Arsenic Removal from Drinking Water by Adsorptive Media EPA Demonstration Project at Golden Hills Community Services District in Tehachapi, CA Final Performance Evaluation Report

by

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Sally Gutierrez, Director National Risk Management Research Laboratory

ABSTRACT

This report documents the activities performed and the results obtained for the arsenic removal treatment technology demonstration project at Golden Hills Community Services District (GHCSD) located in Tehachapi, CA. The objectives of the project were to evaluate (1) the effectiveness of Magnesium Elektron, Inc.'s (MEI) IsoluxTM treatment system in removing arsenic to meet the new maximum contaminant level (MCL) of 10 μ g/L; (2) the reliability of the treatment system; (3) the required system operation and maintenance (O&M) and operator skill levels; and (4) the capital and O&M cost of the treatment process. The types of data collected included system operation, water quality (both across the treatment train and in the distribution system), process residuals, and capital and O&M cost.

The IsoluxTM arsenic treatment system consisted of two adsorption modules arranged in parallel, capable of treating up to 150 gal/min (gpm) of flow. Each module, designed for 75 gpm, consisted of a booster pump, a 1-µm bag filter, and two 20-in × 48-in carbon-steel filtration vessels, each containing nine IsoluxTM-302M media cartridges. Each media cartridge was 4.55-in in diameter and 42.25-in in length and contained 0.32 ft³ of IsoluxTM-302M–a hydrous zirconium oxide media with amphoteric properties. During the performance evaluation study from October 26, 2005, through March 20, 2007, three media runs were performed, each operating for a total run time of 1,377, 1,900, and 1,422 hr (or 21.9, 20.2, and 16.7 hr/day). Average flowrates for the runs were 79, 74, and 85 gpm. Based on the average flowrates, the empty bed contact times (EBCT) ranged from 0.9 to 1.2 min, compared to the design value of 0.5 min.

Among the 13 active wells at GHCSD, only Well C had elevated arsenic concentrations, which averaged 12.2 μ g/L and existed primarily as soluble As(V). The pH values of raw water ranged from 7.4 to 7.9 and averaged 7.6, which is much lower than the zero point of charge for zirconium hydroxide (i.e., 10 to 11).

During Media Run 1, the system treated approximately 61,600 bed volumes (BV) of water before reaching 10 µg/L arsenic breakthrough. This run length was 41% lower than the vendor's estimated 105,000 BV. An excessive amount of sediment was observed in the well water, necessitating frequent replacement of bag filters prior to the adsorption modules. It was possible that particles passed through the bag filters blocked (or partially blocked) some passages on the media cartridges' outer membrane, causing preferential flow and the short run length observed. Examination of the well revealed rusty areas on the drop-pipe, which prompted a decision by GHCSD to rehabilitate the well.

Following the well rehabilitation and media cartridge changeout, Media Run 2 began on April 27, 2006. The system treated 92,800 BV of water before reaching 10 μ g/L arsenic breakthrough. Since Media Runs 1 and 2 operated under similar conditions, the well rehabilitation might have, in fact, contributed to the more extended media life observed. Following media cartridge changeout, Media Run 3 began on August 17, 2006, and ended on March 20, 2007, with the system operating intermittently due to a lower demand in the winter. The system treated approximately 85,100 BV after reaching 10 μ g/L arsenic breakthrough. Similar run lengths were observed during Media Runs 2 and 3. The intermittent system operation (i.e., 16.7 versus 20.2 hr/day) did not seem to affect the media run length.

The treatment system did not require backwash; therefore, spent media cartridges were the only residue generated. Spent Isolux[™]-302M media passed TCLP tests and therefore could be disposed of as non-hazardous waste. However, MEI opted to send the spent media for beneficial reuse.

Comparison of the distribution system sampling results before and after system startup showed a slight decrease in the average arsenic concentration at each of the three sampling locations (i.e., from 2.8, 6.0, and 5.2 μ g/L to 2.0, 3.3, and 3.1 μ g/L, respectively). Most of the time, arsenic concentrations were much

lower than those of the treatment effluent, presumably due to blending of the treated water with untreated water from wells where arsenic levels were not of concern. Lead and copper concentrations at the three sampling locations did not appear to be significantly impacted by the arsenic treatment system.

The capital investment cost was \$76,840, which included \$58,500 for equipment, \$8,500 for engineering, and \$9,840 for installation. Using the system's rated capacity of 150 gpm, the capital cost was \$512/gpm (or \$0.36/gpd).

The O&M cost for the IsoluxTM system included cost for media cartridge replacement and labor for routine operation. Based on the volumes processed during each media run prior to 10 μ g/L arsenic breakthrough, the total O&M cost, including media cartridge replacement for Media Runs 1, 2, and 3, was \$1.35, \$0.89, and \$0.98/1,000 gal, respectively. Routine activities to operate and maintain the system consumed only 2.5 hr per week. Therefore, the estimated labor cost was \$0.14/1,000 gal of water treated, assuming that the system operates at 79.3 gpm for 19.6 hr/day and 7 days/week to produce 653,000 gal of water per week.

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ABBREVIATIONS AND ACRONYMS

AAL	American Analytical Laboratories
AC	asbestos cement
AM	adsorptive media
As	arsenic
ATS	Aquatic Treatment Systems
bgs	below ground surface
BV	bed volumes
Ca	calcium
CDPH	California Department of Public Health
CEQA	California Environmental Quality Act
Cl	chlorine
C/F	coagulation/filtration
Cu	copper
DO	dissolved oxygen
EBCT	empty bed contact time
EPA	U.S. Environmental Protection Agency
F	fluoride
Fe	iron
GFH	granular ferric hydroxide
GHCSD	Golden Hills Community Services District
gpd	gallons per day
gpm	gallons per minute
HIX	hybrid ion exchanger
hp	horsepower
ICP-MS ID IX	inductively coupled plasma-mass spectrometry identification ion exchange
LCR	Lead and Copper Rule
MCL	maximum contaminant level
MDL	method detection limit
MEI	Magnesium Elektron, Inc.
Mg	magnesium
mgd	mega gallons per day
mg/L	milligrams per liter
μg/L	micrograms per liter
μm	micrometer
Mn	manganese
mV	millivolts

Na	sodium
NA	not available
ND	not detected
NH ₃	ammonia
NO ₂	nitrite
NO ₂	nitrate
NRMRL	National Risk Management Research Laboratory
NSF	NSF International
NTU	nephlemetric turbidity units
	hepinemetre turbianty units
0&M	operation and maintenance
OIT	Oregon Institute of Technology
ORD	Office of Research and Development
ORD	ovidation reduction notantial
UKI	oxidation-reduction potential
DE	nolvethylene
Dh	lend
PO	orthophosphate
POE	noint of ontry
POL	point of entry
POU	point of use
psi	pounds per square inch
PVC	polyvinyl chloride
ΔP	pressure differential
A	
QA	quality assurance
QA/QC	quality assurance/quality control
QAPP	Quality Assurance Project Plan
PO	ravarsa asmosis
	relative percent difference
KFD	relative percent unrelence
SDWA	Safe Drinking Water Act
SD WA	silica
SIO ₂	sulfate
SU4 STS	Savarn Trant Sarvigas
SIS	stendard unit
5.0.	standard unit
ТСІ Р	Toxicity Characteristic Leaching Procedure
TDS	total dissolved solids
TO	toda dissolved solids
TOC	total organic carbon
IOC	total organic carbon
U	uranium
V	vanadium
WET	whole effluent toxicity
VV 12 1	whole efficient toxicity
Zpc	zero point of charge
Zr	zirconium

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1.0 INTRODUCTION

1.1 Background

The Safe Drinking Water Act (SDWA) mandates that U.S. Environmental Protection Agency (EPA) identify and regulate drinking-water contaminants that may have adverse human health effects and are known or anticipated to occur in public water supply systems. In 1975, under the SDWA, EPA established a maximum contaminant level (MCL) for arsenic at 0.05 mg/L. Amended in 1996, the SDWA required that EPA develop an arsenic research strategy and publish a proposal to revise the arsenic MCL by January 2000. On January 18, 2001, EPA finalized the arsenic MCL at 0.01 mg/L (EPA, 2001). To clarify implementation of the original rule, EPA revised the rule text on March 25, 2003, to express the MCL as 0.010 mg/L (10 μ g/L) (EPA, 2003). The final rule required all community and non-transient, non-community water systems to comply with the new standard by January 23, 2006.

In October 2001, EPA announced an initiative for additional research and development of cost-effective technologies to help small-community water systems (<10,000 customers) meet the new arsenic standard and to provide technical assistance to operators of small systems in order to reduce compliance cost. As part of this Arsenic Rule Implementation Research Program, EPA's Office of Research and Development (ORD) proposed a project to conduct a series of full-scale, onsite demonstrations of arsenic removal technologies, process modifications, and engineering approaches applicable to small systems. Shortly thereafter, an announcement published in the *Federal Register* requested water utilities interested in participating in Round 1 of this EPA-sponsored demonstration program to provide information on their water systems. In June 2002, EPA selected 17 out of 115 sites to host the demonstration studies.

In September 2002, EPA solicited proposals from engineering firms and vendors for cost-effective arsenic removal treatment technologies for the 17 host sites. EPA received 70 technical proposals for the 17 host sites, with each site receiving one to six proposals. In April 2003, an independent technical panel reviewed the proposals and provided its recommendations to EPA on the technologies that it determined were acceptable for the demonstration at each site. Because of funding limitations and other technical reasons, only 12 of the 17 sites were selected for the demonstration project. Using the information provided by the review panel, EPA, in cooperation with the host sites and the drinking-water programs of the respective states, selected one technical proposal for each site.

In 2003, EPA initiated Round 2 arsenic technology demonstration projects that were partially funded with Congressional add-on funding to the EPA budget. In June 2003, EPA selected 32 potential demonstration sites, and the community water system at Golden Hills Community Services District (GHCSD) in Tehachapi, CA, was one of those selected.

In September 2003, EPA again solicited proposals from engineering firms and vendors for arsenic removal technologies. EPA received 148 technical proposals for the 32 host sites, with each site receiving from two to eight proposals. In April 2004, EPA convened another technical panel to review the proposals and provide recommendations to EPA; the number of proposals per site ranged from none (for two sites) to a maximum of four. The final selection of the treatment technology at sites receiving at least one proposal was made, again through a joint effort of EPA, the state regulators, and the host site. Since then, four sites have withdrawn from the demonstration program, reducing the number of sites to 28. In October 2004, Magnesium Elektron, Inc.'s (MEI) Isolux[™] arsenic treatment system was selected for demonstration at GHCSD in Tehachapi, CA.

As of November 2009, 39 of the 40 systems were operational, and the performance evaluation of 34 systems was complete.

1.2 Treatment Technologies for Arsenic Removal

The technologies selected for the Rounds 1 and 2 demonstration host sites include 25 adsorptive media (AM) systems (the Oregon Institute of Technology [OIT] site has three AM systems), 13 coagulation/filtration (C/F) systems, two ion exchange (IX) systems, and 17 point-of-use (POU) units (including nine under-the-sink reverse osmosis [RO] units at the Sunset Ranch Development site and eight AM units at the OIT site) and one system modification. Table 1-1 summarizes the locations, technologies, vendors, system flowrates, and key source water quality parameters (including As, Fe, and pH) at the 40 demonstration sites. An overview of the technology selection and system design for the 12 Round 1 demonstration sites and associated capital cost is provided in two EPA reports (Wang, et al., 2004 and Chen, et al., 2004). These are posted on the EPA website at http://www.epa.gov/ORD/NRMRL/wswrd/dw/arsenic/tech/index.html.

1.3 Project Objectives

The purpose of the arsenic demonstration program is to conduct full-scale arsenic treatment technology demonstration studies on the removal of arsenic from drinking-water supplies at 40 sites. Specific objectives are to:

- Evaluate the performance of the arsenic removal technologies for use on small systems.
- Determine the required system operation and maintenance (O&M) and operator skill levels.
- Characterize process residuals produced by the technologies.
- Determine the capital and O&M cost of the technologies.

This report summarizes the performance of the Isolux[™] arsenic treatment system at the GHCSD site in Tehachapi, CA, during the study period from October 25, 2005, through March 20, 2007. The types of data collected included system operation, water quality (both across the treatment train and in the distribution system), residuals, and capital and preliminary O&M cost.

				Design	Sourc	e Water Qı	ality
Demonstration				Flowrate	As	Fe	pН
Location	Site Name	Technology (Media)	Vendor	(gpm)	(µg/L)	(µg/L)	(Š.U.)
		Northeast/Ohio					
Wales, ME	Springbrook Mobile Home Park	AM (A/I Complex)	ATS	14	38 ^(a)	<25	8.6
Bow, NH	White Rock Water Company	AM (G2)	ADI	70 ^(b)	39	<25	7.7
Goffstown, NH	Orchard Highlands Subdivision	AM (E33)	AdEdge	10	33	<25	6.9
Rollinsford, NH	Rollinsford Water and Sewer District	AM (E33)	AdEdge	100	36 ^(a)	46	8.2
Dummerston, VT	Charette Mobile Home Park	AM (A/I Complex)	ATS	22	30	<25	7.9
Felton, DE	Town of Felton	C/F (Macrolite)	Kinetico	375	30 ^(a)	48	8.2
Stevensville, MD	Queen Anne's County	AM (E33)	STS	300	19 ^(a)	270 ^(c)	7.3
Houghton, NY ^(d)	Town of Caneadea	C/F (Macrolite)	Kinetico	550	27 ^(a)	$1,806^{(c)}$	7.6
Newark, OH	Buckeye Lake Head Start Building	AM (ARM 200)	Kinetico	10	15 ^(a)	$1,312^{(c)}$	7.6
Springfield, OH	Chateau Estates Mobile Home Park	AM (E33)	AdEdge	250 ^(e)	25 ^(a)	$1,615^{(c)}$	7.3
	•	Great Lakes/Interior Plains			•		
Brown City, MI	City of Brown City	AM (E33)	STS	640	14 ^(a)	127 ^(c)	7.3
Pentwater, MI	Village of Pentwater	C/F (Macrolite)	Kinetico	400	13 ^(a)	466 ^(c)	6.9
Sandusky, MI	City of Sandusky	C/F (Aeralater)	Siemens	340 ^(e)	16 ^(a)	$1,387^{(c)}$	6.9
Delavan, WI	Vintage on the Ponds	C/F (Macrolite)	Kinetico	40	20 ^(a)	$1,499^{(c)}$	7.5
Greenville, WI	Town of Greenville	C/F (Macrolite)	Kinetico	375	17	7827 ^(c)	7.3
Climax, MN	City of Climax	C/F (Macrolite)	Kinetico	140	39 ^(a)	546 ^(c)	7.4
Sabin, MN	City of Sabin	C/F (Macrolite)	Kinetico	250	34	$1,470^{(c)}$	7.3
Sauk Centre, MN	Big Sauk Lake Mobile Home Park	C/F (Macrolite)	Kinetico	20	25 ^(a)	$3,078^{(c)}$	7.1
Stewart, MN City of Stewart		C/F&AM (E33)	AdEdge	250	42 ^(a)	1,344 ^(c)	7.7
Lidgerwood, ND	City of Lidgerwood	Process Modification	Kinetico	250	146 ^(a)	$1,325^{(c)}$	7.2
		Midwest/Southwest	•				
Arnaudville, LA	United Water Systems	C/F (Macrolite)	Kinetico	770 ^(e)	35 ^(a)	$2,068^{(c)}$	7.0
Alvin, TX	Oak Manor Municipal Utility District	AM (E33)	STS	150	19 ^(a)	95	7.8
	Webb Consolidated Independent School						
Bruni, TX	District	AM (E33)	AdEdge	40	56 ^(a)	<25	8.0
Wellman, TX	City of Wellman	AM (E33)	AdEdge	100	45	<25	7.7
	Desert Sands Mutual Domestic Water						
Anthony, NM	Consumers Association	AM (E33)	STS	320	23 ^(a)	39	7.7
Nambe Pueblo, NM	Nambe Pueblo Tribe	AM (E33)	AdEdge	145	33	<25	8.5
Taos, NM	Town of Taos	AM (E33)	STS	450	14	59	9.5
Rimrock, AZ	Arizona Water Company	AM (E33)	AdEdge	90 ^(b)	50	170	7.2
Tohono O'odham							
Nation, AZ	Tohono O'odham Utility Authority	AM (E33)	AdEdge	50	32	<25	8.2
Valley Vista, AZ	Arizona Water Company	AM (AAFS50/ARM 200)	Kinetico	37	41	<25	7.8

Table 1-1. Summary of Rounds 1 and 2 Arsenic Removal Demonstration Locations, Technologies, and Source Water Quality

				Design	Sourc	e Water Qu	ality
Demonstration				Flowrate	As	Fe	pН
Location	Site Name	Technology (Media)	Vendor	(gpm)	(µg/L)	(µg/L)	(S.U.)
		Far West					
Three Forks, MT	City of Three Forks	C/F (Macrolite)	Kinetico	250	64	<25	7.5
Fruitland, ID	City of Fruitland	IX (A300E)	Kinetico	250	44	<25	7.4
Homedale, ID	Sunset Ranch Development	POU RO ^(f)	Kinetico	75 gpd	52	134	7.5
Okanogan, WA	City of Okanogan	C/F (Electromedia-I)	Filtronics	750	18	69 ^(c)	8.0
		POE AM (Adsorbsia/ARM 200/ArsenX ^{np})					
Klamath Falls, OR	Oregon Institute of Technology	and POU AM (ARM 200) ^(g)	Kinetico	60/60/30	33	<25	7.9
Vale, OR	City of Vale	IX (Arsenex II)	Kinetico	525	17	<25	7.5
	South Truckee Meadows General						
Reno, NV	Improvement District	AM (GFH/Kemiron)	Siemens	350	39	<25	7.4
Susanville, CA	Richmond School District	AM (A/I Complex)	ATS	12	37 ^(a)	125	7.5
Lake Isabella, CA	Upper Bodfish Well CH2-A	AM (HIX)	VEETech	50	35	125	7.5
	Golden Hills Community Service						
Tehachapi, CA	District	AM (Isolux)	MEI	150	15	<25	6.9

 Table 1-1. Summary of Rounds 1 and 2 Arsenic Removal Demonstration

 Locations, Technologies, and Source Water Quality (Continued)

AM = adsorptive media process; C/F = coagulation/filtration; HIX = hybrid ion exchanger; IX = ion exchange process; RO = reverse osmosis

ATS = Aquatic Treatment Systems; MEI = Magnesium Elektron, Inc.; STS = Severn Trent Services.

(a) Arsenic existing mostly as As(III).

(b) Design flowrate reduced by 50% due to system reconfiguration from parallel to series operation.

(c) Iron existing mostly as Fe(II).

(d) Withdrew from program in 2007. Selected originally to replace Village of Lyman, NE, site, which withdrew from the program in June 2006.

(e) Facilities upgraded systems in Springfield, OH, from 150 to 250 gpm; in Sandusky, MI, from 210 to 340 gpm; and in Arnaudville, LA, from 385 to 770 gpm.

(f) Including nine residential units.

(g) Including eight under-the-sink units.

2.0 SUMMARY AND CONCLUSIONS

MEI's Isolux[™] arsenic treatment system was installed at GHCSD in Tehachapi, CA, on October 21, 2005, and was put into service on October 25, 2005. Based on the information collected during the performance evaluation study, the following conclusions were drawn relating to the overall project objectives.

Performance of the arsenic removal technology for use on small systems:

- The Isolux[™]-302M media was effective at removing arsenic from drinking water to below the 10 µg/L MCL. The Isolux[™] system achieved useful run lengths of 61,600, 92,800, and 85,100 BV during Media Runs 1, 2, and 3, respectively; this is 12 to 41% lower than the vendor-projected run length of 105,000 BV.
- Accumulation of submicron particles on the media cartridges might have caused preferential flow through the media cartridges and the relatively short run length observed during Media Run 1.
- Most of the time, arsenic concentrations in the distribution system were much lower than those of the treatment system effluent, presumably due to blending of the treated water with untreated water from wells where arsenic was not a concern. Lead and copper did not appear to be impacted by the treatment system.

Simplicity of required system O&M and operator skill levels:

- Under normal operating conditions, the system required little attention from the operator. The daily demand for operator labor was approximately 30 min to inspect the system visually and record operational parameters.
- Daily operation of the system did not require additional skills beyond those necessary to operate the existing water-supply equipment. The system was operated by a State of California-certified operator who has Level 2 certifications for both treatment and distribution systems.

Process residuals produced by the technology:

• Residuals produced by the Isolux[™] system included spent media cartridges only; backwash was not a system requirement. The spent Isolux[™]-302M media passed Toxicity Characteristic Leaching Procedure (TCLP) tests and therefore could be disposed of as a non-hazardous waste. However, MEI sent the spent media for beneficial reuse.

Cost-effectiveness of the technology:

- The capital investment cost for the 150-gpm system was \$76,840, including \$58,500 for equipment, \$8,500 for engineering, and \$9,840 for installation. This cost equated to \$512/gpm (or \$0.36/gpd), not including cost for the building.
- The unit capital cost was \$0.09/1,000 gal if the system operates at a 100% utilization rate. The system actual unit cost was \$0.21/1,000 gal of treated water, based on an average flowrate of 79.3 gpm and an average daily operating time of 19.6 hr/day. The labor cost for routine O&M activities was \$0.14/1,000 gal of water treated.

3.0 MATERIALS AND METHODS

3.1 General Project Approach

Following the predemonstration activities summarized in Table 3-1, the performance evaluation study of the IsoluxTM arsenic treatment system began on October 25, 2005, and ended on March 20, 2007. Table 3-2 summarizes the types of data collected and/or considered as part of the technology evaluation process. The overall system performance was evaluated based on its ability to consistently remove arsenic to below the target MCL of 10 μ g/L for arsenic through the collection of water samples across the treatment train, as described in the Study Plan (Battelle, 2005). System reliability was evaluated by tracking the unscheduled system downtime and the frequency and extent of repair and replacement. The plant operator recorded the unscheduled downtime and repair information on a Repair and Maintenance Log Sheet.

Activity	Date
Introductory Meeting Held	October 13, 2004
Project Planning Meeting Held	April 12, 2005
Draft Letter of Understanding Issued	April 22, 2005
Final Letter of Understanding Issued	May 6, 2005
Request for Quotation Issued to Vendor	May 24, 2005
Vendor Quotation Submitted to Battelle	June 6, 2005
Purchase Order Completed and Signed	July 5, 2005
Engineering Package Submitted to CDPH	August 4, 2005
Final Study Plan Issued	September 23, 2005
Permit issued by CDPH	September 7, 2005
System Installation and Shakedown Completed	October 21, 2005
Performance Evaluation Began	October 26, 2005

 Table 3-1. Predemonstration Study Activities and Completion Dates

CDPH = California Department of Health Services.

Table 3-2.	Evaluation	Objectives and	Supporting	Data Collection	Activities

Evaluation Objective	Data Collection
Performance	-Ability to consistently meet 10 µg/L of arsenic in treated water
Reliability	-Unscheduled system downtime
	-Frequency and extent of repairs, including a description of problems,
	materials and supplies needed, and associated labor and cost
System O&M and	-Pre- and post-treatment requirements
Operator Skill	-Level of automation for system operation and data collection
Requirements	-Staffing requirements, including number of operators and laborers
	-Task analysis of preventative maintenance, including number, frequency,
	and complexity of tasks
	-Chemical handling and inventory requirements
	-General knowledge needed for relevant chemical processes and for health
	and safety practices
Residual Management	-Quantity and characteristics of aqueous and solid residuals generated by
	system operation
System Cost	-Capital cost for equipment, engineering, and installation
	-O&M cost for chemical usage, electricity consumption, and labor

The system O&M and operator skill requirements were assessed through quantitative data and qualitative considerations, including the need for pre- and/or post-treatment; level of system automation; extent of preventative maintenance activities; frequency of chemical and/or media handling and inventory; and general knowledge needed for relevant chemical processes and related health and safety practices. The staffing requirements for system operation were recorded on an Operator Labor Hour Log Sheet.

The cost of the system was evaluated based on the capital cost per gal/min (gpm) (or gal/day [gpd]) of design capacity and the O&M cost per 1,000 gal of water treated. This task required tracking the capital cost for equipment, engineering, and installation, as well as the O&M cost for media replacement and disposal, chemical supply, electricity usage, and labor.

3.2 System O&M and Cost Data Collection

The plant operator performed daily, weekly, and monthly system O&M and data collection according to instructions provided by MEI and Battelle. Each day, the plant operator recorded system operational data, such as pressure, flowrate, totalizer, and hour meter readings (see Appendix A) on a Daily System Operation Log Sheet, and also conducted visual inspections to ensure normal system operations. If any problem occurred, the plant operator contacted the Battelle Study Lead, who determined if the vendor should be contacted for troubleshooting. The plant operator recorded on the Repair and Maintenance Log Sheet all relevant information, including the problem encountered, course of action taken, materials and supplies used, and associated cost and labor incurred. Each week, the plant operator measured several water quality parameters onsite, including temperature, pH, dissolved oxygen (DO), oxidation-reduction potential (ORP), and residual chlorine, and recorded the data on a Weekly Onsite Water Quality Parameters Log Sheet.

The capital cost for the Isolux[™] system consisted of cost for equipment, site engineering, and system installation. The O&M cost consisted primarily of the cost for the media replacement and spent media disposal, electricity, and labor. Electricity consumption was determined using a kilowatt hour meter. Labor for various activities, such as routine system O&M, troubleshooting, repairs, and demonstration-related work, were tracked using an Operator Labor Hour Log Sheet. Routine O&M included activities such as completing field logs, ordering supplies, performing system inspections, and others as recommended by the equipment vendor. Labor was recorded for demonstration-related work, including activities such as performing field measurements, collecting and shipping samples, and communicating with the Battelle Study Lead and the vendor, but was not used for the cost analysis.

