2.46	2.46
α	0.05	0.05
z_α	1.645	1.645
β	0.20	0.20
z_β	0.842	0.842
$\left[\sigma_H^2 + \sigma_C^2 (1 + \delta/100)^2 \right] / \delta^2$	0.509	0.003
$(z_\alpha + z_\beta)^2 \left[\sigma_H^2 + \sigma_C^2 (1 + \delta/100)^2 \right] / \delta^2$	3.15	0.02
$z_\alpha^2 / 2$	1.35	1.35
$(z_\alpha + z_\beta)^2 \left[\sigma_H^2 + \sigma_C^2 (1 + \delta/100)^2 \right] / \delta^2 + z_\alpha^2 / 2$	4.50	1.37
Number of tests required ^a , n	5	2 ^a

Note: ^a The minimum number of tests is three. If 'n' is less than three, 'n' equals three.

Statistics – Chassis Dynamometer Testing

The calculations for the minimum number of tests required to detect a significant emissions reduction or fuel efficiency increase are identical to those presented in the preceding section.

Based on the calculations presented in the preceding section, Table D-1 gives a step-by-step calculation example drawn from Table 2 of Section 5.3.2 for an 80% probability ($\beta =$

0.20) of detecting a 5% and a 50% emission reduction at the 95% confidence level ($\alpha = 0.05$).

Table D-1. Example calculation of minimum number of replicate chassis dynamometer tests to achieve an 80% probability of detecting emissions reductions at a confidence limit of 95%.

	Table 2, Col.1	Table 2, Col. 3
Emission reduction relative to conventional vehicle emission, δ , %	5	50
Known measurement variability for conventional vehicle, σ_C , %	2	2
Known measurement variability for hybrid vehicle, σ_H , %	2	3
α	0.05	0.05
z_α	1.645	1.645
β	0.20	0.20
z_β	0.842	0.842
$\left[\sigma_H^2 + \sigma_C^2 (1 - \delta/100)^2 \right] / \delta^2$	0.304	0.004
$(z_\alpha + z_\beta)^2 \left[\sigma_H^2 + \sigma_C^2 (1 - \delta/100)^2 \right] / \delta^2$	1.88	0.02
$z_\alpha^2 / 2$	1.35	1.35
$(z_\alpha + z_\beta)^2 \left[\sigma_H^2 + \sigma_C^2 (1 - \delta/100)^2 \right] / \delta^2 + z_\alpha^2 / 2$	3.23	1.38
Number of tests required ^a , n	4	2 ^a

Note: ^a The minimum number of tests is three. If 'n' is less than three, 'n' equals three.

References

- CRC. Standard Mathematical Tables, 16th Ed. S. Shelby, Ed. The Chemical Rubber Company, Cleveland, OH. 1968.
- Box, G. E. P., W. G. Hunter, and J. S. Hunter. *Statistics for Experimenters*. John Wiley & Sons, New York, NY. 1978.
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17.10 Appendix J

Calculations to Compare the Hybrid Version of a Heavy Duty Vehicle to the Non-Hybrid Version

Comparative testing of a hybrid vehicle to its non-hybrid “twin,” whether the testing is conducted on a test track or on a chassis dynamometer, involves multiple tests of a baseline conventional vehicle and multiple tests of a hybrid vehicle. This section describes the data analysis procedure that will be used to calculate the emission reductions and increase in fuel efficiency from these data.

This calculation assumes that the same test method (test track or chassis dynamometer) is used for all the testing.

Procedure for Calculating Emission Reduction

Let E_C and E_H refer to the emission rates of a single pollutant for conventional and hybrid vehicles, respectively. Once the E values for the tests are available, the corresponding sample means (\bar{E}_C and \bar{E}_H) and standard deviations (s_C and s_H) are computed using Equations 2 and 3.

$$\bar{E}_C = \frac{\sum_{i=1}^{n_C} E_{C,i}}{n_C} \quad \text{and} \quad \bar{E}_H = \frac{\sum_{i=1}^{n_H} E_{H,i}}{n_H} \quad (2)$$

$$s_C = \sqrt{\sum_{i=1}^{n_C} (E_{C,i} - \bar{E}_C)^2 / (n_C - 1)} \quad \text{and} \quad s_H = \sqrt{\sum_{i=1}^{n_H} (E_{H,i} - \bar{E}_H)^2 / (n_H - 1)} \quad (3)$$

where:

\bar{E}_C = mean emission rate for the conventional vehicle for a single pollutant,

\bar{E}_H = mean emission rate for the hybrid vehicle for a single pollutant,

$E_{C,i}$ = emission rate for a single conventional i^{th} test for a single pollutant,

$E_{H,i}$ = emission rate for a single hybrid i^{th} test for a single pollutant,

n_C and n_H = number of conventional and hybrid tests, and

s_C and s_H = standard deviations of conventional and hybrid tests.