3.3 Sample Collection Procedures and Schedules

To evaluate the system performance, samples were collected from the wellhead, across the treatment plant, and from the distribution system. Table 3-3 provides the sampling schedule and analytes measured during each sampling event. Figure 3-1 presents a flow diagram of the treatment system, along with the analytes and schedule for each sampling location. Specific sampling requirements for arsenic speciation, analytical methods, sample volumes, containers, preservation, and holding times are presented in Table 4-1 of the EPA-endorsed Quality Assurance Project Plan (QAPP) (Battelle, 2004). Appenidx A of the QAPP describes the procedure for arsenic speciation.

3.3.1 Source Water. During the initial site visit on October 13, 2004, one set of source water samples was collected and speciated using an arsenic speciation kit (see Section 3.4.1). The sample tap was flushed for several minutes before sampling; special care was taken to avoid agitation, which might cause unwanted oxidation. Table 3-3 lists analytes for the source water samples.

Sample	Sample	No. of			Sampling
Туре	Locations ^(a)	Samples	Frequency	Analytes	Date
Source Water	IN	1	Once during initial site visit	Onsite: pH, temperature, DO, and ORP Offsite: As(III), As(V), As (total and soluble), Fe (total and soluble), Mn (total and soluble), U (total and soluble), V (total and soluble), V (total and soluble), Na, Ca, Mg, Cl, F, NO ₂ , NO ₃ , NH ₃ , SO ₄ , SiO ₂ , PO ₄ , TDS, TOC, turbidity, and alkalinity	10/13/04
Treatment Plant Water	IN, AC, MA, and MB	4	Second, third, and fourth weeks of each 4- week cycle (regular sampling)	Onsite: pH, temperature, DO, ORP, and Cl ₂ (total) ^(b) Offsite: As (total), Fe (total), Mn (total), Zr (total), Ca, Mg, SiO ₂ , P, turbidity, and alkalinity	See Appendix B
	IN, AC, and TM	3	First week of each 4- week cycle (speciation sampling)	Onsite: pH, temperature, DO, ORP, and Cl ₂ (total) ^(b) Offsite: As(III), As (V), As (total and soluble), Fe (total and soluble), Fe (total and soluble), Zr (total and soluble), Ca, Mg, F, NO ₃ , SO ₄ , SiO ₂ , P, turbidity, and alkalinity.	See Appendix B
Distribution System Water	DS1, DS2, and DS 3	3	Monthly ^(c)	As (total), Fe (total), Mn (total), Pb, Cu, pH, and alkalinity	See Table 4-7

 Table 3-3. Sampling and Analysis Schedule for GHCSD Site

(a) Abbreviations corresponding to sample locations shown in Figure 3-1.

(b) Total chlorine residual analyzed at MB or TM beginning on July 5, 2006.

(c) Four baseline sampling events performed from July to August 2005 before the system became operational.

IN = at wellhead; AC = after chlorination; MA = after Module A; MB = after Module B; TM = after Modules A and B combined.

DS1 to 3 = distribution system sampling location 1 to 3.

DO = dissolved oxygen; ORP = oxidation-reduction potential; TDS = total dissolved solids; TOC = total organic carbon.



Figure 3-1. Process Flow Diagram and Sampling Schedule and Locations

3.3.2 Treatment Plant Water. During the system performance evaluation study, water samples were collected weekly, on a 4-week cycle, for onsite and offsite analyses. For the first week of each 4-week cycle, samples taken at the wellhead (IN), after chlorination (AC), and after Modules A and B combined (TM), were speciated onsite and analyzed for the analytes listed in Table 3-3 under speciation sampling. For the next three weeks, samples were collected at IN, AC, after Module A (MA), and after Module B (MB) and analyzed for the analytes listed in Table 3-3 under regular sampling. Speciation was discontinued on October 10, 2006, and since then, samples were collected weekly from IN, AC, MA, and MB and were analyzed only for total arsenic.

3.3.3 Distribution System Water. Samples were collected from the distribution system to determine any impacts of the Isolux[™] arsenic treatment system on the water chemistry in the distribution system, specifically arsenic, lead, and copper levels. From July to August 2005, prior to the startup of the treatment system, four baseline distribution sampling events were conducted at three locations in the distribution system. Following system startup, distribution system sampling continued on a monthly basis at the same three locations for nine occasions.

Three residences were selected for distribution water sampling, including one each on San Lucas ("DS1"), Tiffany Circle ("DS2"), and Early Dawn Court ("DS3"). Only one residence (DS1) was part of the historic Lead and Copper Rule (LCR) sampling network serviced by the treatment well. Figure 3-2 is a distribution map showing the three sampling locations. The homeowners of the residences collected samples following an instruction sheet developed according to the *Lead and Copper Monitoring and Reporting Guidance for Public Water Systems* (EPA, 2002). The dates and times of last water usage before sampling and sample collection were recorded for calculations of the stagnation time. All samples were collected from a cold-water faucet that had not been used for at least 6 hr to ensure that stagnant water was sampled.

3.3.4 Residual Solids. The IsoluxTM system did not require backwash; therefore, only spent media were collected for residual solid analysis. Nine spent media cartridges from the first media run (from October 26, 2005, to January 17, 2006) were shipped to Battelle on April 13, 2006. Of the nine spent media cartridges, the outer membrane on one cartridge was opened to expose the media. Spent media was sampled across the annular space of the cartridge from (1) the outer surface (i.e., immediately under the porous outer member where water after chlorination entered the media bed); (2) the subsurface (immediately under the outer surface); (3) the middle; and (4) the inner portion (i.e., where water exited the media bed) of the cartridge. Metal analyses were conducted on air-dried and acid-digested samples. Meanwhile, MEI conducted its own TCLP, total threshold limit concentration (TTLC), and soluble threshold limit concentration (STLC) tests on the spent media and provided the results to Battelle.

3.4 Sampling Logistics

Sampling logistics, including arsenic speciation kit preparation, sample cooler preparation, and sample shipping and handling, are discussed below.

3.4.1 Preparation of Arsenic Speciation Kits. The arsenic field speciation method uses an anion exchange resin column to separate the soluble arsenic species–As(V) and As(III) (Edwards, et al., 1998). Resin columns were prepared in batches at Battelle laboratories according to the procedures detailed in Appendix A of the EPA-endorsed QAPP (Battelle, 2004).

3.4.2 Preparation of Sampling Coolers. For each sampling event, a sample cooler was prepared with the appropriate number and type of sample bottles, disc filters, and/or speciation kits. All sample bottles were new and contained appropriate preservatives. Each sample bottle was affixed with a pre-



Figure 3-2. Water Distribution System at GHCSD

printed, colored-coded label consisting of the sample identification (ID), data and time of sample collection, collector's name, site location, sample destination, analysis required, and preservative. The sample ID consisted of a two-letter code for the specific water facility, the sampling date, a two-letter code for a specific sampling location, and a one-letter code designating the arsenic speciation bottle (if necessary). The sampling locations at the treatment plant were color-coded for easy identification. The labeled bottles were separated by sampling location, placed in ZiplockTM bags, and packed in the cooler.

In addition, all sampling- and shipping-related materials, such as disposable gloves, sampling instructions, chain-of-custody forms, prepaid/addressed FedEx air bills, and bubble wrap, were included. The chain-of-custody forms and air bills were complete except for the operator's signature and the sample dates and times. After preparation, the sample cooler was sent to the site via FedEx for the following week's sampling event.

3.4.3 Sample Shipping and Handling. After sample collection, samples for offsite analyses were packed carefully in the original coolers with wet ice and shipped to Battelle. Upon receipt, sample custodians verified that all samples indicated on the chain-of-custody forms, were included and intact. Sample IDs were checked against the chain-of-custody forms, and the samples were logged into the laboratory sample receipt log. The Battelle Study Lead addressed discrepancies noted by the sample custodians with the plant operator.

Samples for metal analyses were stored at Battelle's inductively coupled plasma-mass spectrometry (ICP-MS) laboratory. Samples for other water quality parameters were packed in separate coolers and picked up by couriers from American Analytical Laboratories (AAL) in Columbus, OH, and TCCI Laboratories in New Lexington, OH, both of which were contracted by Battelle for this demonstration study. The chain-of-custody forms remained with the samples from the time of preparation through analysis and final disposition. All samples were archived by the appropriate laboratories for the respective duration of the required hold time and disposed of properly thereafter.

3.5 Analytical Procedures

The analytical procedures described in Section 4.0 of the EPA-endorsed QAPP (Battelle, 2004) were followed by the Battelle ICP-MS Laboratory, AAL, and TCCI Laboratories. Laboratory quality assurance/quality control (QA/QC) of all methods followed the prescribed guidelines. Data quality in terms of precision, accuracy, method detection limits (MDL), and completeness met the criteria established in the QAPP (i.e., relative percent difference [RPD] of 20%, percent recovery of 80-120%, and completeness of 80%). The quality assurance (QA) data associated with each analyte will be presented and evaluated in a QA/QC Summary Report to be prepared under separate cover upon completion of the Arsenic Demonstration Project.

The plant operator conducted field measurements of pH, temperature, DO, and ORP using a VWR Symphony SP90MS handheld multimeter, which was calibrated for pH and DO prior to use following procedures provided in the user's manual. The ORP probe also was checked for accuracy by measuring the ORP of a standard solution and comparing it to the expected value. The plant operator collected a water sample in a clean plastic beaker and placed the VWR probe in the beaker until a stable value was obtained.

4.0 RESULTS AND DISCUSSION

4.1 Facility Description

At an elevation of 3,973 ft above sea level, GHCSD is located immediately west of Tehachapi, CA, and has approximately 7,900 residents. Prior to the demonstration study, there were 13 active wells at GHCSD, but only Well C had elevated arsenic concentrations up to 20 μ g/L. Figure 4-1 shows the Well C pump house, which is located near the southeast corner of the district, east of State Route 202.

Drilled in 1997, Well C was 10-in in diameter and 700 ft deep, with a pumping water level of 517 ft below ground surface (bgs) and a static water level of 258 ft bgs. The well was equipped with a 25-horsepower (hp) Grundfos pump rated for 145 gpm. The maximum flowrate of the well, however, was 100 gpm, yielding 81,462 and 71,687 gpd (on average) of water in 2003 and 2004, respectively. The well was controlled by a telemetry system based on time of day (shut off between 12 p.m. and 6 p.m.), level of water in storage tanks, or both. One 1,000,000- and one 500,000-gal storage tanks, located close to the Well C pump house and a dry van container that housed the new arsenic treatment system (Figure 4-2), were used to store water before it entered the distribution system. An existing chlorination system. (Figure 4-3) provided a total chlorine residual of 1.25 mg/L (as Cl₂) in the distribution system.



Figure 4-1. Well C Pump House

4.1.1 Source Water Quality. Source water samples were collected from Well C on October 13, 2004, by a Battelle staff member who attended an introductory meeting for this project. Source water also was filtered for soluble arsenic, iron, manganese, uranium, and vanadium and was speciated for As(III) and As(V). In addition, pH, temperature, DO, and ORP were measured onsite using a WTW 340i meter. Table 4-1 presents the analytical results from the source water sampling event and compares them



Figure 4-2. Storage Tanks, Well C Pump House, and Dry Van Container



Figure 4-3. Pre-existing Chlorine Addition System

		CDPH	CDPH	Facility	Battelle
		Treated	Raw	Raw	Raw
		Water	Water	Water	Water
Parameter	Unit	Data	Data	Data ^(a)	Data
Date		10/11/00	11/19/03	NA	10/13/04
рН	_	8.0	8.3	8.2	6.9 ^(b)
DO	mg/L	NA	NA	NA	1.7
ORP	mV	NA	NA	NA	4.9
Total Alkalinity (as CaCO ₃)	mg/L	180	170	175, 180*	171
Hardness (as CaCO ₃)	mg/L	183	158	183	179
Turbidity	NTU	0.06	0.19	NA	0.2
TDS	mg/L	NA	NA	NA	292
TOC	mg/L	NA	NA	NA	<0.7
Nitrate (as N)	mg/L	0.34	< 0.44	NA	0.32
Nitrite (as N)	mg/L	< 0.02	< 0.02	NA	< 0.01
Ammonia (as N)	mg/L	NA	NA	NA	< 0.05
Chloride	mg/L	12	15	14, 15*	12.0
Fluoride	mg/L	0.23	0.24	NA	0.2
Sulfate	mg/L	42	45	26, 50*	40.0
Silica (as SiO ₂)	mg/L	NA	NA	28*	27.0
Orthophosphate (as OPO ₄)	mg/L	NA	NA	<0.065*	< 0.06
As (total)	μg/L	9	14	20, 14*	14.7
As (soluble)	μg/L	NA	NA	NA	13.0
As (particulate)	μg/L	NA	NA	NA	1.7
As(III)	μg/L	NA	NA	NA	3.9
As(V)	μg/L	NA	NA	NA	9.2
Fe (total)	μg/L	< 50	< 50	153, 48*	<25
Fe (soluble)	μg/L	NA	NA	NA	<25
Mn (total)	μg/L	< 10	< 10	<10, 5*	8.8
Mn (soluble)	μg/L	NA	NA	NA	5.0
U (total)	μg/L	NA	NA	NA	0.8
U (soluble)	μg/L	NA	NA	NA	0.9
V (total)	μg/L	NA	NA	NA	2.5
V (soluble)	μg/L	NA	NA	NA	2.4
Na (soluble)	mg/L	29	30	24, 31*	34.8
Ca (total)	mg/L	52	45	53, 51*	52.3
Mg (total)	mg/L	13	11	13, 12*	11.8

Table 4-1. Quality of Well C Source Water and GHCSD Treated Water

(a) Provided by the facility to EPA for site selection.

(b) Data questionable.

CDPH = California Department of Public Health; DO = dissolved oxygen;

NA = not available; NTU = nephlemetric turbidity unit; ORP = oxidation-reduction

potential; TDS = total dissolved solids; TOC = total organic carbon;

* = EPA sample analysis

to those provided to EPA for site selection by the California Department of Public Health (CDPH) and the facility.

Arsenic. Total arsenic concentrations in source water ranged from 14 to 20 μ g/L. Based on the October 13, 2004, speciation results, out of 14.7 μ g/L of total arsenic, 13.0 μ g/L existed in the soluble form. Of the soluble fraction, 9.2 μ g/L existed as As(V) and 3.9 μ g/L as As(III). As such, the majority of soluble

arsenic can be removed directly by Isolux[™]-302M media without preoxidation. The presence of As(V) as the predominating arsenic species implies that Well C water is rather oxidizing. This is somewhat contradictory to the relatively low DO and ORP levels (i.e., 1.7 mg/L and 4.9 mV, respectively) measured during the October 13, 2004, sampling event. Care was used during the performance evaluation study to confirm that these, in fact, were the results of erroneous field measurements.

Interfering Ions. According to MEI, the presence of iron, manganese, phosphate, and silica in source water can potentially impact the performance of $Isolux^{TM}$ -302M media. Total iron concentrations in source water ranged from <25 to 153 µg/L. Battelle and CDPH results were less than the respective method reporting limits of 25 and 50 µg/L, respectively. The EPA data was 48 µg/L, close to the Battelle and CDPH data. At 153 µg/L, the facility data was high. Manganese concentrations in raw water were <10 µg/L, and therefore should not impact IsoluxTM-302M media performance.

Orthophosphate concentrations were below the reporting limit of 0.06 mg/L. Silica levels ranged from 27 to 28 mg/L. Based on the data collected during the pilot study, MEI concluded that the presence of these competing ions did not adversely affect IsoluxTM-302M media performance.

Other Water Quality Parameters. pH values of raw water ranged from 8.2 to 8.3, which is at the high end of the operational range from 4.0 to 8.5, and could potentially impact IsoluxTM-302M media performance. Sulfate concentrations ranged from 26 to 50 mg/L; sodium from 24 to 34.8 mg/L; calcium from 45 to 53; and magnesium from 11 to 13 mg/L. Total alkalinity concentrations ranged from 170 to 180 mg/L (as CaCO₃); hardness from 158 to 183 mg/L (as CaCO₃); chloride from 12 to 15 mg/L; and fluoride from 0.2 to 0.24 mg/L. The presence of these ions in source water was not expected to impede arsenic removal by IsoluxTM-302M media.

4.1.2 Distribution System. Prior to and during the performance evaluation study, the distribution system at GHCSD was supplied by 13 wells, of which two were used as stand-by wells and one was used only seasonally. The maximum water demand was 2,050,000 gpd, which usually occurred in July. Water from Well C was pumped first to the 1,000,000- and 500,000-gal storage tanks and then to the distribution system, while water from the other wells was pumped to the distribution system and then to the same storage tanks. The distribution system is composed primarily of polyvinyl chloride (PVC) and asbestos cement (AC) piping. Service lines within residences are mainly copper pipe. Under the U.S. EPA LCR, GHCSD collects samples from customer taps at 20 locations every 3 years. GHCSD also conducts bacterial analysis monthly at 10 specified locations and quarterly at the wellheads.

4.2 Treatment Process Description

The 150-gpm Isolux[™] arsenic treatment system uses Isolux[™]-302M powder media developed by MEI for arsenic removal. Table 4-2 presents physical and chemical properties of the media, which has NSF Standard 61 approval for use in drinking-water applications.

The Isolux^{$^{\text{M}}$} arsenic treatment system at GHCSD consisted of two parallel adsorption modules, each containing a booster pump, a flow regulator, a 1-µm bag filter, and two parallel carbon steel adsorption vessels. Each adsorption vessel contained nine replaceable media cartridges (Figure 4-4), or 36 for the entire system. The system was designed to treat approximately 150 gpm of flow, with 75 gpm by each module. Figure 4-5 is a schematic of MEI's Isolux^{$^{\text{M}}$} arsenic treatment system.

Chlorinated water was supplied to the two adsorption modules by a booster pump. As groundwater was pumped through the media cartridges, soluble arsenic was removed via adsorption, thus reducing total arsenic concentration to below the 10 μ g/L MCL. A flow totalizer/meter was installed on the downstream end of each adsorption module to measure throughput and flowrate through each module.

Parameter	Value		
Matrix	Hydrous zirconium oxide		
Physical form	Amorphous powder		
Color	White, bulky powder		
Specific density	3.25		
Bulk density (lb/ft ³)	60		
Particle size (micron)	1-3 to 40-50		
Mesoporosity (Å)	20–40		
BET surface area (m^2/g)	300–350		
Functional group	Zr-OH		
Ion exchange capacity (meq/g)	8		
Operational pH	4.0-8.5		
Source: MEI			

Table 4-2. Properties of Isolux[™]-302M Media

Source: MEI

Pressure gauges located downstream of the well, flow control valve, bag filter, and adsorption module were used to monitor the system pressure and pressure drop across the treatment modules. The effluent of each module was combined and directed into the storage tanks. The system was instrumented with on/off valves and sample collection ports. The system was installed in an 8-ft \times 40-ft enclosure.



Figure 4-4. Replaceable Isolux[™]-302M Media Cartridges (Provided by MEI)



Figure 4-5. Schematic of MEI's Isolux[™] Arsenic Treatment System (Provided by MEI)

Independent from this demonstration study, GHCSD hosted a pilot study on IsoluxTM-302M media from July 2003 to August 2004 at Well C. Figure 4-6 presents the pilot unit (in the wooden structure) and an IsoluxTM media cartridge used for the pilot study. The initial testing used a 0.8-gpm, 10-in pilot unit equipped with a 5-µm particulate pre-filter, an activated carbon filter, an IsoluxTM media cartridge (containing 1 lb of IsoluxTM-302M media), a flowmeter, and a flow totalizer. After operating for nearly 90



Figure 4-6. Isolux[™] Pilot Facility (left) and Isolux[™] Media Cartridge (right)

days and treating approximately 8,300 gal (or 66,578 bed volumes [BV]) of water, over 2 μ g/L of arsenic were detected in the treated water. The pilot unit was then scaled up to a 10-gpm unit containing 22 lb of IsoluxTM-302M media. Operating at 8 gpm, the unit treated 254,887 gal (or 92,934 BV) of water from March 10 through April 3, 2004, prior to reaching 10 μ g/L of arsenic breakthrough. A second adsorption run with the 10-gpm unit from July 17 through August 29, 2004, yielded slightly better performance results (i.e., 112,099 BVs) than the first run. Results of the pilot study indicated that:

- The Isolux[™] arsenic treatment system could remove arsenic to below a detection limit of 2.0 µg/L. An elevated pH value of 8.2 and competing ions (including silica, phosphate, and iron) in the source water did not adversely affect the performance of Isolux[™]-302M media.
- Pre-treatment of Well C source water was not required.
- Spent Isolux[™]-302M media passed EPA TCLP and California whole effluent toxicity (WET) tests, so they could be disposed of as a non-hazardous waste.
- No backwash was required.

Table 4-3 summarizes the key system design parameters for the Isolux[™] arsenic treatment system. The treatment system includes the following major process and system components:

- Intake Raw water from Well C was chlorinated and fed to the Isolux[™] arsenic treatment system. An hour meter was installed on the well pump to record the operation time.
- **Chlorination** Prior to entering the system, water was injected with chlorine for disinfection purposes. A 12.5% sodium hypochlorite (NaClO) solution was stored in a 35-gal drum and injected by a solenoid-driven metering pump with a maximum capacity of 1.0 gal/hr (gph). Operation of the chlorine feed system was linked to the well pump such that chlorine was injected only when the well was operating. The system operator monitored chlorine consumption weekly by recording the chlorine levels in the chlorine supply tank and by measuring the volume of chlorine added to the tank. The target total chlorine residual was 1.25 mg/L (as Cl₂).
- Isolux[™] Adsorption Two Isolux[™] adsorption modules arranged in parallel provided a total of 150-gpm treatment capacity. Figure 4-7 shows the treatment system installed at GHCSD. Each Isolux[™] adsorption module contained the following elements:
 - Booster Pump With Flow Regulator Use of two booster pumps with flow regulators (one per module) located prior to the adsorption vessels ensured adequate inlet pressure to the treatment system. Each EBARA Model CDU booster pump was constructed of 304L stainless steel, rated at 3 hp, and could provide a maximum flowrate of 95 gpm. The operation of the booster pumps was synchronized with the well pump so that they would turn on and off at the same time. During the performance evaluation study, operation of the booster pumps was found to be unnecessary.
 - Bag Filter Each Isolux[™] module contained a 1-µm bag filter. Source water flowed through the 1-µm bag-type particulate pre-filter to remove any sediment from the source water. The bag filters were changed periodically due to increased pressure readings.
 - Media Vessel Each module contained two 20-in × 48-in media vessels, with each vessel containing nine Isolux[™]-302M media cartridges.

Design Parameter	Value	Remark
No. of modules	2	Arranged in parallel
Module size (in.)	$48 \text{ W} \times 48 \text{L} \times 60 \text{ H}$	_
Module weight (lb)	1,500	As shipped (dry with no media)
Module weight (lb)	3,200	In operation
No. of vessels	4	Two vessels arranged in parallel per
		module; 100 psi-rated carbon steel with
		NSF-rated epoxy coating
Vessel size (in.)	20 OD × 48 H	_
No. of cartridges per vessel	9	36 cartridges total
Cartridge length (in)	42.25	-
Cartridge OD (in)	4.55	_
Cartridge ID (in)	4.35	_
Cartridge outer membrane nominal	30	Constructed of polyethylene porous
pore size (µm)		membrane
Cartridge inner membrane nominal	10	Constructed of polyethylene porous
pore size (µm)		membrane
Cartridge outer membrane thickness	0.20	-
(in)		
Cartridge inner membrane thickness	0.52	—
(in)		
Cartridge weight (lb)	21	-
Type of media used	Isolux -302M	Particle size of 20–40 µm
Quantity of media per vessel (ft ³)	2.88	Each cartridge contained 0.32 ft ³ ; two
		modules each contained 5.7 ft ² ; total
Testa en al minima	2	was 11.4 ft ⁻
Internal piping	2-in schedule 40	_
Inlat and autist a surrestions	PVC glued	
inter and outlet connections	1.5-III PVC lefilate	-
Backwashing requirements	None	
Inlet pressure (psi)	80	
Outlet pressure (psi)	45	Outlet from vessels
Pressure drop (psi)	<30	
A rea of contact (ft^2)	4.1	Per cartridge
Hydraulic loading rate (gpm/ft^2)	1.0	Per cartridge
Estimated bed contact time (min)	0.5	Per cartridge
Peak flowrate (gpm)	150	Maximum flowrate of system
Average daily throughput to system	100.000	Estimate provided by GHCSD
(ond)	100,000	Estimate provided by GITESD
Estimated working capacity (BV)	105 000	Bed volumes to 10 µg/L arsenic
Estimated working capacity (E V)	100,000	breakthrough
Estimated volume to breakthrough	8,950,000	$1 \text{ BV} = 11.4 \text{ ft}^3 = 85.3 \text{ gal}$
(gal)		-
Estimated media life (months)	3	Estimated frequency of media cartridge
		changeout based on average throughput
		of 100,000 gpd
No. of BV/day	1,200	Based on estimated working capacity
		versus estimated media life

 Table 4-3. Isolux[™] Arsenic Treatment System Specifications and Design Parameters



Figure 4-7. Isolux[™] Adsorption Module at GHCSD

- Isolux[™] Media Cartridges Each media cartridge was 4.5-in in diameter by 42-in in \triangleright height and contained approximately 0.32 ft³ of IsoluxTM-302M media. The total amount of media in each module was 5.7 ft³, providing about 0.5 min of contact time at the specified flowrate of 75 gpm. The media are sandwiched between two thin layers of tubular membranes constructed of porous polyethylene (PE). The outer membrane measured 4.55in in diameter by 42.25in in length and had a nominal pore size of 30 um. The inner membrane measured 1.60in in diameter by 42.25in in length and had a nominal pore size of 10 µm. The upper end of the cartridge was completely sealed with a PE endcap; the lower end also was sealed with a PE end-cap but with a discharge tube. Untreated water entered the vessel and passed through the porous outer membrane, coming into contact with the media within the annular space of the cartridge. After contacting the media, the water flowed through the porous inner membrane and into the hollow center portion of the cartridge before flowing downward in the lower (discharge) portion of the vessel. Figure 4-8 presents a schematic of an assembled Isolux[™]-302M media cartridge.
- Media Cartridge Replacement When the capacity of the media cartridges in the vessels was exhausted, the operator replaced the spent media cartridges with virgin ones. Cartridges for both modules were replaced at the same time. Thus, 36 cartridges were needed for complete replacement. One module was completely serviced before service on the second module began. The spent media cartridges were stored at the facility until enough cartridges accumulated to facilitate efficient shipment to MEI.



Figure 4-8. Schematic of Assembled Isolux[™] Media Cartridge

• **Storage Tanks** – Treated water from Well C was stored in the 1,000,000- and 500,000-gal storage tanks before it entered the distribution system.

4.3 Treatment System Installation

4.3.1 System Permitting. The permit application for the $Isolux^{TM}$ system was simplified and expedited by CDPH because (1) only a "temporary" permit was granted and valid for the duration of the EPA demonstration study and (2) waste disposal was not anticipated to be an issue, considering that the $Isolux^{TM}$ system would not require backwashing and that any spent media cartridges would be returned to MEI for disposal.

The submittal for the permit application included a schematic of MEI's Isolux[™] arsenic treatment system, a written description of the system, and an O&M manual. After the vendor incorporated review comments from GHCSD and Battelle, the submittal package was sent to CDPH for review on August 4, 2005. CDPH provided Approval-to-Construct on September 7, 2005.

According to CDPH, upon completion of the EPA demonstration study, GHCSD must secure a permanent permit if it plans to keep the IsoluxTM system and continue its operation. GHCSD must also comply with the California Environmental Quality Act (CEQA) requirements as part of the permitting process. A regular water supply permit application takes 30 days for initial completeness review by CDPH. Once the application has been determined complete, it normally takes 90 days to issue a final permit document.

4.3.2 Building Construction. GHCSD installed the IsoluxTM system in a steel, dry, van container. Required building preparation included grading of the ground, installation of floor drains, interconnection of the piping, and provision of an electrical supply. Distributed by On Site Storage Solutions, the container was 8 ft wide, 40 ft long, and 8 ft high (Figure 4-9). The cost of the container was approximately \$4,218, including delivery.

4.3.3 Installation, Shakedown, and Startup. The $Isolux^{TM}$ arsenic treatment system was delivered to the site on September 16, 2005. The staff of GHCSD performed the off-loading and installation under the supervision of MEI's local engineer. Installation included piping connections to the existing entry and distribution system. System installation was completed on October 21, 2005.



Figure 4-9. Isolux[™] Treatment System Enclosure (Storage Tank in Background)

4.4 System Operation

4.4.1 Operational Parameters. The operational parameters for the performance evaluation study were tabulated and are attached as Appendix A. Key parameters for each media run are summarized in Table 4-4. Media Run 1 began on October 26, 2005, and ended on January 17, 2006, after the arsenic concentration in the system effluent had reached that of system influent. The well was producing a significant amount of sediment/particulate matter, making it necessary to replace the bag filters rather frequently (see Section 4.5.3). Accumulation of well sediment caused a rapid increase in differential pressure (Δp) across the bag filters.

A video log on Well C was conducted by Bakersfield Well and Pump Company on February 13, 2006, to determine if any corrective actions would be necessary. The result revealed rusty areas on the drop-pipe, which prompted GHCSD's decision to rehabilitate the well. From March 7 to 8, 2006, Bakersfield Well and Pump Company performed well rehabilitation, which included (1) pulling the submersible pump and

drop-pipe, (2) wire-brushing and bailing the well casing, and (3) installing 651 ft of new 3-in galvanizedsteel drop-pipe and a new 25-hp Franklin submersible pump rated at 120 gpm. GHCSD also installed a wire strainer upstream of the system to further reduce the amount of sediment/particulate matter to the system. Once the well was rehabilitated and the media cartridges were replaced, Media Run 2 began on April 27, 2006. The treatment system produced water below the arsenic MCL until August 8, 2006, whereupon arrangements were made to replace the media cartridges, again in both modules. Media Run 3 began on August 17, 2006, and continued through March 20, 2007, which concluded the performance evaluation study.

	Media		Media		Media	
Operational Parameter	Run 1		Run 2		Run 3	
Duration ^(a)	10/26/05-01/17/06		04/27/06-08/15/06		08/17/06-03/20/07	
Module	А	В	А	В	А	В
Total operating time (hr)	1,377	1,377	1,900	1,900	1,422	1,422
No. of days in operation (day)	63	63	94	94	85	85
Average daily operating time						
$(hr/day)^{(b)}$	21.9	21.9	20.2	20.2	16.7	16.7
Throughput to 10µg/L As						
breakthrough (gal)	2,676,700	2,579,100	3,903,400	3,697,755	3,883,500	3,249,800
Throughput to 10µg/L As						
breakthrough (BV) ^(c)	62,760	60,470	91,520	86,700	91,100	76,200
Range of/average flowrate (gpm) ^(d)	30–59/	26-59/	23-56/	20-69/	17-71/	21-56/
	40	40	41	37	46	39
Range of/average EBCT (min)	0.72-1.4/	0.72-1.6/	0.75-1.9/	0.62-2.1/	0.60-2.5/	0.76-2.0/
	1.1	1.1	1.1	1.2	0.92	1.1
Range of/average Δp across module	12-26/	8–26/	2-18/	2-19/	2-20/	2-241
(psi)	17	16	11	12	10	13
Range of/average Δp across bag filter	0–38/	0-40/	0-53/	0-40/	0-84/	0-72/
(psi)	6	7	8	8	10	9
Range of/average combined flowrate	62–118/		50–106/		51-126/	
(gpm) ^(e)	79		74		85	
Range of/average daily flowrate	70–97/		NA/		55-142/	
(gpm) ^(f)	94		NA		81	
Cumulative throughput to 10µg/L As						
breakthrough ^(g) (gal)	5,255,800		7,915,800		7,256,800	
Media run length to $10\mu g/L$ As						
breakthrough (BV) ^(h)	61,600		92,800		85,100	

Table 4-4. Summary of Isolux[™] Treatment System Operations

NA=not available.

(a) System shutdown from January 18 through April 26, 2006, due to well rehabilitation activities.

(b) Calculated based on total operating time and number of days in operation.

(c) Calculated based on throughput from individual totalizer and 5.7 ft³ (or 42.65 gal) of media in each module.

(d) Instantaneous flowrate readings from individual flow meters.

(e) Combined instantaneous flowrate readings from both modules.

(f) Calculated by dividing incremental wellhead volume readings by corresponding operating times.

(g) Breakthrough when average arsenic concentration from both modules exceeded 10 μ g/L.

(h) Calculated based on throughput from individual totalizers and 11.4 ft³ (or 85.3 gal) of media in both modules combined.

The Isolux[™] treatment system operated for 1,377, 1,900, and 1,422 hr during Media Runs 1, 2, and 3, respectively, based on the system throughput and average instantaneous flowrate from both modules

combined. During Media Runs 1 and 2, from October 26, 2005, through August 15, 2006 (except when the system was shut down for well rehabilitation), the system operated daily (with some weekends); average operating times were 21.9 and 20.2 hr/day, respectively. Due to seasonal fluctuation in water demand, the system only operated periodically during Media Run 3, with an average operating time of 16.7 hr/day.

During the performance evaluation study, the system throughput values at 10 μ g/L arsenic breakthrough in the combined effluent of both modules were 5,255,800 gal (or 61,600 BV), 7,915,800 gal (or 92,800 BV), and 7,256,800 (or 85,100 BV) during Media Runs 1, 2, and 3, respectively. The BV for the system was calculated based on a total of 11.4 ft³ (or 85.3 gal) of media in both modules, while the BV for each module was based on 5.7ft³ (or 42.65 gal) of media in each module. The total flow processed through the system was based on the sum of the throughput values through each of the two modules measured, with individual totalizers installed on the modules. Individually, the number of BV processed through each module during each media run was slightly different. During Media Runs 1, 2, and 3, Module A processed 62,760, 91,520, and 91,100 BV, or 4%, 6%, and 20% more water than Module B, respectively. This indicated an imbalanced flow between Modules A and B.

Figure 4-10 compares instantaneous flowrates through Module A, Module B, combined instantaneous flowrates, and average flowrates at the wellhead (when the hour meter was functioning correctly). The average flowrates at the wellhead were calculated by dividing incremental volume readings that the wellhead totalizer recorded by the corresponding operating times recorded by the hour meter. Due to lack of equipment and/or equipment failure, hour meter readings used to calculate the average flowrates were available only from December 8, 2005, through January 17, 2006, and from December 26, 2006, through March 20, 2007. The flowrates through each module recorded by the individual flow meters/totalizers



Figure 4-10. Isolux[™] Treatment System Daily Flowrates
installed on the adsorption modules varied significantly, ranging from 17 to 71 gpm through Module A and from 20 to 69 gpm through Module B. The average flowrate for all media runs was 42 and was 38 gpm for Modules A and B, respectively. The average flowrate through Module A was 10% higher than that through Module B, again indicating imbalanced flow. Flowrates calculated based on the totalizer at the wellhead averaged 94 and 81 gpm for Media Runs 1 and 3, respectively, which was approximately 19% higher than the 79 gpm measured by individual flow meters during Media Run 1 and 4.7% lower than the 85 gpm measured by individual flow meters during Media Run 3, respectively. Based on the respective average flowrates, the average EBCTs in Modules A and B were 1.0 and 1.1 min, respectively, which were 100% and 120 % higher than the design value of 0.5 min as shown in Table 4-3.

Figure 4-11 presents measured pressure readings across the Isolux[™] Treatment System. The pressure readings prior to the bag filter at each module varied significantly due to the accumulation of particulate/sediment matter in the bag filter and periodic replacement of the bag filter. Prior to the bag filter, pressure readings ranged from 14 to 106 psi. Inlet or after bag-filter pressure readings varied somewhat, ranging from 11 to 46 psi; outlet pressures remained relatively constant, ranging from 8 to 17 psi.

Figures 4-12 and 4-13, respectively, presents differential pressure (Δp) readings across bag filters and across Modules A and B. Δp readings across the bag filters varied significantly, ranging from 0 to 84 psi. The variation in Δp readings was due mainly to the accumulation of particulates in the bag filter and replacement of the bag filters. The Δp readings across Modules A and B also varied significantly, ranging from 2 to 26 psi and averaging 13 and 14 psi, respectively. The variance in Δp readings across the modules most likely was caused by the significant variation in instantaneous flowrate readings. As shown in Figure 4-14, there is a direct relationship between Δp across Modules A and B and the instantaneous flowrate readings.

4.4.2 System/Operation Reliability and Simplicity. The simplicity of the system operation and operator skill requirements are discussed according to pre-and post-treatment activities, levels of system automation, operator skill requirements, preventative maintenance activities, and frequency of chemical/media handling and inventory requirements.

Pre- and Post-Treatment Requirements. The majority of arsenic in raw water existed as As(V). As such, a pre-oxidation step was not required. However, the facility has a pre-chlorination system in place for disinfectant purposes. The only pre-treatment required was the use of 1-µm bag filters to remove sediments/particulate matter from raw water.

System Automation. All major functions of the treatment system were automated and would require only minimal operator oversight and intervention if all functions were operating as intended. The operator controlled the system operation manually. Once the treated water in the storage tanks reached a determined level, the high-level alarm was triggered, notifying the operator to shut down the system.

Operator Skill Requirements. Under normal operating conditions, the skill requirements to operate the system were minimal. The operator was typically onsite five times per week and spent approximately 30 min each day performing visual inspections and recording system operating parameters on the daily log sheets. The operator replaced the bag filter periodically. Normal operation of the system did not require additional skills beyond those necessary to operate the existing water supply equipment.

The State of California requires that all individuals who operate or supervise the operation of a drinkingwater treatment facility possess a water treatment operator certificate. The state also requires those who make decisions on maintenance and operation of any portion of the distribution system possess a



Figure 4-11. Pressure Readings Across Bag Filter and Module A (top) and Bag Filter and Module B (bottom)







Figure 4-13. Differential Pressure Readings Across Modules A and B



Figure 4-14. Instantaneous Flowrate vs. Differential Pressure

distribution operator certificate (CDPH, 2001). Operator certifications are granted by CDPH after minimum requirements are met; these include passing an examination and maintaining a minimum number of hours of specialized training. There are five grades of operators for both the water treatment (i.e., T1 to T5) and distribution (i.e., D1 to D5), with T5 and D5 being the highest. The operator of the Isolux[™] system possessed T2 and D2 certifications for treatment and distribution, respectively.

Preventive Maintenance Activities. Preventive maintenance tasks included items such as periodic checks of flowmeters and pressure gauges and inspection of system piping and valves. The vendor recommended replacing the bag filters once it was necessary to replace the media cartridges; however, the operator had to replace the bag filters periodically due to increased differential pressure readings.

Chemical/Media Handling and Inventory Requirements. After installation of the IsoluxTM treatment system, chlorine addition continued at the GHCSD site. Inventory requirements for chlorine addition remained the same as before. To facilitate change-out when needed, the only onsite inventory requirements associated with the IsoluxTM system were bag filters and media cartridges.

4.5 System Performance

The performance of the Isolux[™] arsenic treatment system was evaluated based on analyses of water samples collected from the treatment plant and distribution system.

4.5.1 Treatment Plant Sampling. The treatment plant water was sampled on 54 occasions (including one duplicate sampling), with field speciation performed 11 times. Table 4-5 summarizes the analytical results for arsenic, iron, manganese, and zirconium.

				Concentration						
	Sampling						Standard			
Parameter	Location	Unit	Count	Minimum	Maximum	Average	Deviation ^(a)			
	IN - R1	μg/L	9	11.4	14.0	12.7	0.9			
	IN - R2	μg/L	16	10.0	14.4	11.5	1.2			
	IN - R3	μg/L	29	9.8	16.9	12.3	1.4			
	AC - R1	μg/L	9	11.5	13.9	12.5	0.8			
	AC - R2	μg/L	16	10.0	12.8	11.3	0.9			
	AC - R3	μg/L	29	10.4	16.1	12.1	1.2			
	MA - R1	μg/L	5	0.3	12.4	_(b)	_(b)			
As (total)	MA - R2	μg/L	11	5.2	9.3	_(b)	_(b)			
	MA - R3	μg/L	27	5.0	11.1	_(b)	_(b)			
	MB - R1	μg/L	5	0.4	11.9	_(b)	_ ^(b)			
	MB - R2	μg/L	11	3.0	12.2	_(b)	_(b)			
	MB - R3	μg/L	27	0.4	11.3	_(b)	_(b)			
	TM - R1	μg/L	4	0.4	12.2	_(b)	_(b)			
	TM - R2	μg/L	5	1.3	10.5	_(b)	_(b)			
	TM - R3	μg/L	2	4.1	4.7	_(b)	_(b)			
	IN - R1	μg/L	4	11.1	13.9	12.5	1.3			
	IN - R2	μg/L	5	0.4	14.3	11.9	1.6			
	IN - R3	μg/L	2	11.1	12.3	11.7	0.8			
A ~	AC - R1	μg/L	4	12.1	13.9	12.8	0.8			
AS (colublo)	AC - R2	μg/L	5	10.4	12.8	11.7	1.0			
(soluble)	AC - R3	μg/L	2	11.4	12.0	11.7	-			
	TM - R1	μg/L	4	0.4	13.1	_ ^(b)	_(b)			
	TM - R2	μg/L	5	1.3	10.5	_ ^(b)	_(b)			
	TM - R3	μg/L	2	3.9	4.5	_ ^(b)	_(b)			
	IN - R1	μg/L	4	<0.1	0.99	0.49	0.5			
	IN - R2	μg/L	5	<0.1	0.83	0.24	0.4			
	IN - R3	μg/L	2	<0.1	1.7	1.1	-			
A a	AC - R1	μg/L	4	< 0.1	0.31	0.15	0.2			
AS (particulate)	AC - R2	μg/L	5	< 0.1	< 0.1	< 0.1	-			
(particulate)	AC - R3	μg/L	2	0.26	0.78	0.52	-			
	TM - R1	μg/L	4	< 0.1	0.16	_(b)	_(b)			
	TM - R2	μg/L	5	< 0.1	0.22	_(b)	_(b)			
	TM - R3	μg/L	2	0.15	0.21	_(b)	_(b)			
	IN - R1	μg/L	4	2.0	2.8	2.5	0.4			
	IN - R2	μg/L	5	0.14	1.6	0.61	0.4			
	IN - R3	μg/L	2	1.5	1.8	1.6	-			
	AC - R1	μg/L	4	0.46	1.2	0.76	0.3			
As(III)	AC - R2	μg/L	5	0.14	0.96	0.26	0.1			
	AC - R3	μg/L	2	0.24	0.59	0.44	-			
	TM - R1	μg/L	4	0.17	0.96	_ ^(b)	_ ^(b)			
	TM - R2	μg/L	5	0.17	0.43	_(b)	_ ^(b)			
	TM - R3	μg/L	2	0.17	0.58	_(b)	_(b)			
	IN - R1	μg/L	4	8.3	11.1	10.0	1.4			
	IN - R2	μg/L	5	9.4	13.8	11.1	1.7			
$A_{\alpha}(M)$	IN - R3	μg/L	2	9.6	10.4	10.0	_			
AS(V)	AC - R1	μg/L	4	11.4	13.4	12.1	0.9			
	AC - R2	μg/L	5	10.2	12.3	11.5	1.0			
	AC - R3	μg/L	2	11.2	11.4	11.3	-			

Table 4-5. Summary of Analytical Results for Arsenic, Iron, Manganese, and Zirconium

				Concentration						
	Sampling						Standard			
Parameter	Location	Unit	Count	Minimum	Maximum	Average	Deviation ^(a)			
	TM - R1	μg/L	4	< 0.1	12.7	_(b)	_(b)			
AS(V)	TM - R2	μg/L	5	1.1	10.1	_(b)	_(b)			
(Con t)	TM - R3	μg/L	2	3.4	4.3	_(b)	_ ^(b)			
	IN - R1	μg/L	9	<25	<25	<25	-			
	IN - R2	μg/L	16	<25	<25	<25	-			
	IN - R3	μg/L	7	<25	<25	<25	-			
	AC - R1	μg/L	9	<25	<25	<25	-			
	AC - R2	μg/L	16	<25	<25	<25	-			
	AC - R3	μg/L	7	<25	<25	<25	-			
	MA - R1	μg/L	5	<25	<25	<25	-			
Fe (total)	MA - R2	μg/L	11	<25	<25	<25	-			
	MA - R3	µg/L	5	<25	<25	<25	-			
	MB - R1	μg/L	5	<25	<25	<25	-			
	MB - R2	μg/L	11	<25	<25	<25	-			
	MB - R3	μg/L	5	<25	<25	<25	-			
	TM - R1	μg/L	4	<25	<25	<25	-			
	TM - R2	μg/L	5	<25	<25	<25	-			
	TM - R3	μg/L	2	<25	<25	<25	-			
	IN - R1	μg/L	4	<25	<25	<25	-			
	IN - R2	ug/L	5	<25	<25	<25	-			
	IN - R3	ug/L	2	<25	<25	<25	_			
	AC - R1	ug/L	4	<25	<25	<25	_			
Fe (soluble)	AC - R2	$\frac{\mu g}{L}$	5	<25	<25	<25	-			
1 • (Seraere)	AC - R3	$\frac{\mu g}{L}$	2	<25	<25	<25	_			
	TM - R1	$\mu g/L$	4	<25	<25	<25	_			
	TM - R2	$\mu g/L$	5	<25	<25	<25	_			
	TM - R3	$\mu g/L$	2	<25	<25	<25	_			
	IN - R1	$\mu g/L$	9	2.9	53	3.8	0.7			
	IN - R2	$\mu g/L$	16	2.9	43	3.9	0.7			
	IN - R3	$\mu g/L$	7	3.7	4 7	4 1	0.1			
	AC - R1	μ <u>σ</u> /Ι	9	2.8	4.7	3.8	0.5			
	$AC = R^2$	μ <u>σ</u> /Ι	16	2.0	4.5	3.8	0.0			
	AC = R2	$\mu g/L$	2	2.5	3.8	3.6	U.T			
	MA - R1	$\mu g/L$	5	<0.1	0.23	0.12	0.1			
Mn (total)	MA - R2	μg/L μg/I	11	<0.1	2.1	1.0	0.1			
will (total)	MA - R2	μg/L μg/I	5	0.17	0.01	0.56	0.0			
	MR - R1	μg/L μg/I	5	<0.1	0.91	0.30	0.2			
	MB P2	μg/L μg/I	11	<0.1	0.04	0.20	0.3			
	MD - K2	μg/L μg/I	5	0.14	0.93	0.33	0.3			
	TM D1	μg/L μg/I	3	0.11	0.29	0.20	0.1			
	TM D2	μg/L uα/I	4	0.13	0.31	0.25	0.1			
	TM - R2	μg/L wα/I	3	0.38	1.7	0.7	0.5			
		μg/L	<u> </u>	0.30	0.5	0.4	-			
		μg/L	4	<u> </u>	3.5	4.0	0.9			
	$\frac{11N - KZ}{1N - B2}$	μg/L	2	3.8	4.4	4.1	0.2			
М .,	$\frac{11N - K3}{AC - D1}$	μg/L	<u> </u>	3.9	4.5	4.1	-			
VIn	AC - KI	μg/L	4	3.2	4.8	3./ 2.5	0.8			
(soluble)	AC - KZ	μg/L	2	2.1	4.0	3.3	0.5			
	AU - K3	μg/L	<u> </u>	3.3	3.8	3.0	-			
	TM D2	μg/L	4	0.02	0.56	0.25	0.2			
	1 IVI - K2	µg/L	5	0.38	1./	0.72	0.5			

Table 4-5. Summary of Analytical Results for Arsenic, Iron, Manganese, and Zirconium (Continued)

				Concentration								
Parameter	Sampling Location	Unit	Count	Minimum	Maximum	Average	Standard Deviation ^(a)					
Mn												
(soluble)												
(Con't)	TM - R3	μg/L	2	0.30	0.53	0.41	-					
	IN - R1	μg/L	9	< 0.1	< 0.1	< 0.1	-					
	IN - R2	μg/L	16	< 0.1	< 0.1	< 0.1	-					
	IN - R3	μg/L	7	<0.1	<0.1	< 0.1	-					
	AC - R1	μg/L	9	<0.1	< 0.1	< 0.1	-					
	AC - R2	μg/L	16	< 0.1	< 0.1	< 0.1	-					
	AC - R3	μg/L	7	< 0.1	< 0.1	< 0.1	-					
	MA - R1	μg/L	5	< 0.1	< 0.1	<0.1	-					
Zr (total)	MA - R2	μg/L	11	< 0.1	< 0.1	<0.1	-					
	MA - R3	μg/L	5	< 0.1	< 0.1	< 0.1	-					
	MB - R1	μg/L	5	< 0.1	< 0.1	< 0.1	-					
	MB - R2	μg/L	11	< 0.1	< 0.1	< 0.1	-					
	MB - R3	μg/L	5	< 0.1	< 0.1	< 0.1	-					
	TM - R1	μg/L	4	< 0.1	< 0.1	< 0.1	-					
	TM - R2	μg/L	5	< 0.1	< 0.1	< 0.1	-					
	TM - R3	μg/L	2	< 0.1	< 0.1	<0.1	-					

 Table 4-5. Summary of Analytical Results for Arsenic, Iron, Manganese, and

 Zirconium (Continued)

(a) Standard deviation for parameters that were non-detect for all samples or had <3 sample counts are not meaningful and therefore are not presented.

(b) Statistics not meaningful; see arsenic breakthrough curves at MA, MB, and TM locations in Figure 4-16.

See Appendix B for complete analytical results.

One-half of the detection limit was used for non-detect results, duplicate samples were included for calculations.

R1 = Media Run 1; R2 = Media Run 2; R3 = Media Run 3.

Table 4-6 summarizes the results of other water quality parameters. Appendix B contains a complete set of analytical results for the study. Results of the water samples collected throughout the treatment plant are discussed below.

Arsenic Removal. Figure 4-15 contains three bar charts showing the concentrations of total As, particulate As, As(III), and As(V) at the IN, AC, and TM locations for each of the 11 speciation events. Arsenic concentrations in source water were consistent for Media Runs 1, 2, and 3 (Table 4-5). Total arsenic concentrations in source water ranged from 9.8 to 16.9 μ g/L and averaged 12.2 μ g/L. As expected, of the soluble fraction, As(V) was the predominating species, ranging from 8.3 to 13.8 μ g/L and averaging 10.4 μ g/L. As(III) concentrations ranged from 0.14 to 2.8 μ g/L and averaged 1.6 μ g/L. Particulate As concentrations were low, averaging 0.61 μ g/L. The arsenic concentrations measured during the study were consistent with those of the source water sample collected by Battelle on October 13, 2004 (Table 4-1).

As expected, arsenic concentrations at the AC locations were essentially the same as those in source water and were consistent for Media Runs 1, 2, and 3 (Table 4-5). Total arsenic concentrations ranged from 10.0 to 16.1 μ g/L and averaged 12.0 μ g/L. Of the soluble fraction, As(V) was the predominating species, ranging from 10.2 to 13.4 μ g/L and averaging 11.6 μ g/L. Due to prechlorination, and thus oxidation of As(III) to As(V), As(III) concentrations were slightly lower than for source water, ranging from 0.14 to 1.2 μ g/L and averaging 0.49 μ g/L. Particulate As concentrations were low, averaging 0.24 μ g/L.