The raw emission reduction for each pollutant, ER_{RAW} , is then computed as the difference between the mean emission rates for the conventional and hybrid cases, divided by the conventional case mean emission rate, as shown in Equation 4.

$$ER_{RAW} = (\bar{E}_C - \bar{E}_H) / \bar{E}_C \quad (4)$$

The upper and lower bounds of the approximate confidence interval (CI) around ER_{RAW} are computed using Equations 5a and 5b.

$$CI \text{ (upper bound)} = ER_{RAW} + \left\{ \left(t_{\alpha/2} \cdot \sqrt{\frac{s_H^2}{n_H} + (1 - ER_{RAW})^2 \frac{s_C^2}{n_C}} \right) / \bar{E}_C \right\} \quad (5a)$$

$$CI \text{ (lower bound)} = ER_{RAW} - \left\{ \left(t_{\alpha/2} \cdot \sqrt{\frac{s_H^2}{n_H} + (1 - ER_{RAW})^2 \frac{s_C^2}{n_C}} \right) / \bar{E}_C \right\} \quad (5b)$$

In the equations above, $t_{\alpha/2}$ is the $(1 - \alpha/2)$ percentile of the t-distribution, with degrees of freedom, ν , given by Equation 6 (rounded down)², and $\alpha = 1 - (\text{confidence level} / 100\%)$. However, since the testing procedure is interested only in unidirectional *positive* reductions, one-tailed tests will be conducted. Consequently, only the lower bound of the confidence interval will be of interest, and t_α will replace $t_{\alpha/2}$ in Equation 5b. Thus, in tables giving distributions of t for two-tailed tests, use 2α to obtain the critical value. For example, if the confidence level is 95%, then $\alpha = 0.05$; if in addition, $\nu = 5$, then $t_\alpha = 2.015$.

$$\nu = \frac{\left[s_H^2 / n_H + (1 - ER_{RAW})^2 s_C^2 / n_C \right]^2}{\left[(s_H^2 / n_H)^2 / (n_H - 1) \right] + (1 - ER_{RAW})^4 \left[(s_C^2 / n_C)^2 / (n_C - 1) \right]} \quad (6)$$

The fractional values of emission reduction and the confidence intervals are converted to percentages by multiplying by 100 percent.

5.2.2.2 Procedure for Calculating Fuel efficiency Improvement

Let F_C and F_H refer to the fuel efficiency rates in miles per gallon (MPG) for baseline conventional and hybrid vehicles, respectively. Once the F values for the tests are available, the corresponding sample means (\bar{F}_C and \bar{F}_H) and standard deviations (s_C and s_H) are computed using Equations 2 and 3, except that F_C and F_H values are used instead of E_C and E_H values in the formulas.

The raw fuel efficiency increase, FI_{RAW} , is then computed as the difference between the mean fuel efficiency rates for the hybrid and conventional cases, divided by the baseline conventional case mean fuel efficiency rate, as shown in Equation 7.

$$FI_{RAW} = (\bar{F}_H - \bar{F}_C) / \bar{F}_C \quad (7)$$

² The value of ν rounded down from Equation 9 can generally be approximated as $n_C + n_H - 3$.

The upper and lower bounds of the approximate confidence interval (CI) around FI_{RAW} are computed using Equations 8a and 8b.

$$CI \text{ (upper bound)} = FI_{RAW} + \left\{ \left(t_{\alpha/2} \cdot \sqrt{\frac{s_H^2}{n_H} + (1 + FI_{RAW})^2 \frac{s_C^2}{n_C}} \right) / \bar{F}_C \right\} \quad (8a)$$

$$CI \text{ (lower bound)} = FI_{RAW} - \left\{ \left(t_{\alpha/2} \cdot \sqrt{\frac{s_H^2}{n_H} + (1 + FI_{RAW})^2 \frac{s_C^2}{n_C}} \right) / \bar{F}_C \right\} \quad (8b)$$

In the equations above, $t_{\alpha/2}$ is the $(1 - \alpha/2)$ percentile of the t-distribution, with degrees of freedom, ν , given by Equation 9 (rounded down)³, and $\alpha = 1 - (\text{confidence level} / 100\%)$. However, since the testing procedure is interested only in unidirectional *positive* increases, one-tailed tests will be conducted. Consequently, only the lower bound of the confidence interval will be of interest, and t_α will replace $t_{\alpha/2}$ in Equation 5b. Thus, in tables giving distributions of t for two-tailed tests, use 2α to obtain the critical value. For example, if the confidence level is 95%, then $\alpha = 0.05$; if in addition, $\nu = 5$, then $t_\alpha = 2.015$.

$$\nu = \frac{\left[s_H^2 / n_H + (1 + FI_{RAW})^2 s_C^2 / n_C \right]^2}{\left[(s_H^2 / n_H)^2 / (n_H - 1) \right] + (1 + FI_{RAW})^4 \left[(s_C^2 / n_C)^2 / (n_C - 1) \right]} \quad (9)$$

The fractional values of emission reduction and the confidence intervals are converted to percentages by multiplying by 100 percent.