					Concentration					
	Sampling						Standard			
Parameter	Location	Unit	Count	Minimum	Maximum	Average	Deviation ^(a)			
	IN – R1	mg/L	9	176	330	201	48.7			
	IN – R2	mg/L	16	188	200	193	3.8			
	IN – R3	mg/L	7	190	209	201	7.6			
	AC - R1	mg/L	9	176	198	188	7.0			
	AC - R2	mg/L	16	184	205	193	5.6			
	AC - R3	mg/L	7	192	208	202	5.5			
A 11 1: : 4	MA - R1	mg/L	5	176	194	186	7.4			
Alkalinity	MA - R2	mg/L	11	184	200	193	6.4			
$(as CaCO_3)$	MA - R3	mg/L	5	190	209	203	7.7			
	MB - R1	mg/L	5	176	189	182	5.0			
	MB - R2	mg/L	11	188	204	192	4.6			
	MB - R3	mg/L	5	190	203	200	5.5			
	TM - R1	mg/L	4	185	189	187	2.3			
	TM - R2	mg/L	5	171	194	188	9.4			
	TM - R3	mg/L	2	202	207	205	-			
	IN - R1	mg/L	4	0.14	0.20	0.16	0.0			
	IN - R2	mg/L	5	0.20	10.2	2.3	4.4			
	IN - R3	mg/L	2	0.30	0.90	0.60	-			
	AC - R1	mg/L	4	0.14	0.20	0.16	0.0			
Fluoride	AC - R2	mg/L	5	0.20	12.3	3.1	5.2			
	AC - R3	mg/L	2	0.10	0.60	0.35	-			
	TM - R1	mg/L	4	0.14	0.20	0.16	0.0			
	TM - R2	mg/L	5	0.20	8.4	1.9	3.6			
	TM - R3	mg/L	2	< 0.1	0.60	0.33	-			
	IN - R1	mg/L	4	39.0	46.0	42.0	3.2			
	IN - R2	mg/L	5	47.0	49.0	47.8	0.8			
	IN - R3	mg/L	2	46.0	52.0	49.0	-			
	AC - R1	mg/L	4	40.0	46.0	42.6	2.6			
Sulfate	AC - R2	mg/L	5	46.0	56.0	49.4	4.2			
	AC - R3	mg/L	2	46.0	52.0	49.0	-			
	TM - R1	mg/L	4	40.0	46.0	43.3	2.5			
	TM - R2	mg/L	5	46.0	57.0	49.4	4.5			
	TM - R3	mg/L	2	46.0	51.0	48.5	-			
	IN - R1	mg/L	4	0.36	0.48	0.43	0.1			
	IN - R2	mg/L	5	0.56	0.72	0.65	0.1			
	IN - R3	mg/L	2	0.67	0.73	0.70	-			
NUtrata	AC - R1	mg/L	4	0.35	0.48	0.43	0.1			
INITIATE	AC - R2	mg/L	5	0.58	0.75	0.68	0.1			
(as N)	AC - R3	mg/L	2	0.65	0.72	0.69	-			
	TM - R1	mg/L	4	0.35	0.5	0.44	0.1			
	TM - R2	mg/L	5	0.58	0.69	0.64	0.0			
	TM - R3	mg/L	2	< 0.05	0.66	0.34	-			

 Table 4-6.
 Summary of Water Quality Parameter Sampling Results

				Concentration							
	Sampling						Standard				
Parameter	Location	Unit	Count	Minimum	Maximum	Average	Deviation ^(a)				
	IN - R1	mg/L	9	26.7	29.5	27.7	0.8				
	IN - R2	mg/L	16	27.2	31.7	28.4	1.3				
	IN - R3	mg/L	7	26.4	28.6	27.3	0.7				
	AC - R1	mg/L	9	26.9	28.9	27.8	0.6				
	AC - R2	mg/L	16	26.9	32.3	28.5	1.4				
	AC - R3	mg/L	7	26	29.2	27.4	1.0				
~	MA - R1	mg/L	5	26.3	28.3	27.2	0.8				
Silica	MA - R2	mg/L	11	23.8	32.8	28.2	2.3				
$(as SiO_2)$	MA - R3	mg/L	5	25.8	26.9	26.4	0.4				
	MB - R1	mg/L	5	26.7	27.9	27.3	0.5				
	MB - R2	mg/L	11	27.1	32.0	28.9	1.4				
	MB - R3	mg/L	5	25.6	27.8	26.6	1.0				
	TM - R1	mg/L	4	21.0	28.7	26.1	3.5				
	TM - R2	mg/L	5	26.9	30.5	28.0	1.4				
	TM - R3	mg/L	2	24.4	28.3	26.4	-				
	IN - R1	μg/L	9	<10	<10	<10	-				
	IN - R2	μg/L	16	<10	15.7	5.4	3.1				
	IN - R3	μg/L	7	<10	11.1	5.9	2.3				
	AC - R1	μg/L	9	<10	<10	<10	-				
	AC - R2	μg/L	16	<10	11.3	5.4	1.6				
	AC - R3	μg/L	7	<10	11.4	5.9	2.4				
D	MA - R1	μg/L	5	<10	<10	<10	-				
P (eq D)	MA - R2	μg/L	11	<10	<10	<10	-				
(as P)	MA - R3	μg/L	5	<10	<10	<10	-				
	MB - R1	μg/L	5	<10	<10	<10	-				
	MB - R2	μg/L	11	<10	<10	<10	-				
	MB - R3	μg/L	5	<10	<10	<10	-				
	TM - R1	μg/L	4	<10	<10	<10	-				
	TM - R2	μg/L	5	<10	<10	<10	-				
	TM - R3	μg/L	2	<10	<10	<10	-				
	IN - R1	NTU	9	<0.1	1.6	0.3	0.5				
	IN - R2	NTU	16	0.1	4.6	0.6	1.1				
	IN - R3	NTU	7	< 0.1	6.2	1.0	2.3				
	AC - R1	NTU	9	< 0.1	1.1	0.2	0.3				
	AC - R2	NTU	16	0.1	2.6	0.5	0.6				
	AC - R3	NTU	7	0.1	0.3	0.3	0.1				
	MA - R1	NTU	5	< 0.1	1.1	0.3	0.4				
Turbidity	MA - R2	NTU	11	0.1	1.1	0.5	0.3				
	MA - R3	NTU	5	0.1	0.2	0.2	0.0				
	MB - R1	NTU	5	< 0.1	0.2	0.1	0.1				
	MB - R2	NTU	11	0.1	2	0.6	0.7				
	MB - R3	NTU	5	0.1	0.1	0.1	0.0				
	TM - R1	NTU	4	< 0.1	0.2	0.1	0.1				
	TM - R2	NTU	5	0.2	0.5	0.3	0.1				
	TM - R3	NTU	2	0.3	0.5	0.4	-				

 Table 4-6. Summary of Water Quality Parameter Sampling Results (Continued)

				Concentration							
	Sampling						Standard				
Parameter	Location	Unit	Count	Minimum	Maximum	Average	Deviation ^(a)				
	IN - R1	S.U.	9	7.5	7.7	7.6	0.1				
	IN - R2	S.U.	15	7.4	7.7	7.5	0.1				
	IN - R3	S.U.	28	7.4	7.9	7.6	0.1				
	AC - R1	S.U.	9	7.4	7.8	7.6	0.1				
	AC - R2	S.U.	15	7.5	7.7	7.5	0.1				
	AC - R3	S.U.	28	7.5	8.0	7.7	0.1				
	MA - R1	S.U.	8	7.5	7.7	7.6	0.1				
pН	MA - R2	S.U.	14	7.4	7.6	7.5	0.0				
1	MA - R3	S.U.	28	7.5	7.9	7.6	0.1				
	MB - R1	S.U.	8	7.5	7.7	7.6	0.1				
	MB - R2	S.U.	15	7.5	7.7	7.5	0.1				
	MB - R3	S.U.	28	7.5	7.9	7.6	0.1				
	TM - R1	S.U.	6	7.3	7.7	7.5	0.2				
	TM - R2	S.U.	15	7.4	7.7	7.5	0.1				
	TM - R3	S.U.	28	7.5	7.9	7.6	0.1				
	IN - R1	°C	9	15.7	20.3	18.1	1.3				
	IN - R2	°C	15	14.9	30.8	22.1	3.6				
	IN - R3	°C	28	14.5	22.6	17.9	2.3				
	AC - R1	°C	9	16.0	20.6	18.4	1.4				
	AC - R2	°C	15	19.1	26.4	21.4	2.0				
	AC - R3	°C	28	15.2	22.2	18.2	2.0				
	MA - R1	°C	8	14.0	25.6	18.6	3.4				
Temperature	MA - R2	°C	14	19.2	26.3	21.4	2.1				
1	MA - R3	°C	28	15.8	22.0	18.4	1.8				
	MB - R1	°C	8	15.8	25.7	19.2	2.9				
	MB - R2	°C	15	19.1	26.2	21.3	2.1				
	MB - R3	°C	28	15.8	21.9	18.5	1.6				
	TM - R1	°C	6	14.8	19.3	17.8	1.6				
	TM - R2	°C	15	19.2	26.2	21.9	2.0				
	TM - R3	°C	28	15.2	22.9	18.3	2.0				
	IN - R1	mg/L	6	1.8	2.7	2.3	0.3				
	IN - R2	mg/L	13	2.0	3.2	2.5	0.4				
	IN - R3	mg/L	28	1.4	4.5	2.9	0.8				
	AC - R1	mg/L	6	1.7	2.2	1.9	0.2				
	AC - R2	mg/L	13	1.8	3.0	2.2	0.3				
	AC - R3	mg/L	28	1.4	4.2	2.5	0.6				
	MA - R1	mg/L	6	1.8	2.3	2.1	0.1				
DO	MA - R2	mg/L	12	1.9	2.9	2.3	0.3				
	MA - R3	mg/L	28	1.5	3.6	2.6	0.5				
	MB - R1	mg/L	6	1.8	2.9	2.0	2.0				
	MB - R2	mg/L	13	1.7	4.3	2.5	0.7				
	MB - R3	mg/L	28	1.7	3.5	2.6	0.5				
	TM - R1	mg/L	5	1.6	2.6	2.3	0.4				
	TM - R2	mg/L	13	1.7	2.9	2.3	0.3				
	TM - R3	mg/L	28	1.6	3.6	2.6	0.5				

 Table 4-6. Summary of Water Quality Parameter Sampling Results (Continued)

				Concentration						
	Sampling						Standard			
Parameter	Location	Unit	Count	Minimum	Maximum	Average	Deviation ^(a)			
	IN - R1	mV	9	359	472	422	38.3			
	IN - R2	mV	15	257	450	336	54.5			
	IN - R3	mV	28	219	507	319	58.2			
	AC - R1	mV	9	470	647	585	62.5			
	AC - R2	mV	15	280	686	557	125			
	AC - R3	mV	28	288	666	551	132			
	MA - R1	mV	8	597	675	643	24.6			
ORP	MA - R2	mV	14	285	660	597	116			
	MA - R3	mV	28	295	679	573	135			
	MB - R1	mV	8	579	676	645	31.0			
	MB - R2	mV	15	293	679	613	112			
	MB - R3	mV	28	308	682	580	136			
	TM - R1	mV	6	534	680	629	56.7			
	TM - R2	mV	15	66	676	573	179			
	TM - R3	mV	28	311	683	581	136			
	IN - R1	mg/L	9	153	184	174	9.1			
	IN - R2	mg/L	16	158	220	184	15.0			
	IN - R3	mg/L	7	174	207	192	11.2			
	AC - R1	mg/L	9	154	186	175	8.8			
	AC - R2	mg/L	16	116	154	133	9.4			
	AC - R3	mg/L	7	174	209	194	11.9			
Total	MA - R1	mg/L	5	169	184	176	7.5			
Hardness	MA - R2	mg/L	11	163	211	185	11.6			
(as CaCO ₃)	MA - R3	mg/L	5	173	206	188	12.0			
· · · · · · · · · · · · · · · · · · ·	MB - R1	mg/L	5	170	184	176	6.7			
	MB - R2	mg/L	11	166	212	184	11.2			
	MB - R3	mg/L	5	153	206	188	10.6			
	TM - R1	mg/L	4	153	184	173	13.4			
	TM - R2	mg/L	5	171	209	190	14.7			
	TM - R3	mg/L	2	201	215	208	-			
	IN - R1	mg/L	9	100	137	127	10.8			
	IN - R2	mg/L	16	117	161	134	11.1			
	IN - R3	mg/L	7	124	157	141	11.2			
	AC - R1	mg/L	9	101	138	126	10.5			
	AC - R2	mg/L	16	116	154	133	9.4			
	AC - R3	mg/L	7	124	157	143	12.3			
	MA - R1	mg/L	5	122	137	130	6.1			
Ca Hardness	MA - R2	mg/L	11	122	153	135	8.7			
(as CaCO ₃)	MA - R3	mg/L	5	101	155	137	12.8			
	MB - R1	mg/L	5	121	137	130	6.2			
	MB - R2	mg/L	11	122	154	133	8.2			
	MB - R3	mg/L	5	127	154	137	10.9			
	TM - R1	mg/L	4	101	136	124	16.0			
	TM - R2	mg/L	5	122	150	138	11.1			
	TM - R3	mg/L	2	150	160	155	-			

 Table 4-6. Summary of Water Quality Parameter Sampling Results (Continued)

				Concentration							
Parameter	Sampling Location	Unit	Count	Minimum	Maximum	Average	Standard Deviation ^(a)				
	IN - R1	mg/L	9	41.7	52.8	47.2	3.2				
	IN - R2	mg/L	16	41.0	59.7	50.1	4.6				
	IN - R3	mg/L	7	47.0	54.0	51.1	2.8				
	AC - R1	mg/L	9	42.8	55.5	48.8	3.7				
	AC - R2	mg/L	16	39.8	57.8	50.2	4.3				
	AC - R3	mg/L	7	46.5	54.9	51.5	3.0				
Mg	MA - R1	mg/L	5	42.9	49.6	46.3	3.0				
Hardness	MA - R2	mg/L	11	40.7	58.0	50.6	4.2				
(as CaCO ₃)	MA - R3	mg/L	5	45.3	53.5	50.4	3.4				
	MB - R1	mg/L	5	42.7	51.6	46.6	3.8				
	MB - R2	mg/L	11	40.9	57.5	50.2	4.2				
	MB - R3	mg/L	5	44.6	53.6	50.8	3.7				
	TM - R1	mg/L	4	47.3	52.7	48.7	2.6				
	TM - R2	mg/L	5	48.4	58.5	52.2	3.9				
	TM - R3	mg/L	2	50.6	54.5	52.5	-				

 Table 4-6.
 Summary of Water Quality Parameter Sampling Results (Continued)

(a) Standard deviation for parameters that were non-detect for all samples or had <3 sample counts are not meaningful, and therefore are not presented.

See Appendix B for complete analytical results.

One-half detection limit used for nondetect results; duplicate samples were included for calculations.

R1 = Media Run 1; R2 = Media Run 2; R3 = Media Run 3.

The key parameter for evaluating the effectiveness of the $Isolux^{TM}$ system was the concentration of arsenic in the treated water. The arsenic breakthrough curves for each media run are shown in Figure 4-16, in which total arsenic concentrations are plotted against the volume of water treated in gallons and bed volumes (BV).

Bed volumes for MA and MB were calculated based on 5.7 ft³ or 42.65 gal of media in each module; however, bed volumes of the combined effluent (TM) were calculated based on the combined media volume and throughput of both modules, since water at the sampling location had been treated by the entire media volume.

Media Run 1 began with system start-up on October 26, 2005, and ended on January 17, 2006. During Media Run 1, arsenic concentrations at MA and MB reached 10 μ g/L at approximately 61,600 BV, which was 41% lower than the 105,000 BV estimated by the vendor. The bag-filters were changed six times due to increased differential pressure readings caused by the build-up of sediments and particulates. Thus, it was possible that sub-micron particulates that passed through the bag filters accumulated in and partially blocked some of the passages on the media cartridges' outer membrane, causing preferential flow through the media cartridges. Preferential flow could cause portions of a media cartridge to filter a larger amount of water, thus exhausting the media at a higher rate. To investigate the cartridges, analyses were conducted on a spent media cartridge; results are presented in Section 4.5.3.

Media Run 2 began on April 27, 2006, following media cartridge change-out and ended on August 15, 2006. Prior to the start of Media Run 2, the well was bailed and wire-brushed on March 7, 2006, and a wire strainer was installed upstream of the Isolux[™] system to reduce the amount of sediment/particulate matter produced by the well and introduced into the treatment system. During Media Run 2, the initial



Figure 4-15. Concentrations of Various Arsenic Species at IN, AC, and TM Sampling Locations



Figure 4-16. Total Arsenic Concentrations Through Treatment System During Media Runs 1 to 3

arsenic concentrations measured at MA and MB were approximately 6.0 and 4.0 μ g/L, respectively, where they remained until gradually increasing to 10 μ g/L breakthrough. Arsenic concentrations at MB reached 10 μ g/L at about 86,700 BV; arsenic concentrations at MA increased to 9.3 μ g/L after approximately 91,520 BV. However, the average effluent of MA and MB did not exceed 10 μ g/L until August 8, 2006, after approximately 92,800 BV of throughput. Longer media run lengths were observed during Media Run 2; however, the calculated system operating time (i.e., 21.9 versus 20.2 hr/day) and EBCT (i.e., 1.1 versus 1.2 min) were similar. The well thereby rehabilitation might have reduced the amount of sediments and particulates produced by the well, thereby reducing the potential for preferential flow through the media cartridges and thus extending the life of the media.

Media Run 3 began on August 17, 2006, following media cartridge change-out and ended with the conclusion of the performance evaluation study on March 20, 2007. During Media Run 3, initial arsenic concentrations at MA and MB also were elevated at 7.0 and 3.0 μ g/L, respectively. Arsenic concentrations at MA spiked above 10 μ g/L at about 49,700 BV before gradually decreasing to 6.8 μ g/L at 63,600 BV. On March 13, 2007, arsenic concentrations at MB reached 10 μ g/L at about 76,200 BV, while arsenic concentration at MA remained below 10 μ g/L at 7.4 μ g/L after the system had treated approximately 82,000 BV of water. The average effluent of MA and MB exceeded 10 μ g/L on March 20, 2007, after treating approximately 85,100 BV of water. Similar media run lengths were observed during Media Runs 2 and 3; the intermittent system operation (i.e., 16.7 versus 20.2 hr/day) did not seem to affect the media run length.

Iron, Manganese, and Zirconium. The treatment plant water samples were analyzed for total iron, manganese, and zirconium at each sampling event and for soluble iron, manganese, and zirconium during speciation sampling. Total and soluble iron concentrations were below the method detection limit of 25 μ g/L in source water and throughout the treatment train. Manganese concentrations in source water ranged from 2.9 to 5.3 μ g/L, which existed primarily in the soluble form at an average concentration of 4.1 μ g/L. Total manganese concentrations in the effluent of MA and MB averaged 0.6 and 0.3 μ g/L, respectively. Figure 4-17 presents total manganese concentrations versus bed volumes across the treatment train for all media runs. Zirconium concentrations in raw water and across the treatment train were below its detection limit of 0.1 μ g/L, indicating zirconium was not leached from the IsoluxTM-302M media.

pH. The pH of Zero Point of Charge (pH_{zpc}) for zirconium hydroxide based media such as IsoluxTM-302M is 10 to 11. Above the pH of the ZPC, the media surface is negatively charged, and electrostatic repulsion will occur between the surface and an anion; this repulsion must be overcome for sorption to occur by a specific chemical bond. As(V) is more strongly sorbed and affected by pH in the range of 4 to 9 (Siegel, et al., 2007). pH of source water ranged from 7.4 to 7.9 and averaged 7.6, which is well below the pH of the ZPC and within the operational range of 4 to 8.5 (Figure 4-18).

DO and ORP. DO and ORP readings averaged 2.6 mg/L and 359 millivolts (mV), respectively, in source water. Both parameters indicated that the well water was oxidizing, which was consistent with the presence of As(V) in raw water. As a result of prechlorination, the ORP readings at AC, MA, MB, and TM increased to an average of 597 mV.

Other Water Quality Parameters. Alkalinity ranged from 176 to 330 mg/L (as CaCO₃) in raw water and remained unchanged after treatment. Sulfate, fluoride, and nitrate were measured during speciation sampling, and silica was measured at each sampling event. Their concentrations in raw water ranged from 39 to 52 mg/L for sulfate; 0.1 to 0.9 mg/L for fluoride, with one outlier of 10.2 mg/L; 0.4 to 0.7 mg/L (as N) for nitrate; and 26.4 to 31.7 mg/L for silica (as SiO₂) and remained unchanged after treatment.



Figure 4-17. Total Mn Concentrations Through Treatment System During Media Runs 1 to 3



Figure 4-18. Relationship Between pH and Surface Charge of Media (Modified from Stumm and Morgan, 1981)

Total phosphorous (as P) concentrations were below the detection limit of 10 μ g/L for all measurements, except for four detections of (10.2, 10.6, 15.7, and 11.1 μ g/L on March 30, June 13, June 21, and October 4, 2006, respectively) at the IN location and 11.3 and 11.4 μ g/L on June 13 and October 4, 2006, respectively, at the AC location (Appendix B). Total hardness ranged from 153 to 220 mg/L (as CaCO₃), and remained relatively constant throughout the treatment train.

4.5.2 Distribution System Sampling. Distribution water samples were collected at three residences before and after the installation/operation of the IsoluxTM system to determine whether the treatment system had any impacts on the lead and copper levels and water chemistry in the distribution system. The samples were analyzed for pH, alkalinity, arsenic, iron, manganese, lead, and copper; results are presented in Table 4-7. Since system startup, arsenic concentrations in the distribution system decreased slightly from the baseline levels of 2.8, 6.0, and 5.2 µg/L (on average) to 2.0, 3.3, and 3.1 µg/L at the DS1, DS2, and DS3 sampling locations, respectively. These concentrations were somewhat lower than those of the plant effluent (Figure 4-19), presumably due to blending of the treated water with untreated water from wells that did not have elevated arsenic levels.

Lead and copper concentrations ranged from <0.1 to 8.7 μ g/L and 19.9 to 885.1 μ g/L, respectively. No samples exceeded the 15 μ g/L-Pb or 1,300 μ g/L-Cu action levels. Due to blending of water from 12 other wells, it was inconclusive whether these distribution system concentrations had been affected by the arsenic treatment system.

pH, alkalinity, and manganese concentrations remained fairly consistent, with average baseline levels at 7.6, 173 mg/L, and 0.6 μ g/L, and after startup levels at 7.8, 173 mg/L, and 0.2 μ g/L, respectively. Iron was not detected in any samples.

4.5.3 Spent Media Sampling. Samples of spent Isolux[™]-302M media samples from Media Run 1 were collected according to Section 3.3.4 for TCLP and total metals analyses. Figure 4-20 presents photographs taken during spent media sampling.

The TCLP results provided by MEI (Table 4-8) indicated that the Isolux[™]-302M media was nonhazardous and could be disposed of in a standard solid waste landfill. However, MEI opted to send the spent media cartridges to GemChem, Inc., an Environmental Management Company in Lititz, PA, for beneficial reuse. The spent media was combined with similar products for use as fill materials in applications such as quarry reclamation.

					DS	51 ^(a)				DS2							D	S3							
				L	.CR Re	esidenc	е					No	n-LCR	Reside	ence					Noi	n-LCR	Reside	nce		
					1st	draw							1st	draw							1st E	Draw			
Sa I	impling Event	Stagnation Time	Н	Alkalinity (as CaCO ₃)	As	Fe	ЧМ	Pb	Cu	Stagnation Time	Hd	Alkalinity (as CaCO ₃)	As	Fe	nM	Pb	Cu	Stagnation Time	Hd	Alkalinity (as CaCO ₃)	As	Fe	Mn	Pb	Cu
No.	Date	hrs	S.U.	mg/L	µg/L	µg/L	µg/L	µg/L	µg/L	hrs	S.U.	mg/L	µg/L	µg/L	µg/L	µg/L	µg/L	hrs	S.U.	mg/L	µg/L	µg/L	µg/L	µg/L	µg/L
BL1	07/19/05	10.5	7.6	176	3.1	<25	0.8	1.9	221	9.4	7.5	176	6.3	<25	1.1	0.8	110	7.5	7.6	176	4.5	<25	0.5	1.1	773
BL2	08/04/05	11.0	7.6	176	5.1	<25	1.1	0.6	148		Hom	eowner n	iot prese	nt for sai	mple coll	ection.		9.5	7.6	180	5.1	<25	0.8	0.9	789
BL3	08/16/05	8.3	7.7	163	1.7	<25	0.1	1.0	136	9.2	7.6	176	5.1	<25	0.5	0.4	90.7	8.5	7.6	176	6.3	<25	0.6	0.8	724
BL4	08/30/05	9.0	7.6	163	1.5	<25	<0.1	0.3	78.0	8.2	7.5	172	6.6	<25	0.7	0.2	41.1	9.0	7.5	167	4.9	<25	0.6	0.9	724
1	11/01/05	11.8	7.6	176	3.7	<25	0.2	0.5	75.5	9.4	7.8	167	6.7	<25	0.3	0.6	85.7	19.5	7.9	167	6.6	<25	0.4	0.9	885
2	12/06/05	8.5	7.8	145	2.5	<25	0.2	0.2	56.4	8.7	7.8	167	3.9	<25	0.3	0.3	59.7	7.0	8.0	167	3.4	<25	0.3	0.3	357
3	01/04/06	11.5	7.8	180	1.6	<25	<0.1	0.5	53.5	9.6	7.9	180	4.5	<25	<0.1	0.4	105		Home	eowner n	ot preser	nt for san	nple colle	ection.	-
4	05/17/06 ^(b)		Home	eowner no	ot preser	nt for sar	nple colle	ection.		8.4	7.7	155	2.6	<25	18.2	7.5	183	8.0	7.7	159	2.6	<25	18.4	8.7	208
5	06/06/06	8.8	7.8	160	1.6	<25	<0.1	0.1	106	9.1	7.7	173	2.5	<25	0.5	<0.1	19.9	8.5	7.8	169	2.5	<25	0.1	0.2	247
6	07/12/06 ^(c)	12.3	7.7	168	1.4	<25	0.3	0.3	66.0	8.1	7.7	184	2.3	<25	0.4	0.6	133	7.0	NA ^(d)	NA ^(d)	2.4	<25	0.3	0.7	857
7	08/09/06	8.5	7.7	168	1.8	<25	< 0.1	0.3	77.2	9.0	7.7	181	3.8	<25	0.1	0.7	151	8.3	7.7	181	3.7	<25	< 0.1	0.7	508
8	09/13/06	9.0	7.8	165	1.6	<25	<0.1	0.1	106	9.4	7.8	183	1.6	<25	<0.1	0.5	84.4	7.8	7.8	186	1.7	<25	<0.1	0.8	574
9	10/11/06		Home	eowner no	ot preser	nt for sar	nple colle	ection.		8.3	7.6	194	1.9	<25	<0.1	0.9	529	8.8	7.7	210	1.8	<25	<0.1	0.6	130

Table 4-7. Distribution System Sampling Results

(a) BL1 and BL2 were collected from a non-LCR residence.
(b) DS3 sample collected on 05/18/06.
(c) DS3 sample collected on 07/13/06.
(d) Samples were past hold time.
BL = Baseline sampling; NA = data not available.



Figure 4-19. Total Arsenic Concentrations in Distribution System



Figure 4-20. Spent Media Sampling

(Clockwise from Top Left: Spent Media Surface with Outer Membrane Removed, Visual of Spent Media from Outer Surface to Inner Membrane [I] and [II], Sample Collection into Dishes, Mottled Appearance on Outer Surface)

	Isolux [™] -302M
Parameter	Leachate Concentration (mg/L)
As	< 0.05
Ba	1.4
Cd	< 0.05
Cr	< 0.05
Pb	<0.1
Hg	< 0.003
Se	< 0.3
Ag	< 0.05

Table 4-8. TCLP Results of Spent Media

Provided by MEI.

Visual observations of the spent media cartridge indicated sediment accumulation on the outer membrane of the cartridge and on the outer surface of the annular space immediately under the outer membrane. Figure 4-21 shows dark to light brown colors of the outer membrane of a typical cartridge removed from the system. Once the outer membrane was cut away, the outer surface of the media displayed a mottled appearance (Figure 4-22), which may be indicative of the actual distribution of the incoming flow. Iron concentrations of the spent media taken across the annular space of the cartridge averaged 800, 30, <0.5, and 128 μ g/g for the outer surface, subsurface, mid-portion, and inner portion, respectively, thus confirming the visual observations of sediment accumulation on the media. The iron concentration measured at the inner portion was higher than at the mid-portion; this suggests channeling of the incoming flow, which might have contributed, in part, to the short run length observed during Media Run 1.



Figure 4-21. Spent Media Cartridge Removed from Isolux[™] System (Provided by MEI)



Figure 4-22. Spent Media Cartridge with Outer Membrane Cut Away (Provided by MEI)

Table 4-9 presents the results of metals analyses. Arsenic concentrations across the annular space of the media cartridge were relatively consistent, averaging 271, 285, 321, and 249 μ g/g from the outer surface to the inner portion. These values were lower than the loading (i.e., 814 μ g/g or about 0.08%) based on the system throughput and the arsenic concentrations before and after the treatment system. The differences observed most likely were caused by the relatively small quantaties of the samples taken for the metal analyses. Also, the results of Al, Si, P, Mn, and Cu analyses further support the speculation of channeling, which resulted in metal concentrations measured at the inner portion being higher than those of the mid-portion of the media cartridge.

4.6 System Cost

The system cost was evaluated based on the capital cost per gpm (or gpd) of the design capacity and the O&M cost per 1,000 gal of water treated. The capital cost included the cost for equipment, site engineering, and installation. The O&M cost included cost for media cartridges, bag filters, electricity, and labor.

4.6.1 Capital Cost. The capital investment for equipment, site engineering, and installation of the IsoluxTM treatment system was \$76,840 (see Table 4-10). The equipment cost was \$58,500 (or 76% of the total capital investment), which included \$48,000 for two 75-gpm IsoluxTM Modules, \$8,000 for 36 IsoluxTM technology media cartridges (18 media cartridges per module), and \$2,500 for shipping.

The engineering cost included the cost for preparing the required permit application submittal, including system specifications, P&IDs, electrical diagrams, interconnection of piping layouts, and obtaining the required permit approval from CDPH. The engineering cost was \$8,500, or 11% of the total capital investment.

Sample						An	alyte Co	oncentra	tion (µg	g/g)				
Description	Analysis	Mg	Al	Si	Р	Ca	Mn	Fe	Ni	Cu	Zn	As	Cd	Pb
	А	576	535	410	722	5,925	790	847	0.7	38.2	724	258	1.9	1.3
Outer	В	541	485	380	734	6,030	748	755	0.6	37.7	723	279	1.8	1.3
surface	С	602	512	375	736	6,083	776	799	0.8	39.4	749	275	1.9	1.3
	Average	573	511	389	731	6,013	771	800	0.7	38.4	732	271	1.8	1.3
	А	551	187	353	636	5,620	<125	30.3	< 0.5	5.8	789	304	2.1	< 0.5
Subaurface	В	551	186	379	626	5,645	<125	33.8	< 0.5	5.6	752	290	2.1	< 0.5
Subsultace	С	500	169	248	627	5,486	<125	26.0	< 0.5	5.4	755	262	2.0	< 0.5
	Average	534	181	327	629	5,584	-	30.0	-	5.6	765	285	2.0	-
	А	500	78.2	400	309	5,617	<125	< 0.5	< 0.5	< 0.5	587	334	2.0	< 0.5
Mid nortion	В	481	47.6	284	280	5,258	<125	< 0.5	< 0.5	< 0.5	574	307	2.1	< 0.5
Mid-portion	С	519	66.8	417	303	5,592	<125	< 0.5	< 0.5	< 0.5	572	322	1.9	< 0.5
	Average	500	64.2	367	297	5,489	-	-	-	-	577	321	2.0	-
	А	481	116	455	383	5,458	156	118	< 0.5	5.0	578	234	2.0	< 0.5
Innor portion	В	525	144	441	380	5,686	154	133	< 0.5	5.2	584	268	1.9	< 0.5
miler portion	C	517	122	426	372	5,554	162	134	< 0.5	5.2	587	246	2.1	< 0.5
	Average	508	127	441	378	5,566	157	128	-	5.1	583	249	2.0	-

Table 4-9. Spent Media Analysis

The installation, shakedown, and startup cost covered the labor and materials required to unload, install, and test the system for proper operation. All installation activities were performed by MEI and GHCSD; startup and shakedown activities were performed by MEI with the operator's assistance. The installation, startup, and shakedown costs, were \$9,840, or 13% of the total capital investment.

			% of Capital								
Description	Ouantity	Cost	Cost								
Equipment											
Isolux [™] 75 gpm module 2 \$48,000 -											
Isolux [™] technology media cartridges	36	\$8,000	_								
Freight	-	\$2,500	_								
Equipment Total	-	\$58,500	76%								
Engine	ering										
Vendor material	-	\$1,500	_								
Vendor labor		\$2,000									
Subcontractor material	-	\$2,000									
Subcontractor labor	-	\$3,000									
Engineering Total	-	\$8,500	11%								
Installation, Shaked	lown, and St	artup									
Material (mechanical)	-	\$500	_								
Material (electrical)	-	\$300									
Vendor labor (mechanical)	-	\$6,480									
Vendor travel	-	\$2,560									
Installation, Shakedown, and Startup	-	\$9,840	13%								
Total Canital Investment	_	\$76.840	100%								

Table 4-10. Capital Investment for MEI's Isolux[™] Treatment System

The total capital cost of \$76,840 was normalized to \$512/gpm (\$0.36/gpd) of design capacity using the system's rated capacity of 150 gpm (or 216,000 gpd). The total capital cost also was converted to an annualized cost of \$7,253/year, using a capital recovery factor of 0.09439 based on a 7% interest rate and a 20-year return. Assuming that the system was operated 24 hours a day, 7 days a week at the design flow rate of 150 gpm to produce 78,840,000 gal of water per year, the unit capital cost would be \$0.09/1,000 gal. This calculation assumed that the system operated 24 hr/day at its rated capacity. The system operated 19.6 hr/day (on average) at approximately 79.3 gpm (on average) (see Table 4-4). Based on this reduced use rate, the system would produce only 34,038,700 gal of water in one year (assuming 365 days per year), and the unit capital cost would increase to \$0.21/1,000 gal.

4.6.2 Operation and Maintenance Cost. The O&M cost included media cartridge replacement and disposal, electricity consumption, and labor. Table 4-11 summarizes the O&M cost.

The cost to replace and dispose of the spent media cartridges represented the majority of the O&M cost (i.e., \$7,080 for 36 cartridges in two modules). By averaging this cost over the useful life of the media, the unit cost per 1,000 gal of water treated was plotted as a function of the media life (i.e., run length in BV), as shown in Figure 4-23. The media run length (in BV) was calculated by dividing the system throughput (in gal) by the quantity of media in both modules (i.e., 11.4 ft³ [or 85.3 gal]). The IsoluxTM system processed an average of 61,600, 92,800, and 85,100 BV prior to reaching the 10 µg/L arsenic breakthrough during Media Runs 1, 2, and 3, respectively. Based on these volumes, the unit media replacement cost was \$1.35, \$0.89, and \$0.98/1,000 gal, respectively.

Category	Value	Remarks
Media	Cartridge Replacen	nent
Isolux [™] media cartridges (\$/changeout)	\$6,480	36 cartridges (18 cartridges/module)
Transportation	\$600	36 cartridges (18 cartridges/module)
Media cartridge replacement (\$/1,000 gal)	See Figure 4-23	
Elec	tricity Consumptio	n
Electricity Cost (\$/1,000 gal)	\$0.001	Electrical cost negligible
	Labor	
Labor (hr/week)	2.5	30 min/day, 5 day/week
Labor Cost (\$/1,000 gal)	\$0.14	Labor rate = $37.5/hr^{(a)}$
Total O&M Cost (\$/1,000 gal)	See Figure 4-23	

Table 4-11. O&M Cost for MEI's Isolux[™] Treatment System

(a) O/M labor would be higher if a contract operator was required.

The IsoluxTM treatment modules contained booster pumps that required electricity; however, the booster pumps were not used during the study. Therefore, additional electrical cost incurred by the IsoluxTM system operation was assumed to be negligible.

Under normal operating conditions, routine labor activities to operate and maintain the system consumed 2.5 per week as noted in Section 4.4.2. Assuming that the system operates at an average flowrate of 79.3 gpm for 19.6 hr/day and 7 day/week to produce 653,000 gal of water per week, the estimated labor cost would be \$0.14/1,000 gal of water treated.



Note: 1 BV = media volume in both modules

Figure 4-23. Total O&M Cost, Including Media Replacement

5.0 REFERENCES

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APPENDIX A

OPERATIONAL DATA

	I I					Well C												Т	reatment Syst	em											
					Totalizer to Treatment	Totalizer to Treatment	Volume In	Average Flowrate	Mod 1	lule A Flow Fotalizer	Module A Cum Flow Totalizer	Module A Volume In	Module A Bed Volumes	Mod 1	dule B Flow Fotalizer	Module B Cum Flow Totalizer	Module B Volume In	Module B Bed Volumes	Total Water Treated	Cum Water Treated	Cum Bed Volumes		Module	A Press	sure (psig	3)		Module B	Pressure	a (psig)	
Week	Day of Week	Date and Time	Meter Hours	Op Hours	acre-ft	gal	gal	gpm	gpm	gal	gal	gal	BV	gpm	gal	gal	gal	BV	gal			Before Bag- Filter	After Bag- Filter	Outlet	ΔP Across Bag- Filter	ΔP Across Module	Before Bag- Filter	After Bag- Filter (Ac B Dutlet F	ΔP ross lag- A ilter N	ΔP cross lodule
	T	10/25/05 16:00	NM	NA NA	446.95	145,436,879	80.810	NA NA	43	33,500	33,500	33,500	785	45	31,400	31,400	31,400	736	64,900	64,900 152,300	761	31	NM 32	15	NA	NA 18	30	NM 28	14	2	
1	R	10/27/05 11:40	NM	NA	447.60	145.649.040	122.350	NA	41	142,500	142,500	65.300	3.341	38	138.800	138.800	63,700	3.254	129.000	281.300	3.298	32	30	14	2	16	31	28	12	3	16
	F	10/28/05 8:15	NM	NA	447.93	145,754,795	105,755	NA	43	187,700	187,700	45,200	4,401	40	182,200	182,200	43,400	4,272	88,600	369,900	4,336	32	30	14	2	16	32	28	12	4	16
	M	10/31/05 6:25	NM	NA	448.96	146,090,282	335,487	NA	41	363,300	363,300	175,600	8,518	34	336,900	336,900	154,700	7,899	330,300	700,200	8,209	40	32	12	8	20	42	23	12	19	11
	Т	11/1/05 8:00	NM	NA	449.31	146,205,799	115,517	NA	40	424,800	424,800	61,500	9,960	36	388,000	388,000	51,100	9,097	112,600	812,800	9,529	44	29	13	15	16	46	23	12	23	11
2	W	11/2/05 8:15	NM	NA	449.65	146,315,134	109,334	NA	40	483,300	483,300	58,500	11,332	31	435,000	435,000	47,000	10,199	105,500	918,300	10,766	52	30	12	22	18	56	24	11	32	13
	F	11/4/05 6:30	NM	NA	449.99	146 528 922	103 477	NA	38	104 500	587,800	50,300	13 782	38	3 103 000	538,000	50,600	12 614	100,000	1.125.800	13,198	20	20	12	2	16	20	20	11	0	15
	M	11/7/05 6:45	NM	NA	451.34	146 866 687	337 765	NA	38	268,900	752 200	164 400	17,637	38	267 700	702 700	164 700	16 476	329 100	1 454 900	17 056	24	24	9	0	15	24	24	8	0	16
	T	11/8/05 6:15	NM	NA	451.68	146,976,672	109,985	NA	38	322,200	805,500	53,300	18,886	37	320,900	755,900	53,200	17,723	106,500	1,561,400	18,305	26	26	10	0	16	24	24	8	0	16
	W	11/9/05 6:45	NM	NA	452.03	147,089,911	113,239	NA	37	364,900	848,200	42,700	19,887	37	363,500	798,500	42,600	18,722	85,300	1,646,700	19,305	23	23	10	0	13	23	23	8	0	15
3	R	11/10/05 6:45	NM	NA	452.37	147,199,896	109,985	NA	38	419,000	902,300	54,100	21,156	37	416,400	851,400	52,900	19,962	107,000	1,753,700	20,559	24	24	11	0	13	24	23	11	1	12
	F	11/11/05 8:27	NM	NA	452.72	147,314,112	114,215	NA	38	476,000	959,300	57,000	22,492	37	470,300	905,300	53,900	21,226	110,900	1,864,600	21,859	25	25	11	0	14	25	24	11	1	13
	Su	11/13/05 8:25	NM	NA	453.05	147,423,440	105,334	NA NA	39	589,000	1,013,800	56,500	25,017	32	5 521,100	1 002 700	46 600	23,417	107,300	2 075 000	24,326	39	30	13	2 9	17	39	20	13	14	12
	M	11/14/05 12:00	NM	NA	453 78	147 660 988	132 112	NA	31	589 400	1 072 700	400	25 151	31	568,000	1,002,100	300	23,517	700	2 075 700	24 334	24	24	10	0	14	24	24	11	0	13
	T	11/15/05 7:10	NM	NA	454.05	147,747,545	86,556	NA	36	631,500	1,114,800	42,100	26,138	36	610,300	1,045,300	42,300	24,509	84,400	2,160,100	25,324	26	26	11	0	15	26	26	11	0	15
4	W	11/16/05 6:25	NM	NA	454.31	147,830,847	83,302	NA	37	672,000	1,155,300	40,500	27,088	37	651,000	1,086,000	40,700	25,463	81,200	2,241,300	26,275	28	32	14	4	18	28	28	14	0	14
	R	11/17/05 6:55	NM	NA	454.64	147,940,832	109,985	NA	37	726,000	1,209,300	54,000	28,354	36	5 704,500	1,139,500	53,500	26,717	107,500	2,348,800	27,536	30	30	14	0	16	28	28	12	0	16
	M	11/21/05 6:20	NM	NA	454.65	147,941,483	651	NA	57	726,300	1,209,600	300	28,361	56	5 704,900	1,139,900	400	26,727	700	2,349,500	27,544	38	38	12	0	26	38	38	12	0	26
5	1	11/22/05 6:20	NM	NA	455.03	148,068,064	126,581	NA NA	42	789,300	1,272,600	59,600	29,838	42	820,600	1,200,100	60,200	28,138	123,200	2,472,700	28,988	32	32	12	0	20	32	32	12	0	20
	M	11/28/05 7:45	NM	NA	455.57	148 240 851	55 318	NA NA	40	876,500	1 359 800	27 600	31,230	45	846 200	1 281 200	25 600	29,440	53,200	2 641 000	30,961	50	32	14	18	24	50	30	12	20	10
	T	11/29/05 8:20	NM	NA	455.95	148,366,130	125,279	NA	40	939,300	1,422,600	62,800	33,355	38	905,800	1,340,800	59,600	31,437	122,400	2,763,400	32,396	70	32	14	38	18	70	30	12	40	18
	Ŵ	11/30/05 8:50	NM	NA	456.34	148,492,385	126,255	NA	43	1,001,100	1,484,400	61,800	34,804	42	967,300	1,402,300	61,500	32,879	123,300	2,886,700	33,842	32	32	12	0	20	30	30	12	0	18
6	R	12/1/05 6:50	NM	NA	456.69	148,607,251	114,866	NA	40	1,056,800	1,540,100	55,700	36,110	41	1,023,100	1,458,100	55,800	34,188	111,500	2,998,200	35,149	30	32	12	2	20	30	32	12	2	20
	F	12/2/05 8:45	NM	NA	457.10	148,739,364	132,112	NA	40	1,120,900	1,604,200	64,100	37,613	40	1,087,500	1,522,500	64,400	35,698	128,500	3,126,700	36,655	30	32	14	2	18	30	30	14	0	16
	Sa	12/3/05 9:00	NM	NA	457.47	148,860,087	120,723	NA NA	39	1,179,600	1,662,900	58,700	38,989	40	1,146,500	1,581,500	59,000	37,081	117,700	3,244,400	38,035	30	31	14	1	1/	30	31	14	1	1/
	M	12/4/05 8:00	NM	NA	457.83	149,970,233	113,239	NA NA	39	1,230,100	1 774 700	55,300	40,314	38	1 291 400	1,038,200	88 200	40.478	143 500	3 501 100	41 045	29	30	14	0	16	20	29	14	0	10
	T	12/6/05 8:00	NM	NA	458.53	149,205,662	116,168	NA	39	1,348,500	1,831,800	57,100	42,950	38	3 1,314,400	1,749,400	23,000	41,018	80,100	3,581,200	41,984	30	30	14	0	16	30	30	14	0	16
7	W	12/7/05 8:00	0.0	0.0	458.88	149,318,250	112,588	NA	39	1,404,500	1,887,800	56,000	44,263	37	1,368,000	1,803,000	53,600	42,274	109,600	3,690,800	43,268	32	31	14	1	17	32	30	14	2	16
	R	12/8/05 8:00	22.4	22.4	459.22	149,430,839	112,588	83.8	40	1,462,500	1,945,800	58,000	45,623	35	1,419,700	1,854,700	51,700	43,487	109,700	3,800,500	44,555	40	30	14	10	16	40	30	14	10	16
	F	12/9/05 8:00	46.1	23.7	459.55	149,536,594	105,755	74.4	44	1,522,500	2,005,800	60,000	47,029	26	1,463,300	1,898,300	43,600	44,509	103,600	3,904,100	45,769	48	32	14	16	18	52	22	14	30	8
	M T	12/12/05 12:00	71.0	24.9	459.88	149,643,976	107,382	71.9	44	1,597,800	2,081,100	75,300	48,795	44	1,497,800	1,932,800	34,500	45,318	109,800	4,013,900	47,056	32	32	14	0	18	32	32	14	0	18
	W	12/13/05 6:45	93.0	22.0	460.22	149,750,690	105 104	83.4	40	1,649,900	2,133,200	52,100	51,016	40	1,550,200	2 036 600	52,400	40,540	104,500	4,118,400	49,201	32	32	14	0	18	32	30	14	- 2	16
8	R	12/15/05 8:00	139	25.0	460.93	149,985,320	123,327	82.2	39	1,760,400	2,243,700	59,500	52,607	40	1,661,900	2,096,900	60,300	49,165	119,800	4,340,600	50,886	30	28	14	2	14	28	28	12	0	16
1	F	12/16/05 5:50	162	23.0	461.27	150,095,956	110,636	80.2	38	1,813,600	2,296,900	53,200	53,855	40	1,716,400	2,151,400	54,500	50,443	107,700	4,448,300	52,149	30	28	12	2	16	28	28	10	0	18
1	Sa	12/17/05 8:40	189	27.0	461.66	150,222,862	126,906	78.3	37	1,874,300	2,357,600	60,700	55,278	38	1,779,400	2,214,400	63,000	51,920	123,700	4,572,000	53,599	32	30	12	2	18	30	30	12	0	18
	Su	12/18/05 8:25	213	24.0	461.99	150,332,848	109,985	76.4	36	1,925,900	2,409,200	51,600	56,488	38	1,834,700	2,269,700	55,300	53,217	106,900	4,078,900	54,852	38	30	14	8	16	30	30	14	0	16
	T	12/19/05 6:40	235	22.0	462.30	150,433,396	100,549	76.2	34	2 020 000	2,455,800	46,600	58 715	30	1 942 600	2,321,300	56,300	54,427	104 700	4,777,100	57 231	40 42	28	14	10	16	38	30	14	12	16
9	w	12/21/05 10:00	235	27.0	463.00	150.659.875	118,771	73.3	31	2.073.000	2,556,300	52,100	59,937	39	2.006.600	2,441,600	64.000	57.247	116,100	4,997,900	58,592	48	26	12	22	14	46	28	12	18	16
	R	12/22/05 6:50	307	21.0	463.27	150,748,383	88,509	70.2	30	2,110,300	2,593,600	37,300	60,811	39	2,055,000	2,490,000	48,400	58,382	85,700	5,083,600	59,597	54	24	12	30	12	52	28	10	24	18
	Т	1/3/06 14:35	310	3.00	463.317	150,763,352	14,968	83.2	45	2,116,600	2,599,900	6,300	60,959	51	2,063,300	2,498,300	8,300	58,577	14,600	5,098,200	59,768	70	32	10	38	22	68	32	10	36	22
	W	1/4/06 8:00	340	30.0	463.813	150,924,750	161,398	89.7	44	2,193,400	2,676,700	76,800	62,760	46	5 2,144,100	2,579,100	80,800	60,471	157,600	5,255,800	61,615	30	30	10	0	20	30	30	10	0	20
11	R	1/5/06 8:00	364	24.0	464.217	151,056,212	131,462	91.3	43	2,256,400	2,739,700	63,000	64,237	44	2,208,800	2,643,800	64,700	61,988	127,700	5,383,500	63,113	30	30	10	0	20	30	30	10	0	20
1	F	1/6/06 12:40	392	28.0	464.685	151,208,499	152,287	90.6	43	2,329,700	2,813,000	/ 3,300	67.074	43	2,283,900	2,718,900	/5,100	64,200	96 600	5,628,500	65 985	30	30	12	0	18	30	30	12	36	18
1	Su	1/8/06 8:40	437	22.5	465.382	151,435.303	109,009	80.7	41	2,439,900	2,923,200	62,500	68,539	41	2,396,600	2,831,600	63,800	66,392	126,300	5,754,800	67,465	33	34	15	1	19	30	32	15	2	17
i	M	1/9/06 8:30	460	23.4	465.746	151,553.748	118,446	84.4	40	2,496,600	2,979,900	56,700	69,869	40	2,453,300	2,888,300	56,700	67,721	113,400	5,868,200	68,795	31	30	14	1	16	31	30	12	1	18
1	Т	1/10/06 8:00	484	23.6	466.102	151,669,591	115,842	81.8	40	2,553,800	3,037,100	57,200	71,210	39	2,453,300	2,888,300	0	67,721	57,200	5,925,400	69,465	31	30	14	1	16	31	30	12	1	18
12	W	1/11/06 15:00	515	31.0	466.562	151,819,275	149,684	80.5	39	2,627,300	3,110,600	73,500	72,933	38	2,581,100	3,016,100	127,800	70,717	201,300	6,126,700	71,825	36	30	14	6	16	36	28	12	8	16
	R	1/12/06 7:25	531	16.0	466.799	151,896,395	77,120	80.3	38	2,665,100	3,148,400	37,800	73,819	37	2,618,200	3,053,200	37,100	71,587	74,900	6,201,600	72,703	40	30	14	10	16	40	28	14	12	14
1	F	1/13/06 7:00	580	23.0	467.134	152,005,404	109,009	79.0	35	2,717,500	3,200,800	52,400	75,048	38	2,6/1,900	3,106,900	53,700	74,002	108,100	6 415 900	75,947	48	30	14	18	16	48	30	14	30	16
—	Ja	1/14/00 8.30	530	20.0		102,110,090	111,207	11.3	52	2,101,300	0,201,200	50,400	10,230	30	2,120,100	5,104,700	57,000	74,202	100,200	3,110,000	10,210	52	20	14	34	14	00	55			10
13	м	1/16/06 9:00	580	0.0	467,420	152.098 468	NA	NA	59	2,768,200	3.251.500	300	76,237	59	2,730,000	3,165,000	300	74,209	600	6.416.500	75,223	42	40	16	2	24	41	40	14	1	26
1		1/17/06 7:20	602	22.0	467 922	150 000 500	124.065	07.1	41	2 925 100	2 209 400	56,000	77 571	20	2 795 200	2 220 200	EE 200	75 505	112 200	6 528 700	76 538	20	20	14		16	20	20	10	10	10

Table A-1. U.S. EPA Arsenic Demonstration Project at Tehachapi, CA – Daily System Operation Log Sheet



Table A-1. U.S. EPA Arsenic Demonstration Project at Tehachapi, CA – Daily System Operation Log Sheet (Continued)