³ The value of ν rounded down from Equation 9 can generally be approximated as $n_C + n_H - 3$.

17.11 Appendix K

Drive Cycles: Time-Speed-Distance Data and Summary Statistics

[Reserved]

18 Endnotes

¹ The primary use of SAE J1321 is to measure the fuel economy impact of various truck components. The percent fuel economy improvement approach is well-suited to this purpose.

² A hybrid vehicle can generally be defined as a vehicle in which the motive power comes from two sources: a consumable fuel converter (e.g., internal combustion engine) and a rechargeable energy storage system (RESS).

³ Line haul and regional combination tractor-trailers use more fuel than all other heavy duty on-highway vehicles combined, due to high annual mileage, and have significant potential to save fuel by reducing aerodynamic and rolling drag. Intermodal drayage trucks contribute significantly to CO₂ and other emissions in and around marine port facilities. The remaining heavy duty vehicles included in this initial version have strong near-term potential to realize significant fuel savings by adopting hybrid technology.

⁴ SAE International, *Constant Volume Sampler System for Exhaust Emissions Measurement* – SAE Surface Vehicle Standard J1094, 1992.

⁵ Preliminary testing indicates dynamometer to track differences of about 4% with coupled dynamometer rolls (10% with uncoupled rolls), on passenger vehicles. This difference may be explained by tire/surface interactions. However, both track and chassis dynamometer tests demonstrated directionally consistent and statistically equivalent differences to changes in drive cycle for various vehicles. US Environmental Protection Agency, Dynamometer and Track Measurement of Car Fuel Economy - EPA-460/3-81-002, March, 1981.

⁶ Only a few chassis dynamometers exist that can accommodate tractor-trailer combination trucks. Also, track tests directly factor aerodynamic effects; for the highway-speed drive cycles typical of trailer-tractor combination trucks, aerodynamic effects can have a significant impact on fuel consumption.

⁷ However, it has been demonstrated that even tests conducted in laboratories have differences in repeatability within a given laboratory and differences in reproducibility among laboratories. Reference “Interlaboratory Crosscheck of Heavy duty Vehicle Chassis Dynamometers” Final Report CRC Project No. E-55-1, May, 2002.

⁸ The transient drive cycles typical of single unit or truck body heavy duty vehicles are likely to be more easily replicated on a chassis dynamometer than on a test track. A reasonable number of chassis dynamometer facilities exist to accommodate lighter-weight single unit or truck body heavy duty vehicles, partly because the federal government established an optional chassis dynamometer emissions certification test for engines used in heavy duty vehicles up to 14,000 pounds GVWR.

⁹ SAE J1321 is a paired-truck test. This test procedure is single truck test. Therefore, for the SAE J1321 cites in this document, ignore references to two test vehicles.

¹⁰ To be comparable, each vehicle must be able to accomplish the same functions, with similar performance, utility, and durability attributes. In certain instances, comparability may require selecting test vehicles produced by the same manufacturer. In other instances, comparability may mean selecting test vehicles that are close competitors within the same market niche. A test vehicle can be from a previous year relative to the comparison vehicle, if the engine is functionally unchanged between the two years and if

all other vehicle characteristics are substantially similar, with the exception of the design options being tested.

¹¹ If a hand held wind indicator is used, it must have an accuracy equivalent to the wind-sensing equipment available from Edmund Scientific Company, Barrington, NJ, or Dwyer Instrument, Inc., Michigan City, IN.

¹²

¹³ Use the correlation guidance established by EPA in its chassis dynamometer emissions testing [get cite].

¹⁴ SAE Recommended Practice J2263. *Road Load Measurement Using Onboard Anemometry and Coastdown Techniques*. October 1996.

¹⁵ SAE Procedure J2264. *Chassis Dynamometer Simulation of Road Load Using Coastdown Techniques*, April, 1995.