A-2

											/stem	reatment Sys	Т										1	Well C						1	
No. No. <th>Prossura (psia)</th> <th>Modulo B Pros</th> <th></th> <th>a)</th> <th>uro (neir</th> <th></th> <th>Modula</th> <th></th> <th>Cum Bed</th> <th>water</th> <th>er Cum</th> <th>Total Water</th> <th>Module B Bed</th> <th>Module B</th> <th>Module B Cum Flow</th> <th>dule B Flow</th> <th>Mo</th> <th>Module A Bed</th> <th>Module A</th> <th>Module A Cum Flow</th> <th>Ile A Flow</th> <th>Modu</th> <th>Average</th> <th>Volume In</th> <th>Totalizer to</th> <th>Totalizer to</th> <th></th> <th></th> <th></th> <th></th> <th></th>	Prossura (psia)	Modulo B Pros		a)	uro (neir		Modula		Cum Bed	water	er Cum	Total Water	Module B Bed	Module B	Module B Cum Flow	dule B Flow	Mo	Module A Bed	Module A	Module A Cum Flow	Ile A Flow	Modu	Average	Volume In	Totalizer to	Totalizer to					
Med Med Med Med Med	ΔP Across ΔP Bag- Across	After Bag-	Before Bag-	ΔP Across	ΔP Across Bag-	AFIES	After Bag-	Before Bag-	volumes	Baleu		Treated	volumes	Volume III	Totalizer	lotanzer	Γ	Volumes	Volume in	Totalizer	Janzer	Ĩ	Flowrate	Volume in	Treatment	Treatment	Ор	Meter		Day of	
0 0 1 1000000000000000000000000000000000000	Itlet Filter Module	Filter Outlet	Filter 28	Module 13	Filter 0	Outlet 11	Filter 24	Filter 24	97.852	346.800	0 8.3	gal 126.600	BV 98.654	gal 55,400	gal 4.207.600	gal 0 6.992.900	gpm 30	BV 97.050	gal 71.200	gal 4.139.200	gal 6.964.300	gpm 41	gpm NA	gal 128.533	gal 161.870.230	acre-ft 497.450	Hours	Hours	Date and Time 8/14/2006 11:49	Week	Week
Normal with a second	12 1 15	27 12	28	12	1	12	5 24	25	98,948	440,300	00 8,4	5 93,500	99,615	41,000	4,248,600	3 7,033,900	1 33	98,281	52,500	4,191,700	7,016,800	41	NA	95,668	161,965,898	497.744	NA	NM	8/15/2006 8:34	T	43
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	12 11 8	20 12	31	17	3	10	27	30	3,562	303,800	00 3	303,800	3,560	151,500	151,500	1 7,185,400	1 34	3,571	152,300	152,300	7,169,100	30	NA	305,551	162,271,448	498.683	NA	NM	8/21/2006 11:58	M	
44 5 1	10 18 8	3 18 10	32	4	20	10	3 14	34	5,271	449,600	0 4	3 74,300	5,503	41,200	234,400	5 7,268,300	6 35	5,046	29,800	215,200	7,232,000	20	NA	71,913	162,418,854	498.915	NA	NM	8/23/2006 5:55	w	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	8 17 18	26 8	43	3	34	8	5 11	45	6,304	537,700	00 5	7 88,100	6,777	54,300	288,700	1 7,322,600	8 31	5,838	33,800	249,000	7,265,800	20	NA	159,121	162,506,062	499.404	NA	NM	8/24/2006 8:20	R	44
No. No. <th>14 1 10</th> <th>24 14</th> <th>25</th> <th>7</th> <th>1</th> <th>14</th> <th>2 21</th> <th>22</th> <th>7,142</th> <th>609,200 726,200</th> <th>0 6</th> <th>117,000</th> <th>7,850</th> <th>45,800</th> <th>334,500</th> <th>7,368,400</th> <th>1 41</th> <th>6,441</th> <th>25,700</th> <th>274,700</th> <th>7,291,500</th> <th>49</th> <th>NA</th> <th>67,683</th> <th>162,573,745</th> <th>499.612</th> <th>NA</th> <th>NM</th> <th>8/25/2006 8:12</th> <th>F</th> <th></th>	14 1 10	24 14	25	7	1	14	2 21	22	7,142	609,200 726,200	0 6	117,000	7,850	45,800	334,500	7,368,400	1 41	6,441	25,700	274,700	7,291,500	49	NA	67,683	162,573,745	499.612	NA	NM	8/25/2006 8:12	F	
Image: state in the s	10 0 8	3 18 10	19	5	1	10	5 16	15	9,597	818,600	00 8	92,400	10,066	41,600	429,000	7,462,900	5 30	9,135	50,800	389,600	7,406,400	39	NA	93,390	162,785,580	500.263	NA	NM	8/27/2006 8:29	Su	
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	12 0 8	20 12	20	7	1	11	7 18	17	10,905	930,200	00 g	5 111,600	11,245	50,300	479,300	7,513,200	2 30	10,572	J 61,300	450,900	7,467,700	38	NA	113,239	162,898,819	500.611	NA	NM	8/28/2006 11:12	М	
4 1	10 0 7	17 10	17	7	0	9	6 16	16	11,924	017,100	0 1,0	2 86,900	12,162	39,100	518,400	7,552,300	3 30	11,693	47,800	498,700	7,515,500	38	NA	88,509	162,987,328	500.883	NA	NM	8/29/2006 8:25	T	
i 1 0 0.0 0.0 0.0 0.00	10 2 6	3 16 10	18	6	0	10	6 16	16	14,219	212,900	0 1,1	82,400	14,216	36,700	606,000	7,639,900	2	14,230	45,700	606,900	7,623,700	36	NA	198,169	163,185,497	501.235	NA	NM	8/31/2006 9:17	R	45
Image: Problem 1 Image: Problem 2 Problem 2<	10 0 8	18 10	18	6	0	10	6 16	16	15,152	292,500	00 1,2	79,600	15,051	35,600	641,600	7,675,500	1 29	15,261	44,000	650,900	7,667,700	35	NA	80,374	163,265,871	501.739	NA	NM	9/1/2006 5:30	F	
θ 2000 LG 000 LG <th>9 0 8</th> <th>17 9</th> <th>17</th> <th>6</th> <th>0</th> <th>8</th> <th>14</th> <th>14</th> <th>16,426</th> <th>401,100</th> <th>0 1,4</th> <th>8 108,600</th> <th>16,193</th> <th>48,700</th> <th>690,300 729,600</th> <th>7 7,724,200</th> <th>3 26</th> <th>16,666</th> <th>48 500</th> <th>710,800</th> <th>7,727,600</th> <th>36</th> <th>NA NA</th> <th>109,985</th> <th>163,375,856</th> <th>502.077</th> <th>NA NA</th> <th>NM</th> <th>9/2/2006 9:48</th> <th>Sa</th> <th></th>	9 0 8	17 9	17	6	0	8	14	14	16,426	401,100	0 1,4	8 108,600	16,193	48,700	690,300 729,600	7 7,724,200	3 26	16,666	48 500	710,800	7,727,600	36	NA NA	109,985	163,375,856	502.077	NA NA	NM	9/2/2006 9:48	Sa	
θ Ξ <thξ< th=""> Ξ <thξ< th=""> <thξ< th=""></thξ<></thξ<></thξ<>	11 2 7	18 11	20	6	2	12) 18	20	18,382	568,000	00 1,5	79,100	17,951	35,700	765,300	7,799,200	1 27	18,821	43,400	802,700	7,819,500	33	NA	80,374	163,544,738	502.596	NA	NM	9/4/2006 6:40	M	
μ μ	12 5 6	18 12	23	6	2	10	3 16	18	19,506	663,900	00 1,6	95,900	18,983	44,000	809,300	7,843,200	8 27	20,038	51,900	854,600	7,871,400	31	NA	96,644	163,641,382	502.893	NA	NM	9/5/2006 9:32	T	46
$ \begin{array}{ c c c c c c c c c c c c c c c c c c c$	12 5 6	18 12	23	6	22	10	16	22	20,438	/43,400 815,600	1,7	79,500	19,857	37,300	846,600 884 500	7,880,500	1 28	21,027	42,200	896,800 931 100	7,913,600	30	NA NA	80,048	163,721,431	503.139	NA	NM NM	9/6/2006 8:27 9/12/2006 8:15	W	<u> </u>
F F	12 0 8	20 12	20	6	1	12	/ 18	17	23,499	004,500	2,0	188,900	23,311	109,400	993,900	8,027,800	5 30	23,695	79,500	1,010,600	8,027,400	38	NA	189,708	163,984,679	503.948	NA	NM	9/14/2006 11:45	R	47
4 ************************************	12 0 8	20 12	20	6	0	12	3 18	18	24,317	074,200	2,0	69,700	24,040	31,100	1,025,000	8,058,900	30	24,600	38,600	1,049,200	8,066,000	38	NA	71,263	164,055,942	504.167	NA	NM	9/15/2006 16:25	F	
m m	12 2 10	22 12	24	8	0	12	20	20	24,324	282,000	0 2,0	207 200	24,047	300	1,025,300	3 8,059,200 5 8 152 300	7 43	24,607	300	1,049,500	8,066,300	51	NA	200 883	164,056,593	504.169 504.814	NA	NM	9/18/2006 15:48	M	48
a b C < 0	9 0 9	3 18 S	18	8	1	9	5 17	16	27,988	387,400	2,2	2 105,400	27,332	47,000	1,165,400	1 8,199,300	2 31	28,652	58,400	1,222,000	8,238,800	40	NA	106,731	164,373,207	505.142	NA	NM	9/21/2006 0:00	R	40
Image: Probability of the state o	11 2 11	22 11	24	9	2	11	2 20	22	28,001	388,500	2,3	1,100	27,344	500	1,165,900	2 8,199,800	6 42	28,666	J 600	1,222,600	8,239,400	50	NA	976	164,374,183	505.145	NA	NM	9/25/2006 9:10	М	49
9 1	13 4 9	22 13	26	8	4	12	20	24	29,306	499,800	2,4	28,900	28,537	12 200	1,216,800	8,250,700	2 34	30,082	60,400	1,283,000	8,299,800	41	NA	113,239	164,487,422	505.493	NA	NM	9/26/2006 8:36	T	
W W Us2000 65 21 W 0.06 (17) 0.06 (25) 0.06 (17) 0.06 (25) 0.06 (17) 0.06 (25) 0.06 (25) 0.06 (25) 0.06 (25) 0.06 (25) 0.06 (25) 0.06 (25) 0.06 (25) 0.06 (25) 0.05 (25)	14 3 13	2 22 11	30	9	14	10	0 24	29	30,843	630,900	0 2,5	102,200	29,984	48,400	1,278,500	8,312,400	9 38	31,709	53,800	1,352,400	8,369,200	41	NA	104,128	164,619,860	505.900	NA	NM	10/2/2006 14:50	T	50
11 11 01/02/006 12.0 NO NO <th>11 9 11</th> <th>22 11</th> <th>31</th> <th>7</th> <th>14</th> <th>11</th> <th>2 18</th> <th>32</th> <th>31,873</th> <th>718,800</th> <th>00 2,7</th> <th>87,900</th> <th>30,981</th> <th>42,500</th> <th>1,321,000</th> <th>6 8,354,900</th> <th>4 36</th> <th>32,774</th> <th>45,400</th> <th>1,397,800</th> <th>8,414,600</th> <th>38</th> <th>NA</th> <th>89,160</th> <th>164,709,020</th> <th>506.174</th> <th>NA</th> <th>NM</th> <th>10/4/2006 6:54</th> <th>W</th> <th></th>	11 9 11	22 11	31	7	14	11	2 18	32	31,873	718,800	00 2,7	87,900	30,981	42,500	1,321,000	6 8,354,900	4 36	32,774	45,400	1,397,800	8,414,600	38	NA	89,160	164,709,020	506.174	NA	NM	10/4/2006 6:54	W	
by p 0.05500 f 100 km 0.01 km 0.02 km 0.01 km	12 18 12	24 12	42	8	22	12	2 20	42	33,356	845,300	2,8	126,500	32,441	62,300	1,383,300	8,417,200	9 43	34,279	64,200	1,462,000	8,478,800	41	NA	127,882	164,836,902	506.567	NA	NM	10/10/2006 8:23	Т	51
B R 1032/00573 80 M4 607/007 186 607/007 186 607/007 186 180/007 180/007 180/007 180/007 180/007 180/007 180/007 180/007 180/007 180/007 180/007 180/007 180/007 180/07	12 1 16	24 14	29	13	04	14	25	26	34,542	946,400	0 2,8	4 100	33,897	2 500	1,442,900	8 479 300	2 33	35,252	41,500	1,503,500	8,520,300	20	NA	96,590	164,935,498	506.884	NA	NM	10/23/2006 10:50	R T	52
Image: Note of the stand of the st	14 1 13	5 27 14	28	10	1	14	5 24	25	37,438	193,500	00 3,1	243,000	36,406	107,000	1,552,400	8,586,300	8 39	38,478	136,000	1,641,100	8,657,900	49	NA	245,026	165,185,080	507.637	NA	NM	10/25/2006 7:01	R	53
14 10 10 100	12 2 18	30 12	32	14	2	12	3 26	28	37,642	210,900	0 3,2	9 17,400	36,589	7,800	1,560,200	4 8,594,100	3 54	38,703	9,600	1,650,700	8,667,500	64	NA	17,897	165,202,977	507.692	NA	NM	10/30/2006 14:20	M	
b 1	12 4 16	28 12 3 31 14	32	9	6	13	2 26	32	38,760	306,200	0 3,3	5 95,300	37,593	42,800	1,603,000	2 8,636,900 3 8,660,900	4 42	40.614	29.000	1,703,200	8,720,000	61	NA	95,668	165,298,644	507.986	NA	NM	10/31/2006 6:35	w	54
55 T 11/72020 500 No. No. No	13 19 5	18 13	37	8	14	14	6 22	36	42,292	607,500	00 3,6	248,300	40,884	116,400	1,743,400	1 8,777,300	7 41	43,707	131,900	1,864,100	8,880,900	44	NA	251,534	165,603,870	508.924	NA	NM	11/3/2006 8:12	F	
66 w 11114000000 40242 000 1000 40242 000 <	13 8 17	30 13	38	10	12	14	6 24	36	42,305	608,600	00 3,6	3 1,100	40,896	500	1,743,900	1 8,777,800	1 51	43,721) 600	1,864,700	8,881,500	58	NA	1,302	165,605,171	508.928	NA	NM	11/7/2006 8:08	T	55
B8 W 11/24/2006 232 NM NM 509/2581 11/57/2501 34/1 509/2581 350/2581 36/2582 36/2 36/2 36/2 37/1 46/8 37/1 37/1 37/1 37/1 37/1 37/2 <th< th=""><th>14 30 20</th><th>30 10 4 34 14</th><th>44 64</th><th>14</th><th>48</th><th>10</th><th>30</th><th>68</th><th>42,496</th><th>705.900</th><th>0 3,0</th><th>1 10,500</th><th>41,061</th><th>45.300</th><th>1,751,600</th><th>* 8,765,700 7 8.831.000</th><th>5 547</th><th>43,923</th><th>35,500</th><th>1,873,300</th><th>8,890,100</th><th>32</th><th>NA</th><th>81,350</th><th>165,622,092</th><th>508.980</th><th>NA</th><th>NM</th><th>11/15/2006 18:05</th><th>w</th><th>56</th></th<>	14 30 20	30 10 4 34 14	44 64	14	48	10	30	68	42,496	705.900	0 3,0	1 10,500	41,061	45.300	1,751,600	* 8,765,700 7 8.831.000	5 547	43,923	35,500	1,873,300	8,890,100	32	NA	81,350	165,622,092	508.980	NA	NM	11/15/2006 18:05	w	56
99 T 125/2006 848 NM NM Sol 288 165/72.375 10.419 A 6 8.80 156.800 5.000 42.427 530 737.800 73.93 10.500 37.8400 53.580 22.21 11.80 <th< th=""><th>13 19 2</th><th>15 13</th><th>34</th><th>9</th><th>30</th><th>16</th><th>5 25</th><th>55</th><th>43,545</th><th>714,400</th><th>00 3,7</th><th>8,500</th><th>42,256</th><th>4,800</th><th>1,801,900</th><th>8,835,800</th><th>2 50</th><th>44,842</th><th>3,700</th><th>1,912,500</th><th>8,929,300</th><th>48</th><th>NA</th><th>8,460</th><th>165,711,902</th><th>509.256</th><th>NA</th><th>NM</th><th>11/29/2006 8:23</th><th>W</th><th>58</th></th<>	13 19 2	15 13	34	9	30	16	5 25	55	43,545	714,400	00 3,7	8,500	42,256	4,800	1,801,900	8,835,800	2 50	44,842	3,700	1,912,500	8,929,300	48	NA	8,460	165,711,902	509.256	NA	NM	11/29/2006 8:23	W	58
66 M 1/2/2/2/08 5/0 NM NM 500 2014 53.2 PA P 4.000 44000 44.000 4	16 0 19	35 16	35	14	1	16	30	31	43,668	724,900	00 3,7	3 10,500	42,373	5,000	1,806,900	1 8,840,800	1 51	44,971	5,500	1,918,000	8,934,800	64	NA	10,413	165,722,315	509.288	NA	NM	12/5/2006 8:48	T	59
bit W 1227/2006 82:3 3615 233 590 450 992.27 NA 158 001200 158.30 452.00 435.85 992.20 3442.90 455.05 222.20 151 12 4 6 222.20 F 12252000 151.00 47.32 28.857.400 1500 47.73 28.857.400 1500 47.73 28.857.400 1500 47.73 28.857.400 1500 47.73 28.857.400 45.529 85.800 42.000 45.529 85.800 42.000 47.12 26.11 10 24.25 10 10 45.52 10.800 45.259 85.800 42.000 45.529 85.800 42.000 45.52 23.800 42.000 47.12 10 44.20 44.20 10.100 45.52 11.100 45.200 11.100 45.200 11.100 45.200 11.100 45.200 11.100 45.200 11.100 45.200 11.100 45.200 11.100 45.200 11.100 45.200	15 0 21	36 15	36	15	2	16	3 31	33	43,737	730,800	0 3,7	12 900	42,427	2,300	1,809,200	8,843,100	5 50	45,055	3,600	1,921,600	8,938,400	51	NA NA	5,532	165,727,847	509.305	NA NA	3 502	12/12/2006 8:09	M	60
B R 12282000 651 3.33 244 500 101 500 1205500 47.703 28 6.84 400 44.570 93.500 3.93.64.00 46.148 24 10 11 8 52 20 C T T222007081-13 3662 56 510.149 166.115.37 68.27 144.00 44.500 93.500 3.93.64.00 47.732 28 57.500 144.00 40.200 47.732 28.7500 144.00 40.200 47.733 20.200 140.00 44.250 93.600 56.400 44.250 93.500 3.93.600 56.400 44.250 47.733 40.200 140.00 44.250 93.600 56.400 48.260 14.200 140.00 44.250 140.00 44.250 140.00 44.250 140.00 44.251 120.00 140.00 44.260 150.00 120.00 140.00 140.00 140.00 44.260 140.00 24.200 140.00 140.00 120.00 140.00 120.00 120.00	11 2 9	20 12	20	6	4	12	2 18	22	45,052	842,900	00 3,8	5 99,200	43,585	43,200	1,858,600	8,892,500	5 29	46,525	56,000	1,984,300	9,001,100	36	NA	99,247	165,839,785	509.649	23.5	3,615	12/27/2006 8:26	Ŵ	61
IP 1/22/05/00 1/1 3.66 2.55 910.00 1/2.67 2.50 1/2.67 2.50 1/2.67 2.50 1/2.67 2.50 1/2.67 2.50 1/2.67 2.50 1/2.67 2.50 1/2.67 2.50 1/2.67 2.50 1/2.67 2.50 1/2.57 2.50 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.57 1/2.57 2.55 1/2.57 2.57 1/2.57 2.55 1/2.57 2.57 1/2.57 2.55 1/2.57 2.55 1/2.57 2.55 2.27 1/2.57 2.55 2.27 1/2.57 1/2.57 2.55 2.27 1/2.57 1/2.57 1/2.57 1/2.57 1/2.57 1/2.57 1/2.57	10 3 10	20 10	23	5	8	11	16	24	46,148	936,400	00 3,9	93,500	44,570	42,000	1,900,600	8,934,500	3 28	47,733	51,500	2,035,800	9,052,600	33	NA	94,041	165,933,825	509.938	24.4	3,639	12/28/2006 8:51	R	01
ex vi 1/22/07 8/35 558 225 510 449 166/18/275 98/271 Vi 1/22/07 1/21/0	10 6 9	26 11	25	4	12	10	0 14 7 18	20	47,120	122,000	0 4,0	2 300	45,529	40,900	1,941,500	8 976 500	+ 20 2 40	46,734	42,700	2,078,500	9,095,300	20 43		02,320	166,018,104	510.191	25.4	3,005	1/2/2007 8:38	F	-
R 14/42:07 14/2 3.718 28.8 51.84 166.218.876 102.516.400 35.90 50.500 53.9 20.687 10 44.485 102.700 42.228.00 45.505 70 12 10 58 2 46 25 T 11/2007 16.0 3.716 10.3 3161 43.45 100.717.20 22.228.00 45.53 27.100 52.247 31.9 100.2005 10.00 50.393 45.200 44.500 55.58 21 21 20 11 20 6 21 22 22 21 21 21 21 21 21 21 21 21 21 21 21 21 21 21	10 21 15	i 25 10	46	4	36	10) 14	50	48,301	120,100	0 4,1	97,800	46,877	56,400	1,999,000	9,032,900	3 40	49,733	41,400	2,121,100	9,137,900	26	NA	98,271	166,116,375	510.499	23.9	3,689	1/3/2007 8:39	Ŵ	62
m involution	10 21 15	25 10	46	2	58	10	12	70	49,505	222,800	0 4,2	102,700	48,458	67,400	2,066,400	5 9,100,300	35	50,560	35,300	2,156,400	9,173,200	17	NA	102,501	166,218,876	510.814	29.8	3,719	1/4/2007 14:20	R	L
63 W 11110207 b c3 3765 18.3 511143 168 c23 552 82 9977 75.8 14 9235 500 2278700 453361 22 128 2002 1432000 53384 22000 4425700 55384 221 20 13 17 722 22 F 11112007 042 3316 25.0 5111301 168 c20 169 c3301 55202 148 c300 113 c300 113 c30 20 113 c30 26 21	14 1 15	29 14	30	11	1	14	25	26 24	49,523	224,300 343,700	0 4,2	1,500	48,474 49.604	48.200	2,067,100	9,101,000	9 40 9 38	50,579	300	2,157,200	9,245.200	55	NA 73.3	325	166,219,201	510.815 511.188	27.6	3,719	1/8/2007 8:10	T	
K 111/22007 9:08 3.790 25.01 511.729 166.516.617 93.044 62.030 54.680 24.9.10.2007 0.100 55.208 2.11 201 31 1 7 22.2 22.2 65 111/22007 91.01 3.819 3.80 512.026 166.613.260 14.643 64.2 65 9.780.00 23.800 55.800 2.228.100 61.00 52.202 14.800 4.615.800 54.113 38 29 14 7 15 42 35. 66 M 11232007 8.113 3913 72.4 513.603 167.126.416 378.813 867 68 9.44.800 2.68.800 61.618 54.9 9.58.600 34.91.800 512.700 65.777 33 31.800 512.700 65.775.707 74 9.33.800 2.59.800 61.000 54.99.91 45.755.800 2.69.900 45.775 30.90 15.80 41.118 42.27.700 85.200 2.69.800 61.618 51.99.900 65.765 61.61	13 1 9	22 13	23	7	1	13	20	21	51,884	425,700	0 4,4	82,000	50,394	33,700	2,149,000	9,182,900	1 28	53,381	48,300	2,276,700	9,293,500	41	75.6	82,977	166,423,552	511.443	18.3	3,765	1/10/07 8:03	Ŵ	63
in 1/22/2007 10:0 3:80 512 028 166.612.008 144.63 642 65 9.406,500 2286,100 56.100 222.22 14.800 4.815,800 54.113 30 512 028 166.612.200 14.643 642 65 9.406,500 2286,100 56.200 2286,100 56.200 55.200 54.113 50 44.11 512.445 166.412.800 166.442.83 66 T 1122/2007,800 3.841 21.9 512.445 36.200 168.800 54.925.800 54.800 55.863 135.100 4.400 22.65 14.463 36.21 11 19 14 46 34 66 T 1126/2007 7.65 3.937 23.8 14.058 14.051 11.057 39.42 30.00 11.8 42 33.00 11.46 34 63.83 14.40 33.00 11.40 43.83 42 9.39.00 2.400 64.138 33.00 11.40 33.00 11.40 30.00 11.40 30.00 </th <th>13 0 9 13 0 8</th> <th>22 13</th> <th>22</th> <th>7</th> <th>1</th> <th>13</th> <th>20</th> <th>21</th> <th>52,536 53,939</th> <th>481,300</th> <th>00 4,4 00 4 6</th> <th>55,600</th> <th>50,394</th> <th>0 71 000</th> <th>2,149,000</th> <th>9,182,900</th> <th>5 28</th> <th>54,685</th> <th>48 700</th> <th>2,332,300</th> <th>9,349,100</th> <th>36</th> <th>62.0 54.7</th> <th>93,064 82,001</th> <th>166,516,617</th> <th>511.729 511.981</th> <th>25.0</th> <th>3,790</th> <th>1/11/2007 9:08</th> <th>R</th> <th></th>	13 0 9 13 0 8	22 13	22	7	1	13	20	21	52,536 53,939	481,300	00 4,4 00 4 6	55,600	50,394	0 71 000	2,149,000	9,182,900	5 28	54,685	48 700	2,332,300	9,349,100	36	62.0 54.7	93,064 82,001	166,516,617	511.729 511.981	25.0	3,790	1/11/2007 9:08	R	
b5 T 11222007 8:00 3.841 21.9 512.445 166,749,003 136,343 103.8 49 9.478,000 2.461,200 77,000 57,707 47 9.323,600 2.880,000 55,800 515,000 475,000 55,690 56,690 56,690 56,690 56,790	14 7 21	2 35 14	42	15	7	14	5 29	36	54,113	615,800	00 4,6	14,800	52,202	6,100	2,226,100	3 9,260,000	0 53	56,030	8,700	2,389,700	9,406,500	65	64.2	14,643	166,613,260	512.026	3.80	3,819	1/22/2007 10:01	M	65
66 M 1/22/2007 511 3913 72.4 513.003 107.126.416 376.813 86.0 268.000 66.800 6.61.818 549.628.000 265.500 371.800 51.227.00 60.0055 351 381 17 1 19 42.2 38 M 2/252007 151 3.942 5.20 61.747 31.005 107.277.77.00 61.005 597.949 145.200 61.757 30.01 15 1 18 42 37 M 2/252007 151 3.942 5.20 61.747 31.00 61.348 67 977.700 61.00 65.188 69.90.200 27.000 61.005 57.000 57.00 61.048 33 30 15 31 15 40.33 30 15 31 16 43 63.93 41.41 42.38 41.44 42.38 41.44 42.33 40.44 42.33 40.44 42.33 41.44 42.33 41.44 42.33 41.44 42.33	14 12 20	34 14	46	11	19	14	25	44	55,696	750,900	00 4,7	3 135,100	53,693	63,600	2,289,700	9,323,600	7 47	57,707	71,500	2,461,200	9,478,000	49	103.8	136,343	166,749,603	512.445	21.9	3,841	1/23/2007 8:00	T	65
M 2/2/2007 15:15 3.942 5.20 514.072 167.281.307 6.833 NA 7 9.732.600 2.4600 85.876 52 9.593.600 2.859.700 3.200 60.024 7.600 5.2785.700 61.848 33 32 14 1 18 42 37 T 2/2/2007 15:16 3.955 1.2.8 514.414 167.380.316 109.009 141.18 67 9.779.200 6.100 2.657.600 6.1085 107.200 5.387.000 63.1164 33 33 15 3 15 3 15 3 15 3 15 3 15 3 15 3 15 33 30 15 33 30 15 33 30 15 33 30 15 33 33 14 4 20 46 33 30 15 33 34 14 4 20 46 33 33 34 14 4 20 46	16 4 22 15 3 18	38 16	42	19	1	17	30	35	60,055	267 900	00 5,1	371,800	58,500	205,000	2,494,700	9,528,600	B 54	61,618	166,800	2,628,000	9,644,800	68 57	86.7 103.7	376,813	167,126,416	513.603 514.058	23.8	3,913	1/29/2007 8:11	M	66
67 T 28/2007 E18 3.95 12.8 514.414 167.390.316 109.009 141.9 59 9.79.100 277.200 61.300 65.118 43 63.93.30 2.605.400 47.00 61.095 107.200 58.87.900 63.103 33 30 16 33 15 40 33 68 M 2/12/2007 613 3.961 4.90 514.530 167.428.662 32.215 108.6 70 9.815.000 27.98.200 77.900 65.08 55 9.655.400 2.62.500 13.900 61.472 31.800 5.419.700 63.837 38 34 14 42 20 46 38 69 T 2/12/207 91.33 366 167.423.128 105.65 59.79.200 63.001 63.737 38 34 14 42 20.46 38 69 T 2/12/207 91.31 3.961 4.30 67.697 41 9.791.100 2.681.55 9.655.400 2.62.968 151.500 <th< th=""><th>14 5 23</th><th>37 14</th><th>42</th><th>18</th><th>1</th><th>14</th><th>3 32</th><th>33</th><th>61,846</th><th>275,500</th><th>00 5,2</th><th>7,600</th><th>60,024</th><th>3,200</th><th>2,559,700</th><th>9,593,600</th><th>6 52</th><th>63,676</th><th>4,400</th><th>2,715,800</th><th>9,732,600</th><th>67</th><th>NA</th><th>6,833</th><th>167,281,307</th><th>514.079</th><th>5.20</th><th>3,942</th><th>2/5/2007 15:15</th><th>М</th><th></th></th<>	14 5 23	37 14	42	18	1	14	3 32	33	61,846	275,500	00 5,2	7,600	60,024	3,200	2,559,700	9,593,600	6 52	63,676	4,400	2,715,800	9,732,600	67	NA	6,833	167,281,307	514.079	5.20	3,942	2/5/2007 15:15	М	
W 2///2007 82e 3.995 1.00 514.431 107,398,847 5.532 92.2 69 9./97,100 2/80,300 65,169 66 59,61,150 2.200 61,147 3.800 5.81,197 68.357 38 16 3 20 46 38 68 T 2/12/2007 925 3.995 24.2 515.001 107,581,325 153,263 105.8 58 9.902,800 2.625,500 637,00 65,013 38 28 13 10 15 45 30 7 2/13/2007 925 3.995 24.2 515.001 107,593,3287 155,982 97.07 56 89.77 41 97.100 2.860,00 63,700 62,7667 41 9.1100 2.780,00 63,700 57.200 65.133 38 28 13 10 15.4 45 30 69 T 2.720207 61.11 41.11 23.1 62.00 63.000 78.81 40 92.490.00 2.800 77.122	15 7 18	33 15	40	15	3	15	3 30	33	63,103	382,700	00 5,3	5 107,200	61,095	45,700	2,605,400	9,639,300	8 43	65,118	61,500	2,777,300	9,794,100	59	141.9	109,009	167,390,316	514.414	12.8	3,955	2/6/2007 8:18	Т	67
68 T 21/32007 528 3865 242 515.001 167.651/328 163.253	10 8 22	38 16	46	20	3	16	36	39	63,537	367,900 419,700	0 5,3	5,200	61,147	2,200	2,607,600	9,641,500	9 56 R 54	65,608	3,000	2,780,300	9,797,100	69 70	92.2	5,532	167,395,847	514.431	1.00	3,956	2/1/2007 8:26	M	<u> </u>
W 2P1407 1128 4011 281 515.468 167.733.287 151.962 97.0 66 9.41.0001 2.924.200 38.200 68.563 56 779.900 2.748.000 60.800 64.332 999.000 667.213.001 697.419 45 281 121 141 482 28 69 T 2.226/2007 5:00 4.014 531 515.520 167.730.287 151.852 167.730.201 697.419 45 281 12 171 16 54 29 70 M 2.266/2007 5:00 4.014 531 515.220 167.730.287 133.280 74.900 2.981.000 144.200 67.792 393.200 6.14.4500 77.180 82.3 13 28 17 66 28 71 2.270207 8:11 4.111 2.39 517.15 10.33.600 33.3800 80.300 77.688 219.943.00 2.891.000 64.500 77.371 86 16 0 24 40 16 10.	13 15 17	5 <u>30</u> 13	40	15	10	13	3 28	38	65,313	571,200	00 5,5	151,500	62,966	63,700	2,685,200	9,719,100	7 41	67,667	87,800	2,886,000	9,902,800	58	105.6	153,263	167,581,325	515.001	24.2	3,985	2/13/2007 9:25	T	68
bbs 1 22/82/07 0.91 53.1 0.91 51.5 22 107,7 <th>13 20 15</th> <th>28 13</th> <th>48</th> <th>14</th> <th>12</th> <th>14</th> <th>28</th> <th>40</th> <th>66,474</th> <th>670,200</th> <th>5,6</th> <th>99,000</th> <th>64,392</th> <th>60,800</th> <th>2,746,000</th> <th>9,779,900</th> <th>3 36</th> <th>68,563</th> <th>38,200</th> <th>2,924,200</th> <th>9,941,000</th> <th>56</th> <th>97.0</th> <th>151,962</th> <th>167,733,287</th> <th>515.468</th> <th>26.1</th> <th>4,011</th> <th>2/14/07 11:28</th> <th>W</th> <th></th>	13 20 15	28 13	48	14	12	14	28	40	66,474	670,200	5,6	99,000	64,392	60,800	2,746,000	9,779,900	3 36	68,563	38,200	2,924,200	9,941,000	56	97.0	151,962	167,733,287	515.468	26.1	4,011	2/14/07 11:28	W	
70 T 22272007811 4,111 23.9 517.091 168,261,411 119,422 83.3 54 10,336,600 3313,800 80,300 77,808 521 9,61,000 73,700 66,669 117,300 6,241,800 73,717 78 27 15 61 88 18 M 3/82007 9:13 4,113 1.90 577,116 168,261,411 119,422 83.3 54 10,336,600 3,313,800 50,000 77,834 55 9,964,300 2,300,400 2,41,800 73,777 36 38 16 0 20 44 40 71 3/82,007 9:10 4,184 47.02 168,764,437 155,164 10,7.3 59 10,424,900 3,401,008 241,002,800 2,202,800 6,4500 70,006 6,4500 71,007 7,2941 27,5706 6,78,700 78,297 30 28 14 2 14 26 32 30 14 14 14 38 30 30 <	12 25 17	29 12	54	16	17	12	28	45	67,190 71,800	124,500	0 5,7	393 200	64,411	800	2,746,800	9,780,700	/ 41 5 ⊿/	69,977	249.000	2,984,500	10,001,300	62	101.1	322,146	167,750,208	515.520 516 724	53.1	4,014	2/20/2007 0:00	M	69
M 3/35/2007 9:13 4,113 1.90 517.115 188.269.221 7,810 68.3 71 10.338,400 3.319,600 58.00 77,834 55 9,964,300 2,904,000 2,600 66,716 8.200 6.250,000 73.271 36 36 16 0 20 44 40 T 3/36/2007 9:20 4,137 24.1 57.592 168,424.437 155:16 10.73.3 59 10,429.400 348,000 2,694,900 64,500 70.228 153,000 66,700 78.297 30 30 14 0 168 34 7 3/36/2007 9:10 4,104 42.10 145,000 3,86,000 66,000 70,000 78.297 30 28 14 2 14 26 32 7 3/32/2007 14.04 42.14 28.875 10.837.4669 170.835 95.5 52 10.864,000 366,000 66,000 76,207 168.00 86,200 36 29.41 27.500 80.20<	11 70 7	18 11	88	15	51	12	3 27	78	73,175	241,800	0 6,2	117,300	68,659	37,000	2,928,000	1 9,961,900	8 21	77,698	80,300	3,313,800	10,330,600	54	83.3	119,422	168,261,411	517.091	23.9	4,111	2/27/2007 8:11	T	70
1 3/8/2007 9:20 4.137 24.1 517.592 188.424.437 155.216 107.3 59 10.424.900 3.408.100 289.900 64.500 70.228 153.000 6.403.00 75.064 30 30 14 0 16 38 34 R 3/8/2007 9:10 14.184 47.0 518.450 188.738 99.0 55 58.900 58.900 29.99.900 64.150 157.00 72.291 275.700 83.920 71.900 72.911 275.700 83.920 73.927 30 28 14 2 14 26 32 23.92 30 28 14 2 14 26 32 23.92 30 26 11 4 15 38 30 7 M 31/122007 8.32 4.214 0.20 518.860 10.682.200 3.664.600 90.085.941 49 10.217.100 3.183.200 700 74.633 16.800 88.4700 83.90 83.90 83.90 <	16 4 24	40 16	44	20	0	16	36	36	73,271	250,000	00 6,2	8,200	68,716	2,400	2,930,400	5 9,964,300	4 55	77,834	5,800	3,319,600	10,336,400	71	68.5	7,810	168,269,221	517.115	1.90	4,113	3/5/2007 9:13	М	
N 3/12/2017 8.30 4.244 248 518.375 100.034.004 2/19.183 99.07 100.094.000 60.000 60.000 60.000 7/2 101.171.000 1/12.007 1/2.017 1/12.007 3/2 3	14 4 20	34 14	38	16	0	14	30	30	75,064	403,000	0 6,4	153,000	70,228	64,500	2,994,900	2 10,028,800	9 42	79,909	88,500	3,408,100	10,424,900	59	107.3	155,216	168,424,437	517.592	24.1	4,137	3/6/2007 9:20	T P	71
M 3/12/2007 8-32 4.214 0.20 518.980 168.876,092 1.627 135.6 60 10,662,200 3.665,400 900 85.941 49 10,217,100 3,183,200 700 74,643 1.600 6.846,600 80,288 36 29 13 7 16 43 34 T 3/13/2007 9:50 4.239 25.4 519.441 199,026,101 150.009 98.4 50 10,765,000 37.46700 87.848 451,028,700 3249,800 66.600 76,204 147.900 6.996,500 82.2022 40 28 13 12 15 46 30 T 3/19/2007 8:30 4,264 24.4 519,854 169,160,492 134,390 91.8 54 10,834,500 381,700 87,848 45 10,243,700 3249,800 66.600 76,204 147,907 83,584 46 29 14 17 15 51 64 30 T 3/20/200718 24,244 14,90	12 8 18	30 12	20	14	4	11	26	30	80,270	847,000	0 6,8	168,300	74,627	71,900	3,182,500	10,144,500	40	85,920	96,400	3,664,500	10,681,300	52	95.5	170,835	168,874,465	518.975	29.8	4,214	3/9/2007 14:04	F	L
1 31132207 8:30 4.264 24.4 519.441 199.026.101 190.049 98.4 501 0.765.001 3.249.800 66.600 76.204 147.900 6.996.500 82.0222 401 28 13 12 15 46 30 73 T 319/2007 8:30 4.264 24.4 519.854 169.160.492 134.390 91.8 54 10.834.500 85.170 3.249.800 66.600 76.204 147.900 6.996.500 82.0222 401 28 13 12 15 46 30 73 T 319/2007 8:30 4.264 24.4 519.854 169.160.492 134.390 91.8 54 10.834.500 3.817.000 62.200 77.663 133.200 71.297.700 83.584 46 29 14 17 15 15 36 7 3/20/2078.12 42.82 19.0342.500 3.873.000 61.300 79.100 127.000 85.874 55 16 129 11 <th>13 9 21</th> <th>34 13</th> <th>43</th> <th>16</th> <th>7</th> <th>13</th> <th>6 29</th> <th>36</th> <th>80,288</th> <th>848,600</th> <th>6,8</th> <th>3 1,600</th> <th>74,643</th> <th>700</th> <th>3,183,200</th> <th>0 10,217,100</th> <th>1 49</th> <th>85,941</th> <th>900</th> <th>3,665,400</th> <th>10,682,200</th> <th>60</th> <th>135.6</th> <th>1,627</th> <th>168,876,092</th> <th>518.980</th> <th>0.20</th> <th>4,214</th> <th>3/12/2007 8:32</th> <th>М</th> <th>72</th>	13 9 21	34 13	43	16	7	13	6 29	36	80,288	848,600	6,8	3 1,600	74,643	700	3,183,200	0 10,217,100	1 49	85,941	900	3,665,400	10,682,200	60	135.6	1,627	168,876,092	518.980	0.20	4,214	3/12/2007 8:32	М	72
73 T 3/20/2017 812 4282 17.9 50:001 129:5001 129:501 100:001 100:001 001,000 001,001 001,000 00,001 001,000 00,0000 00,0000 00,000000	14 16 16	30 14	46 E1	15	12	13	28	40	62,022	120 700	0 6,9	133,200	76,204	62,500	3,249,800	10,283,700	45	87,848	81,300	3,746,700	10,763,500	50	98.4	150,009	169,026,101	519.441	25.4	4,239	3/13/2007 9:50	M	<u> </u>
	15 23 20	35 15	58	11	29	15	29	- 55	85,074	256,800	00 7,2	127,100	79,100	61,300	3,373,300	5 10,407,200	5 45	91,055	65,800	3,883,500	10,900,300	44	120.6	129,509	169,290,001	520.252	17.9	4,282	3/20/2007 8:12	T	73

Table A-1. U.S. EPA Arsenic Demonstration Project at Tehachapi, CA – Daily System Operation Log Sheet (Continued)

1 BV = 5.7 ft3 = 42.65 gal for each module, 1 BV = 11.4 ft3 = 85.3 gal for two modules

APPENDIX B

ANALYTICAL DATA

Sampling Da	ate		10/26/05	;)		11/0	1/05			11/0	8/05			11/1	5/05	
Sampling Loca	ation	IN	AC	тм	IN	AC	МА	МВ	IN	AC	МА	MB	IN	AC	МА	МВ
Parameter	Unit															
Bed Volume	BV	-	-	1.8	-	-	10.0	9.1	-	-	18.9	17.7	-	-	26.1	24.5
Alkalinity	mg/L ^(a)	176	185	185	185	176	180	180	189	198	189	176	330	189	176	180
Fluoride	mg/L	0.2	0.2	0.2	-	-	-	-	-	-	-	-	-	-	-	-
Sulfate	mg/L	46	46	46	-	-	-	-	-	-	-	-	-	-	-	-
Nitrate (as N)	mg/L	0.47	0.48	0.47	-	-	-	-	-	-	-	-	-	-	-	-
Total P	μ g/L ^(b)	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10
Silica (as SiO ₂)	mg/L	27.8	28.0	21.0	27.7	27.8	27.3	27.6	26.7	27.2	26.3	26.7	27.1	26.9	26.7	26.9
Turbidity	NTU	<0.1	0.1	0.1	<0.1	0.2	0.2	0.1	0.4	<0.1	<0.1	<0.1	0.1	0.2	1.1	0.2
рН	S.U.	7.5	7.6	7.5	7.5	7.4	7.5	7.5	7.6	7.6	7.7	7.6	7.5	7.5	7.5	7.5
Temperature	°C	18.2	17.2	17.9	20.3	20.6	25.6	25.7	18.3	18.8	18.7	18.7	19.1	19.5	19.7	19.6
DO	mg/L	NA ^(d)	NA ^(d)	NA ^(d)	1.8	1.7	2.1	1.9	-	-	-	-	-	-	-	-
ORP	mV	444	616	589	449	470	649	653	468	642	647	659	359	593	623	625
Total Chlorine	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Hardness	mg/L ^(a)	177	176	178	181	182	184	183	181	176	184	184	173	174	174	172
Ca Hardness	mg/L ^(a)	130	128	131	133	134	134	134	133	129	137	137	131	131	130	129
Mg Hardness	mg/L ^(a)	47.9	47.9	47.3	47.7	48.2	49.6	48.8	48.0	46.7	47.2	46.8	41.7	42.8	43.3	43.1
		14.0	12.7	0.4	12.7	12.6	0.3	0.7	12.8	12.5	0.3	0.8	13.7	13.9	0.8	1.3
AS (IUIAI)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
As (soluble)	µg/L	13.1	12.4	0.4	-	-	-	-	-	-	-	-	-	-	-	-
As (particulate)	µg/L	0.9	0.3	<0.1	-	-	-	-	-	-	-	-	-	-	-	-
As (III)	µg/L	2.0	0.6	0.6	-	-	-	-	-	-	-	-	-	-	-	-
As (V)	µg/L	11.1	11.8	<0.1	-	-	-	-	-	-	-	-	-	-	-	-
Fe (total)	µg/L	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25
Fe (soluble)	µg/L	<25	<25	<25	-	-	-	-	-	-	-	-	-	-	-	-
Mn (total)	µg/L	3.5	3.7	0.1	3.6	3.6	0.2	0.6	3.9	3.9	<0.1	<0.1	4.4	4.8	0.2	0.5
Mn (soluble)	µg/L	3.4	3.2	0.2	-	-	-	-	-	-	-	-	-	-	-	-
Zr (total)	µg/L	<0.1	<0.1	0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Zr (soluble)	µg/L	<0.1	<0.1	0.1	-	-	-	-	-	-	-	-	-	-	-	-

Table B-1. Analytical Results from Long-Term Sampling At Tehachapi, CA

(a) As CaCO₃.
(b) As P.
(c) Water quality parameters measured on 10/25/05.
(d) Water quality parameter not measured.

IN – influent; MA = after module A; MB = after module B; TM = after combined module effluent.

NA = not available.

Sampling Da	ate		11/29/05			12/0	6/05			12/13/05	1		01/04/06	i
Sampling Loc	ation	IN	AC	тм	IN	AC	МА	МВ	IN	AC	тм	IN	AC	тм
Parameter	Unit										10.0			
Bed Volume	BV (2)	-	-	32.4	-	-	43.0	41.0	-	-	48.3	-	-	61.6
Alkalinity	mg/L ^(a)	176	189	189	185	189	189	185	185	180	185	189	194	189
Fluoride	mg/L	0.1	0.1	0.1	-	-	-	-	0.2	0.1	0.1	-	-	-
Sulfate	mg/L	39	41	44	-	-	-	-	40	40	40	-	-	-
Nitrate (as N)	mg/L	0.48	0.47	0.50	-	-	-	-	0.42	0.42	0.42	-	-	-
Total P	μg/L ^(b)	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10
Silica (as SiO ₂)	mg/L	27.2	27.2	27.5	28.1	27.9	27.5	27.6	29.5	28.9	28.7	27.5	27.7	27.3
Turbidity	NTU	0.3	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	1.6	1.1	0.2	0.3	0.1	0.2
рН	S.U.	7.6	7.6	7.3	7.7	7.6	7.6	7.6	7.7	7.6	7.6	7.7	7.8	7.7
Temperature	°C	15.7	16.0	14.8	17.0	17.5	17.7	17.5	17.3	17.7	18.0	18.5	19.1	19.3
DO	mg/L	2.7	2.2	2.3	2.6	1.8	1.8	1.8	2.2	2.2	2.3	2.2	1.7	2.5
ORP	mV	472	578	534	388	647	667	672	398	618	651	409	494	644
Total Chlorine	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Hardness	mg/L ^(a)	184	186	184	171	178	169	170	153	154	153	177	174	176
Ca Hardness	mg/L ^(a)	137	138	136	127	123	126	127	100	101	101	128	127	128
Mg Hardness	mg/L ^(a)	46.3	48.2	47.4	43.4	55.5	42.9	42.7	52.8	53.3	52.7	48.6	47.5	47.6
		11.4	11.5	3.3	11.8	11.5	7.4	6.8	12.1	12.5	9.1	13.4	13.3	12.2
AS (IOIAI)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-
As (soluble)	µg/L	11.8	12.1	3.2	-	-	-	-	11.1	13.0	9.9	13.9	13.9	13.1
As (particulate)	µg/L	<0.1	<0.1	0.2	-	-	-	-	1.0	<0.1	<0.1	<0.1	<0.1	<0.1
As (III)	µg/L	2.4	0.7	1.0	-	-	-	-	2.8	1.2	0.9	2.8	0.5	0.4
As (V)	µg/L	9.4	11.4	2.2	-	-	-	-	8.3	11.8	9.0	11.1	13.4	12.7
Fe (total)	µg/L	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25
Fe (soluble)	µg/L	<25	<25	<25	-	-	-	-	<25	<25	<25	<25	<25	<25
Mn (total)	µg/L	3.6	3.6	0.2	2.9	2.8	<0.1	<0.1	3.8	3.7	0.2	5.3	4.7	0.3
Mn (soluble)	µg/L	3.5	3.5	0.0	-	-	-	-	3.7	3.3	0.3	5.3	4.8	0.6
Zr (total)	µg/L	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Zr (soluble)	µg/L	-	-	-	-	-	-	-	<0.1	<0.1	<0.1	-	-	-
(-) 1-0-00	1													

Table B-1. Analytical Results from Long-Term Sampling At Tehachapi, CA (Continued)

(a) As CaCO₃.(b) As P.

Sampling Da	ate		01/1	0/06			05/02/06			05/1	0/06			05/1	6/06			05/24/06	;
Sampling Loca	ation				MP			-				ИР				MD			-
Parameter	Unit	IN	AC	MA	MB	IN	AC	IM	IN	AC	MA	MB	IN	AC	MA	MB	IN	AC	INI
Bed Volume	BV	-	-	71.2	67.7	-	-	5.5	-	-	2.8	18.5	-	-	11.5	25.1	-	-	24.8
Alkalinity	mg/L ^(a)	194	194	194	189	192	196	192	192	188	184	188	200	184	184	192	191	191	191
Fluoride	mg/L	-	-	-	-	0.2	0.2	0.2	-	-	-	-	-	-		-	0.2	0.2	0.2
Sulfate	mg/L	-	-	-	-	48	48	46	-	-	-	-	-	-		-	47	46	46
Nitrate (as N)	mg/L	-	-	-	-	0.7	0.7	0.6	-	-	-	-	-	-		-	0.6	0.6	0.6
Total P	μ g /L ^(b)	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10
Silica (as SiO ₂)	mg/L	27.9	28.2	28.3	27.9	28.3	28.6	26.9	28.9	28.5	23.8	28.6	29	28.6	28.3	30	27.2	27.9	27.3
Turbidity	NTU	0.2	0.1	0.3	0.2	0.3	0.2	0.2	0.3	0.2	0.4	0.1	0.3	0.2	0.3	0.2	0.4	0.6	0.4
рН	S.U.	7.7	7.8	7.7	7.7	7.7	7.7	7.7	7.5	7.5	7.4	7.5	7.6	7.5	7.5	7.5	7.6	7.5	7.5
Temperature	°C	18.2	19.0	14.0	19.0	14.9	20.1	20.4	30.8	20.4	20.3	19.4	22.3	20.6	20.9	21.0	20.0	20.0	23.2
DO	mg/L	2.2	1.8	2.0	2.3	2.1	3.0	2.5	-	-	-	-	-	-	-	-	2.8	2.1	2.4
ORP	mV	413	609	675	676	450	686	66.4	337	571	629	634	388	392	541	563	353	652	644
Total Chlorine	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Hardness	mg/L ^(a)	171	176	170	173	185	180	182	180	187	182	185	213	212	211	212	181	182	171
Ca Hardness	mg/L ^(a)	123	127	122	121	134	130	132	129	134	130	132	154	154	153	154	130	131	122
Mg Hardness	mg/L ^(a)	48.1	48.8	48.3	51.6	50.3	49.6	50.0	51.5	52.8	51.8	53.6	58.7	57.8	58.0	57.5	50.6	51.0	48.4
As (total)	ua/l	12.5	12.4	12.4	11.9	12.8	12.8	1.3	11.9	12.2	6.2	3.8	12.6	11.9	5.8	3.3	14.4	12.3	6.2
	P9/2	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
As (soluble)	µg/L	-	-	-	-	12.0	12.2	1.3	-	-	-	-	-	-	-	-	14.3	12.3	6.0
As (particulate)	µg/L	-	-	-	-	0.8	0.5	<0.1	-	-	-	-	-	-	-	-	<0.1	<0.1	0.2
As (III)	µg/L	-	-	-	-	0.6	0.2	0.2	-	-	-	-	-	-	-	-	0.5	0.1	0.2
As (V)	µg/L	-	-	-	-	11.4	12.0	1.1	-	-	-	-	-	-	-	-	13.8	12.1	5.8
Fe (total)	µg/L	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25
Fe (soluble)	µg/L	-	-	-	-	<25	<25	<25	-	-	-	-	-	-		-	<25	<25	<25
Mn (total)	µg/L	3.4	3.3	<0.1	<0.1	4.3	4.1	0.4	4.0	4.1	1.6	0.9	3.7	3.7	1.5	0.8	4.0	4.0	1.7
Mn (soluble)	µg/L	-	-	-	-	4.1	4.0	0.5	-	-	-	-	-	-		-	4.4	3.9	1.7
Zr (total)	µg/L	<0.1	<0.1	<0.1	<0.1	0.3	<0.1	0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	0.1	<0.1	<0.1	<0.1	<0.1
Zr (soluble)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-		-	-	-	-

Table B-1. Analytical Results from Long-Term Sampling At Tehachapi, CA (Continued)

(a) As CaCO₃.