¹⁶ SAE International, *Constant Volume Sampler System for Exhaust Emissions Measurement* SAE Surface Vehicle Information Report J1094, revised June, 1992

¹⁷ Long-duration idling is not addressed in this drive cycle, since the objective is to measure on-road fuel economy. If idling fuel consumption is desired, the ARB idle mode test is recommended. There are many alternatives to overnight idling. These include truck stops that offer shore power (and HVAC); on-board auxiliary power units (APUs); driver tag-teams. Strategies to reduce overnight idling can be found at <http://www.epa.gov/smartway/idling.htm>.

¹⁸ [reserved - ARB drive cycle cite]

¹⁹ See SAE 2002-01-1753, *Development and Initial Use of a Heavy duty Diesel Truck Test Schedule for Emissions Characterization*, Mridul Gautam, et al., and SAE 2006-01-3474 *Fuel Economy Improvements and NOx Reduction by Reduction of Parasitic Losses: Effect of Engine Design*, L. Joseph Bachman, et al.

²⁰ SAE Surface Vehicle Information Report J1343, *Information Relating to Duty Cycles and Average Power Requirements of Truck and Bus Engine Accessories*, August, 2000; SAE SAE J1341, *Test Method for Measuring Power Consumption of Hydraulic Pumps for Trucks and Buses*, July, 1981; SAE J1339, *Test Method for Measuring Power Consumption of Truck and Bus Engine Fans*, August, 2002; and, Southwest Research Institute Final Letter Report, *Emissions and Fuel Economy Testing of Three Utility Trucks*, SwRI Project No. 03.11602, September, 2005.

²¹ Average payload for class 8 over-the-road freight carriers in EPA SmartWay Transport Partnership.

²² SAE Surface Vehicle Recommended Practice, *Recommended Practice for Measuring Fuel Economy and Emissions of Hybrid-Electric and Conventional Heavy duty Vehicles*, SAE J2711, September, 2002.

²³ For a typical 5-axle tractor-trailer combination truck, applicable federal over-axle limits are 12,000 pounds on the steer axle, and 34,000 each on the drive and trailer axles, respectively.

²⁴ §3.7 of the SAE Surface Vehicle Recommended Practice, *Recommended Practice for Measuring Fuel Economy and Emissions of Hybrid-Electric and Conventional Heavy duty Vehicles*, SAE J2711, September, 2002,

²⁵ SAE J1711 §3.7, points out that to measure a fuel consumption value that is within $\pm 3\%$ of the vehicle's true, representative fuel consumption the change in energy stored in the RESS must be less than $\pm 1\%$ of the total fuel energy consumed over the test cycle.

²⁶ The value of k for a gas varies with pressure; the variation is significant at high pressures. EPA experimenters at the National Fuel and Vehicle Emissions Laboratory have found that a value of 1.8 yields good results for nitrogen at pressures from 2000 to 5000 pounds per square inch – typical pressures for hybrid hydraulic accumulators. The actual value has little impact on the calculation of NEC, however, if there is little difference between starting and final accumulator pressure, and hence little difference in starting and final SOC.

²⁷ Clark, Nigel N., Xie, Wenwei, Gautam, Mridul, Lyons, Donald W., Norton, Paul, and Balon, Thomas. Hybrid Diesel-Electric Heavy duty Bus Emissions: Benefits of Regeneration and Need for State of Charge Correction. SAE Paper No. 2000-02-2955. Presented at the International Fall Fuels and Lubricants Meeting and Exposition. Baltimore, MD. October 2000.

²⁸ SAE Surface Vehicle Recommended Practice, *Road Load Measurement and Dynamometer Simulation Using Coastdown Techniques*, February, 1996; SAE Surface Vehicle Recommended Practice, *Road Load Measurement Using Onboard Anemometry and Coastdown Techniques*, October, 1996; SAE Surface Vehicle Recommended Practice, *Chassis Dynamometer Simulation of Road Load using Coastdown Techniques*, April, 1995.

²⁹ Southwest Research Institute, *Testing and Analysis Support for the SmartWay Transport Partnership*, Final Report SwRI Project 08.1166.15.101, June, 2006.

³⁰ Op cit. Ref. **Error! Bookmark not defined..**

³¹ U.S. EPA (Environmental Protection Agency). *Guidance on Technical Audits and Related Assessments for Environmental Data Operations*, EPA QA/G-7. EPA/600/R-99/080, <http://www.epa.gov/quality/qs-docs/g7-final.pdf>. Office of Environmental Information, U.S. Environmental Protection Agency. Washington, DC. January 2000.

³² U.S. EPA (Environmental Protection Agency). *Guidance on Assessing Quality Systems*, EPA QA/G-3. EPA/240/R-03/002. <http://www.epa.gov/quality/qs-docs/g3-final.pdf>. Office of Environmental Information, U.S. Environmental Protection Agency. Washington, DC. March 2003.

19. List of Figures and Tables

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