(b) As P.

(c) Media replacement took place on February 20, 2006.

Sampling Da	ite		05/3	0/06			06/0	6/06			06/1	3/06			06/21/06	i		6/28/2	2006 ^(c)	
Sampling Loca	ation								MD				ИБ			-				
Parameter	Unit	IN	AC	WA	INIB	IN	AC	MA	MB	IN	AC	MA	INIB	IN	AC	IWI	IN	AC	MA	INIR
Bed Volume	BV	-	-	22.1	33.2	-	-	28.9	39.1	-	-	33.9	44.4	-	-	42.3	-	-	43.3	52.6
Alkalinity	mg/L ^(a)	192	192	200	188	190	194	198	194	200	200	200	204	190	186	190	192	200	196	192
Fluoride	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	0.2	0.2	0.2	-	-	-	-
Sulfate	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	47	56	57	-	-	-	-
Nitrate (as N)	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	0.7	0.7	0.7	-	-	-	-
Total P	μ g /L ^(b)	10.2	<10	<10	<10	<10	<10	<10	<10	10.6	11.3	<10	<10	15.7	<10	<10	<10	<10	<10	<10
Silica (as SiO ₂)	mg/L	27.2	26.9	25.8	27.1	29.0	29.0	28.5	28.9	29.8	30.1	29.9	30.1	27.2	27.7	27.7	30	29.5	29.3	29.3
Turbidity	NTU	0.5	0.2	0.4	0.4	0.3	0.5	0.7	0.5	0.4	0.6	0.5	0.4	0.3	0.4	0.5	0.3	0.3	0.3	2
pН	S.U.	7.5	7.5	7.5	7.5	7.6	7.6	7.5	7.5	7.6	7.6	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.5
Temperature	°C	20.9	20.3	20.3	20.3	25.7	25.9	26.0	26.1	18.8	19.1	19.2	19.1	22.3	21.8	21.6	26.6	26.4	26.3	26.2
DO	mg/L	2.8	2.6	2.2	2.4	2.3	2.1	2.1	2.1	2.4	2.2	2.5	2.5	2.5	2.1	2.3	3.2	2.3	2.9	2.8
ORP	mV	257	280	285	293	273	454	647	668	332	371	390	409	388	667	676	376	638	659	665
Total Chlorine	mg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
Total Hardness	mg/L ^(a)	158	156	163	166	170	171	178	174	186	190	192	182	220	200	209	188	184	179	180
Ca Hardness	mg/L ^(a)	117	116	122	125	120	122	125	122	137	140	141	133	161	143	150	133	129	126	128
Mg Hardness	mg/L ^(a)	41.0	39.8	40.7	40.9	49.4	49.1	53.1	51.4	49.2	50.5	50.9	48.8	59.7	57.0	58.5	54.6	54.3	52.9	52.2
As (total)		10.1	10.0	5.2	3.0	10.7	10.6	5.8	3.4	11.5	11.9	7.1	3.5	10.4	10.2	4.1	11.1	11.1	5.8	6.2
AS (IOIAI)	µg/∟	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
As (soluble)	µg/L	I	-	-	-	1	-	-	-	I	-	-	-	10.1	10.4	4.4	-	-	-	-
As (particulate)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	0.3	<0.1	<0.1	-	-	-	-
As (III)	µg/L	I	-	-	-	1	-	-	-	I	-	-	-	0.7	0.2	0.2	-	-	-	-
As (V)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	9.4	10.2	4.3	-	-	-	-
Fe (total)	µg/L	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25
Fe (soluble)	µg/L	I	-	-	-	1	-	-	-	I	-	-	-	<25	<25	<25	-	-	-	-
Mn (total)	µg/L	2.9	2.9	1.1	0.3	3.2	3.3	0.8	0.4	3.6	3.8	2.1	1.0	4.3	3.6	0.5	4.3	4.5	1.0	0.9
Mn (soluble)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	4.1	3.6	0.5	-	-	-	-
Zr (total)	µg/L	<0.1	0.7	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Zr (soluble)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table B-1. Analytical Results from Long-Term Sampling At Tehachapi, CA (Continued)

(a) As CaCO₃.

(b) As P.(c) Water quality parameters measured on 06/27/06.

Sampling Da	ite		07/0	5/06			07/1	1/06			07/18/06	;		07/26	6/06 ^(c)			08/02	2/06 ^(d)	
Sampling Loca	ation		40		МР		40		МР		40	TM				МР		40		МР
Parameter	Unit	IN	AC	MA	INIB	IN	AC	MA	INIB	IN	AC	IW	IN	AC	MA	INIB	IN	AC	WA	INIB
Bed Volume	BV	-	-	50.9	60.2	-	-	58.8	66.0	-	-	69.5	-	-	75.4	80.9	-	-	82.7	86.7
Alkalinity	mg/L ^(a)	193	193	197	188	193	197	197	193	188	205	171	188	196	192	192	189	189	185	189
Fluoride	mg/L	-	-	-	-	-	-	-	-	10.2	12.3	8.4	-	-	-	-	-	-	-	-
Sulfate	mg/L	-	-	-	-	-	-	-	-	48	46	49	-	-	-	-	-	-	-	-
Nitrate (as N)	mg/L	-	-	-	-	-	-	-	-	0.7	0.7	0.7	-	-	-	-	-	-	-	-
Total P	μg/L ^(b)	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10
Silica (as SiO ₂)	mg/L	27.3	27.6	28	28	27.8	26.9	27.2	27.6	27.3	27.3	30.5	27.8	28.2	28.5	28.5	31.7	32.3	32.8	32
Turbidity	NTU	0.2	0.6	0.4	0.3	4.6	2.6	0.5	1.8	0.5	0.6	0.4	0.1	0.7	0.4	0.2	0.1	0.2	0.1	0.2
рН	S.U.	7.4	7.5	7.5	7.5	7.6	7.5	7.5	7.5	7.6	7.6	7.5	7.6	7.6	7.6	7.6	7.8	7.8	7.8	7.8
Temperature	°C	21.7	20.8	20.5	20.4	22.9	21.4	21.4	21.3	21.2	21.0	21.7	22.1	21.6	21.6	21.6	20.3	20.2	20.2	20.2
DO	mg/L	2.8	2.0	2.2	4.3	3.1	2.3	2.3	2.2	2.0	2.0	1.7	2.2	2.0	2.0	1.7	2.5	1.9	2.3	2.1
ORP	mV	275	551	647	661	350	564	647	656	338	632	666	265	645	660	665	310	563	638	661
Total Chlorine	mg/L	-	-	-	1.27	-	-	-	1.3	-	-	1.6	-	-	-	1.3	-	-	-	1.4
Total Hardness	mg/L ^(a)	181	186	185	183	181	187	191	183	169	165	198	186	186	187	186	181	183	185	181
Ca Hardness	mg/L ^(a)	132	135	134	133	135	138	141	135	121	118	145	136	135	136	135	136	137	137	133
Mg Hardness	mg/L ^(a)	49.7	50.6	50.7	50.1	46.9	49.7	50.6	48.4	47.2	46.7	53.3	50.2	50.9	50.8	51.1	45.6	46.0	47.6	47.5
As (total)	ua/l	10.0	10.4	6.7	5.3	10.4	10.3	6.1	6.5	10.5	10.6	6.8	11.1	10.8	7.0	9.4	11.8	11.7	7.3	10.7
	µ9/⊏	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
As (soluble)	µg/L	-	-	-	-	-	-	-	-	11.0	11.0	7.0	-	-	-	-	-	-	-	-
As (particulate)	µg/L	-	-	-	-	-	-	-	-	<0.1	<0.1	<0.1	-	-	-	-	-	-	-	-
As (III)	µg/L	-	-	-	-	-	-	-	-	0.9	0.3	0.3	-	-	-	-	-	-	-	-
As (V)	µg/L	-	-	-	-	-	-	-	-	10.0	10.6	6.7	-	-	-	-	-	-	-	-
Fe (total)	µg/L	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25
Fe (soluble)	µg/L	-	-	-	-	-	-	-	-	<25	<25	<25	-	-	-	-	-	-	-	-
Mn (total)	µg/L	4.2	3.7	1.5	0.6	4.1	4.2	1.0	0.3	3.6	3.5	0.5	3.7	3.5	0.2	0.2	4.1	3.8	0.3	0.1
Mn (soluble)	µg/L	-	-	-	-	-	-	-	-	3.8	2.7	0.6	-	-	-	-	-	-	-	-
Zr (total)	µg/L	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Zr (soluble)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table B-1. Analytical Results from Long-Term Sampling At Tehachapi, CA (Continued)

(a) As CaCO₃.

(b) As P.

(c) Water quality parameters measured on 07/25/06.
(d) Water quality parameters measured on 08/01/06.

IN - influent; MA = after module A; MB = after module B; TM = after combined module effluent.

NA = not available.

Sampling Da	ate		08/0	8/06			08/15/06	;		08/22/06	;		08/2	9/06			09/0	5/06	
Sampling Loca	ation	INI	AC	МА	MR	INI	AC	тм	INI	AC	тм	INI	AC	МА	MB	INI	AC	МА	MR
Parameter	Unit					IIN		1 141			1 141	IIN							
Bed Volume	BV	-	-	91.5	94.1	-	-	98.4	-	-	4.4	-	-	11.7	12.2	-	-	20.0	19.0
Alkalinity	mg/L ^(a)	193	189	189	189	198	190	194	209	207	207	209	203	209	201	199	208	208	202
Fluoride	mg/L	-	-	-	-	0.7	2.6	0.6	0.9	0.6	0.6	-	-	-	-	-	-	-	-
Sulfate	mg/L	-	-	-	-	49	51	49	46	46	46	-	-	-	-	-	-	-	-
Nitrate (as N)	mg/L	-	-	-	-	0.6	0.8	0.6	0.7	0.7	0.7	-	-	-	-	-	-	-	-
Total P	μg/L ^(b)	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10
Silica (as SiO ₂)	mg/L	27.9	27.7	28.1	28.3	28.7	28.6	27.8	27.1	27.3	24.4	26.7	26.8	25.8	25.6	26.4	26	26.3	26
Turbidity	NTU	0.2	0.6	1.1	0.3	0.1	0.1	0.2	0.3	0.3	0.3	<0.1	0.2	0.1	0.1	0.1	0.1	0.2	0.1
рН	S.U.	7.5	7.5	7.5	7.5	7.5	7.5	7.5	7.6	7.6	7.5	7.6	7.5	7.5	7.5	7.5	7.6	7.6	7.5
Temperature	°C	20.5	20.5	20.1	20.5	20.9	21.0	21.5	21.7	21.8	21.2	20.8	20.9	20.9	20.7	22.6	22.2	22.0	21.9
DO	mg/L	2.1	1.8	2.0	1.9	2.0	2.2	2.5	1.9	2.1	2.2	2.8	2.0	2.0	2.0	2.1	2.1	2.1	2.1
ORP	mV	296	634	651	663	356	623	660	507	664	484	323	614	613	655	304	623	652	659
Total Chlorine	mg/L	-	-	-	1.5	-	-	1.5	-	-	1.3	-	-	-	1.5	-	-	-	1.4
Total Hardness	mg/L ^(a)	186	182	185	188	187	186	190	193	202	201	207	209	206	206	174	174	173	178
Ca Hardness	mg/L ^(a)	137	133	136	137	139	137	139	144	153	150	157	157	155	154	124	124	123	127
Mg Hardness	mg/L ^(a)	49.3	48.8	49.3	51.1	48.4	48.9	50.9	48.4	49.6	50.6	50.5	51.5	50.2	51.7	50.3	50.3	49.8	50.9
As (total)	ug/l	12.4	12.2	9.3	12.2	12.7	12.3	10.5	12.6	12.8	4.1	12.1	11.9	7.3	2.7	11.0	10.8	7.1	2.5
AS (IOIAI)	µg/∟	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-
As (soluble)	µg/L	-	-	-	-	12.4	12.8	10.5	12.3	12.0	3.9	-	-	-	-	-	-	-	-
As (particulate)	µg/L	-	-	-	-	0.4	<0.1	<0.1	0.4	0.8	0.1	-	-	-	-	-	-	-	-
As (III)	µg/L	-	-	-	-	1.6	0.5	0.4	1.8	0.6	0.6	-	-	-	-	-	-	-	-
As (V)	µg/L	-	-	-	-	10.8	12.3	10.1	10.4	11.4	3.4	-	-	-	-	-	-	-	-
Fe (total)	µg/L	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25
Fe (soluble)	µg/L	-	-	-	-	<25	<25	<25	<25	<25	<25	-	-	-	-	-	-	-	-
Mn (total)	µg/L	4.1	3.7	0.2	0.2	4.0	3.9	0.4	4.1	4.8	0.3	4.0	3.8	0.9	0.3	4.1	3.7	0.3	0.1
Mn (soluble)	µg/L	-	-	-	-	4.2	3.5	0.4	4.3	3.8	0.3	-	-	-	-	-	-	-	-
Zr (total)	µg/L	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Zr (soluble)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table B-1. Analytical Results from Long-Term Sampling At Tehachapi, CA (Continued)

(a) As CaCO₃.
(b) As P.
Sampling D	ate		09/1	2/06			09/20/0	6		09/2	6/06			10/0	4/06	
Sampling Loc Parameter	ation Unit	IN	AC	МА	MB	IN	AC	тм	IN	AC	МА	МВ	IN	AC	МА	MB
Bed Volume	BV	-	-	21.8	20.7	-	-	26.7	-	-	30.1	28.6	-	-	32.8	31
Alkalinity	mg/L ^(a)	190	192	190	190	195	202	202	198	198	205	203	208	203	205	203
Fluoride	mg/L	-	-	-	-	0.3	0.1	<0.1	-	-	-	-	-	-	-	-
Sulfate	mg/L	-	-	-	-	52	52	51	-	-	-	-	-	-	-	-
Nitrate (as N)	mg/L	-	-	-	-	0.7	0.7	<0.05	-	-	-	-	-	-	-	-
Total P	μg/L ^(b)	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	<10	11.1	11.4	<10	<10
Silica (as SiO ₂)	mg/L	27.1	27.1	26.1	26	28.6	29.2	28.3	27.6	27.6	26.9	27.5	27.6	27.6	26.7	27.8
Turbidity	NTU	0.3	0.1	0.2	0.1	6.2	0.3	0.5	0.1	0.1	0.2	0.1	0.2	0.2	0.2	0.1
рН	S.U.	7.5	7.5	7.5	7.5	7.5	7.6	7.5	7.5	7.6	7.5	7.6	7.7	7.8	7.8	7.8
Temperature	°C	20.5	20.4	20.4	20.3	20.0	20.0	20.3	21.0	20.7	20.5	20.6	16.5	17.1	17.4	17.4
DO	mg/L	2.1	1.5	2.0	1.8	1.5	1.8	1.5	2.5	2.1	2.2	2.0	3.7	2.6	2.6	2.7
ORP	mV	356	631	655	674	261	600.7	675	344	594	644	658	316	598	664	671
Total Chlorine	mg/L	-	-	-	1.3	-	-	1.3	-	-	-	1.4	-	-	-	1.3
Total Hardness	mg/L ^(a)	192	192	190	186	205	205	215	187	188	183	185	188	190	187	186
Ca Hardness	mg/L ^(a)	145	145	144	142	151	152	160	134	134	130	132	134	135	134	132
Mg Hardness	mg/L ^(a)	47.0	46.5	45.3	44.6	54.0	53.1	54.5	53.8	54.9	53.4	53.6	53.7	54.7	53.5	53.2
As (total)	µg/L	12.1 -	11.6 -	8.0 -	2.5 -	12.8 -	11.7 -	4.7 -	13.2 -	11.8 -	7.1 -	2.6 -	12.0 -	11.9 -	7.5 -	2.8 -
As (soluble)	µg/L	-	-	-	-	11.1	11.4	4.5	-	-	-	-	-	-	-	-
As (particulate)	µg/L	-	-	-	-	1.7	0.3	0.2	-	-	-	-	-	-	-	-
As (III)	µg/L	-	-	-	-	1.5	0.2	0.2	-	-	-	-	-	-	-	-
As (V)	µg/L	-	-	-	-	9.6	11.2	4.3	-	-	-	-	-	-	-	-
Fe (total)	µg/L	<25	<25	<25	<25	123	<25	<25	<25	<25	<25	<25	<25	<25	<25	<25
Fe (soluble)	µg/L	-	-	-	-	<25	<25	<25	-	-	-	-	-	-	-	-
Mn (total)	µg/L	4.7	4.8	0.5	0.1	4.1	3.6	0.6	3.9	3.8	0.6	0.2	3.7	3.7	0.5	0.3
Mn (soluble)	µg/L	-	-	-	-	3.9	3.5	0.5	-	-	-	-	-	-	-	-
Zr (total)	µg/L	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1	<0.1
Zr (soluble)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Table B-1. Analytical Results from Long-Term Sampling At Tehachapi, CA (Continued)

(a) As $CaCO_3$.

(b) As P.

Table B-1.	Analytical Results	from Long-Term	Sampling At 7	Fehachapi, CA ((Continued)
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Sampling Da	Sampling Date 10/10/06						10/1	9/06			10/2	5/06			10/3	1/06		11/07/06			
Sampling Loca	tion	IN	AC	МА	мв	IN	AC	МА	мв												
Parameter	Unit																				
Bed Volume	BV	-	-	34.3	32.4	-	-	35.3	33.8	-	-	38.5	36.4	-	-	39.9	37.6	-	-	43.7	40.9
рН	S.U.	7.9	8.0	7.9	7.9	7.7	7.7	7.7	7.7	7.6	7.6	7.6	7.6	7.6	7.6	7.6	7.5	7.7	7.7	7.7	7.7
Temperature	°C	18.0	18.3	18.7	18.6	18.5	18.9	19.0	19.0	16.5	17.1	17.3	17.5	15.5	16.0	16.4	16.9	19.9	20.1	20.2	20.2
DO	mg/L	2.2	1.8	2.1	1.8	2.3	2.4	2.5	2.5	3.4	2.9	2.9	3.0	2.9	3.0	3.2	2.8	1.4	1.4	1.5	1.7
ORP	mV	350	654	671	679	327	622	656	664	280	666	677	680	322	654	676	681	249	631	651	659
Total Chlorine	mg/L	-	-	-	1.4	-	-	-	1.3	-	-	-	1.5	-	-	-	1.4	-	-	-	1.5
An (total)	110/	12.3	12.0	7.7	2.7	12.9	13.3	9.7	3.4	12.7	12.0	6.7	3.1	11.8	11.0	6.8	2.7	12.6	13.0	7.3	3.0
AS (IUIAI)	µg/L	12.0	12.2	7.4	2.6	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Sampling Dat	e		11/1	5/06			11/2	9/06			12/0	5/06			12/1	2/06		12/27/06			
Sampling Locat	tion	IN	٨٢	МА	MB	IN	۸С	МА	MB	IN	AC	МА	MB	IN	٨٢	МА	MB	IN	٨٢	МА	MB
Parameter	Unit																				
Bed Volume	BV	-	-	44.8	42.1	-	-	44.8	42.3	-	-	45.0	42.4	-	-	45.1	42.4	-	-	46.5	43.6
рН	S.U.	7.7	7.7	7.7	7.6	7.7	7.7	7.7	7.7	7.6	7.7	7.7	7.7	7.7	7.7	7.7	7.7	7.7	7.7	7.6	7.6
Temperature	°C	17.8	18.0	18.3	18.4	14.5	15.2	15.8	16.3	17.5	17.8	18.1	18.2	16.0	16.5	16.9	16.9	14.5	15.4	15.8	15.8
DO	mg/L	3.1	2.7	2.8	2.5	2.4	2.1	2.3	2.4	3.2	2.9	2.9	3.0	4.5	2.8	3.1	3.1	4.3	4.2	3.6	3.5
ORP	mV	373	664	674	680	343	666	679	681	402	641	676	682	373	615	679	682	388	600	620	627
Total Chlorine	mg/L	-	-	-	1.35	-	-	-	1.5	-	-	-	1.4	-	-	-	1.3	-	-	-	1.2
		10.3	10.4	6.7	2.7	10.6	10.7	5.0	2.1	10.7	10.4	5.7	2.3	12.8	12.6	6.5	2.9	16.9	16.1	11.1	4.4
AS (IUIAI)	µg/L	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-

Sampling Dat	Sampling Date 01/03/07					01/1	0/07			01/2	3/07			01/3	0/07		02/06/07				
Sampling Locat	ion	INI	AC	МА	MR	IN	AC	МА	MR	IN	AC	MA	MR	INI	A.C.	MA	MR	IN	AC	МА	MR
Parameter	Unit	IIN	AC	IVIA			AC	IVIA			AC	WIA		IIN	AC	IVIA			AC	MA	
Bed Volume	BV	-	-	49.7	46.9	-	-	53.4	50.4	-	-	57.7	53.7	-	-	63.6	59.9	-	-	65.1	61.1
рН	S.U.	7.7	7.7	7.7	7.7	7.6	7.6	7.6	7.6	7.7	7.7	7.7	7.7	7.4	7.5	7.5	7.5	7.6	7.6	7.7	7.7
Temperature	°C	17.1	17.7	17.9	18.0	16.3	16.9	17.2	17.3	15.8	16.6	17.0	17.3	16.5	16.7	17.2	17.4	18.2	18.6	18.8	18.8
DO	mg/L	3.6	3.2	3.2	3.3	3.1	2.9	3.1	2.9	3.5	3.0	3.1	3.1	2.7	2.3	2.5	2.5	3.2	2.8	2.7	2.5
ORP	mV	313	505	536	551	320	638	654	657	301	490	536	553	290	629	647	654	310	516	540	551
Total Chlorine	mg/L	-	-	-	1.4	-	-	-	1.3	-	-	-	1.4	-	-	-	1.3	-	-	-	1.5
As (total)	µg/L	14.2	13.9	10.1	3.8	13.3	13.0	8.7	5.1	13.2	12.7	7.5	4.9	13.7	12.7	6.8	7.1	11.3	11.3	7.0	6.8
As (total)	µg/L	14.2 -	13.9 -	10.1	3.8 -	- 13.3	13.0 -	8.7 -	5.1 -	- 13.2	12.7	7.5 -	4.9 -	13.7	12.7 -	6.8 -	7.1 -	- 11.3	11.3 -	7.0 -	

IN – influent; MA = after module A; MB = after module B; TM = after combined module effluent. NA = not available.

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Table B-1.	Analytical Result	s from Long-Te	erm Sampling At	Tehachapi, CA	(Continued)
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Sampling Da	Sampling Date 02/13/07						02/2	0/07			02/2	7/07			03/0	6/07		03/13/07			
Sampling Loca	tion	IN	AC	МΔ	MB	IN	AC	МΔ	MB	IN	AC	МΔ	MB	IN	AC	МΔ	MB	IN	AC	МΔ	MB
Parameter	Unit		70				70		mb		70				70		me		70		mb
Bed Volume	BV	-	-	67.7	63.0	-	-	70.0	64.4	-	-	77.7	68.7	-	-	79.9	70.2	-	-	87.8	76.2
рН	S.U.	7.5	7.6	7.6	7.6	7.8	7.8	7.7	7.7	7.8	7.8	7.8	7.8	7.7	7.6	7.7	7.7	7.8	7.7	7.8	7.7
Temperature	°C	15.1	16.0	16.4	16.9	17.9	18.2	18.4	18.4	15.0	16.0	16.1	16.5	19.9	19.9	19.8	19.8	19.8	19.8	19.9	19.8
DO	mg/L	3.9	2.8	2.9	2.8	2.7	2.2	2.5	2.4	2.8	2.8	3.0	3.1	2.4	2.4	2.5	2.7	2.6	2.5	2.7	2.6
ORP	mV	263	288	295	308	285	337	366	371	285	330	347	354	235	325	338	340	284	294	313	318
Total Chlorine	mg/L	-	-	-	1.4	-	-	-	1.6	-	-	-	1.6	-	-	-	1.3	-	-	-	1.5
As (total)	μg/L	10.5	10.7	6.8	6.8	13.3	13.6	8.5	8.6	11.9	11.5 -	7.1	8.9	9.8	10.4	6.2	8.1	11.6	11.5	7.4	10.2

Sampling Date	9	03/20/07								
Sampling Locat	ion	IN	۸C	МΔ	MB					
Parameter	Unit		Z							
Bed Volume	BV	-	-	91.1	79.1					
рН	S.U.	7.5	7.5	7.5	7.5					
Temperature	°C	17.5	17.9	18.4	18.4					
DO	mg/L	3.4	2.7	3.1	3.2					
ORP	mV	219	332	335	331					
Total Chlorine	mg/L	-	-	-	1.5					
As (total)	ug/l	12.8	12.8	9.1	11.3					
AS (IUIAI)	µy/∟	-	-	-	-					

IN – influent; MA = after module A; MB = after module B; TM = after combined module effluent. NA = not available.